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High-Performance Catalytic Four-Channel Hollow Fibers with Highly Dispersed Nickel Nanoparticles Prepared by Atomic Layer Deposition for Dry Reforming of Methane

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ABSTRACT: Highly dispersed nickel (Ni) nanoparticles (NPs) with an average particle size of 4.3 nm were uniformly deposited on the outer surface, the inner channel surface, and inside the pores of 20 cm long four-channel α -Al₂O₃ hollow fibers (HFs) by atomic layer deposition (ALD) for dry reforming of methane (DRM). Cerium oxide (CeO₂) was added to promote the catalytic performance of Ni/ Al₂O₃-HF catalysts. Rationally designed filling methods, by tuning the reactor size and inert fillings, can reduce the catalyst bed voidage in a fixed bed reactor for better reactant gas distribution, effectively utilize the Ni reactive sites, and achieve excellent catalytic performance. It was found that the CeO₂-promoted Ni/Al₂O₃-HF catalyst was highly active and highly stable without deactivation during an overall 400-h DRM test at 850 °C. CeO₂ with reversible valence states



could participate in surface reactions; especially, the formation of $CeAlO_3$ provided sufficient surface Ce^{3+} for CO_2 activation and enhanced the stability and reusability of the HF catalysts.

1. INTRODUCTION

With the increasing demand in dealing with CO₂ emission from fossil fuels, industry-scale carbon fixation technology via CO₂ utilization is highly demanded.¹⁻⁴ Dry reforming of methane (DRM) has drawn a great deal of interest from researchers by offering an economically feasible route to deal with the excessive CO₂ emission and converting two greenhouse gases into valuable synthesis gas (syngas).^{1,5} Besides, DRM could effectively utilize the main components $(CH_4 \text{ and } CO_2)$ of biogas from the digestion of biomass and incorporate them into the renewable energy system.⁶⁻⁸ Although DRM has not been applied for industrial applications, DRM exhibits great potential in lowering the CO₂ footprint for decarbonization milestones and producing syngas with a low H_2/CO ratio suitable for C_{5+} production.⁹⁻¹³ Nickel-based catalysts, with low cost and high initial activity, are intensively investigated for DRM,⁹ and the catalytic performance can be further improved by introducing promoters, such as $\text{CeO}_{2^{\prime}}^{14,15}$ MgO,^{16,17} and La₂O₃.¹⁸

For potential industrial application of DRM, a pressure drop in the catalyst bed is directly related to the operating cost and safety of the fixed bed reformer, and thus, the support shape is a very critical factor for DRM catalyst design.^{9,19} The geometric property of multichannel design can allow a much higher throughput rate without causing a corresponding high pressure drop and equipment impairment.⁹ Mathematical modeling demonstrated that the multichannel cylinder-shaped catalyst support could achieve high effectiveness, low pressure drop, and excellent heat transfer performance, as compared to sphere-shaped, cylinder-shaped, or single-channel cylindershaped catalysts.²⁰ Besides, it was reported that a four-channel cylinder-shaped catalyst had the highest methane conversion in the practical DRM test among different shaped catalysts (e.g., sphere, cylinder, trilobe, Raschig ring, and four-channel cylinder).²¹ Due to its high thermal and mechanical stability and strong interaction with Ni nanoparticles, 22,23 Al₂O₃ is commonly used as a support for Ni-based catalysts for the DRM reaction. In this study, a 20 cm long four-channel structured α -Al₂O₃ hollow fiber (HF) was chosen as the catalyst support for the DRM reaction, with a high surface area to volume ratio $(3,000 \text{ m}^2 \text{ m}^{-3})$, which is much higher than that of regular catalyst supports,²⁴ and a low-pressure drop due to its channeling design.

Ultrasmall Ni nanoparticles (NPs) can provide high catalytic activity for DRM and limit the graphitic carbon growth by size limitation.^{1,26} Compared to relatively large Ni NPs prepared by

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traditional liquid methods, atomic layer deposition (ALD) can deposit small Ni NPs uniformly on the Al2O3 substrate. Besides nm-scale or μ m-scale catalyst substrates (e.g., nanoparticles or micron-size particles), only a few works have contributed to extending ALD to mm-level scale or cm-level scale porous substrates, such as flat membranes or HFs.²⁷⁻ Especially, for mm- or cm-scale 3D geometric structures, it would be highly desired to uniformly deposit film or NPs with Ångström level precision on the 3D-structure substrate.³⁰ As for a tubular structure, TiO₂ ALD thin film was uniformly coated on 10 cm long polysulfone HFs in a forced-flow ALD reactor,²⁷ and Al₂O₃ ALD thin film was coated on porous polypropylene hollow fibers for better membrane performance.²⁹ However, ALD has not been applied to deposit active metal NPs onto large complex substrates, such as ceramic HFs with an \sim 20 cm length in this study. It would be important to utilize ALD technology to deposit metal NPs onto large substrates.

In this work, Ni NPs were uniformly deposited on 20 cm long HFs by ALD, followed by the addition of CeO₂ as a promoter using the traditional incipient wetness method to prepare high-performance HF-supported Ni-based catalysts. Multiple 20 cm long hollow fibers were tested for DRM reactions with high gas flow rates. Long-term stability tests of a total of ~400 h at 850 °C were conducted, and the regeneration process for catalyst recycling was studied in detail.

2. EXPERIMENTAL SECTION

2.1. Catalyst Preparation. Four-channel α -Al₂O₃ HFs,²⁵ as shown in Figure 1a, were used as catalyst supports. The HFs had a diameter of \sim 3.36 mm and a length of 20 cm, with a channel diameter of ~0.97 mm. ALD was used to deposit Ni NPs on 20 cm long four-channel α -Al₂O₃ HFs by a homemade ALD reactor, as schematically shown in Figure 1b (details described in our previous work).³¹ Bis(cyclopentadienyl)nickel (NiCp₂, Alfa Aesar) and hydrogen (Airgas, 99.99%) were used as precursors for Ni ALD, and the reaction temperature was set at 300 °C. Several 20 cm long HFs were loaded in the reactor, as shown in Figure 1b. Before ALD, the HFs in the reactor were preheated at 150 °C overnight to remove any moisture adsorbed on HFs. During the first half cycle of Ni ALD, NiCp₂ vapor was delivered into the reactor from a bubbler heated at 85 °C using N₂ as a carrier gas; the dosing time was 600 s for sufficient chemisorption of NiCp2 on the HFs, unless it was specifically mentioned. Then, the hollow fibers underwent a flush in 6 mL min⁻¹ N_2 for 600 s, followed by an evacuation process by a vacuum pump for 10 s. In the second half-reaction of Ni ALD, procedures with the same period were conducted but using H₂ as a precursor to remove the organic ligands left on Ni precursors adsorbed on the substrate surface. In this study, two cycles of Ni ALD were conducted, and the samples were denoted as Ni/Al₂O₃-HF catalysts. The Ni loading was 0.091 ± 0.005 wt %.

The incipient wetness (IW) method was used to introduce CeO₂ onto the Ni/Al₂O₃-HF catalyst. Ce(NO₃)₃·6H₂O (cerium nitrate hexahydrate, Alfa Aesar, 99.99%) was used as the precursor. The Ni/Al₂O₃-HF catalyst was soaked in a $Ce(NO_3)_3$ solution for 1 h, dried at 100 °C under continuous stirring, and then calcined in air at 500 °C for 3 h. The samples were denoted as CeO2-Ni/Al2O3-HF catalysts. The Ce loading was 0.010 wt %.

For X-ray photoelectron spectroscopy (XPS) and hydrogen temperatue-programed reduction (H₂-TPR) analysis, α -Al₂O₃ fillings.



Figure 1. (a) Photo of four-channel α -Al₂O₃ hollow fibers and

schematic images of (b) the ALD reactor system for Ni ALD on

multiple 20 cm hollow fibers with the scheme of HFs loaded in the

ALD reactor and (c) the DRM reactor system and (d, e, f) different

catalyst loading methods for HF supported catalysts: (d) a single HF

catalyst in the 4 mm i.d. quartz tube reactor, (e) three HF catalysts in the 8 mm i.d. quartz reactor without quartz rod fillings, and (f) three

HF catalysts in the 8 mm i.d. quartz tube reactor with quartz rod

nanoparticles were used as catalyst supports. Ni NPs were

deposited by ALD, and CeO₂ was added as the promoter by

the IW method, using the same procedures for HF catalysts.

reforming of methane reaction was carried out in a homemade

2.2. Dry Reforming of Methane Reaction. The dry

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fixed bed catalytic reactor system, as shown schematically in Figure 1c. One tube furnace (Carbolite Gero, Ltd.) was used for heat supply. Mass flow controllers (MKS Instruments) were used to control the gas flow rates. K-type thermocouples (Omega Engineering) were used to measure the temperature inside the quartz tube reactor. A gas chromatograph (SRI 8610C) was used to analyze the compositions of the gas product. A cold trap tank was set to remove any water generated as the byproduct. The reactor pressure was monitored by a pressure gauge and kept constant at atmospheric pressure.

Different catalyst bed filling methods were tested for HFsupported catalysts in DRM reactions, as shown in Figures 1d-1f. A quartz tube with 4 mm i.d. was used to fit a single HF catalyst, as shown in Figure 1d. To accommodate more HFs for scale-up purpose, a quartz tube with 8 mm i.d. was used for three 20 cm HFs, as shown in Figure 1e. Besides, several inert quartz rods were used as fillings for better gas distribution for three 20 cm HF tests in an 8 mm i.d. quartz tube, as shown in Figure 1f.

Before the reaction, the catalyst sample was first reduced in 100 mL min $^{-1}$ 20 vol % $H_2/80$ vol % År at 800 $^{\circ}C$ for 1 h. The temperature ramped to 850 °C at 10 °C min⁻¹ in Ar flow, and then, Ar gas was switched to the reactant gas (50 vol % CH_4 / 50 vol % CO₂) when the temperature reached 850 °C. In this study, the DRM reaction for a certain time without returning to ambient temperature and without regeneration to remove coking was defined as a cycle of DRM reaction. To test the recyclability of the Ni/Al₂O₃-HF catalysts, a regeneration process between cycles of the DRM test consisted of oxidation in 100 mL min⁻¹ 20 vol % $O_2/80$ vol % Ar gas flow at 700 °C for 1 h first and then reduction at 800 °C in 100 mL min⁻¹ 20 vol % $H_2/80$ vol % Ar gas flow for 1 h.

2.3. Catalyst Characterization. Inductively coupled plasma-optical emission spectroscopy (ICP-OES) was applied to analyze the Ni content on the HF catalyst, using 2000D PerkinElmer. H₂SO₄, H₃PO₄, and H₂O₂ were used to digest the HF-supported catalysts for ICP-OES. Transmission electron microscopy (TEM) was applied to measure the size of the deposited Ni NPs using an FEI Tecnai F20 transmission electron microscope. XPS was conducted using a Kratos Axis 165 X-ray photoelectron spectrometer, using monochromatic Al K α as the radiation source. X-ray diffraction (XRD) was conducted using a Philips X-Pert multipurpose diffractometer. H₂-TPR was conducted using a Micromeritics AutoChem II 2920 with 10 vol % $H_2/90$ vol % Ar admix gas from 100 to 900 °C at 10 °C/min. Temperature-programmed oxidation (O₂-TPO) was conducted using the homemade reactor with a QMS200 mass spectrometer (Stanford Research System) in a 10 vol % $O_2/90$ vol % Ar gas mixture from 100 to 900 °C at 10 °C/min.

3. RESULTS AND DISCUSSION

3.1. Deposition of Ni NPs on a 20 cm Long HF by ALD. In our previous study, HFs were broken into short pieces (\sim 0.8 cm long) and then deposited by Ni ALD.³¹ To achieve scale-up production of the ALD-prepared 20 cm long Ni/ Al₂O₃-HF, multiple 20 cm HFs were directly hung in the reactor for Ni ALD, and the dosing time was investigated as an important factor. Figure 2 depicts the effects of the dosing time on Ni loading and catalytic performance of the catalysts for the DRM test. In Figure 2a, for the 20 cm long Al₂O₃-HF support, the Ni loading increased when the dosing time



Figure 2. Effects of the precursor dosing time during Ni ALD on (a) Ni loading of the 20 cm long Ni/Al₂O₃-HF catalyst and (b) CH₄ conversion for the DRM test. Four-cm middle parts from the 20 cm long Ni/Al₂O₃-HF catalyst prepared by ALD were used as catalysts for the DRM reaction. Photos of the cross-sectional surface of the HF cut from the middle part of the 20 cm long Ni/Al₂O₃-HF with Ni ALD dosing times of (c) 600 s and (d) 120 s.

increased from 120 to 240 s, and the Ni loading reached a constant value when the dosing time further increased from 560 to 720 s. The increase of Ni loading with the increase of the dosing time indicated that the substrate surface was not saturated with the Ni precursor, so NiCp₂ continued to react with surface hydroxyl groups until the chemisorption of NiCP₂ on the Al₂O₃-HF surface was saturated.^{32,33} Besides, the catalytic performance of the catalysts exhibited a similar tendency as the Ni loading increased, as shown in Figure 2b and Figure S1. Notably, there is no such trend for Ni loading

on the 0.8 cm Al₂O₃-HF vs the ALD precursor dosing time. Very similar Ni loading values were found for Ni ALD on the 0.8 cm Al₂O₃-HF as the precursor dosing time increased, indicating that the saturation of NiCp₂ on the 0.8 cm Al₂O₃-HF was much quicker than that on the 20 cm long Al₂O₃-HF even with a shorter precursor dosing time. For Ni ALD scalingup from the 0.8 to 20 cm Al₂O₃-HF support, the longer hollow fibers required a longer precursor dosing time to reach the saturation state for the chemisorption because of the longer diffusion length in the long HFs; a longer saturation time could be needed for the upper part of the 20 cm Al₂O₃-HF because the NiCp₂ precursor entered the ALD reactor from the bottom. Ascribed to the self-limiting nature of ALD, the chemisorption of NiCP₂ could be saturated once the surface sites were occupied when the dosing time was sufficient, and thus the geometric difference would not lead to partial accumulation, resulting in a uniform and repeatable deposition of Ni NPs.

Figures 2c and 2d exhibit the morphology of the HF catalysts that were cut from the 20 cm long Ni/Al₂O₃-HF catalysts. For the 20 cm Ni/Al₂O₃-HF with a dosing time of 120 s, the inner channel was almost white (the same color as the Al_2O_3 HF support), while the outer surface was gray, indicating that the low dosing time was not enough for the precursor to diffuse into the inner channel, especially for the 20 cm long HFs. In contrast, for the 20 cm Ni/Al₂O₃-HF with a dosing time of 600 s, both the HF surface and the inner channel surface are gray, which resulted from the full saturation of both outer and inner surfaces with a long precursor dosing time. Besides, the cross-section of the 20 cm Ni/Al₂O₃-HF with a dosing time of 600 s was also gray, the same as that of the inner channel and outer surface. During the ALD process, the precursor molecules could not only enter the inner channel from both ends of the hollow fibers but also diffuse into the inner channel from the outer surface via the pore of hollow fibers (~0.9 μ m²⁵). These Ni NPs in the pores would be accessible for the reactant gases during DRM.

Different techniques were used to verify the uniformity of Ni NPs deposited on HF substrates. As shown in Figure 3, the ALD-prepared 20 cm Ni/Al_2O_3 -HF was uniformly gray, as



Figure 3. (a) Photos of the 20 cm long Ni/Al₂O₃–HF after 2 cycles of Ni ALD and (b) the STEM image of the ALD-prepared Ni/Al₂O₃–HF. (c) Ni ICP-OES results of ALD-prepared Ni/Al₂O₃–HF catalysts from one batch of Ni ALD.

compared to the white fresh HFs (Figure 1a), indicating the uniform deposition of Ni NPs by ALD. The Ni/Al₂O₃-HF catalysts were also checked by TEM, as shown in Figure 3b. The average size of Ni NPs was about 4.3 nm, with high and uniform Ni dispersion. In addition, ICP-OES results in Figure 3c indicate that the Ni loadings on different HFs were similar for the same batch of ALD-prepared 20 cm long Ni/Al₂O₃-HFs.

To indirectly check whether Ni NPs were uniformly deposited on 20 cm long HFs, one 20 cm long Ni/Al₂O₃– HF was broken into three pieces, i.e., upper part, middle part, and lower part. Each piece was about 4 cm long and was tested for the DRM reaction. The DRM results are shown in Figure 4.



Figure 4. (a) Ni loading, (b) CH_4 conversion, (c) CH_4 reforming rate, and (d) H_2/CO ratio using a 4 cm upper part, a 4 cm middle part, and a 4 cm lower part (cut from a 20 cm long Ni/Al₂O₃-HF prepared by ALD) for the DRM test in a quartz tube reactor with 4 mm i.d.

Each piece from different parts of one single 20 cm long HF exhibited similar methane conversion, methane reforming rates, and H_2/CO ratio for the DRM test, which confirmed that the ALD process could uniformly deposit Ni NPs on multiple 20 cm long hollow fibers. In this study, the 20 cm long HFs were hung vertically in a vertical ALD tube reactor, and the precursors were fed from the bottom of the reactor; the saturation of precursor adsorption on the HFs' surface could be achieved so that the effects of position difference of HFs were not that significant, which was ascribed to the self-limitation and self-termination nature of the ALD process. In one word, ALD could be upscaled to prepare multiple 20 cm long HF catalysts with excellent uniformity and high dispersion of Ni NPs.

3.2. Effects of the Filling Method of HF-Supported Catalysts. The filling method of the catalyst bed could be an important factor for the DRM test. As shown in Figure 5 and Figure S2, three types of bed filling methods for HF catalysts in a quartz tube reactor were studied. Notably, the different filling methods of HF-supported Ni catalysts resulted in different catalytic performances, and the addition of CeO₂ as the promoter significantly improved the activity for the Ni/Al₂O₃— HF catalyst, which will be discussed in the next section. For the filling method, it could be seen that the best performance was achieved by loading a single Ni/Al₂O₃—HF or CeO₂—Ni/ Al₂O₃—HF in a 4 mm i.d. quartz tube with a minimum void between the reactor and HF, with ~95% CH₄ conversion at



Figure 5. CH₄ conversion and voidage of the cross-section area of the catalyst bed for different catalyst bed filling methods of 20 cm Ni/Al₂O₃-HFs and 20 cm CeO₂-Ni/Al₂O₃-HFs for DRM at 850 °C at GHSV of 2,850 \pm 50 L_{CH₄} g_{Ni}^{-1} h⁻¹.

gas hourly space velocity (GHSV) of about 2,850 $L_{CH_4} \ {g_{Ni}}^{-1}$ h⁻¹, whereas three packed 20 cm CeO₂–Ni/Al₂O₃–HFs showed a comparable conversion of ~93% in an 8 mm i.d. quartz tube with inert quartz rod fillings between HFs. For three 20 cm CeO₂–Ni/Al₂O₃–HFs, the conversion was ~89% without any inert fillings, as compared to ~93% of the case with inert fillings.

The voidage of the catalyst bed, which is defined as the proportion of the unoccupied volume in a catalyst bed,²¹ is considered an important factor for the filling method. Take the Ni/Al_2O_3 -HF as an example, the least bed voidage at 0.47 and the highest methane conversion at 94.6% were achieved for a single HF in a 4 mm i.d. quartz tube. Using the same three 20 cm Ni/Al₂O₃-HFs inside an 8 mm i.d. quartz tube reactor, a voidage of 0.52 and a methane conversion of 89.5% were achieved with the usage of inert fillings, whereas a higher voidage of 0.64 and a lower methane conversion of 87% were achieved without any inert fillings. As discussed in the previous section, Ni NPs prepared by ALD were deposited everywhere on the porous HF support, including the outer surface, the inner surface, and inside the pores of the HFs. The inert quartz rod fillings can prevent gas "bypass" and distribute/drive the reactant gas into the inner channel and the pores of HFs. The irrational catalyst bed design might lead to an unbalanced reactant gas distribution, and some Ni sites surrounding more void areas might need to catalyze more reactant gas, whereas some Ni sites might only catalyze a few molecules of reactant gases and not be efficiently utilized. For instance, for the three 20 cm HFs without inert fillings, the Ni sites of one upper HF would catalyze more reactant gas, whereas the lower two would catalyze less reactant gases, similar to the "bypass". By rationally filling the catalyst bed, the voidage could be effectively reduced, therefore increasing the contact between gas and catalyst and increasing overall reactant conversion.

3.3. CeO₂-Promoted Ni/Al₂O₃-HF Catalysts. To prepare a high-performance Ni/Al₂O₃-HF catalyst, CeO₂ was used as a promoter to enhance the catalytic performance. One single 20 cm Ni/Al₂O₃-HF catalyst and one single 20 cm CeO₂-Ni/Al₂O₃-HF catalyst were tested at 850 °C for DRM in a 4 mm i.d. quartz tube. As shown in Figure 6, during 48 h of the DRM reaction, both the Ni/Al₂O₃-HF and CeO₂-Ni/Al₂O₃-HF exhibited methane conversion around ~95% and a H₂/CO ratio around 0.97. Ni/Al₂O₃-HF exhibited a gradual



Figure 6. (a) CH₄ conversion and (b) H₂/CO ratio during the DRM reaction using a single 20 cm Ni/Al₂O₃-HF and a single 20 cm CeO₂-Ni/Al₂O₃-HF in a 4 mm i.d. quartz tube at 850 °C. GHSV = 2,850 $L_{CH_4} g_{Ni}^{-1} h^{-1}$ with a total flow rate of 220 mL min⁻¹.

deactivation behavior, with methane conversion decreasing from 94.7% to 88.4% within 48 h of the reaction. In contrast, the CeO₂-Ni/Al₂O₃-HF had an activation behavior in the initial 20 h, from 88.4% to 95.3%, which could be ascribed to further reduction of Ni(II) to active Ni(0) sites due to the presence of CeO₂. Besides, the H₂/CO ratio also increased from 0.94 to 0.97 due to the activation behavior. As shown in Table 1, the activity of the CeO₂-Ni/Al₂O₃-HF in this work exhibited great activity, compared to some other highperformance catalysts from the literature. After 20 h of the DRM reaction, the methane conversion of the CeO₂-Ni/ Al₂O₃-HF was highly stable, indicating that CeO₂ could significantly enhance the stability of the Ni/Al₂O₃-HF during DRM conditions, in terms of coke formation or sintering.

To get insight into the effects of CeO₂ for the enhancement of the catalytic performance, the Ni/Al₂O₃–HF and CeO₂– Ni/Al₂O₃–HF catalysts were tested under different values of GHSV, as shown in Figure 7 and Figure S3. At low GHSV (~830 $L_{CH_4} g_{Ni}^{-1} h^{-1}$), the Ni/Al₂O₃–HF and CeO₂–Ni/ Al₂O₃–HF exhibited identical conversion of ~96% with the H₂/CO ratio at ~0.97, which was close to the equilibrium conversion. At GHSV of ~1,660 $L_{CH_4} g_{Ni}^{-1} h^{-1}$, the CH₄ conversion of the CeO₂–Ni/Al₂O₃–HF still reached the equilibrium conversion (~96%) with the H₂/CO ratio at ~0.97, whereas the conversion of the Ni/Al₂O₃–HF decreased to ~92% with the H₂/CO ratio at 0.96, indicating a higher reaction rate of the CeO₂–Ni/Al₂O₃–HF. At a higher value of

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Гаb	le 1.	Comparison	of the	Catalytic	: Per	formance	for	DRM i	in Th	is V	Vork	and	the	Literature	
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catalyst	preparation method	GHSV, mL/g _{cat} /h	temp, °C	$X_{{ m CH}_4\prime}$ %	$r_{\rm CH_4}$, $\rm L_{\rm CH_4}/g_{\rm Ni}/h$	ref
CeO ₂ -Ni/Al ₂ O ₃ -HF	ALD	6,500	850	95	2,700	this work
Ni/Al ₂ O ₃	ALD	36,000	850	97	1,840	34
Ni/Al ₂ O ₃ -ZrO ₂	impregnation+ plasma	60,000	850	94.5	285	35
Ni/ZSM-5	impregnation	12,000	800	95	114	36
$Ni/Ce_{0.2}Zr_{0.8}O_2$	coprecipitation	216,000	800	92	442	37
Ni-Mo/SBA-15-La ₂ O ₃	impregnation	12,000	800	98	120	38
MgO-Ni/SBA-15	impregnation	36,000	800	97	175	39
Ni-Ce/Mg-Al-O	impregnation	72,000	800	93	280	40
Ni-Zr/MCM-41	coprecipitation	50,000	800	95	590	41
Ni-CaO-ZrO ₂	coprecipitation	158,000	850	90	430	42



Figure 7. CH₄ conversion as a function of GHSV for DRM reactions using three HFs of a 20 cm long Ni/Al₂O₃-HF and three HFs of a 20 cm CeO₂-Ni/Al₂O₃-HF for DRM at 850 °C.

GHSV, the effect of equilibrium was less significant, and therefore, the CeO₂–Ni/Al₂O₃–HF exhibited higher activity than that of the Ni/Al₂O₃–HF. For instance, at GHSV of ~2,980 $L_{CH_4} g_{Ni}^{-1} h^{-1}$, the CH₄ conversion of the CeO₂–Ni/Al₂O₃–HF reached ~88% with the H₂/CO ratio at ~0.94, as compared to the CH₄ conversion at ~83% and the H₂/CO ratio at ~0.92 of the Ni/Al₂O₃–HF. In short, CeO₂ could significantly improve the activity of the Ni/Al₂O₃–HF catalyst for DRM.

To study the effects of CeO₂ on the chemical states of the Ni element, Figure 8a illustrates the Ni 2p 3/2 XPS spectra of the reduced Ni/Al₂O₃ and reduced CeO₂-Ni/Al₂O₃ catalysts. All XPS spectra were calibrated at 284.5 eV using the adventitious carbon in C 1s (as shown in Figure S4). Ni could be deconvoluted into various species, with the metallic Ni peak located at ~852.0 eV, NiO located at ~854.4 eV, and NiAl₂O₄ located at ~856.4 eV. Besides, due to the shakeup phenomena of the peaks, the satellite peaks of Ni(0) and Ni(II) were located at ~857.9 eV and ~861.3 eV, respectively.43 Among the Ni species, the spinel NiAl₂O₄ was highly stable, even under highly reductive, high-temperature DRM reaction conditions, and the existence of NiAl₂O₄ indicated that the interaction between NiO and Al₂O₃ in the ALD-prepared Ni/ Al_2O_3 catalyst was too strong to be completely reduced to active metallic Ni sites.^{22,44} Compared to the reduced Ni/ Al₂O₃ catalyst, the reduced CeO₂-Ni/Al₂O₃ catalyst exhibited a smaller amount of NiAl₂O₄ and more metallic Ni in the XPS spectra, which indicated that CeO₂ could improve the



Figure 8. (a) XPS spectra of Ni 2p3/2 core levels of reduced Ni/ Al_2O_3 and reduced CeO_2 -Ni/ Al_2O_3 and (b) the H_2 -TPR profiles of the Ni/ Al_2O_3 and CeO_2 -Ni/ Al_2O_3 .

reducibility of $NiAl_2O_4$ and release more active metallic Ni sites from $NiAl_2O_4$.

H₂-TPR in Figure 8b was conducted to determine the interaction between Ni and the support. Generally, the peaks for the Ni/Al₂O₃ system could be assigned to NiO (free from Al₂O₃) at ~400 °C, NiO-Al₂O₃ (NiO interacted with Al₂O₃) at 500–700 °C, and spinel NiAl₂O₄ at 800 °C, respectively.^{22,45} In our previous work, the interaction between NiO and Al₂O₃ for the Ni/Al₂O₃ catalyst prepared by ALD was observed due to its unique chemisorption-based growth.³⁴ As shown in Figure 8b, it would be seen the H₂-TPR profile in the Ni/Al₂O₃ ranged from 240 to 850 °C, which indicated there were

various species, including NiO, NiO-Al₂O₃, and NiAl₂O₄. For CeO₂-Ni/Al₂O₃, the H₂-TPR profile ranged from 210 to 830 °C, including NiO, NiO-Al₂O₃, and NiAl₂O₄. The lower reduction temperature indicated the CeO₂ enhanced the overall reducibility of the catalyst. Besides, it can be seen that there was less NiAl₂O₄ for CeO₂-Ni/Al₂O₄, meaning that CeO₂ could effectively assist the reduction of NiAl₂O₄ and keep Ni in a metallic state during DRM.

The morphology and lattice structure of the spent catalysts, i.e., Ni/Al_2O_3 -HF and CeO_2 -Ni/Al_2O_3-HF, were checked by STEM and XRD, as shown in Figure 9 and Figure S5. In



Figure 9. STEM images of the (a) spent Ni/Al₂O₃–HF and (b) spent CeO₂–Ni/Al₂O₃–HF catalysts.

TEM images, it could be seen that the spent Ni/Al₂O₃-HF catalyst had an average Ni particle size of 18.9 ± 4.8 nm, whereas the spent CeO₂-Ni/Al₂O₃-HF catalyst had an average Ni particle size of 16.4 ± 3.3 nm. The smaller average Ni particle size of the spent CeO₂-Ni/Al₂O₃-HF indicated that CeO₂ could also effectively inhibit the sintering of Ni NPs and enhance the stability of the catalyst during DRM reaction.

3.4. Long-Term Stability and Regeneration Tests. To scale up the DRM test with multiple HFs, three pieces of 20 cm long CeO_2-Ni/Al_2O_3-HF catalysts were tested in terms of stability and recyclability. Quartz rod fillers were applied to minimize the voids between CeO_2-Ni/Al_2O_3-HF catalysts. The results are shown in Figure 10. In this test, the total flow rate reached 660 mL min⁻¹, at GHSV of 2,540 $L_{CH_4} g_{Ni}^{-1} h^{-1}$. For the first cycle of DRM, the reactant gases were 660 mL min⁻¹ (50 vol % CH₄/50 vol % CO₂). There was an obvious activation process in the initial 15 h of reaction, since the CH₄ conversion increased from 78% to 93% gradually. During the following 200 h of the test, notably, no deactivation was observed, indicating that the CeO_2-Ni/Al_2O_3-HF catalyst was highly stable for the DRM reaction.

To further investigate the stability and the recyclability of the catalyst, the CeO₂–Ni/Al₂O₃–HF catalyst underwent a regeneration process (first oxidized in 100 mL min⁻¹ 20 vol % O₂/80 vol % Ar gas flow at 700 °C for 1 h and then reduced at 800 °C in 100 mL min⁻¹ 20 vol % H₂/80 vol % Ar gas flow for 1 h), and then, it was tested under an even higher gas flow rate of 880 mL min⁻¹, at GHSV of 3,400 $L_{CH_4} g_{Ni}^{-1} h^{-1}$. Due to the much higher flow rate of feed gases, a lower CH₄ conversion of ~81% was observed; there was no catalytic activity loss during this 400-h test including 200 h before regeneration and 200 h after regeneration. The same catalyst underwent another regeneration process, and then, it was tested for the third cycle of DRM at 2,540 $L_{CH_4} g_{Ni}^{-1} h^{-1}$ and 3,400 $L_{CH_4} g_{Ni}^{-1} h^{-1}$ to test the catalyst recyclability. The same CH₄ conversion and the same product composition (H₂/CO ratio of ~0.96 at 2,540

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Figure 10. (a) CH₄ conversion and (b) H₂/CO ratio of the CeO₂– Ni/Al₂O₃–HF catalyst in gas flow for the long-term stability DRM test at 850 °C: the first cycle of DRM reaction at GHSV of 2,540 L_{CH₄} g_{Ni}^{-1} h⁻¹, the second cycle at GHSV of 3,400 L_{CH₄} g_{Ni}^{-1} h⁻¹, and the third cycle of DRM reaction at GHSV of 2,540 L_{CH₄} g_{Ni}^{-1} h⁻¹ or 3,400 L_{CH₄} g_{Ni}^{-1} h⁻¹.

 $L_{CH_4}~g_{Ni}^{-1}~h^{-1}$ and ~0.94 at 3,400 $L_{CH_4}~g_{Ni}^{-1}~h^{-1})$ were obtained, as compared to the results of the first cycle and second cycle of the DRM tests. Therefore, the CeO₂-promoted catalyst exhibited superior stability and recyclability for the DRM tests.

CeO2 greatly enhanced the stability of the pristine Ni/ Al₂O₃-HF catalyst and the regenerated catalyst for DRM, and no activity loss was found for the regenerated CeO₂-Ni/ Al₂O₃-HF. To get insight into catalyst regeneration, XPS was applied using the CeO₂-Ni/Al₂O₃ catalyst at different states, including reduced (the fresh catalyst underwent H2-treatment), spent (the reduced catalyst further underwent DRM), oxidized (the spent catalyst further underwent oxidation), and regenerated (the oxidized catalyst further underwent H₂treatment). For Ce 3d profiles in Figure 11a, Ce⁴⁺ includes Ce 3d5/2 peaks (v at 881.9 eV, v'' at 886.2 eV, and v''' at 897.8 eV) and Ce 3d3/2 peaks (u at 900.5 eV, u'' at 904.8 eV, and u'' at 916.3 eV), whereas Ce³⁺ includes Ce 3d5/2 peaks (v_o at 880.8 eV and v' at 884.6 eV) and Ce 3d3/2 peaks (u_o at 899.1 eV and u' at 903.1 eV).^{46,47} Notably, the Ce element exhibited changeable chemical states, indicating that CeO₂ was not inert in the redox atmosphere and might participate in surface reactions.^{47,48} The reversible oxidation state of Ce can achieve oxygen storage capacity and assist the oxygen transfer for catalytic reactions; therefore, the chemical state of Ce plays an



Figure 11. XPS spectra of (a) Ce 3d and (b) O 1s core levels of reduced CeO₂-Ni/Al₂O₃, spent CeO₂-Ni/Al₂O₃, oxidized CeO₂-Ni/Al₂O₃, and regenerated CeO₂-Ni/Al₂O₃.

important role in the catalytic reaction. Especially, CeO_x can interact with Al₂O₃ under a reductive atmosphere at high temperature (T > 500 °C), when Al³⁺ ions diffuse into the vacant sites of the CeO_x lattice at the CeO_x-Al₂O₃ interface, and CeAlO₃ will be favorably formed, 45,48,49 providing more Ce³⁺ than CeO₂ does. 45,48,49 For this work, a high concentration of Ce³⁺ was observed for the reduced or regenerated CeO₂-Ni/Al₂O₃ with a high Ce³⁺ ratio (ν_0 % + $v'\% + u_0\% + u'\%$) at ~39% and a low Ce⁴⁺ diagnostic peak (u'''%) at ~3%, which were close to the reported values of CeAlO₃ but far from that of CeO₂ only.⁵⁰⁻⁵² Under this circumstance, the catalytic activity of the regenerated catalyst could be highly repeatable because of the reversible form of CeAlO₃ at the reductive atmosphere and CeO₂-Al₂O₃ mixed oxides at the oxidative atmosphere. In addition, the chemical states of oxygen species are shown in Figure 11b. It could be seen that the reduced and regenerated CeO₂-Ni/Al₂O₃ had more surface oxygen sites, which means that there were more coordinatively unsaturated oxygen sites or oxygen vacancy sites. The oxygen species under different chemical states also confirmed the variant roles of CeO₂ that participated in the catalytic surface reactions. During the DRM reaction, CeAlO₃ will act as CO_2 adsorption sites and participate in CO_2

dissociation, which helps store O-species originated from CO_2 and transfers O-species to the adsorbed CH_x for the DRM reaction. The enhanced CO_2 activation would benefit the DRM reaction and decrease the carbon formation, which was also demonstrated by O_2 -TPO (Figure S6) that CeO_2 could strongly suppress the carbon formation.

4. CONCLUSIONS

In this work, Ni NPs were deposited on 20 cm long fourchannel α -Al₂O₃ HFs by ALD for DRM. With a longer precursor dosing time during ALD than that for 0.8 cm long HFs, Ni NPs with an average particle size of 4.3 nm could be uniformly dispersed on the porous 20 cm long HF surfaces, including the inner channel surface, pores, and outer surface, whereas ALD with a short precursor dosing time could mainly deposit Ni NPs on the outer surface of HFs. The uniform deposition of Ni NPs was verified by TEM, ICP-OES, and catalytic testing of the catalysts from different parts of a single HF. Reducing the voidage of a catalyst bed, by adjusting the reactor tube size or adding inert fillings, can better distribute gas flow to achieve higher catalytic performance for DRM. It was found that a single HF catalyst in a 4 mm i.d. quartz tube reactor exhibited the best performance, and the three-packed 20 cm long CeO₂-Ni/Al₂O₃-HF showed comparable 93% conversion with inert quartz rods as filling in a quartz tube with an 8 mm i.d. A DRM test of three-packed 20 cm long CeO₂-Ni/Al₂O₃-HF catalysts exhibited excellent performance (93% conversion) at harsh conditions (850 °C, 660 mL min⁻¹ 50 vol % $CH_4/50$ vol % CO_2 mixture), and no deactivation was observed for a 200-h DMR test followed by another 200-h test after catalyst regeneration. CeO₂ exhibited different valence states in the reductive/oxidative atmosphere. The formation of CeAlO₃ under H_2 atmosphere at the CeO_x-Al₂O₃ interface could stabilize Ce³⁺ and provide sufficient surface Ce³⁺, which could serve as active sites for CO₂ activation and enhance the catalytic performance.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.iecr.1c03705.

 H_2/CO ratio of activity test and stability test, XPS spectra of reduced and spent catalysts, XRD profiles of spent catalysts, and O₂-TPO profiles of spent catalysts (PDF)

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Notes

The authors declare no competing financial interest.

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