

# A FLEXIBLE DECISION SUPPORT TOOL FOR MAINTENANCE FLOAT SYSTEMS - A SIMULATION APPROACH

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## ABSTRACT

This paper is concerned with the use of simulation as a decision support tool in maintenance systems, specifically in MFS (*Maintenance Float Systems*). For this purpose and due to its high complexity, in this paper the authors explore and present a way to develop a flexible MFS model, for any number of machines in the workstation, spare machines and maintenance crews, using *Arena* simulation language. Also in this paper, some of the most common performance measures are identified, calculated and analysed. Nevertheless this paper would concentrate on the two most important performance measures in maintenance systems: system availability and maintenance total cost. As far as these two indicators are concerned, it was then quite clear that they assumed different behaviour patterns, especially when using extreme values for periodic overhauls rates. In this respect, system availability proved to be a more sensitive parameter.

Keywords: Simulation, Discrete Event Simulation, Maintenance, Preventive Maintenance, Waiting Queue Theory, Float Systems.

## 1. INTRODUCTION

According to (Pegden et al., 1990), simulation can be understood as the process of construction of a real system representative model, as well as an experimental process aiming to a better understanding of their behavior and to assess the impact of alternative operations strategies. Thus, simulation may also be considered as a decision support tool that allows to predict and to analyze the performance of complex systems and processes as they are in many real systems. In addition, with the use of simulation we acquired a capacity to forecast and to achieve quickly the importance of taking some decisions about the system under analysis.

In some real systems like production areas, services such as transport companies, health service systems and factories, the main goal is to achieve high levels of competitiveness and operational availability. In this environment the need for equipment to work continuously is essential in order to maintain high levels of productivity. This is why MFS has an important role

on equipment breakdown and production stoppage has a high and direct impact on production process efficiency and, as a consequence, on their operational results. Therefore, maintenance control and equipment use optimization become not only an important aspect for the mentioned reasons, but also for personnel security matters and to prevent negative environmental impact. This maintenance control and optimization of equipment utilization can be achieved implementing preventive maintenance actions that increase equipment control and avoid unexpected stoppage. However, to overestimate these actions makes the maintenance costs too high for the required availability.

The integration of the maintenance management with materials and human resources is an advantage in production systems that involve identical equipment such as float systems – involving the existence of spare equipment to replace those that fail or need review. Then, the direct and indirect costs due equipment stoppage are minimized and the level of production or service requirements fulfilled. Although the existence of spare equipment is important to maintain the production process working it is recommended to keep the number of spare equipment in an optimal level for economic reasons.

Mainly due to the non-existence of a specific simulator for the maintenance field, we had a great difficulty in choosing an appropriate simulation tool. However, (Dias et al., 2005) had a definite contribution as far as the simulation tool decision is concerned.

In fact, the choice of *Arena*® as a simulation language was based on the fact that its hierarchical structure offers different levels of flexibility, thus allowing the construction of extremely complex models, allied to a strong visual component (Kelton et al., 2004; Dias et al., 2011; Dias et al., 2006; Pidd, 1993 and Pidd, 1989).

Having referred the importance of studying MFS, the research background section of this paper will focus on the literature review on analytical models, but also on some type of simulation metamodels for this type of maintenance systems.

Next, the description of the MFS section, describes the MFS model used, which formed the basis for the development of our simulation model with the purpose

of analysing system availability and total maintenance cost, as global efficiency measures.

The following section describes new developments on a previous simulation model towards flexibility. In fact, the model presented in (Peito et al., 2011) will gain the capacity to automatically generate a specific simulation program for each specific MFS desired. The program will then be adapted for specific situations with no need of further coding effort. In fact the new proposed tool is intended exclusively to give a response to a type-standard configuration of MFS. Nevertheless, within this type-standard configuration, the user could easily evaluate different strategies under different number of resources available (active machines, maintenance crews and spare machines). This way, the resulting MFS model aims to fill a gap in terms of computer solutions currently existing for this specific type of maintenance systems.

Then we present some results of both global efficiency measures under consideration, in order to evaluate its sensitivity, its precision and its robustness.

Conclusions and Future Developments are the closing sections for this paper.

## 2. RESEARCH BACKGROUND

A literature survey on the field of maintenance systems, regarding the use of discrete event simulation, shows a significant number of scientific publications. Recently, (Alabdulkarim et al., 2013) present a complete set of research works where maintenance costs, maintenance reliability, maintenance operations performance, are some of the most important issues discussed. (Chen and Tseng, 2003), however, are the only authors which main focus is MFS.

In this respect (MFS), (Lopes 2007) refers some studies where simulation has been used to produce results based on specified parameters. Due to the fact that these simulation models were only concerned with the input/output process, without dealing with what is happening during the simulation data process, some metamodels have emerged (Madu and Kuei, 1992b; Madu and Lyeu, 1994; Kuei and Madu, 1994; Madu, 1999; Alam et al., 2003). The metamodels express the input/output relationship through a regression equation. These metamodels can also be based on taguchi methods (Kuei and Madu, 1994) or on neuro networks (Chen and Tseng, 2003). These maintenance system models were also recently treated on an analytical basis by (Gupta and Rao, 1996; Gupta, 1997; Zeng and Zhang, 1997; Shankar and Sahani, 2003; Lopes, 2007). However, the model proposed by (Lopes, 2007) is the only one that deals, simultaneously, with three variables: number of maintenance teams, number of spare equipment, and time between overhauls, aiming the optimization of the system performance. Although this proposed model already involves a certain amount of complexity it may become even more complex by adding new variables and factors such as: a) time spent on spare equipment transportation, b) time spent on spare equipment installation; c) the introduction of more

or different ways of estimating efficient measures; d) allowing the system to work discontinuously; e) speed or efficiency of the repair and revision actions; f) taking into account restrictions on workers timetable to perform the repair and revision actions; g) taking into account the workers scheduling to perform the repair and revision actions; h) taking into account the possibility of spare equipment failure; etc. Anyway these mentioned approaches would aim at ending up with MFS models very close to real system configurations. In fact, the literature review showed that most of the works published, involving either analytical or simulation models, concentrate on a single maintenance crew, or on a single machine on the workstation or even considering an unlimited maintenance capacity – thus overcoming the real system complexity and therefore not quite responding to the real problem as it exists.

As far as the model presented by (Lopes et al., 2005; Lopes et al., 2006; Lopes, 2007) is concerned it is assumed that systems works continuously, its availability is not calculated and the system optimization is only based on the total maintenance cost per time unit. Moreover, it considers that the total system maintenance cost is the same without taking into account the number of machines unavailable, which in many real situations it is not the best option. Finally the referred analytical model only allows that its failures occur under an homogeneous Poisson process (HPP).

Another important aspect on the companies' management strategic definition is to have their tasks correctly planned. To help this planning procedure it is important to know different indicators such as: machine availability, equipment performance and maintenance costs, among others. Therefore one should consider new factors that affect these float systems indicators, such as the possibility of some machine failure, efficiency, repair time, etc.

Moreover, when preventive maintenance policy is used, the time for individual replacement is smaller than time for group replacement. It means that the latter situation requires more machine on the process to be stopped, and also implies an increase for a certain time, on the maintenance crews.

In general companies' policy lies on using economic models to define their best strategies. Profits maximization or costs minimization are the most frequent goals used. However, strictly from the maintenance point of view availability is frequently used as an efficient measure of the system performance, and sometimes more important than the cost based process. In this work availability is calculated dividing the time the system is up ( $T_{up}$ ) by the time the system is up plus the time the system is down ( $T_{down}$ ) for maintenance reasons. Some authors, however, calculate availability through the ratio between MTBF and  $[MTBF+MTTR]$ . Being, MTBF the *Mean Time Between Failures* and MTTR the *Mean Time To Repair*.

### 3. DESCRIPTION OF THE MFS

Our model represents a typical *Maintenance Float System* (MFS) and it is composed of a workstation, a maintenance center with a set of maintenance crews to perform overhauls and repair actions and a set of spare machines (Figure 1). The workstation consists of a set of identical machines and the repair center of a limited number of maintenance crews and a limited number of spare machines. However, the model we have adopted, being a typical MFS, presents certain specificities both as far as the philosophy of the maintenance waiting queues are concerned, and related to the management of the maintenance crews.

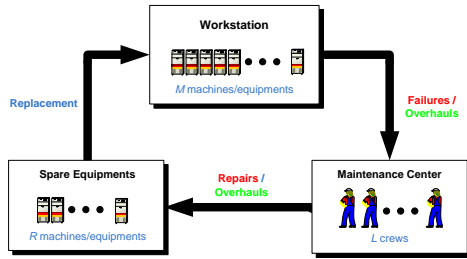


Figure 1: Typical Maintenance Float System

This model follows the one proposed and developed by (Lopes, 2005; Lopes et al., 2006; Lopes et al., 2007), considering  $M$  active machines,  $R$  independent and identical spare machines and  $L$  maintenance crews. The active machines considered operate continuously. Machines that fail are taken from the workstation and sent to the maintenance park waiting queue, where they will be assisted according to arrival time. Machines that reach their optimal overhaul time are kept in service until the end of a period  $T$  without failures. However they will be also kept on a virtual queue to overhaul. If the number of failed machines plus the number of machines requiring overhaul is lower than the number of maintenance crews available, machines are replaced and repaired according to FIFO (*First In First Out*) rule. Otherwise if it exceeds the number of maintenance crews, the machines will either be replaced (while there are spare machines available) or will be sent to the maintenance queue. The machines that complete a duration period  $T$  or time between overhauls in operation without failures are maintained active in the workstation, where they wait to be assisted, and they are replaced when they are removed from the workstation, to be submitted to a preventive action. Its replacement is assured by the machine that leaves the maintenance center in the immediately previous instant. If an active machine happens to fail it waits for the accomplishment of an overhaul, then it will be immediately replaced, if a spare machine is available or as soon it is available.

In this version of our model it is assumed that the  $M$  active machines of the workstation have a constant failure rate while the model runs.

Time between failures are assumed as independent and identically distributed following an Exponential Distribution for all machines (failures occur under a

*Homogeneous Poisson Process*). However, during a simulation run, this value could be adjusted based on time between overhauls. Obviously a smaller time between overhauls implies greater time between failures.

As far as time to overhaul and time to repair are concerned, we have assumed the *Erlang-2* distribution, even though considering overhaul time significantly lower than the repair time.

Now, for our MFS, the variables used are the following:

1. Number of active machines ( $M$ );
2. Number of maintenance crews ( $L$ );
3. Number of spare machines ( $R$ );
4. Machine-Overhauls rate ( $\lambda_{rev}$ );
5. Machine-Initial Failures rate ( $\lambda_f$ );
6. Crews-Repair rate ( $\mu_{rep}$ );
7. Crews-Overhaul rate ( $\mu_{rev}$ );
8. Failure cost ( $C_f$ );
9. Repair cost ( $C_{rep}$ );
10. Overhaul cost ( $C_{rev}$ );
11. Replacement cost ( $C_s$ );
12. Cost due to loss production ( $C_{lp}$ );
13. Holding cost per time unit ( $h$ );
14. Labour cost per time unit ( $k$ );
15. Time to convey and install spare machine ( $T_{ConvInst}$ ).

The developed simulation model for our MFS allows us to estimate the following global efficiency measures:

- a) Average system availability ( $AvgSAv$ );
- b) Total maintenance cost per time unit ( $AvgTCu$ );

However, some other performance measures are also estimated, such as:

- c) Average number of missing machines at the workstation ( $AvgM_{eq}$ );
- d) Average number of machines in the maintenance waiting queue ( $AvgLq$ );
- e) Average waiting time in the maintenance waiting queue ( $AvgWt$ );
- f) Average operating cycle time ( $AvgD$ );
- g) Probability of existing 1 or more idle Machines ( $Prob_{im}$ );
- h) Probability of the system being fully active ( $Prob_s$ );

and still, some individual efficiency measures per machine or maintenance crew, i.e.,

- i) Utilization rate per machine;
- j) Utilization rate per maintenance crew;
- k) Number of overhauls and repair actions performed per maintenance crew;
- l) Average availability per machine.

#### 4. INCREASING FLEXIBILITY OF THE SIMULATION MODEL

The Arena® simulation language environment, used in the previous development (see details on Peito et al., 2011), has been now revisited, aiming to give flexibility to the previous model. The user, now, would be able to automatically generate a simulation program according to specific characteristics of the MFS, namely varying the number of active machines ( $M$ ), the number of maintenance crews ( $L$ ) and the number of spare machines ( $R$ ). However, the steps towards the development of the previous simulation model were all kept and are presented in Figure 2, for a better understanding of the simulation model developed.

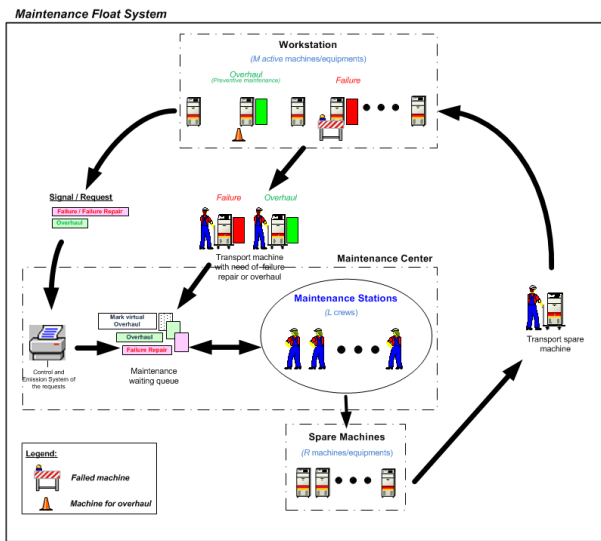


Figure 2: Steps for simulation model development

Figures 3 and 4 explicit the global logical simulation model before and after gaining flexibility, underlining its different developed components:

1. Active machines (*workstation*);
2. Statistics 1 (*Recording Machines  $T_{up}$* );
3. Maintenance queue;
4. Machines' transportation (*by the maintenance crews*);
5. Spare machine request;
6. Maintenance center (*set of maintenance Stations*);
7. Release machines to the set of spare machines;
8. Statistics 2 (*Recording Machines  $T_{up}$  and  $T_{down}$* );
9. Spare machines (*in the start of the system*).

This logical model configuration choice was kept identical for the MFS (figures 3 and 4), providing again a clear global visualization of the undergoing operations and a great simplicity to make changes in the model. In fact the logical model, after increasing flexibility, will appear even more simplified – see Figure 4. The implementation of Arena resource sets, the inclusion of

indexed variables and data arrays and also a set of control variables, replacing previous Arena internal variables, have definitely contributed to a simplified model.

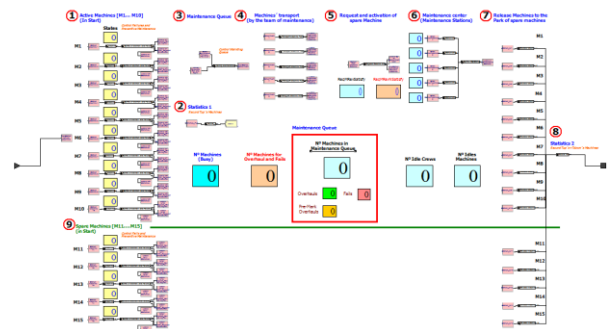


Figure 3: Arena® Logic Model before increasing flexibility

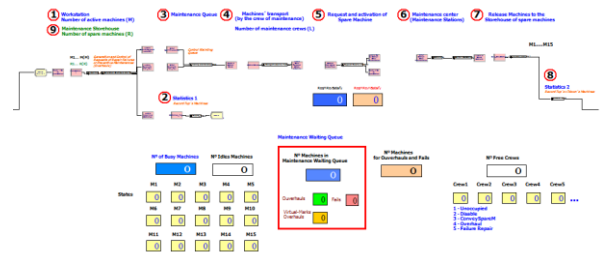


Figure 4: Arena® Logic Model after increasing flexibility

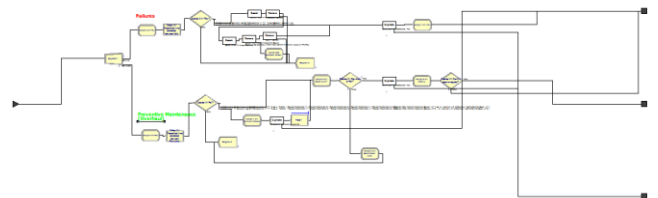


Figure 5: Generation and control system for repair and overhaul requests before increasing flexibility

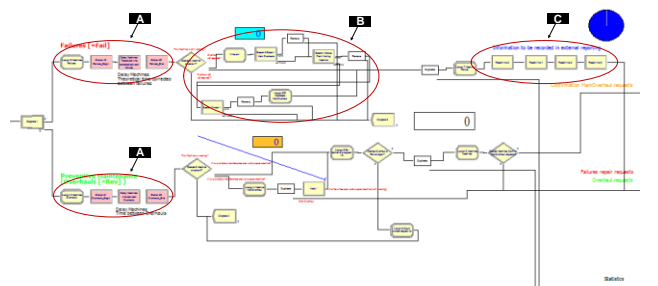


Figure 6: Generation and control system for repair and overhaul requests after increasing flexibility

The components 1 and 9 after increasing flexibility (Fig. 6) include now a generation and control system for all repair and overhaul requests of all machines, this was not the case in the previous model (Figure 5). For this control system to be effective, it would also be

necessary to guarantee absolute independence of each type of request for every machine. For this purpose, a mechanism for attribute identification was developed. With this mechanism, it is now possible to identify the state of each machine and the occurrence of every type of machine request (failure or overhaul), at any instant – entity number and color (see Figure 6, zone A).

In Figure 6 (Zone B), a small change has occurred. In fact, some Arena Blocks have been replaced by Arena Modules. This way, planned changes to some parameters are now easy to implement once Arena shows data in a simple table format.

Finally, Figure 6, Zone C shows four *ReadWrite* Arena modules, allowing the registration, in an excel worksheet, of the failure instants and the number of failures for each machine.

The maintenance waiting queue is defined through a synchronization of events between the component 3 and 4. In the component 4 (figures 7 and 8) there is a "control mechanism", which only allows a request to proceed if there is a free maintenance crew. Component 4 will now include the use of an Arena *Resource Set* for the maintenance crews, selecting the available maintenance crew that has the least number of services allocated.

The rules for the maintenance queue management were all kept unchanged. In fact, FIFO (*First In First Out*) is the rule for the maintenance queue management, except for the case when the total number of maintenance requests (overhauls plus repair actions) exceed the number of maintenance crews available – in this case, machines requiring repair action have priority over machines requiring overhauls.

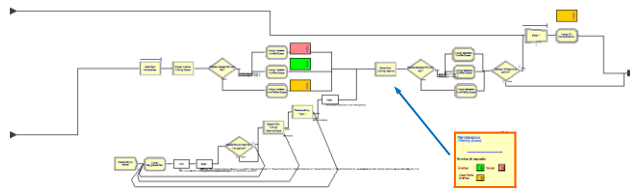


Figure 7: Maintenance waiting queue before increasing flexibility

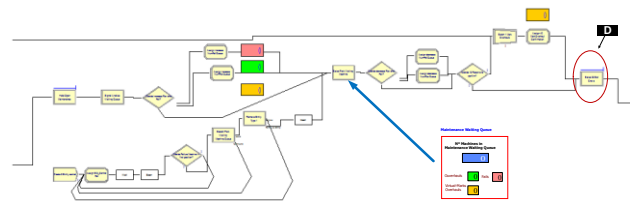


Figure 8: Maintenance waiting queue after increasing flexibility

Component 4 (figures 7 and 8) has also been changed and now includes an *Assign Module* in Zone D. Besides the identification of the maintenance crew and the machine transport state (for a spare machine or a failed machine or even a machine needing overhaul),

this Module also updates the number of maintenance crews that are free.

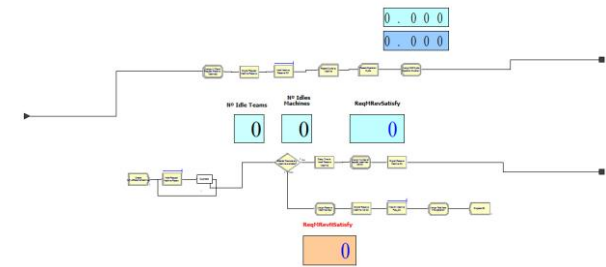


Figure 9: Request and activation of spare machines before increasing flexibility

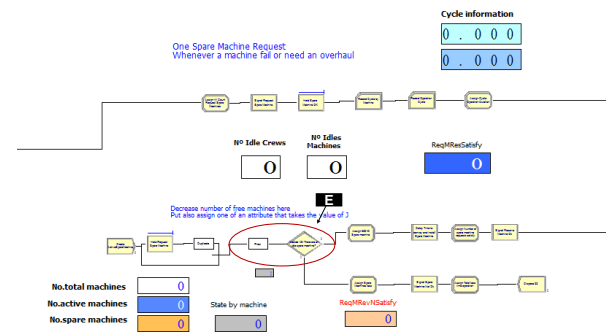


Figure 10: Request and activation of spare machines after increasing flexibility

In component 5 (figures 9 and 10) that performs the request of a spare machine, performed by a maintenance crew, there is only a small change in Zone E, that is related with the demand with one free available machine. Now the model includes a *Search Block* that searches for a free machine.

In component 6 (Figure 11), the change is in the structure of the component. In fact, the discrete variables are now indexed discrete variables – this way, it is possible to individually save a set of performance indicators for both types of maintenance operations.

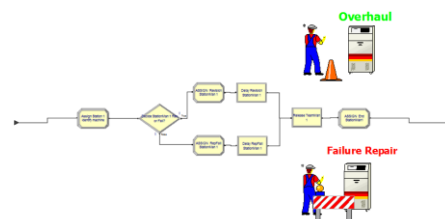


Figure 11: Identification and statistics of the states of the maintenance crew

In component 7, responsible for releasing machines under maintenance crew actions whenever they finish their work, either repairing or performing overhauls, all *Release Modules* have been replaced by a single *Release Block* – this was possible once now only a single indexed discrete variable is capable of saving all the information related to each machine.





Figure 12: Record statistics

Components 2 and 8 (Figure 12) which are responsible to record fundamental statistical data to calculate adequate efficiency measures, do not suffered any change.

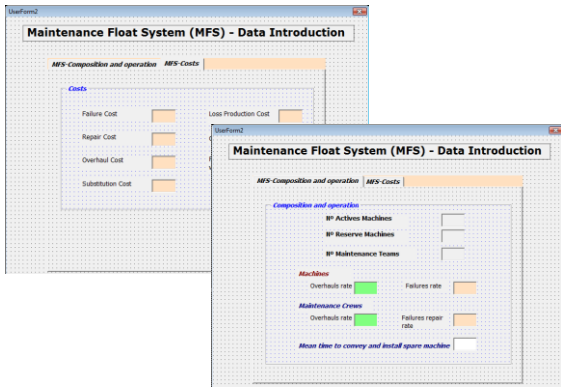


Figure 13: Screenshot of the data input area before increasing flexibility

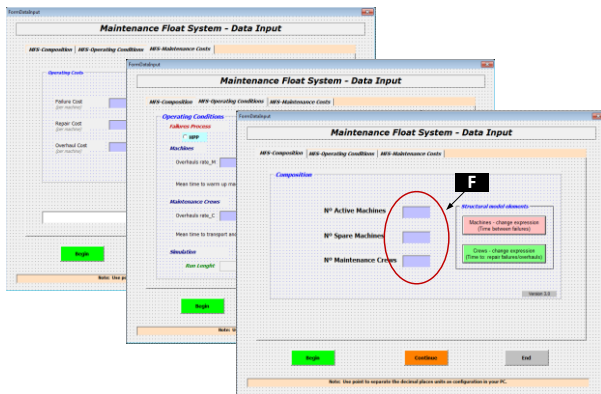


Figure 14: Screenshot of the data input area after increasing flexibility

This work, making previous simulation model gaining flexibility, allows the user to get a simulation model for any *Maintenance Float System* desired – regardless the number of active machines, the number of maintenance crews and the numbers of spare machines. After inputting these three values (Zone F, figures 14), the user will instantly get the appropriate simulation model automatically generated.

**Animation**

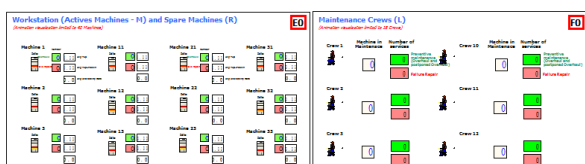


Figure 15: Screenshot of the detailed animation area of the Workstation (limited to  $M = 40$ ,  $L = 18$ )

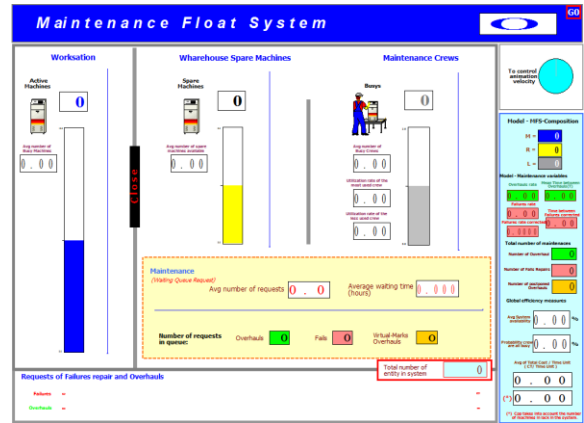


Figure 16: Screenshot of the global animation area of the Workstation

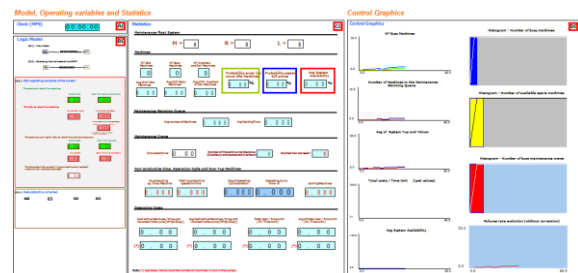


Figure 17: Screenshot of the Operating variables, Statistics and Graphics control area

The presentation of model animation (Figures 15 and 16) and output statistics (Figure 17) had changes relatively to the version presented in (Peito et al., 2011).

**5. SIMULATION RESULTS AND DISCUSSION**

This paper focus on the two general performance measures mentioned above – system availability and total maintenance cost per time unit, which were determined considering a *Maintenance Float System* with 10 active and identical machines ( $M$ ), 5 spare machines ( $R$ ) and 5 maintenance crews ( $L$ ).

Simulation length was set to 9.000 hours (approximately one year) – warm-up period was set to 3.500 hours.

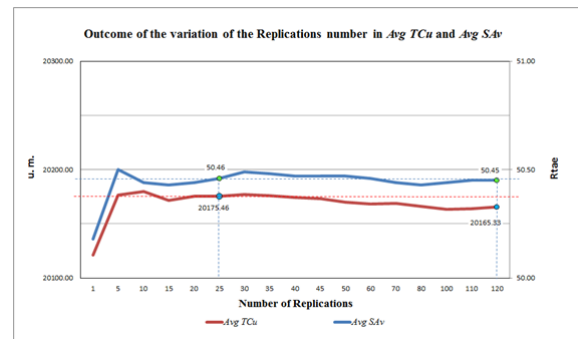


Figure 18: Outcome of the variation of the Replications number in  $AvgTCu$  and  $AvgSAv$  variables

For each set of input parameters and pattern for variables, the simulation output variables  $AvgSAv$ ,  $AvgTCu$  and  $AvgTCu^*$  were estimated based on 25

replications – for an adequate system stabilization and results robustness for both performance measures (Figures 18 and 19) and also due to computational time required to run the model.

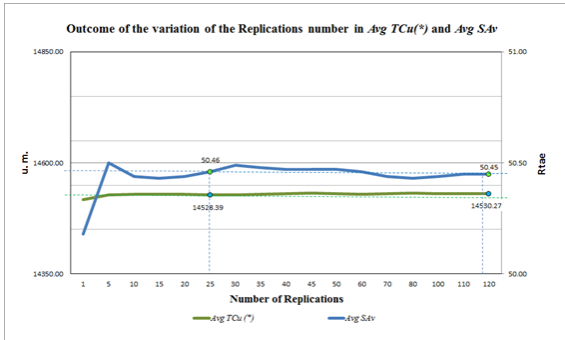


Figure 19: Outcome of the variation of the Replications number in  $AvgTCu(*)$  and  $AvgSAv$  variables

Bearing in mind the fifteen variables of MFS previously referred, simulation models were used to test and estimate the behavior of the two global efficiency measures mentioned on the previous section. Simulation models were carried out for (1-60) hypothetical scenarios with different overhauls rates ( $\lambda_{rev}$ ). These different overhauls rates are associated with different times between overhauls ( $T$ ) which are defined accordingly to the preventive maintenance policy aiming the best option.

Table 1: Global efficiency measures outcomes in the MFS model after 25 replications

*(Values estimated by simulation after 25 replication)*

Scenario	$\lambda_{rev}$ (/hour)	$T$ (hour)	$AvgSAv$ (%)	$AvgTCu$ (m.u./hour)	$AvgTCu(*)$ (m.u./hour)
1	0,10	10,000	29,25	21064,60	17304,37
2	0,20	5,000	34,75	21127,96	16646,80
3	0,30	3,333	40,79	21065,24	15870,35
4	0,40	2,500	45,26	20915,39	15287,79
5	0,50	2,000	48,12	20751,46	14908,68
...	...	...	...	...	...
52	9,00	0,111	48,71	20195,00	14776,87
53	15,00	0,067	48,52	20212,24	14807,21
54	20,00	0,050	48,54	20228,63	14815,57
55	25,00	0,040	48,56	20223,63	14814,18
56	30,00	0,033	48,54	20230,24	14816,98
57	35,00	0,029	48,62	20226,82	14811,16
58	40,00	0,025	48,54	20229,16	14820,31
59	45,00	0,022	48,50	20228,80	14822,78
60	50,00	0,020	48,52	20226,42	14815,55

(\*) Considers that the cost of lost production changes in function of the number of active machines lacking in the system.

A first global analysis of the values presented in tables 1 and 2 indicate that the precision obtained on the three efficient measures analysed is different. An individual analysis of each measure indicates that  $AvgTCu$  shows the smaller variation (MPO lower). In Table 1 it can also be observed that when  $T$  takes very small values ( $T \leq 0.111$  or  $\lambda_{rev} \geq 9$ ) the three efficient

measures [ $AvgTCu$ ,  $AvgTCu(*)$  and  $AvgSAv$ ] are kept practically unchangeable. This fact can be confirmed in Figure 20 or in Table 2 where the MPO for these values of  $T$  is extremely low, almost zero. On the other hand, when  $T$  assumes very high values ( $T \geq 2,5$  or  $\lambda_{rev} \leq 0,4$ ) the efficiency measures  $AvgTCu(*)$  and  $AvgSAv$  present high MPO values in opposition to  $AvgTCu$  that shows very small values. In Table 2 it can also be observed that  $AvgTCu$  presents the lowest MPO average value of the three efficiency measures and that  $AvgSAv$  has the highest value.

Table 2: Observe percentage change in the global efficiency measures after 25 replications

MPO - Percentage change observed			
Scenario	$AvgSAv$	$AvgTCu$	$AvgTCu(*)$
1-2	15,83%	0,30%	-3,95%
2-3	14,80%	-0,30%	-4,89%
3-4	9,87%	-0,72%	-3,81%
4-5	5,95%	-0,79%	-2,54%
...	...	...	...
52-53	-0,14%	0,06%	0,10%
...	...	...	...
58-59	-0,07%	0,00%	0,02%
59-60	0,04%	-0,01%	-0,05%
<b>Max.</b>	<b>15,83%</b>	<b>-0,79%</b>	<b>-4,89%</b>
<b>Mean</b>	<b>0,80%</b>	<b>-0,07%</b>	<b>-0,27%</b>

In order to simplify the interpretation and analysis of these global efficiency measures, figures 20, 21 and 22 pinpoint the maximum and minimum values (table 2 and 3) as well as other points considered relevant for the analysis.

Table 3: Maximum values of the main efficiency measures

	Statistics (Maximum)	$\lambda_{rev}$ (/hour)	$T$ (hour)
$AvgSAv$ (%)	50,70%	0,90	1,111
$AvgTCu$ (m.u./hour)	21127,96	0,20	5,000
$AvgTCu(*)$ (m.u./hour)	17304,37	0,10	10,000

Note: Red points in the graphics

Table 4: Minimum values of the main efficiency measures

	Statistics (Minimum)	$\lambda_{rev}$ (/hour)	$T$ (hour)
$AvgSAv$ (%)	29,25%	0,10	10,000
$AvgTCu$ (m.u./hour)	20096,90	1,80	0,556
$AvgTCu(*)$ (m.u./hour)	14518,77	1,20	0,833

Note: Yellow points in the graphics

Tables 3 and 4 show that the  $T$  value corresponding to the minimum value of  $AvgSAv$  corresponds the maximum value, as expected, of  $AvgTCu(*)$ . When compared with the minimum of  $AvgTCu$ , there is a significant  $T$  gap ( $\approx 5$  hours), although, its remains practically the same when the value of  $T$  changes from 5 to 10 hours (Figure 20).

When comparing the  $T$  value corresponding to the maximum value of  $AvgSAv$  with the  $T$  value corresponding to the minimum value of  $AvgTCu(*)$ , there is only a small gap, which is clearly higher in the case of the  $T$  value corresponding to the minimum of the  $AvgTCu$  (Figure 22).

Table 5: Correlation coefficients

	$T$	$AvgSAv$	$AvgTCu$	$AvgTCu(*)$
$T$	1	-0,9021	0,8279	0,9017
$AvgSAv$	-0,9021	1	-0,7980	-0,9986
$AvgTCu$	0,8279	-0,7980	1	0,8237
$AvgTCu (*)$	0,9017	-0,9986	0,8237	1

A careful analysis of the correlation coefficients of three efficiency measures, table 5, shows that  $T$  variations are better explained by  $AvgSAv$  and  $AvgTCu(*)$  ( $\approx 90\%$ ). It is also verified that there is a high inverse correlation between  $AvgSAv$  and  $AvgTCu(*)$  ( $\approx 99,8\%$ ). However when  $AvgTCu$  is compared with  $AvgTCu(*)$  or with  $AvgSAv$ , the correlation coefficient decreases to 82,37% and to 79,80%, respectively. This partially explains why in tables 3 and 4 the  $T$  value corresponding to the maximum of  $AvgSAv$  does not correspond exactly to the  $T$  value corresponding to the minimum of the  $AvgTCu$  and  $AvgTCu(*)$  and that difference being higher in the case of  $AvgTCu(*)$  (Figure 22).

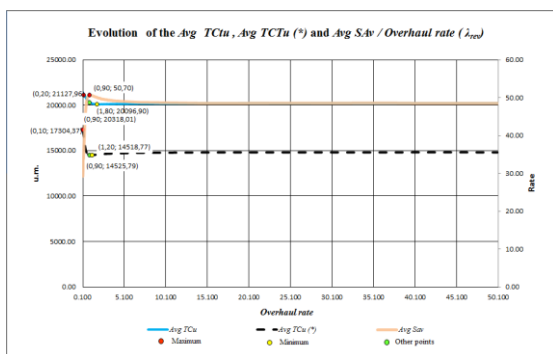


Figure 20: Evolution of the  $AvgTCtu$ ,  $AvgTCTu(*)$  and  $AvgSAv / Overhaul rate (\lambda_{rev})$

As it can be observed in Figure 20 and more clearly in figures 21 and 22, for the MFS analyzed, the three global measures of efficiency being studied only present small variations for values of  $\lambda_{rev}$  between 0,10 and 9,00 (or  $T$  between 10,000 and 0,111 hours). For values of  $\lambda_{rev}$  higher than 9.00 the three global measures of efficiency remain practically unchanged.

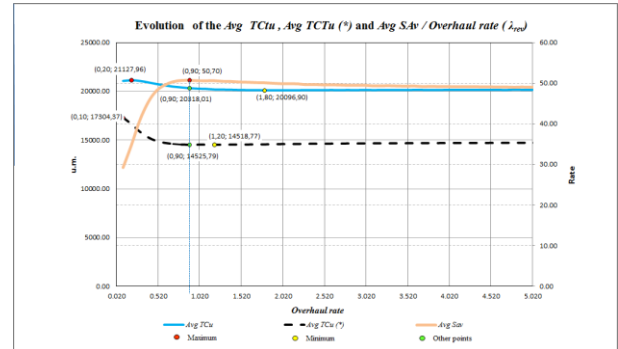


Figure 21: Evolution of the  $AvgTCtu$ ,  $AvgTCTu(*)$  and  $AvgSAv / Overhaul rate (\lambda_{rev})$  [Zoom Figure 20]

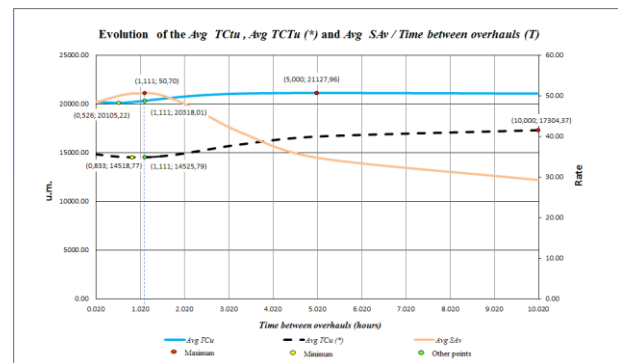


Figure 22: Evolution of the  $AvgTCtu$ ,  $AvgTCTu(*)$  and  $AvgSAv / Time between overhauls (T)$

Table 6: Comparison among the  $AvgTCu$  values estimates by the simulation model and analytic model (Lopes, 2007)

$T$	Model	$AvgTCu$ (m.u./hour)	$AvgTCu(*)$ (m.u./hour)	$\Delta_1$ (%)	$\Delta_2$ (%)	$\Delta_3$ (%)
1,66	Simulation	20381,74	14554,5	-40%	-12%	-25%
	Analytic	18130,56	----	----		
3,33	Simulation	20126,65	14555,62	-38%	-19%	-17%
	Analytic	16968,39	----	----		
1,66	Simulation	20111,24	14628,02	-37%	-16%	-18%
	Analytic	17303,65	----	----		
3,33	Simulation	21065,24	15870,35	-33%	-16%	-14%
	Analytic	18167,34	----	----		
<b>Mean</b>				<b>-37%</b>	<b>-16%</b>	<b>-18%</b>

Note:  $M=10$ ;  $R=5$ ;  $L=5$ .  
 (\*) Considers that the cost of lost production changes in function of the number of active machines lacking in the system.  
 $\Delta_1$  – Difference among Simulation  $AvgTCu$  and Simulation  $AvgTCu(*)$   
 $\Delta_2$  – Difference among Simulation  $AvgTCu$  and Analytic  $AvgTCu$   
 $\Delta_3$  – Difference among Analytic  $AvgTCu$  and Simulation  $AvgTCu(*)$

In Table 6 there is a comparison between the values obtained from the simulation model developed by the authors in a former (Peito et al 2011) and the analytical model developed by (Lopes 2007). The sample size of the results presented and compared in this case was limited by the number of results presented by the author in her work (Lopes, 2007). In this table it can be verified that when the two global efficiency measures are both estimated from the simulation model the difference ( $\Delta_1$ ) is on average -37%, presenting



$AvgTCu$  always higher values. However when  $AvgTCu$  is estimated through the analytical model that difference ( $\Delta_3$ ) is on average -18%. When the same efficiency global measure based on the analytical model is compared with the one calculated based on the simulation model,  $AvgTCu$ , this if calculated from the analytical model presents lower values, on average, of 16%. It is also observed that the analytical model always presents for its efficiency measure values that lie between the two efficiency measures estimated from the simulation model.

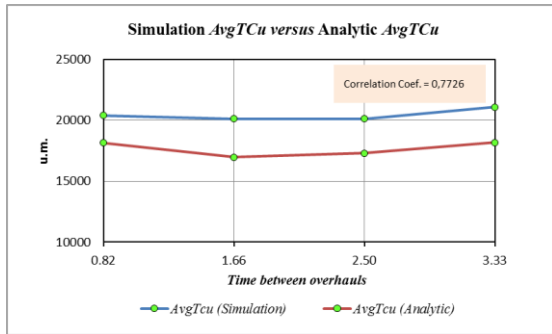


Figure 23: Comparison among the  $AvgTCu$  values estimates by the simulation model and by the analytic model (Lopes, 2007)

Finally, through Figure 23 it can be verified that the behavior of  $AvgTCu$  is identical in both models. However this results analysis lacks confirmation due to small sample size dimension.

## 6. CONCLUSIONS

Firstly, this paper shows how to develop an advanced simulation model, incorporating flexibility. This target would be reached by developing and incorporating new modules in our simulation tool, following past experiences found on literature (Dias et al. 2005, 2006 and Vilc et al. 2009, 2010) where the automatic generation of simulation programs enables desired model flexibility, i.e., making the model generating specific simulation programs for specific *Maintenance Float Systems*. This new development of our simulation model for our *Maintenance Float System* presents:

- More flexibility

This was the main challenge for the work presented in this paper. The automatic generation of simulation models, depending on the three main maintenance system variables –  $M$ , number of active machines;  $L$ , number of maintenance crews;  $R$ , number of reserve machines. In fact, the user would just have to introduce  $M$ ,  $L$  and  $R$  and, instantly, he will get the adequate simulation model to run and experiment.

- More interactivity

Now the user has the possibility to interact with the simulation model during each simulation run. In fact the user can now modify all variables of the maintenance system under

analysis and can, therefore, evaluate system behaviour under different maintenance strategies.

- Better information

This model now offers much better maintenance information. Indeed, the strong visual aspect offered by the developed model clarifies the actual process inside the system. This allows a better understanding of the different interactions in the model and of the simulation results.

This paper also shows that the estimated values for the performance measures analysed (system availability and total maintenance cost per time unit) present similar values for the simulation model and analytical model, as far as a *Maintenance Float System* with  $M=10$ ,  $R=5$  and  $L=5$  is concerned. Also, it is quite clear that variance is different for both global efficiency measures analysed, especially when using extreme values for periodic overhauls rates. In this respect,  $AvgSav$  is the most sensitive parameter. As expected, the least sensitive parameter is  $AvgTCu$ , as it does not take into consideration the number of available machines, i.e., the cost for production loss is constant, irrespective of the number of available machines in the system.

However, the greatest overall contribution of this paper is therefore related to the construction of a flexible simulation decision support tool for MFS, where several efficiency measures of MFS are involved. Thus, in any classic MFS (number of active machines, number of spare machines and maintenance crews) subject to preventative actions and accidental actions of maintenance, this tool deals with the evaluation of its efficiency in terms of costs and in terms of availability. Also, considering simultaneously preventive maintenance actions and accidental maintenance actions, represents another novelty, once the simulation models found on the literature would approach these issues individually. Moreover, this simulation tool enables to tackle large scale float systems, up to  $\pm 1000$  active machines,  $\pm 1000$  spare machines and  $\pm 1000$  maintenance crews. On the other hand, the diversity of efficiency measures calculated in the MFS simulation model really helps the decision maker to take the appropriate decisions. Finally this model presents the advantages usually associated with simulation models, namely a better understanding of the functioning of the system, the possibility of identifying the critical points of the system and the easy adaptation of the simulation model to reflect changes in the operating conditions of the system.

## 7. FUTURE DEVELOPMENTS

The simulation model here presented, incorporating analysis of usual performance measures, also drives its concern towards new efficiency measures, enabling new trends for the analysis and discussion of the best decisions as far as a specific *Maintenance Float System* is concerned. Nevertheless the authors are now aiming

to the development of an advanced simulation model, incorporating still more flexibility. This target would be reached by developing and incorporating new modules in our simulation tool, in order to also incorporate maintenance systems where failure rates would also vary while the model runs, i.e., where a *Non Homogeneous Poisson Process* (NHPP) is present. These mentioned future developments also intend to potentiate the known capability of simulation to efficiently communicate with managers and decision makers, even if they are not simulation experts.

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