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Generation and delivery of free hydroxyl radicals using a remote plasma

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Abstract

We demonstrate a new gas-based OH[•] generation source using a low power radio frequency driven atmospheric pressure plasma configured to deliver the radical flux into the far effluent region, well away from interference from other plasma factors such as electric fields, currents, and ultraviolet radiation. Using He–H₂O gas chemistry isolated from the laboratory air, the plasma generated flux contains OH[•] and other radicals including, O and HO₂ as well as H₂O₂ which, along with, was found to vary with H₂O vapour content and absorbed power density. Peak flux values were 2.3 nmol s⁻¹ and 0.23 nmol s⁻¹ for H₂O₂ and OH[•] respectively at a distance of 50 mm from the plasma, with 790 ppmv H₂O and a power density of ~10⁸ W m⁻³. The maximum OH[•] flux density was 4.5 × 10¹⁹ m⁻² s⁻¹ falling to 1.7 × 10¹⁹ m⁻² s⁻¹ at 110 mm, equivalent to generation rates of 74 μM s⁻¹ and 28 μM s⁻¹. Despite high OH[•] recombination rates at the plasma exit, the escaping flux is still significant, indicating a viable delivery capability to downstream targets. Its performance with regard to OH[•] generation rates compares well with traditional OH[•] generation techniques such as radiolysis, advanced oxidation processes and enhanced Fenton-chemistry approaches where OH[•] production rates are sub-μM s⁻¹. Delivering precisely quantifiable OH[•] fluxes provides new opportunities for scientific studies and technological opportunities in cell biology, atmospheric chemistry, protein unfolding and systematic dose studies for plasma-based and other OH[•] related potential medical treatments.

Supplementary material for this article is available [online](#)

Keywords: atmospheric pressure plasma, hydroxyl, OH radical, plasma effluent, reactive oxygen species, global model

(Some figures may appear in colour only in the online journal)

1. Introduction

The hydroxyl radical, OH[•], plays an important role in numerous areas including atmospheric chemistry [1], water treatment and pollution remediation [2], antibiotics and

disinfection [3], tumour therapy [4, 5] and protein studies [6], among others. Fenton chemistry has found wide application as a hydroxyl source, however other areas require alternative approaches to avoid unwanted byproducts, to operate outside low pH environments or achieve much faster reaction times [7]. For example, with protein footprinting, direct OH[•] generation via synchrotron radiolysis of H₂O [8, 9] or excimer laser photolysis of H₂O₂, Chen *et al* have demonstrated ultra-fast and irreversible labelling of proteins capable of following their folding/unfolding dynamics [10]. Other, more accessible, direct techniques including electrospray and plasma generated



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OH^\bullet are currently being explored [11]. OH^\bullet is considered the most reactive and toxic radical in biology and selective OH^\bullet generation approaches have been proposed for cancer therapy. Gamma radiolysis is known to produce a high concentration of OH^\bullet radicals with strong evidence that these play an important, even dominant role, in DNA destruction and tumour cell death. In enhanced chemodynamic therapy, photodynamic, photothermal, sonodynamic and radiation therapies are used to enhance Fenton-like reactions from nanomedicines in the acidic tumour microenvironment [4, 12, 13].

Atmospheric pressure plasmas have attracted considerable attention in the past decade as radical sources for application as possible medical treatments for wound healing and cancer [14]. These plasma devices are efficient generators of reactive oxygen and nitrogen species, producing a rich cocktail of species in the gas phase at high concentrations which can be delivered directly to tissue [15, 16]. Plasmas can also produce high UV photon fluxes, injected currents and electric fields and have been shown to induce significant biological effects [17]. Considerable effort has gone into characterising the complex plasma physical and chemical properties on the one hand and attempting to correlate plasma species fluxes with biological outcomes on the other. There are many cold plasma sources designs, and these can generally be classified as either plasma jet (APPJ) or dielectric-barrier discharge (DBD) and can further categorised as either direct-contact or indirect-contact. In the former, the treatment target, including liquid, forms part of the plasma electrical circuit while in the latter, the circuit is isolated, but the plasma is sufficiently close to allow species interaction. Commercially available devices such as the kINPen [14, 18] and PlasmaDerm [19] are examples of direct and indirect sources respectively. Irrespective of the electrical circuit, it can be argued that all such plasmas are effectively coupled to the treatment substrate since the plasma-substrate gap is either very small or electric-field propagation via ionisation waves recreates the plasma downstream [20, 21]. This has the advantage of delivering the high radical fluxes required but brings with it certain technological and scientific disadvantages. The associated electric fields, currents and UV radiation along with potentially high temperature gradients, flow induced turbulence and impurity re-entry into the plasma creates significant challenges for real-time monitoring and responsive control in a clinical environment. From a scientific perspective, the interplay of these multiple synergistic factors represents a major obstacle to systematic plasma-liquid characterisation and simulation, while the inclusion of biological interactions adds an additional layer of complexity that delays our fundamental understanding and predictive capabilities. In this work we aim to investigate a truly non-coupled remote plasma operating at a sufficient stand-off distance from a liquid substrate. By isolating the plasma itself from the ambient environment, and thus excluding air ingress, we have much greater control of the gas chemistry. Using the plasma interaction of helium and water vapour only, we can generate various HO_x (x : 0–2) and O species as the primary radicals, along with H_2O_2 . Other species (e.g. $\text{O}_2(\text{a}^1 \Delta)$, O_3) may be present but at much lower concentrations [22]. While OH^\bullet flux levels may not match

those of direct contact plasmas [23], the relative purity of the radical source and the absence of electric fields and currents may prove to be a major advantage for applications such as tumour therapy or protein footprinting. Also, such as source provides a new tool for investigating individual factors relevant to plasma-biological interactions, allowing thereafter incremental increases in the complexity of plasma chemistry and determination of synergistic or multivariate effects.

Changing the water vapour content of the feed gas has been found to be an effective way to control the OH^\bullet radical concentration within the plasma region and therefore in the APPJ effluent itself [22, 24–27]. Noble gas plasma interaction with trace water vapour gives rise to many species and reactions due to multiple pathways including electron impact ionisation, excitation, and dissociative attachment as well as ion-molecule reactions. The use of an radio frequency (RF) excited plasma ensures the plasma region is restricted to a short distance (\sim mm) from its electrodes [28]. In air, the effective rate coefficient for OH^\bullet recombination is $1.6 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$ with trace (\sim 10 pM) components, e.g. CO, present [29, 30]. In the plasma effluent, however, the OH^\bullet is isolated from ambient air for most of the flight time, and its lifetime is determined primarily by two-body ($\text{OH}^\bullet + \text{OH}^\bullet \rightarrow \text{H}_2\text{O} + \text{O}$), ($\text{OH}^\bullet + \text{HO}_2 \rightarrow \text{O}_2 + \text{H}_2\text{O}$), ($\text{OH}^\bullet + \text{O} \rightarrow \text{O}_2 + \text{H}$) or three-body ($\text{H} + \text{OH}^\bullet + \text{H}_2\text{O} \rightarrow 2\text{H}_2\text{O}$) recombination reactions [22]. Attri *et al* report OH^\bullet lifetimes in the gas phase above a liquid surface of \sim 4 ms for high OH^\bullet concentration levels around 10^{22} m^{-3} and by inference \sim 1 ms for typically reported plasma OH^\bullet concentrations [31]. This is a directly-coupled plasma source and hence high densities of H^\bullet radicals may be expected at the liquid surface which could contribute significantly to OH^\bullet recombination at the gas-liquid interface [32]. However, with remote plasmas, knowledge of OH^\bullet lifetimes and uptake by liquid are not known.

Measurement of neutral and ionic species have been performed in the plasma and afterglow regions via laser-induced fluorescence (LIF) [33, 34], ultraviolet (UV) and vacuum ultraviolet (VUV) absorption [35, 36], two-photon LIF (TALIF) [26, 37, 38], and mass spectrometry [26, 39–43] among others. Willems *et al* and Benedikt *et al* measured the OH^\bullet and O species densities in the field-free effluent of a He- H_2O RF (13 MHz) plasma jet, up to 25 mm from the RF plasma source [26, 43]. Near the plasma, they observed an increase in OH^\bullet density \sim 10^{20} m^{-3} as the H_2O content increased, saturating at \sim 5000 ppmv. Similar results have been obtained by Bruggeman *et al* in the plasma region [44]. At 20 mm from the plasma, the OH^\bullet density had decreased by over an order of magnitude, for a gas flow of 1.4 SLM and $[\text{H}_2\text{O}] > 7000$ ppmv [26] while under similar conditions, H_2O_2 concentrations remain relatively constant and HO_2 is no longer present. Verreycken *et al*, with an Ar- H_2O jet into air, observed the reduction in OH^\bullet density by a factor of 10 within 8 mm from the plasma at high H_2O content [33]. Reuter *et al*, using TALIF, determined atomic oxygen density up to 100 mm from the RF He plasma nozzle [45]. However, in this case VUV emission from oxygen lines was sufficient to maintain the oxygen density by photo-dissociation, over long distances. Outside the plasma region, dissociative

recombination of H_2O^+ can be a dominant pathway for OH^\bullet formation, where H_2O^+ is often formed by penning ionisation with He metastables [32]. In the absence of additional oxygen, loss mechanisms along the jet axis may involve OH^\bullet recombination with H^\bullet radicals to form H_2O and three-body recombination to form H_2O_2 [32]. The $\text{H}_2\text{O} + \text{OH}^\bullet \rightarrow \text{H}_2\text{O} + \text{OH}^\bullet$ reaction is symmetric and therefore not of significance [46].

For most chemistries, it is difficult to measure gas phase species directly beyond the afterglow/near effluent regions; downstream liquid chemical analysis or simulation therefore have been used to infer upstream plasma chemistry [47–49]. With both directly coupled kHz jets [47, 49], and remote RF jets [48], there is strong evidence that species (H_2O_2 , OH^\bullet) measured in liquid are created in the plasma gas phase. While liquid chemical probing offers the possibility of determining gas species density profiles upstream, such measurements have not been reported, although Kawasaki *et al* obtained relative measurements of ROS variation with distance up to 30 mm, for a directly coupled jet, and Plimpton *et al* bubbled plasma (O_3^-) effluent through H_2O_2 to generate OH^\bullet in liquid far downstream [50, 51]. Overall, where measurements have tracked changes with distance, such distances are generally <10–20 mm and species densities are observed to drop by a factor of 10. Experimental determination however, of OH^\bullet fluxes and their decay over extended distances from the plasma, has not been carried out.

In this work we present an RF APP operating in helium with a controlled admixture of water vapour for remote radical delivery. We investigate the plasma's ability to deliver reactive molecules to a sample solution up to 110 mm downstream of the plasma by quantifying the flux of H_2O_2 and OH^\bullet at the gas/liquid interface. At this distance the sample is far enough removed from the plasma region that any species measured are the result of transport alone and not from plasma interaction with the liquid itself. The effect of feed gas humidity on both the power absorbed by the plasma and OH^\bullet production is reported, and an optimum humidity for maximum OH^\bullet delivery discussed. Specie fluxes were used as inputs to a zero-dimensional (0D) kinetics model, modified to simulate the progression of species densities generated in the plasma region into the far effluent. Trends in measured fluxes with changing plasma conditions were compared against the model's output to test the model's validity at predicting long range delivery of OH^\bullet and H_2O_2 . The performance of the remote plasma source with regard to OH^\bullet production rates is compared with other OH^\bullet generating sources such as radiolysis, advanced oxidation processes (AOPs) and enhanced Fenton chemistry approaches as well as with direct contact and directly coupled plasma devices.

2. Methods

The RF APP used in this study (figure 1) consists of a 2 mm inner diameter quartz capillary surrounded coaxially by two 1 mm diameter copper ring electrodes, separated by 2 mm. A 13.56 MHz wave was generated by a Cesar RF power generator and coupled to the electrodes with the aid of an MFJ

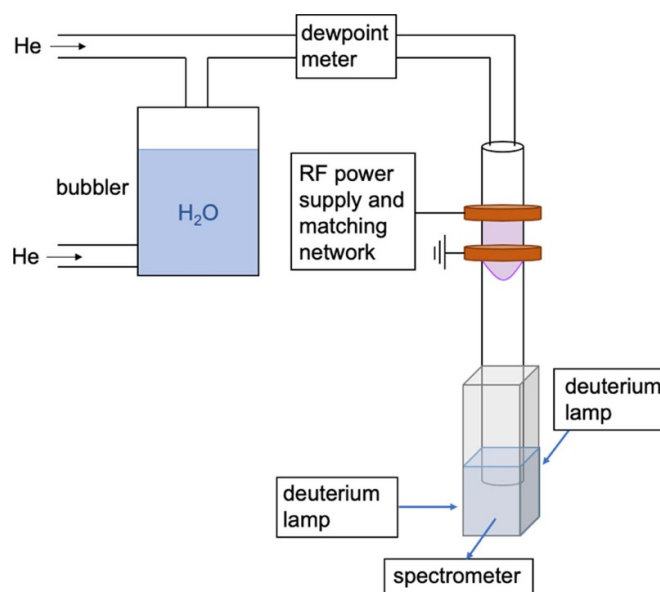


Figure 1. Schematic overview of the experimental setup, showing the APPJ and bubbler system for the admixing of water to the helium feed gas.

antennae tuner. A more detailed description and operation of this RF APP device can be found in [52].

Helium was fed through the quartz capillary at a mass flow rate of 1.0 SLM and the power absorbed by the plasma device monitored using an inline RF VI probe (Impedans Octiv Suite). The plasma was operated up to a maximum absorbed power of 1.9 W and assuming a cylindrical geometry, the volume was estimated from the length of the luminous region, from which the power density was estimated as $\sim 75 \text{ MW m}^{-3}$. The visible bulk of the plasma was confined to the interelectrode region with the visible plasma plume extending a maximum of 3 mm beyond the electrodes. To guarantee remote operation, a plasma–liquid distance of >10 mm provides a sufficient safety margin and at an average gas velocity of $>10 \text{ m s}^{-1}$, radical transport times are in the millisecond range. The water content of the plasma feed gas was controlled by mixing two flows; a dry helium flow (CP grade) controlled by one mass flow controller (MFC), and a humidified helium flow controlled by another MFC. The humidified helium was produced by passing dry helium through a water bubbler. Water content could then be regulated by varying the ratio of the dry to humidified helium flows while keeping the total flow at 1.0 SLM. Saturation of the humidified flow was not necessary as the water content was measured using a dew point meter (Xentaur LPDT) with an accuracy of $\pm 3^\circ \text{C}$, placed between the mixing point of the two flows and the entrance to the plasma.

H_2O_2 concentration was calculated from UV absorbance spectroscopy measurements of titanium (IV) oxysulphate (TiS) solution (Sigma Alrich 495 379). A deuterium lamp (Ocean Optics DH-2000-BAL) was used in combination with an Ocean Optics spectrometer (QE65 Pro). TiS was added to the sample cuvette at a concentration of 100 mM, which reacts with H_2O_2 to produce pertitanic acid with a characteristic

absorbance at 407 nm. Absolute calibration was performed using the absorbance of several samples containing known H_2O_2 concentrations. OH^\bullet concentration was calculated from fluorescence emission spectroscopy measurements. Sample excitation and emission was measured using the same light source and spectrometer. Terephthalic acid (TA) (Sigma Aldrich 185361), was used at a concentration of 2 mM in 5 mM sodium hydroxide solution. TA reacts with OH^\bullet to form 2-hydroxyterephthalic acid (HTA) which emits at 425 nm when excited with UV at 310 nm. While the rate constant for the addition of OH^\bullet to TA is around $4.0 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$ [53], in O_2 containing solutions subsequent reactions produce HTA with a 35% yield [54, 55]. OH^\bullet flux was therefore calculated by dividing the rate of HTA formation by 35% and the effective area of OH^\bullet delivery to the sample, equal to the cross-sectional area of the capillary. Sample HTA concentration was calculated from calibration data obtained by plotting 2-hydroxyterephthalic (Sigma Aldrich, 752525) concentration against emission intensity. The TA reaction requires O_2 which over time will be expelled from the liquid by the He gas flow. We observed a fall in O_2 concentration in 5 ml liquid, subjected to 1 slm He flow, from 7 ppmv initially to 0.1 ppmv after 2 min. However, the plasma acts as a source of O_2 and from the model we observe at 50 mm (figure 6(b)), our closest measurement distance, that the O_2 flux is greater than that of OH^\bullet . Since the reaction is catalytic, i.e. O_2 is not consumed, sufficient replenishment is obtained from the plasma.

Liquid samples were contained in a quartz micro cuvette, held in place with an Ocean Optics CUV cuvette holder. This setup enabled *in situ* spectroscopy measurements to be taken during plasma treatment. The quartz capillary could be extended distances of 50–110 mm from the lower plasma electrode, and the micro cuvette located at a distance that positioned the exit of the quartz capillary 5 mm beneath the liquid sample surface. Sample volumes were restricted to 0.5 ml; larger volumes resulted in sample ejection from the cuvette during treatment, while smaller volumes failed to provide a bubble free region at the bottom of cuvette for consistent spectroscopy measurements. Because the outlet of the APPJ was positioned beneath the liquid surface with a continuous flow of helium escaping the cuvette, it is reasonable to assume that the plasma system does not contain any significant atmospheric contaminants. In previous surface treatment experiments, a combination of high OH^\bullet concentrations generated near the plasma–liquid interface and limited diffusion, meant absolute calculations of the amount of OH^\bullet transferred from the plasma to the liquid were not possible [56]. Bubbling with the plasma effluent produces a homogeneous distribution of OH^\bullet and HTA throughout the sample, enabling more accurate OH^\bullet density calculations. Control measurements consisted of the sample being treated with helium only.

ZDPlasKin [57], a 0D chemical reaction kinetics solver, was used to model the plasma region and downstream species densities. The model used herein accounted for 58 species and 739 reactions that revolved around the He, H and O products produced in a typical He/ H_2O plasma. The relevant reactions were taken from a previous study by Aghaei and Bogaerts [58], however no N containing reactions were included since

high purity He (99.999%) was used throughout, and the capillary outlet is submerged and isolated from air. Rate equations, if not constant, are calculated using electron/gas temperature dependent reaction rates from literature and are integrated in time using the built-in solver. Electron transport coefficients and the rate of electron impact reactions are calculated via Bolsig+, automatically called by ZDPlasKin. See Table 1 in supplementary data for the complete list of species and reactions used. Plasma geometry, gas pressure and gas temperature are taken from the experiment and provided as starting conditions. The species concentrations with distance downstream from the plasma i.e. the cathode electrode, is determined from the temporal evolution of the plasma chemistry, once the plasma (ions and electrons) is switched off. Using a constant gas velocity in the capillary, of 5.3 ms^{-1} , we convert to a distance response. We define the time period from 0 to $5 \times 10^{-4} \text{ s}$ as the interelectrode plasma region (0–3 mm) and 5×10^{-4} – $2 \times 10^{-2} \text{ s}$ as the downstream region of the ground electrode to the sample interface (3–110 mm). Two input parameters were changed in the model at $5 \times 10^{-4} \text{ s}$. The plasma gas temperature, initially set at 320 K [59], was reduced to the ambient value of 295 K. The OH density at 50 mm is insensitive (<5% variation) to the downstream temperature between 295 K and 320 K. The plasma voltage was applied up to $5 \times 10^{-4} \text{ s}$ and then reduced to zero. The RF voltage magnitude was estimated from *in-situ* impedance measurements and associated circuit model. All reactions are included for both parts of the model, including electron impact ionisation and excitation reactions. The model outputs of particle density were converted to flux by considering gas velocity and capillary cross-sectional area.

3. Results

Plasma treatment was initially performed with a constant water vapour concentration of 600 ppmv with the liquid at a distance 50 mm from the ground electrode ($Z = 50 \text{ mm}$). During helium treatment of the controls, HTA concentration increased by 24%, which coincided with a decrease in volume of ~25%, irrespective of gas composition (helium or plasma effluent). Evaporation of the water solvent alone was therefore identified as the cause, and an evaporation correction factor was therefore applied to all concentration measurements. See supplementary data S1. The maximum treatment time was 10 min, to maintain the liquid surface level above the inserted capillary. At 50 mm from the plasma, H_2O_2 density is shown to increase linearly over 5 min, reaching a maximum density of $3.7 \times 10^{23} \text{ m}^{-3}$ (610 μM) for a plasma power of 1.9 W (figure 2(a)). H_2O_2 flux, calculated from the rate of density increase in the cuvette (figure 2(a)) divided by the capillary cross-section area, also increases with plasma power (figure 2(b)) from the minimum absorbed power at 0.08 W to a maximum flux of $1.95 \times 10^{20} \text{ m}^{-2} \text{ s}^{-1}$ at 1.9 W. At low powers H_2O_2 flux increases linearly but starts to saturate at powers higher than 0.54 W. This flux calculation assumes that all incident H_2O_2 transfers to the liquid due to the high Henry constant [60].

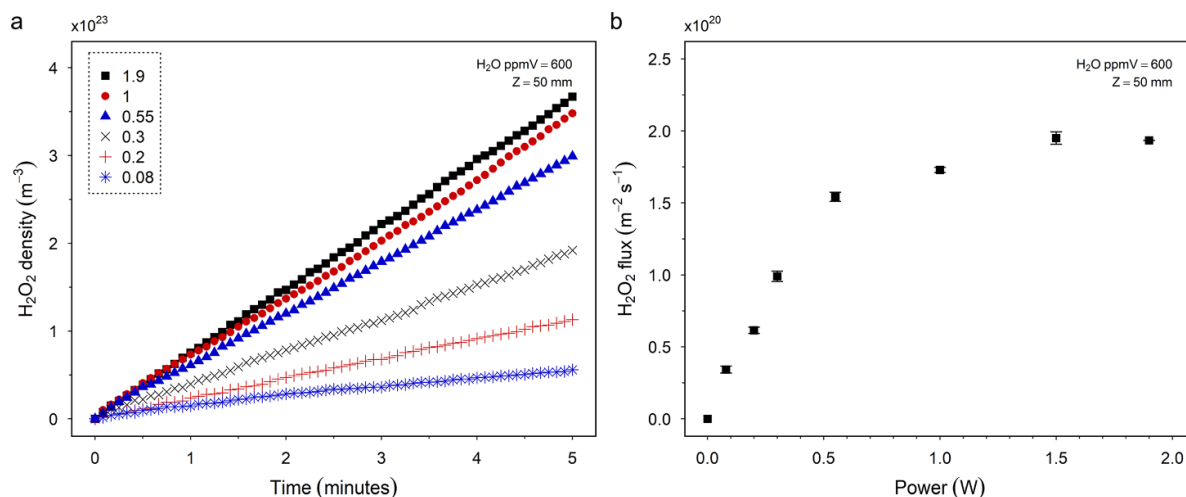


Figure 2. Concentration of H₂O₂ generated in water containing 100 mM titanium oxysulphate. The sample was located 50 mm downstream and treated using a plasma generated with helium containing H₂O at 600 ppmv. H₂O₂ density was calculated *in situ* from the absorbance of pertitanic acid at 407 nm. (a) Density of H₂O₂ produced over time for a range of plasma powers. (b) Average H₂O₂ flux density produced over 5 min of plasma treatment for increasing plasma power.

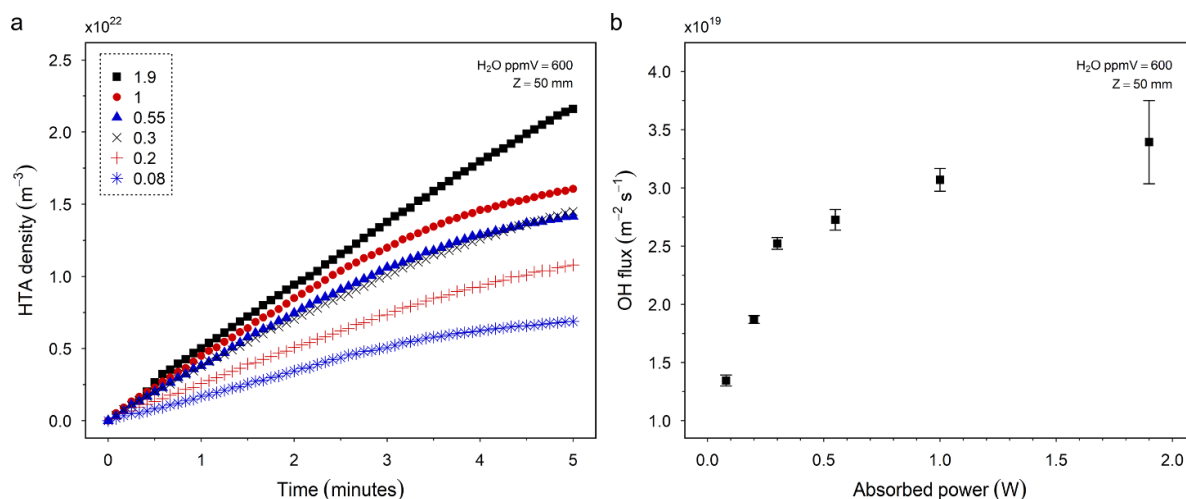


Figure 3. OH[•] density measurements in water containing 2 mM terephthalic acid and 5 mM sodium hydroxide. Sample was located 50 mm downstream and treated using a plasma generated with helium containing H₂O at 600 ppmv. OH[•] density was calculated *in situ* from the fluorescence emission of HTA at 430 nm. (a) Sample OH[•] density over time for various plasma powers. Density increased linearly for the first 3 min, after which the rate decreased. (b) Maximum OH[•] flux delivered at the liquid interface over the first 2 min of plasma treatment for increasing plasma absorbed power.

Using a similar experimental setup as above, the density of HTA produced in a solution of terephthalic acid was measured over 5 min of plasma treatment (figure 3(a)). HTA density increases almost linearly for the first 3 min, after which the rate of HTA increase slows. OH[•] flux was calculated using the maximum rate of HTA formation (see methods), in this case over the first 2 min. The OH[•] flux is shown figure 3(b) to increase linearly at low absorbed power but tend to saturate at powers >0.5 W. A maximum flux of $3.4 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ is produced at an absorbed power of 1.9 W.

Admixing H₂O to the helium feed gas allowed a maximum plasma operating range up to 4500 ppmv H₂O. The minimum achievable concentration was 7 ppmv in the complete system when operating with pure helium, while above 4500 ppmv H₂O, the plasma became unstable and was extinguished.

Keeping the applied power constant, the variation in plasma absorbed power for a given water concentration is shown in figure 4. The maximum absorbed power was 0.77 W at 15 ppmv H₂O and decreases to ~0.12 W by 4400 ppmv, 15% of the maximum.

OH[•] flux measurements were repeated under the same conditions, at a fixed applied power of 70 W and the variation with H₂O concentration is shown in figure 5(a). The initial flux at 7 ppmv of $1.6 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ increases steeply, reaching a maximum flux of $2.4 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ at 790 ppmv H₂O. Above 790 ppmv, the OH[•] flux decreases for increasing water content, and by 4400 ppmv H₂O, reaches a flux similar to that at <10 ppmv. The model humidity was set at 600 ppmv and the excitation voltage increased to a value of 395 V (from 0 to $5 \times 10^{-4} \text{ s}$) to normalise the density of OH[•] calculated

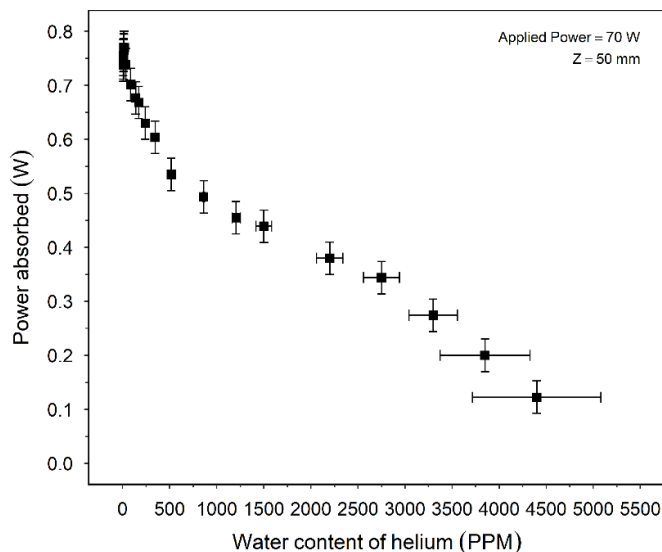


Figure 4. Power absorbed by the plasma for varying water content of the helium feed gas. Water content was controlled by admixing a water saturated helium feed to a pure helium feed and measured using a dew point meter (Xentaur LPDT). Absorbed power was measured across all H₂O concentrations using an Impedans Octiv Suite 2.0 VI probe, while operating at a constant input power. Horizontal and vertical error bars indicate manufacturers specified accuracy of the dew point meter and VI probe respectively.

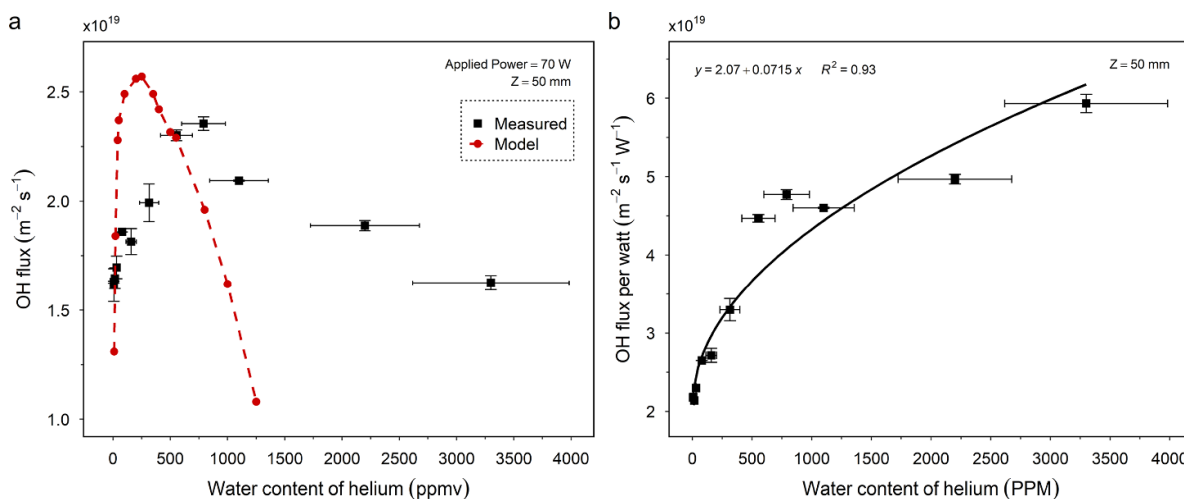


Figure 5. (a) Change in the OH[•] flux delivery for varying helium feed gas H₂O concentration at 70 W applied plasma power. Also shown is the model’s predicted variation in OH[•] flux with changing H₂O content. Both show an ideal water content for maximum OH[•] delivery. (b) OH[•] flux per watt, calculated by normalising the raw OH[•] flux with the absorbed plasma power at each H₂O concentration. The trendline indicates a possible OH[•] flux per watt $\sqrt{[H_2O]}$ relationship.

at 0.001 s (equivalent to 50 mm @ 5.3 m s⁻¹) to that measured experimentally at 50 mm. Voltage was then kept constant while water content varied around 600 ppmv. The resulting model flux is plotted alongside the data in figure 5(a). OH[•] flux was predicted to increase slightly as the water content decreased, resulting in a maximum at ~200 ppmv as opposed to the measured maximum at 790 ppmv. OH[•] flux decreased drastically <50 ppm, similar to the measured flux, however the model predicted a more abrupt decrease in OH[•] at higher ppmv. Simulated flux decreased by an order of magnitude by 1700 ppmv, whereas the plasma was still able to deliver a meaningful OH[•] flux up to at least 3300 ppmv. From the absorbed power characteristic, figure 4, the OH[•] flux per watt

absorbed power is plotted against H₂O, figure 5(b), and shows a sub-linear relationship at high vapour content. The OH[•] flux per watt absorbed appears to follow a near $\sqrt{[H_2O]}$ relationship, with the maximum delivered at the maximum H₂O concentration sustained by the plasma. A possible physical basis for this relationship is discussed later.

Species flux at the liquid interface was measured for increasing distance from the plasma region, while operating at the maximum absorbed power of 1.9 W. Distance of sample from the plasma did not affect the absorbed power. The capillary exit was maintained below the sample surface at all distances to avoid ambient air ingress. Figure 6(a) shows measurements of OH[•] and H₂O₂ flux values at distances of 50,

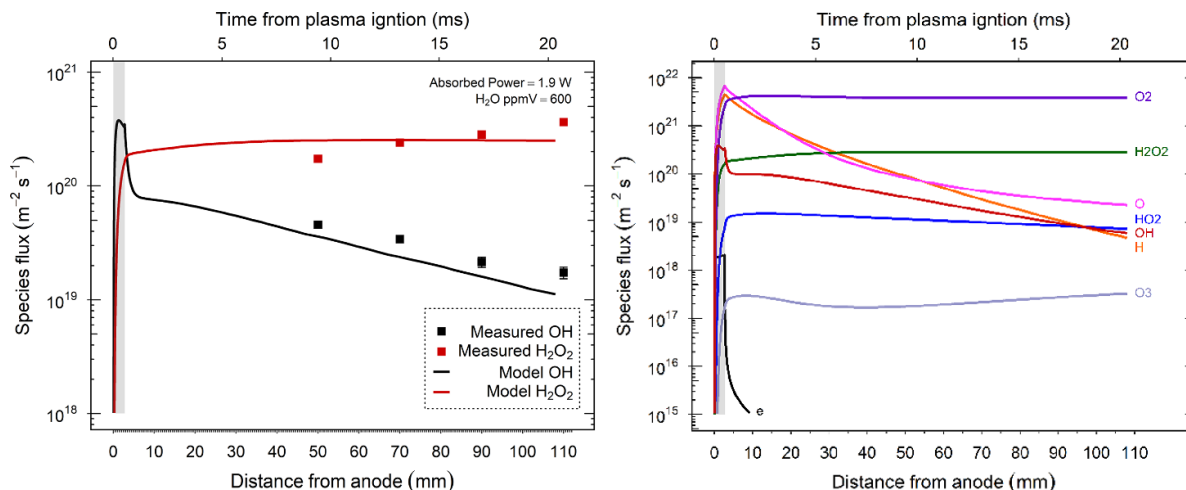


Figure 6. (a) Experimental and model results of OH^\bullet and H_2O_2 densities for increasing distance from the plasma at an initial 600 ppmv H_2O content. Model simulates the flux from the start of the plasma region (0–3 mm, shaded region) up to a distance of 110 mm. Measurements were taken at 50, 70, 90 and 110 mm from the end of the plasma (ground electrode), with absorbed power kept constant at 1.9 W. Measurements were carried out in triplicate. (b) Flux rates of other reactive species present in the effluent under identical input parameters.

70, 90 and 110 mm from the ground electrode. Keeping other parameters constant, the model's plasma region voltage was increased to best fit the fluxes measured at these distances. The model shows a fast decay in OH^\bullet within 2 mm from the plasma edge which is followed by a slower exponential decay over larger distances, similar to that seen experimentally. Modelled H_2O_2 flux is lower than OH^\bullet inside the plasma region, however, immediately increases outside the plasma and continues to rise slowly with distance.

Calibrating the model's flux rates of OH^\bullet and H_2O_2 against experiment enables us to predict the flux rates of other reactive species present in the effluent. Figure 6(b) shows that while the flux rates of H and O are much higher than OH^\bullet and HO_2 at a relatively short distance from the plasma, they also have a faster decay rate over these initial distances.

4. Discussion

Over the distance range 50 mm to 110 mm, set by experimental limitations, we observe a $\sim 60\%$ fall in maximum OH^\bullet flux from $4.5 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ to $1.7 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$. Using the model results, a value of $3.2 \times 10^{20} \text{ m}^{-2} \text{ s}^{-1}$ is estimated at the plasma edge, equivalent to a density in the plasma of $\sim 6.1 \times 10^{19} \text{ m}^{-3}$. Since the Henry solubility constant for OH^\bullet is low, $3.8 \times 10^{-4} \text{ M Pa}^{-1}$ [60], the liquid surface solubility limit is $\sim 20 \mu\text{M}$ for the equivalent partial pressure. We therefore need to determine if this limit impacts on OH^\bullet measurements in the liquid. The time evolution of $[\text{OH}^\bullet]$ in a shallow surface layer ΔX can be numerically simulated using a simplified flux—reaction model,

$$[\text{OH}^\bullet](t) = \frac{\Gamma \Delta T}{1000 N_A \Delta X} - \sum_{m=1}^{m=N} k_m [S_m] [\text{OH}^\bullet] \Delta T \quad (1)$$

where Γ is the OH^\bullet flux density, S_m the reacting species and k_m the associated rate constants. Considering only the $\text{OH}^\bullet + \text{TA}$

($k_{\text{OH}^\bullet\text{-TA}} = 4 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$) [53] and $\text{OH}^\bullet + \text{OH}^\bullet$ reactions ($k_{\text{OH}^\bullet\text{-OH}^\bullet} = 4 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$), the surface OH^\bullet concentration reaches a steady-state of $\sim 6 \mu\text{M}$ in less than 1 μs , assuming no surface depletion of the TA probe. The surface layer depth, estimated using the equation $\Delta X^2 = D_{\text{OH}^\bullet} \Delta T$, and a OH^\bullet diffusion constant of $2.3 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$ [61], is 1.5 nm for ΔT of 1 ns. Under worst-case conditions of static unmixed fluid along with TA depletion, the Henry limit would be reached in ~ 30 ms, with an ultimate steady state OH^\bullet concentration of $\sim 100 \mu\text{M}$. However, since the He gas is bubbled through the fluid, a well-mixed solution is obtained and the Henry limit is unlikely to affect OH^\bullet transfer into solution. The Henry limit for H_2O_2 is approximately four orders of magnitude higher than that for OH^\bullet .

Direct comparison with OH^\bullet production rates obtained from other OH^\bullet generation sources is difficult. Generally, values of OH^\bullet concentration in liquid are reported, representing the dynamic balance between generation and loss, whereas flux density values can represent an actual production rate of deliverable species, provided radical losses due to the chemical probe dominate all other reactions, i.e. by using a high reaction rate scavenger at high concentration. Terephthalic acid has a rate constant similar in magnitude to other possible OH^\bullet reactions with trace species (OH^\bullet , HO_2 , O_2^-) and much higher than the $\text{OH}^\bullet + \text{H}_2\text{O}_2$ ($3 \times 10^7 \text{ M}^{-1} \text{ s}^{-1}$) reaction. Although the use of a scavenger to determine species concentration will also involve competing reactions, the scavenger concentration is typically much higher than that of any other relevant species. At a TA concentration of 2 mM, the assumption that the measured $\text{TA} \rightarrow \text{HTA}$ conversion represents substantially all OH^\bullet reactions in liquid is reasonable. We can therefore convert our observed flux density values to concentration rates with a negligible loss of accuracy, $74 \mu\text{M s}^{-1}$ (50 mm) and $28 \mu\text{M s}^{-1}$ (110 mm), for comparison with the non-plasma-based literature. These rates assume flux scales with area, e.g. using extended plasma arrays (the

rate would be 0.23 nmol s^{-1} for a plasma jet). In gamma radiolysis, typical dose rates are 10^{-3} – $10^{-2} \text{ Gy s}^{-1}$ [62] and for low LET radiation, the OH^\bullet *G*-value is 2.8 at room temperature, equivalent to a production rate of 0.001 – $0.030 \text{ } \mu\text{M s}^{-1}$, while with x-ray radiolysis, production levels of $0.3 \text{ } \mu\text{M s}^{-1}$ have been reported [63]. In AOPs with UV excitation, direct measurements of rates [64, 65] or of OH^\bullet concentrations [66, 67] indicate rates up to $\sim 0.01 \text{ } \mu\text{M s}^{-1}$ whereas with VUV excitation of the gas phase, $70 \text{ } \mu\text{M s}^{-1}$ has been demonstrated [68]. OH^\bullet generation via the traditional Fenton, or Fenton-like reactions, can be enhanced using an external electric field [69] and/or heterogeneous catalysts to deliver rates in the range 0.1 – $1.0 \text{ } \mu\text{M s}^{-1}$ [70, 71], while the addition of high concentrations of H_2O_2 further increases the rate to 1 – $10 \text{ } \mu\text{M s}^{-1}$ [72, 73].

For comparison with similar remote RF plasma sources, measured OH^\bullet densities (m^{-3}) in the gas phase are often the preferred metric. Gas phase density can be converted to flux density for comparison where gas flow and velocity values are given. Maximum reported flux densities are in the range 2×10^{19} – $2 \times 10^{21} \text{ m}^{-2} \text{ s}^{-1}$, with the variability due mainly to the H_2O content, which ranged from 500 ppmv to 11 000 ppmv, and the background gas into which the plasma flows (air or inert) [22, 43, 44, 74–76]. The H_2O to OH^\bullet conversion efficiency ($N_{\text{OH}}/N_{\text{H}_2\text{O}}$) i.e. the number of OH^\bullet generated per H_2O molecule varies from approximately 1% to 0.1%, decreasing with increasing water content. These high flux density values represent conditions measured within the plasma region. However, Schroter *et al* [22] observe a 75% reduction in flux for a gap of 5 mm, with the He plasma effluent isolated from air, while Benedikt *et al* also reports a fall of $\sim 80\%$ over 20 mm [26]. For argon flowing into an air gap, Li *et al* observed $\sim 90\%$ fall over 12 mm [34]. The measurements shown in figure 6(a), for distances up to 110 mm, represent the first such far effluent measurements of OH^\bullet and show that while a sharp reduction in flux density is likely over the initial 5 mm, thereafter the reduction is much more gradual. Overall, the final flux at 110 mm is $\sim 5\%$ of the mean value at zero gap and by comparison, the remote RF plasma demonstrates a performance capability well above that of other, non-plasma OH^\bullet generation sources, while avoiding the complex additional interactions and species associated with directly coupled plasmas.

We also compared the remote RF OH^\bullet flux densities with those for direct contact or directly coupled plasma sources and configurations. Measurements are either obtained from gas phase, as with the RF plasmas above, or using chemical probes in liquid. In the latter case, for many reported OH^\bullet measurements, only the steady-state OH^\bullet concentration is given, and the information regarding the time to reach steady-state is absent. Low frequency-driven (kHz) plasmas often display a long luminous jet plume due to the propagation of ionisation waves, which maintain the plasma a significant distance beyond the plasma electrodes [77]. Gas phase flux densities are reported in the range 5×10^{20} – $10^{22} \text{ m}^{-2} \text{ s}^{-1}$, close to the plasma ($< 4 \text{ mm}$) and within the plume [33, 78, 79]. Here the plasmas were driven via pin/needle electrodes and electrically coupled to the liquid, while Yonemori *et al*, report a lower

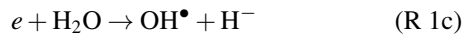
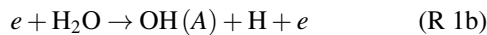
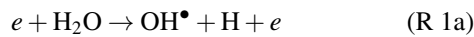
value of $2 \times 10^{20} \text{ m}^{-2} \text{ s}^{-1}$ for insulated DBD electrodes [80]. Verreyken *et al* report a factor of 10 reduction in flux when the gap is increased by 7 mm.

From liquid concentration rates and plasma geometry, we extracted equivalent flux densities. For example, Gorbanev *et al* [49] used a parallel field 4 mm diameter plasma jet (18 kV, 25 kHz), with various He– O_2 (0%–0.5%)– H_2O (0%–4%) gas mixtures at 4–10 mm from liquid. The liquid remained in contact with the plasma plume and the background environmental gas was He. The maximum OH^\bullet concentration was $24 \text{ } \mu\text{M}$ ($> 2000 \text{ ppmv H}_2\text{O}$, 0% O_2), equivalent to a OH^\bullet delivery rate of $0.4 \text{ } \mu\text{M s}^{-1}$. The OH^\bullet concentration was measured by electron paramagnetic resonance (EPR), using 5,5-dimethyl-1-pyrroline N-oxide (DMPO–OH) (100 mM) and, with a liquid sample volume of $100 \text{ } \mu\text{L}$ the equivalent OH^\bullet flux density is $1.9 \times 10^{18} \text{ m}^{-2} \text{ s}^{-1}$. Including 0.2% O_2 with He instead of H_2O reduces the flux by $> 0\%$, while a further 30% reduction is observed for the oxygen–water mixture He– O_2 (0.2%)– H_2O ($> 2000 \text{ ppmv}$). Additional OH^\bullet formation due to plasma-induced UV-photolysis directly in liquid was found to be negligible. UV-photolysis rates of $\sim 1 \text{ pM s}^{-1}$ have also been reported for a similar plasma (1 kV, 35 kHz) with argon [31]. Chauvin *et al* (10 kV, 10 kHz) report a rate of $0.4 \text{ } \mu\text{M s}^{-1}$ and a slightly lower equivalent OH^\bullet flux density, $2 \times 10^{18} \text{ m}^{-2} \text{ s}^{-1}$ [81]. In this case, the liquid was placed near the limit of the plume and the background gas constituents were He/air ($\sim 80:20$). Uchiyama *et al* (18 kV, 20 kHz) obtained $4 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ for Ar/air near the edge of the plume but this reduced by an order of magnitude with an additional gap of 10 mm outside the plume [63]. These devices utilised isolated DBD electrode configurations while the electrically coupled pin/needle configuration produced a higher flux density, $1 \times 10^{20} \text{ m}^{-2} \text{ s}^{-1}$ [82]. With larger scale (DBD, streamer or spark) water treatment reactors, typical rates are $\leq 0.05 \text{ } \mu\text{M s}^{-1}$, although Kovačević *et al* using O_2 gas, and a continuous flow water electrode demonstrated maximum OH^\bullet production rates of $12 \text{ } \mu\text{M s}^{-1}$ [83–87]. The fact that OH^\bullet production rates for the remote non-coupled He– H_2O device are similar or higher than directly coupled in-contact plasmas is somewhat surprising since, in the latter, radical generation is expected to be continuous over the whole path from plasma to target. One likely reason is the inevitable presence of air in directly coupled configurations leading to the high-rate production of other radicals (e.g. NO^\bullet , NO_2^\bullet , NO_2^-) which act as OH^\bullet scavengers in the gas and liquid phases [82]. Even without air, the presence of high H^\bullet radical concentrations will efficiently recombine with OH^\bullet at the liquid surface [32].

The OH^\bullet radical can be formed by electron impact ionisation, excitation, or attachment of water as well as through metastable—neutral reactions, ion molecule/cluster reactions, ion-ion recombination, and Penning ionisation [25]. At lower water concentration, metastable reactions can be important with electron impact dissociation and dissociative electron detachment becoming dominant at $\sim 3000 \text{ ppmv}$ [33, 34]. Assuming a simple loss model with equal OH^\bullet and H^\bullet recombination rates, the OH^\bullet density is expected to follow the density of H_2O via a $N_{\text{H}_2\text{O}}^{0.5}$ relationship, as observed by Bruggeman *et al* up to $\sim 1\% \text{ H}_2\text{O}$ [44], although other reports

show N_{OH^\bullet} following a linear relationship with $N_{\text{H}_2\text{O}}$ up to ~ 5000 ppmv before saturating [26, 33]. Above 6000 ppmv, the OH^\bullet density saturates at $2\text{--}4 \times 10^{20} \text{ m}^{-3}$ [26, 33, 44]. These values are similar to the estimated plasma N_{OH^\bullet} in this work of $5 \times 10^{20} \text{ m}^{-3}$ at 600 ppmv H_2O . Regarding peroxide, a linear $\text{H}_2\text{O}_2\text{--H}_2\text{O}$ relationship has been observed [43, 47, 48]. There are, however, discrepancies in reported concentrations between different measurement techniques [26, 43]. For example, OH^\bullet density values of $1.5 \times 10^{20} \text{ m}^{-3}$ have been reported from cavity ring down spectroscopy and UV absorption, but $\sim 6 \times 10^{19} \text{ m}^{-3}$ from mass spectroscopy at 2000 ppmv. Discrepancies will also reflect the differences in measurement principle that is potentially amplified with instrument location with respect to the plasma source. For example, LIF measurements of OH^\bullet at increasing distances from the plasma report increasing discrepancy with those from absorption measurements at the same location, the latter showing almost constant $[\text{OH}^\bullet]$ with distance up to 9 mm, while LIF indicates an almost one order of magnitude fall [33]. However, absorption measurements are line integrated therefore less affected by increasing radial diffusion with distance, hence will more reliably capture the total OH^\bullet flux.

The results show that feed gas humidity plays a fundamental role in the characteristics of the plasma jet used in these experiments. Power absorbed, along with OH^\bullet and H_2O_2 radical production are all shown to be sensitive to the water precursor content. OH^\bullet production pathways depend on plasma conditions and include via electron dissociation of water or water dissociation products (HO_2 , H_2O_2). Other pathways include He metastable interaction with H_2O and H_2O clusters and excited oxygen or He ion interactions with H_2O [22, 76, 88, 89]. The model of Schroter *et al* [22] of an RF jet indicates electron dissociation of water is dominant at the initial stages of the plasma i.e.



whereas at later stages, within plasma or after-glow reactions such as $\text{H} + \text{HO}_2 \rightarrow 2\text{OH}^\bullet$ and $\text{H} + \text{H}_2\text{O}_2 \rightarrow \text{OH}^\bullet + \text{H}_2\text{O}$ can become important. Brisset *et al* [76] with a similar jet and simulation model noted the reaction $\text{H}_2\text{O}^+ + \text{H}_2\text{O} \rightarrow \text{OH}^\bullet + \text{H}_3\text{O}^+$ was a significant source of OH^\bullet well within the plasma. By comparison, the plasma device used here is ≤ 3 mm in length, equivalent to the initial stages of [22] where reaction R1 is dominant. It is expected therefore that the OH^\bullet density is largely dependent on a variation in both water content and electron density, which in turn is dependent on power. As previously shown in He– O_2 plasmas, an increase in molecular dissociation with absorbed power is a result of a linear increase in electron density with

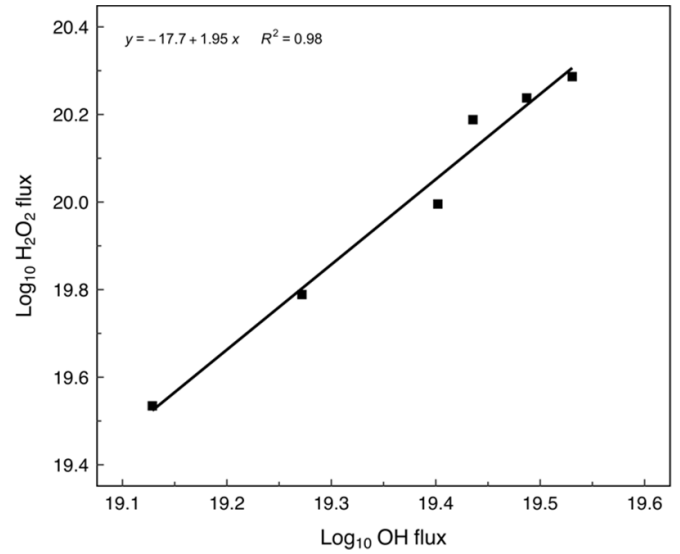
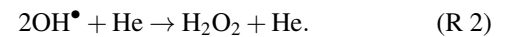


Figure 7. Log (OH^\bullet) vs log (H_2O_2) fluxes under identical operating conditions indicating a gradient of 1.95 close to the expected $[\text{H}_2\text{O}_2]$ dependence on $[\text{OH}^\bullet]^2$.

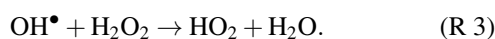
power [38] and a similar trend is therefore also expected for He– H_2O . However, above 0.5 W the increase in OH^\bullet is sub-linear (figure 3(b)), a trend also observed with H_2O_2 . Since the primary source of H_2O_2 is via the recombination of OH^\bullet ,



We expect H_2O_2 flux to depend on $[\text{OH}^\bullet]^2$ and a log plot of H_2O_2 versus OH^\bullet indicates a gradient of 1.95, (figure 7). At powers above 0.5 W, at fixed H_2O concentrations, both OH^\bullet and H_2O_2 flux tend to saturate at values of $3.5 \times 10^{19} \text{ s}^{-1}$ and $1.9 \times 10^{20} \text{ s}^{-1}$ respectively. Since a change in the OH^\bullet production mechanism is not expected at enhanced electron densities i.e. R1 still holds, the saturation indicates increasing losses, which are consistent with R2.

At fixed applied power with increasing H_2O up to ~ 800 ppm, (figure 5(a)) the linear increase in OH^\bullet flux is consistent with R1. The significant decrease in absorbed power with H_2O beyond 800 ppmv (figure 4) is likely the main factor leading to the rapid fall in OH^\bullet flux (figure 5(a)), despite the enhanced precursor concentration at high H_2O . For a constant applied power, a reduction in absorbed power with increased H_2O has also been directly observed or inferred by others [26, 33]. At low H_2O concentrations (< 100 ppmv), the plasma remains electropositive and helium ion species dominate. However as $N_{\text{H}_2\text{O}}$ increases, the plasma becomes more electronegative and the dominant ion species are impurity generated (OH^+ , H_2O^+ , H_3O^+ , $\text{H}^+(\text{H}_2\text{O})_n$ ion clusters). At > 3000 ppmv, negative ion species, $(\text{OH}^-\text{H}_2\text{O})_n$ $n = 1\text{--}3$, become dominant [39]. These are formed by dissociative electron attachment to H_2O and subsequent hydration are a significant source of electron loss and a decrease in absorbed power. Also at high water content, an increasing proportion of energy losses into rotational and vibrational excitation and a different

electron energy distribution function reduce the rate of dissociation and lead to saturation in OH[•] generation. However, from the normalised plot of flux per watt absorbed (figure 5(b)), the approximate square root relationship indicates that power reduction is not the only factor. This saturation with H₂O was also observed by [26] who noted an increase in the O/OH[•] ratio with increasing H₂O, the atomic oxygen derived from either OH[•] dissociation or recombination. It was suggested therefore that the reaction OH[•] + O → O₂ + H provides an increasing significant loss channel at higher H₂O concentrations. However, plasma effluent chemistry may be significantly different from that in the near plasma region as short-lived and charged species recombine rapidly at the plasma edge and long-range transport is dominated by more stable neutral species such as HO₂ and H₂O₂. Simulations [22] in the near-plasma afterglow region indicate the main consumption pathway of OH[•] is via its reaction with H₂O₂,



It is therefore more likely that the higher densities of H₂O₂ produced at higher powers are the primary loss channel for OH[•] radicals over the 50 mm path length from plasma to collection liquid. The main H₂O₂ generation mechanism in the gas phase is via OH[•] three-body recombination, R2 (OH[•] + OH[•] + M → H₂O₂ + M) [47].

Combining the generation and loss reactions from R1 and R2 we can estimate the steady state OH[•] concentration as,

$$[\text{OH}^{\bullet}] = \sqrt{\frac{k_1 [n_e]}{k_2 [\text{He}]}} \sqrt{[\text{H}_2\text{O}]} = k^* \sqrt{\text{H}_2\text{O}} \quad (2)$$

where k_1 and k_2 are the rate constants for R1 and R2 respectively, and the slope k^* , can be obtained from figure 5(b), for 50 mm distance. To obtain the equivalent slope in the plasma region, the flux density at the plasma edge is taken from figure 6(a), and the ratio of fluxes at 0 mm and 50 mm is used as a scaling factor, leading to a value of k^* (0 mm) of $2.7 \times 10^{18} \text{ m}^{-3/2}$. See supplementary data S2. After compensating for a difference in power densities, comparison with a similar characteristic by Bruggeman *et al*, gives a k^* value ratio equal to ~ 0.5 [44], which is commensurate with the difference in electron density between the two systems [44].

The model simulation proved reliable in predicting the OH[•] flux characteristics of the plasma effluent. A maximum flux delivery was predicted at ~ 200 ppmv, similar to that seen experimentally at 790 ppmv. While previous studies have shown that OH[•] density in the plasma region continues to increase with humidity [26, 33, 44], the data here shows that trends in plasma density are not necessarily an indication of trends in the effluent. The model proved accurate at predicting both the OH[•] and H₂O₂ fluxes over extended distances. This enabled the flux of other reactive species in the effluent to be estimated with reasonable reliability. As evidenced by the model, while high flux delivery of H₂O₂ up to 110 mm was expected due to its long lifetime, the effluent also delivers multiple highly reactive species, such as OH[•], H and O over long distances.

5. Conclusions

We have demonstrated a new gas-based OH[•] generation source using a low power RF-driven atmospheric pressure plasma configured to deliver the radical flux into the far effluent region, well away from interference from other plasma factors such as electric fields, currents and UV radiation. Using He–H₂O gas chemistry isolated from the laboratory air, the effluent flux contains H₂O₂ and OH[•] with measured flux values of 2.3 nmol s^{-1} and 0.23 nmol s^{-1} respectively at a distance of 50 mm from the plasma. The OH[•] flux density was $4.5 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ falling to $1.7 \times 10^{19} \text{ m}^{-2} \text{ s}^{-1}$ at 110 mm, equivalent to generation rates of $74 \mu\text{M s}^{-1}$ and $28 \mu\text{M s}^{-1}$. The simulation results show that in addition to OH, the reactive species O, HO₂ and H[•], are also delivered with similar flux densities at 110 mm. Millimetre scale RF-driven plasmas are an ideal configuration for remote delivery of selected species as the plasma itself is restricted to mainly within the electrode region, rather than extending well beyond the electrodes in a long jet, as found with lower frequency plasma configurations. It is well known that short-lived radicals suffer very high recombination rates within a few millimetres of the RF plasma exit. Despite this, the escaping flux is still significant, indicating a viable delivery capability to downstream targets. Its performance with regard to OH[•] generation rates compares well with traditional OH[•] generation techniques such as radiolysis, AOPs and enhanced Fenton-chemistry approaches where rates are sub $\mu\text{M s}^{-1}$ and the potential therefore exists for a large enhancement of OH[•] supply using RF plasma arrays. Alternatively, the use of single plasma devices delivering precisely quantifiable OH[•] fluxes provides new opportunities for scientific studies in cell biology, atmospheric chemistry, protein unfolding and systematic dose studies for plasma-based and other OH[•] related medical treatments. The potential also exists for OH[•] and other radical transport over longer distances in fixed or flexible tubing, opening the possibility for direct *in-vivo* studies leading to new radical-based treatments and tumour therapies.

Data availability statement

The data that support the findings of this study are available upon reasonable request from the authors.

Acknowledgments

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