

High resolution wind-tunnel investigation about the effect of street trees on pollutant concentration and street canyon ventilation

Original

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1 Wind-tunnel investigation about the effect of street
2 trees on canyon ventilation

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9 **Abstract**

10 Greening cities is a key solution to improve the urban microclimate and mit-
11 igate the impact of climate change. However, the effect of tree planting on
12 pollutant dispersion in streets is still a debated topic. To shed light on this
13 issue, we present a wind-tunnel experiment aimed at investigating the effect of
14 trees on street canyon ventilation. An idealized urban district was simulated
15 by an array of blocks, and two rows of model trees were arranged at the sides
16 of a street canyon oriented perpendicularly with respect to the wind direction.
17 Reduced scale trees were chosen to mimic a realistic shape and aerodynamic be-
18 haviour. Three different spacings between the trees were considered. A passive
19 scalar was injected from a line source placed at ground level and concentration
20 measurements were performed in the whole canyon. Results show that the pres-
21 ence of trees alters the concentration field in the street with a progressive shift
22 from a nearly two-dimensional to a three-dimensional field depending on tree
23 density. The main finding is that, despite the significant spatial variability of
24 the mean concentration induced by the trees, their presence does not affect the
25 overall ventilation efficiency as the bulk exchange velocity between the street
26 canyon and the overlying atmosphere remains almost constant in the different
27 configurations.

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28 **Introduction**

29 Urban vegetation plays a key role for the livability of cities (Bozovic et al.,
30 2017). Beyond its aesthetic role, the presence of vegetation brings numerous
31 environmental benefits in urban areas. Evapotranspiration and shading have
32 cooling effects that mitigate the urban heat island (Oliveira et al., 2011; Geor-
33 gakis and Santamouris, 2017). The large surface area per unit volume of vege-
34 tative structures facilitates particle deposition which acts as a sink for pollutant
35 particles (Litschke and Kuttler, 2008). Moreover, vegetation has a fundamen-
36 tal role in the hydrological cycle: water infiltration in vegetated soils retains
37 stormwater from entering the drainage system, thus reducing the risk of flash
38 floods (Livesley et al., 2016; Busca and Revelli, 2022).

39 While the social and environmental benefits of vegetation in cities are well
40 recognized, the role of vegetation on pollutant dispersion is still controversial
41 (Janhäll, 2015) and depends on the non-trivial interaction between the flow
42 field, the vegetative elements, and the surrounding built environment (Abhijith
43 et al., 2017). This is particularly true in street canyons, where the turbulent
44 flow field is strongly influenced by the geometry of the canyon, its orientation
45 with respect to the external wind (Soulhac et al., 2008), the presence of ob-
46 stacles (Buccolieri et al., 2022), and the properties of the building walls, e.g.,
47 wall roughness and temperature (Allegrini et al., 2013; Murena and Mele, 2016;
48 Marucci and Carpentieri, 2019; Fellini et al., 2020). The presence of vegetated
49 façades on the building walls, for example, alters the near-wall velocity and may
50 result in a reduction of the turbulent air exchange (Li et al., 2022). Low-level
51 hedges, instead, generally improve the air quality at street level and thus help
52 reducing the dose of pollutants inhaled by pedestrians (Gromke et al., 2016).

53 The interaction between turbulent flow and vegetation is even more complex
54 in tree-lined avenues, where trees occupy a significant volume of the canyon and
55 their effect on pollutant dispersion depends on the properties and shape of the
56 crowns, the height of the trunks, and the planting pattern (Vos et al., 2013;
57 Huang et al., 2019). A pioneering series of wind-tunnel experiments was per-

58 formed by Gromke and Ruck (2007, 2009, 2012) to investigate this scenario. In
59 their first studies, trees were modelled as a row of small-scale trees with spher-
60 ical, permeable crowns on thin stems, placed in the middle of a street canyon
61 of unit height to width ratio H/W (Gromke and Ruck, 2007). The wind was
62 perpendicular to the canyon axis. The flow field within the canyon and the
63 concentration at the canyon walls were explored by varying different properties
64 of the trees (crown diameter, tree height, tree spacing). A relevant increase of
65 concentration at the upwind wall and a slight decrease of concentration at the
66 downwind wall were observed. These variations were more marked when the
67 canyon was occupied by the greatest volume of vegetation (large diameter of
68 crowns and small distance between the trees). To better investigate the effect
69 of tree crown porosity, in a later study, trees were replaced with a metallic cage
70 filled with different amounts of synthetic wadding material (Gromke and Ruck,
71 2009). They found that concentrations are sensitive to crown porosity only for
72 high porosity values ($> 97\%$). Adopting the same experimental conditions, Buc-
73 colieri et al. (2009, 2011) simulated a large street canyon ($H/W = 0.5$) with two
74 rows of trees. They also analysed the case of an approaching wind inclined by
75 45° with respect to the street axis. The aspect ratio of the canyon and the wind
76 direction turned out to be more influential with respect to vegetation density
77 and crown porosity. However, they evidenced that neglecting the presence of
78 vegetation in the streets would lead to significant errors in the predictions of
79 concentration levels.

80 The modification of the airflow and concentration field within streets due to
81 tree planting has been widely studied also by means of numerical simulations.
82 Reynolds-averaged Navier-Stokes (RANS) models proved to be able to qualita-
83 tively reproduce the experimental results (e.g. Gromke et al., 2008; Buccolieri
84 et al., 2009, 2011; Gromke and Blocken, 2015; Vranckx et al., 2015) but Large
85 Eddy Simulations provide a better agreement as they solve the intermittent and
86 unsteady fluctuations of the turbulent flow which plays a major role in venti-
87 lation dynamics (e.g., Salim et al., 2011; Moonen et al., 2013). However, the
88 advantages of LES involve higher computational costs that can increase by an

89 order of magnitude compared to RANS (Salim et al., 2011). Merlier et al. (2018)
90 showed that, thanks to its computational efficiency, LES with the lattice Boltz-
91 mann method (LBM) is a promising technique to predict dispersion in street
92 canyons with tree plantings.

93 Despite remarkable advances in numerical models, simulating complex and
94 porous geometries such as trees and their effect on pollutant dispersion still rep-
95 resents a challenge. Wind-tunnel experiments are thus highly recommended to
96 improve and validate existing models. To our knowledge, there is currently no
97 experimental dataset that provides a complete characterization of the concen-
98 tration field in a three-dimensional street canyon with different configurations of
99 tree planting. For these reasons, we present in this work the results from a wind-
100 tunnel experiment aimed at evaluating how tree planting influences the concen-
101 tration field within a street canyon. To this aim, we reproduce a street canyon
102 oriented perpendicular with respect to the wind direction, with two lateral rows
103 of trees and a linear source of gas to mimic vehicular emissions. To provide
104 a detailed description of the phenomenon, the concentration field is measured
105 on a high-refined measurement grid with around 1000 sampling points for each
106 configuration of tree density. The reference configuration is that of a canyon
107 closed laterally, i.e. it does not communicate with side streets. Although this
108 is an uncommon configuration, it allows us to accurately estimate the exchange
109 of pollutants between the canyon and the atmosphere above. Experiments have
110 however also been performed in a laterally open canyon, showing that the spatial
111 pattern of concentration is not significantly affected by the presence of lateral
112 openings.

113 In Section 1, the experimental setup and the adopted measurement tech-
114 niques are presented. In Section 2, we discuss the similarity criteria for the
115 aerodynamic modelling of trees and for the boundary layer in the wind tunnel.
116 The characterization of the concentration field in the street canyon is reported
117 in Section 3, together with the estimate of the ventilation efficiency. Moreover,
118 the effect of lateral conditions due to different extremities (street intersections,
119 open or closed canyon) is discussed in Section 4. Finally, the conclusions and

120 perspectives of the work are presented in Section 5.

121 **1. Experimental setup and measurement techniques**

122 *1.1. Wind-tunnel setup*

123 The experiments were performed in the atmospheric wind tunnel at the
124 laboratory Laboratoire de Mécanique des Fluides et d'Acoustique (LMFA) at
125 the École Centrale de Lyon. The aerodynamic circuit is composed by an axial
126 fan which induces wind velocities between 0.5 and 6 m/s, flow diverging and
127 converging systems, and an upwind grid for the generation of homogeneous
128 turbulence. A heat exchanger system regulates the air temperature with a
129 precision of 0.5 K. The test section of the wind tunnel is 12 m long, 3.5 m wide,
130 and 2 m high.

131 To simulate an idealized urban district (Fig. 1), the floor of the entire test
132 section was overlaid with an array of square blocks (panel a in Fig. 2). The
133 blocks were 50 cm wide and 10 cm high and made of wood and polystyrene.
134 The spacing between the obstacles was 10 cm in the spanwise direction and
135 20 cm in the lengthwise direction. In this way, we obtained a street network
136 composed of square canyons (height to width ratio $H/W = 1$) aligned with the
137 wind direction intersecting larger perpendicular streets ($H/W = 0.5$). The two
138 different proportions were selected to avoid channeling effects along the wind
139 direction and to recreate tree-lined boulevards in the direction perpendicular
140 to the wind. The blockage ratio of the model to the cross-section of the wind
141 tunnel was 5%.

142 A neutrally stratified boundary layer approximately 1.1 m depth was gener-
143 ated by combining the effect of a row of 0.95 m high Irwin spires (Irwin, 1981),
144 placed at the beginning of the test section, and the building-like obstacles on
145 the floor. Moreover, the obstacles were covered by 5 mm high bolts to generate
146 further roughness and accelerate the full development of the boundary layer.
147 The free stream velocity at the top of the boundary layer (U_∞) was kept con-
148 stant around 5 m/s. More details about the boundary layer above the obstacles

149 is given in Section 2.2.

150 The reference street canyon (see photo reported in Fig. 2.c) was placed
151 perpendicular to the wind direction, at a distance of approximately 9 meters
152 from the beginning of the test section. Its length (L), width (W), and height
153 (H) measured 1.0 m, 0.2 m, and 0.1 m, respectively (Fig. 2.b and d). In a 1:200
154 scale, the street canyon matches fairly well a typical tree-lined boulevard, 40 m
155 wide and flanked by 20 m high buildings, as in typical European city centres
156 (e.g., Barcelona, Turin, Lyon). Note that, in the experiment, the length of the
157 canyon does not cover the whole width of the test section. This choice is made
158 in order to define a control volume in which to apply the mass balance for an
159 accurate estimate of the ventilation efficiency (see Section 3.2). We are aware
160 that other boundary conditions are possible, for instance street intersections or
161 an indefinitely long canyon. The effects of different lateral extremities will be
162 discussed in Section 4.

163 To simulate urban vegetation in the street canyon, model trees were aligned
164 along two lateral rows 14 cm apart. Three different configurations for the tree
165 density were analysed: in configuration *Zero* (panel d), the street canyon was
166 empty. In configuration *Half* (panel e), seven equally spaced trees were arranged
167 along each lateral row. In configuration *Full* (panel f), the lateral rows were
168 composed of fourteen trees with no space between them. The aerodynamic
169 characterization of model trees is reported in Section 2.1.

170 To simulate vehicular emissions, a tracer was emitted by a linear source at the
171 centre of the reference street canyon. The source consisted of a stainless steel
172 tube pierced with needles emitting ethane in a gas homogenization chamber,
173 located in a slot cut in the tunnel floor. From this chamber the gas was released
174 homogeneously at street level from a 65 cm long and 1 cm wide metallic grid.
175 This design aims at minimizing the vertical momentum and maximize the lateral
176 homogeneity of the emission (Meroney et al., 1996; Marro et al., 2020). Ethane
177 was chosen as a tracer, since it has approximately the same density of air (the
178 density ratio between ethane and air being about 1.03). The source released a
179 mixture of air and ethane with a total flow rate of 4 l/min and thus a negligible

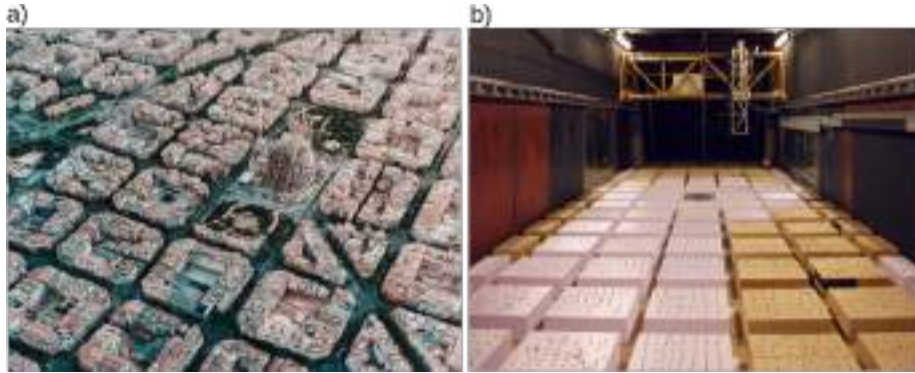


Figure 1: (a) Aerial view of the city of Barcelona (Spain). Source: *Barcelona From Above* by Ian Harper. (b) The modelled urban canopy in the wind tunnel.

180 injection velocity at street level of approximately 0.01 m/s. The percentage of
181 ethane was around 5% in volume, corresponding to a flow rate of around 0.2
182 l/min. The supply of the two gases was monitored by two digital mass-flow
183 controllers (Alicat Scientific MC-Series) working in a range between 0.5 and 20
184 Nl/min.

185 1.2. Measurement techniques

186 The concentration field within the reference street canyon was measured
187 using a Flame Ionisation Detector (FID) system (Fackrell, 1980), which is com-
188 monly used for measurements in urban-like geometries (Pavageau and Schatz-
189 mann, 1999; Carpentieri et al., 2012; Fellini et al., 2020). To avoid the disruption
190 of the local flow, a straight 30 cm long sampling capillary tube was mounted on
191 the FID head, which was positioned above the test section so as not to affect
192 the flow field. The sampling frequency of the FID signal was fixed at 1000 Hz
193 (Nironi et al., 2015). The instrument works in the range 0-10 Volt and it can
194 detect concentration values between 0 and 5000 ppm with an accuracy of about
195 1-2 ppm.

196 The measurements were performed in statistically steady conditions: a con-
197 stant flow rate of ethane was injected from the ground level source and the
198 concentration within the cavity was measured at around 1000 sampling points

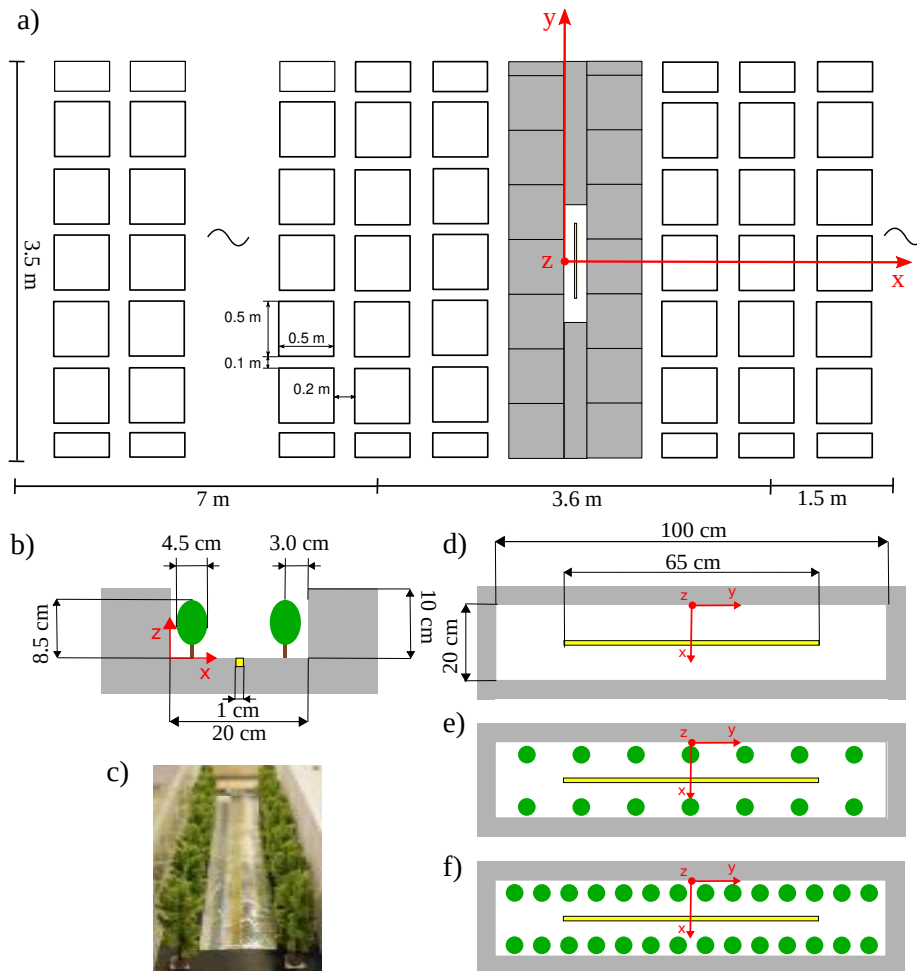


Figure 2: (a) Sketch of the urban canopy in the test section of the tunnel. The blocks delimiting the reference street canyon are coloured grey. Sketch (b) and photo (c) of the front view of the street. Top view of the street canyon model for the different configurations of tree density: (d) *Zero*, (e) *Half*, (f) *Full*. The yellow line represents the pollutant source

199 for each configuration of tree density. The measurement grid was defined to
200 characterize the entire three-dimensional volume in detail (see Fig. 1 in the
201 Supplementary Material). For each point, we fixed a sampling time of 2 min-
202 utes which provides a reliable estimate of the mean concentration. Moreover,
203 before and after each acquisition, the background concentration was recorded
204 by stopping the emission for 15 seconds (and leaving time for the transients to
205 settle). The background concentration, which was assumed to evolve linearly
206 with time from its initial to its final value, was then subtracted from the signals
207 (Marro et al., 2020; Vidali et al., 2022).

208 The velocity field above the obstacles was characterized (Section 2.2) by
209 means of a Hot-Wire Anemometer (HWA) at constant temperature, using an
210 X-wire probe with acceptance angle of 45° . In this way, two velocity components
211 of the velocity field were measured simultaneously. The platinum probe wire was
212 1 mm long and with a diameter of $5 \mu\text{m}$. The small size of the hot-wire element
213 enables good spatial resolution of the velocity field while the low thermal inertia
214 of the material ensures fast response, allowing the detection of high-frequency
215 fluctuations of the turbulent flow (Comte-Bellot, 1976). An acquisition time of
216 1 minute at a frequency of 4000 Hz was adopted for each sampling point.

217
218 For the aerodynamic characterization of the model trees (presented in Sec-
219 tion 2.1), their drag coefficient was measured in a small closed-circuit wind
220 tunnel with a 30 cm x 30 cm test section and able to generate velocities up to
221 25 m/s. The tunnel was equipped with an external load cell with a precision of
222 0.01 N. Different layouts of trees were attached to a removable plate connected
223 with the load cell. The drag coefficient was estimated for a varying wind velocity
224 inside the tunnel. Moreover, the aerodynamic porosity of the model trees was
225 evaluated by performing velocity measurements upwind and downwind a single
226 tree on a regular grid by means of a Pitot tube.

227 **2. Similarity criteria**

228 *2.1. Aerodynamic characterization of model trees*

229 To investigate the effect of trees in urban areas by means of wind-tunnel
230 experiments, buildings and vegetative structures need to be modelled in small
231 scale. Similarity criteria are then necessary to transfer small-scale findings in
232 the wind tunnel to full-scale applications. For impermeable and rigid structures,
233 like buildings, dynamical similarity between the experiment and the real appli-
234 cation exists if the model and the full-scale object are geometrically similar and
235 the value of the Reynolds number is the same (Tritton, 2012). In case of fully
236 turbulent flows around bluff bodies and/or with complex geometries, this con-
237 dition is weakened and flow similarity is assumed as far as the Reynolds number
238 is sufficiently large. On the other hand, less knowledge is available about the
239 appropriate similarity criteria for vegetative structures. From a fluid dynamical
240 point of view, vegetation is a complex porous medium made of branches and
241 leaves giving rise to the development of boundary layers, wakes, and recircula-
242 tion zones (Gromke and Ruck, 2008). Moreover, due to their flexibility, trees
243 can sway with the wind and induce fluid-structure interactions.

244 In previous wind-tunnel experiments, trees, windbreaks, and canopies have
245 been modelled by using different materials, e.g., brushes, cotton balls, metal
246 screens, and plastic stripes. Aerodynamic validation of the adopted structures
247 was done by analysing different fundamental features of the interaction between
248 the trees and the flow field, as the drag coefficient, the characteristics of the
249 wakes behind the trees (Meroney, 1968), the ratio between tree height and
250 roughness length (Meroney, 1980), the leaf area density (Chen et al., 1995), or
251 the sway frequency (Stacey et al., 1994). More systematically, Gromke and Ruck
252 (2008) analysed the aerodynamic characteristics of 12 small-scale modelled trees
253 made of different materials and porosity. Measurements of the drag coefficient
254 and of the flow field around the crowns evidenced the drag coefficient as a key
255 scale parameter for the modelling of trees. Manickathan et al. (2018) compared
256 the aerodynamic behaviour of model and natural trees in a wind tunnel. They

257 found that, together with the drag coefficient, the aerodynamic porosity of the
258 tree crown is another key parameter to compare natural and model trees.

259 In accordance with these studies, we mimicked natural trees with plastic
260 trees for railway modelling and we characterized their aerodynamic behaviour
261 by estimating their aerodynamic porosity and their drag coefficient. We also
262 investigated their optical porosity. The trees were 8.5 cm high (h_T) and 4.5 cm
263 wide (w_T), with crowns in plastic porous material on plastic trunks. Under the
264 conditions of the experiment, tree models behaved like rigid bodies and thus
265 deformations and fluid-structure interactions could be neglected.

266

Aerodynamic porosity (α_p) is defined (Guan et al., 2003) as the ratio of the
time average wind speed behind the obstacle (U_b) and the average speed of the
approaching wind (U_{ref}):

$$\alpha_p = \frac{\int_{A_c} U_b(x, y) dA_c}{\int_{A_c} U_{ref}(x, y) dA_c}, \quad (1)$$

267 where A_c is the projected frontal area of the obstacle. In other words, aero-
268 dynamic porosity determines the portion of the flow that passes through the
269 porous material with respect to the flow that diverges from the obstacle. To
270 estimate α_p , we performed velocity measurements upstream and downstream
271 a single tree that was placed on a raised block in the wind tunnel so that the
272 incident flow was not affected by the boundary layer and the integral at the de-
273 nominator in Eq. 1 could be replaced by the simple product $U_{ref} \cdot A_c$. Behind
274 the tree (in the first plane not occupied by the tree branches) point velocities
275 were measured on a regular and dense grid and a two-dimensional velocity field
276 was obtained through spatial interpolation. The average velocity was then esti-
277 mated by integrating the velocity field over the tree silhouette (Fig. 3.b). The
278 mean speed upstream (U_{ref}) and downstream (U_b) the tree were 4.95 m/s and
279 1.48 m/s, respectively. By means of Eq. 1, we obtained $\alpha_p = 0.3$, a value in line
280 with that of common natural trees, as hollies and cypresses (see square markers
281 in Fig. 3.d from the study of Manickathan et al. (2018)).

282

The optical porosity β_p is another commonly used parameter to characterize the vegetation and it can be easily estimated by elaborating digital photos (Velarde et al., 2018). It is defined as the ratio between the open surface of a porous material and its total surface. Through a digital elaboration of the photo capturing the frontal view of the model tree (Fig. 3.a), we delimited the silhouette of the tree and obtained its cross-section, $A_c \approx 3.5 \times 10^{-3} \text{ m}^2$. Then, we estimated the optical porosity, $\beta_p \approx 0.05$, as the ratio of the number of white pixels to the total number of pixels within the silhouette of the tree. According to the empirical relationship found experimentally by Guan et al. (2003), the optical porosity (β_p) is related to the aerodynamic porosity as:

$$\alpha_p \simeq \beta_p^n, \quad (2)$$

283 where the exponent n was estimated by Guan et al. (2003) equal to 0.4 for re-
 284 alistic windbreak. Introducing our estimated values for α_p and β_p in Eq. 2, we
 285 find $n \approx 0.402$ that is consistent with the cited study. The relation in Eq. 2 can
 286 then be conveniently used for deriving the aerodynamic porosity when velocity
 287 measurements cannot be directly performed.

288

The drag coefficient is defined as:

$$c_d = \frac{2F}{\rho_a U_{ref}^2 A_c}, \quad (3)$$

289 where F is the drag force [N], ρ_a is air density [kg/m^3], U_{ref} is the reference
 290 velocity [m/s] for the approaching wind, and A_c is the projected frontal area of
 291 the tree [m^2]. The drag force F was measured by means of a load cell, while
 292 the velocity U_{ref} was measured with a Pitot tube, as explained in Section 1.2.

293 In Fig. 3.b, we report the drag coefficient as a function of the wind velocity
 294 U_{ref} and Reynolds number Re for four different faces of a single model tree, ob-
 295 tained by rotating the vertical axis of the tree at intervals of 90° . The Reynolds
 296 number was calculated as $Re = U_{ref} H_T / \nu$, where H_T is the tree height and ν
 297 is the air kinematic viscosity ($\nu \approx 1.55 \times 10^{-5} \text{ m}^2/\text{s}$ at a temperature of 25°C).
 298 Except for the values at low speed (where the experimental uncertainty of the

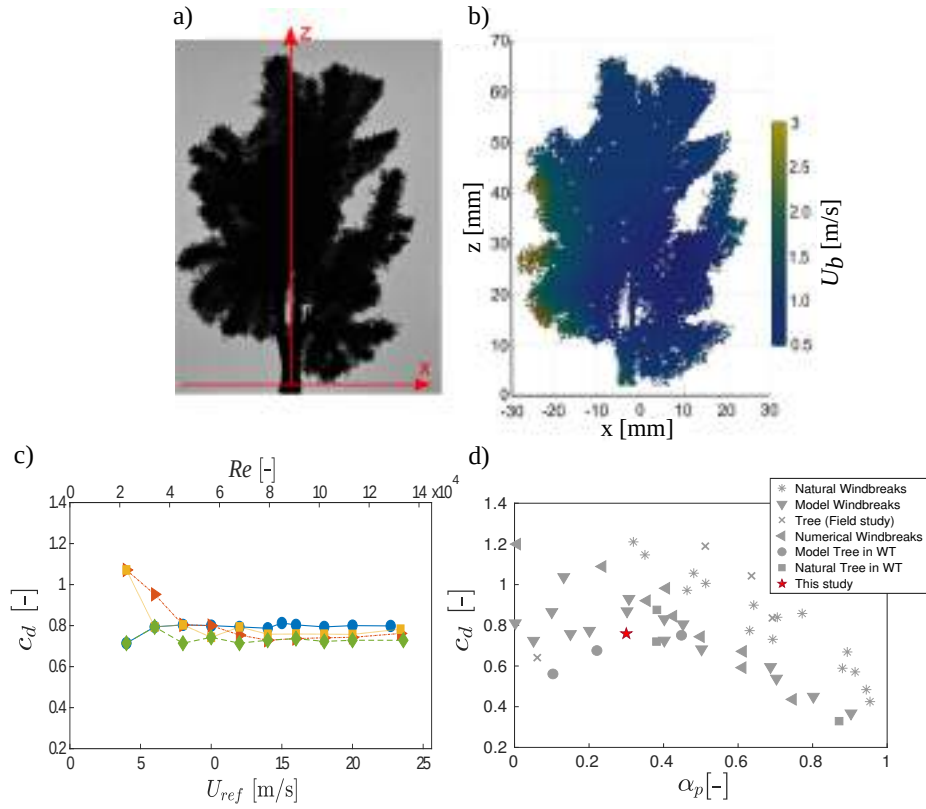


Figure 3: a) Front photo of the model tree. b) 2D velocity field downstream the tree obtained by spatial interpolation of point velocity measurements for the estimation of α_p . c) Drag coefficient as a function of Reynolds number and wind velocity for four different positions (reported by different colours) of a single model tree, obtained by rotating the vertical axis of the tree at 90° intervals. b) Drag coefficient and aerodynamic porosity for various model trees and natural trees. From the study of Manickathan et al. (2018).

299 measurement is large), the drag coefficient rapidly converges to a constant value
300 around 0.75. As shown in Fig. 3.d, this value is in line with the drag coefficient
301 of natural trees and confirms that the model trees adopted in this study present
302 realistic aerodynamic properties.

303 We note that natural trees undergo foliage reconfiguration and their drag
304 coefficient decays with increasing wind speed (Manickathan et al., 2018). This
305 is not found in our model trees that do not deform. However, since in this
306 study we focus on moderate velocities in a street canyon, we are not interested
307 in reproducing the flexibility of natural trees.

308 2.2. Characterization of the boundary layer

309 To characterize the wind flow over the obstacles, we measured vertical ve-
310 locity profiles in different positions of the wind tunnel.

311 The evolution of the boundary layer along the central axis of the wind tunnel
312 (from $x = -1.27$ m to $x = 1.27$ m) is shown in the right part of Fig. 4.a
313 (blue top x -axis). The good overlapping between the curves reveals that the
314 flow is fully developed when it approaches the reference canyon ($x = 0$), i.e.
315 its development in the stream-wise direction is so slow that changes over the
316 fetch can be neglected. As already introduced in Section 1.1, the height of
317 the boundary layer (δ) is around 1.1 m, while the free-stream velocity (U_∞)
318 is around 5 m/s. The characteristic Reynolds numbers based on the obstacle
319 height are $Re_\infty = U_\infty H / \nu \approx 3.3 \times 10^4$ and $Re_H = U_H H / \nu \approx 1.25 \times 10^4$, where
320 U_H is the mean horizontal velocity at $z = H$. These values are sufficiently high
321 to ensure fully-developed turbulent flow. For a square cavity, Allegrini et al.
322 (2013) obtained a Reynolds independent flow for Re_∞ above 1.3×10^4 , while
323 Castro and Robins (1977) and Marucci and Carpentieri (2019) showed that the
324 condition was met for Re_H larger than 4000.

Four velocity vertical profiles were measured at different positions within a
periodic unit of the urban canopy (see the inset and the velocity profiles on the
left side of Fig. 4.a, red bottom x -axis). The influence of the single obstacles
is evident in the lower part of the velocity profiles (i.e. the roughness sublayer)

where a high scatter can be observed up to $z = 0.15 \delta$. Above this height, the inertial sublayer develops and the flow variables depend on the vertical coordinate only. In this zone, the mean velocity profile is usually modelled by the logarithmic law:

$$\frac{U}{u_*} = \frac{1}{\kappa} \ln \frac{z - d}{z_0}, \quad (4)$$

325 where z_0 is the aerodynamic roughness, d is the zero-plane displacement, and u_*
 326 is the friction velocity. In the literature, several techniques have been developed
 327 to determine the values of these parameters (Raupach et al., 2006). Here, we
 328 compare the results from two different methods.

329 In the first method (Salizzoni et al., 2008), the values of the three parameters
 330 were selected so as to minimize the sum of the square difference between the
 331 logarithmic velocity profile and the measurements (Fig. 4.b). The logarithmic
 332 profile only applies to a fraction of the full velocity profile. Moreover, in urban
 333 boundary layers, the inertial sublayer is squeezed by the roughness sublayer that,
 334 as seen above, extends beyond the height of the obstacles. This fact makes the
 335 delimitation of the inertial zone even more complex than in boundary layers
 336 developing over smooth or slightly rough walls. For these reasons, we explored
 337 different extensions of the fitted region in the range $0.15 < z/\delta < 0.4$. The
 338 resulting parameters were estimated equal to $u_*/U_\infty = 0.051$, $z_0/\delta = 9 \times 10^{-4}$,
 339 and $d/\delta = 0.085$.

340 In the second method, the friction velocity u_* was inferred from the vertical
 341 profile of the Reynolds shear stress $-\overline{u'w'}$, where u' and w' are the turbulent
 342 fluctuations of the horizontal and vertical velocity, respectively. Except for
 343 a thin layer close to the wall, where viscous effects are dominant, the total
 344 stress ($\tau = \rho_a u_*^2$) in the surface layer almost matches with the Reynolds stress,
 345 which is observed to be almost constant in this layer. Thus, we can write:
 346 $\tau = \rho_a u_*^2 = -\rho_a \overline{u'w'}$. Following this method, we have analysed the vertical
 347 profile of the Reynolds stresses (Fig. 4.c) which was obtained as a spatial average
 348 over the four horizontal positions reported in the inset of Fig. 4.a. A constant-
 349 stress region (red filled markers) was detected for $0.14 < z/\delta < 0.36$ and the

350 corresponding u_*/U_∞ was evaluated equal to 0.046. We note that varying the
 351 extension of the considered constant-stress region in the range $H/\delta < z/\delta < 0.4$,
 352 slight changes (of the order of 4 %) in the estimated value of u_*/U_∞ are found.
 353 The aerodynamic roughness ($z_0/\delta = 5 \times 10^{-4}$) and the zero-plane displacement
 354 ($d/\delta = 0.1$) were then estimated through a linear regression of the logarithmic
 355 law in the semi-log domain.

356 The results from the two methods are slightly different but in line with
 357 previous experimental studies (Rafailidis, 1997; Salizzoni et al., 2008; Garbero
 358 et al., 2010). However, since the Reynolds stresses measured by a 45° X-probe
 359 HWA are usually underestimated by about 10%-20% (Tutu and Chevray, 1975;
 360 Cheng et al., 2007; Marro et al., 2020), we adopt the parameters estimated by
 361 minimum mean square error, namely (in non-normalized values) $u^* = 0.29$ m/s,
 362 $d = 0.09$ m, $z_0 = 1 \times 10^{-3}$ m.

363

The vertical profiles of the standard deviation of the velocity components
 (σ_u , σ_v , and σ_w) and of the turbulent kinetic energy (k) are reported in Figs. 4.d
 and e. The profiles are representative of a well developed urban boundary layer
 (Garbero et al., 2010) and can be useful for the implementation and validation
 of CFD simulations. To this aim, we also provide in Fig. 4.f the vertical profile
 of the turbulent kinetic energy dissipation rate (ε), which is a fundamental
 parameter for turbulence closure models. The dissipation rate was estimated
 from the HWA measurements as:

$$\varepsilon = \frac{15\nu}{U^2} \overline{\left(\frac{\partial u}{\partial t}\right)^2}, \quad (5)$$

364 by employing the isotropic approximation and Taylor's hypotheses of frozen tur-
 365 bulance (Hinze, 1975). The vertical profile of ε agrees well with the production
 366 rate of turbulent kinetic energy, here estimated as $\mathcal{P} \approx -\overline{u'w'} \frac{\partial \bar{u}}{\partial z}$. This shows
 367 that in most of the boundary layer, the production and dissipation of turbulent
 368 kinetic energy can be assumed to be in local equilibrium (Nironi et al., 2015).

369

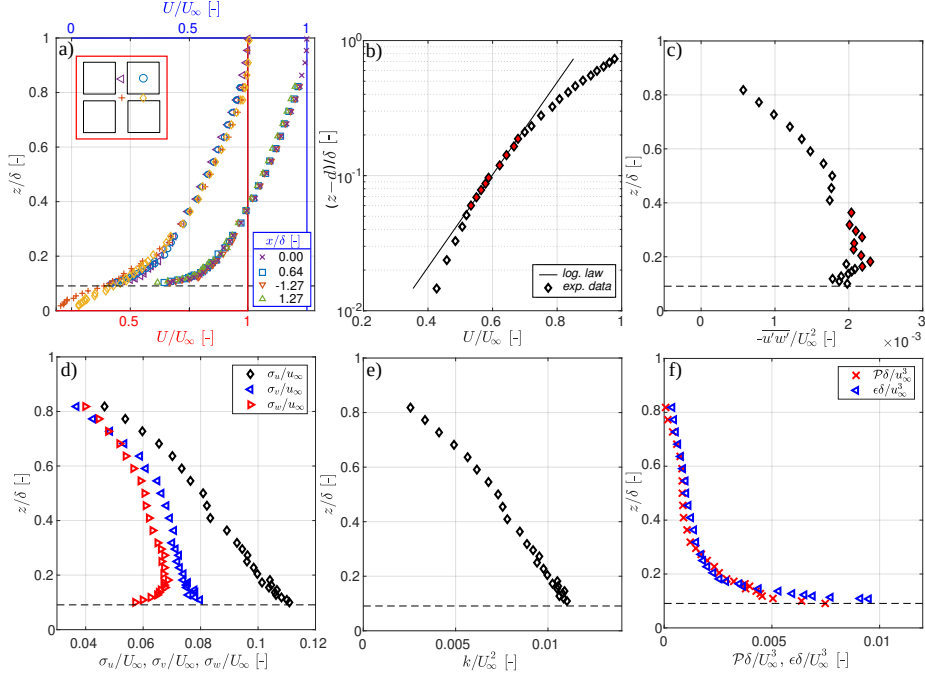


Figure 4: a) Mean velocity at 4 different position in a periodic unit (red bottom x -axis) and at 4 different distances along the streamwise direction of the wind tunnel (blue top x -axis). For the two groups of profiles, a vertical line corresponding the $U/U_\infty = 1$ is reported. The horizontal dashed line corresponds to the canyon roof level (H). b) Mean velocity obtained as average over four different positions. The line represents the logarithmic law with $u_*/U_\infty = 0.051$, $z_0/\delta = 9 \times 10^{-4}$, and $d/\delta = 0.085$. The full symbols indicate the region where the logarithmic law applies. c) Reynolds stresses $-\overline{u'w'}$. The full symbols indicate the constant-stress region. d) Standard deviation of the three velocity components. e) Turbulent kinetic energy. f) Production and dissipation rate of turbulent kinetic energy.

370 **3. Street canyon ventilation**

371 *3.1. Mean concentration field*

372 The mean concentration field inside the street canyon was characterized for
373 the three configurations of tree density presented in Fig. 2. As mentioned above
374 (Section 1.2), the concentration of ethane - released from the line source - was
375 measured on around 1000 sampling points (for each configuration) distributed
376 on a three-dimensional grid, by means of a Flame Ionization Detector. The non-
377 dimensional concentration is expressed as $\overline{C}^* = CU_\infty L_s \delta / Q_{et}$, where C is the
378 time-averaged concentration of ethane in each sampling point, L_s is the source
379 length, and Q_{et} is the mass flow rate of ethane. In the following, the results are
380 presented in two-dimensional sections obtained from linear interpolation of the
381 measured data. For a complete visualisation of the concentration field inside
382 the canyon refer to Section 2 of the Supplementary Material.

383 Figure 5 shows two cross-sections for each configuration of tree density. Pan-
384 els a-c report the concentration field on a lateral cross-section ($y/H \approx -15$),
385 whereas panels d-f correspond to the central (around $y/H \approx 0$) cross-section.
386 Regardless of the presence of trees, a clear increase in the concentration from
387 the downwind wall to the upwind wall can be observed in all the sections. This
388 pattern is in accordance with previous studies (Gromke and Ruck, 2007, 2009)
389 and evidences the action of the main recirculating cell of the velocity field inside
390 the canyon: fresh air enters the canyon at the downwind wall and transports the
391 pollutant (emitted in the centre of the street) to the upwind wall, where part
392 accumulates at the lower corner, part is moved outside and part is entrained
393 towards the downwind wall. The horizontal inhomogeneity of the concentration
394 field results in a significant difference in air quality at the pedestrian level (i.e.
395 at $z/H = 0.2$). This difference is accentuated in the presence of trees: in a
396 canyon without vegetation (Fig. 5.a and d), the concentration at the downwind
397 wall is roughly 3 times lower than the one at the upwind wall, while in presence
398 of trees this difference increases up to 8 times in the lateral section (Fig. 5.b
399 and c). We also remark that, for the non-vegetated canyon, the concentration

400 field remains almost unchanged along the longitudinal axis of the canyon (panel
401 a and d) while the presence of trees alters this behaviour: in both the *Half* and
402 *Full* configurations, pollutant concentration in the central section (panel e and
403 f) is significantly lower than in the lateral one (sections b and c).

404 To better visualize the spatial distribution of the concentration field, we
405 show in Fig. 6 the horizontal section along the canyon axis, at $z/H=0.5$. The
406 concentration gradient along the x -axis, from the downwind to the upwind wall,
407 is clearly visible in all three configurations. As found above, this gradient is
408 enhanced in the vegetated canyons. Analysing the concentration near the walls
409 (see also the entire cross sections at $x/H = 0.1$ and $x/H = 1.9$ in the Sup-
410plementary Material), we find that this is due to an average increase in the
411 concentration at the upwind wall in the vegetated canyons, rather than to a
412 decrease of the concentration at the downwind wall, which remains almost con-
413stant in the different configurations. This result is in line with the study of
414 Buccolieri et al. (2009) who found that the presence of trees lead to a significant
415 increase in pollutant concentration at the upwind wall and slight to moderate
416 decrease at the downwind wall.

417 Figure 6 also shows that along the longitudinal axis (y -axis), the concentra-
418 tion is almost homogeneous in the *Zero* configuration (panel a), except for the
419 low values at the edges of the domain due to the limited length of the linear
420 source. On the other hand, the homogeneity along the y -axis is lost when trees
421 are added. In the *Full* configuration (panel c), it is possible to identify a region
422 with lower concentration in the middle of the canyon and two nearly symmetric
423 accumulation regions at its sides. In the *Half* configuration (panel b), the con-
424 centration field is even more heterogeneous and three accumulation regions can
425 be identified. The same spatial distribution can be inferred from Fig. 7, where a
426 vertical section in the middle of the canyon ($x/H=1$) is represented. Again, we
427 observe a homogeneous concentration field in the empty canyon, while pollution
428 peaks are evident in the *Half* and *Full* configurations. Along the vertical axis,
429 the concentration remains fairly constant. This is typical in the centre of the
430 canyon and was already visible when focusing on vertical profiles at $x/H=1$ in

431 Fig. 5. Moving towards the upwind wall (Fig. 8 shows the vertical section at
432 $x/H=0.15$), however, the concentration is greater at street level and a gradient
433 along the vertical axis emerges.

434 By averaging the concentration over the vertical direction (z), we obtain (see
435 Fig. 9) the concentration profile along the longitudinal axis (y), in the centre
436 of the canyon ($x/H=1$). The profiles highlight the transition from an homo-
437 geneous concentration in the empty canyon to a spatial distribution exhibiting
438 pronounced peaks in the vegetated canyons. Furthermore, the increment in
439 the number of trees produces a decrease in the minimum concentration in the
440 centre of the canyon and a slight intensification of the maximum values. We
441 note that the cross-sections shown above in Fig. 5 were taken at the minimum
442 ($y/H \approx 0$) and maximum (left side, $y/H \approx -15$) concentration values for each
443 configuration.

444 Finally, from the characterization of the concentration field along the canyon
445 (Figs. 6-8), some observations on the local effect of trees on pollution can
446 be deduced. For both configurations with trees, the inhomogeneity along the
447 longitudinal axis (y) is maintained along the x -axis (Fig. 6), both near the two
448 rows of trees ($x/H \rightarrow 0$ and $x/H \rightarrow 2$) and in the centre ($x/H \rightarrow 1$). Furthermore,
449 the number of concentration peaks (2 and 3 in the *Full* and *Half* configurations,
450 respectively) and their spacing do not correspond to the number and spacing of
451 the trees, represented by dashed lines in Figs. 6 to 8. These two aspects, namely
452 the concentration inhomogeneity along the y -axis in the centre of the street and
453 the independence of the concentration peaks on tree pattern, suggest that the
454 variation of the concentration field along the canyon is not due to local effects
455 of trees acting as obstacles. Rather, the presence of trees seems to modify the
456 dynamics of flow and dispersion within the whole canyon leading to a different
457 spatial organization of the concentration field at the canyon-scale.

458 3.2. Vertical exchange velocity

459 While the previous section highlighted the effect of trees on the spatial pat-
460 tern of the concentration field, in this section we investigate the effect of veg-

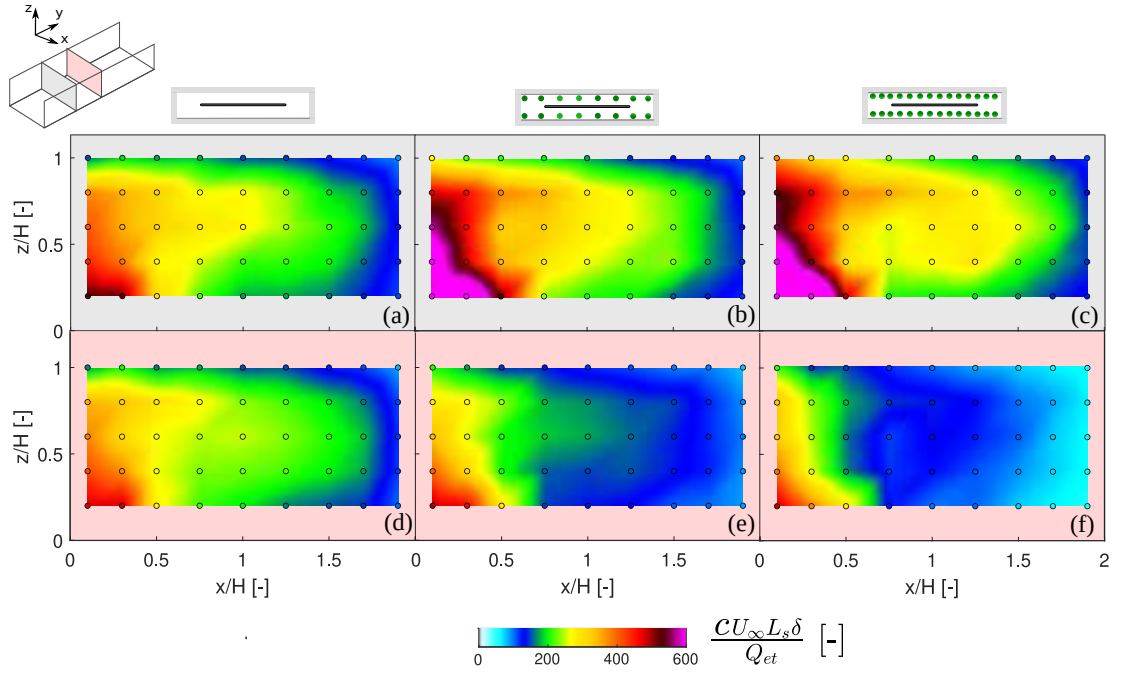


Figure 5: Mean concentration of the passive scalar on a lateral cross-section at $y/H \approx -15$ (first line) and in the centre of the canyon $y/H \approx -0$ (second line). *Zero* (a and d), *Half* (b and e) and *Full* (c and f) configurations are shown. Measurement points are reported as circles colored according to the measured value.

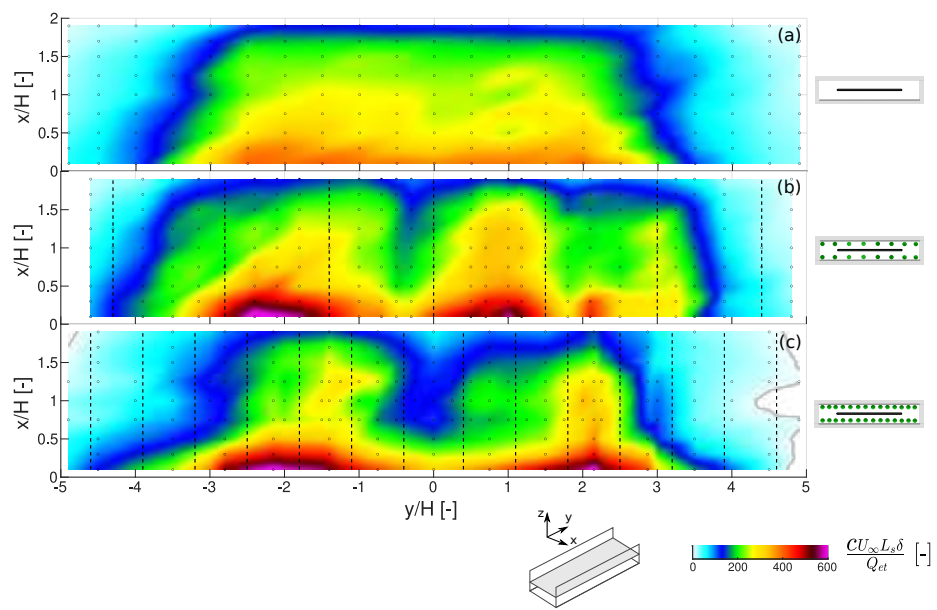


Figure 6: Mean concentration of the passive scalar on the horizontal section at $z/H=0.5$. *Zero* (a and d), *Half* (b and e) and *Full* (c and f) configurations are shown. The position of trees is represented by dashed lines. Measurement points are reported as circles colored according to the measured value.

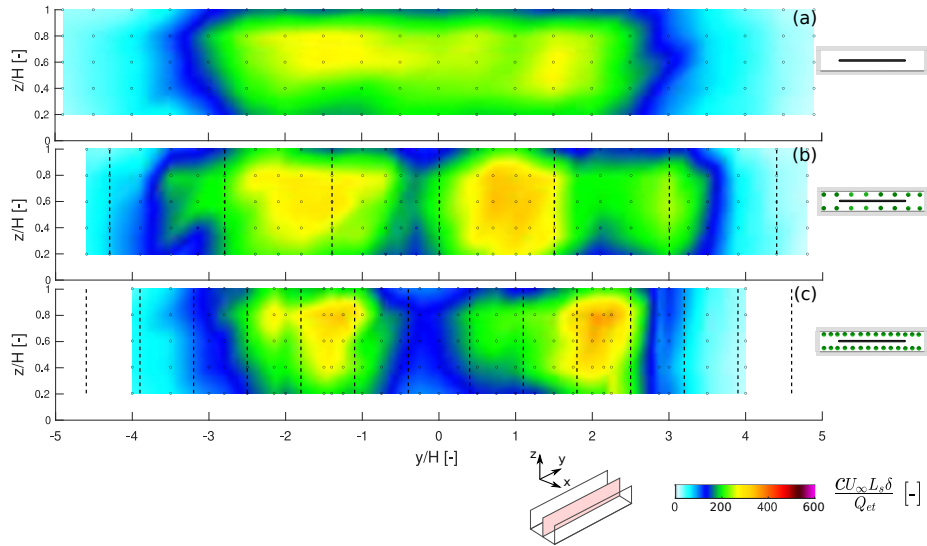


Figure 7: Mean concentration of the passive scalar on a vertical section at $x/H=1$. *Zero* (a and d), *Half* (b and e) and *Full* (c and f) configurations are shown. The position of trees is represented by dashed lines. Measurement points are reported as circles colored according to the measured value.

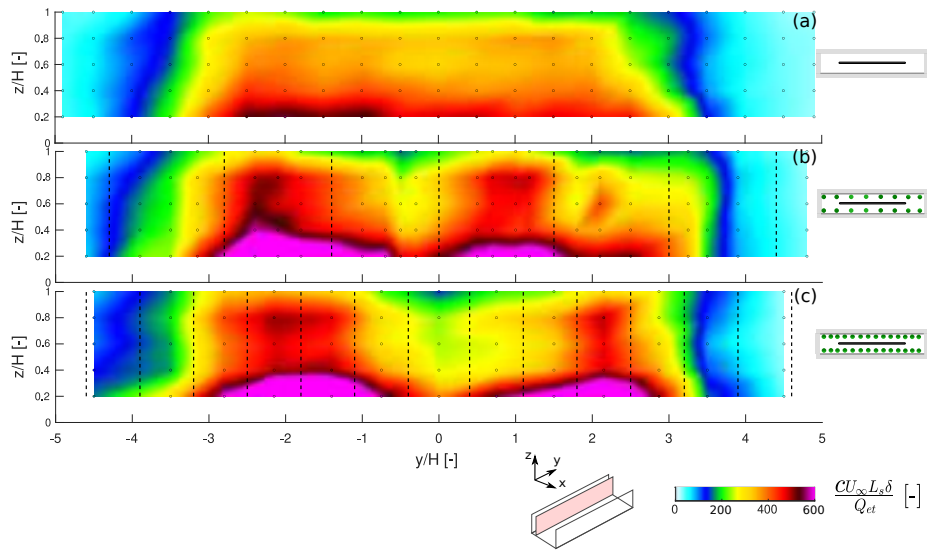


Figure 8: Mean concentration of the passive scalar on a vertical section at $x/H=0.15$. *Zero* (a and d), *Half* (b and e) and *Full* (c and f) configurations are shown. The position of trees is represented by dashed lines. Measurement points are reported as circles colored according to the measured value.

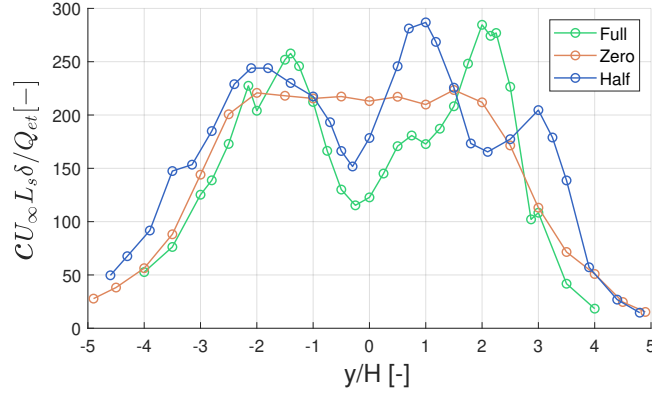


Figure 9: Concentration profile along the canyon axis ($x/H = 1$) for the three configurations of tree density. Each point is obtained as the average concentration along the vertical axis (z).

461 etation on the ventilation efficiency of the canyon. To this aim, we adopt a
 462 box model with one degree of freedom to evaluate the wash-out velocity of the
 463 canyon for the different configurations of tree density.

The canyon is described as a unique box with volume-averaged concentration and a domain boundary surface at the roof height (of area $L \cdot W$). The mass balance for the canyon reads:

$$V \frac{\partial C_{vol}}{\partial t} + \int_{-L/2}^{L/2} \int_0^W [\overline{w\bar{c}}]_{z=H} dx dy = Q_{et}, \quad (6)$$

where V is the volume of the canyon, Q_{et} is the mass flow rate of ethane at the source, C_{vol} is the mean concentration in the canyon, and $\overline{w\bar{c}}$ is the mass flux of passive scalar in the vertical direction. This latter is provided by the time-averaged product of the instantaneous vertical velocity w and concentration c . Following Soulhac et al. (2013), the vertical flux at roof level can be parametrized as the product of a bulk exchange velocity u_d and the difference between the concentration within the canyon (C_{vol}) and the concentration in the external flow (C_{ext}):

$$u_d(C_{vol} - C_{ext})WL = \int_{-L/2}^{L/2} \int_0^W [\overline{w\bar{c}}]_{z=H} dy dx. \quad (7)$$

In steady state conditions (i.e. $\partial C_{vol}/\partial t = 0$) and assuming that C_{ext} is neg-

ligible, Eqs. 6 and 7 can be combined, and the exchange velocity expressed as (Salizzoni et al., 2009):

$$u_d = \frac{Q_{et}}{C_{vol}WL}. \quad (8)$$

or in non-dimensional form as:

$$\frac{u_d}{U_\infty} = \frac{L_s\delta}{C_{vol}^*WL}, \quad (9)$$

464 where C_{vol}^* is the non-dimensional concentration averaged over the volume and
 465 L_s is the source length inside the volume. Thanks to this formulation, the
 466 vertical exchange velocity can be easily estimated from the quantities measured
 467 in the experiment: the flow rate at the source Q_{et} is imposed and monitored
 468 by a mass-flow rate controller, while the FID measurements inside the street
 469 canyon provide the average concentration in the entire volume (C_{vol}^*).

470 In this regard, we recall that the choice of reproducing a canyon closed at
 471 the lateral edges was made to simplify the estimation of the exchange velocity
 472 u_d . Otherwise, in the case of a canyon with lateral street intersections, the
 473 mass balance in Eq. 6 would also include the flux of passive scalar along the
 474 longitudinal direction (i.e. the mass flux $\overline{v\bar{c}}$ provided by the transversal velocity
 475 v along y and integrated at the lateral boundaries of the domain, at $y = -L/2$
 476 and $y = +L/2$). This additional term would also appear in Eqs. 8 and 9 and
 477 thus the estimation of u_d would require additional coupled measures of velocity
 478 and concentration. In the case of an infinitely long canyon (i.e. a canyon long as
 479 the wind-tunnel width), the balance would be applied to a reference volume since
 480 the fine characterization of the entire canyon length would be experimentally
 481 unfeasible. Also in this case, the estimate of the transverse mass flux at the
 482 lateral boundaries of the reference volume would be necessary to estimate u_d .

483 The mean concentration within the canyon was estimated with different spa-
 484 tial averaging techniques of the measurements: (i) the rough mean of the data,
 485 (ii) the mean weighted by the volume associated to each measurement point,
 486 and (iii) the mean over a regular concentration grid obtained from interpolation
 487 of the measurements. Table 1 reports the values of C^* obtained with these
 488 different methods. The greatest differences in the estimation of C^* are found

489 for the *Full* configuration, where the measurement grid is more irregular due to
 490 the presence of trees. In this case, the method adopted for the spatial integra-
 491 tion can affect the results. Regardless the method used, we observe that the
 492 concentration average in the whole volume of the canyon remains substantially
 493 unchanged with the density of trees. This evidences that, while the spatial
 494 variation of the concentration field (Figs. 5-8) significantly varies due to the
 495 presence of trees, the average pollution level inside the canyon remains almost
 496 unaltered. This is a remarkable and unexpected result, as it is generally believed
 497 that trees, acting as aerodynamic obstacles, are responsible for the accumulation
 498 of pollutants in the street.

499 To better quantify the effect of trees on street canyon ventilation, we use
 500 Eq. 9 to estimate the exchange velocity u_d , starting from C_{vol}^* . The values
 501 of u_d are also presented in Table 1 and show, once again, that the influence
 502 of trees on ventilation efficiency is almost negligible. Furthermore, a trend of
 503 u_d with the vegetation density is absent, being the *Half* configuration the one
 504 exhibiting the lowest exchange rate. We also note that the estimated values of
 505 u_d are higher with respect to those found by Salizzoni et al. (2009), Soulhac
 506 et al. (2013), and Fellini et al. (2020) for a square cavity ($H/W=1$), confirming
 507 that the enlargement of the cavity enhances canyon ventilation.

508 The values reported in Table 1 have been estimated considering the entire
 509 canyon as the reference volume. In Fig. 10, we show how the estimate of u_d
 510 varies as a function of the size of the reference volume. To this aim, we consider a
 511 reference volume centred at $y=0$, extended to the entire width (W) and height
 512 (H) of the canyon, but of variable length (L_{vol}) along the longitudinal axis
 513 (y). For the estimate of u_d by means of Eq. 9, the average concentration is
 514 estimated as the mean of the measurement data interpolated over a regular grid
 515 ('Interpolation' in Table 1) inside the reference volume, the source length L_s
 516 becomes the effective length included inside the reference volume (L'_s in Fig.
 517 10) and the length L is replaced by L_{vol} . For the empty canyon, the exchange
 518 rate is almost unchanged as the reference volume increases. This is due to the
 519 homogeneity of the concentration field along y . In the *Full* configuration, the

		Rough	Weighted	Interpolation
$C_{vol}^* [-]$	<i>Zero</i>	155.45	162.50	155.43
	<i>Half</i>	198.61	178.75	178.74
	<i>Full</i>	178.76	143.00	162.50
$u_d/U_\infty [-]$	<i>Zero</i>	0.023	0.022	0.023
	<i>Half</i>	0.018	0.020	0.020
	<i>Full</i>	0.020	0.025	0.022

Table 1: Estimate of the volume-averaged (normalised) concentration C_{vol}^* for different spatial averaging techniques of the concentration inside the canyon: (i) rough mean, (ii) mean weighted on the reference volume of each measurement point, and (iii) mean of the three-dimensional interpolated concentration field. The corresponding values of the vertical exchange velocity u_d/U_∞ , calculated by means of Eq. 9, are also reported.

520 velocity u_d is greatly overestimated if a volume less than 40% of the total canyon
521 is considered. The reason for this is that, according to the balance in Eq. 9,
522 the lower concentration in the centre of the canyon results in a misleading high
523 ventilation efficiency. The *Half* configuration shows an intermediate behaviour
524 between the two. This analysis highlights the importance of a characterization
525 of the concentration field on an extended volume for a correct evaluation of the
526 overall ventilation efficiency. To analyse the effect of the presence of trees in
527 the street, characterizing a single two-dimensional section or a limited volume
528 in the middle of the canyon may lead to false conclusions.

529 4. Discussion about the effect of lateral boundaries

530 As mentioned above, the canyon geometry with closed extremities was adopted
531 to ensure a correct and straightforward estimate of the ventilation efficiency.
532 However, this geometry is unusual compared to classic experimental investi-
533 gations (and realistic urban geometries) and could raise the question that the
534 lateral walls modify the flow field and therefore the dispersion process. For
535 this reason, in this section we briefly discuss the effect of the lateral edges of
536 the canyon on the concentration field. To do this, we compare the results pre-

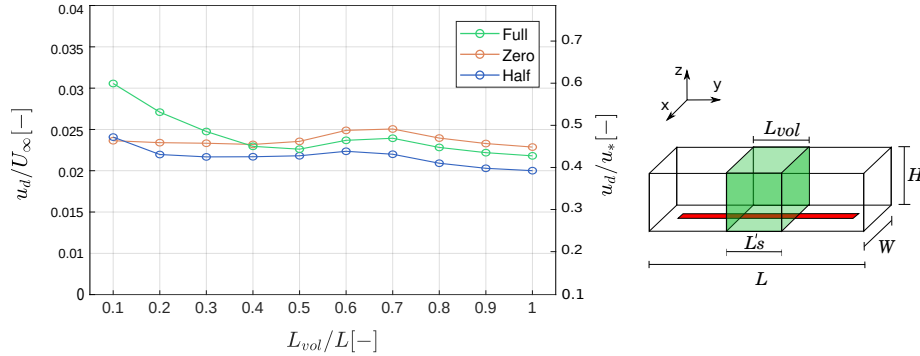


Figure 10: Estimate of the exchange velocity u_d as a function of the length (L_{vol}) of the reference volume along the longitudinal axis of the canyon.

537 sented in the previous section with concentration measurements performed in
 538 the same wind tunnel, with identical experimental conditions, but with slightly
 539 different street geometries. We note that these measurements were performed
 540 on a coarser grid with respect to that adopted for the investigation of the closed
 541 canyon. While these measurements provide a qualitative description, a deep
 542 analysis of the influence of lateral boundaries goes beyond the scope of this
 543 paper.

544 In the first laterally-open geometry (Fellini, 2021), the reference canyon is
 545 part of the network of streets that reproduces the idealized urban district. The
 546 canyon is 50 cm long and is limited laterally by two street intersections (Fig.
 547 11). Although the length-to-width (L/W) ratio is lower and a regular array
 548 of building is here present, the street geometry is similar to that adopted by
 549 Gromke and Ruck (2007, 2009), where a laterally open canyon is reproduced.
 550 Concentration measurements were performed over 4 cross-sections (sections 1 to
 551 4) covering all the canyon length and placed at $y/H \pm 1.88$ and $y/H \pm 0.63$. Re-
 552 sults for an empty canyon and a canyon with a full density of trees are presented
 553 in panels b and d of Fig. 11, respectively. The density of trees corresponds to
 554 the *Full* configuration presented in Section 1.1. Panels c and e refer to the
 555 canyon with closed lateral edges and report the concentration measured in the

556 cross-sections taken at the y/H positions closest to those of sections 1 to 4.
557 Without trees, pollution levels are significantly lower in the open canyon (panel
558 b) with respect to the laterally closed one (panel c). This is an expected re-
559 sult, as the formation of corner eddies near the intersections provide additional
560 turbulent exchange that favours the canyon ventilation. Despite this variation
561 in the pollution levels, we observe a similar trend for the concentration that
562 remains almost unchanged along the longitudinal axis. The same observations
563 can be made for the vegetated canyon: the presence of lateral intersections de-
564 creases the average concentration in the canyon but the trend along y is similar
565 with open (panel d) and closed ends (panel e). In this case, sections 1 and 4
566 exhibit an increase in the concentration with respect to section 2 and 3. This
567 trend is in line with the results found in Section 3.1 and suggests that trees
568 induce a three-dimensional concentration field.

569 A similar comparison is performed for the geometry presented in Fig. 12.a.
570 In this case, the canyon is extended to the entire width of the wind tunnel
571 ($W/H = 35$). The other geometrical properties of the canyon, as well as the
572 experimental conditions, are the same as presented in Section 1.1. Concentra-
573 tion measurements are available in four cross-sections placed in the range at
574 $y/H \pm 1.07$ and $y/H \pm 0.36$. In both the *Zero* and *Full* configurations, the
575 concentration values (panels b and d) are extremely similar to those found in
576 the closed cavity (c and e). The concentration field remains constant along the
577 axis of the canyon in the absence of trees (panel b), while in the *Full* configu-
578 ration the concentration tends to increase in sections 1 and 4 which are located
579 near the two peaks evident in Fig. 9. We note that the compared sections are
580 not in exactly the same position along the y -axis, the differences being up to
581 3 cm. This may explain the slightly higher concentration in section 4 of the
582 vegetated canyon (panels d and e). Furthermore, we highlight that in panels c
583 and d the concentration distribution and the effect of the main canyon vortex
584 can be visualized in greater detail due to the higher spatial resolution in the
585 measurements.

586 The comparisons discussed in this section suggest that the results presented

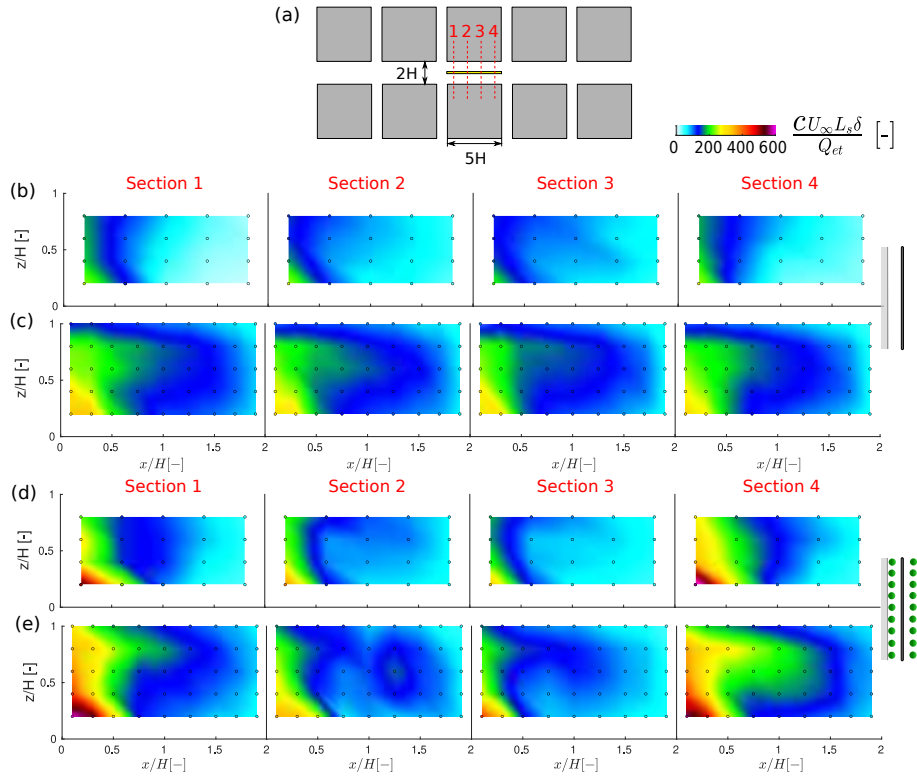


Figure 11: (a) Canyon with street intersections at the lateral extremities. Concentration in 4 cross-sections for the configuration without trees (b) and with dense trees (d). Comparison with the concentration in the closed cavity, in the *Zero* (e) and *Full* configurations.

587 in Sections 3.1 and 3.2 can be extended, with good approximation, to the stan-
 588 dard case of an indefinitely long canyon. The closure of the lateral ends does not
 589 seem to alter the ventilation dynamics. The geometry with lateral intersections,
 590 on the other hand, presents more marked differences but the presence of trees
 591 seems, even in this case, to trigger the same transition from a two-dimensional
 592 to a three-dimensional concentration field.

593 5. Conclusions

594 We have investigated the effect of trees on ventilation efficiency and pollu-
 595 tant dispersion in an urban street canyon. In a wind tunnel, we have reproduced

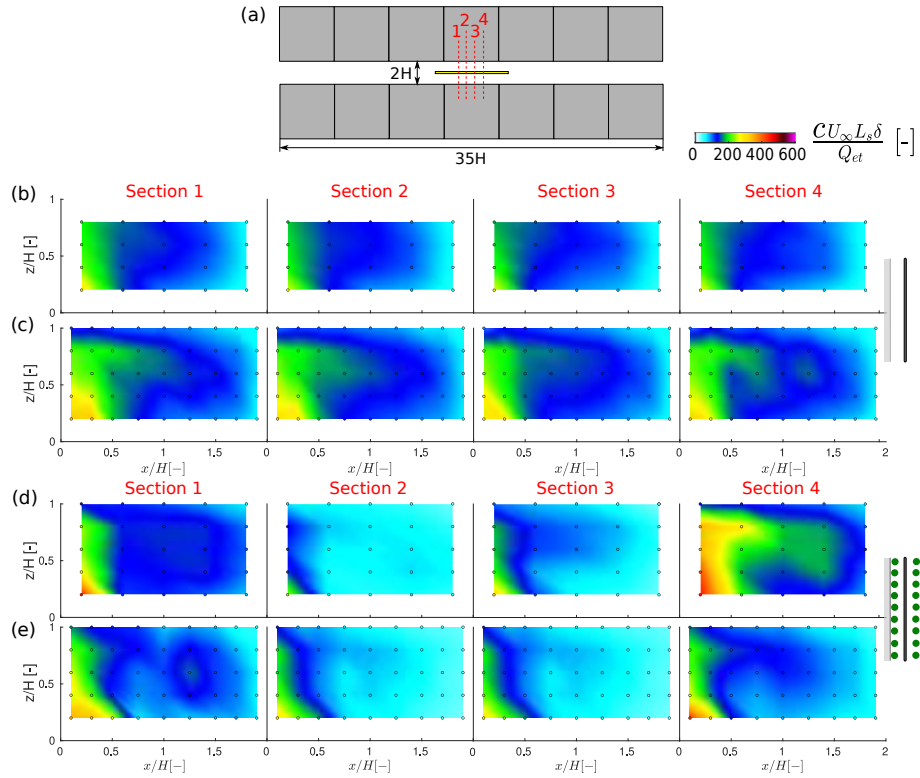


Figure 12: (a) Canyon extended to the width of the wind tunnel. Concentration in 4 cross-sections for the configuration without trees (b) and with dense trees (d). Comparison with the concentration in the closed cavity, in the *Zero* (e) and *Full* configurations.

596 a well-developed urban boundary layer over an idealized urban district simu-
597 lated by an array of square blocks. We performed velocity measurements by
598 means of an X-wire HWA in order to provide an accurate description of the
599 flow field above the obstacles. The concentration field was measured by means
600 of a FID within a reference street canyon modelled as a closed cavity oriented
601 perpendicular with respect to the wind direction. Three different configurations
602 of tree density were analysed: a non-vegetated canyon (*Zero* configuration), a
603 canyon with two rows of sparse trees (*Half* configuration), and a canyon with
604 two rows of dense trees (*Full* configuration). The model trees were aerodynam-
605 ically characterized by means of their drag coefficient and crown porosity.

606 The results show that the concentration field is homogeneous along the lon-
607 gitudinal axis of the canyon in the *Zero* configuration, and can be considered
608 nearly two-dimensional. On the other hand, the vegetated streets present a
609 remarkable three-dimensional spatial distribution of the concentration field. In
610 particular, concentration peaks alternating with low polluted regions are ob-
611 served along the canyon both in the *Half* and *Full* configurations and especially
612 at pedestrian level. Moreover, the presence of trees lead to a significant increase
613 of pollutant concentration at the upwind wall of the street, while the average
614 concentration at the downwind wall is almost constant in the different configu-
615 rations. Despite the great influence of trees on the spatial pattern of pollution,
616 the average concentration in the entire volume of the canyon does not vary with
617 the tree density, highlighting a compensation effect between the different regions
618 of the street.

619 The ventilation efficiency of the canyon was assessed by estimating the bulk
620 transfer velocity between the canyon and the boundary layer aloft. To this aim, a
621 mass balance within the laterally closed canyon was performed. In line with the
622 result about the mean concentration, the estimated velocity is almost constant
623 among the three configurations, confirming that the vegetation density does not
624 affect the overall ventilation efficiency. On the other hand, we demonstrated
625 that the characterization of the concentration field over an extended reference
626 volume is necessary to accurately estimate the transfer velocity when trees are

627 present.

628 Finally, we discussed the effect of the canyon lateral extremities on disper-
629 sion dynamics. To this aim, we compared the outcomes from two experiments
630 with slightly different canyon geometries. The presence of lateral street intersec-
631 tions increases the ventilation of the canyon and therefore decreases the average
632 pollution levels. However, both in the case of a non-vegetated canyon and in
633 the presence of trees, the trend of the concentration along the longitudinal axis
634 is similar to that found in this study. If we consider a canyon that extends to
635 the entire width of the wind tunnel, the concentration pattern is quite similar
636 to that observed in the configuration with closed ends and longitudinal mass
637 fluxes are quite negligible. Therefore, the results of this study can be general-
638 ized to the case of an infinitely long street canyon, which is a classical geometry
639 adopted in both experimental and numerical studies.

640 To conclude, thanks to the detailed characterization of the concentration
641 field, we showed that trees have a non-trivial effect on the spatial distribu-
642 tion of the pollutant concentration, leading to a highly inhomogeneous scalar
643 field and strong pollution gradients at the pedestrian level. This suggests that
644 the presence of trees affect the turbulent flow field within the canyon. A new
645 measurement campaign is currently underway to investigate the reasons for the
646 formation of pollution peaks in the presence of trees. To this aim, we character-
647 ize the structure of the turbulent flow field within the canyon and the vertical
648 turbulent mass fluxes at the roof level. While the vertical exchange velocity u_d
649 is an average quantity over the entire volume, the analysis of the vertical tur-
650 bulent fluxes should highlight whether there are spatial heterogeneities in the
651 exchange between the canyon and the atmosphere.

652 Moreover, we found that the presence of two rows of trees does not inhibit
653 the overall canyon ventilation. This result has important implications in prac-
654 tice. The estimated value of the vertical exchange velocity can be included
655 as a constant in parametric models that simulate pollutant dispersion in cities
656 (McHugh et al., 1997; Soulhac et al., 2011; Fellini et al., 2019).

657 Finally, the huge dataset provided by this experimental study can be of great

658 use for the validation of numerical simulations. To this end, the characterization
659 of the boundary layer and of the aerodynamic properties of trees (described in
660 the Section 2) are fundamental information.

661 **Data availability**

662 The experimental dataset is available on the website: [https://github.com/
663 sfellini/Tree_alpha90_HW05.git](https://github.com/sfellini/Tree_alpha90_HW05.git). We provide the concentration data inside
664 the canyon and the characterization of the flow field above the buildings.

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