

MARKOV CHAIN-BASED COST-OPTIMAL CONTROL CHARTS FOR HEALTHCARE DATA

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ABSTRACT

Control charts have traditionally been used in industrial statistics, but are constantly seeing new areas of application, especially in the age of Industry 4.0. This paper introduces a new method, which is suitable for applications in the healthcare sector, especially for monitoring a health-characteristic of a patient. We adapt a Markov chain-based approach and develop a method in which not only the shift size (i.e. the degradation of the patient's health) can be random, but the effect of the repair (i.e. treatment) and time between samplings (i.e. visits) too. This means that we do not use many often-present assumptions which are usually not applicable for medical treatments. The average cost of the protocol, which is determined by the time between samplings and the control limit, can be estimated using the stationary distribution of the Markov chain.

Furthermore, we incorporate the standard deviation of the cost into the optimisation procedure, which is often very important from a process control viewpoint. The sensitivity of the optimal parameters and the resulting average cost and cost standard deviation on different parameter values is investigated. We demonstrate the usefulness of the approach for real-life data of patients treated in Hungary: namely the monitoring of cholesterol level of patients with cardiovascular event risk. The results showed that the optimal parameters from our approach can be somewhat different from the original medical parameters.

KEYWORDS: control chart; cost-effectiveness; Markov-chain; healthcare

1 INTRODUCTION

Statistical process control, and with it control charts enjoy a wide range of use today, and have seen great developments, extensions and generalisations since the original design of Shewhart.¹ This proliferation of methods and uses can at part be attributed to the fact that information is becoming available in ever increasing quantities and in more and more areas.

Even though control charts have originally been designed with statistical criteria in mind, the development of cost-efficient control charts also began early. Duncan in his influential work from 1956 developed the basis for a cycle based cost-effective control chart framework which is still very popular today and is implemented in statistical software packages such as in R.²⁻⁴ Cost-efficient solutions are often the focus in industrial and other settings besides statistical optimality.

Statistical process control, including control charts can be found in very different environments in recent literature. For example in mechanical engineering, e.g. Zhou et al.,⁵ where the authors develop a T^2 bootstrap control chart, based on recurrence plots. Another example is the work of Sales et al.⁶ at the field of chemical engineering, in their work they use multivariate tools for monitoring soybean oil transesterification. It is not a surprise that the healthcare sector has seen an increased use of control chart too. Uses within this sector range from quality assurance to administrative data analysis and patient-level monitoring, and many more.^{7,8} In one example control charts were used as part of system engineering methods applied to healthcare delivery.⁹ Other examples include quality monitoring in thyroid surgery,¹⁰ monitoring quality of hospital care with administrative data¹¹ and chronic respiratory patient control.¹²

Cost-efficient control charts have not been widely used in healthcare settings, but there are some examples which deal with cost monitoring and management. In one work \bar{X} and R charts were used to assess the effect of a physician educational program on the hospital resource consumption.¹³ Another article is about a hospital which used control charts for monitoring day shift, night shift and daily total staffing expense variance, among other variables.¹⁴ Yet another paper documents a case study about primary care practice performance, where control charts were used to monitor costs associated with provider productivity and practice efficiency. Further costs monitored were net patient revenue per relative value unit, and provider and non-provider cost as a percent of net revenue.¹⁵ Even though these studies used control charts for cost monitoring or optimisation purposes, they did not deal with the same problems as this paper, as our method focuses on cost-optimisation by finding the optimal parameters of the control chart setup.

The aim of this study is to present a cost-efficient control chart framework which was specifically designed with use on healthcare data in mind. Specifically, we would like to use control charts for the purposes of analysing and controlling a healthcare characteristic of a patient over time, such as the blood glucose level. Traditionally, the minimal monitoring and process cost is achieved by finding the optimal parameters, namely the sample size, time between samplings and critical values.¹ If one desires to find the optimal parameters for a cost-optimal control chart for a healthcare process, then the proper modelling of the process is critical, since if the model deviates greatly from reality, then the resulting parameters and costs may not be appropriate. Of course this presents several problems as certain typical assumptions in control chart theory will not hold for these kind of processes. Namely the assumption of fixed and known shift size, which is problematic because healthcare processes can often be drifting in nature and can produce different shift sizes. Another assumption is the perfect repair, which in this case means that the patient can always be fully healed, which is obviously often impossible. Lastly, the time between shifts is usually set to be constant, but in a healthcare setting with human error and non-compliance involved, this also needs to be modified. Furthermore, since these processes can have undesirable erratic behaviour, the cost standard deviation also needs to be taken into account besides the expected cost.

The control chart design which is presented here for dealing with these problems is the Markov chain-based framework. This framework was developed by Zempléni et al. in 2004 and was successfully applied on data collected from a Portuguese pulp plant.¹⁶ Their article provided suitable basis for generalisations. Cost-efficient Markov chain-based control charts build upon Duncan's cycle based model, as these also partition the time into different segments for cost calculation purposes. The previ-

ous paper from 2004¹⁶ has already introduced the random shift size element, in this paper we expand upon that idea and develop further generalisations to create cost-efficient Markov chain-based control charts for healthcare data.

The article is organized in the following way: Section 2 starts with basic definitions and notions needed to understand the more complicated generalisations. Subsection 2.2 discusses the mathematics behind the aforementioned new approaches in the Markov chain-based framework. Subsection 2.3 deals with the problems introduced by discretisation - which is needed for the construction of the transition matrix - and also explains the calculation of the stationary distribution, and defines the cost function. Analysis of results and examples will be provided with the help of program implementations written in R. Section 3 shows an example of use for the new control chart methods in healthcare settings. This example involves the monitoring of low-density lipoprotein levels of patients at risk of cardiovascular events. Section 4 concludes the theoretical and applied results.

2 METHODS

The methods and R implementation in this paper largely depend on the works of Zempléni et al. The first part of this section gives a brief introduction to the methods used in their paper.¹⁶

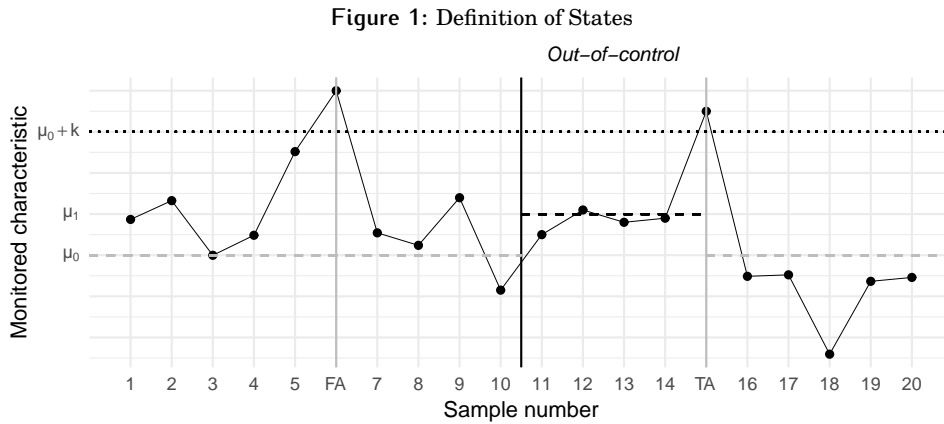
2.1 The Markov-chain-based Framework

Consider a process which is monitored by a control chart. We will show methods for processes which can only shift to one (positive) direction, monitored by a simple X -chart, with sample size $n = 1$. This aims to model the monitoring of a characteristic where the shift to only one direction is interesting or possible, and the monitoring is focused at one patient at a time. Several assumptions are made for the base model. The process distribution is normal with known parameters μ_0 and σ . We will denote its cumulative distribution function by ϕ . The shift intensity $1/s$ is constant and known and the shift size δ^* is fixed. It is also assumed that the process does not repair itself, but when repair is carried out by intervention, it is perfect. The repair is treated as an instantaneous event. All costs related to repairing should be included in the repair cost, for example if a major repair entails higher cost, then this should also be reflected in the calculation. The time between shifts is assumed to be exponentially distributed. The above assumptions ensure that the probabilities of future transitions are only dependent on the current state. This is the so-called Markov property, and the model under consideration is called a Markov chain. The states of this Markov chain are defined at the sampling times and the type of the state depends on the measured value and the actual (unobservable) background process, namely whether there was a shift from the target value in the parameter. This way four basic state types are defined:

- No shift - no alarm: in-control (INC)
- Shift - no alarm: out-of-control (OOC)
- No shift - alarm: false alarm (FA)
- Shift - alarm: true alarm (TA)

A graphical representation of this process can be seen on Figure 1. The transition matrix of this Markov chain can be seen below.

$$\begin{array}{cccc} \text{In-control} & \text{Out-of-control} & \text{False alarm} & \text{True alarm} \\ \left[\begin{array}{cccc} (1-F(h))\phi(k) & F(h)\phi(k-\delta^*) & (1-F(h))(1-\phi(k)) & F(h)(1-\phi(k-\delta^*)) \\ 0 & \phi(k-\delta^*) & 0 & 1-\phi(k-\delta^*) \\ (1-F(h))\phi(k) & F(h)\phi(k-\delta^*) & (1-F(h))(1-\phi(k)) & F(h)(1-\phi(k-\delta^*)) \\ (1-F(h))\phi(k) & F(h)\phi(k-\delta^*) & (1-F(h))(1-\phi(k)) & F(h)(1-\phi(k-\delta^*)) \end{array} \right] \end{array}$$



Here $F()$ is the cumulative distribution function of the exponential distribution with expectation $1/s$, where s is the expected number of shifts in a unit time interval. h is the time between consecutive observations and ϕ is the cumulative distribution function of the process. k is the control limit and δ^* is the size of the shift. After calculating the stationary distribution of this Markov chain, one can define a cost function for the average total cost:

$$E(C) = \frac{c_s + p_3 c_f + p_4 c_r}{h} + p_2 c_o + p_4 c_o B \quad (1)$$

where p_i is the probability of state i , in the stationary distribution. c_s , c_f , c_o and c_r are the cost of sampling, false alarm, out-of-control operation and repair respectively. B is the fraction of time between consecutive observations where the shift occurred and remained undetected:³

$$B = \frac{h s e^{hs} - e^{hs} + 1}{h s (e^{hs} - 1)}$$

An economically optimal chart, based on the time between samplings and the control limit can be constructed by minimising the cost function.

2.2 Generalisation

The previous simple framework can be used for more general designs. Zempléni et al.¹⁶ used this method to set up economically optimal control charts where shifts are assumed to have a random size and only the distribution of the shift size is known. This means that the shift size is no longer assumed to be fixed and known, which is important in modeling various processes not just in healthcare, but in industrial or engineering settings too. This requires expanding the two shifted states to account for different shift sizes. Let τ_i denote the random shift times on the real line and let ρ_i be the shift size at time τ_i . Let the probability mass function of the number of shifts after time t from the start be denoted by ν_t . ν_t is a discrete distribution with support over \mathbb{N}^0 . Assume that ρ_i follows a continuous distribution, which has a cumulative distribution function with support over $(0, \infty)$, and that the shifts are independent from each other and from τ_i . If the previous conditions are met, the resulting random process has monotone increasing trajectories between samplings, which are step functions. The cumulative distribution function of the process values for a given time t from the start can be written the following way:

$$Z_t(x) = \begin{cases} 0 & \text{if } x < 0, \\ \nu_t(0) + \sum_{k=1}^{\infty} \nu_t(k) \Psi_k(x) & \text{if } x \geq 0 \end{cases} \quad (2)$$

where $\Psi_k()$ is the cumulative distribution function of the sum of k independent, identically distributed ρ_i shift sizes. The $x = 0$ case means there is no shift. The probability of zero shift size is just the probability of no shift occurring, which is $\nu_t(0)$.

Let us assume now that the shift times form a homogeneous Poisson process, and the shift size is exponentially distributed, independently of previous events. The choice of the exponential distribution was motivated by the tractability of its convolution powers as a gamma distribution. The cumulative distribution function of the shift size by (2) is then:

$$Q_t(x) = \begin{cases} 0 & \text{if } x < 0, \\ n_t(0) + \sum_{k=1}^{\infty} n_t(k)Y_k(x) & \text{if } x \geq 0 \end{cases} \quad (3)$$

where n_t is the probability mass function of the Poisson distribution, with parameter ts - the expected number of shifts per unit time multiplied by the time elapsed - representing the number of shifts in the time interval $(0;t)$. Y_k - the shift size cumulative distribution function, for k shift events - is a special case of the gamma distribution, the Erlang distribution $E(k, \frac{1}{\delta})$, which is just the sum of k independent exponential variates each with mean δ .

The framework can be generalised even further by not assuming perfect repair after a true alarm signal. This means that the treatment will not have perfect results on the health of the patient, or - in industrial or engineering settings - that the machines cannot be fully repaired to their original condition. In this case, the imperfectly repaired states act as out-of-control states. It is assumed that the repair cannot worsen the state of the process, but an imperfectly repaired process will still cost the same as an equally shifted out-of-control process, thus repaired and out-of-control states do not need distinction during the cost calculation. Different approaches can be considered for modeling the repair size distribution. The one applied here uses a random variable to determine the distance from the target value after repair. A natural choice for the distribution of this random variable could be the beta distribution since it has support over $[0, 1]$ - the portion of the distance compared to the current one after repair. Also, the flexible shape of its density function can model many different repair processes. Because of these considerations we will assume that the proportion of the remaining distance from μ_0 after repair - R - is a $Beta(\alpha, \beta)$ random variable, with known parameters.

Yet another generalisation is the random sampling time. In certain environments, the occurrence of the sampling at the prescribed time is not always guaranteed. For example in healthcare, the patient or employee compliance can have significant effect on the monitoring, thus it is important to take this into account during the modeling too. Here it is modeled in a way, that the sampling is not guaranteed to take place - e.g. the patient may not show up for control visit. This means that the sampling can only occur according to the sampling intervals, for example at every n th days, but is not a guaranteed event. One can use different approaches when modeling the sampling probability, here we consider two cases. The first one assumes that too frequent samplings will decrease compliance. This assumption is intended to simulate the situation in which too frequent samplings may cause increased difficulty for the staff or the patient - leading to decreased compliance. The probability of a successful sampling as a function of the prescribed time between samplings is modeled using a logistic function:

$$T_h^* = \frac{1}{1 + e^{-q(h-z)}}$$

where $q > 0$ is the steepness of the curve, $z \in \mathbb{R}$ is the value of the sigmoid's midpoint and h is the time between samplings.

In the other approach it is assumed that too frequent samplings will decrease compliance and increased distance from the target value will increase compliance. This assumption means that a heavily deteriorated process or health state will ensure a higher compliance. The probability of a successful sampling as a function of the prescribed time between samplings and the distance from the target value is modeled using a modified beta distribution function:

$$T_h^*(w) = P\left(W_h < \frac{w + \zeta^*}{V + 2\zeta^*}\right)$$

where W_h is a beta distributed $Beta(a/h, b)$ random variable, w is the distance from the target value, h is the time between samplings, V is the maximum distance from μ_0 taken into account - the distance where we expect maximal possible compliance. The shifts in the values of w and V are needed to

acquire probabilities strictly between 0 and 1, since deterministic behaviour is undesirable even in extreme cases. These shifts are parametrised by the $\zeta^* > 0$ value, which should typically be a small number. It is important to note, that these are just two ways of modeling the sampling probability. Other approaches and distributions may be more appropriate depending on the process of interest.

The shift size distribution, the repair size distribution and the sampling probability, together with the control chart let us model and monitor the behaviour of the process. The resulting process is monotone increasing between samplings and has a downward "jump" at alarm states - as the repair is assumed to be instantaneous. Usually a wide range of different cost types are associated with the processes and their monitoring, these include the costs associated with operation outside the target value. Since the operator of the control chart only receives information about the process at the time of the sampling, the proper estimation of the process behaviour between samplings is critical. Previously, at the perfect repair and non-stackable, fixed shift size model, this task was reduced to estimating the time of shift in case of a true alarm or out-of-control state, since otherwise the process stayed at the previous value between samplings. The estimation of the process behavior with random shift sizes and random repair is more difficult.

The expected out-of-control operation cost can be written as the expectation of a function of the distance from the target value. At (2) the shift size distribution was defined for a given time t , but this time we are interested in calculating the expected cost for a whole interval. We propose the following calculation method for the above problem:

Proposition. *Let H_j be a random process whose trajectories are monotone increasing step functions defined by τ_i shift times and ρ_i shift sizes as in (2), with starting value $j \geq 0$.*

The expected value of a function of H_j over an ϵ long interval can be written as:

$$E_\epsilon(f(H_j)) = \frac{\int_{t_0}^{t_0+\epsilon} \int_0^\infty 1 - Z_t(f^{-1}(x-j)) dx dt}{\epsilon} \quad (4)$$

where $Z_t()$ is the shift size cumulative distribution function given at (2), $f()$ is an invertible, monotonic increasing function over the real line and t_0 is the start point of the interval.

Proof. Let us observe that the inner integral in the numerator - $\int_0^\infty 1 - Z_t(f^{-1}(x-j)) dx$ - is just the expected value of a function of the shift size at time t , since we know that if X is a non-negative random variable, then $E(X) = \int_0^\infty (1 - F(x)) dx$, where $F()$ is the cumulative distribution function of X . In other words, the inner integral in the numerator is the expected value the process $f(H_j)$, t time after the start. Furthermore, observe that this expected value is a continuous function of t . We are looking for the expectation of $\int_0^\infty 1 - Z_t(f^{-1}(x-j)) dx$ over $[t_0, t_0 + \epsilon]$, which is (4). \square

For practical purposes we can apply the previous, general proposition to our model of Poisson-gamma mixture shift size distribution, thus we assume that the shift size distribution is of the form of (3). The connection between the distance from the target value and the resulting cost is often assumed not to be linear: often a Taguchi-type loss function is used - the loss is assumed to be proportional to the squared distance, see e.g. the book of Deming.¹⁷ Applying this to the above proposition means $f(x) = x^2$. Since we are interested in the behaviour of the process between samplings, $t_0 = 0$ and $\epsilon = h$, thus:

$$\begin{aligned} E_h(H_j^2) &= \frac{\int_0^h \left[e^{-ts} j^2 + \left(\sum_{k=1}^\infty \frac{(ts)^k e^{-ts}}{k!} \cdot \int_0^\infty (x+j)^2 \frac{(1/\delta)^k x^{k-1} e^{-x/\delta}}{(k-1)!} dx \right) \right] dt}{h} \\ &= \frac{\int_0^h e^{-ts} j^2 + \sum_{k=1}^\infty \frac{(ts)^k e^{-ts}}{k!} (k\delta^2 + (k\delta + j)^2) dt}{h} = \frac{\int_0^h 2\delta^2 ts + (\delta ts + j)^2 dt}{h} \\ &= hs\delta \left(\delta + \frac{hs\delta}{3} + j \right) + j^2 \end{aligned} \quad (5)$$

where first we have used the law of total expectation - the condition being the number of shifts within the interval. If there is no shift, then the distance is not increased between samplings, this case is included by the $e^{-ts} j^2$ term before the inner integral. Note that the inner integral is just $E(X+j)^2$ for a gamma - namely an Erlang($k, \frac{1}{\delta}$) - distributed random variable. When calculating the sum, we

used the known formulas for $E(N^2)$, $E(N)$ and the Poisson distribution itself - where N is a Poisson(ts) distributed random variable.

2.3 Implementation

DISCRETISATION For cost calculation purposes we would like to find a discrete stationary distribution which approximates the distribution of the monitored characteristic at the time of samplings. This requires the discretisation of the above defined functions, which in turn will allow us to construct a discrete time Markov chain with discrete state space.

A vector of probabilities is needed to represent the shift size probability mass function $q_t(i)$ during a sampling interval:

$$q_t(i) = \begin{cases} n_t(0) & \text{if } i = 0, \\ \sum_{k=1}^{\infty} n_t(k)(Y_k(i\Delta) - Y_k((i-1)\Delta)) & \text{if } i \in \mathbb{N}^+ \end{cases}$$

where Δ stands for the length of an interval, one unit after discretisation. For $i = 0$ the function is just the probability of no shift occurring.

The discretised version of the repair size distribution can be written the following way:

$$R(l, m) = P\left(\frac{m}{l+1/2} \leq R < \frac{m+1}{l+1/2}\right)$$

where l is the number of discretised distances closer to μ_0 than the current one - including μ_0 . m is the index for the repair size segment we are interested in, with $m = 0$ meaning perfect repair ($m \leq l$). The repair is assumed to move the expected value towards the target value by a random percentage, governed by $R()$. Even though discretisation is required for practical use of the framework, in reality the repair size distribution is continuous. To reflect this continuity in the background, the probability of perfect repair is set to be 0 when the repair is random. l is set to be 0 when there is no repair, meaning $R(0, m) \equiv 1$. The $1/2$ terms are necessary for correcting the overestimation of the distances from the target value, introduced by the discretisation: in reality, the distance can fall anywhere within the discretised interval, without correction the maximum of the possible values would be taken into account, which is an overestimation of the actual shift size. After correction the midpoint of the interval is used, which can still be somewhat biased, but in practical use with fine discretisation this effect is negligible.

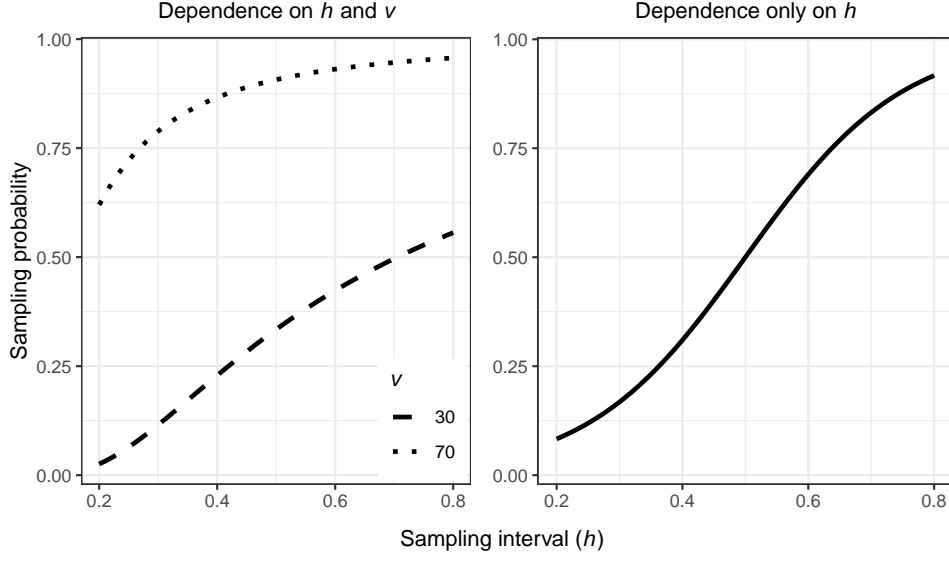
When the sampling probability depends on the time between samplings only, the model is unchanged, since both the time between samplings and the sampling probability can be continuous. However, when the probability also depends on the shift size, discretisation is required here as well:

$$T_h(v) = P\left(W_h < \frac{v+\zeta}{V_d+\zeta} - \frac{1}{2(V_d+\zeta)}\right)$$

now v is the state distance from the target value in discretised units, and V_d is the number of considered intervals - discretised shift sizes. The $\frac{1}{2(V_d+\zeta)}$ term is necessary for correcting the overestimation of the distances from the target value. The denominators contain simply $V_d + \zeta$ instead of $V_d + 2\zeta$, because $v + \zeta$ is already strictly smaller than $V_d + \zeta$, since the smallest discretised state is 0 and thus the greatest is $V_d - 1$. This ensures that the probability can never reach 1. Example curves for the successful sampling probability can be seen in Figure 2. It shows that longer time between samplings and greater distances from the target value increase the probability of successful sampling.

TRANSITION MATRIX AND STATIONARY DISTRIBUTION The transition probabilities can be written using the $\phi()$ process distribution, the $q_t(i)$ shift size distribution, the $R()$ repair size distribution and

Figure 2: Sampling probabilities for $q = 8$, $z = 0.5$ on the left, and for $\alpha = 1$, $\beta = 3$, $V_d = 100$, $\zeta = 1$ on the right



the $T_h()$ sampling probability. For the ease of notation let us define the $S()$ and $S'()$ functions, the first for target states without alarm and the latter for target states with alarm:

$$S(g, v, l) = [T_h(v)\phi(k - \Delta'(v)) + (1 - T_h(v))] \sum_{m \in \mathbb{N}^0, m \leq l, m \leq v} q_h(g - m)R(l, m)$$

$$S'(g, v, l) = T_h(v)[1 - \phi(k - \Delta'(v))] \sum_{m \in \mathbb{N}^0, m \leq l, m \leq v} q_h(g - m)R(l, m)$$

where $\Delta'(v)$ is a function defined as

$$\Delta'(v) = \begin{cases} 0 & \text{if } v = 0, \\ i\Delta - \frac{\Delta}{2} & \text{if } v = 1, \dots, V_d - 1 \end{cases}$$

$k - v\Delta$ would simply be the critical value minus the size of the shift in consideration. The $-\frac{\Delta}{2}$ term is added, because without it, the shift size would be overestimated. The total number of discretised distances is V_d , thus the number of non-zero distances is $V_d - 1$. g is the total shift size possible in discretised units when moving to a given state, v is the distance, measured as the number of discretised units from the target value, l is the index of the actual partition and m is the index for the repair size segment we are interested in with $m = 0$ meaning perfect repair. Note, that as before, l is set to be 0 when there is no repair, meaning $R(0, m) \equiv 1$. $S()$ and $S'()$ are functions which combine the three distributions into the probability we are interested in. The possible values of m are restricted this way, because the parameter of the $q_h()$ function must be non-negative. A more intuitive explanation is, that we assumed positive shifts and a negative $g - m$ would imply a negative shift. It can be seen that the probability of a state without an alarm - the $S'()$ function - is increased with the probability of unsuccessful sampling - the $1 - T_h(v)$ term. Of course it is still possible to not receive an alarm even though the sampling successfully occurred.

Using the $S()$ and $S'()$ functions one can construct the transition matrix:

$$\Pi = \begin{array}{c} \left. \begin{array}{cccc|cccc} \text{In-control} & \text{Out-of-control} & \text{False alarm} & \text{True alarm} & & & & \\ S(0,0,0) & S(1,1,0) & S(2,2,0) & \dots & S'(0,0,0) & S'(1,1,0) & S'(2,2,0) & \dots \\ 0 & S(0,1,0) & S(1,2,0) & \dots & 0 & S'(0,1,0) & S'(1,2,0) & \dots \\ 0 & 0 & S(0,2,0) & \dots & 0 & 0 & S'(0,2,0) & \dots \\ \vdots & \vdots & \vdots & & \vdots & \vdots & \vdots & \\ S(0,0,0) & S(1,1,0) & S(2,2,0) & \dots & S'(0,0,0) & S'(1,1,0) & S'(2,2,0) & \dots \\ 0 & S(1,1,1) & S(2,2,1) & \dots & 0 & S'(1,1,1) & S'(2,2,1) & \dots \\ 0 & S(1,1,2) & S(2,2,2) & \dots & 0 & S'(1,1,2) & S'(2,2,2) & \dots \\ \vdots & \vdots & \vdots & & \vdots & \vdots & \vdots & \ddots \end{array} \right\} \end{array}$$

The size of the matrix is $2V_d \times 2V_d$ since every shift size has two states: one with and one without alarm. The first V_d columns are states without alarm, the second V_d are states with alarm. One can observe, that once the process leaves the healthy state it will never return. This is due to the nature of the imperfect repair we have discussed.

The transition matrix above defines a Markov chain with a discrete, finite state space with one transient, inessential class (in-control and false alarm states) and one positive recurrent class (out-of-control and true alarm states). The starting distribution is assumed to be a deterministic distribution concentrated on the in-control state, which is to say that the process is assumed to always start from the target value. In finite Markov chains, the process leaves such a starting transient class with probability one. The problem of finding the stationary distribution of the Markov chain is thus reduced to finding a stationary distribution within the recurrent classes of the chain. Since there is a single positive recurrent class which is also aperiodic, we can apply the Perron–Frobenius theorem to find the stationary distribution.¹⁸

Theorem. *Let A be an $n \times n$, irreducible matrix with non-negative elements, $x \in \mathbb{R}^n$ and*

$$\lambda_0 = \lambda_0(A) = \sup\{\lambda : \exists x > 0 : Ax \geq \lambda x\}.$$

Then the following statements hold:

- 1) λ_0 is an eigenvalue of A with algebraic multiplicity of one, and its corresponding eigenvector x_0 has strictly positive elements.
- 2) The absolute value of all other eigenvalues is less than or equals λ_0 .
- 3) If A is also aperiodic, then the absolute value of all other eigenvalues is less than λ_0 .

One can apply this theorem to find the stationary distribution of Π . If we consider now Π without the inessential class - let us denote it with Π' - then $\lambda_0(\Pi') = \lambda_0(\Pi'^T) = 1$. Moreover, the stationary distribution - which is the left eigenvector of Π' , normalised to sum to one - is unique and exists with strictly positive elements. Finding the stationary distribution is then reduced to solving the following equation: $\Pi'^T f_0 = f_0$, where f_0 is the left eigenvector of Π' . This amounts to solving $2V_d - 2$ equations - the number of states minus the in-control and false alarm states - for the same number of variables, so the task is easily accomplishable. The stationary distribution is then:

$$P = \frac{f_0}{\sum_{i=1}^{2V_d-2} f_{0i}}.$$

COST FUNCTION Using the stationary distribution, the expected cost can be calculated:

$$E(C) = c_s \frac{1}{h} (T' \cdot P) + \frac{\sum_{i=1}^{V_d-1} (c_{rb} + c_{rs} \Delta^2(i)) P_{ri}}{h} + c_o (A^2 \cdot P)$$

This cost function incorporates similar terms as previously (1). The first term deals with the sampling cost: $T' = \{T_h(1), T_h(2), \dots, T_h(V_d - 1), T_h(1), T_h(2), \dots, T_h(V_d - 1)\}$ is the vector of successful sampling probabilities repeated in a way to fit the length and order of the stationary distribution. This first term uses the expected time between samplings, $\frac{1}{h} (T' \cdot P)$, instead of simply h , which would just be

the minimal possible time between samplings. The second term deals with the repair costs and true alarm probabilities. P_{r_i} is the true alarm probability for shift size i . The repair cost is partitioned into a base and shift-proportionate part: c_{rb} and c_{rs} . The true alarm probability is used, since it is assumed that repair occurs only if there is an alarm. The last term is the average cost due to operation while the process is shifted. The connection between the distance from the target value and the resulting cost is assumed to be proportional to the squared distance. This is modeled using the A^2 vector, which contains the weighted averages of the expected squared distances from the target value between samplings:

$$A_i^2 = \sum_{j=1}^i E_h(H_{\Delta'(j)}^2) M_{ij}$$

where $E_h(H_{\Delta'(j)}^2)$ is calculated using (5). j indicates one of the possible starting distances immediately after the sampling, and i indicates the state - shift - of the process at the current sampling. M_{ij} is the probability that $\Delta'(j)$ will be the starting distance after the sampling, given that the current state is i . These probabilities can be written in a matrix form:

$$\begin{array}{c} \text{Distance from the target value starting from 0} \\ \left[\begin{array}{ccccc} 0 & 1 & 0 & 0 & \dots \\ 0 & 0 & 1 & 0 & \dots \\ 0 & 0 & 0 & 1 & \dots \\ \vdots & \vdots & \vdots & \vdots & \\ 0 & 1 & 0 & 0 & \dots \\ 0 & R(1,0) & R(1,1) & 0 & \dots \\ 0 & R(2,0) & R(2,1) & R(2,2) & \dots \\ \vdots & \vdots & \vdots & \vdots & \end{array} \right] \end{array} \begin{array}{l} \left. \begin{array}{l} \dots \\ \dots \\ \dots \\ \dots \end{array} \right\} \text{Out-of-control} \\ \left. \begin{array}{l} \dots \\ \dots \\ \dots \end{array} \right\} \text{True alarm} \end{array}$$

It can be seen, that when the process is out-of-control without alarm, the distance is not changed. The probabilities for the alarm states are calculated using the $R()$ repair size distribution.

So far only the expected cost was considered during the optimisation. In certain fields of application the reduction of the cost standard deviation can be just as or even more important than the minimisation of the expected cost. Motivated by this, let us consider now the weighted average of the cost expectation and the cost standard deviation:

$$G = pE(C) + (1-p)\sigma(C)$$

Now G is the value to be minimised and p is the weight of the expected cost ($0 \leq p \leq 1$). The cost standard deviation can easily be calculated by modifying the cost function formula. All of the previous models can be used without any significant change, one simply changes the value to be minimised from $E(C)$ to G .

2.4 Comparison of Different Scenarios

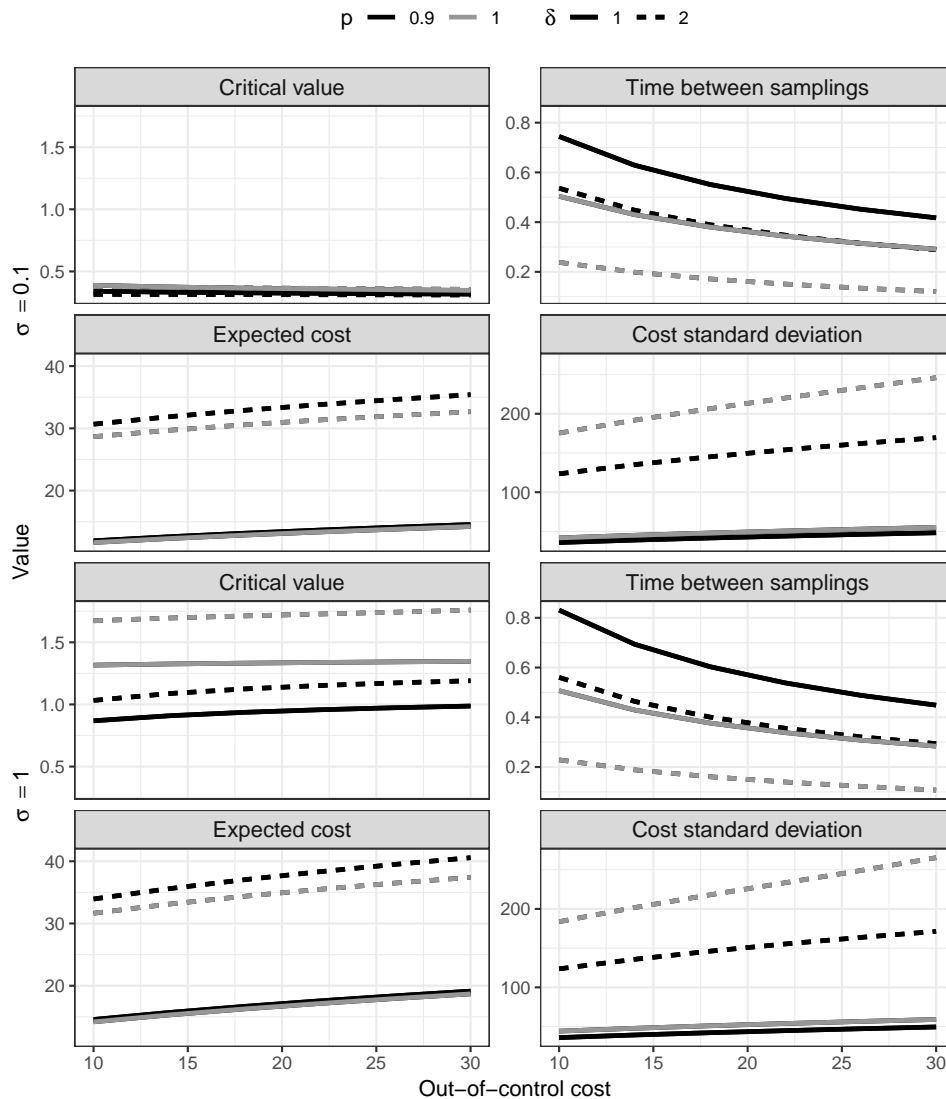
Implementation of the methods was done using the R programming language. Supplying all the necessary parameters, one can calculate the G value of the process for one time unit. It is also possible to minimise the G value by finding the optimal time between samplings and control limit. All the other parameters are assumed to be known. The optimization step can be carried out using different tools, the results presented here were obtained with the built-in `optim()` R function: box-constrained optimization using PORT routines,¹⁹ namely the Broyden-Fletcher-Goldfarb-Shanno (L-BFGS-B) algorithm. The optimisation procedure can be divided into three steps. First, the transition matrix needs to be constructed from the given parameters. After this, the stationary distribution of the Markov chain is computed. In the third step, the G value is calculated using the stationary distribution and the cost function. The optimisation algorithm then checks the resulting G value and iterates the previous steps with different time between sampling and/or control limit parameters until it finds the optimal ones.

DEPENDENCE ON PARAMETERS The testing was done using a moderate overall compliance level. This is required because low compliance can result in extreme behaviour in the optimisation such as taking the maximum or minimum allowed parameter value. An example for this is when the sampling probability depends on both the time between samplings and the state of the process: if the compliance level is also relatively low, then given certain parameter setups the optimal time between samplings will tend to zero. This will essentially create a self-reporting system as the increased distance from the target value will eventually increase the compliance and the sampling will take place. In a health-care environment this would mean that the patient is told to come back for a control visit as soon as possible, but the patient will show up only when the symptoms are severe enough. This kind of process behaviour is undesirable in many cases, for example when the time between samplings cannot be set arbitrarily.

The results obtained are shown in Figure 3. One may observe the weak dependence of the critical

Figure 3: Optimal parameters and the resulting expected cost and cost standard deviation as function of the process standard deviation (σ), out-of-control cost (c_o), expected shift size (δ) and weight parameter (p) for $s = 0.2, \alpha = 1, \beta = 3, a = 0.01, b = 1, c_s = 1, c_{rb} = 10, c_{rs} = 10$

Top: $\sigma = 0.1$, Bottom: $\sigma = 1$



value on the out-of-control cost. The time between samplings should be decreased with the increase

of the out-of-control cost, and the average cost and the cost standard deviation increase with the out-of-control cost, as expected. The effect of the expected shift size on the critical value depends on the process standard deviation, as increased shift size results in markedly increased critical values only in the case of $\sigma = 1$. Higher expected shift size entails less time between samplings, and increased expected cost and cost standard deviation. One can assess, that if the cost standard deviation is taken into account during the optimisation procedure ($p = 0.9$), then lower critical value should be used with increased time between samplings. This is logical, because the increased time between sampling will lead to less frequent interventions, thus a less erratic process. Of course, at the same time we do not want to increase the expected cost, so the critical value is lowered. The cost standard deviation is decreased, as expected. What is interesting to note is that the expected costs have barely increased compared to the $p = 1$ setup. This is important, because it shows that by changing the parameters appropriately, the cost standard deviation can be lowered - sometimes substantially - while the expected cost is only mildly increased. Several scenarios entail relatively large cost standard deviations, this is partly due to the Taguchi-type loss function used during the calculations. The process standard deviation σ has noticeable effect on the critical value only: lower critical values should be used for lower standard deviations, as expected.

SENSITISING RULES The effect of sensitising rules¹ was investigated using simulation, since the implementation of theoretical calculations would have resulted in a hugely inflated transition matrix which poses a serious obstacle in both programming a running times.

Optimal parameters were calculated for $p = 0.9$, $\sigma = 1$, $s = 0.2$, $\delta = 2$, $\alpha = 1$, $\beta = 3$, $a = 0.01$, $b = 1$, $c_s = 1$, $c_{rb} = 10$, $c_{rs} = 10$, $c_{rs} = 20$. The resulting optimal parameters were $h = 0.38$ and $k = 1.14$. This parameter setup entailed an expected cost of $E(C) = 37.75$ and cost standard deviation of $\sigma(C) = 150.33$. The probability of alarm states together was $\sum_i P_{r_i} = 0.201$. Simulations were run for 50000 sampling intervals which equals 19000 unit time. Simulations from the first 100 sampling intervals were discarded as it was regarded as a burn-in stage.

First, we present the baseline simulation results - the ones without additional rules. Overall, the simulation achieved an acceptable level of convergence to the theoretical stationary distribution. The empirical expected cost was $\bar{C} = 36.51$. The proportion of alarm states was 0.192. The calculation of the empirical standard deviation was carried out by taking into account the data of only every 30th sampling interval to deal with the autocorrelation of neighboring values. The empirical standard deviation using this method was $s^* = 199.37$. It is important to note that the empirical results can be somewhat inaccurate, depending on the particular simulation results and the parameters used. This is due to the large variance and slow convergence of the standard deviation. Nonetheless, for this particular scenario the theoretical and empirical results were quite close to each other, thus we will compare the effect of sensitising rules to this baseline simulation.

The first rule we investigated was the one which produces an alarm in case of three consecutive points outside the $\frac{2}{3}k$ warning limit but still inside the control limit. Running the simulation with the extra rule resulted in $\bar{C} = 37.42$, $s^* = 171.57$ and a ratio of all alarm states together of 0.194, all of these values are within the hypothesised confidence interval. We can see no major difference in any of these values compared to the baseline.

The second rule was the same as the first one, except this time two consecutive points outside the $\frac{2}{3}k$ warning limit were enough to produce an alarm signal. The results were $\bar{C} = 36.54$, $s^* = 190.91$ and 0.200 for the proportion of alarm states. Again, no apparent differences can be seen, but it is worth noting the proportion of alarm states is somewhat higher in this case than the at the baseline or the previous rule, and this was also seen with repeated simulation.

Overall, the effect of the investigated sensitising rules seems to be minimal on the results. Further investigation is required of the the possible effects in case of other parameter setups and rules.

3 APPLICATION

In the following paragraphs we show a real life healthcare example as the application of the previously introduced methods. Two approaches will be presented: one with and one without taking the standard deviation into account. The example problem is to minimise the healthcare burden generated by patients with high cardiovascular (CV) event risk. The model is built upon the relationship between the low-density lipoprotein (LDL) level and the risk of CV events, thus the LDL level is the process of interest.²⁰

Parameters were estimated from several sources. The list below gives information about the meaning of the parameter values in the healthcare setting and shows the source of the parameter estimations.

Parameter values and sources

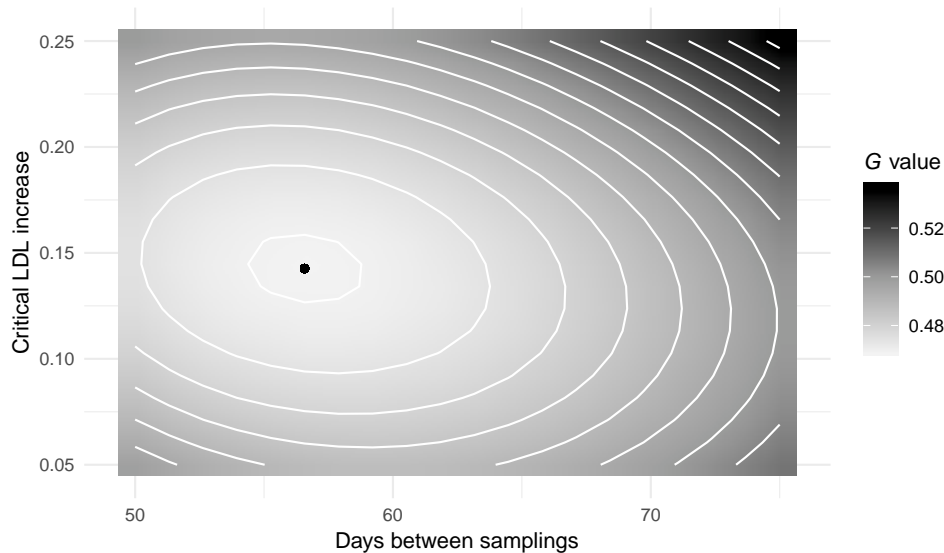
Parameter value	Meaning	Parameter source
$\mu_0=3$ mmol/l	Target value.	Set according to the European guideline for patients at risk. ²¹
$\sigma=0.1$ mmol/l	Process standard deviation.	Estimated using real life data from Hungary, namely registry data through the Healthware Consulting Ltd.
$\delta=0.8/3$	Expected shift size, 0.8 increase in LDL per year on average.	Estimated with the help of a health professional.
$s=1/120$	Expected number of shifts in a day, 3 shifts per year on average.	Estimated with the help of a health professional.
$\alpha = 0.027, \beta = 1.15$	Parameters of the repair size beta distribution.	Estimated using an international study which included Hungary. ²¹
$q = 0.1, z = 30,$	Parameters of the sampling probability logistic function.	Patient non-compliance in LDL controlling medicine is quite high, and this is represented through the parametrisation of the logistic function. ²²
$c_s=\text{€}5.78$	Sampling cost.	Estimated using the LDL testing cost and visit cost in Hungary.
$c_o=\text{€}5.30$	Shift-proportional daily out-of-control cost.	Estimated using real world data of cardiovascular event costs from Hungary
$c_{rb}=\text{€}11.50$	Base repair cost.	Estimated using the simvastatin therapy costs in Hungary
$c_{rs}=\text{€}8.63$	Shift-proportional repair cost.	Estimated using the simvastatin therapy costs in Hungary

It is very difficult to give a good estimate for the type and the parameters of a distribution that properly models the non-compliance, thus the results here can at best be regarded as close approximations to a real life situation. This is not a limiting factor, as patients themselves can have vast differences in their behaviour, so evaluation of different scenarios are often required, and will also be presented here. Since high LDL levels rarely produce noticeable symptoms, the sampling probability only depends on the time between samplings, thus the sampling probability was modeled by the logistic function and

not by the beta distribution.²³ It is important to note that the proportional costs increase according to a Taguchi-type loss function, thus huge expenses can be generated if the patient's health is highly out-of-control.

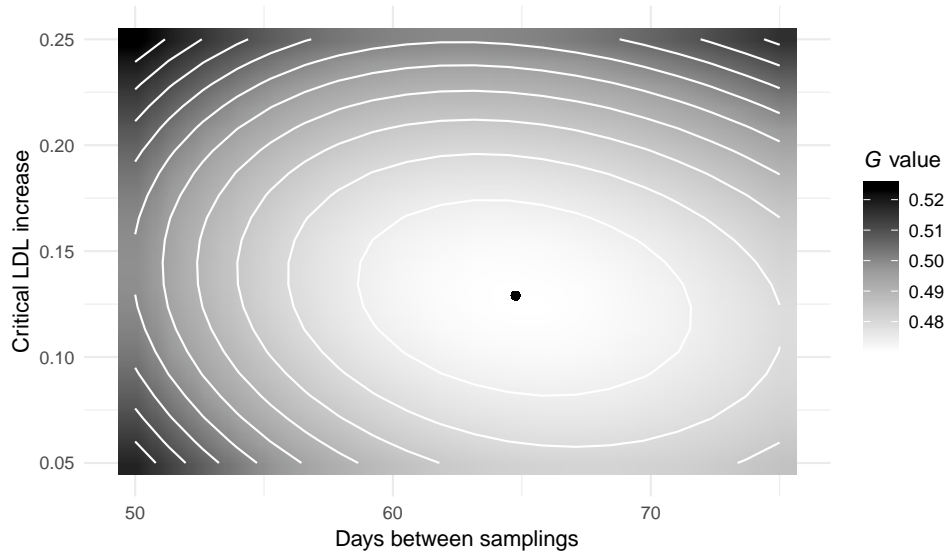
OPTIMISATION USING ONLY THE COST EXPECTATION The optimal parameters for the case when the cost standard deviation was not taken into account were 56.57 days and 0.143 mmol/l for the time between samplings and the critical increase in the LDL level from the guideline value respectively. These parameters entailed an average daily cost of €0.469 and standard deviation of €0.562. This result is interesting, because the optimisation says that we should use a somewhat higher critical value than the one according to the guideline - 0 mmol/l critical increase would be the original 3 mmol/l value - but we should monitor the patients more often than usual - times of the LDL measurements are usually several months or years apart. It is important to note, that this is a strictly cost effective viewpoint which could be overwritten by a health professional. Nonetheless, the results provide a possible new approach to the therapeutic regime for controlling LDL level. Often, it is good to look at the interaction between the parameters and the resulting average cost, especially in situations where the optimal parameters cannot be used because of real life reasons. The heat map of Figure 4 shows

Figure 4: Expected cost as function of the time between samplings and the critical value



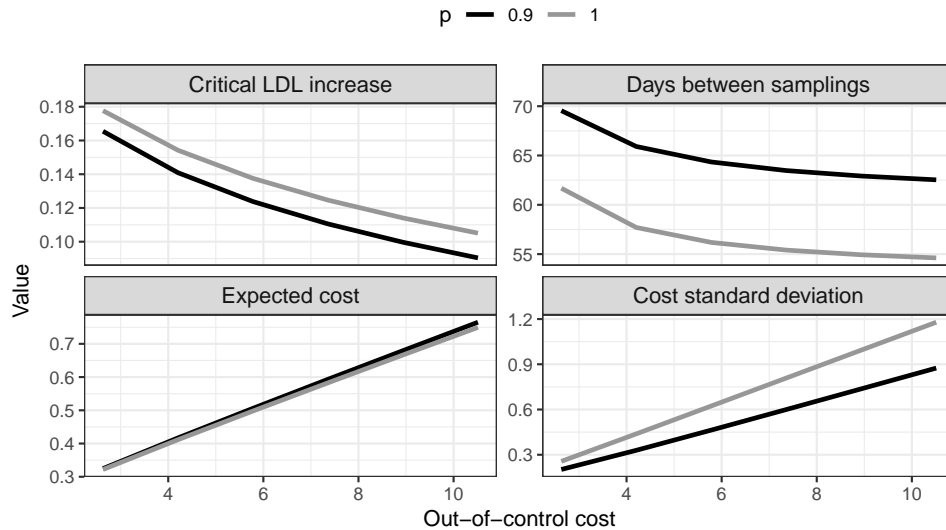
the average cost as the function of the different parameter values. The dot in the lightest area of the figure corresponds to the optimal cost. Any other point entails a higher average cost. It can clearly be seen that too low or high critical values will both increase the average daily cost. What is interesting - for this scenario - is that the change in the time between samplings entails relatively low change in the critical LDL increase: even if the time between control visits is changed the critical value should stay around 0.12 – 0.18 mmol/l.

OPTIMISATION USING COST EXPECTATION AND COST STANDARD DEVIATION In this part, the cost standard deviation is also taken into account with $p = 0.9$, thus the weight of the standard deviation in the calculation of G is 0.1. The optimal parameters found by our approach were 64.76 days and 0.129 mmol/l for the time between samplings and critical increase in the LDL level respectively. These parameters entailed an average daily cost of €0.477 and standard deviation of €0.418. The inclusion of the cost standard deviation into the model has somewhat increased the time between control visits and decreased the critical value. The expected cost somewhat increased, while the cost standard deviation was moderately decreased. Figure 5 shows the previous heat map with non-compliance included in the model. It can be seen that the elliptical shape of the heat map has not changed: the change in the time between control visits still does not entail great change in the critical value.

Figure 5: G value as function of the time between samplings and the critical value

SENSITIVITY ANALYSIS As there were uncertainty about the estimation of several parameters, it is important to assess the effect of different parameter setups. The results for different out-of-control costs are plotted for both approaches. The results can be seen in Figure 6.

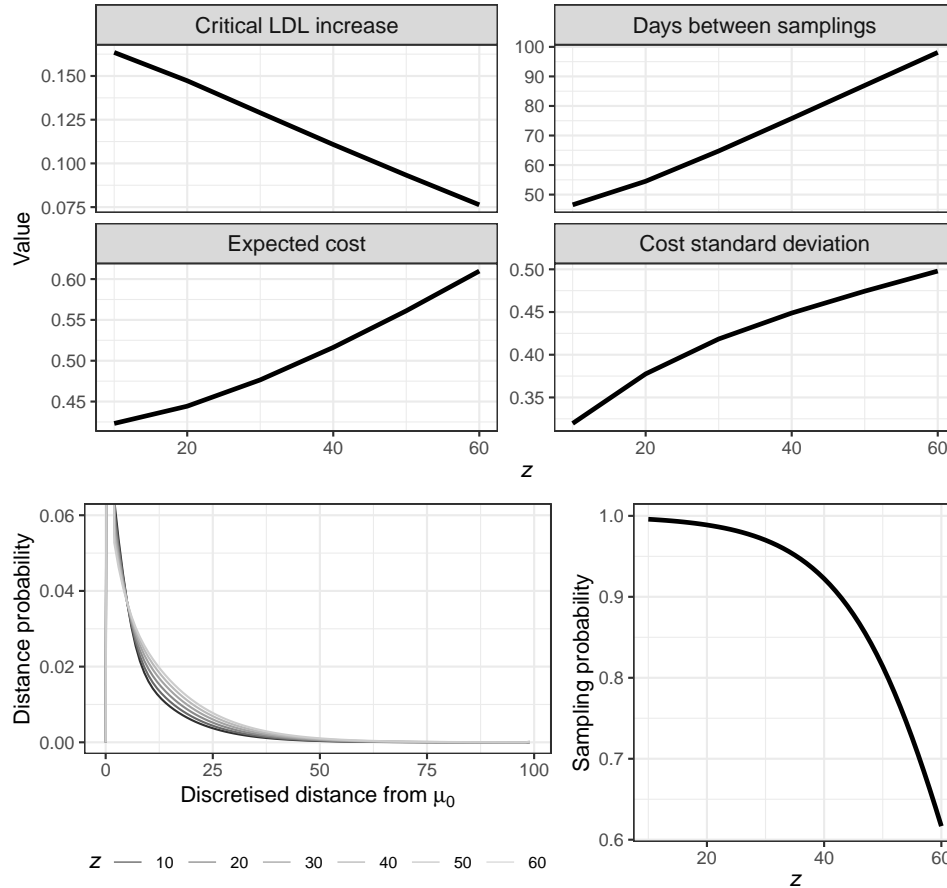
Figure 6: Parameters, average total cost and cost standard deviation as function of the out-of-control cost



The critical value and time between samplings decrease and the average cost and cost standard deviation increase with higher out-of-control costs. Just as on the heat maps, one can observe here, that if the cost standard deviation is taken into account in the optimisation, then the critical value should be lowered and the time between samplings increased. One can observe, that a substantial decrease can be achieved in the cost standard deviation while the cost expectation barely changes.

Uncertainty was also high around the estimation of the sampling probability. The sigmoid's midpoint so far was $z = 30$ days, meaning that the probability of sampling was 0.5 at $h = 30$ and increased with h . Figure 7 contains results for different z values. One can observe, that as the probability of successful sampling decreases - the value of z is increased - the critical value decreases and the time

Figure 7: Top: parameters, average total cost and cost standard deviation as function of the sigmoid's midpoint (z), Bottom left: distance distributions: lighter lines corresponds to greater z values, Bottom right: sampling probability as function of z , for $h = 64.76$



between samplings increases. This can be explained by the increased uncertainty of the sampling: More time between samplings entails higher patient compliance, and when the visit occurs a low critical value is used to ensure treatment. The cost expectation and standard deviation increases with lower sampling probabilities. There are only minor differences between the stationary distributions, nonetheless it can be seen that lower sampling probability is associated with higher probabilities for greater distances from the target value. The last panel shows how the sampling probability decreases with increasing z values for a fixed h .

4 CONCLUSIONS

Cost-optimal control charts based on predominantly Duncan's cycle model are found in a wide variety of areas. Even though the benefit of using these charts in industrial and engineering settings is unquestionable, the numerous assumptions needed about the processes makes the applicability of the traditional models problematic in certain environments. Motivated by the desire to apply cost-optimal control charts on processes with erratic behaviour and imperfect repair mechanism - such as ones found in healthcare - this paper presented a Markov chain-based framework for the generalisation of these control charts, which enabled the loosening of some of the usual assumptions.

Cost-optimisation of control charts are usually carried out by finding the optimal critical value, time between samplings and sample size. Our work concentrated on the monitoring of a single element at a time - e.g. a patient - thus the methods presented here always used a sample size of 1.

Building on and expanding the work of Zempléni et al.¹⁶ we discussed three types of generalisations: the random shift size, the imperfect repair and the non-compliance. The random shift size means that only the distribution of the shift size and its parameters are assumed to be known. This let us monitor processes which are potentially drifting in nature. The second generalisation - the imperfect repair - assumed that the process stays out of control even after repair, but on a level closer to the target value than before. This type of repair response is often observed in treatments in healthcare, but may be found in other areas too. The third generalisation was intended to help the modeling of patient or staff non-compliance. We implemented this concept in a way that allows sampling times to be skipped by a probability governed by a distribution or function with known parameters.

Since the processes modeled with the above loosened assumptions can create complicated trajectories between samplings, the mathematical description of these was also necessary. We proposed an expectation calculation method of a function of the values taken on by the process between samplings. The application of this proposition while assuming exponentially distributed shift sizes, Poisson distributed event numbers and Taguchi-type loss function yielded a compact formula for the expectation.

We implemented our theoretical results in the R programming language and investigated the effect of parameter estimation uncertainty on the optimal parameters and the resulting expected cost and cost standard deviation. We also tested the effect of involving the cost standard deviation in the optimisation procedure itself. We found that typically the critical value increases and the time between samplings decreases with the expected shift size. Also, higher expected shift sizes entail higher expected costs and cost standard deviations. It was seen that with the increase of the out-of-control cost - in most cases - the critical value stagnated, the time between samplings decreased, and the expected cost and the cost standard deviation increased. The involvement of the cost standard deviation in the optimisation procedure lowered the standard deviation while the cost expectation barely increased. We have found no evidence that sensitising rules - such as values outside the warning limit - would change the results substantially.

We presented an example of real-life application involving low-density lipoprotein monitoring. The results indicated that the cost-optimal critical value is somewhat higher and the cost-optimal time between control visits is less than the ones usually used according to medical guidelines.

In the era of Industry 4.0, the cost-optimal control charts presented here can be applied to a wider range of processes than the traditional ones. Nonetheless there are still areas worth investigating. One of the features still missing is the proper modeling of the repair procedure, since it was assumed to be an instantaneous event, which may not be appropriate in many situations. The mathematical elaboration of a continuous model involving e.g. time series could also be beneficial.

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