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SPECIALTY SECTION This article was submitted to Smart Grids, a section of the journal Frontiers in Energy Research

RECEIVED 25 September 2022 ACCEPTED 30 November 2022 PUBLISHED 18 January 2023

CITATION

Lv G, Ji Y, Zhang Y, Wang W, Zhang J, Chen J and Nie Y (2023), Optimization of building microgrid energy system based on virtual energy storage. *Front. Energy Res.* 10:1053498. doi: 10.3389/fenrg.2022.1053498

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Optimization of building microgrid energy system based on virtual energy storage

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With the continuous development of building microgrids, it is crucial to explore and study the energy-saving potential of buildings to resolve energy shortages and environmental protection problems. Therefore, to realize the efficient and economical operation of a building microgrid, a new multi-objective optimization method is proposed for the planning and operation of building microgrid considering virtual energy storage. First, virtual energy storage model of the building microgrid is established based on the heat storage characteristics of the building itself. Second, a multi-objective optimization model of the building microgrid considering virtual energy storage is constructed by considering the investment cost and the comprehensive operation benefits as the objectives as well as the constraints of cooling, heating, power balance. Finally, based on the original gray wolf swarm algorithm, the niche processing mechanism and gray weighted correlation method are introduced to optimize the configuration and operation of the building microgrid. For a typical building microgrid in summer and winter, the simulation results reveal that the proposed method improves the overall economy of planning the building microgrid system and its operation and user experience via virtual energy charge and discharge management.

KEYWORDS

building heat storage characteristics, building microgrid, gray weighted correlation degree, multi-objective optimization, virtual energy storage

1 Introduction

Promoting the development of clean energy systems based on distributed energy is a major strategic choice worldwide. At present, research has shown that the proportion of energy consumption in the end-use energy systems of buildings is increasing annually, which has significant potential for energy conservation and emission reduction. Therefore, energy-saving solutions for mining buildings have become crucial approaches to solve the shortage of energy demand and achieve the double carbon goal (Dounis et al., 2009; Zhao et al., 2015).

A building microgrid system is a multi-energy joint energy supply system formed by integrating natural gas, heating, energy storage, and distributed energy systems along with

related technologies into the building energy supply system. To ensure the safe and reliable operation of the system, it is effective to use the diversity of energy supply modes to satisfy the diversified needs of users and use the energy storage system and related control technologies to reduce the impact of fluctuations in the output of clean energy (Guan et al., 2010; Hca et al., 2021). Owing to the integration of supply side energy supply, renewable energy, and demand side cold/heat/electricity load demand, and other elements in the system, new requirements are proposed as follows: 1) ensure the of renewable energy. 2) realize consumption the complementary advantages of various forms of energy on the supply side and cooperative configuration operation to reduce the operation cost of the microgrid. 3) and ensure the energy optimization management for safe and economic operation of the building microgrid system (Wang et al., 2021; Chang et al., 2022).

At present, there has been research progress on the optimal configuration strategy of microgrid energy systems. Liu et al. (2019) proposed a comprehensive energy planning strategy based on the improved kriging model, which rapidly and accurately obtained the optimal capacity allocation scheme of the system. Bahmani et al. (2021) established a cooperative method in which a network of energy hubs collaborates to share adjustable energy. Each hub comprises a combined heat and power unit, electrical chiller, renewable sources, absorption chiller, and boiler. Mixed integer linear programming was used to determine the optimal comprehensive economic cost of the system. Li et al. (2020) considered the uncertainty of wind power and proposed a comprehensive energy system planning strategy based on a scenario method, aiming at investment and wind curtailment costs. Qiu et al. (2015) developed a microgrid energy system planning model to minimize the total investment cost based on the electrical-pneumatic coupling phenomenon. To obtain both the optimal structural configuration and energy management dispatch for multi-energy systems, a generic optimal planning framework was proposed in (Ma et al., 2018) and mixed-integer linear programming was employed to minimize the overall cost. Han et al. (2018) considered the volatility of distributed energy resources, net income of the entire operation cycle, penetration of renewable energy, and reliability of the power supply, and established a three-objective two-stage planning model. Lin et al. (2021) considered the economy and reliability of an integrated energy system and proposed a planning model based on an improved collaborative algorithm to coordinate the complex relationship between the two performance indexes, and they verified the effectiveness of the model using a practical example. Based on the above literature, it is evident that for integrated energy system research, the minimum operating cost of the system is usually selected as the optimization objective, and there are several deterministic constraints, such as power balance and equipment output. However, load changes caused by environmental costs and temperature constraints is given less priority.

Simultaneously, by exploiting the complementary characteristics of various power sources in the building microgrid energy system, peak shaving and valley filling can be realized and the energy utilization rate can be improved through the charge and discharge regulation of the energy storage system. However, the initial investment in configuring energy storage equipment is high, and virtual energy storage technology provides a potential solution to the problem. Wang et al. (2020) conducted a detailed study on the virtual energy storage technology of an air conditioning load, established a virtual energy storage energy model, and verified the feasibility of using the virtual energy storage of an air conditioning load for power grid regulation. Zhu et al. (2019) considered virtual energy storage on the user side and established a comprehensive energy system scheduling model including the temperature control load and electric vehicle with consideration of the uncertainty of weather. The simulation results reveal that virtual energy storage has a positive significance in reducing the capacity of energy storage equipment. Jin et al. (2017) considered the characteristics of virtual energy storage and batterycoordinated operation and proposed a control strategy for stabilizing the power fluctuation of a microgrid tie line. Currently, research on the joint optimization of the energy storage optimization link and other energy supply equipment in building microgrid energy systems needs more in-depth analysis.

In summary, this paper proposes a method for capacity configuration and operation optimization of building microgrid systems considering virtual energy storage through the optimal adjustment of temperature. The main contributions of this study are the following.

- Based on the thermal storage characteristics of buildings, a virtual energy storage system model of the building microgrid is constructed. The charge and discharge management of virtual energy storage is realized to achieve low-carbon operation of building microgrid systems.
- 2) The proposed strategy considers the principle of virtual energy storage to construct a multi-objective optimization model to improve the operation economy of the building microgrid.
- 3) The comprehensive benefits and user satisfaction are introduced as the objectives. Under meeting customer satisfaction index, the proposed strategy increases comprehensive benefits through virtual energy storage charging and discharging management.
- 4) The gray wolf algorithm based on niche technology was employed to solve the optimization problem. Based on the non-dominated solution set, the optimal solution of the system configuration and operation was obtained using the gray-weighted correlation degree evaluation index.



5) Structure and mathematical model of building microgrid system

2 Structure of building microgrid system

With the continuous development of distributed energy technology, various energy equipment, such as refrigeration units, gas turbines, heat storage tanks, energy storage equipment, and PV equipment, are connected to buildings. This energy equipment can realize complementary and cooperative effects among energy sources to satisfy the diversified needs of users and improve the overall operational efficiency of the system (Favre-Perrod, 2005; Pazouki et al., 2014).

In this study, a variety of energy devices were applied to a building microgrid system, the structure of which is illustrated in Figure 1. Absorption chillers and electric chillers satisfy the cooling demand of buildings, and the cooling power of absorption chillers originates from gas turbines. The thermal power demand originates from the gas turbine, thermal storage system, and virtual energy storage system in the building. The virtual thermal energy storage is the indoor energy change caused by the temperature change. The electric load power originates from photovoltaics, energy storage equipment, and the external power grid. From the above process, it is evident that the building microgrid system formed by the cold thermal–electrical structure and the external power grid are interconnected.

3 System modeling

3.1 Photovoltaic device

Photovoltaic equipment can convert solar radiation energy into electrical energy *via* photovoltaics, and the conversion efficiency primarily depends on the illumination and ambient temperature, which can be expressed as follows (Ma et al., 2016):

$$P_{pv,t} = \eta \times Y_{pv} \left(\frac{I_T(t)}{I_S} \right), \tag{1}$$

where η represents the energy conversion efficiency (%), $Y_{\rm pv}$ indicates the capacity of the photovoltaic panel (kW), $I_{\rm T}({\rm t})$

represents the solar radiation intensity (kW/m²) received by the photovoltaic panel at time *t*, and $I_s = 1 \text{ kW/m}^2$.

3.2 Electric refrigerator

The refrigerator was cooled by consuming electric energy, and its cooling power was as follows:

$$Q_{\text{EC},t} = P_{\text{EC},t} I_{\text{COP}}^{\text{EC}},\tag{2}$$

where $I_{\text{COP}}^{\text{EC}}$ indicates the ratio of the rated cooling capacity to the rated power of the electric refrigerator, $Q_{\text{EC},t}$ corresponds to the refrigeration power (kW), and $P_{\text{EC},t}$ denotes the electric power consumed (kW).

3.3 Micro gas turbine

The active power output of the micro gas turbine is as follows:

$$P_{\mathrm{mt},t} = \eta_{\mathrm{mt}} P_{\mathrm{gas}},\tag{3}$$

where η_{mt} indicates the power generation efficiency of the micro gas turbine, $P_{\text{mt},t}$ denotes the active output (kW), and P_{gas} represents the natural gas power consumed (kW).

3.4 Absorption chiller

The small gas turbine drives the absorption chiller through the residual energy in the industrial production process, and its cooling power is as follows:

$$Q_{\rm AC,t} = H_{\rm AC,t} I_{\rm COP}^{\rm AC},\tag{4}$$

where $H_{AC,t}$ indicates the heat consumption power (kW), I_{COP}^{AC} denotes the ratio of the rated cooling capacity to the rated power of the absorption chiller, and $Q_{AC,t}$ represents the cooling power (kW).

3.5 Energy storage device

We adopted the conventional battery model, and the change relationship of the state of charge is as follows:

$$SOC_{bt}(t) = SOC_{bt}(t-1) + \frac{[S_{ch}(t)P_{ch}(t)\eta_{ch} - (S_{dis}(t)P_{dis}(t)/\eta_{dis})]\Delta t}{S_{bt}^{max}}, \quad (5)$$

where $SOC_{bt}(t)$ represents the state of charge of the battery, P_{ch} and P_{dis} denote the charging and discharging powers of the battery (kW), respectively, η_{ch} and η_{dis} denote the charging and

discharging efficiencies, respectively, and $S_{sh}(t)$ and $S_{dis}(t)$ represent the charge and discharge states of the battery, respectively.

3.6 Heat storage device

The heat-storage model is similar to the energy-storage battery model, and the relationship between the state of charge and heat power is as follows (Lu et al., 2015):

$$SOC_{\rm H}(t) = SOC_{\rm H}(t-1) + \frac{\left[P_{\rm ch,H}(t)\eta_{\rm ch,H} - \left(P_{\rm dis,H}(t)/\eta_{\rm dis,H}\right)\right]\Delta t}{S_{\rm H}^{\rm max}},$$
(6)

where $SOC_{\rm H}(t)$ indicates the state of charge, $P_{\rm ch,H}$ and $P_{\rm dis,H}$ denote the heat charging and discharging power (kW), respectively, and $\eta_{\rm ch,H}$ and $\eta_{\rm dis,H}$ refer to the heat charging and discharging efficiencies, respectively, $S_{\rm H}^{\rm max}$ denotes the capacity of the heat storage device (kW).

3.7 Building virtual energy storage system

A building can be regarded as a heat storage body because of its thermal inertia and heat storage characteristics of indoor air. Thus, when the indoor temperature changes within a certain range are compared with the constant set temperature, the heating or cooling capacity of the building also changes correspondingly relative to the cooling and heating capacity at a constant set temperature. This change can be regarded as the characteristics of the virtual energy storage of the building, and the difference in the value of this heat change can be regarded as the storage and discharge power of the virtual energy storage (the heat change caused by the difference between the set value and the actual value of the temperature).

The relationship between heat inside and outside the building and temperature is:

$$Q_{H} - Q_{d} = C \times \rho \times V \times \frac{d(T_{out} - T_{in})}{dt},$$

$$Q_{d} - Q_{AC} = C \times \rho \times V \times \frac{d(T_{in} - T_{out})}{dt}.$$
(7)

Eq. 7 represents the two operating conditions of heating in winter and cooling in summer: where Q_H indicates the heating power in winter (kW), Q_d denotes the heat dissipation power of the building (kW), Q_{AC} corresponds to the cooling power in summer (kW), ρ symbolizes the air density (kg/m³), *C* denotes the specific heat capacity of the air (J/(kg.°C)), *V* refers to the indoor volume (m³), and T_{out} and T_{in} are the indoor and outdoor temperatures (°C), respectively.

Taking summer cooling as an example, the key factors affecting the heat change in the building include three parts:

the indoor heat change caused by solar radiation, difference between the heating power, and the cooling equipment power in the building, as shown below:

$$K_{\text{wa}} S_{\text{wa}} (T_{\text{out}} - T_{\text{in}}) + K_{\text{wi}} S_{\text{wi}} (T_{\text{out}} - T_{\text{in}})$$

+IS_{wi} SC + Q_{in} - Q_{cl} = ΔQ , (8)

where ΔQ indicates the indoor heat change value of the building (kW), K_{wa} and K_{wi} denote the heat transfer coefficients of the outer wall and the outer window (W/(m² K)), respectively, S_{wa} and S_{wi} denote the area of outer wall and outer window (m²), respectively, *I* indicates the solar radiation intensity (kW/m²), SC denotes the shading coefficient, Q_{in} denotes the heating power in the building (kW), and Q_{cl} indicates the cooling power (kW).

4 Operation model of building optimal configuration

4.1 Objective function

In the capacity allocation process, with the goal of minimizing the comprehensive benefit of building equipment and equipment investment costs, a multi-objective optimization function is constructed as follows:

$$\min \begin{cases} F_1 = \frac{1}{C_1 + C_3 - C_2}, \\ F_2 = C_4, \end{cases}$$
(9)

where F_1 indicates the comprehensive income of the building micro network (1/yuan), C_1 represents the operation and maintenance cost of the equipment in the building (yuan), C_2 represents the comprehensive income and user satisfaction of the building (yuan), C_3 represents the environmental and fuel costs of the building microgrid system (yuan), and F_2 refers to the investment cost of each piece of equipment of the building microgrid system (yuan), expressed by C_4 .

4.2 Objective function F_1

4.2.1 Operation and maintenance cost

$$C_{1} = \sum_{t=1}^{N} \left(C_{pv} P_{pv,t} + C_{bt} P_{bt,t} + C_{ec} P_{ec,t} + C_{gas} P_{gas,t} + C_{H} P_{H,t} + C_{ac} P_{ac,t} + C_{ph,t} P_{ex,t} \right) \Delta t,$$
(10)

where C_{pv} , C_{bt} , C_{ec} , C_{gas} , C_{H} , and C_{ac} denote the unit time operation and maintenance costs (yuan/kWh) of photovoltaic devices, batteries, electric refrigerators, micro gas turbines, heat storage tanks, and absorption chillers, respectively, $P_{ex,t}$ indicates the electric power exchanged between the building microgrid and

the external power grid (kW); $C_{\rm ph,t}$ denotes the unit power purchase cost at *t* (yuan/kWh), which adopts the time-of-use price to guide the user's power consumption behavior, $P_{\rm pv,t}$, $P_{\rm bt,t}$, $P_{\rm ec,b}$, $P_{\rm mt,t}$, $P_{\rm H,b}$ and $P_{\rm ac,t}$ refer to the outputs (kW) of photovoltaic device, storage battery, electric refrigerator, micro gas turbine, heat storage tank, and absorption refrigerator, respectively, at time *t*; N = 24, $\Delta t = 1$.

4.2.2 Comprehensive income and user satisfaction

$$C_{2} = \sum_{t=1}^{N} \left(\left(C_{\text{pvsu}} P_{\text{pv,t}} + C_{\text{btsu}} P_{\text{bt,t}} \right) \Delta t + \lambda \left| T_{\text{in,t}} - T_{\text{set}} \right| \right), \quad (11)$$

where the first item indicates the photovoltaic consumption income, and C_{pvsu} denotes the photovoltaic subsidy price (yuan/kWh). The second item corresponds to the peakshaving income from energy storage, and C_{btsu} refers to the peak-shaving auxiliary service price, $P_{bt,t}$ indicates the battery power participating in the peak-shaving period t (kW). The energy storage device was charged at the low-load valley and discharged at a high load peak. Through the low storage and high discharge mechanism, it can fill the valley and cut the peak, and increase the peak regulation income of the system. The third item is user satisfaction; λ denotes the energy penalty factor, $T_{in,t}$ indicates the actual temperature in the building, and T_{set} represents the set temperature (°C).

4.2.3 Environmental cost and fuel cost

$$C_{3} = \sum_{t=1}^{N} (K_{SP}C_{S} + K_{NP}C_{N} + K_{CP}C_{C})P_{mt,t}\Delta t + \sum_{t=1}^{N} C_{mt}P_{mt,t}\Delta t,$$
(12)

where the first term indicates the environmental cost, and K_{sp} , K_{np} , and K_{cp} denote the emission intensities of SO₂, NO_x, and CO₂, respectively, produced by the gas turbine, which are 0.01026, 0.01702, and 0.000928 kg/kWh, respectively (Zhang et al., 2017; EPA et al., 2021). $P_{mt,t}$ indicates the output (kW) of the gas turbine at time *t*, and C_{s} , C_{n} , and C_{c} represent the unit treatment costs of SO₂, NO_x, and CO₂ produced by the gas turbine, which are 0.21, 0.13, and 14.824 yuan/kg, respectively (Zhang et al., 2017; EPA et al., 2021). The second item indicates the fuel cost; C_{mt} denotes the fuel cost per hour of the unit gas turbine, which is 0.3894 yuan/kWh.

4.2.4 Objective function F_2

$$C_{4} = (S_{\rm mt}c_{\rm mt} + S_{\rm bt}c_{\rm bt} + S_{\rm ec}c_{\rm ec} + S_{\rm pv}c_{\rm pv} + S_{\rm ac}c_{\rm ac} + S_{\rm H}c_{\rm H}), \quad (13)$$

where S_{mt} , S_{bt} , S_{ec} , S_{pv} , S_{ac} , and S_{H} denote the installation capacities (kW) of the micro gas turbine, battery, electric

refrigerator, photovoltaic device, absorption refrigerator, and heat storage tank, respectively, and c_{mt} , c_{bt} , c_{ec} , c_{pv} , c_{ac} , and c_{H} denote the unit capacity installation costs (yuan/kW) of the micro gas turbine, battery, electric refrigerator, photovoltaic device, absorption chiller, and heat storage tank, respectively.

4.3 Constraints

4.3.1 Electric power balance constraint

$$P_{\text{ex},t} + P_{\text{PV},t} + P_{\text{bt},t} = P_{\text{el},t} + P_{\text{EC},t},$$
 (14)

where $P_{el,t}$ indicates the electric power load (kW) at time *t* and $P_{ex,t}$ represents the power (kW) of the connecting line; that is, the electric power exchanged between the building microgrid and the external power grid.

4.3.2 Cooling power constraint

$$Q_{\text{AC},t} + Q_{\text{EC},t} = Q_{\text{cool},t}, \qquad (15)$$

where $Q_{\text{cool,t}}$ is the cooling power load (kW) at time *t*.

4.3.4 Thermal power balance constraint

$$Q_{\text{heat},t} - Q_{\text{out},t} - \eta_{\text{eh}} P_{\text{mt},t} = \Delta Q, \qquad (16)$$

where $Q_{\text{heat},t}$ denotes the thermal power load (kW) at time *t*, $Q_{\text{out},t}$ represents the thermal power output (kW) of the thermal storage device at time *t*, and η_{eh} denotes the electric heating ratio of the micro-gas turbine.

4.3.5 Equipment configuration and operating output upper and lower limit constraints

$$\begin{cases} S_{EC}^{\min} \leq S_{EC} \leq S_{EC}^{\min}, \\ S_{mt}^{\min} \leq S_{mt} \leq S_{mt}^{\max}, \\ P_{ex}^{\min} \leq P_{ex} \leq P_{ex}^{\max}, \\ P_{EC}^{\min} \leq P_{EC} \leq P_{EC}^{\min}, \\ P_{mt}^{\min} \leq P_{mt} \leq P_{mt}^{\max}, \end{cases}$$
(17)

where Smin * and Smax * represent the lower and upper capacity limits of each device (kW), respectively, and *P*min * and *P*max * denote the lower and upper output limits of each device (kW), respectively.

4.3.6 Constraints related to energy storage system

Charging and discharging power constraint:

$$\begin{cases} 0 \le P_{\rm dis}(t) \le P_{\rm dis}^{\rm max} S_{\rm dis}(t), \\ 0 \le P_{\rm ch}(t) \le P_{\rm ch}^{\rm max} S_{\rm ch}(t). \end{cases}$$
(18)

Charging and discharging state transition constraint:

$$S_{\rm ch}(t) + S_{\rm dis}(t) = 1.$$
 (19)

Power storage constraints:

$$SOC_{bt}^{\min} \le SOC_{bt}(t) \le SOC_{bt}^{\max}$$
. (20)

Configure capacity constraints:

$$S_{\rm bt}^{\rm min} \le S_{\rm bt}\left(t\right) \le S_{\rm bt}^{\rm max},\tag{21}$$

where P_{ch} max and P_{dis} max denote the maximum power (kW) of the charge and discharge, respectively; SOC_{bt}^{max} and SOC_{bt}^{min} represent the upper and lower limits of the state of charge of the battery, respectively; and S_{bt}^{max} and S_{bt}^{min} represent the upper and lower limits of the configuration capacity (kW), respectively.

4.3.7 Indoor temperature expectation interval constraint

$$T_{\rm in}^{\rm min} \le T_{\rm in} \le T_{\rm in}^{\rm max},\tag{22}$$

where *T*max and *T*min denote the expected upper and lower limits of the indoor temperature (°C), respectively.

5 Multi-objective solution strategy

We optimize the configuration of various types of equipment in a building based on virtual energy storage. The optimal mathematical model is established with the state of charge of the battery, output of the refrigerator, input and output power of the heat storage system, and indoor temperature of the building as the decision variables. The constraints include the power balance of the cooling, heating, and power loads; the upper and lower limits of the equipment; and the constraints of the equations and inequalities related to the energy storage system. It is difficult to solve complex problems with many variables and constraints using traditional algorithm strategies; therefore, this study introduces an improved multiparticle swarm wolf optimization (MPSWO) to optimize the solution. Based on the original swarm wolf algorithm, the niche processing mechanism and gray weighted correlation index are introduced, and the population diversity and self-regulation ability are introduced into the PSWO algorithm (Mirjalili et al., 2014).

5.1 Niche technology

Niche technology forms a niche for each wolf based on the distance between wolves. Using the update iteration principle of particle swarm optimization algorithm, the wolves in the wolf group are also regarded as a group of particles. Subsequently, the PSO algorithm is employed to update each group of particles once in speed and position. For the updated particle swarm returning to the wolf swarm, a sharing mechanism is employed to improve the hunting ability of the wolves and provide the best location according to the distance between the wolves. The crowding distance of the gray wolf is improved based on the notion of particle swarm optimization and can be expressed as

$$d_{ij} = \|x_i - x_j\| = \sqrt{\sum_{k=1}^{N} (x_{ik} - x_{jk})^2},$$
 (23)

where x_i and x_j represent any 2 Gy wolves. For a given parameter, the fitness can be expressed as

$$f_{i}^{1} = \frac{f_{i}}{\sum_{i=1}^{N} S(d_{ij})},$$
(24)

where f_i represents the original fitness and $S(d_{ij})$ represents the sharing function. When the distance between the gray wolves is less than the radius R of the small mirror, the sharing function can be calculated as follows:

$$S(d_{ij}) = 1 - \left(\frac{d_{ij}}{R}\right)^{\lambda},$$
(25)

where λ symbolizes the shape parameter.

5.2 Non-dominated sorting selection strategy based on gray weighted correlation degree

The gray correlation degree analysis method is based on the similarity between the obtained non-dominated solution set curve and optimal dominated curve. The closer the curve, the higher the degree of correlation between the corresponding sequences and the higher the ranking priority. The gray weighted correlation degree was obtained by combining the analytic hierarchy process to select the optimal solution. The steps are as follows (Si et al., 2019).

5.2.1 Preprocessing of objective function matrix

The objective function data matrix is calculated. Because the dimensions of each objective of the proposed optimization strategy are inconsistent, it is necessary to conduct dimensionless processing; thus, the following matrix can be obtained:

$$F = \left[f_i(k)\right]_{N \times m},\tag{26}$$

where $f_i(k) = (\tilde{f}_i(k)/f_i(1)) (k = 1, 2, ..., m, i = 1, 2, ..., N),$ $\tilde{f}_i(k)$ indicates the original value, and $f_i(1)$ the first element of the vector f_i .

5.2.2 Calculating the gray relational degree

First, the intermediate difference matrix is obtained to obtain the minimum difference a and maximum difference b. Then, according to the correlation coefficient formula, the correlation coefficient matrix is calculated as follows:

$$\begin{cases} a = \min_{i} \min_{k} |f_{0}(k) - f_{i}(k)|, \\ b = \max_{i} \max_{k} |f_{0}(k) - f_{i}(k)|, \\ Y = [y_{i}(k)]_{N \times m}, \\ y(f_{0}(k), f_{i}(k)) = \frac{a + \mu b}{|f_{0}(k) - f_{i}(k)| + \mu b}, \end{cases}$$
(27)

where μ is the resolution coefficient, usually taken as 0.5.

1) Determining the corresponding weight of each optimization objective

The corresponding weight ω_k of the *k*th optimization index is determined based on the analytic hierarchy process, as shown in Eqs 28, 29:

$$R = \begin{bmatrix} r_{11} & r_{12} & \cdots & r_{1m} \\ r_{21} & r_{22} & \cdots & r_{2m} \\ \vdots & \vdots & \ddots & \vdots \\ r_{m1} & r_{m2} & \cdots & r_{mm} \end{bmatrix},$$
(28)

$$\omega_k = \frac{1}{m} \sum_{j=1}^m \frac{r_{kj}}{\sum_{l=1}^m r_{lj}} (k = 1, 2, \dots, m),$$
(29)

where r_{ij} indicates the relative importance of optimization objectives *i* and *j*.

5.2.3 Determining the gray weighted correlation degree

The gray weighted correlation degree of the *i*th optimal solution of the Pareto solution set is calculated using Eq. 30

$$\xi_{i} = \sum_{k=1}^{n} \omega_{i} y(x_{0}(k), x_{i}(k)).$$
(30)

According to the size of the gray weighted correlation degree, the solution set is sorted, and a compromise solution is selected. The higher the degree of correlation, the higher is the ranking priority.

5.3 Solution procedure

Initialization algorithm parameters: The population size of the gray wolf was N = 50, and the maximum iteration number was iterax = 100. The initial populations that meet the upper and lower limit constraints of each equipment inequality in the building were randomly generated. Each individual is represented as the feasible value of all control

TABLE 1 Equipment	electrical	parameters.
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Parameter			
Micro-turbine efficiency			
Micro gas turbine thermoelectric ratio			
Micro gas turbine power upper and lower limit (kW)			
Electric refrigerator energy efficiency ratio			
Upper and lower limit of state of charge (pu)			
Upper and lower limit of battery configuration capacity (kWh)			
Maximum charge and discharge power (kW)			
Battery charging efficiency			
Battery discharge efficiency			
Photovoltaic use and maintenance cost (yuan/kWh)			
Battery maintenance cost (yuan/kWh)			
Maintenance cost of electric refrigerator (yuan/kWh)			
Maintenance cost of micro gas turbine (yuan/kWh)			
Photovoltaic subsidy electricity price (yuan/kWh)			
Electricity price for peak shaving auxiliary services (yuan/kWh)			
Use energy penalty factor			
Set temperature (°C)			

variables and coded according to real numbers. Vector u_{ij} represents the *j*th equipment control variable of the *i*th individual, and u_{ij}^{max} and u_{ij}^{min} represent their upper and lower limits, respectively.

- Calculate the fitness value of each wolf in the population, and select the first three best wolves to save them as α, β, and γ.
- 2) According to the four steps of the gray wolf algorithm, including encirclement, hunting, attack, and search, update the current gray wolf individual position and relevant algorithm parameters.
- 3) Randomly add M new gray wolves to maintain population diversity.
- 4) According to niche technology and fitness-sharing mechanisms (23)–(25), adjust the fitness of individuals in the niche.
- 5) Adopt roulette strategy to select *N* excellent gray wolves to enter the next-generation and calculate the fitness to obtain the global optimal value.
- 6) Determine whether the number of iterations is satisfied; if the number of iterations iter is greater than the maximum number of iterations iter^{max}, end the loop and output the result, and obtain the compromise solution by sorting according to the gray weighted correlation degree; otherwise, proceed to step 2).

6 Case study

6.1 Input data and assumptions

The commercial complex is located at $37^{\circ}54'N$, $112^{\circ}33'E$. The building is a single-family building with a length of 70 m, width of 50 m, a 3-storey height, and a total of 33 floors. The exterior walls of the building are made of cement bricks, the windows are made of PVC material and plastic, and double-layer sound insulation vacuum glass is used. The location of the commercial complex is a provincial capital city facing north. Based on the survey data and the relationship between the building windows and the direct angle of the Sun, this study approximately takes $IS_{win}SC$ as $0.45IS_{win}$, and the air density ρ and air specific heat capacity *C* are respectively considered as 1.2 kg/m^3 and $1000 \text{ J/kg}^\circ\text{C}$; centralized office hours are from 8:00 to 20:00.

When the time-of-use electricity price is adopted, the electricity price and load changes can be effectively transmitted to the user side to guide and change the electricity consumption behavior of users, thereby improving the economic level of the building microgrid operation. In this study, the time-of-use electricity price is utilized to purchase the electricity shortage of the microgrid from the external power grid to guide the electricity consumption behavior of users in the building. The electricity price is 0.65 yuan/kWh from 10 to 20 h, and the electricity price is 0.45 yuan/kWh from 0 to 9 h and 21-24 h. The price of natural gas is 2.68 yuan/m³, and the price of its equivalent unit calorific value is 0.45 yuan/kWh. The upper limit of the tie line power between the building microgrid and the external grid is set to 400 kW, while the other simulationrelated parameters are listed in Table 1.

6.2 Simulation example and result analysis

To verify the effectiveness of the building comprehensive energy optimization model and optimization algorithm proposed in this study, the initial values of the optimization variables are obtained according to a uniform distribution within the constraint range, and the following two scenarios are set for calculation and analysis:

Case 1. Optimization of a single scene in winter (December); Case 2: Optimization of a single scene in summer (June);

6.3 Typical scenarios in winter

For the Case 1 scenario, December is winter in the north, the solar light intensity is low, and the temperature difference between day and night is large. To improve the energy-saving



TABLE 2 Optimization results of building microgrid system for Case 1.

Equipment name	Capacity	Investment cost/yuan	Operation and maintenance cost/yuan
Battery	375/kWh	562,500	180
Gas Turbine	650/kW	130,000	468
Photovoltaic	60/kW	60,000	115.2
Heat storage tank	200/kW	14,400	57.6
Electric refrigerator	50/kW	20,000	48
Absorption chiller	200/kW	16,000	120

level of the building microgrid system, based on the principle of virtual energy storage in buildings, the temperature in the building is actively reduced in winter, forming a virtual energy storage thermal load response of the building, as illustrated in Figure 2. Based on the virtual energy storage of this building, the optimal configuration calculation in the typical scenario of Case 1 is performed, and the typical daily operation results are listed in Table 2.

It is evident from the results in Table 2 that solar energy resources are not particularly abundant in winter, and the photovoltaic configuration capacity is small, as presented in Figure 3. The primary function of the electric energy storage system is to cooperate with the photovoltaic system to enhance the utilization rate of photovoltaics simultaneously, play the role of peak shaving and valley filling and emergency load support, and improve the economic level of the comprehensive energy system of the building. The capacity of the battery energy storage system is configured to 375 kWh.

As the main energy supply equipment of the building system, the gas turbine provides electricity and thermal power to the building system, and is the main adjustment method for the building microgrid integrated energy system. Ensuring a reliable supply of heat load is also one of the reasons for the larger configuration of gas turbines.

The absorption refrigeration unit converts the heat generated by the gas turbine power generation into the











TABLE 3 Optimization results of the building microgrid system under Case 2.

Equipment name	Capacity	Investment cost/yuan	Operation and maintenance cost/yuan
Battery	800/kWh	1200000	384
Gas Turbine	350/kW	70,000	252
Photovoltaic	80/kW	80,000	153.6
Heat storage tank	80/kW	5,760	23.04
Electric refrigerator	150/kW	60,000	144
Absorption chiller	250/kW	20,000	150

cooling load; however, it needs to effectively cooperate with the heat storage tank to ensure reliable operation of the heat load system of the building integrated system. Therefore, under the conditions of a typical winter day, the facility configuration capacity in relation to the heat load is higher. In contrast, the cooling load of electric refrigeration and air conditioners is low in winter, and refrigeration equipment is configured according to the lower limit in typical winter scenarios.

Under the calculation conditions of Case 1, to make the configuration capacity of the building microgrid system more reasonable, the optimal scheduling of each piece of equipment on a typical day is performed. The results are presented in Figures 4–6, and the cost-effectiveness of the economical operation is as follows: the environmental cost, fuel cost, photovoltaic consumption benefit, and building virtual energy storage benefit are 309, 2,360, 137, and 189 yuan, respectively. As shown in the figure, owing to the active reduction in indoor temperature in winter, the virtual energy storage of the building has a charging effect to reduce the operating cost of the system. However, in winter, owing to the small amount of heat transferred by sunlight, the operation mode of heat storage and heat storage systems is relatively simple. To ensure a heat supply, gas turbines make the operation mode of the entire integrated energy system inflexible, and the unbalanced power in the microgrid is adjusted by the external grid.



6.4 Typical scenarios in summer

For the Case 2 scenario, June is summer in the north, the solar light intensity is high, and the temperature difference between day and night is small. To enhance the energy-saving level of the building microgrid system, based on the principle of virtual energy storage in the building, the temperature in the building is actively increased in summer, and the virtual energy storage and cooling load response of the building is formed, as illustrated in Figure 7. Based on the virtual energy storage of the building, the optimization calculation is performed under the typical scenario of Case 2, and the typical daily operation results are listed in Table 3.

As indicated in Table3, considering that solar energy resources are particularly abundant in summer, the photovoltaic capacity configuration is relatively high, as depicted in Figure 8. The primary function of an electric energy storage system is to cooperate with the photovoltaic system to improve the utilization rate of photovoltaics. Simultaneously, the economic level of the building's comprehensive energy system can be improved as much as possible through the strategy of low storage and high discharge. The capacity configuration is 800 kWh. In summer, the cooling load demand is primarily considered, and the heating load is small. The gas turbine supplies a small amount of cooling load to the system *via* the absorption chiller; therefore, the gas turbine is configured to 350 kW in a typical summer scenario. In contrast, cooling load-related facilities have a higher configuration capacity to ensure a reliable supply of the cooling load of the building integrated system.

Under the calculation conditions of Case 2, the optimal scheduling results for the building microgrid system are presented in Figures 9-11, and the cost-effectiveness of the economical operation is as follows: the environmental cost, fuel cost, photovoltaic consumption benefit, and building virtual energy storage benefit are 259, 1,640, 337 and 209 yuan, respectively. It is evident from the figure that, owing to the strong sunlight in summer and the small heating load of the gas turbine, the electric energy storage system participates in the energy storage adjustment, which makes the operation mode of the entire integrated energy system more flexible, and the balance of the electric heating and cooling load does not depend on the external power grid. Therefore, in a typical summer scenario, the time-of-use electricity price mechanism of the external power grid can maximize the effect of low storage and high discharge in the building microgrid system to maximize the economic benefit of the building microgrid.

6.5 Algorithm convergence analysis

We proposed an improved multi-objective gray wolf optimization algorithm based on niche technology, and the





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gray weighted correlation index was employed to evaluate and analyze the optimization results. Figure 12 illustrates the multi-objective convergence curve of a typical winter day. The convergence curve was relatively smooth and stable. The 100 fitness function values (non-dominated solutions) obtained by optimization were closely distributed around the gray wolf population (dominated solution set), indicating that the niche technique used in this study effectively improved the ability of non-dominated solutions to approach optimal solutions. Simultaneously, multiple non-dominated solutions improved the selectivity of users and obtained the optimal proportion of investment costs and comprehensive benefits through the gray-weighted correlation value. In summary, the multi-objective gray wolf optimization algorithm based on niche technology proposed in this paper exhibits good convergence in the optimization and solution of a building microgrid system.

7 Conclusion

In this study, we constructed a virtual energy storage system model based on the thermal storage characteristics of a building. On this basis, a capacity configuration and operation optimization method for a building microgrid integrated energy system that considers virtual energy storage was proposed. Through theoretical analysis and simulation, the following conclusions were drawn:

- Virtual energy storage technology was integrated into the optimization model of the building microgrid energy system. By adjusting the indoor temperature of the building to satisfy user requirements, energy management based on virtual energy storage improved the operating economy of the building microgrid system.
- 2) User satisfaction reflected the control effect of virtual energy storage to a certain extent. The larger the indoor temperature control range, the more obvious the virtual energy storage control effect, which indicated that the system had general requirements for user satisfaction and lower operating costs. In contrast, the system had higher requirements for user satisfaction and higher operating costs.
- 3) The improved multi-objective gray wolf optimization algorithm based on niche technology effectively coordinated the optimization relationship between comprehensive benefits and investment costs, improving the ability of non-dominated solutions to approach the optimal solution, and effectively determining the optimal solution through the gray-weighted correlation degree evaluation method, reducing the investment cost of the building microgrid system, and enhancing the comprehensive operation benefit of the building system.

The virtual energy storage system can better respond to the power system to fill valleys and cut peaks, and reduce operating costs of integrated energy systems. At the same time, it improves new energy digestion capacity to reduce carbon emissions. These provide new ideas for green and low-carbon operation of integrated energy system.

Data availability statement

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

Author contributions

GL and YJ conceived of and designed the study. YZ and YN translated the articles and prepared the tables. JZ constructed and solved the model. JC and YN wrote the first draft of the manuscript. WW drew the microgrid system diagrams. All authors contributed to the revision of the manuscript and read and approved the submitted version.

Funding

This work is supported by the Science and Technology Project of State Grid Corporation of China (Grant No. 5100-202155289A-0-0-00) "Research on implementation path of new-type power system with new energy as the main body". The funder was not involved in the study design, collection, analysis, interpretation of data, the writing of this article, or the decision to submit it for publication.

Acknowledgments

The authors would like to thank the sponsorship of Science and Technology Project of State Grid Corporation of China.

Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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10.3389/fenrg.2022.1053498

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