

Continuous cellular automata on irregular tessellations: mimicking steady-state heat flow

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Abstract—Leaving a few exceptions aside, cellular automata (CA) and the intimately related coupled-map lattices (CML), commonly known as continuous cellular automata (CCA), as well as models that are based upon one of these paradigms, employ a regular tessellation of an Euclidean space in spite of the various drawbacks this kind of tessellation entails, such as its inability to cover surfaces with an intricate geometry, or the anisotropy it causes in the simulation results. Recently, a CCA-based model describing steady-state heat flow has been proposed as an alternative to Laplace’s equation that is, among other things, commonly used to describe this process, yet, also this model suffers from the aforementioned drawbacks since it is based on the classical CCA paradigm. To overcome these problems, we first conceive CCA on irregular tessellations of an Euclidean space after which we show how the presented approach allows for a straightforward simulation of steady-state heat flow on surfaces with an intricate geometry, and, as such, constitutes a full-fledged alternative for the commonly used and easy-to-implement finite difference method, and the more intricate finite element method.

Index Terms—cellular automata; coupled-map lattice; irregular tessellations; heat flow

I. INTRODUCTION

Ever since the publication of Conway’s ‘Game of Life’ [1], cellular automata (CA), originally conceived by von Neumann in the early 1950s [2], and the closely related coupled-map lattices (CML) [3], also known as continuous cellular automata (CCA), have aroused numerous researchers’ interest, which comes forward by the growing number of publications on these topics. In fundamental sciences, much attention has been paid to the dynamical properties of (C)CA [4], [5], [3], [6], whereas many sound (C)CA-based models have been developed in various scientific disciplines, such as epidemiology [7], [8], fire science [9], [10], [11], geography [12], (micro)biology [13], [14], [15], medical science [16], [17], and transportation [18], [19]. A comprehensive review of the (C)CA-based models that have been developed recently in geomorphology can be found in [20].

Nonetheless a few recent studies have highlighted CA on other regular tessellations of the Euclidean plane [11], [21], [22], most of the above-mentioned studies use a square tessellation of the two-dimensional Euclidean space owing to its implementational simplicity and computational efficiency [23]. Although such a tessellation allows for a thorough study of a (C)CA’s dynamical properties, it suffers from several

drawbacks hampering the widespread use of (C)CA-based models as full-fledged alternatives of well-established models based upon partial differential equations. First, by limiting the discretization of the spatial domain to regular n -polytopes, the applicability of (C)CA-based models becomes restricted to spatial domains with a rather simple geometry that imposes even elementary boundary conditions [24], [25]. Second, a square tessellation artificially restricts the number of possible flow directions [22] in (C)CA-based mass flow models that are getting commonly used in hydrological and geological studies [26], [27], [28], [29]. Third, the use of a regular tessellation often results in artificially anisotropic patterns [30]. Fourth, the classical (C)CA paradigm hinders the use of spatio-temporal data in vector format, which is built up from a set of geometric primitives, as well as the integration of the (C)CA concept in existing, vector-based geographical information systems software. Fifth, it can be questioned whether (C)CA based upon a regular tessellation give rise to possible side-effects on the simulation results as a consequence of the regularity involved in its topology [31], [32], [33].

In order to overcome these barriers, (C)CA on irregular tessellations of \mathbb{R}^n can be conceived. Such tessellations can be obtained easily by relying on a rich variety of already well-established tessellation methods, such as the Delaunay tessellation, which are often built-in in mathematical software packages or are distributed free of charge as add-ons. By means of this paper, in which we formalize CCA on irregular tessellations and illustrate their usability, we hope to instigate the development of CCA-based models that benefit from weakening the topology constraint that is adhered to by the classical CCA paradigm.

In Section II we briefly present the mathematical formalization of CCA on irregular tessellations, while their graph representation is addressed in Section III. In the ultimate section of this paper we illustrate the usability and strengths of the irregular CCA paradigm for describing steady-state heat flow.

II. CONTINUOUS CELLULAR AUTOMATA ON IRREGULAR TESSELLATIONS

A. Definition

First, we state the definition of a CCA on an arbitrary tessellation of an n -dimensional Euclidean space, which con-

stitutes an extension to the classical CCA paradigm that predominantly relies on a square or cuboid tessellation of \mathbb{R}^2 or \mathbb{R}^3 , respectively.

Definition 2.1: A continuous cellular automaton (CCA) \mathcal{C} can be represented as a sextuple

$$\mathcal{C} = \langle \mathcal{T}, S, s, s_0, N, \Phi \rangle ,$$

where

- (i) \mathcal{T} is a countably infinite tessellation of an n -dimensional Euclidean space \mathbb{R}^n , consisting of non-overlapping cells c_i , $i \in \mathbb{N}$, that allows for a complete coverage of \mathbb{R}^n .
- (ii) S is an infinite set of states, often $S \subseteq \mathbb{R}$.
- (iii) The output function $s : \mathcal{T} \times \mathbb{N} \rightarrow S$ yields the state value of cell c_i at the t -th discrete time step, i.e. $s(c_i, t)$.
- (iv) The function $s_0 : \mathcal{T} \rightarrow S$ assigns to every cell c_j an initial state, i.e. $s(c_i, 0) = s_0(c_i)$.
- (v) The neighborhood function $N : \mathcal{T} \rightarrow \bigcup_{p=1}^{\infty} \mathcal{T}^p$ maps every cell c_i to a finite sequence $N(c_i) = (c_{i_j})_{j=1}^{|N(c_i)|}$, consisting of $|N(c_i)|$ distinct cells c_{i_k} .
- (vi) $\Phi = (\phi_i)_{i \in \mathbb{N}}$ is a family of functions

$$\phi_i : S^{|N(c_i)|} \rightarrow S ,$$

each ϕ_i governing the dynamics of cell c_i , i.e.

$$s(c_i, t+1) = \phi_i(\tilde{s}(N(c_i), t)) ,$$

$$\text{where } \tilde{s}(N(c_i), t) = (s(c_{i_j}, t))_{j=1}^{|N(c_i)|} .$$

Since the formulation of premises (i), (v) and (vi) in this definition differs from the original paradigm as proposed by Kaneko [3], we elaborate on them in the remainder of this section.

B. Tessellations of \mathbb{R}^2

Seen the fact that the CCA-based models presented in the subsequent sections describe phenomena occurring in the Euclidean plane, we restrict the discussion to tessellations of \mathbb{R}^2 . For that purpose, we consider a countably infinite, irregular tessellation \mathcal{T} of the Euclidean plane, which can be envisaged as a set $\mathcal{P}^2 = \{p_1^2, p_2^2, \dots, p_i^2, \dots\}$ of convex 2-polytopes, i.e. polygons, p_i^2 , which, on their turn, can be assembled from a set of line segments p_j^1 that can be denoted as

$$\mathcal{P}_i^1 = \left\{ p_{i_1}^1, p_{i_2}^1, \dots, p_{i_{l_i^1}}^1 \right\} ,$$

where l_i^1 indicates the number of line segments needed to construct p_i^2 . Sticking to this notation, the set of line segments needed to construct all p_i^2 in \mathcal{T} is then given by $\mathcal{S} = \bigcup_i \mathcal{P}_i^1$. Figure 1(b) visualizes this construction for a convex polygon p_i^2 belonging to a tessellation \mathcal{T} of \mathbb{R}^2 . Clearly, every line segment p_j^1 in \mathcal{P}_i^1 can be formed by connecting two points in \mathbb{R}^2 such that

$$\mathcal{P}_i^0 = \left\{ p_{i_1}^0, p_{i_2}^0, \dots, p_{i_{l_i^0}}^0 \right\} ,$$

constitutes the set of vertices p_j^0 from which p_i^2 can be assembled (Fig. 1(c)), whereas $\mathcal{E} = \bigcup_j \mathcal{P}_j^0$ is the set of endpoints necessary to construct all line segments in \mathcal{T} .

In case one is faced with an irregular tessellation of a 3- or higher-dimensional Euclidean space, the above-outlined line of reasoning can be extended by envisaging its tessellation as a set $\mathcal{P}^n = \{p_1^n, p_2^n, \dots, p_i^n, \dots\}$ of convex n -polytopes that are built up from $(n-1)$ -polytopes, which can be further decomposed in $(n-2), (n-3), \dots, 0$ -polytopes.

C. The neighborhood function N

In order to streamline the construction of the sequence $(c_{i_j})_{j=1}^{|N(c_i)|}$, we first introduce the intuitive concept of so-called m -dimensional contact.

Definition 2.2: Two n -polytopes $p_i^n, p_j^n \in \mathcal{T}$ have m -dimensional contact, with $m \leq n$, if they share at least one m -polytope.

Clearly, it follows that m -dimensional contact between n -polytopes implies $0, 1, \dots, (m-1)$ -dimensional contact. The former definition can now be used to unambiguously set up a subset $\mathcal{N}_i \subset \mathcal{T}$, further referred to as a topological neighborhood, containing those cells $c_j \in \mathcal{T}$ that are considered c_i 's neighbors.

Definition 2.3: The m -th order topological neighborhood \mathcal{N}_i^m of an n -polytope $p_i^n \in \mathcal{T}$, with $0 \leq m < n$, contains all n -polytopes $p_j^n \in \mathcal{T}$ that have m -dimensional contact with p_i^n , i.e. $\mathcal{N}_i^m = \{p_j^n \in \mathcal{T} \mid \mathcal{P}_i^m \cap \mathcal{P}_j^m \neq \emptyset\}$.

If tessellations of \mathbb{R}^2 are considered, Definition 2.3 allows the construction of either a 0-th or 1-st order topological neighborhood, which are better known as the Moore and von Neumann neighborhood, respectively. Both neighborhoods are illustrated in Fig. 2 for a convex polygon c_1 in an irregular tessellation of \mathbb{R}^2 . It should be clear that the geometric discrepancies existing between cells in \mathcal{T} , which can be traced back to differences between the position of the n -polytopes' centroids, and, the polygons' circumference and area are not taken into account for pinning down a cell's topological neighborhood. Obviously, these geometric characteristics could be used to exclude cells not fulfilling certain criteria from the topological neighborhoods, and, as such, give rise to a restricted topological neighborhood $\mathcal{N}_i^{m,R}$. For instance, if tessellations of \mathbb{R}^2 are at stake, a threshold can be imposed on the minimum proportion of c_i 's circumference that must be shared with c_j so that c_j is still considered c_i 's neighbor. Figure 2(c) shows the restricted topological neighborhood of a convex polygon c_1 enclosing those cells c_j belonging to \mathcal{N}_1^1 that make up at least 20% of c_1 's circumference. Unless stated otherwise, a Moore neighborhood is used throughout the remainder of this paper.

D. Transition function ϕ_i

According to Def. 2.1 every c_i in \mathcal{T} has its distinct transition function ϕ_i governing its dynamics. Yet, we can contemplate the family of CA for which $\phi_i = \Theta$ is the same for all $c_i \in \mathcal{T}$.

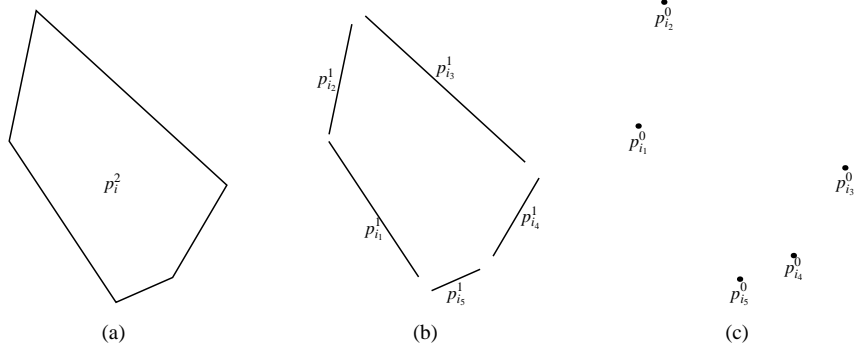


Fig. 1. Assembly of vertices $p_{i_j}^0$ in \mathbb{R}^2 leading to line segments $p_{i_k}^1$ that on their turn can be joined to form the polygon p_i^2 .

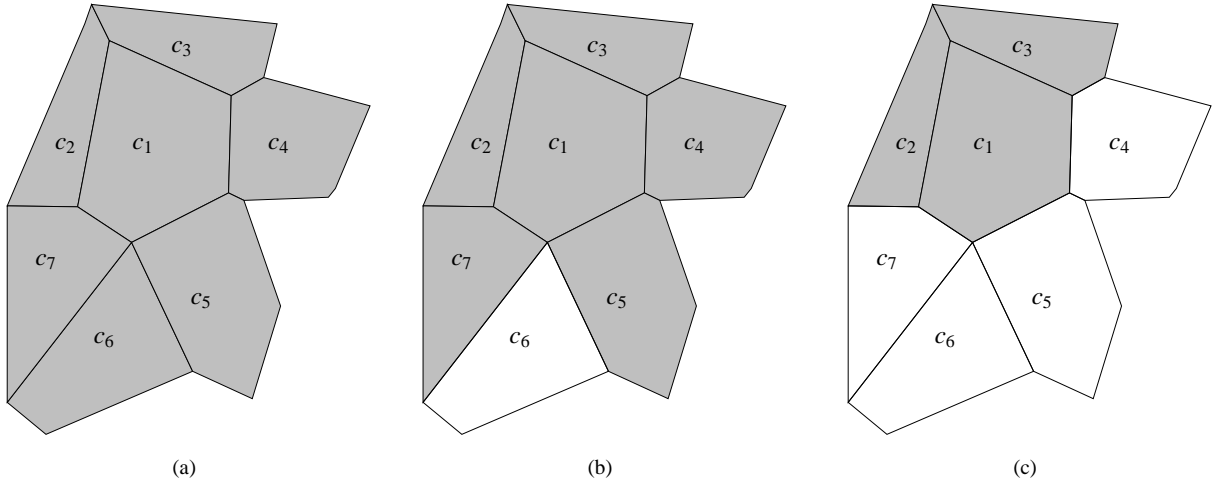


Fig. 2. Moore (a), von Neumann (b) and (c) restricted topological neighborhood of a convex polygon c_1 .

Definition 2.4: A homogeneous continuous cellular automaton (CCA) is a CCA fulfilling premises (i)-(v) of Definition 2.1 and for which there exists a $\Theta : \bigcup_{k \in \mathbb{N}} S^k \rightarrow S$ such that

$$s(c_i, t+1) = \Theta(\tilde{s}(N(c_i), t)).$$

Essentially, most works on CCA merely concern homogeneous CCA [34], [35].

III. GRAPH REPRESENTATION OF CCA ON IRREGULAR TESSELLATIONS

In order to simplify their implementation and to elucidate the irregular CCA paradigm, a graph representation of CCA on irregular tessellations of \mathbb{R}^n can be exploited. If a topological neighborhood is considered (Cfr. Def. 2.3), \mathcal{T} is mapped on an undirected graph $G(V, E)$, with vertex set $V = \mathcal{T}$ and E representing the edge set of G , assembled in accordance with Definition 2.3. Hence, an edge e_{ij} exists between two vertices c_i and c_j if $c_j \in N(c_i)$. On the other hand, if the geometric characteristics of c_i must be taken into account when constructing $N(c_i)$, a directed graph $G_d(V, E_d)$ should be employed, since $c_j \in \mathcal{N}_i^{m,R}$ does not necessarily imply that $c_j \in \mathcal{N}_i^{m,R}$.

Figure 3(a) shows a finite 2D tessellation of a compact subset of \mathbb{R}^2 consisting of 15 irregular polygons, while its

projection onto an undirected graph G is given in Fig. 3(b). Dashed edges only exist if a Moore neighborhood is at stake, since a von Neumann neighborhood discards polygons that have 0-dimensional contact. Hence, if the latter is at stake only the non-dashed edges are present.

IV. MODELING STEADY-STATE HEAT FLOW

A. A generalized CCA-based model for steady-state heat flow

As an exemplary diffusion process, we consider in this section the steady-state flow of heat through a two-dimensional rectangular surface $S \subset \mathbb{R}^2$ that is commonly addressed using Laplace's equation:

$$\nabla^2 T(x, y) = 0, \quad (1)$$

where $T(x, y)$ denotes the steady-state temperature expressed in degrees centigrade at every point (x, y) in S .

For setting up a CCA-based model describing steady-state heat flow, which is necessarily based upon discrete spatial entities (*i.e.* cells c_i), it can be reasoned that if such a cell is surrounded by a given number of neighboring cells, each maintained at constant temperature, it will reach a steady-state temperature after a sufficient amount of time that is completely determined by the temperature of its neighbors.

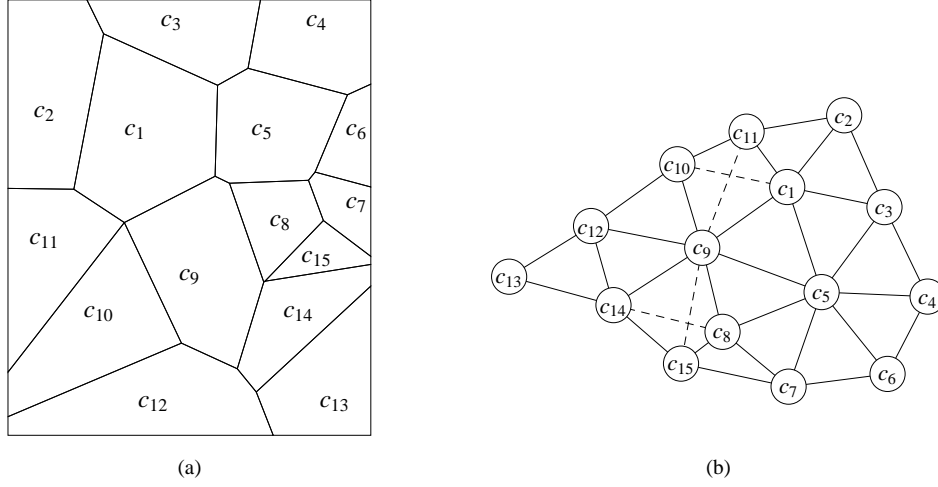


Fig. 3. Representation of a discrete irregular tessellation of a compact subset of \mathbb{R}^2 (a) and the graph G obtained after mapping this tessellation on G (b). Dashed vertices only exist when a Moore neighborhood is considered.

More specifically, this steady-state temperature will be the average value of the temperatures at which the neighboring cells are maintained. Hence, if we discard the difference in the length of the common line segment through which neighboring cells exchange heat, and which unavoidably exists between cells in an irregular tessellation of \mathbb{R}^2 , the steady-state temperature in the cells of \mathcal{T} can be obtained by iteratively evaluating

$$W(c_i, t+1) = \Theta(\tilde{s}(N(c_i), t)) = \frac{\sum_{c_j \in N(c_i)} W(c_j, t)}{|N(c_i)|}, \quad (2)$$

for all c_i , until $|W(c_i, t+1) - W(c_i, t)| \leq \phi, \forall c_i \in \mathcal{T}$, where ϕ is a given halting criterion and $W(c_i, t)$ denotes the temperature expressed in degrees centigrade in cell c_i at the t -th time step. In contrast with $T(x, y)$, $W(c_i, t)$ constitutes a discrete function since it yields a value for discrete cells and time steps only. Taking into account the discrepancies between the length of the exchange ‘surface’, Eq. (2) can be modified to:

$$W(c_i, t+1) = \Theta(\tilde{s}(N(c_i), t)) = \frac{1}{C_{ii}} \sum_{c_j \in N(c_i)} W(c_j, t) C_{ij}, \quad (3)$$

where C_{ij} denotes the length of the line segment that is shared by c_i and c_j . It should be clear that Eqs. (2) and (3) constitute the transition function of a homogeneous CCA $\mathcal{C} = \langle \mathcal{T}, S, s, s_0, N, \Theta \rangle$, with $\mathcal{T} = \{c_1, c_2, \dots\}$, $S = \mathbb{R}$, $s(c_i, t) = W(c_i, t)$, $s_0(c_i) = W(c_i, 0)$, $N(c_i) = \mathcal{N}_i^0$, and Θ being the right-hand-side of Eq. (2) or (3). Essentially, Eqs. (2) and Eq. (3) constitute an extension to the CCA proposed by Schiff [36] for describing heat flow on a square tessellation that suffers from several drawbacks as discussed in Section I.

B. Assessing the validity of the CCA-based model

In order to demonstrate the validity of Eq. (2), we consider the heat flow in a square plate, which is subject to the boundary conditions

$$\begin{aligned} T(0, y) &= 0, & 0 < y < s, \\ T(s, y) &= 0, & 0 < y < s, \\ T(x, 0) &= T_b, & 0 \leq x \leq s, \\ T(x, s) &= T_t, & 0 \leq x \leq s, \end{aligned}$$

where s is the side length of the plate. Since an analytical solution can be found for this boundary value problem a sound assessment of Eq. (2)’s validity becomes possible. The latter solution can be found straightforwardly by separation of variables, and can be simplified to

$$\begin{aligned} T(x, y) &= 4T_t \sum_{m=1}^{+\infty} \frac{\sinh(m^* y s^{-1}) \sin(m^* x s^{-1})}{m^* \sinh(m^*)} + \\ &4T_b \sum_{m=1}^{+\infty} \frac{\sinh(m^* (s-y) s^{-1}) \sin(m^* x s^{-1})}{m^* \sinh(m^*)} \end{aligned} \quad (4)$$

where $m^* = (2m-1)\pi$ was introduced for reasons of clarity. In the remainder of this subsection, we consider a steel plate with side length $s = 1$, $T_t = 50$ and $T_b = 50$. The simulations with the CCA-based model were performed using a regular tessellation consisting of 100×100 square cells and a value of 10^{-7} was selected for ϕ , while 200 terms of the series in Eq. (4) were taken into account. Figure 4, depicting the steady-state temperature distribution along three horizontal cross-sections obtained using the analytical solution (Eq. (4)) on the one hand, and the CCA-based model (Eq. (2)) on the other hand, and Fig. 5 visualizing the absolute difference between $W(c_i, t_\phi)$ and the corresponding $T(x_i^g, y_i^g)$, where t_ϕ is the number of time steps needed such that $|W(c_i, t+1) - W(c_i, t)| \leq \phi, \forall c_i \in \mathcal{T}$ and (x_i^g, y_i^g) represents c_i ’s center of gravity, clearly show the close agreement between the simulated temperature distributions obtained with both approaches. The good agreement between

TABLE I
AVERAGE ABSOLUTE DIFFERENCE μ_e BETWEEN $W(c_i, t_\phi)$, WHERE t_ϕ IS THE NUMBER OF TIME STEPS NEEDED SUCH THAT $|W(c_i, t+1) - W(c_i, t)| \leq \phi, \forall c_i \in \mathcal{T}$, AND THE CORRESPONDING $T(x_i^g, y_i^g)$, WHERE (x_i^g, y_i^g) REPRESENTS c_i 'S CENTER OF GRAVITY, TOGETHER WITH t_ϕ .

$ \mathcal{T} $ (-)	μ_e (°C)	t_ϕ (-)
25×25	0.90	1397
50×50	0.52	4904
100×100	0.28	17352
150×150	0.19	36308

both approaches is further confirmed by Table I that lists the average absolute difference μ_e between $W(c_i, t_\phi)$ and the corresponding $T(x_i^g, y_i^g)$ together with t_ϕ . As expected, it indicates that μ_e drops as we are working towards the continuum limit $|\mathcal{T}| \rightarrow \infty$. In order to verify the comparability between the results obtained using the CCA-based model on the one hand, and a finite difference approximation of Eq. (1) on the other hand, we implemented an implicit finite difference scheme for this equation, which was solved iteratively for 100×100 nodes located in the centers of gravity of the CCA's cells. As such, we assessed that the mean absolute difference between the simulated temperature of both approaches was only 0.01, whereas the maximum discrepancy was 3.4. This clearly indicates the comparability existing between both approaches, as such granting reliability to the approach we propose.

Figure 5 further shows that the regions in which the discrepancies between the simulation results obtained using the approaches at stake are the most pronounced, are located in the corners of the tessellated surface, whereas the smallest discrepancies can be found in the surface's center. These discrepancies can be attributed to the fact that $W(c_i, t+1)$ is calculated using the temperature values in cells that share an edge with c_i , as well as cells that merely share a vertex with c_i since a Moore neighborhood is employed. As such, neighboring cells that are not directly facing c_i have the same influence on the determination of $W(c_i, t+1)$ as the facing ones, which, physically speaking, would entail a flow of heat through c_i 's four corner points that is equally large as the heat flow through its sides. In order to work around this artifact that is inevitably related to the use of a square tessellation, either the steady-state temperature distribution can be computed using Eq. (3) or one can give up the square tessellation and resort to a more intricate meshing method yielding cells which state can be iteratively calculated by means of Eq. (3). Yet, the first workaround is not more than a stopgap since then it is assumed that cells merely sharing a vertex with c_i have no influence at all on $W(c_i, t+1)$, which is as doubtful as granting them equal importance as cells sharing an edge with c_i .

C. The CCA-based model's strengths exemplified

In the remainder of this section, we consider the flow of heat that originates from a tube (radius 0.4 cm) conducting

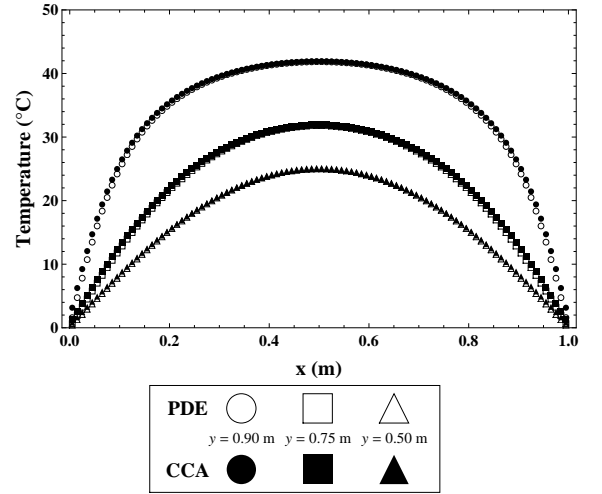


Fig. 4. Steady-state temperature distribution along three horizontal cross-sections obtained using the analytical solution (Eq. (4)) on the one hand, and the CCA-based model (Eq. (2)), on the other hand.

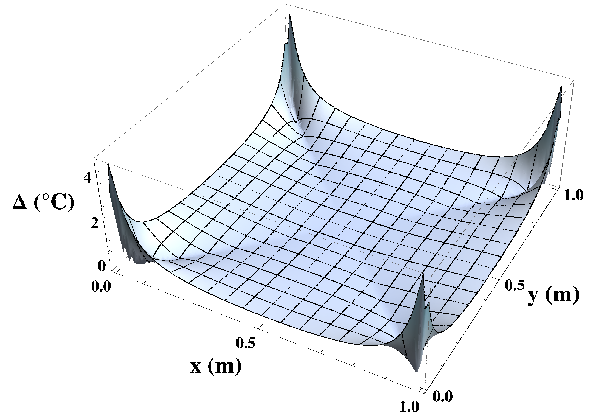


Fig. 5. Absolute difference, denoted Δ (°C), between $W(c_i, t_\phi)$ and the corresponding $T(x_i^g, y_i^g)$, where t_ϕ is the number of time steps needed such that $|W(c_i, t+1) - W(c_i, t)| \leq \phi, \forall c_i \in \mathcal{T}$ and (x_i^g, y_i^g) represents c_i 's center of gravity.

a fluid maintained at a temperature of 50°C. This tube is homogeneously wrapped up with a lagging material and the wrapped tube is contained in a box of which the sides are maintained at a temperature of 20°C. Seen the fact that the temperature of the fluid, as well as the sides of the box are maintained constant, it is to be expected that a steady-state temperature distribution will be reached inside the box after a sufficient amount of time. Obviously, the geometry of the surface that needs to be tessellated, together with the circular boundary condition obstructs the use of a regular tessellation, though, a Delaunay tessellation can be employed for discretizing. Figure 6 depicts a transversal cross-section through this construction and shows the Delaunay tessellation, consisting of 12,688 cells, that was used to mesh the space enclosed between the box' sides and the tube.

After implementing the boundary conditions as indicated

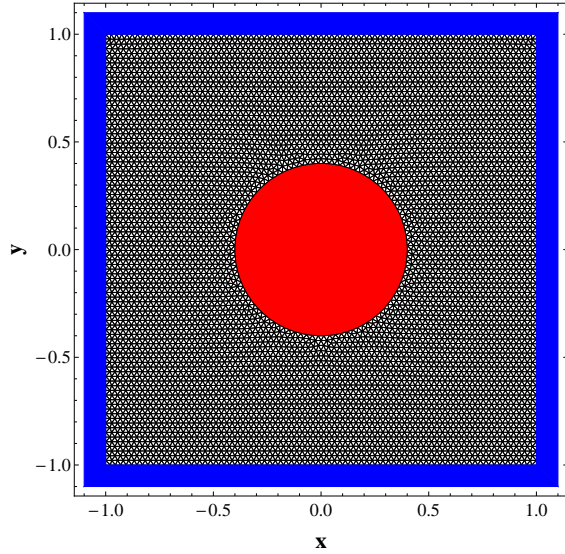


Fig. 6. Schematic overview of a transversal cross-section through a box containing a tube homogeneously wrapped up with lagging material. The sides of the box are maintained at 20°C, while a warm fluid (50°C) is flowing through the tube.

in Fig. 6, the steady-state temperature distribution in the lag-filled area was computed iteratively using Eq. (2) and is visualized in Fig. 7(a). In order to satisfy the halting criterion, 6,048 iterative evaluations of Eq. (2) were needed. Figure 7(b) depicts the temperature distribution along four cross-sections through the medium. For comprehensiveness, we should emphasize that the latter figure was obtained by taking the values of the cells of which the center of gravity was located the closest to the equidistant points along each of the four cross-sections.

D. Comparison with other numerical techniques

Nonetheless we leave a thorough comparison between the results obtained using the above presented CCA-based model on the one hand, and well-established numerical techniques that have been developed for approximating the solution of the Laplace equation if intricate boundary conditions and/or geometries are involved on the other hand, to future work, we briefly place the former methodology against both the finite difference method (FDM) and the finite element method (FEM). Typically, the former method discretizes a PDE based upon a square tessellation of \mathbb{R}^2 , which inevitably leads to the same difficulties as the ones facing when using the CCA-based model on such a tessellation. Besides, the central difference approximation of Eq. (1) collapses to Eq. (2) if the discretization size in both the x - and y -direction are the same. With regard to the FEM, it is clear that it coincides with the CCA-based approach in the sense that it relies on the same meshing methods that are used by FEM, but setting up a sound finite element approximation of the problem at hand is certainly not as straightforward as implementing Eq. (2) or (3). Unavoidably, these equations yield an approximation of Eq. (1), but likewise, one may not lose sight of the fact

that also FDM and FEM yield only an approximate solution of Eq. (1).

Unavoidably, a thorough comparison between the performance of the CCA-based models on the one hand and the FEM and FDM on the other hand will lead to the question whether either a continuous model or a discrete model is the most appropriate starting point for numerical modeling. To emphasize this dilemma, we may refer to Toffoli [37] who remarked already in 1984 that is questionable to stick to PDEs as a starting point for numerical modeling as soon as symbolic manipulations are no longer possible since (1) they represent a *stylized* form of the process(es) at stake, (2) we need to discretize them in order to find a numerical approximation, and (3) real-valued variables are rounded off. Perhaps, discrete models might offer a less roundabout way to model natural processes?

V. CONCLUSION

In this paper we established the mathematical constructs that are needed to make use of the irregular CCA paradigm to build models upon that can be of use in applied sciences, and we illustrated this paradigm's usability for a CCA-based model describing steady-state heat flow. Although we obtained the tessellation used throughout this paper by means of a well-established meshing method, it could be equally well deduced from a vector-based geographical information system that exploits irregular polygons as one of its three major data types, in addition to vertices and line segments, to encode spatial information.

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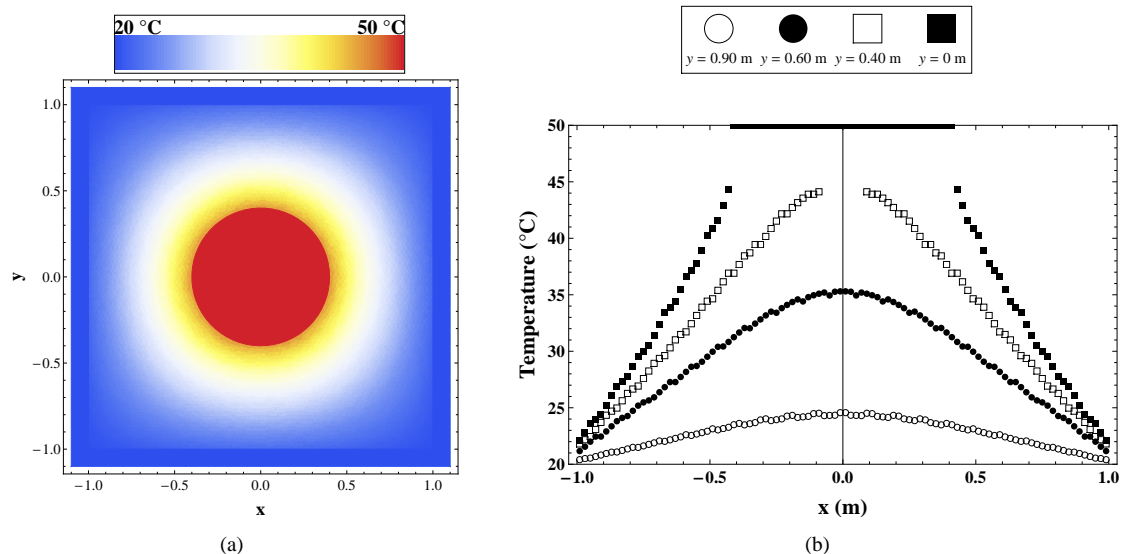


Fig. 7. Steady-state temperature distribution in the lag-filled area (a) and along four cross-sections through the medium (b).

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