

Study of the Influence of β -Radiation on the Properties and Mineralization of Different Starch-Based Biomaterials

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Received 8 June 2004; revised 29 October 2004; accepted 29 October 2004

Published online 19 May 2005 in Wiley InterScience (www.interscience.wiley.com). DOI: 10.1002/jbm.b.30260

Abstract: In this work, the effects of β -radiation are assessed, for the first time, on starch-based biodegradable polymers, with the aim of using it as an alternative sterilization process to the previously studied sterilization methods. Different doses of radiation were used in order to investigate the possibility of using this sterilization technique as a treatment to tailor the surface and bulk properties (namely mechanical) of these polymers. The as-treated substrates were characterized by water-uptake measurements and contact angle (θ) measurements. The mechanical properties of the materials were characterized by tensile tests by means of ultimate tensile strength (UTS) and strain at break (ϵ_r). The fracture of the surfaces was observed by scanning electron microscopy (SEM). Dynamic mechanical analysis (DMA) was also used to characterize the viscoelastic behavior of the irradiated materials. The main effect of sterilization with β -radiation over the starch-based polymers seems to be a surface modification by an increase of the hydrophilicity. Nevertheless, because β -radiation did not significantly affect the mechanical properties, it can be regarded as an effective way of modifying the surface for applications where more hydrophilic surfaces are desirable. © 2005 Wiley Periodicals, Inc. *J Biomed Mater Res Part B: Appl Biomater* 74B: 560–569, 2005

Keywords: β -radiation; starch-based biodegradable polymers; dynamic mechanical analysis (DMA); sterilization

INTRODUCTION

The increased demands placed on biomaterials for both currently approved and novel emerging applications continue to stimulate the interest in improving the performance of existing medical-grade polymers and developing new polymeric systems. Starch-based polymers present an enormous potential to be widely used in the biomedical and the environmental fields, as they are biodegradable, inexpensive (when compared to other biodegradable polymers) from renewable origin, and available in large quantities.^{1–3} On the other hand, they exhibit a biocompatible behavior already demonstrated by *in vitro*^{4–6} and *in vivo* studies.⁶ Indeed, this class of materials has recently been proposed for a wide range of biomedical applications including bone replacement/fixation

and filling of bone defects,^{7,8} hydrogels for drug delivery,^{9,10} or bone cements.¹¹ Furthermore, starch-based polymers can also be converted into complex geometries with interesting mechanical properties, by using standard equipment developed for the processing of synthetic polymers^{12,13} or by different innovative methodologies.^{14,15} These constructs are being proposed to be used as temporary scaffolds for several tissue engineering approaches.^{12–15}

Starch-based systems, under consideration for being used in tissue replacement/fixation or as tissue engineering scaffolds, must exhibit mechanical properties that match, as close as possible, those of human bone. This should be associated to a degradation kinetics adequate for tissue healing that is to be replaced or fixed.^{12,16,17} In addition, by the incorporation of bonelike inorganic fillers, such as hydroxyapatite (HA)^{18–22} or bioactive glasses,^{23,24} it is possible to develop bioactive degradable composites with an interesting range of mechanical properties. It was also reported^{18,25} that the physical properties of those materials can be further optimized by controlling the morphologic developments within the molds by using nonconventional processing routes. When coated

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Contract grant sponsor: Portuguese Foundation for Science and Technology (FCT); contract grant number: SFRH/BD/10956/2002

Contract grant sponsor: Portuguese Foundation for Science and Technology (FCT) POCTI and/or FEDER programs

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with a bonelike apatite layer, biodegradable polymers also have a great potential to be used as bone-repairing materials because they can exhibit not only mechanical properties analogous to the natural bone but also a bioactive character.^{26–29}

No matter how optimized a biomaterial is, it will always have to resist the final step of sterilization before implantation. Sterilizability and storage stability are necessary for any material used in a medical application.^{30,31} It is then important to investigate the stability of a material after sterilization and to determine the most convenient sterilization methodology. Furthermore, sterilization can be used as a treatment to improve mechanical properties (crosslinking) and tailor the surface properties of polymeric biomaterials.³² In this context, the effects of ethylene oxide (EtO) sterilization over the properties of starch-based polymers were already studied in previous works, namely its influence on the formation of a biomimetic coating.^{33,34} Nevertheless, its attractiveness is decreasing due to the toxicity and flammability of the EtO gas,³⁵ as well as some concerns and lobbying strategies related to possible cancer-inducing effects.³⁶ On the other hand, sterilization by high-energy radiation has the advantages of high efficiency, negligible thermal effects, high penetration, and being a chemically cleaner process.^{31,37} γ -radiation sterilization is widely studied for application with biodegradable polymeric biomaterials.^{38,39} One side effect of γ -rays is on the bulk properties of the polymers, due to the high penetrability of this type of radiation. The influence of γ -radiation on starch has been studied in the past years with regard to the agricultural and food chemistry fields. It is well known that this type of radiation induces physicochemical transformations in starch granules.⁴⁰ The breakdown of glycoside bond and decomposition of macromolecules accompanied by the creation of macromolecules with smaller chains is the primary reaction occurring under the influence of irradiation.⁴¹ Apart from these effects, small molecular products are created, caused by glycoside bond destruction at chains termini.⁴² A decrease in both crystalline phase content and the ordered distributions of amylose and amylopectin macromolecules in starch granules, connected with these chemical changes, was observed by authors such as Ciesla and colleagues.⁴³

Recent advances in electron beam technology have made this mode of sterilization a worthy competitor to the traditional γ processing. Increased available energy, compact design, improved reliability, and the absence of a source that steadily depletes with time are some of the reported advantages.⁴⁴ Although the primary event of interaction with matter is different between γ -radiation and electrons, the major interaction is still Compton scattering for both cases. It is mainly the shower of secondary electrons that initiates the ionization events that triggers numerous chemical reactions, many of which lead to oxidative degradation. Although the main interaction with matter is basically the same for γ and high-energy electrons, differences between the two modes remain. The penetration of β -radiation is lower than in the case of γ -radiation, which will be advantageous for preserv-

ing the mechanical bulk properties of materials,⁴⁴ for example, biodegradable polymers.

This preliminary work aims at evaluating the effects of β -radiation on both the mechanical performance and degradation behavior of starch-based biodegradable polymers, as well as to assess the potential of β -radiation as alternative sterilization method to previously studied sterilization methods. Furthermore, different radiation doses were also tentatively investigated as possible routes for tailoring the surface and bulk properties (namely mechanical) of these starch-based biodegradable polymers.

MATERIALS AND METHODS

Materials

The studied materials included injection-molded blends of starch with: (i) poly(ethylene vinyl alcohol) (SEVA-C, 50/50 wt %), (ii) cellulose acetate (SCA, 50/50 wt %), and (iii) polycaprolactone (SPCL, 30/70 wt %). The materials were injection molded in a Klockner Desma FM-20 (Fridingen/Donau, Germany), in order to produce standard ASTM tensile dumbbell samples with a cross-section of $2 \times 4 \text{ mm}^2$. These materials were subjected to 25, 50, and 100 kGy doses of β -radiation according to the standard procedure of *IonMed Esterilizacion*, S.A. (Madrid, Spain), using a Rhotron TT2 electron accelerator (10 MeV).

Mechanical Properties

Tensile tests were performed in order to evaluate the influence of β -radiation doses on the mechanical behavior of the starch-based materials. The samples were tested in order to determine the modulus of elasticity (e-modulus), the ultimate tensile strength (UTS), the strain at break (ϵ_b) and the energy to break point (U_b). Five samples were tested for each condition. These tests were performed on an Instron 4505 universal mechanical testing machine (Canton, MA, U.S.A.) fitted with an Instron 2703 10-mm gauge length resistive extensometer under controlled conditions (23°C, 55% RH). The crosshead speed was 5 mm/min until 1% strain was reached (for more precision); the speed was then increased to 50 mm/min until fracture.

SEM Analysis of Tensile Fracture Surfaces

After performing tensile tests on the studied materials, the morphology of the obtained surface fractures was observed by scanning electron microscopy (SEM), in a Leica Cambridge S360 (Cambridge, UK) or in a HITACHI S4100 (Tokyo, Japan). All the samples were previously gold-coated in a Sputter Jeol JFC 1100 equipment (Tokyo, Japan).

DMA Analysis

The investigation of the viscoelastic properties of biodegradable polymeric-based systems may be of great interest because one can not only simulate the physiological dynamical

loading, but can also access relevant fundamental information at the molecular level, both from a structural and dynamic perspective. In a more practical point of view, besides the typical quasistatic mechanical properties (elastic modulus or ultimate strength and strain), an implantable biomaterial should exhibit adequate rheological properties that should preferentially match those of the tissues with which it will be in contact. The dynamic mechanical analysis technique (DMA) is a very suitable tool to investigate the viscoelastic properties of polymers in a wide range of temperatures and frequencies.⁴⁵

DMA characterization was performed in order to evaluate the possible effects of β -radiation on the viscoelastic behavior of different starch-based materials. For this study, injection-molded samples were shaped into specimens of 5×20 mm and tested under a three-point bending loading scheme, using a PerkinElmer DMA7e apparatus (Norwalk, CT) with controlled cooling accessory. High purity helium was used as a purge gas, increasing the thermal conductivity inside the furnace. Temperature was scanned from -30 to 130°C at $4^\circ\text{C}/\text{min}$ at a frequency of 1 Hz. The specimens were placed over a bending platform with a 15-mm span and a 5-mm knife-edge probe tip that provided the mechanical excitation: a static stress of 0.36 MPa for SEVA-C and SCA and 0.12 MPa for SPCL superimposed to a dynamic stress of 0.30 MPa for SEVA-C and SCA and 0.10 MPa for SPCL. Those stress values were sufficiently small to assure that the mechanical response of the specimens is within the linear viscoelastic regime. A minimum of three samples were analyzed and averaged for each condition.

Studies in Wet Conditions

Studies in wet conditions are of a great importance for any degradable biomaterial¹⁷ because when implanted, it will inevitably be in the presence of the body fluids that will diffuse into the bulk of the polymer as degradation takes place.

For water-uptake measurements, all samples were weighed before immersed in distilled water (at room temperature) and every 2 h, during the first 12 h of immersion. After that period, weights were recorded every 24 h until the end of the experiment time (7 days). The samples were carefully removed from the water-containing flasks and immediately weighed for determination of wet weight as a function of the immersion time. Water-uptake is given by:

$$\text{Water absorbed} = [(m_f - m_i)/m_i] \times 100 \quad (1)$$

where m_i is the initial weight of the sample and m_f is the sample weight after a given time of immersion.

The degradation behavior was assessed after several pre-fixed aging periods (0, 3, 7, 15, and 60 days) for materials before and after increasing doses of β -radiation, in an isotonic saline solution (NaCl 0.154 M). For each period, three samples were used. At the end of each aging period, the samples were removed from the solution and then dried up to

exhaustion (6 days at 60°C), in order to determine the dry weight loss, which is given by:

$$\% \text{ Weight loss} = [(m_i - m_d)/m_i] \times 100 \quad (2)$$

where m_i is the initial weight of the sample and m_d is the sample dry weight after a given time of immersion.

Contact-angle measurements

In previous works, SEVA-C has demonstrated to be a quite hydrophilic substrate.^{17,27} In this work, contact-angle measurements were performed on all the starch-based polymer samples before and after increasing doses of β -radiation in order to detect any eventual modification in the surface of the material. Contact-angle measurements were obtained by the sessile drop method using a standard contact angle apparatus (Krüss, Hamburg, Germany). The measurements were performed with the aid of an image analysis system (G2/G40) installed in the apparatus. Duplicate measurements were recorded for each drop deposition. The average values were recorded after 5 s of the drop deposition (settling time). Ten average values were recorded for each condition and a final average value was calculated. All the measurements were made at room temperature and the probe liquid was distilled water.

RESULTS AND DISCUSSION

Mechanical Properties

The effect of β -radiation over the mechanical properties and chemical structure of starch polymers (SEVA-C, SPCL, and SCA) was studied. All the materials were subjected to different doses of β -radiation: 25, 50, and 100 kGy. Tensile tests were performed in order to evaluate inevitable mechanical properties changes resulting from the sterilization process. Table I presents the tensile results as function of increasing radiation doses.

The tensile test results show that the mechanical properties of the starch-based blends such as SEVA-C and SCA appear to be less affected by β -radiation. However, β -radiation seems to affect SPCL more extensively. In general, β -radiation affects the stiffness, strength, and ductility in different ways for each material. For SEVA-C, the decrease in stiffness and ductility and the simultaneous increase in strength may be an indication of a possible decrease in crystallinity. Because sterilization with EtO has been already tested for this particular material, it is interesting to compare the previously obtained results with those obtained here. Data for the mechanical properties of this material after exposure to EtO sterilization, as reported previously,³³ indicated that some degradation took place. A decrease in the modulus of 9% and 29%, after one and two consecutive sterilization cycles, respectively, were observed, as well as a concomitant decrease in crystallinity. The gas absorbed in the structure was re-

TABLE I. Tensile Results for Samples Subjected to Different Doses of β Radiation

Material	Dose (kGy)	Stiffness E-modulus (GPa)	Strength UTS (MPa)	Ductility ϵ_b (%)	Toughness U_b (J)
SEVA-C	0	1.89 \pm 0.34	33.2 \pm 0.9	52.3 \pm 1.8	1.03 \pm 0.032
	25	1.89 \pm 0.12	39.1 \pm 0.1	21.3 \pm 0.3	0.51 \pm 0.049
	50	1.76 \pm 0.06	36.3 \pm 0.6	31.1 \pm 0.5	0.67 \pm 0.002
	100	1.64 \pm 0.07	37.3 \pm 0.4	23.8 \pm 5.8	0.51 \pm 0.124
SCA	0	1.01 \pm 0.11	26.1 \pm 0.8	11.9 \pm 1.1	0.21 \pm 0.01
	25	1.28 \pm 0.05	33.8 \pm 1.0	9.2 \pm 1.2	0.19 \pm 0.02
	50	1.56 \pm 0.19	34.7 \pm 1.1	8.6 \pm 1.3	0.19 \pm 0.03
	100	1.45 \pm 0.14	34.8 \pm 2.3	6.8 \pm 0.9	0.13 \pm 0.01
SPCL	0	0.22 \pm 0.03	24.1 \pm 1.6	641.0 \pm 10.8	8.36 \pm 0.24
	25	0.33 \pm 0.04	22.1 \pm 0.5	606.4 \pm 16.8	7.50 \pm 0.34
	50	0.30 \pm 0.03	18.4 \pm 1.5	574.9 \pm 62.6	6.59 \pm 1.03
	100	1.07 \pm 0.38	14.2 \pm 0.2	299.5 \pm 17.0	2.34 \pm 0.11

ported as a plasticizer, increasing the ductility of these type the polymers.³³

Studies performed by Kowalski and colleagues⁴⁶ have helped to determine 25 kGy as the standard radiation dose for γ -radiation. However, even using this dose, effects in the bulk structure of different materials have been reported.^{31,46–48} In the herein studied β -radiation doses, the maximum decrease in modulus obtained was 13% after an exposure to the maximum dose of 100 kGy, which is four times higher than the recommended dose for γ -radiation. For the recommended dose (25 kGy), no significant change in the stiffness of SEVA-C is observed. These observations clearly indicate a negligible effect of β -radiation on bulk stiffness of the SEVA-C samples when applied under the typical radiation dosages of γ -radiation. Even though a decrease in ductility is observed upon β -radiation, these results are still attractive as it shows possible to sterilize the material without inducing any severe modifications of its bulk properties. Although β -radiation relies on the same basic principles as γ -radiation, the two methods differ in their interaction with matter. While γ -rays are characterized by high penetration and low dose rate, β -radiation is characterized by low penetration and high dose rate,⁴⁹ which may justify the obtained differences in the mechanical behavior.

For SCA, an enhancement in both the stiffness and the strength occurs for increasing β -radiation doses. This different behavior for SCA as compared to SEVA-C may be intimately related to the different nature and chemistry of the two blends. In fact, SEVA-C is an interpenetrated network (IPN) composed by starch and ethylene-vinyl alcohol copolymer (50/50 wt %), while SCA is a nonmiscible blend composed of starch and cellulose acetate (50/50 wt %). In the case of SCA, the β -radiation may induce more extensively free radical formation and crosslinking of both natural polymers, which can ultimately lead to their degradation of the material for high radiation levels. It is important to note that in spite of an increase in both stiffness and strength occurs with increasing β -radiation doses up to 50 kGy, a continuous decrease in ductility and toughness is observed upon β -radiation, which may be an indication of a possible competing phenomenon between crosslinking and blend degradation. However, these statements will require further chemical and structural characterization to support them. In spite of that, the observed variations in mechanical performance anticipate some variation in the degradation behavior of SCA for different β -radiation doses.

The exposure of SPCL to β -radiation causes its stiffening and a strong decrease of the respective ductility. For the

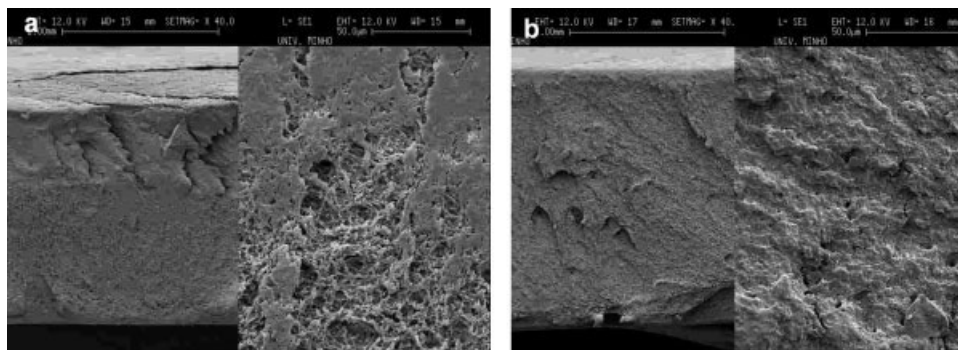


Figure 1. SEM micrographs of the fracture surfaces of SEVA-C (a) before and (b) after β -sterilization, using a radiation dose of 100 kGy.

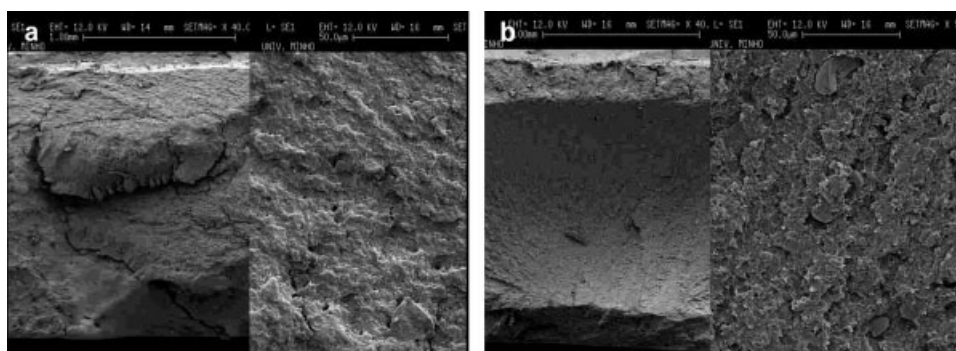


Figure 2. SEM micrographs of the fracture surfaces of SCA (a) before and (b) after β -sterilization, using a radiation dose of 100 kGy.

highest dose, the influence of the β -radiation is evident. These results emphasize once more the importance of the nature and chemistry of the blend on the effect of radiation dose on mechanical properties. SPCL can be regarded as an homogeneous compatible blend of starch with poly(caprolactone) (PCL; 30/70 wt %), where poly(caprolactone) is believed to play a prominent role. The variation in mechanical behavior may suggest a similar molecular mechanism for SPCL upon radiation as that proposed for SCA based on the free radical formation and occurrence of crosslinking and/or molecular degradation. In this respect the poly(caprolactone) fraction is assumed to play an important role, as the decrease in toughness observed for SPCL upon radiation dose is consistent with an embrittlement of the blend, which could hardly be explained with structure variations within the starch fraction exclusively. This variation may be largely dominated by structure variations within the much more crystalline synthetic phase. This stiffening effect is consistent with the mechanical dynamical analysis (DMA) results and is believed to be dominated by an eventual decrease in crystallinity of the poly(caprolactone) phase arisen due to crosslinking and degradation competing phenomena.

SEM Analysis of Tensile Fracture Surfaces

The morphology of the surface fractures produced during the tensile tests performed on the materials before and after

exposure to the different β -radiation doses was analysed by SEM. Figures 1 to 3 present the morphology of fracture surfaces before sterilization and after exposing the samples to a radiation dose of 100 kGy. By this technique is clearly not possible to observe any large differences in the fracture surfaces of both SEVA-C and SCA (Figures 1 and 2, respectively), as function of the radiation dose. However, for SPCL some differences in the fracture behavior are observable (Figure 3). SPCL usually exhibits necking during plastic deformation with significant fibril formation, as it can be seen from Figure 3(a). This deformation behavior is slightly altered upon β -radiation exposure: the necking of SPCL still occurs but without signs of extended fibril formation [Figure 3(b)].

DMA Analysis

Dynamic mechanical analysis (DMA) has been shown by our group to be an adequate technique for the solid-state rheological characterization of new biomaterials.^{9,50,51} In this work both the storage modulus, E' , and the loss factor, $\tan \delta$, were monitored as a function of the temperature for the different materials, subjected to the different β -radiation doses. The corresponding thermograms are shown in Figures 4 to 6.

For all materials $\tan \delta$ is found to vary around 0.1, near body temperature, which indicates that such systems are able

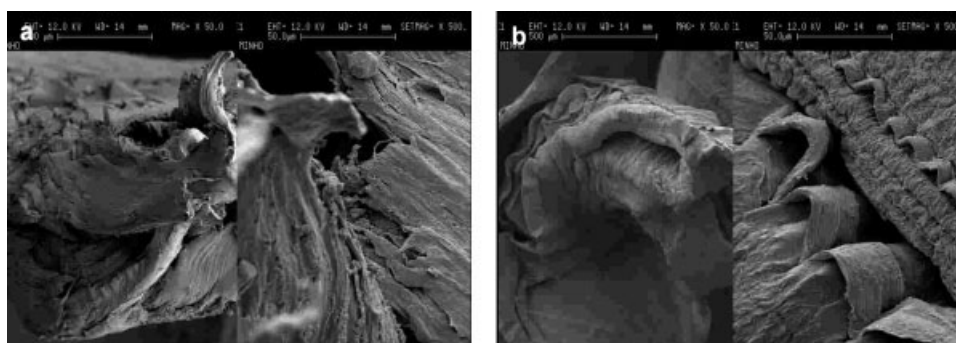


Figure 3. SEM micrographs of the fracture surfaces of SPCL (a) before and (b) after β -sterilization, using a radiation dose of 100 kGy.

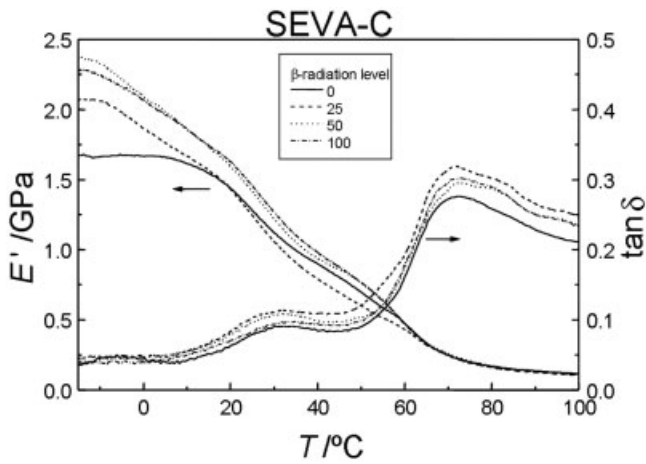


Figure 4. DMA spectrum of SEVA-C before and after being submitted to different doses of β -radiation.

to dissipate a significant fraction of imposed mechanical energy. The values of E' at room temperature are also of the same order of magnitude of the e-modulus (Table I).

SEVA-C presents the most complex behavior among the studied materials. Two clear relaxation processes may be detected in the temperature range analyzed, that contribute for deeper decreases of stiffness during heating. The process at $\sim 30^\circ\text{C}$ has been assigned to the dynamic glass transition of the ethylene-vinyl alcohol copolymer fraction (being specially adequate for dissipating energy near physiological temperature), and the process at $\sim 70^\circ\text{C}$ was ascribed to molecular motions within the starch fraction.^{51,52} The higher temperature peak is also detected in SCA (Figure 5). No appreciable changes are found in the DMA thermogram of SEVA-C. Due to the heterogeneous character of such blends, significant variations are found when one repeats DMA experiments on the same material. Such fluctuations are of the order of the ones observed in the materials that were previously subjected to different levels of β -radiation.

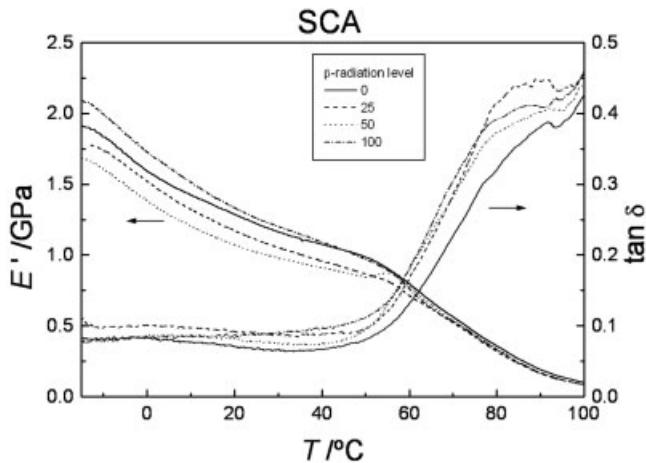


Figure 5. DMA spectrum of SCA before and after being submitted to different doses of β -radiation.

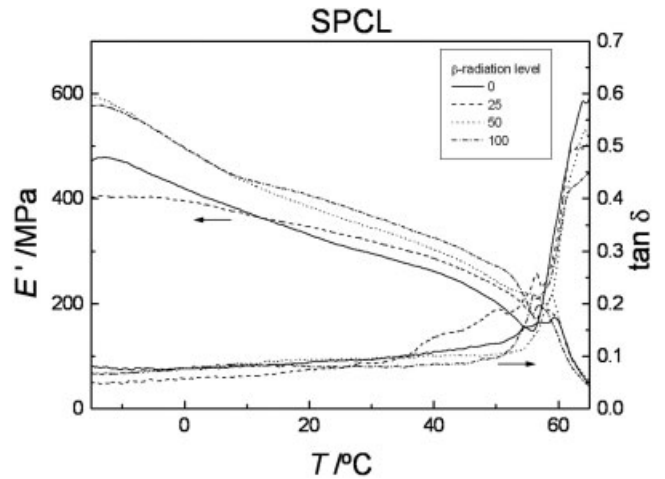


Figure 6. DMA spectrum of SPCL before and after being submitted to different doses of β -radiation.

No appreciable variations are again found in the viscoelastic properties of the SCA biomaterials upon being subjected to β -radiation. One may be tempted herein to ascribe a tendency for increasing $\tan \delta$ with increasing radiation dose.

Regarding the SPCL materials, a peak at $\sim 80^\circ\text{C}$ is not detectable because the poly(caprolactone) melts at $\sim 60^\circ\text{C}$, preventing the DMA study towards higher temperatures. As the glass transition of the synthetic polymer is ca. -35°C , this process is not visible in the studied temperature window. The storage modulus lines (E') appear to indicate that materials stiffen when subjected to β -radiation. This result is consistent with the previously presented tensile test results (Table I) and respective SEM micrographs of the fracture surfaces (Figure 3).

Water-Uptake Ability

Water-uptake studies can give valuable information on the behavior of a biodegradable material in the presence of the body fluids. Figures 7 to 9 show the water-uptake behavior of the materials submitted to different doses of β -radiation,

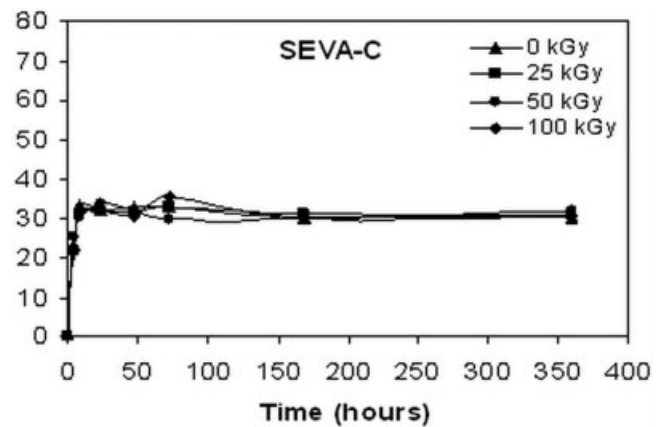


Figure 7. Water uptake of SEVA-C submitted to different doses of β -radiation.

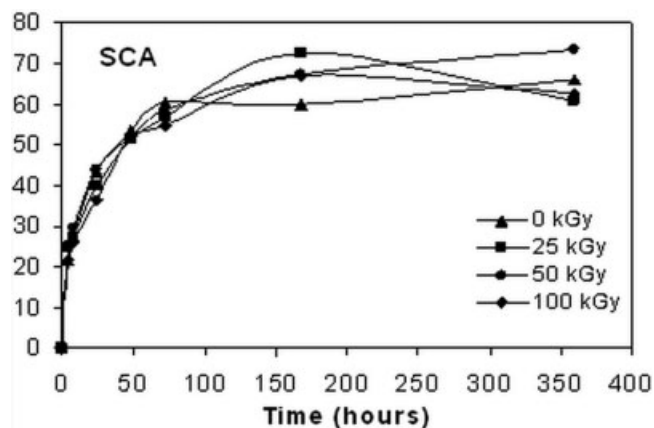


Figure 8. Water uptake of SCA submitted to different doses of β -radiation.

calculated from water-uptake experiments that last up to 15 days.

The degree of equilibrium hydration varies for each type of material. The different results for the degrees of hydration may result from a conjugated effect of: (i) different amounts of starch hydroxyl groups for each material (SEVA-C contains 50% of starch, SCA 50%, and SPCL 30%); (ii) the different hydrophobic/hydrophilic character of the polymers blended with starch in each material; (iii) the type of structure exhibited by each blend. In the case of SEVA-C and SCA, because the amount of starch in the structure is the same, the differences in the degree of hydration may be related with the type of structure that for SEVA-C is an interpenetrated network while in case of SCA is a nonmiscible blend. Consequently, SCA structure is more favorable for water molecules to be absorbed. In case of SPCL, the low degree of hydration can be justified by the presence of lower amounts of starch in the structure and by the hydrophobic character exhibited by the poly(caprolactone).

There is no significant change in the swelling ability of SEVA-C with increasing doses of β -radiation. In the case of

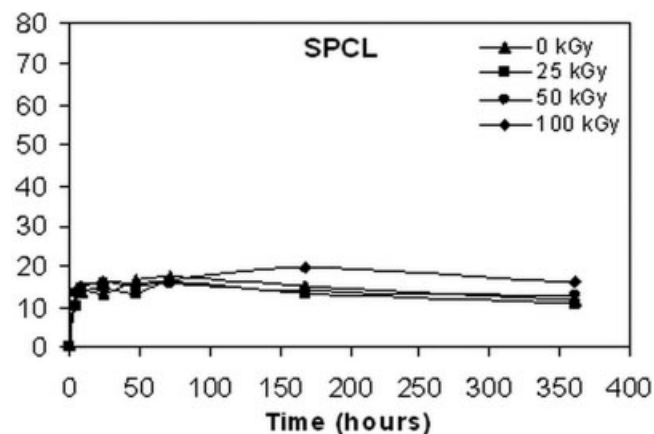


Figure 9. Water uptake of SPCL submitted to different doses of β -radiation.

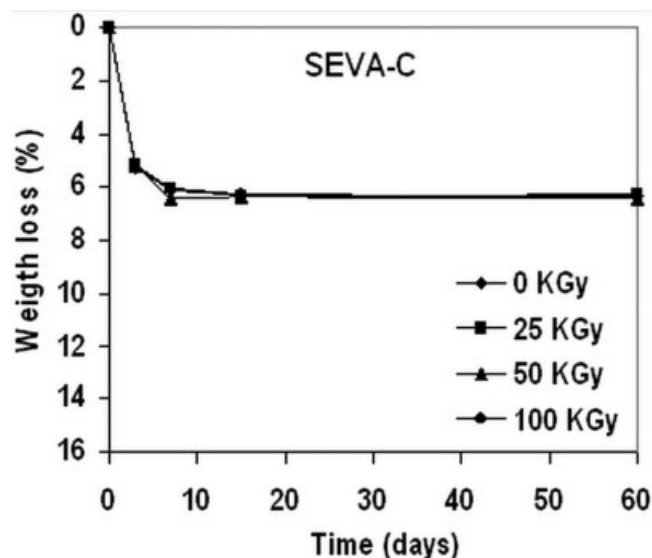


Figure 10. Degradation behavior of SEVA-C with increasing doses of β -radiation.

SCA and SPCL (Figures 8 and 9), there is some increase in the degree of hydration for the higher doses of radiation.

Degradation Behavior

Together with the water-uptake studies, the degradation tests are also very important for predicting the lifetime of a bio-degradable polymer when implanted. Figures 10 to 12 show the weight loss of SEVA-C, SCA, and SPCL materials in an isotonic saline solution at 37°C with immersion time up to 60 days. The differences in the weight loss for each material can be justified by the influence of the same factors that justify the differences in the water-uptake ability, as it has been previously described.

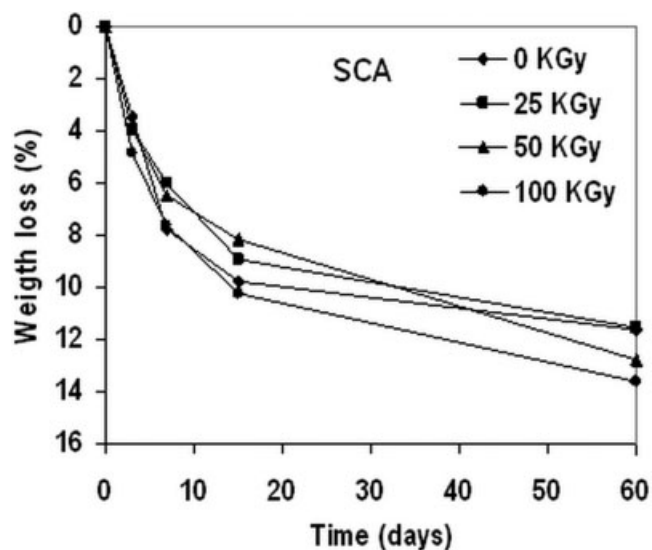


Figure 11. Degradation behavior of SCA with increasing doses of β -radiation.

Figure 10 presents the characteristic degradation profile of SEVA-C material. The amount of weight loss with immersion time was not affected by the radiation doses applied as expected from the results obtained by tensile testing and DMA analysis. For SCA samples (Figure 11), it is possible to observe some increase in the weight loss with increasing doses of radiation, indicating that some degradation is taking place. This increase is more evident after 1 week of immersion in the isotonic saline solution. In case of SPCL (Figure 12), after just 3 days of immersion in the isotonic salt solution, it was possible to observe some increase in the weight loss with increasing doses of radiation indicating that a degradation process is also taking place.

Contact-Angle Measurements

Contact-angle measurements were obtained in order to study the wettability of the different surfaces with increasing doses of β -radiation. Figure 13 represents the water contact angles measured on the different surfaces by the sessile drop technique (using water as testing liquid).

After a 25 kGy dose of radiation, all the materials seem to show a decrease in the contact angle that resulted from an increase in the hydrophilicity of the surfaces. This is particularly evident in case of SCA and SPCL. For radiation doses higher than 25 kGy, the contact angle was not significantly affected, which indicates only 25 kGy are sufficient to induce the modification in the surface. Although the swelling ability of the polymers was not greatly affected by β -radiation, this sterilization method was able to modify the surface by increasing its hydrophilicity. In this way, if we can consider β -radiation as a sterilization method that does not affect significantly the mechanical properties and degradation behavior of the materials, we can also see it as an effective way of modifying the surface for applications where hydrophilic surfaces are desirable. Examples of such applications are

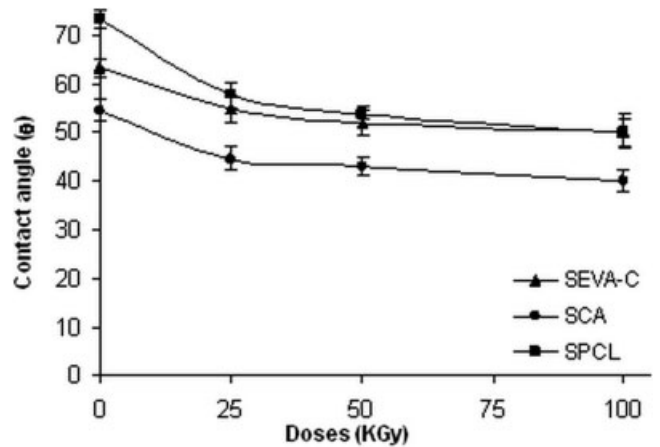


Figure 13. Evolution of the water contact angle with β -radiation doses for the different materials.

surface treatments to enhance cell adhesion and proliferation, and to induce bioactivity as shown in some of our previous works.⁵³

CONCLUSIONS

The main effect of the sterilization method with β -radiation over the starch-based polymers seems to be a surface modification by an increase of the hydrophilicity. However, SCA and SPCL seem to exhibit both higher water-uptake ability and weight loss for the higher doses of radiation, possibly due to some degradation of the polymeric structure. Nevertheless, because β -radiation did not significantly affect the mechanical properties, it can be regarded as an effective way of modifying the surface for applications where more hydrophilic surfaces are desirable.

IonMed Esterilizacion, SA, is acknowledged for performing β -radiation sterilization.

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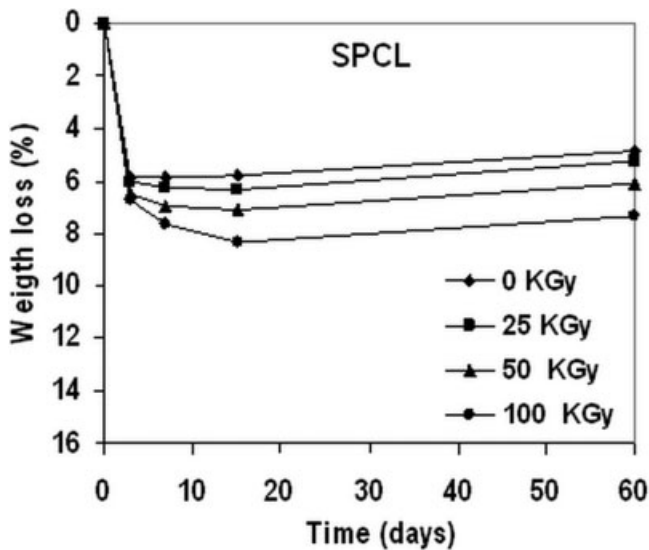


Figure 12. Degradation behavior of SPCL with increasing doses of β -radiation.

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