## **Capillarity**

### Original article

# CO<sub>2</sub> adsorption and separation properties of M-MOF-74 materials determined by molecular simulation

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#### Abstract:

This study simulated the adsorption and separation of  $CO_2$  by the metal-organic frameworks material M-MOF-74, established the skeleton model of M-MOF-74 series adsorbent, and calculated the adsorption of  $CO_2$  pure component gas and  $CO_2/N_2$  mixed gas on M-MOF-74 series adsorbent by the grand canonical Monte Carlo method. Among the  $CO_2$ adsorption performances of MOF-74 materials with metal centers of Mg, Co, Ni, and Zn, Mg-MOF-74 had the highest  $CO_2$  adsorption capacity, adsorption selection coefficient and adsorption heat. When mixed gas was adsorbed, the law of  $CO_2$  adsorption was consistent with that of pure  $CO_2$  adsorption. The size law of adsorption heat on MOF-74 was similar to that of adsorption amount. Our findings demonstrated that the interaction between the metal-organic framework material and  $CO_2$  is greater than that between the material and  $N_2$ . The interaction between the gas and the MOF-74 series adsorbent was the main factor affecting the adsorption amount, which reveals the strong influence of metal central atoms on the amount of gas adsorption. Our findings provide new ideas for the design of efficient adsorbent materials.

#### 1. Introduction

In the face of the global increase in atmospheric  $CO_2$  levels, various materials have been proposed for  $CO_2$  adsorption, while most of these are targeted at major  $CO_2$  emission sites with high  $CO_2$  concentrations such as chemical plants, iron works, thermal power plants, etc. (Zhen et al., 2012; Meconi and Zangi, 2020). However, with the development of the global economy, the number of cars is increasing day by day and they account for 9.2% of total  $CO_2$  emissions (Sun et al., 2022). The research and development of materials that absorb low-concentration  $CO_2$  from automobile exhausts to control carbon dioxide emissions is of great significance for carbon neutralization and global warming (Hua and Dong, 2022).

Compared with activated carbon, zeolite and other solid adsorbents, metal-organic frameworks have higher adsorption selectivity (Pham et al., 2016; Singh et al., 2020). The technology of carbon capture and storage is widely used to greatly expand the selection range of adsorbents. Among the variety of material structures, those from the M-MOF-74 series can effectively adsorb CO<sub>2</sub> due to their open metal sites, which has been proved for CO<sub>2</sub> capture (Millward and Yaghi, 2005; Kuppler et al., 2009; Liu et al., 2012). Caskey (Caskey et al., 2008) found that a huge amount of CO<sub>2</sub> was adsorbed by Mg-MOF-74 whose adsorption capacity could reach 8.6 mmol/g for CO2 under conditions of 298 K and 1 bar, and their open metal sites significantly affected CO<sub>2</sub> adsorption capacity and selectivity. Yazaydın and Bae (Yazaydın et al., 2009; Bae and Long, 2013) screened 14 kinds of MOFs for lowpressure CO<sub>2</sub> adsorption and separation, and found that MOFs with open metal sites could adsorb a large amount of CO<sub>2</sub> under low pressure, much higher than other types of MOFs. A large number of studies have demonstrated that MOFs exhibit improved CO<sub>2</sub> adsorption performance due to their open metal sites, thus are widely utilized in CO2 adsorption and separation.

Herein, molecular dynamics simulation was used to estab-

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Fig. 1. Schematic diagram of the Mg-MOF-74 model: (a) Framework model and (b) atom distribution.

**Table 1.** Charge of each atom in the M-MOF-74 model<br/>(Yazaydın et al., 2009).

No	Charge (e)			
110.	Mg-MOF-74	Zn-MOF-74	Co-MOF-74	Ni-MOF-74
1	1.458	1.206	1.139	1.100
2	-0.714	-0.670	-0.684	-0.677
3	-0.909	-0.659	-0.645	-0.623
4	-0.784	-0.702	-0.731	-0.679
5	0.800	0.767	0.832	0.789
6	-0.260	-0.292	-0.292	-0.239
7	0.492	0.325	0.315	0.358
8	-0.280	-0.147	-0.110	-0.201
9	0.197	0.172	0.176	0.172

lish a model for evaluating the adsorption and separation performances of M-MOF-74 materials for  $CO_2$  and  $N_2$ . Based on this model, the effects of the open metal sites of M-MOF-74 materials on their  $CO_2$  performance indicators, such as adsorption selectivity, adsorption capacity, and adsorption heat, were examined.

#### 2. Methodology

#### 2.1 Model

The crystal structure of Mg-MOF-74 was determined according to the Cambridge Crystallographic Data Centre. M-MOF-74 materials (M = Mg, Zn, Co, Ni) can be obtained by appropriately adding, deleting and modifying some atoms (Dietzel et al., 2005). Fig. 1 demonstrates the framework model and atom distribution of Mg-MOF-74 with the following lattice parameters: a = b = 2.611 nm, c = 0.672 nm,  $\alpha = \beta = 90^{\circ}$ ,  $\gamma = 120^{\circ}$ .

Table 1 illustrates the charge distribution of each atom in the M-MOF-74 model shown in Fig.2(b), and Table 2 presents the Lennard Jones (L-J) parameters for the atoms in M-MOF-74. The interaction energy of each atom E in the system is derived from the Coulomb and L-J potential equation:

Table 2. L-J potential parameters of atoms in M-MOF-74(Mayo et al., 1990; Rappe et al., 1992).

Atomic type	σ (Å)	ε/kB (K)
С	3.898	47.856
Н	3.195	7.649
0	3.405	48.158
Zn	4.054	27.677
Mg	3.021	55.857
Co	2.872	7.045
Ni	2.834	7.548

**Table 3.**  $CO_2$  and  $N_2$  model parameters (Potoff and<br/>Siepmann, 2001; Yu et al., 2015).

Parameters	CO <sub>2</sub>		N <sub>2</sub>	
Charge (e)	С	0.7	Ν	0
charge (c)	0	-0.35	-	-
Bond distances (Å)	C=O	1.175	$N{\equiv}N$	1.105
Bond angle	O=C=O	179.983°	$N{\equiv}N$	180°

$$E_{ij} = 4\varepsilon_{ij} \left[ \left( \frac{\sigma_{ij}}{\gamma_{ij}} \right)^{12} - \left( \frac{\sigma_{ij}}{\gamma_{ij}} \right)^6 \right] + \frac{q_i q_j}{4\pi\varepsilon_0 \gamma_{ij}}$$
(1)

where  $\gamma_{ij}$  denotes the distance between particles;  $\sigma_{ij}$  means the depth of potential well;  $\varepsilon_{ij}$  represents the depth of potential energy; q is the charge of atoms;  $\varepsilon_0$  is the vacuum dielectric constant that is equal to  $8.8542 \times 10^{-12} \text{ C}^2/(\text{N} \times \text{m}^2)$ . Based on the Lorentz-Berthelot (L-B) mixing rules, the cross-terms were employed for calculating the L-J potential function.

Fig. 2 presents the schematic diagram of the  $CO_2$  and  $N_2$  models, and the model parameters are shown in Table 3.

#### 2.2 Computational methods

The GCMC simulation was implemented based on Materials Studio (Akkermans et al., 2013), and the Universal For-



Fig. 2. Schematic diagram of the  $CO_2$  and  $N_2$  models: (a)  $CO_2$  and (b)  $N_2$ .



**Fig. 3.** Comparison of simulated and experimental XRD patterns of M-MOF-74.

ce Field was employed in the GCMC simulation (Yang et al., 2018). The skeleton material was regarded as a rigid structure in the simulation, and van der Waals interaction force was calculated using the atom-based method and described by using L-J potential function. Periodic boundary conditions were adopted, and the cut-off radius was 12.8 Å. The Ewald addition method was implemented for calculating the electrostatic interactions. The interaction of different particles was calculated by L-B mixing rules. The modeling was carried out in a total of  $3 \times 10^6$  steps. Herein, the first  $1.5 \times 10^6$  steps were employed for systematic equilibrium, and the last  $1.5 \times 10^6$  steps were adopted for the calculation of adsorption data.

#### 2.3 Model and verification

Fig. 3 compares the simulated X-Ray Diffraction (XRD) pattern of M-MOF-74 and the experimental XRD pattern of Ni-MOF-74 (Chen et al., 2015). For the XRD pattern  $(2\theta = 5-50^{\circ})$ , the experimental XRD pattern shows good agreement with the simulated XRD pattern. The optimized Mg-MOF-74 cell constants are a = b = 2.61102 nm, and c = 0.67192 nm. The simulated cell volume V = 3.9669 nm<sup>3</sup> (a = b = 2.602 nm, c = 0.672 nm, V = 3.941 nm<sup>3</sup>) is within 1% error compared with the data (Caskey et al., 2008). Table 4 shows the specific surface area of the M-MOF-74 material model, which is slightly larger than that obtained in the experiment (Choi et al., 2017), because the model is ideal and there may

Table 4. M-MOF-74 specific surface area.

Model	Simulation (m <sup>2</sup> /g)	Experiment (m <sup>2</sup> /g) *
Mg-MOF-74	1,851.04	1,525
Zn-MOF-74	1,422.38	1,134
Co-MOF-74	1,466.55	1,356
Ni-MOF-74	1,451.33	1,239

\* from Choi et al. (2017).



Fig. 4. CO<sub>2</sub> adsorption isotherm curves of M-MOF-74.

be impurities in the synthesized MOFs. Thus, it is inferred that the model established in this paper has high reliability and can be simulated in the next step.

#### 3. Results and discussion

## **3.1** Adsorption performance of M-MOF-74 for pure CO<sub>2</sub>

With reference to the effect of different metal central atoms on the amount of  $CO_2$  adsorption, the  $CO_2$  capacity adsorbed by M-MOF-74 was calculated under the conditions of 298 K and 0-1,200 kPa. This work presents the adsorption capacity, adsorption site and adsorption heat of the system as the performance indicators.

Fig. 4 illustrates the adsorption isotherm curves of four metal-organic framework materials. The adsorption isotherms



Fig. 5. Diagram of adsorption points.

of the 4 MOFs have the same trend, which belong to the type I isotherm. At the initial stage, the amount of CO<sub>2</sub> adsorption rises rapidly in the lower pressure range due to the presence of metal adsorption sites, where CO<sub>2</sub> can be preferentially adsorbed. However, with the pressure increasing, the rising curve of  $CO_2$  adsorption capacity tends to be flat. Due to the increase in adsorption capacity, the preferential adsorption sites in MOF-74 materials are gradually filled, and the framework is gradually occupied by CO2 gas. Thus, the interaction between the gas and the framework is weakened. Among the four materials, Mg-MOF-74 has the largest specific surface area and pore volume. At the initial stage of adsorption, the gas molecules can obtain a larger contact area and storage space (Bergmann et al., 2015); therefore, the CO<sub>2</sub> adsorption capacity with regard to the four framework materials is in the descending order of Mg-MOF-74 > Co-MOF-74  $\approx$  Ni-MOF-74 > Zn-MOF-74.

In order to further understand the adsorption position of  $CO_2$  molecules in the metal-organic frameworks, the adsorption locations of the Mg-MOF-74 were illustrated in Fig. 5, where the red dots represent the adsorption points of  $CO_2$ . According to the diagram of adsorption points, it is concluded that  $CO_2$  molecules are first adsorbed near these bare metal sites, and there are a few scattered adsorption sites at the center of the framework pore. This indicates that, for M-MOF-74, the adsorption of  $CO_2$  by the framework materials is mainly determined by the interaction of different metal centers for  $CO_2$  molecules.

Adsorption heat represents the thermal effect in the adsorption process of adsorbate, which is caused by the reduction in the molecular motion speed of gas molecules, the reduction in kinetic energy and the release of heat in the adsorption process. Adsorption heat is an important index to measure the strength of adsorption capacity of the adsorbent, and its value reflects the strength of interaction between adsorbent material and gas. The CO<sub>2</sub> adsorption heat with regard to M-MOF-74 is illustrated in Fig. 6, where Mg-MOF-74 has the largest heat from CO<sub>2</sub> adsorption and the order of CO<sub>2</sub> adsorption heat basically corresponds to the order of adsorption capacity. Mg-MOF-74 has the strongest interaction with CO<sub>2</sub>, while Zn-MOF-74 has the weakest.

## **3.2** Adsorption performance of M-MOF-74 for CO<sub>2</sub>/N<sub>2</sub>

Fig. 7 shows the  $CO_2/N_2$  (15/85 v/v%) adsorption of M-MOF-74, where the ratio of  $CO_2$  to  $N_2$  is 15:85 (Yang et al.,



Fig. 6. The adsorption heat of CO<sub>2</sub> for M-MOF-74.

2012; Yang et al., 2018). The addition of N<sub>2</sub> molecules can reduce the amount of CO<sub>2</sub> adsorption, and the CO<sub>2</sub> adsorption capacity of the four skeleton materials is in the descending order of Mg-MOF-74 > Co-MOF-74  $\approx$  Ni-MOF-74 > Zn-MOF-74, as shown in Fig. 7(a). The adsorption capacity for N<sub>2</sub> is smaller than that for CO<sub>2</sub> because the unsaturated metal site in the adsorbate has a strong adsorption ability for gas molecules with a large quadrupole distance. When comparing the quadrupole moments of CO<sub>2</sub> and N<sub>2</sub>, that of CO<sub>2</sub> is larger than N<sub>2</sub>. Hence, the interaction of the material with N<sub>2</sub> is small, and the N<sub>2</sub> adsorption capacity of 4 skeleton materials is in the descending order of Mg-MOF-74  $\approx$  Zn-MOF-74 > Co-MOF-74  $\approx$  Ni-MOF-74, as demonstrated in Fig. 7(b).

To further analyze the difference in the CO<sub>2</sub> adsorption capacity of M-MOF-74 (M = Mg, Zn, Co, Ni) under twocomponent CO<sub>2</sub>/N<sub>2</sub> gas, the adsorption locations of the Mg-MOF-74 were shown in Fig. 8. Here, Fig. 8(a) demonstrates the adsorption locations of  $CO_2$  on Mg-MOF-74, and Fig. 8(b) illustrates the adsorption locations of CO2 and N2 molecules on Mg-MOF-74, where the red dots represent the adsorption points of CO<sub>2</sub> and the green dots stand for the adsorption points of N<sub>2</sub>. Based on the distribution of adsorption sites, it is inferred that when N<sub>2</sub> molecules are added, they can replace some preferential CO<sub>2</sub> adsorption sites, and some open sites are switched to adsorb N<sub>2</sub> instead of CO<sub>2</sub>. Hence, CO<sub>2</sub> is partly dispersed in the skeleton. Due to the presence of N<sub>2</sub> molecules, the CO<sub>2</sub> adsorption capacity of Mg-MOF-74 is reduced as some of the adsorption sites can no longer adsorb this molecule.

The selective adsorption coefficient is used to calculate the influence of the components with different partial pressures on the adsorption capacity of the mixed system, which is an important parameter used for evaluating the separation performance of the mixed gas.

The adsorption selectivity coefficient *S* is calculated as follows:

$$S_{1/2} = \frac{x_1/x_2}{y_1/y_2} \tag{2}$$

where subscript 1 and 2 denote CO<sub>2</sub> and N<sub>2</sub>, respectively;  $x_1$  and  $x_2$  represent the molar components of two components in the adsorption phase, respectively;  $y_1$  and  $y_2$  stand for the mo-



Fig. 7.  $CO_2$  and  $N_2$  adsorption of M-MOF-74: (a)  $CO_2$  and (b)  $N_2$ .



Fig. 8. Diagram of adsorption points: (a)  $CO_2$  and (b)  $CO_2/N_2$ .



Fig. 9. Selective adsorption coefficient of M-MOF-74.

lar components of two components in the gas phase, respectively.

The adsorption selectivity coefficients of the four adsorbent materials for the mixed gas are further calculated, as shown in Fig. 9. The selectivity coefficients of all materials are greater than 1, indicating that M-MOF-74 has a selective adsorption effect for  $CO_2$  in the mixed gas and the interaction between

CO<sub>2</sub> gas and materials is strong; therefore, CO<sub>2</sub> will be preferentially adsorbed. Among the four materials, Mg-MOF-74 has the highest CO<sub>2</sub> selective adsorption coefficient, while Zn-MOF-74 has the lowest. Under the condition of 100 kPa and 298 K, the CO<sub>2</sub> selective adsorption coefficient of the four skeleton materials is in the descending order of Mg-MOF-74 > Ni-MOF-74 > Co-MOF-74 > Zn-MOF-74.

#### 4. Conclusions

In the present work, a molecular dynamics simulation method was developed to establish a M-MOF-74 model, which was used to investigate the  $CO_2$  adsorption performances of MOF-74 materials with metal centers of Mg, Co, Ni and Zn and their selectivity for  $CO_2/N_2$ . Among the four materials, Mg-MOF-74 had the highest  $CO_2$  adsorption capacity, adsorption selection coefficient and adsorption heat. In comparison with the adsorption capacity of pure  $CO_2$  and the selectivity of mixed gas in M-MOF-74 series materials, Mg-MOF-74 had the best adsorption and separation performance. It was also highlighted that the gas is mainly adsorbed near the metal central atom of M-MOF-74, the amount of adsorption is affected by the interaction between the metal central atom and the gas, and the interaction between them could be expressed by the heat of adsorption. This study revealed the influence of metal central atoms on the amount of gas adsorption, thereby providing some ideas for the design of efficient adsorbent materials.

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#### **Conflict of interest**

The authors declare no competing interest.

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