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journal homepage: www.elsevier.com/locate/jmrt**Original Article****Microstructure and corrosion resistance of highly <111> oriented electrodeposited CoNiFe medium-entropy alloy films**

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ABSTRACT

The medium-entropy alloy is a newly intriguing material showing superb properties. A simple, one-step method was developed to electrodeposit CoNiFe medium-entropy alloy films from a sulfate and citrate bath. The microstructure and corrosion resistance were investigated in CoNiFe films with varying deposition current densities. It shows the face-centered cubic structure with a <111> preferential orientation. HRTEM-EDS observations further show information on the nanostructure and element distribution. The films exhibit a strong corrosion resistance in 3.5 wt.% NaCl solution. The films electrodeposited with a current density of 44.4 A/dm² shows a low self-corrosion current density of 4.72×10^{-6} A·cm⁻² in 3.5 wt.% NaCl solution. The corrosion mechanism was proposed in combination with electrochemical impedance spectroscopy results. The outstanding properties were attributed to the near-equimolar ternary components. The results lay a solid foundation for developing of highly oriented medium-entropy alloy films with strong corrosion resistance.

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1. Introduction

Many kinds of metallic materials have been used in offshore engineering, e.g., shipbuilding and offshore oil platform

construction [1,2]. However, it is increasingly difficult to use only conventional metallic materials, e.g., stainless steels, to meet all growing engineering requirements [3]. Compositionally complex alloys (CCAs) possess an excellent combination of properties, making them hopeful candidates for future

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engineering applications, such as applications that require high hardness [4], high strength [5,6], strong corrosion resistance [7–9], strong radiation resistance [10], good wear resistance [11], and even superb catalytic properties [12,13]. Among CCAs, medium-entropy alloys (MEAs) have attracted attention as an emerging metallic material [14–18]. Recently, MEAs have received great attention from surface engineering researchers owing to their mechanical properties and corrosion resistance [19–21].

Among the preparation methods of MEAs, electrodeposition is a one-step method to prepare nanocrystalline metallic materials, which is an energy- and cost-saving method. Considering the environmentally hazardous consequences of chromium plating electrolytes [22], the electrodeposition of Cr-free MEAs, e.g., CoNiFe, shows attractive prospects for both environmental friendliness and high performance. In fact, there is a great challenge for the development of electrodeposited MEAs. The major reason for the poor success in the field of electrodeposited MEAs is the complexity of electrolytes required to codeposit multiple elements [19]. There is still limited information about electrodeposited MEAs. In several works on electrodeposited high-entropy alloys (HEAs), there are urgent problems, including a) replacing certain expensive organic ionic liquids or solvents [23–26] and b) obtaining controllable chemical compositions and microstructures [27,28]. On the other hand, the existing results of electrodeposited films of Co-Fe [29], Co-Ni [30], Ni-Fe [31] alloys, and even the results of other binary alloys [32–34] are still valuable for the development of electrodeposited CoNiFe MEAs. For example, it has been widely reported that the current intensity remarkably affects the microstructure and properties of electrodeposited films [35–39]. This provides a simple path for obtaining films with different microstructures. Unfortunately, there is still a lack of information on the corrosion resistance of electrodeposited MEA films, since only a limited amount of work on electrodeposited MEAs has been carried out.

Here, we report the synthesis of a series of highly <111>-oriented CoNiFe MEA films by an electrodeposition process. The resulting films exhibit controllable microstructures and high corrosion resistance and are suitable for applications in offshore engineering.

2. Experimental

2.1. Electrodeposition

First, pure copper was cut into small pieces used for substrates. A series of CoNiFe MEA films were prepared on the substrates at room temperature using direct current electrodeposition. Prior to use, the substrates were polished with grit paper and then cleaned with dilute sulfuric acid. The electrolytic bath consisted of 14.2 mM CoSO_4 , 76.1 mM NiSO_4 , 7.2 mM FeSO_4 , 466.4 mM $\text{C}_6\text{H}_8\text{O}_7$, 163.2 mM $\text{C}_6\text{H}_5\text{Na}_3\text{O}_7$, 1.3689 M NaCl, 404.3 mM H_3BO_3 , 7.3 mM $\text{C}_7\text{H}_4\text{NNaO}_3\text{S}$ and 0.3 mM $\text{C}_{12}\text{H}_{25}\text{SO}_4\text{Na}$ (pH 2.5). The electrolytic bath was prepared using ultrapure water. The MEAs were deposited with a varying current density, i.e., 44.4 A/dm^2 , 66.7 A/dm^2 , 88.9 A/dm^2 and 111.1 A/dm^2 . During deposition, a graphite plate was used as the negative electrode, and the solution was degassed

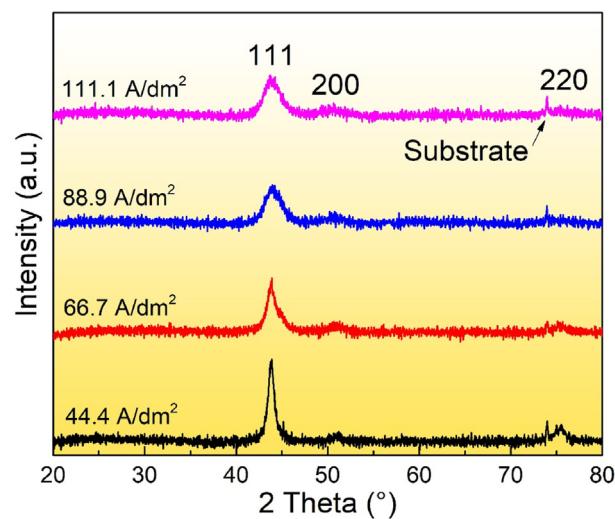


Fig. 1 – XRD patterns of CoNiFe MEA films as a function of current density.

with air. The deposition rate was evaluated using weight gain (see Fig. S1).

2.2. Structural characterization

The crystal structure of the MEA films was determined by X-ray diffraction (XRD, Rigaku Ultima IV) with Cu K α radiation. The operating voltage was 40 kV, while the operating current was 30 mA. The surface morphology was analyzed using field emission scanning electron microscopy (FE-SEM, Zeiss Merlin Compact and FEI Sirion) equipped with energy dispersive spectrometry (EDS, Oxford Instruments X-Max). The free-standing TEM specimen was mechanically peeled off from the substrate. The microstructure features were also examined in detail by scanning transmission electron microscopy (STEM, Talos F200X) with energy dispersive spectrometry (EDS, Oxford Instruments X-Max) operating at an accelerated voltage of 200 kV.

2.3. Electrocatalytic measurements

Electrochemical tests were carried out using an electrochemical workstation (CHI-760 E) in a 3.5 wt.% NaCl solution at room temperature. Various electrodeposited MEA films were used as working electrodes with an exposed area of 1.0 cm^2 . A KCl saturated silver/silver chloride (Ag/AgCl) electrode was selected as the reference electrode, while a platinum mesh was used as the counter electrode. The open circuit potential (OCP) of each sample was continuously monitored for 30 min to obtain a steady potential, and the results were shown in Fig. S2. Electrochemical impedance spectroscopy (EIS) was recorded at 0 V. The frequency range was from 0.1 Hz to 10 MHz, while the sinusoidal perturbation was 5 mV. The EIS data was fitted using a software. Potentiodynamic polarization was carried out with a scanning rate of 1.0 mV/s. The potential was swept from -0.5 V to 0.1 V . The polarization curves were analyzed to acquire the electrochemical parameters using the Tafel extrapolation method.

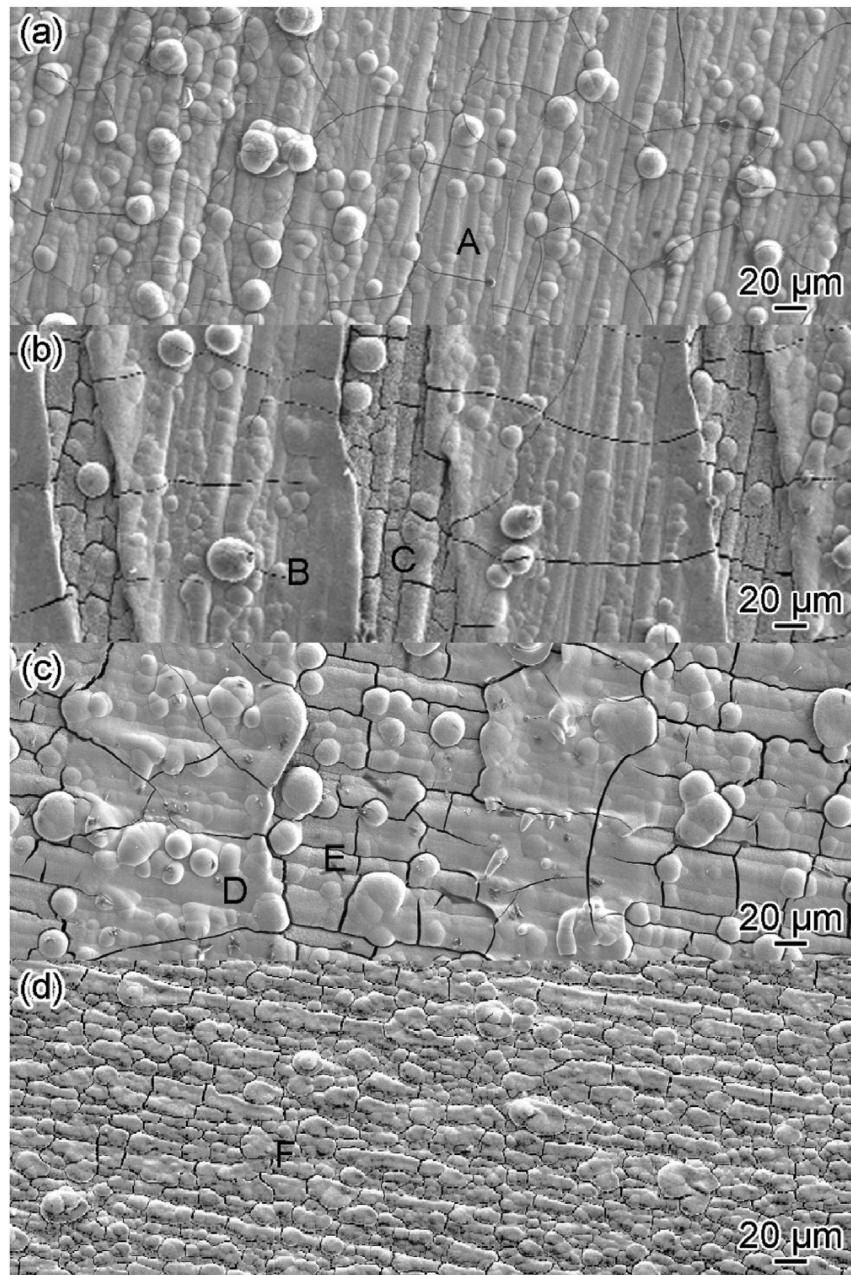


Fig. 2 – SEM images of CoNiFe MEA films with different current densities of (a) $44.4 \text{ A}/\text{dm}^2$, (b) $66.7 \text{ A}/\text{dm}^2$, (c) $88.9 \text{ A}/\text{dm}^2$ and (d) $111.1 \text{ A}/\text{dm}^2$.

3. Results

As shown from the XRD patterns in Fig. 1, all MEA films exhibit face-centered cubic (FCC) structures. It shows a strong (111) peak and weak (200) (220) peaks. Furthermore, it was observed that the (111) peaks broadened with an elevated deposition rate. Among all the MEA films, there is a highly <111> preferred orientation. This can be attributed to the reasonable process parameters of direct current electrodeposition.

Fig. 2 shows the surface morphology of the MEA films obtained at different current densities, i.e., $44.4 \text{ A}/\text{dm}^2$, $66.7 \text{ A}/\text{dm}^2$, $88.9 \text{ A}/\text{dm}^2$ and $111.1 \text{ A}/\text{dm}^2$. Interestingly, different surface morphologies were developed, depending on the

current density. The differences in chemical composition of the microstructure were evaluated with the aid of EDS results, as shown in Table 1. Combined with the XRD results, the MEA film obtained at a low current density of $44.4 \text{ A}/\text{dm}^2$ shows near-equimolar ternary components with an FCC structure. The MEA films obtained at a higher current density of $66.7 \text{ A}/\text{dm}^2$ and $88.9 \text{ A}/\text{dm}^2$ show two FCC phases with different chemical compositions. Ni-rich phase was formed at high current density. When the current density is as high as $111.1 \text{ A}/\text{dm}^2$, the MEA film consists entirely of Ni-rich phase. On the other hand, the different crack laws of the two phases can also enable the two phases to be identified. Fig. 3 shows the EDS mapping results of the CoNiFe MEA film with a current density

Table 1 – EDS results of CoNiFe MEA films (at. %).

	Co	Ni	Fe
A	34.5%	33.1%	32.4%
B	38.9%	27.6%	33.5%
C	26.1%	52.3%	21.6%
D	36.5%	25.7%	37.9%
E	20.1%	59.8%	20.1%
F	18.5%	60.9%	20.6%

of $88.9 \text{ A}/\text{dm}^2$. It shows the differences between the distribution of elements in the two phases.

Fig. 4 shows the HAADF image and EDS results of the MEA film obtained at a current density of $44.4 \text{ A}/\text{dm}^2$. The Co, Ni and Fe element mapping images reveal a uniform chemical composition. In Fig. 5, it shows the HRTEM image. Notably, each bump-like microstructure in the SEM images (Fig. 2) includes a large amount of nanosized grains, which is consistent with the existing works on conventional binary alloys [40–43]. The d-spacing of the grain marked by the yellow line is measured to be 0.206 nm . It is indexed as the plane $(111)_{\text{FCC}}$. The typical size of the grain is $\sim 4 \text{ nm}$, which is referenced to the grain marked in yellow.

Polarization curves were measured to study the corrosion behavior of the CoNiFe MEA films in 3.5% NaCl solution (Fig. 6). The self-corrosion current density (i_0) and self-corrosion potential (E_0) were collected from the polarization curves and are listed in Table 2. Notably, although the self-corrosion potentials showed similar values, the self-corrosion current densities became larger with increasing current density. Among all the MEA films, the film with a current density of $44.4 \text{ A}/\text{dm}^2$ showed the strongest corrosion resistance in 3.5 wt.% NaCl solution, and its self-corrosion current density was

$4.72 \times 10^{-6} \text{ A} \cdot \text{cm}^{-2}$. This shows the advantage of the microstructure with a near-equimolar chemical composition.

Fig. 7 shows the EIS test results of MEA films and corresponding fitting curves. In all curves, there was an oblique line in the low-frequency region and a capacity loop in the high-frequency region observed, which can be attributed to the Nernst diffusion-controlled process and the charge transfer process of the corrosion, respectively. R_s [$Q (R_{ct}W)$] [44] was selected as the equivalent circuit, where R_s was the solution resistance from the reference electrode to the working electrode, Q was the constant phase element, R_{ct} was the charge transfer (Faraday) process, and W was the Warburg impedance controlled by Nernst diffusion.

The calculated values of the elements are listed in Table 3. With the increased current density from $44.4 \text{ A}/\text{dm}^2$ to $111.1 \text{ A}/\text{dm}^2$, the R_s of the solution resistance almost remained, while Q was increased. Such Q reflected the increase in the double layer capacity [45]. However, the decrease in R_{ct} and W values reflects the acceleration of the charge transfer and Nernst diffusion processes during corrosion. This means that the mechanism turned to the Nernst diffusion controlling process from the mixed-controlling process. The largest value of R_{ct} was 331.2Ω in the MEA film with a current density of $44.4 \text{ A}/\text{dm}^2$. This indicates the large resistivity of the corrosion process in the 3.5 wt.% NaCl solution.

4. Discussion

4.1. Growth mechanism of electrodeposited MEAs

The above micrographs of electrodeposited MEAs show different morphologies as a result of simply changing the

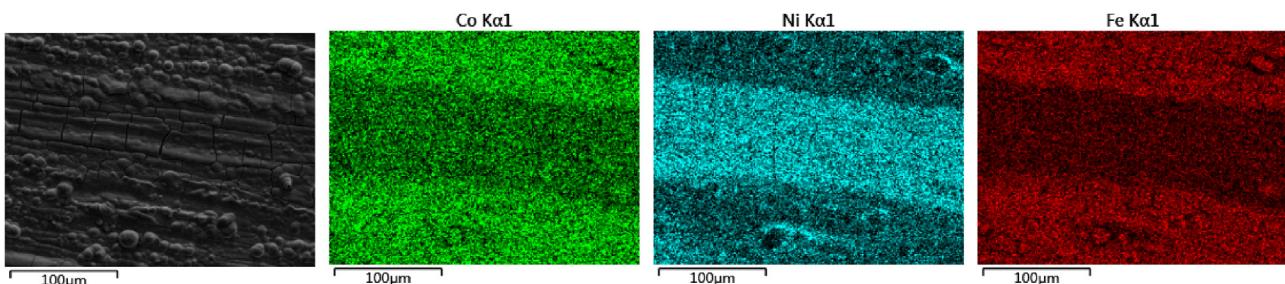


Fig. 3 – EDS mapping results of the CoNiFe MEA film with a current density of $88.9 \text{ A}/\text{dm}^2$.

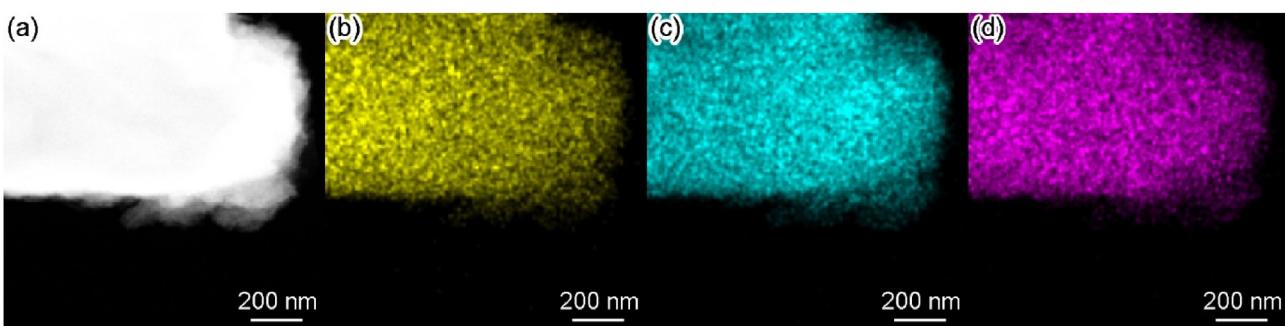


Fig. 4 – HAADF image and EDS mapping results of the MEA film with a current density of $44.4 \text{ A}/\text{dm}^2$. (a) HAADF image, (b) Co mapping, (c) Ni mapping and (d) Fe mapping.

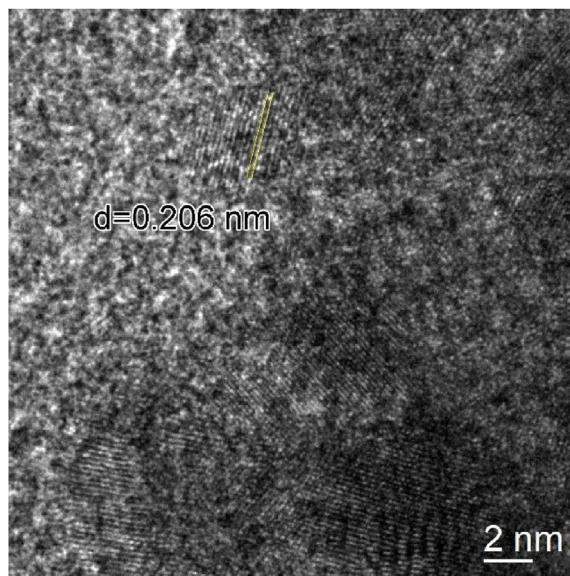


Fig. 5 – HRTEM image of the MEA film with a current density of $44.4 \text{ A}/\text{dm}^2$.

current density. Notably, the nucleation rate depends on the current density during electrodeposition [46]. Thus, the growth cannot be speeded continuously since a higher current density favors nucleation more than growth. At high current densities, there is an excess supply of Ni ions, which leads to nonuniform growth of nucleation perpendicular to the substrate [47]. Crystallization involves the incorporation of adions in the crystal lattice either by the formation of crystals or the building of as-grown crystals [48]. Crystal formation can be promoted by a high adatom population, high overpotential and low surface diffusion rate [49]. With a higher current density, both the adatom population and overpotential increased. As a result, the nucleation rate was increased at high current densities. The rate of nucleation formation, v , can be described as [50],

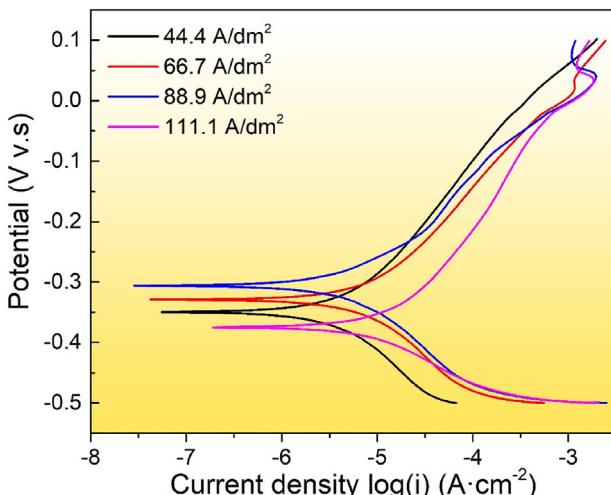


Fig. 6 – Polarization curves of CoNiFe MEA films with different current densities.

Table 2 – Self-corrosion current density (i_0) and self-corrosion potential (E_0) of MEA films with different electrodeposition current densities in 3.5% NaCl solution.

Current density (A/dm^2)	$i_0 (\text{A} \cdot \text{cm}^{-2})$	$E_0 (\text{V v.s.})$
44.4	4.72×10^{-6}	-0.350
66.7	8.59×10^{-6}	-0.323
88.9	8.72×10^{-6}	-0.306
111.1	1.54×10^{-5}	-0.375

$$v = K_1 \exp(-K_2/|\eta|) \quad (1)$$

where K_1 is the proportionality constant, K_2 including the current density is the amount of energy needed for nucleation, and η is the crystallization overpotential. It was inferred that the overpotential increased with the higher current density, and then the nucleation rate was increased. Notably, several works on conventional binary electrodeposited alloys [48,51,52] reported that the chemical composition changes with the current density as different positive ions were present in different concentrations in the bath during electrodeposition. In the current work, there were Co, Ni and Fe ions in different concentrations in the bath. There was phase separation induced by high current densities in the microstructure of electrodeposited MEA films. In fact, it shows a simple method to prepare medium/high entropy composites *in situ*, which is likely to be used to prepare medium/high entropy heterostructures in one step for energy and catalysis applications.

4.2. Relationship between the microstructure and corrosion resistance in MEAs

The CoNiFe MEA films deposited at different current densities show various microstructures. The one with a current density of $44.4 \text{ A}/\text{dm}^2$ shows a single FCC phase with a near-equimolar chemical composition. Those with current densities of $66.7 \text{ A}/\text{dm}^2$ and $88.9 \text{ A}/\text{dm}^2$ were medium-entropy composites that consisted of a Ni-rich FCC phase and a Ni-

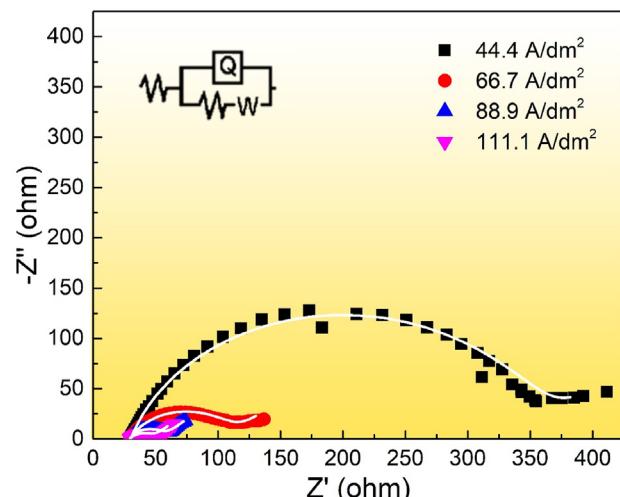


Fig. 7 – EIS test results of CoNiFe MEA films and corresponding fitting curves.

Table 3 – Calculated parameters of the equivalent circuits of the EIS results.

Current density (A/dm ²)	R _s (Ω)	Q (S·s ⁿ)	n	R _{ct} (Ω)	W (S·s ^{0.5})
44.4	30.05	1.728×10^{-4}	0.8058	331.2	0.03165
66.7	29.43	5.932×10^{-4}	0.7087	84.36	0.04475
88.9	30.05	1.017×10^{-3}	0.7642	26.81	0.05249
111.1	29.57	2.406×10^{-3}	0.6321	19.65	0.07359

poor FCC phase. Another one with a current density of 111.1 A/dm² shows a Ni-rich FCC phase. Phase engineering [53] was proposed to obtain excellent performance combinations via different phase structures in CCAs [54,55]. Based on the results in the current work, MEAs with a near-equimolar chemical composition show advantages for anti-corrosion applications. In particular, a 3.5 wt.% NaCl solution was selected as the corrosive medium. A 3.5 wt.% NaCl solution is widely considered for use in anti-corrosion materials for marine applications, as its pH and chloride level are very comparable to those of sea water.

Notably, the electrodeposited nanocrystalline CoNiFe MEA with a highly <111> orientation shows a low self-corrosion current density and a self-corrosion potential, e.g., 4.72×10^{-6} A·cm⁻² and -0.350 V in the MEA with a current density of 44.4 A/dm². Electrodeposited CoNiFe MEAs show greater anti-corrosion properties than 700 °C × 1 h-annealed, cold-rolled CoNiFe MEAs with a self-corrosion current density of 2.34×10^{-5} A·cm⁻² [8]. The outstanding anti-corrosion properties distinguish the electrodeposited MEA films from currently available MEAs, meaning that if MEAs are prepared using a specific electrodeposition process, the MEAs can have potential for anti-corrosion applications.

5. Conclusions

In summary, we united the microstructure and corrosion resistance of CoNiFe MEA films with varying deposition current densities. The films show the FCC structure with a <111> preferential orientation. It shows a low self-corrosion current density of 4.72×10^{-6} A·cm⁻² in a 3.5 wt.% NaCl solution. The corrosion mechanism was proposed in combination with EIS results. The outstanding properties were attributed to the near-equimolar ternary components. The results lay a solid foundation for the development of highly oriented MEA films with strong corrosion resistance.

CRediT authorship contribution statement

W.Y. Huo: Conceptualization, Methodology, Investigation, Writing - original draft, Writing - review & editing, Supervision. S.Q. Wang: Investigation, Formal analysis. F. Fang: Writing - review & editing, Supervision. S.Y. Tan: Formal analysis. L. Kurpaska: Writing - review & editing. Z. Xie: Writing - review & editing. H.S. Kim: Writing - review & editing. J.Q. Jiang: Writing - review & editing.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgements

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Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.jmrt.2022.07.175>.

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