



Chap.4. Elastic Lidar Systems

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MEASUREMENTS:

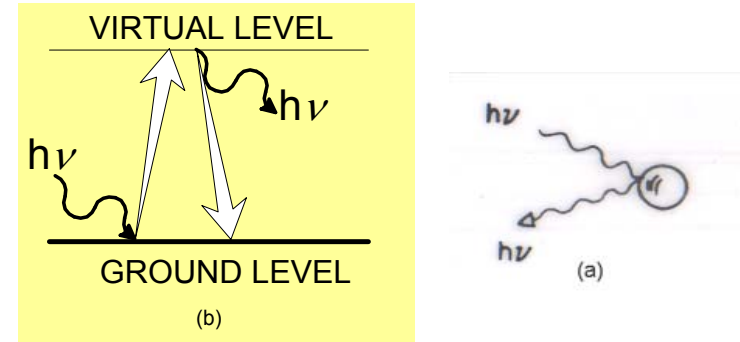
- Direct:
Aerosol/molecular composed intensity returns
- Indirect:
(Usually requires calibrating conditions/hypotheses)

Optical parameters, pollution concentration and flux rate, wind

LASER TYPES:

- Ruby ($\lambda = 694.3 \text{ nm}, 347.2 \text{ nm}$)
- Nd:YAG ($\lambda = 1064, 532 \text{ nm}, 355 \text{ nm}$)
- Excimer ($\lambda \sim 350 \text{ nm}$)

ELASTIC INTERACTION



Types of interaction:

- 1) *Rayleigh scattering*
(molecules, $r \ll \lambda$)
- 2) *Mie scattering*
(aerosols, $r \approx \lambda$)

Types of elastic lidar:

- 1) *Backscatter lidar*
- 2) *Doppler lidar*

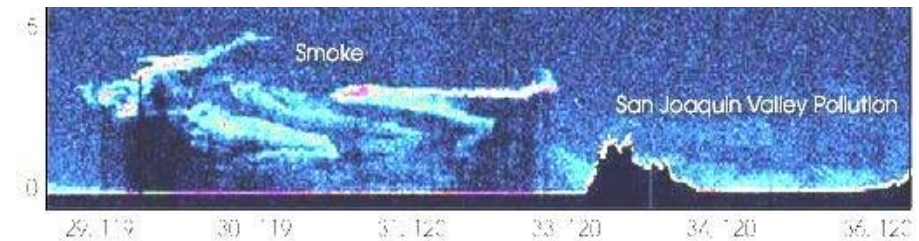
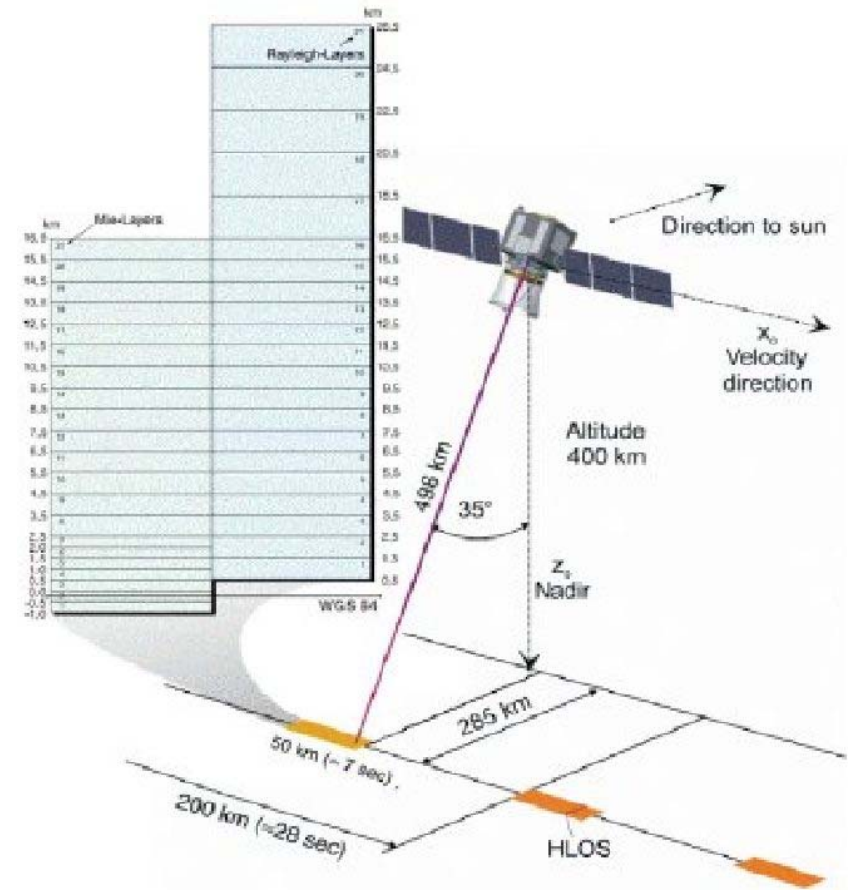
APPLICATIONS

ENVIRONMENTAL

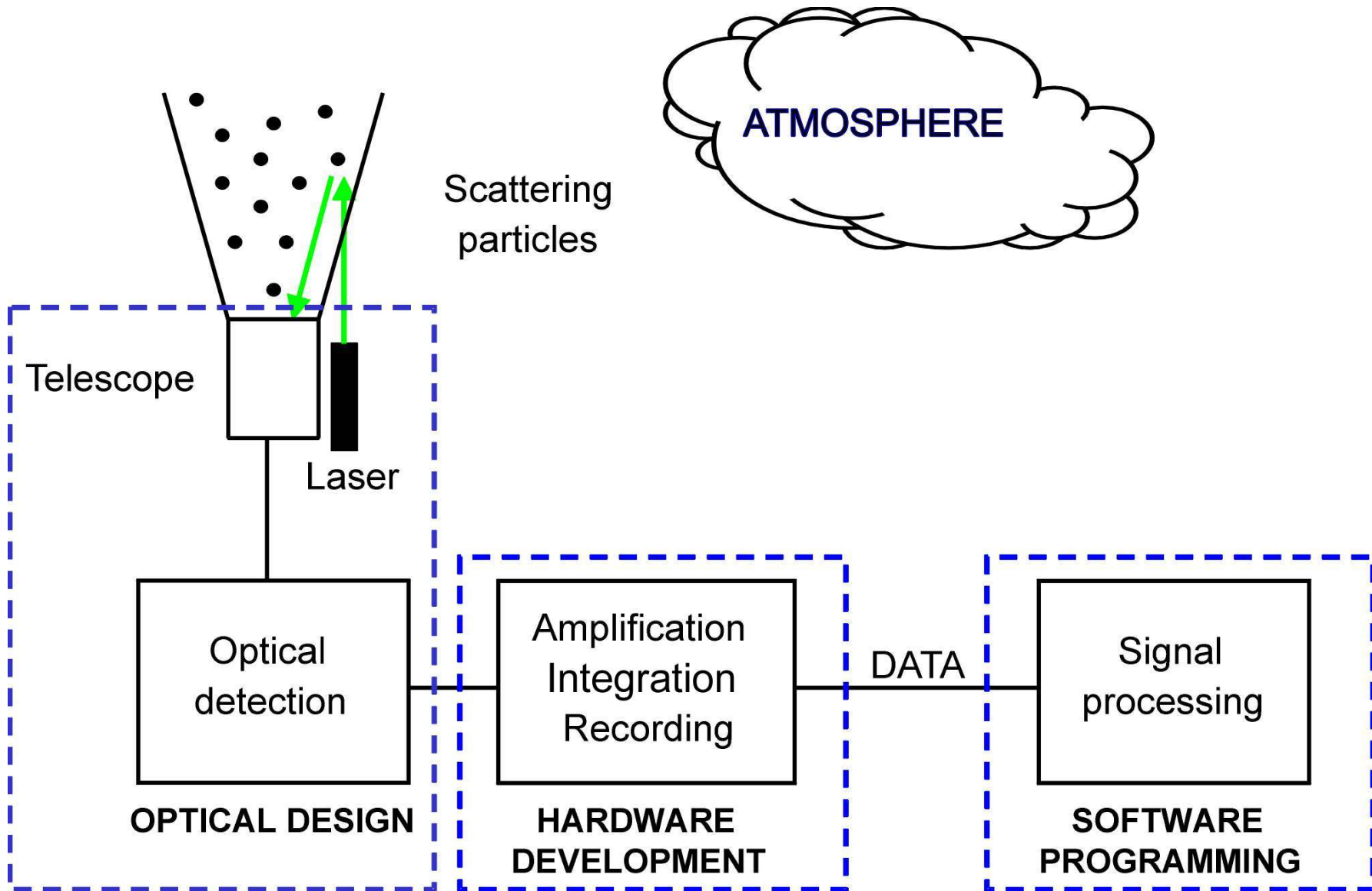
- *Pollution monitoring (source strength and location), Fires*
- *Transport models*
 - Air-quality *regulations*
 - Air-mass fluxes
- *Aerosols role*
 - Earth-atmosphere radiative budget
 - Photochemical effects
 - Air-mass tracers (e.g. wind tracers)

METEOROLOGICAL AND FSO COMMUNICATIONS

- *PBL (Planetary Boundary Layer)*
- *Cloud extent and monitoring*
- *Estimation of atmospheric attenuation (dB/km)*



ARCHITECTURE (I)



RECEIVING OPTICAL SYSTEM

- *Telescope*
 - “optical antenna”
 - effective area, A_r

$$FOV = \frac{r_d}{f} \quad [rad]$$

- *Inteference filter*
 - limits background power

$$P_{back} = L_b(\lambda) A_r d\Omega d\lambda$$

- *O/E converter*
 - Photodiode, PMT
 - Conditioning chain

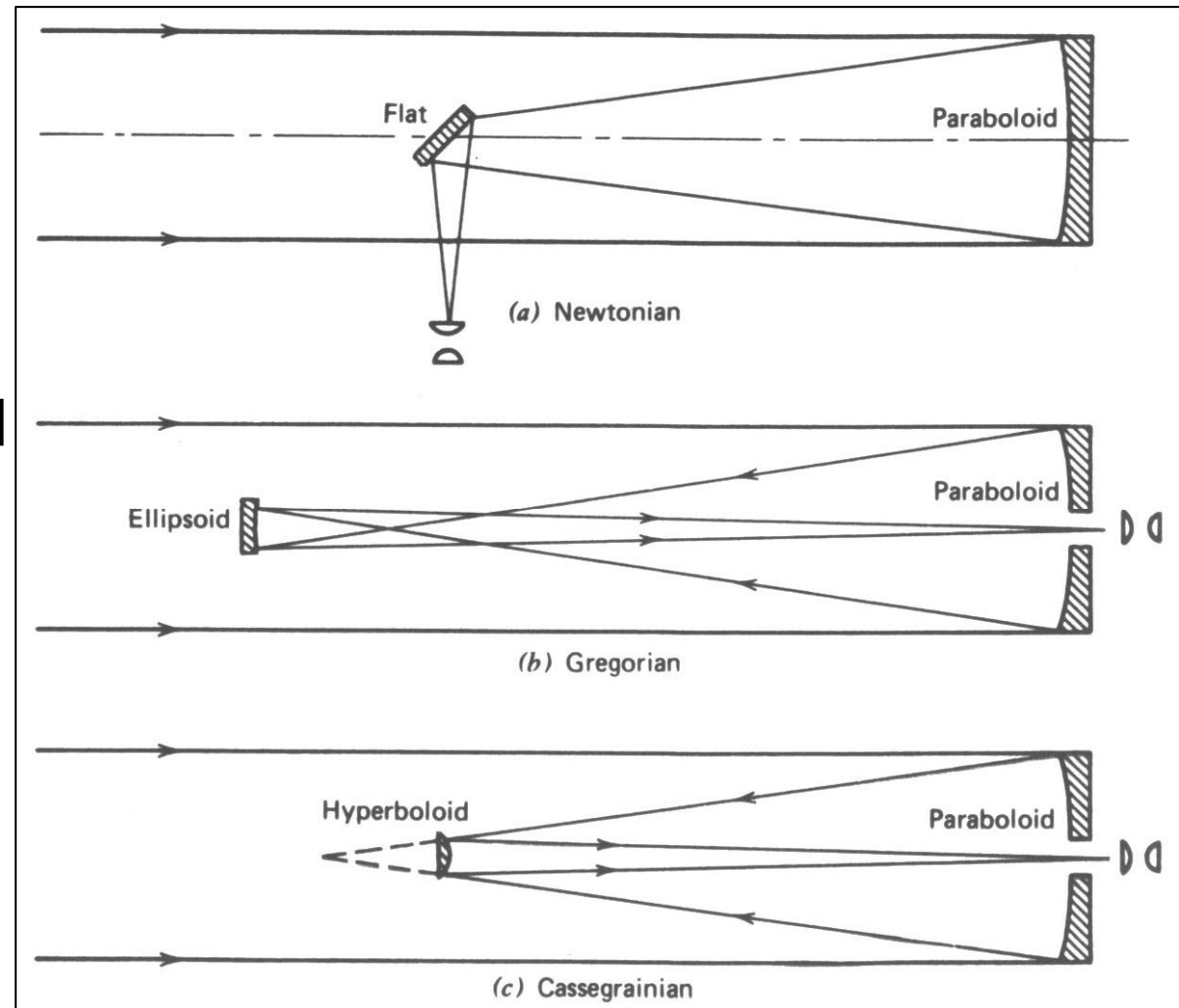
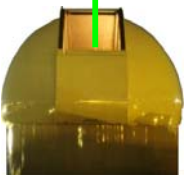
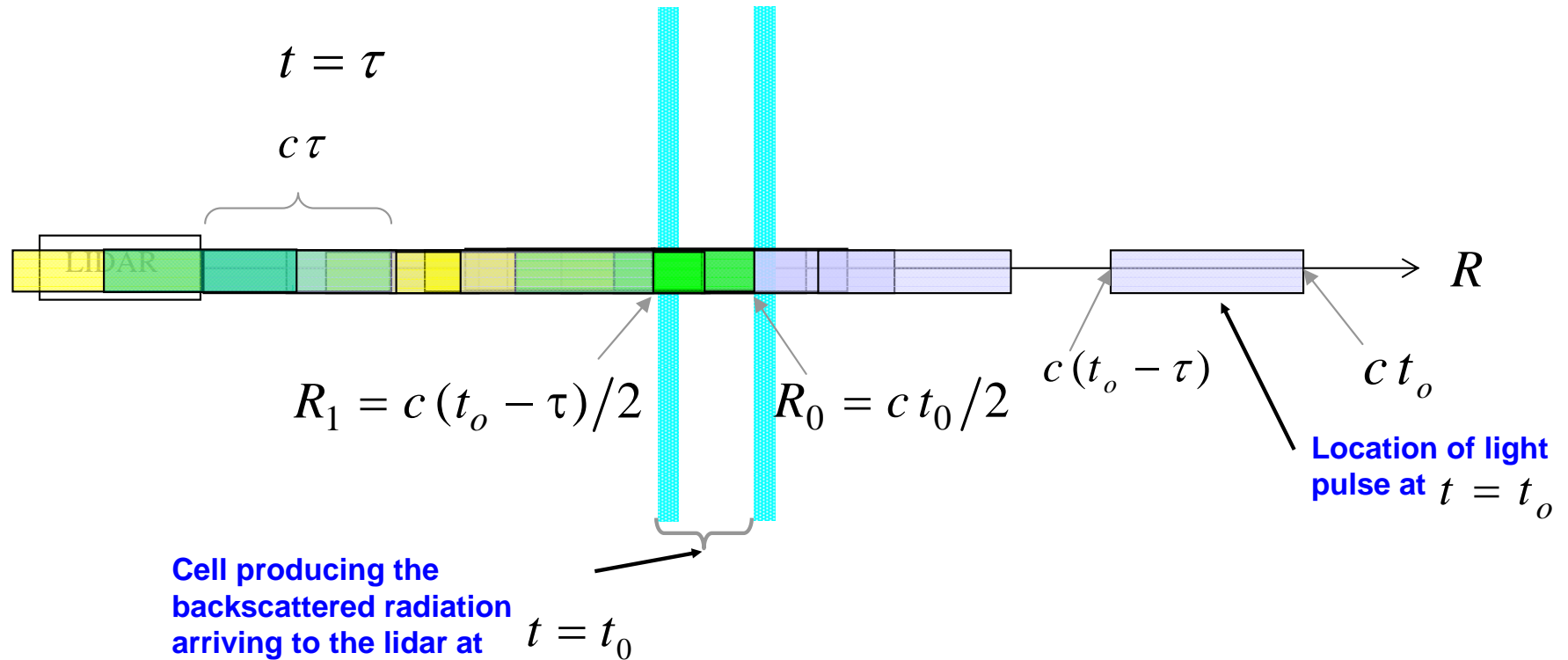


Fig. SOURCE: Measures (1992); R.M. Measures, "Laser Remote Sensing. Fundamentals and Applications". John Wiley & Sons, 1984. (Reprint de 1992, Krieger Publishing Company).



SPATIAL RESOLUTION (I)

INTERACION OF A LIGHT PULSE WITH THE ATMOSPHERE

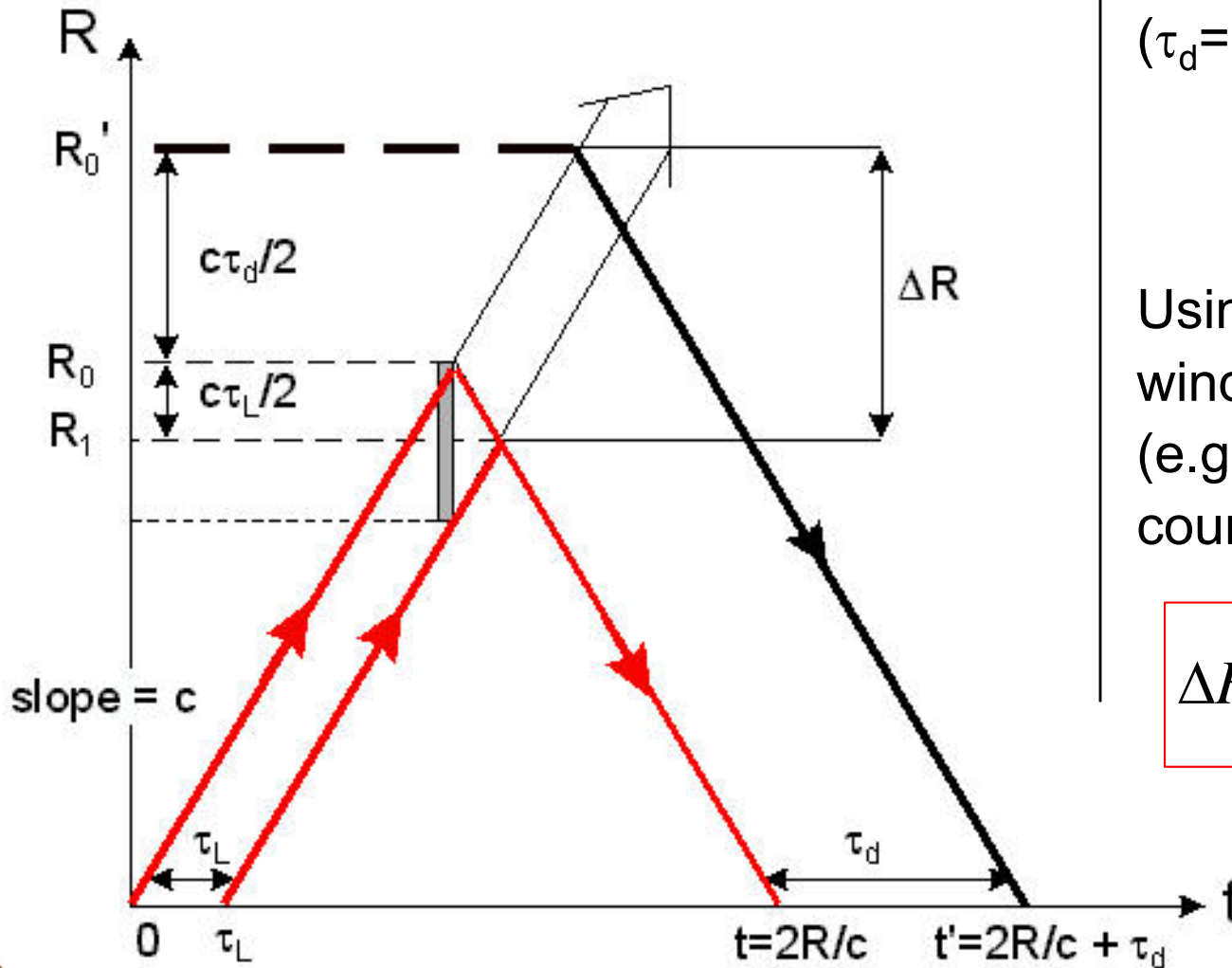


- The **max range** from which energy is received at time t is R_0 .
- At the same time t , additional energy is received from ranges illuminated by portions of the pulse transmitted after the leading edge, the **min. range** from which energy is received is R_1 .

SPATIAL RESOLUTION (II)

SPACE-TIME DIAGRAM

(rectangular-shaped laser pulse, τ_L)

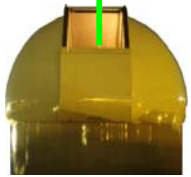


Using analog recording ($\tau_d=0$),

$$\Delta R_a = \frac{c\tau_L}{2}$$

Using a **time detection** window of length $\tau_d=1/f_s$ (e.g., A/D sampling, photon counting),

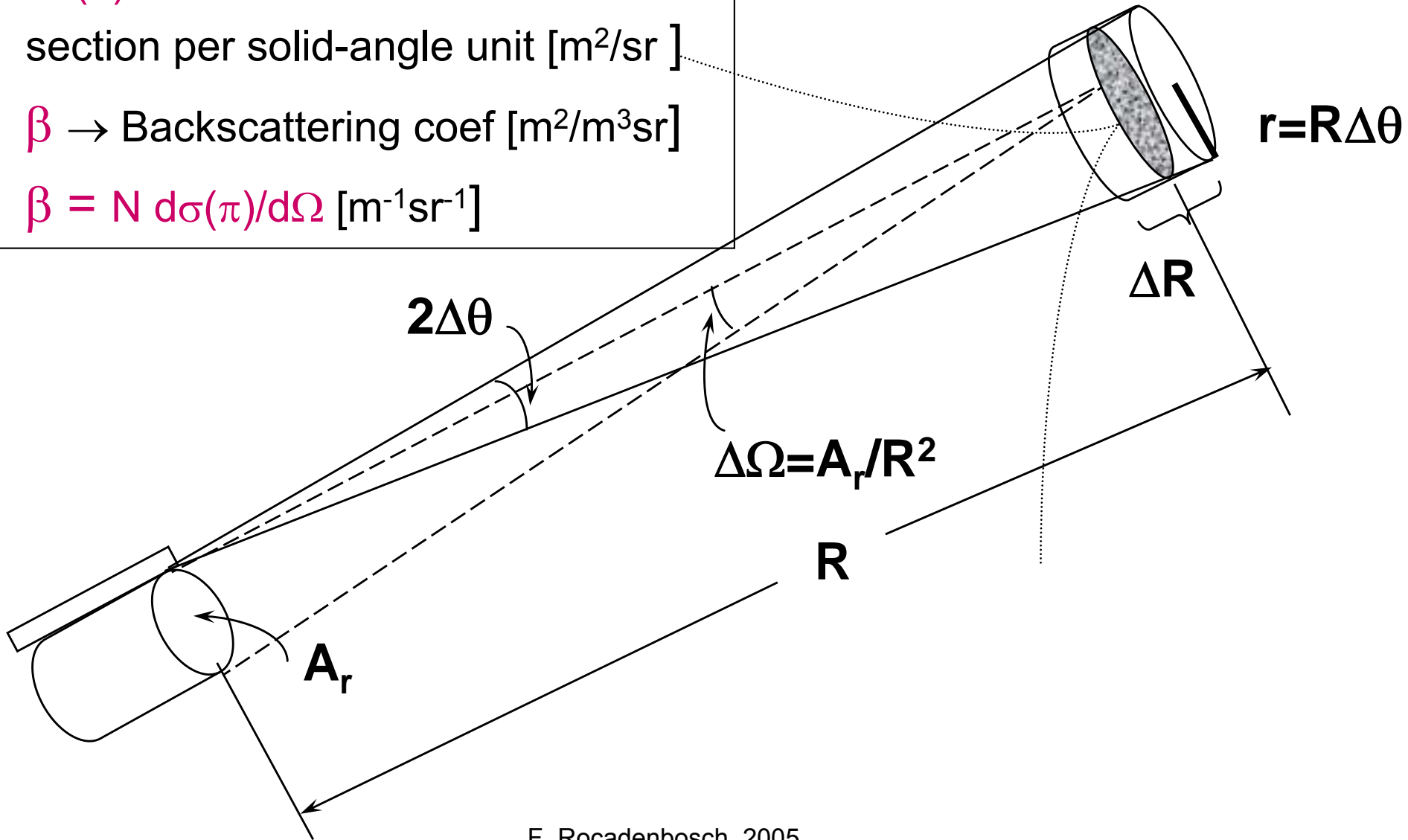
$$\Delta R = \frac{c(\tau_L + \tau_d)}{2} \approx \frac{c\tau_d}{2}$$



THE (ELASTIC) LIDAR EQUATION (I)

N → Particle concentration [part/m³]
 $d\sigma(\pi)/d\Omega$ → Backscatter cross-section per solid-angle unit [m²/sr]
 β → Backscattering coef [m²/m³sr]
 $\beta = N d\sigma(\pi)/d\Omega$ [m⁻¹sr⁻¹]

WITHIN THE SCATTERING VOLUME:



THE (ELASTIC) LIDAR EQUATION (II)

BASIC INTERVENING MAGNITUDES

1) Laser emitted power per pulse (τ_L), P_0 [W] $P_0 = \frac{E}{\tau_L}$

2) Incident power density on the atmospheric resolution cell, E_{in} [W/m²]

$$E_{in}(R) = \frac{P_0}{\pi r^2} \exp\left[-\int_0^R \alpha(u) du\right], \quad r = R\Delta\theta$$

3) Cell-backscattered power per solid-angle unit, K_{sca} [W/sr]

$$K_{sca}(R) = \beta(R)E_{in}(R)V \quad \text{with} \quad \begin{cases} V = \pi r^2 \Delta R \\ \Delta R = c\tau_L/2 \end{cases}$$

4) Backscattered power collected by the telescope, $P(R)$ [W]

$$P(R) = K_{sca}(R)\Delta\Omega \exp\left[-\int_0^R \alpha(x) dx\right], \quad \Delta\Omega = \frac{A_r}{R^2}$$

5) Finally,

$$P(R) = \frac{E \frac{c}{2} A_r}{R^2} \beta(R) \exp\left[-2\int_0^R \alpha(u) du\right]$$

THE (ELASTIC) LIDAR EQUATION (III)

Elastic LIDAR Equation (simple scattering)

$$P(\lambda, R) = \frac{K}{R^2} \beta(\lambda, R) \exp\left[-2 \int_0^R \alpha(\lambda, r) dr\right] \xi(R)$$

where:

$\alpha(\lambda, R)$ atmospheric optical extinction coef. [m^{-1}]

$\beta(\lambda, R)$ atmospheric optical backscatter coef. [$\text{m}^{-1}\text{sr}^{-1}$]

– where
$$\beta(\lambda, R) = \bar{N}(R) \frac{d\bar{\sigma}(\pi)}{d\Omega},$$

– N is the average density of aerosols + molecules [$\text{m}^2/\text{m}^3\text{sr}$]

$\xi(R)$ overlap factor [], $0 \leq \xi(R) \leq 1$

$P(R)$ optical return power [W]

K system constant [W m^3],
$$K = \frac{Ec}{2} A_r$$

where:

E (peak) energy [J]

A_r effective telescope area [m^2]

THE LIDAR EQUATION (IV)

ATMOSPHERIC OPTICAL COEFFICIENTS

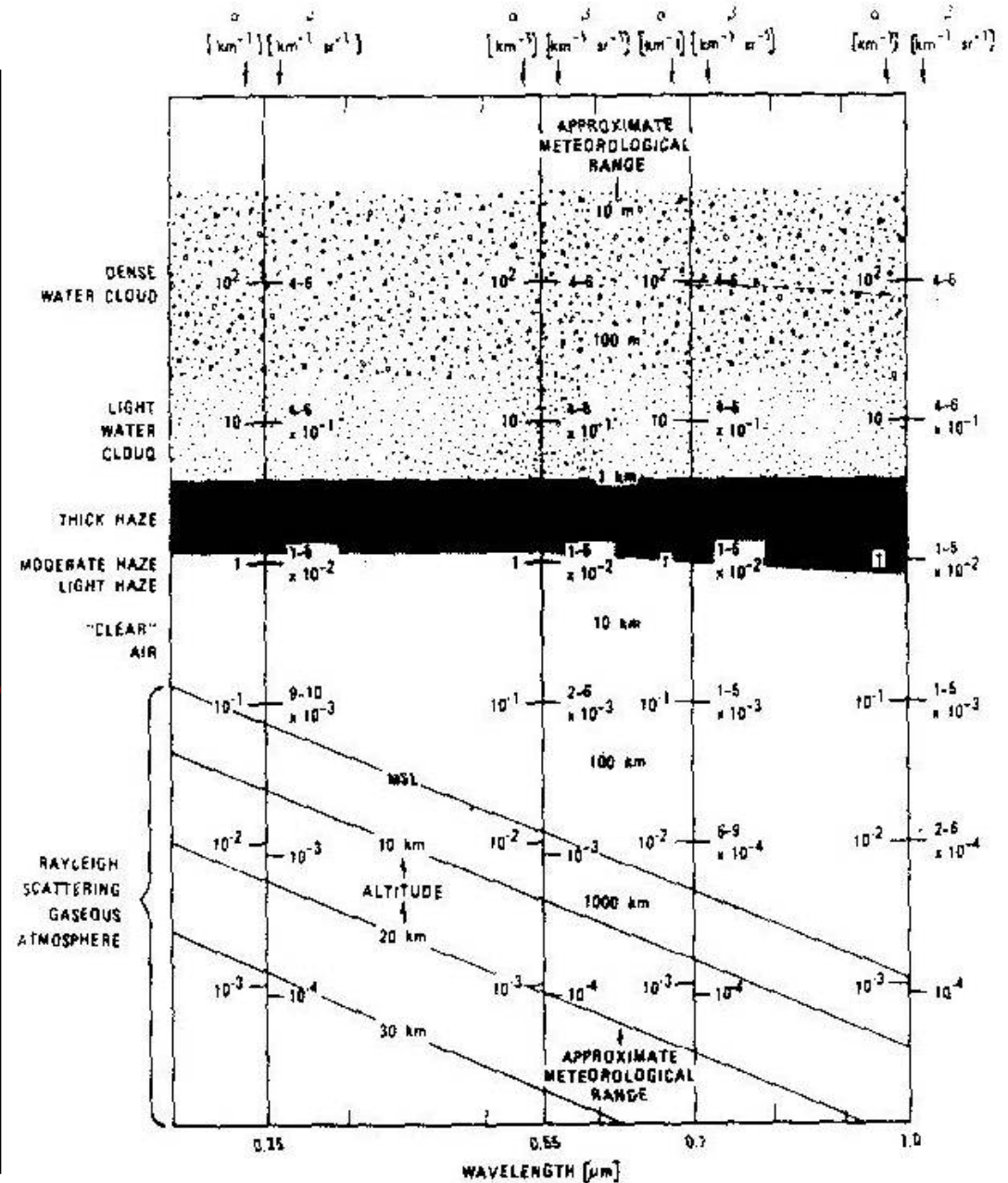
SOURCE: Measures (1992).

Concerning the lidar Eq., note that:

$$\alpha_\lambda(R) = \alpha_\lambda^{aer}(R) + \alpha_\lambda^{mol}(R) + \alpha_\lambda^{abs}(R) \approx 0$$

$$\beta_\lambda(R) = \beta_\lambda^{aer}(R) + \beta_\lambda^{mol}(R)$$

Fig. SOURCE: R.T.H. Collis and P.B. Russell, "Lidar Measurement of Particles and Gases by Elastic Backscattering and Differential Absorption," Chap.4 in *Laser Monitoring of the Atmosphere*, E.D. Hinkley, Ed., (Springer-Verlag, New York, 1976), pp.71-102.



THE LIDAR EQUATION (V)

FURTHER COMMENTS:

1) Assuming a homogeneous atmosphere and ideality system conditions, the lidar equation takes its simplest form:

$$P(R) = \frac{K}{R^2} \underbrace{\beta}_{\text{backscatter}} \underbrace{\exp(-2\alpha R)}_{\text{transmittance}}$$

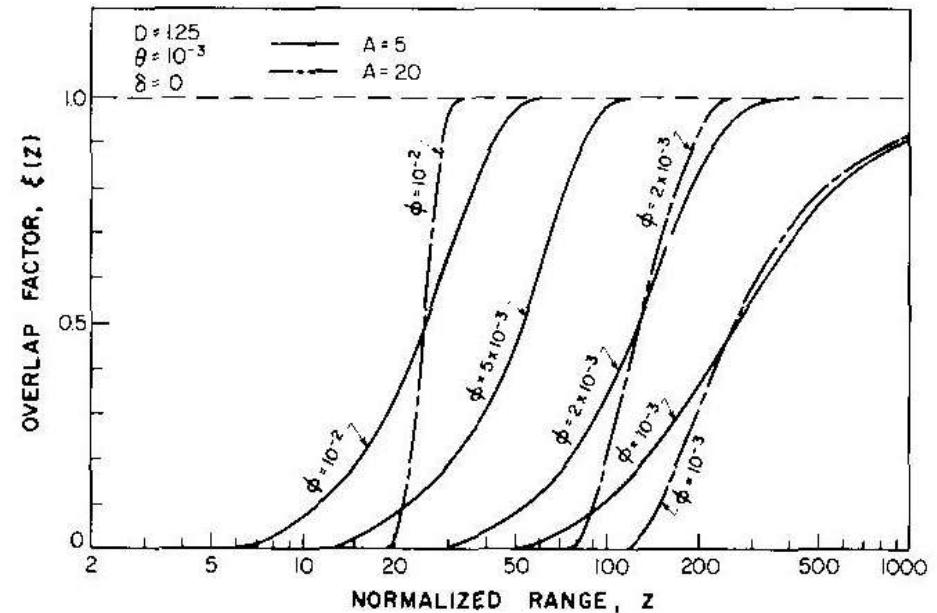
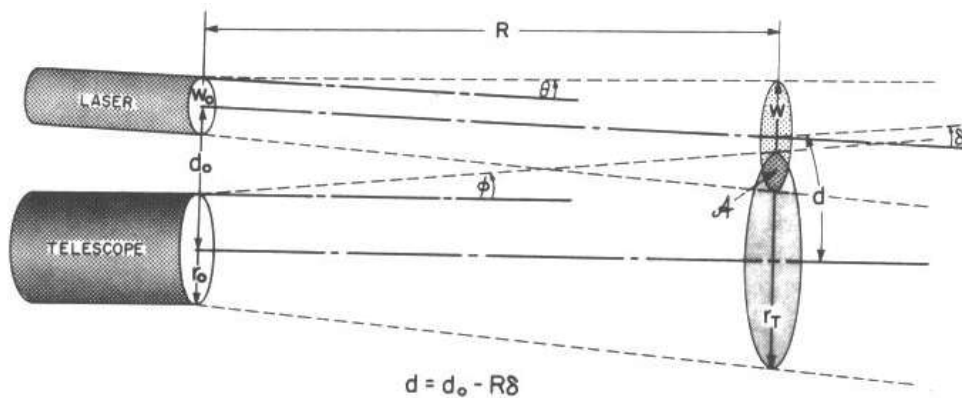
2) Note the *LIDAR optical thickness (COT)* and related *transmissivity!*

$$T(\lambda, R) = \exp[-2COT(R)]; \quad COT(R) = \int_0^R \alpha(\lambda, r) dr$$

THE LIDAR EQUATION (VI)

OPTICAL OVERLAP FACTOR (OVF)

The telescope cannot “read” the full atmospheric cross-section illuminated by the laser beam (i.e., does not lie within its FOV)



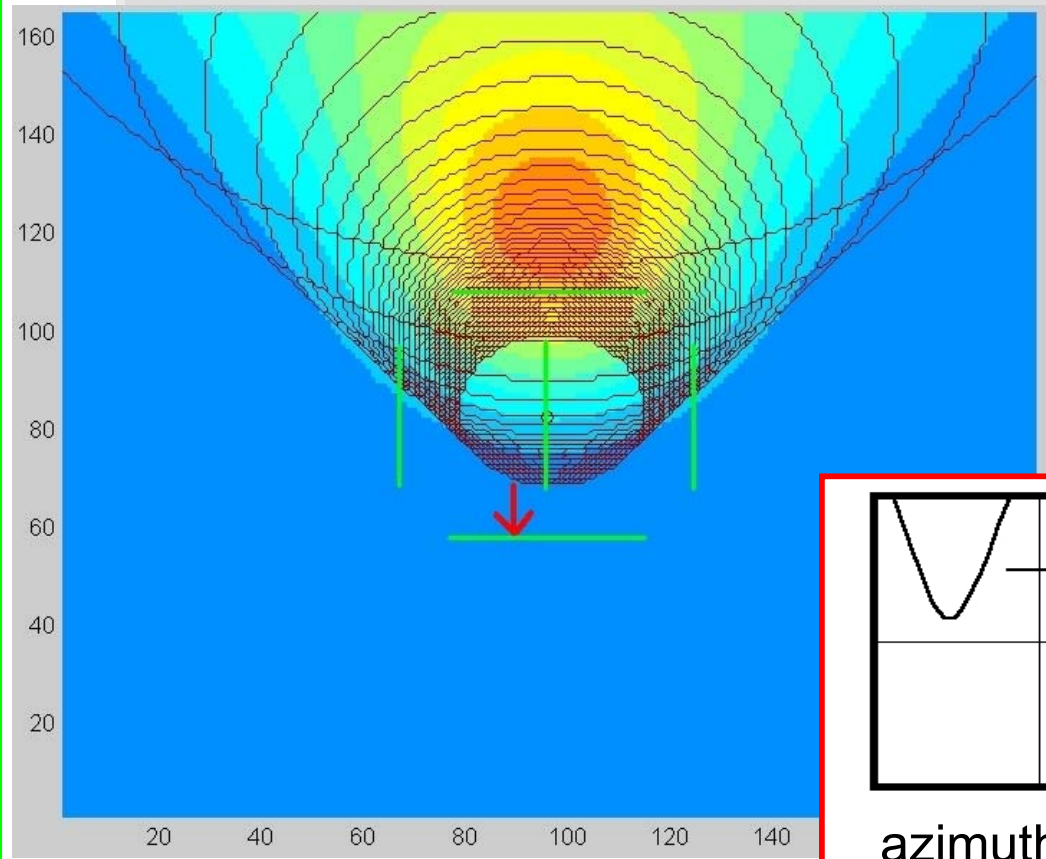
It is a function of many geometrical and optical parameters of both the laser and telescope.

Fig. SOURCE: Measures (1992).



LIDAR (LASER RADAR)

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THE LIDAR EQUATION (VII)

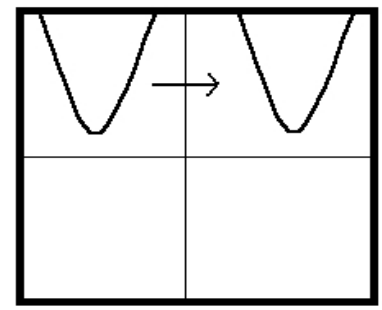
OVF OPTICAL ALIGNMENT

Atmospheric laser foot-print imaged is (telesc. far-field):

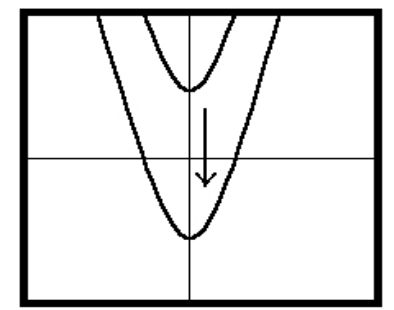
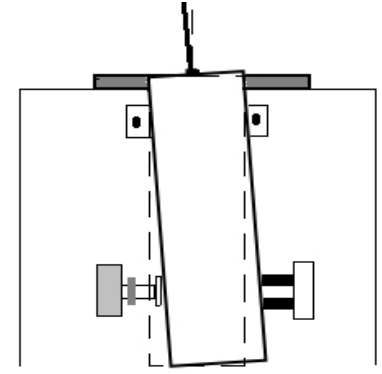
$$y_i = -\frac{f}{R} \left[\pm \sqrt{W_o^2 + \theta^2 R^2} + d_o - \delta R \right]$$

A) $y_i = -\underbrace{f [\pm \theta]}_{\text{size}} - \underbrace{f [\Omega(R) - \delta]}_{\text{y-position}}$

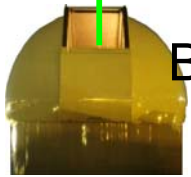
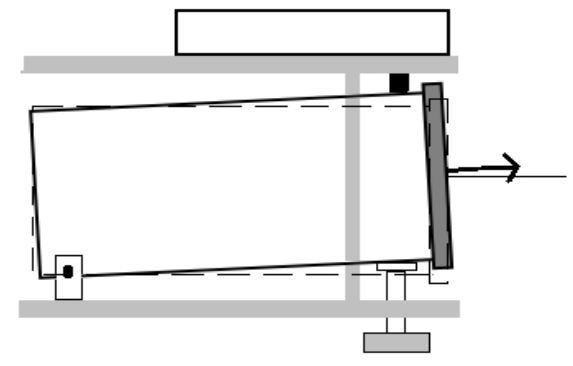
B) $y_i = -\underbrace{\frac{f}{R} [\pm W_o]}_{\text{size}} - \underbrace{f [\Omega(R) - \delta]}_{\text{y-position}}$



azimuth adj.



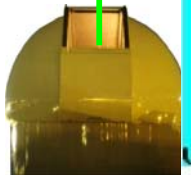
elevation adj.



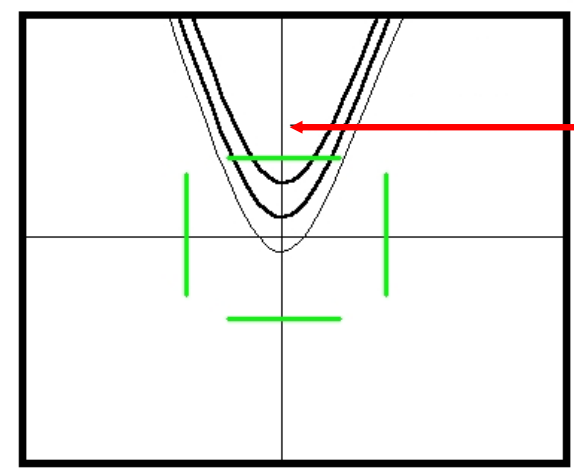
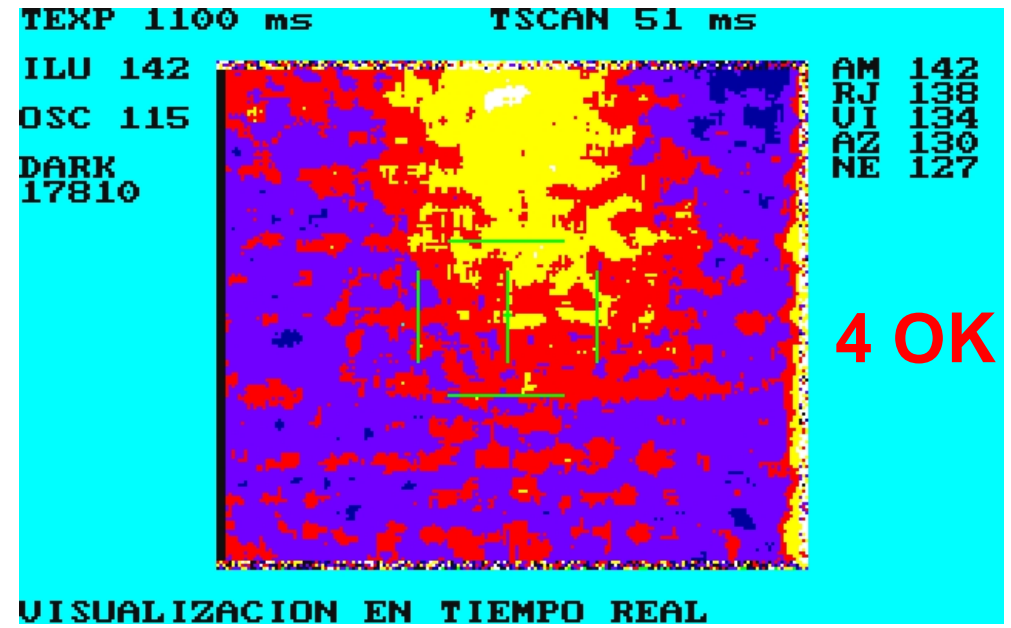
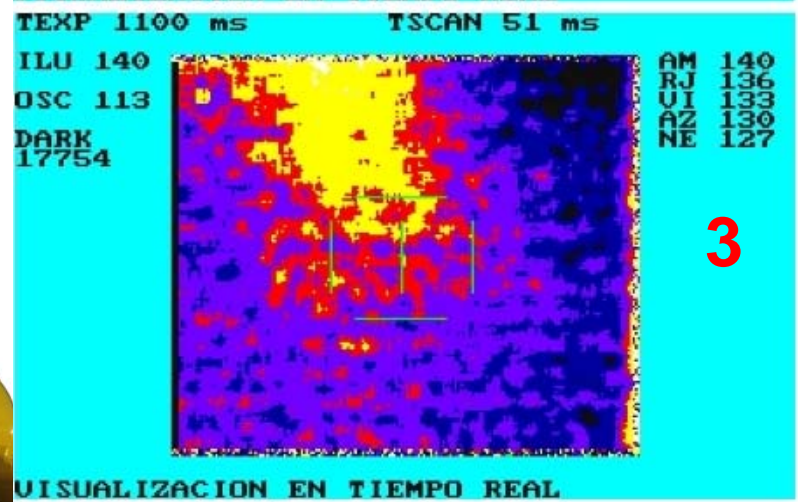
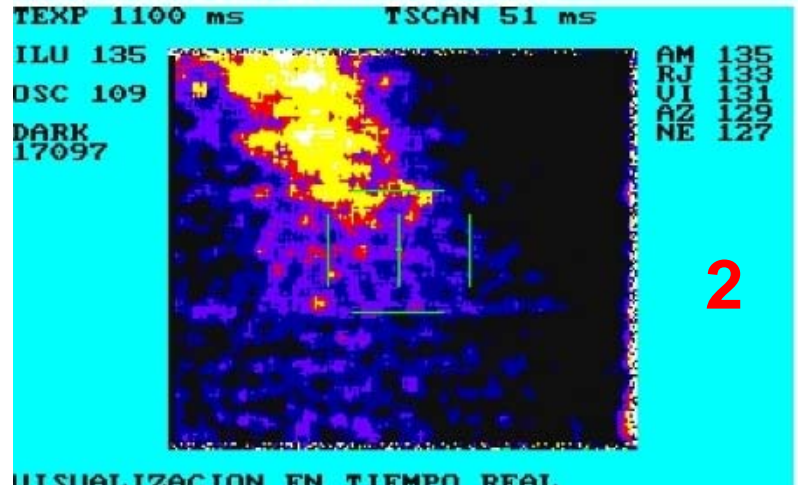
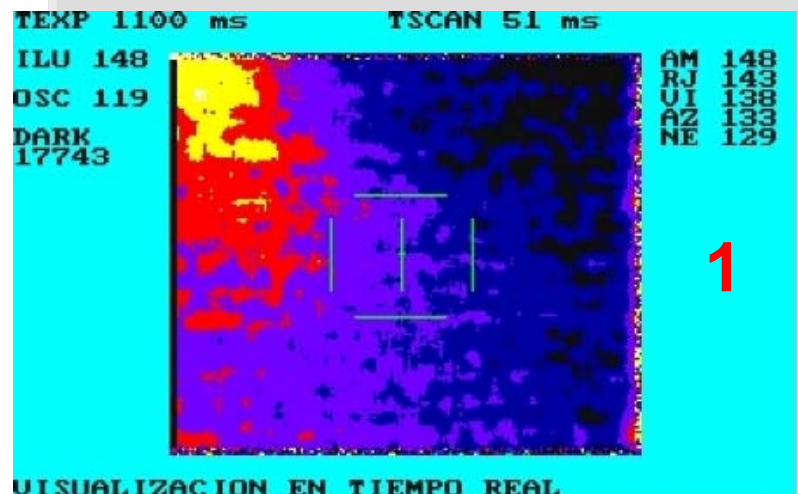


LIDAR (LASER RADAR)

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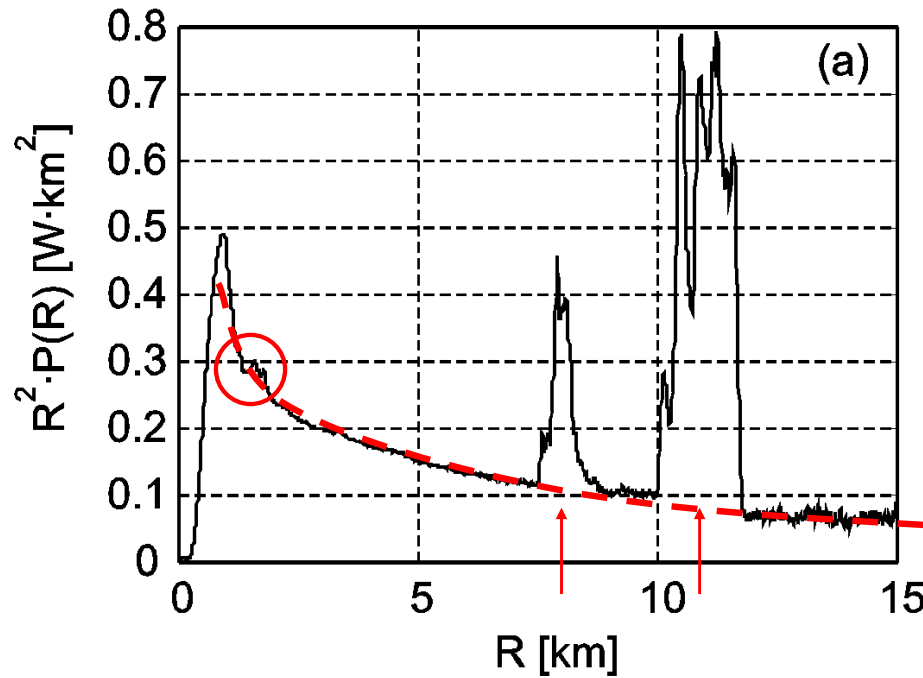


THE LIDAR EQUATION (VIII)



brightest area
REF

THE LIDAR EQ. (IX): BASIC INVERSIONS



RANGE CORRECTION (R^2P):

Backscatter-transmittance plot

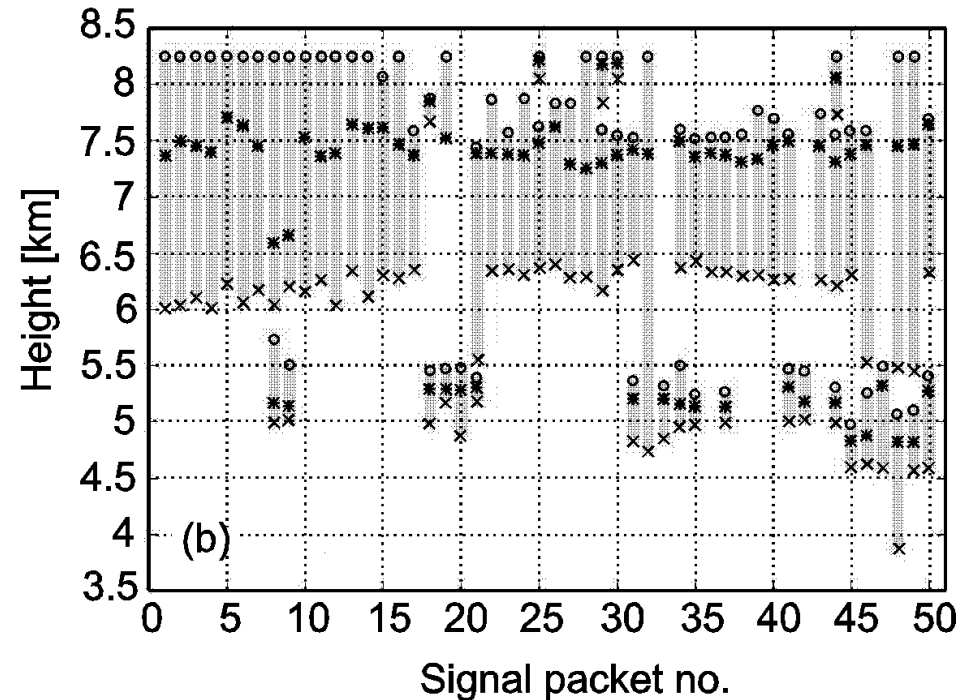
Reveals atmospheric structure

- *Mixing aerosol layer*
- *Cloud structure*

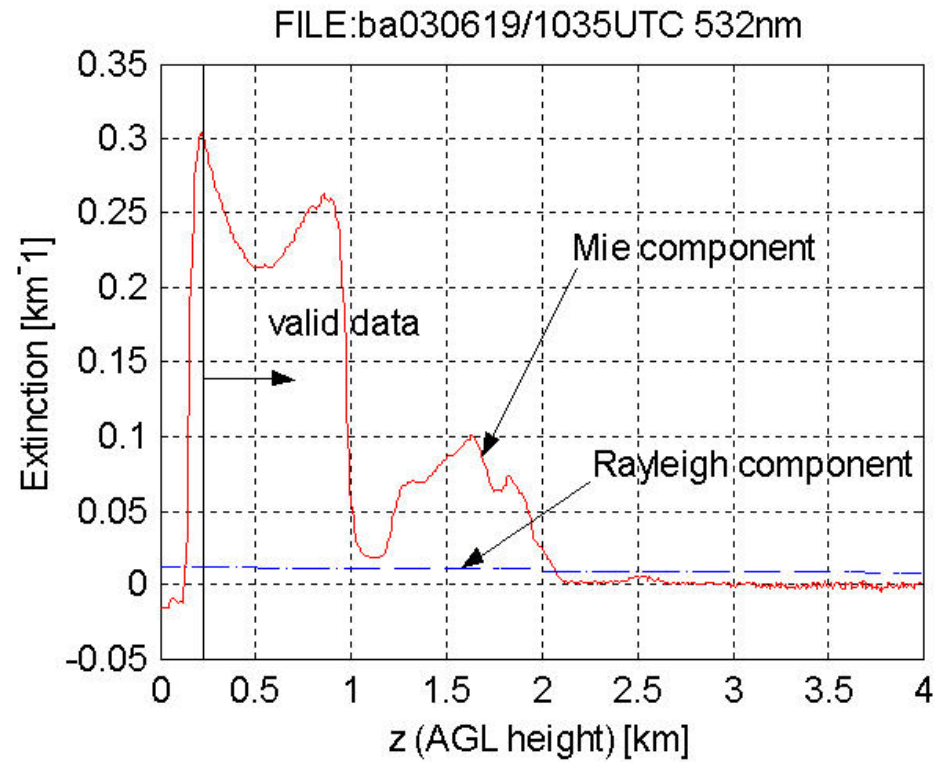
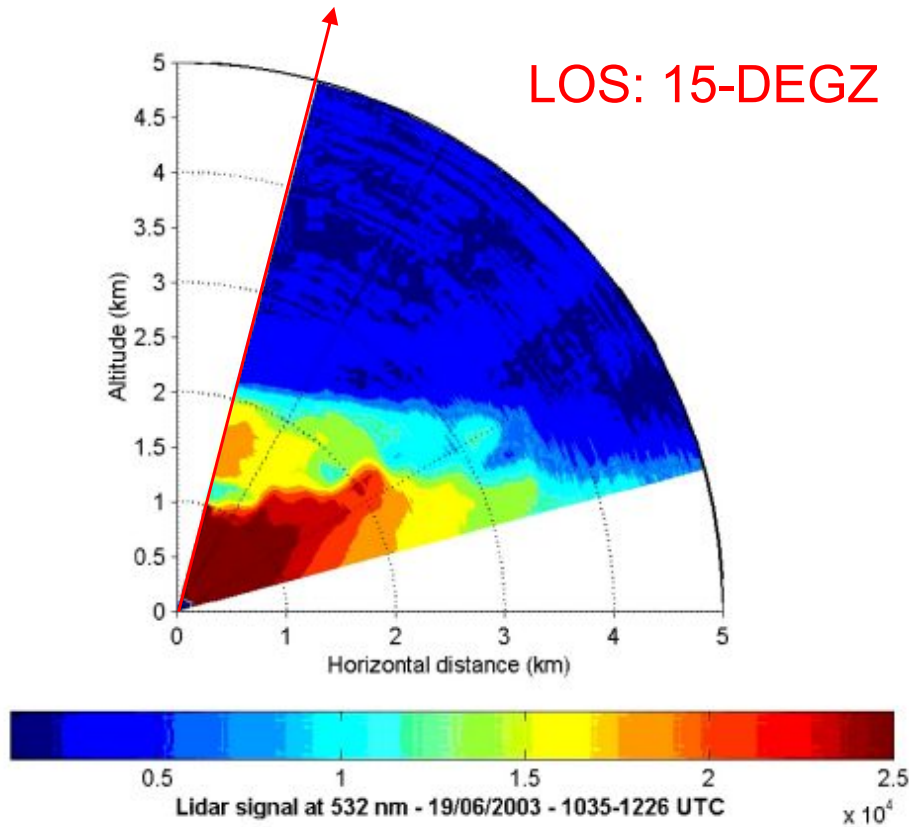
CEILOMETRY:

Cloud-height extent monitoring

- *Cloud base, peak, top*
- *No. of layers*

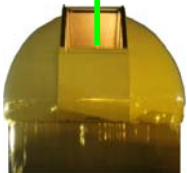


THE LIDAR EQ. (X): BASIC INVERSIONS

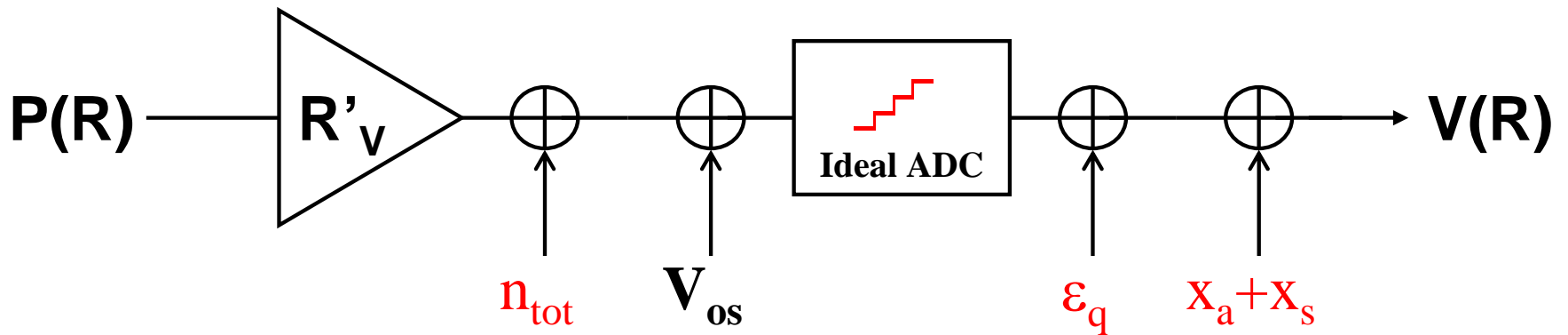


LOS: 15-DEGZ

- For optically “clear” atmospheres, the “range-corrected” (R^2P), “backscatter” and “extinction” representations look very much alike.



SIGNAL CONDITIONING (I): RECEIV. CHAIN



$$V(R) = R'_v P(R) + n_{tot} + V_{os} + \underbrace{U^{fof}(R) + \epsilon^d + X^s(R) + X^e(R)}_{\text{unwanted terms}}$$

- R'_v : Net Voltage **Responsivity** (V/W)
 - V_{os} : Total system offset (user+drift+**background**)
 - n_{tot} : Total noise (photodetection + electronic)
 - ϵ_q : Quantization noise
 - $X_{a,s}$: **A/S**ynchronous interferences
- $$V_{OS} = R'_v P_{Back} + V_{drift} + V_{user} + \sum \frac{dV_{drift}}{dt} \Delta t$$

unwanted terms

Sampling at f_s , detection time $\tau_d = 1/f_s$, so that

$$\Delta R \approx \frac{c\tau_d}{2} = \frac{c}{2f_s}$$

SIGNAL CONDITIONING (II): KEYS

RECEIVER CHAIN

1) Mapping function

$$V(R) = R_i G P(R) + V_{OS}$$

2) Operational settings

a) Map B to $-V_{max}$

$$P(R \rightarrow \infty) = P_{back}$$

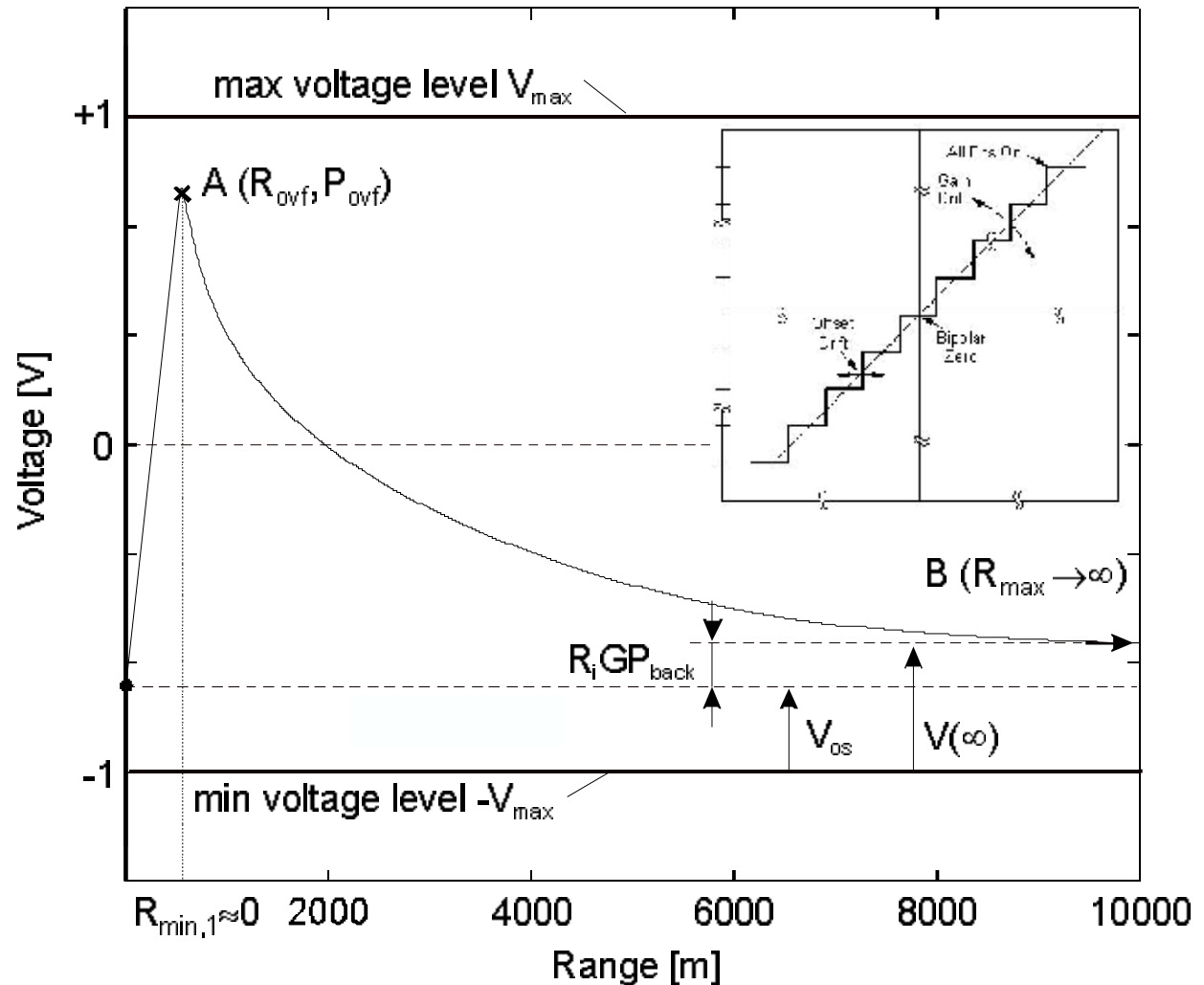
$$V_{OS} = -V_{max} - R_i G P_{back}$$

b) No ADC saturation

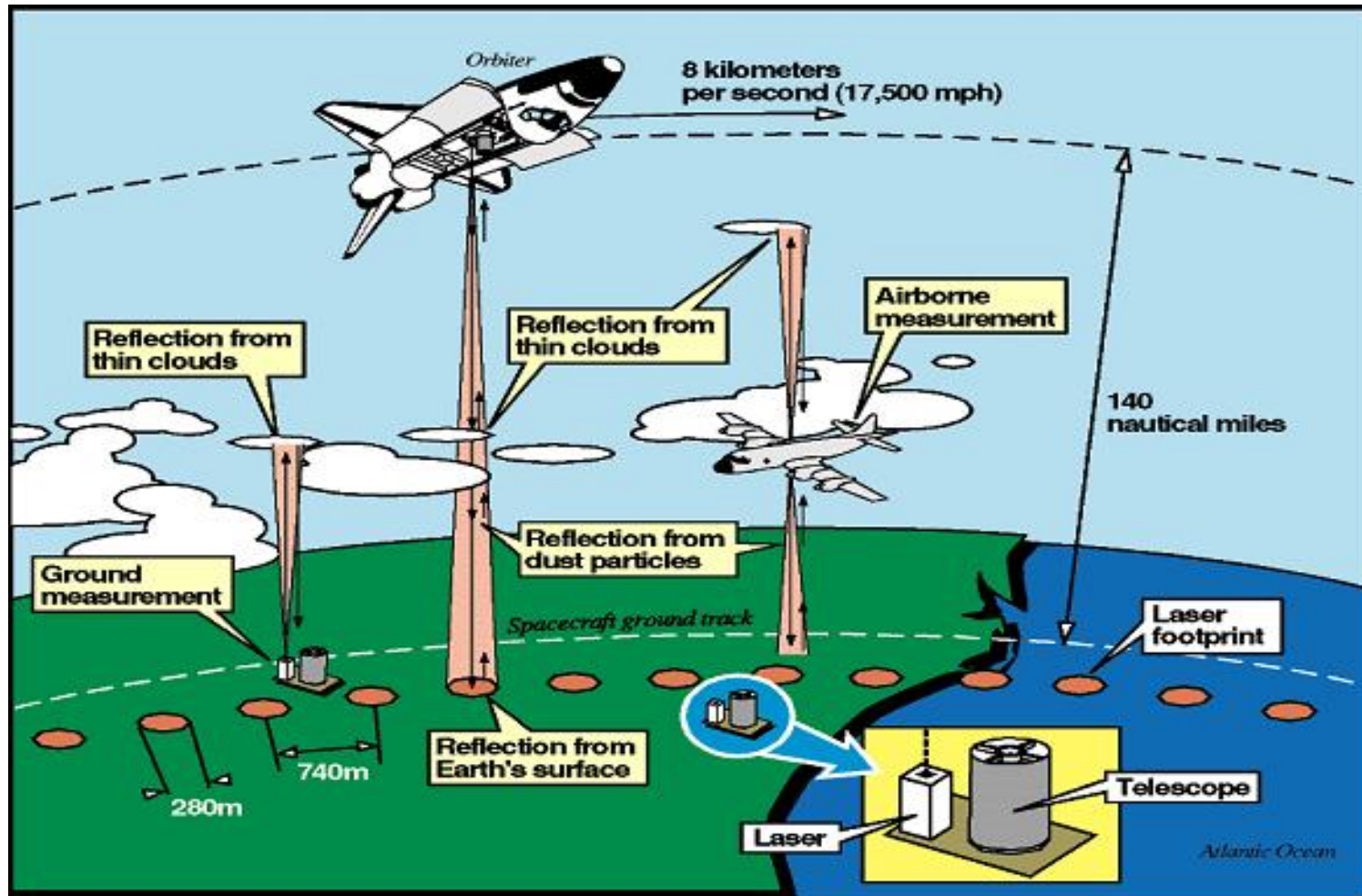
$$G = \frac{V_{max} - V_{OS}}{R_i P_{max}}$$

3) Intensity Display

$$V'(R) = V(R) - V(\infty)$$

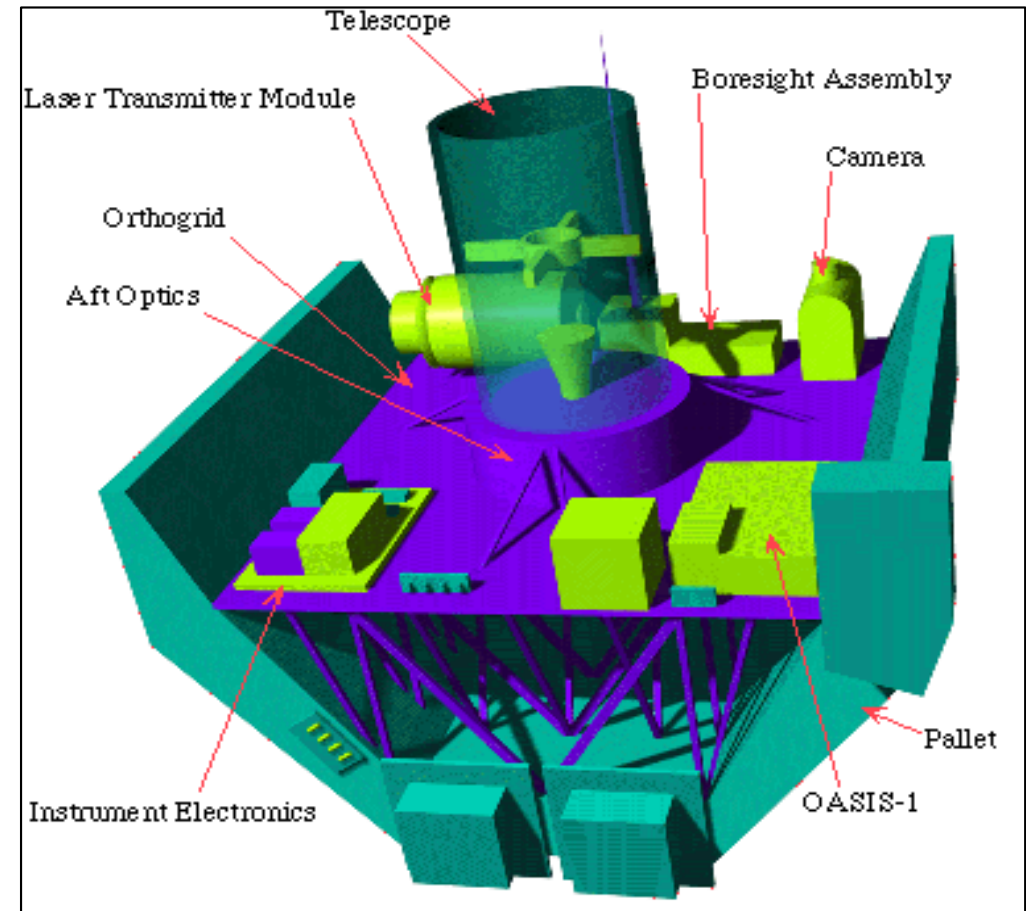
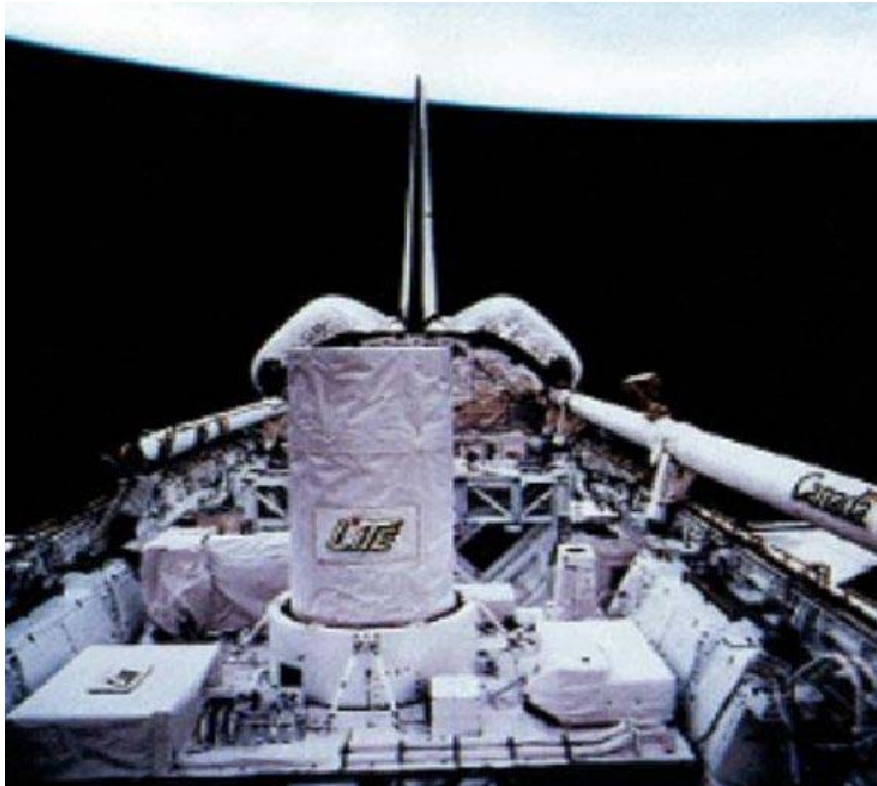


NASA, Lidar In-space Technology Experiment (LITE)



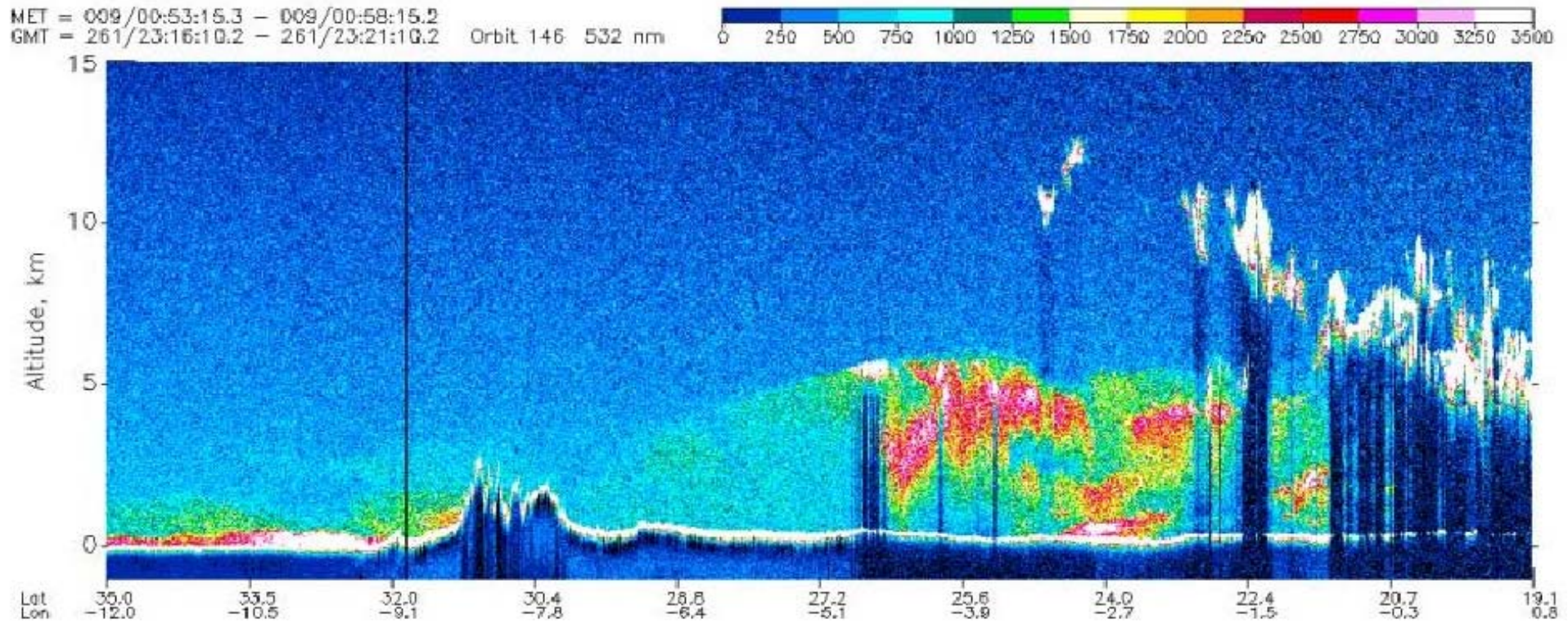
SPECS: Elastic lidar, Nd:YAG (1064, 532, 355 nm), Discovery 1994.
APLIC: Clouds & stratosphere aerosol density, temperature

LITE (Lidar In-space Technology Experiment)



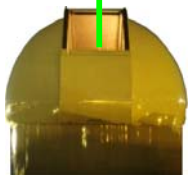
SOURCE:
<http://www-lite.larc.nasa.gov/>

BACKSCATTER LIDAR & RSCH AGENCIES



OTHER PROJECTS (ESA)

- *ATLID: similar to LITE (NASA)*
- *ALADIN: wind lidar space-borne sensor*



CLOUD AND AEROSOL M-LIDAR

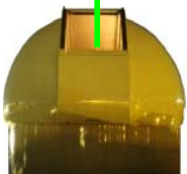
Transmitter	Laser : Nd:YAG, SHG 532 nm
Output wavelength	532 nm
Output energy per pulse	4 μ J
Repetition rate	5 kHz
Pulse duration	< 1 ns
Effective aperture	314 cm ²
Field of view (full angle)	55 μ rad
Filter bandwidth	0.5 nm
Detector	APD
Detection mode	Photon counting
Acquisition time	> 0.8 s
Vertical resolution	15 m
Size (diameter x height)	220 x 1000 mm
Weight	12.5 kg

MAIN FEATURES:

- *Self-alignment of emission and reception axes*
- *Eye-safe*
- *Compact and portable*

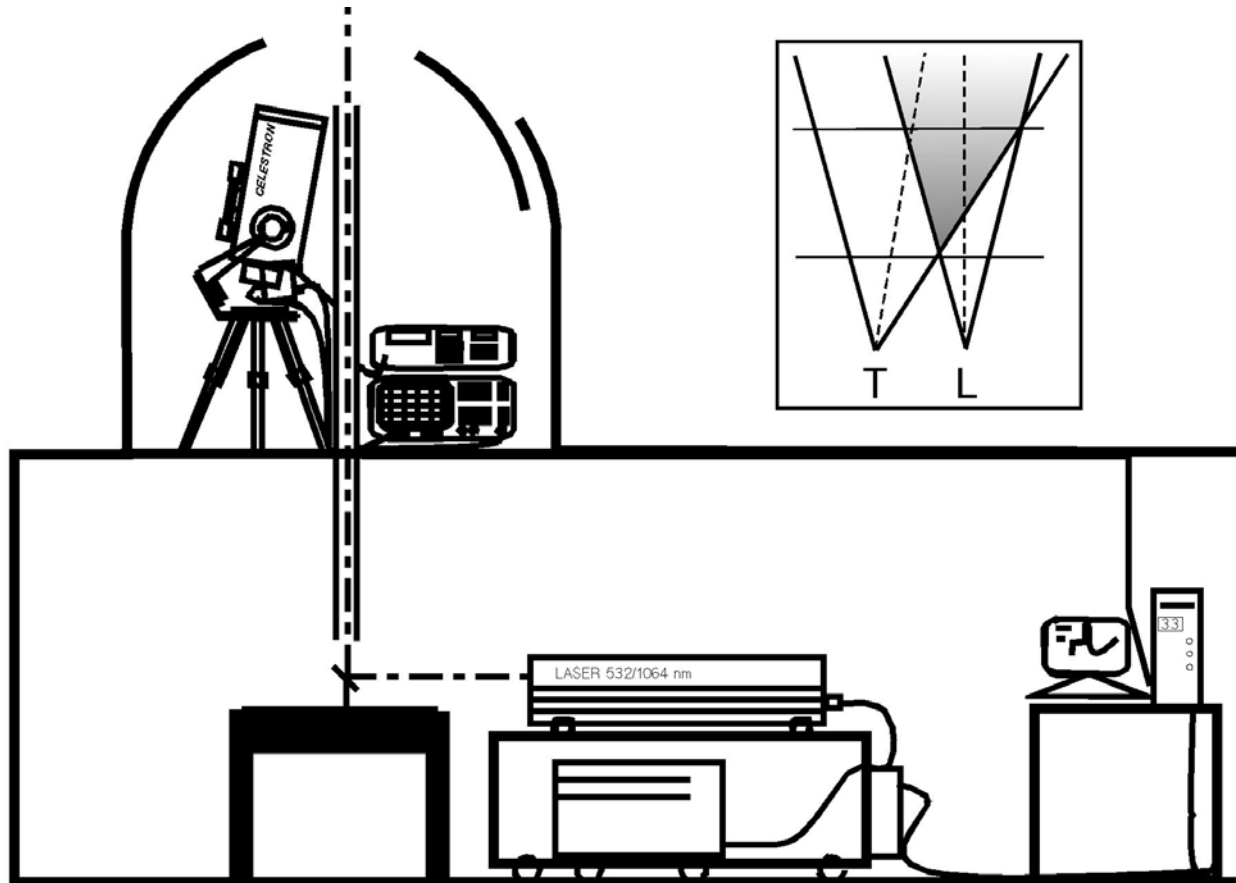


SOURCE: CIMEL Electronique,
<http://www.cimel.fr> (Mod. CE370-2)



EXAMPLES: BACKSCATTER LIDAR - UPC 1996

LASER		RECEIVER		SYSTEM SPECS	
Gain medium	Nd:YAG	Focal length	2 m	Configuration	Vertical biaxial
Energy	0.5 J/532 nm	Aperture \varnothing	20 cm	System NEP	$70 \text{ fW} \cdot \text{Hz}^{-1/2}$
Divergence	0.1 mrad	Detector	APD (EGG C30954)	Min. Det. Power	$< 5 \text{ nW}$
Pulse length	10 ns	Net Responsivity	$6 \times 10^1 - 3 \times 10^6 \text{ V/W}$	Acquisition	20 Msps/12bit
PRF	10 Hz	Bandwidth	10 MHz	Spatial resolution	7.5 m



DISTINCTIVE SPECS:

(as compared to μW RADARS)

$\Delta R = 7.5 \text{ m!}$

$\Delta t = 1 \text{ min}$

LIDAR (LASER RADAR)

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BACKSCATTER LIDAR - UPC 1996

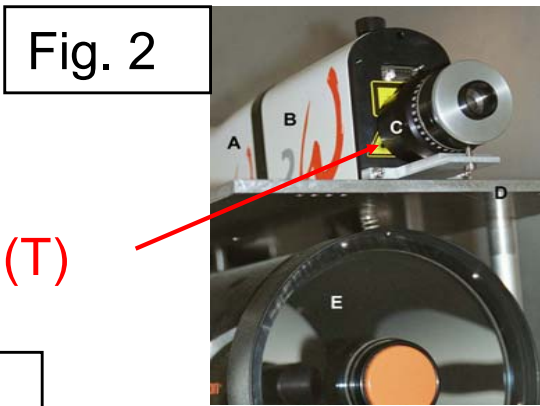
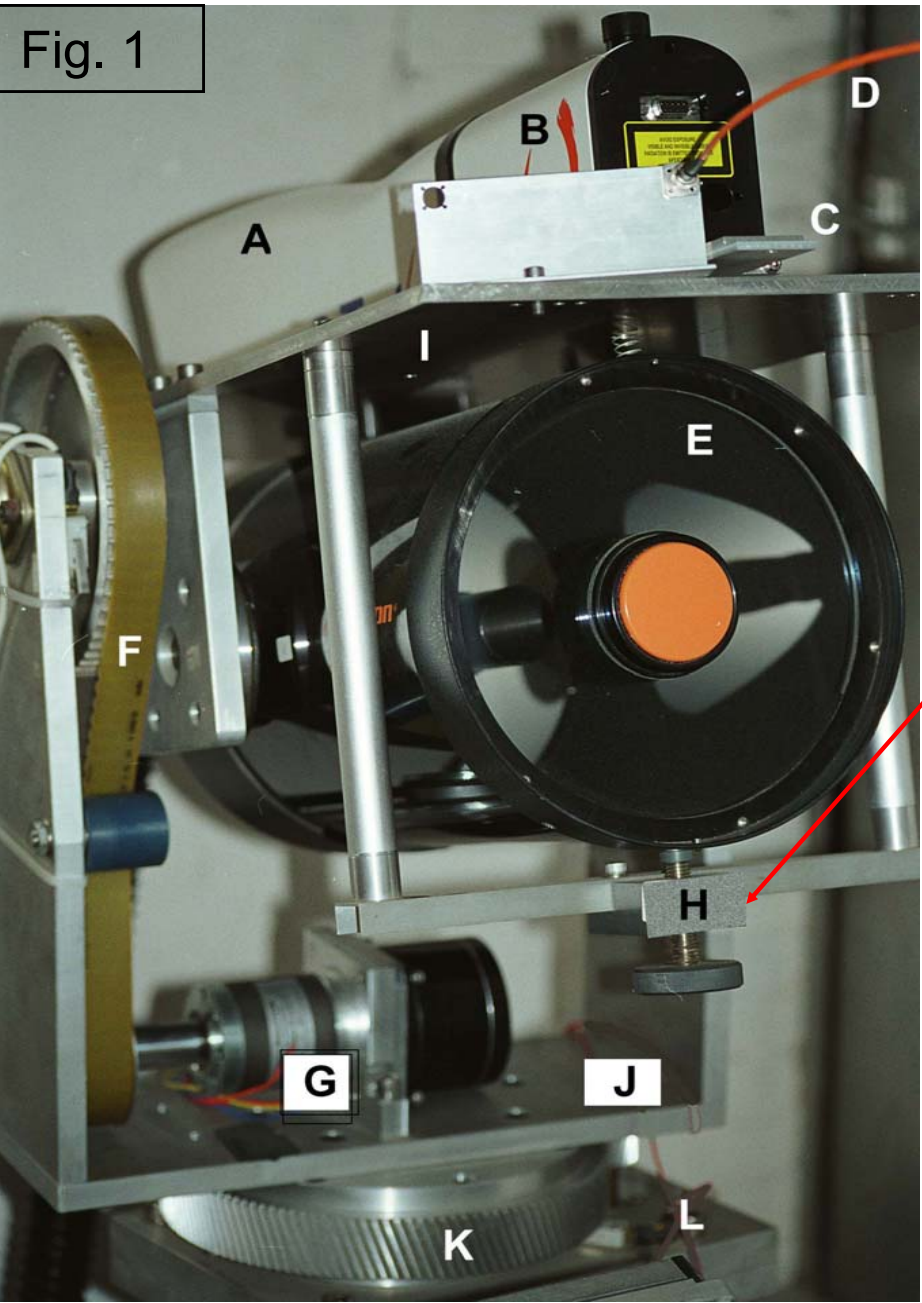
LASER		RECEIVER		SYSTEM SPECS	
Gain medium	Nd:YAG	Focal length	2 m	Configuration	Vertical biaxial
Energy	0.5 J/532 nm	Aperture \varnothing	20 cm	System NEP	70 fW·Hz ^{-1/2}
Divergence	0.1 mrad	Detector	APD (EGG C30954)	Min. Det. Power	< 5 nW
Pulse length	10 ns	Net Responsivity	6×10 ⁻¹ -3×10 ⁶ V/W	Acquisition	20 Msps/12bit
PRF	10 Hz	Bandwidth	10 MHz	Spatial resolution	7.5 m



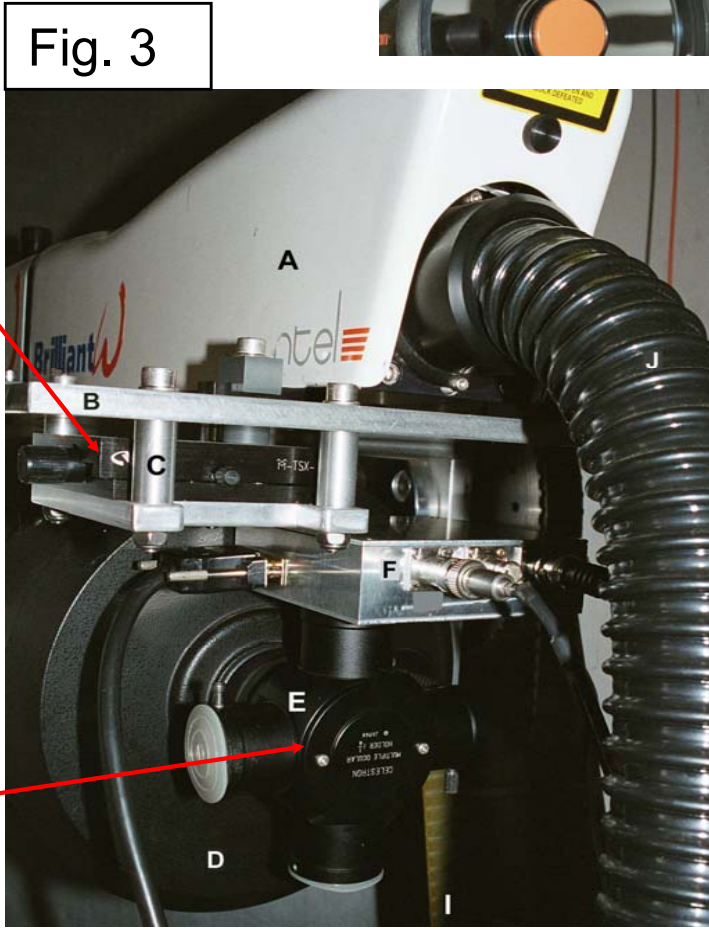
LIDAR (LASER RADAR)

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ADVANCED CONFIGURATIONS: SRL - UPC 2004



Polarim. Subs. (T)



Polarim. Subs. (R)

Alignment



LIDAR (LASER RADAR)

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Lidar 3D MAIN.vi

File Edit Operate Project Windows Help

Offset: $-9.00E-1$
 IP: 1
 PPI: 30

Receiver

Yr: 265.00 M: 46.00
 G. Trans.: 3700 HV: ON
 Gac Level: 1 Gac value: 0.98

Target
 Elevation: 0.00
 Azimut: 0.00

APD: ON Integrating pulse: 14

0 Saving packet

INTEGRATING STATUS

MANUAL MOTORS

LAMPS OFF LASER OFF
 LAMPS ON LASER ON

Second Window Start (m): 0

Total Range: 1200

3 5000 10000 15000 20000 25000 30000 35000 40000 45000 50000

1 [0.4]

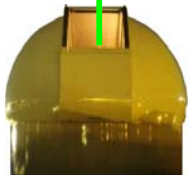
This If sentence will send data to Serial Port 0 if Data

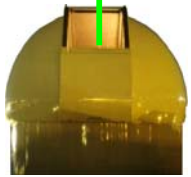
These is the header sent to the Router. It is included the number of bytes of length

These is the header sent to the Router. It is included the number of bytes of length

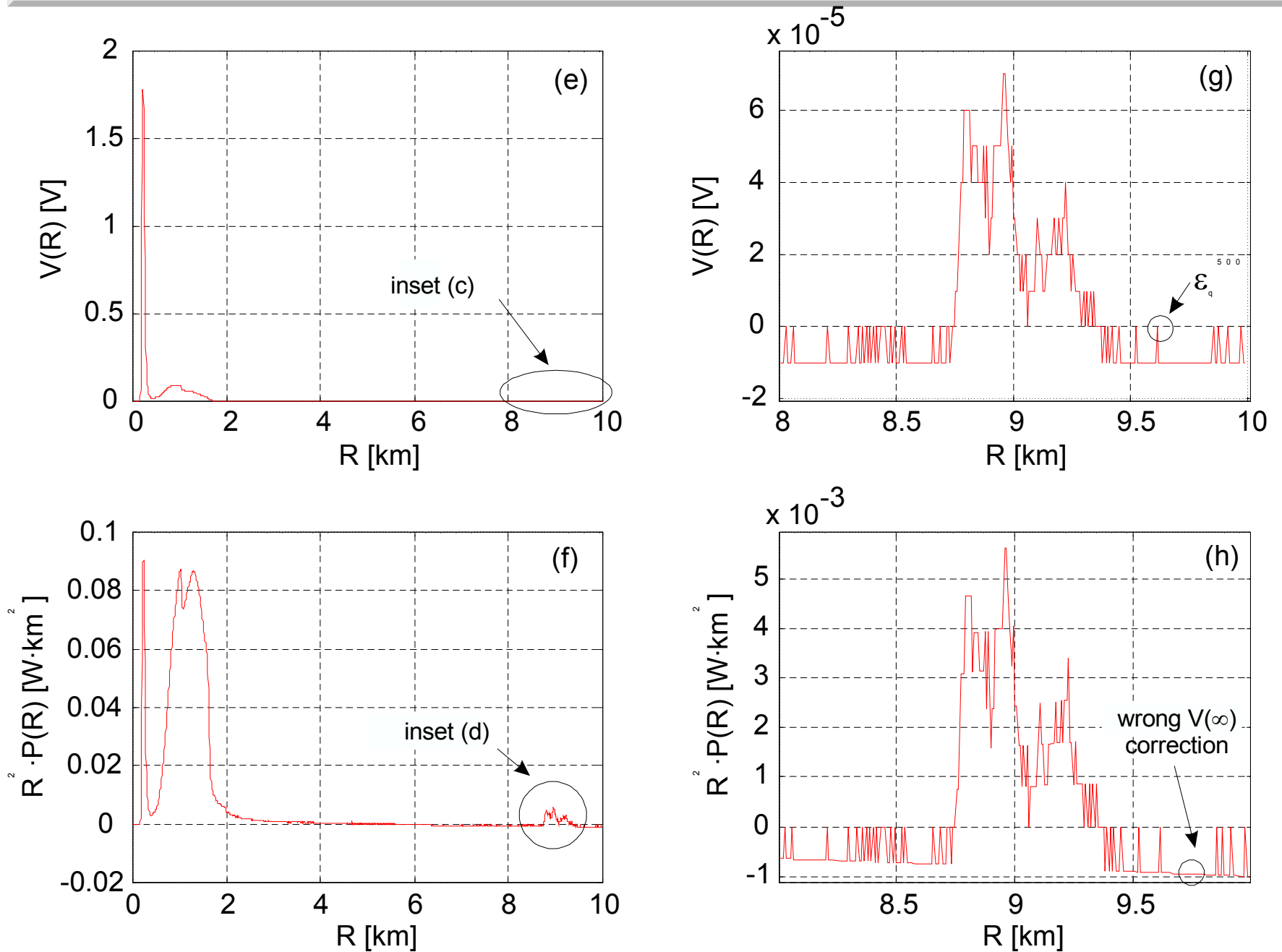
This locates space in formatted string for one or two digits

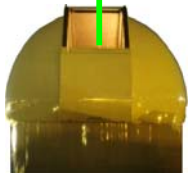
Indexer Codes.
 The HGL Code or Command written below is sent to motor indexer



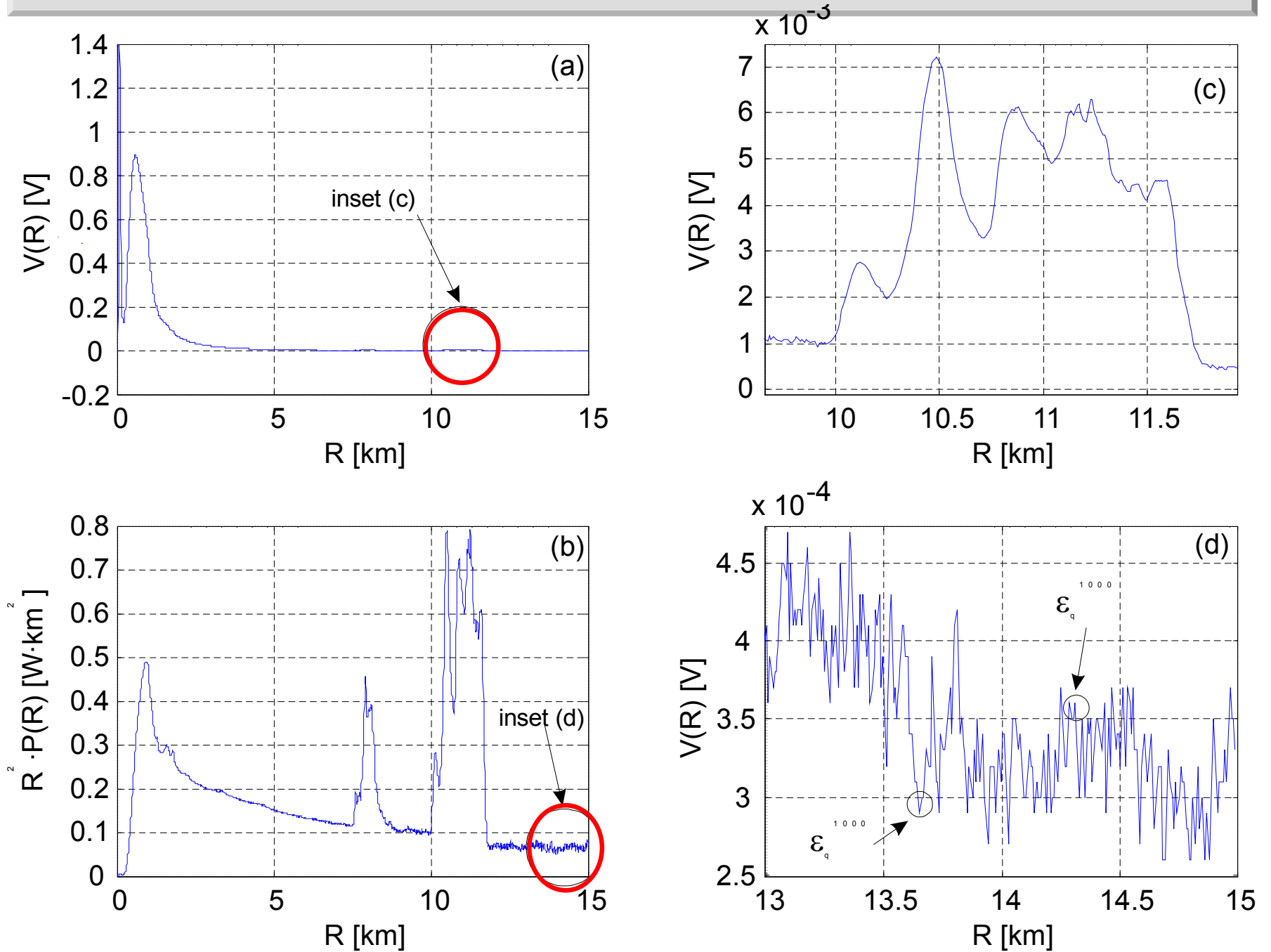


EXAMPLE OF BAD SIGNAL CONDITIONING





EXAMPLE OF GOOD SIGNAL CONDITIONING



WINDOWED EXPLORATION (I)

CONCEPT

-We accommodate range A-B into the ADC at the odd pulses and C-D at the even ones.

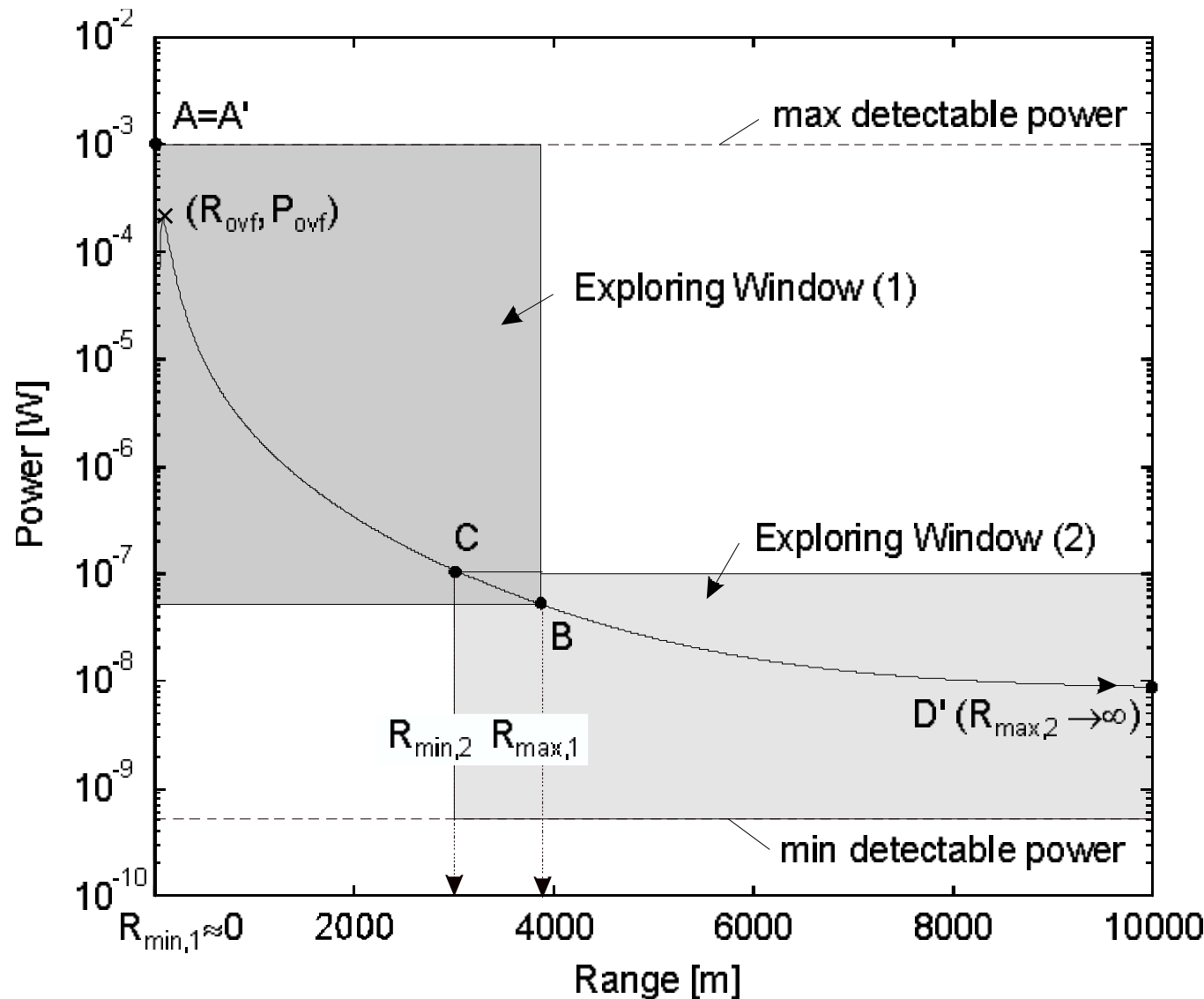
-Hence, ADC dyn. range doubles!

REQUIREMENTS

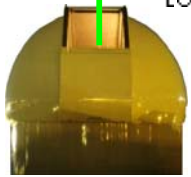
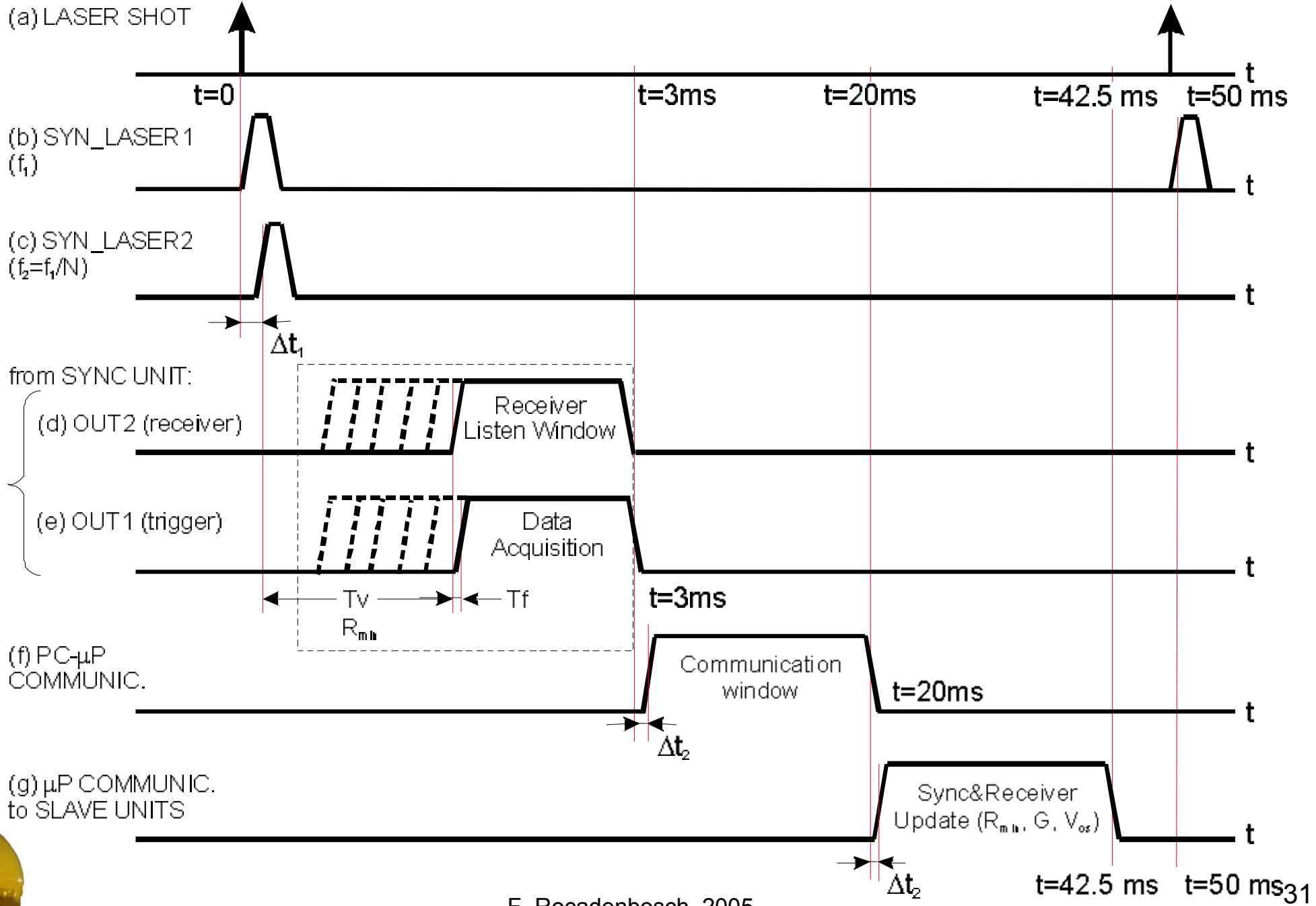
1) Each window is defined by a set

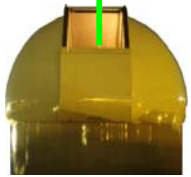
$$(G, V_{OS}, R_{min})$$

2) Synchronous G and V_{OS} update

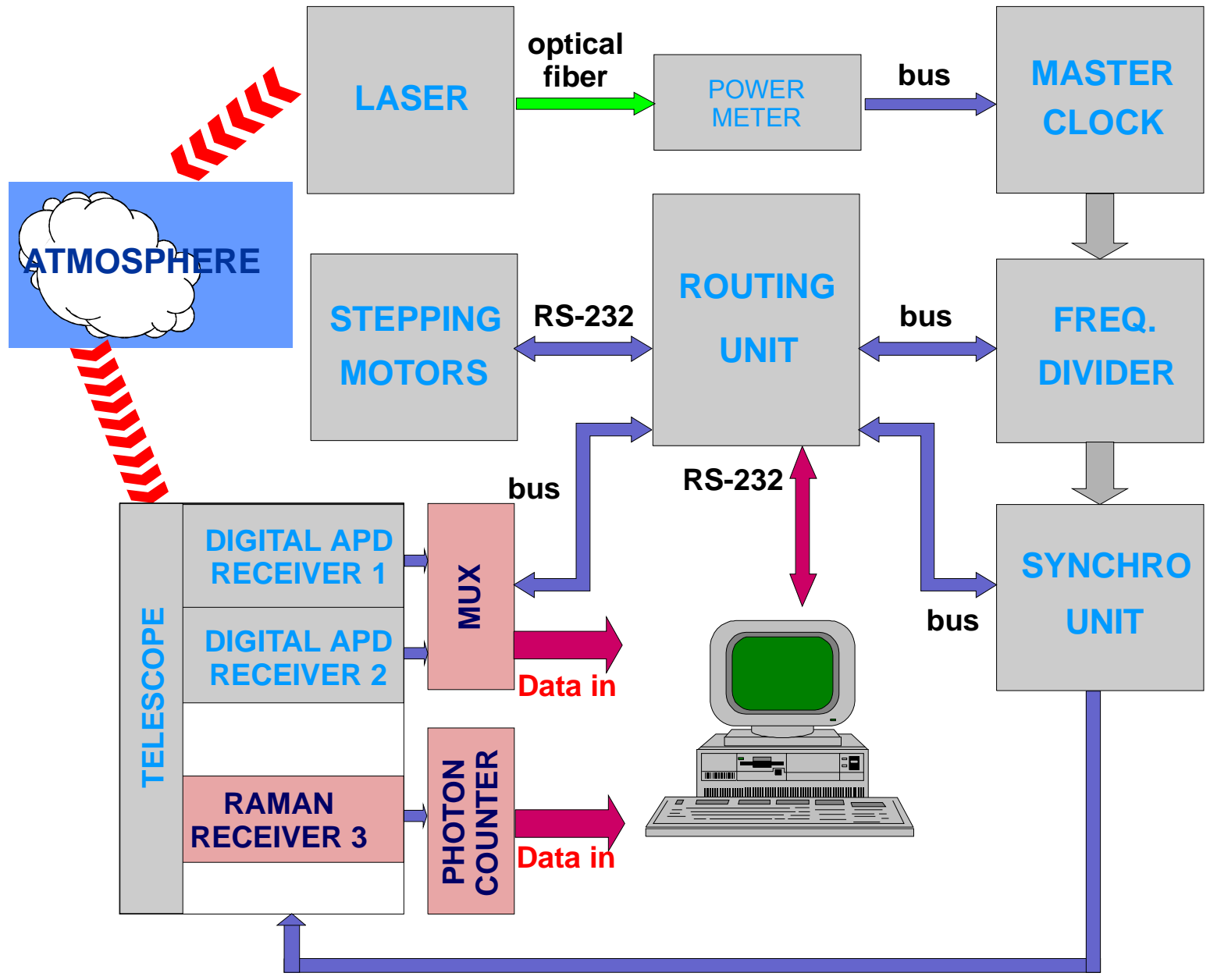


WINDOWED EXPLORATION (II)





SRL SYSTEM CONFIGURATION



PN SEQUENCES (I)

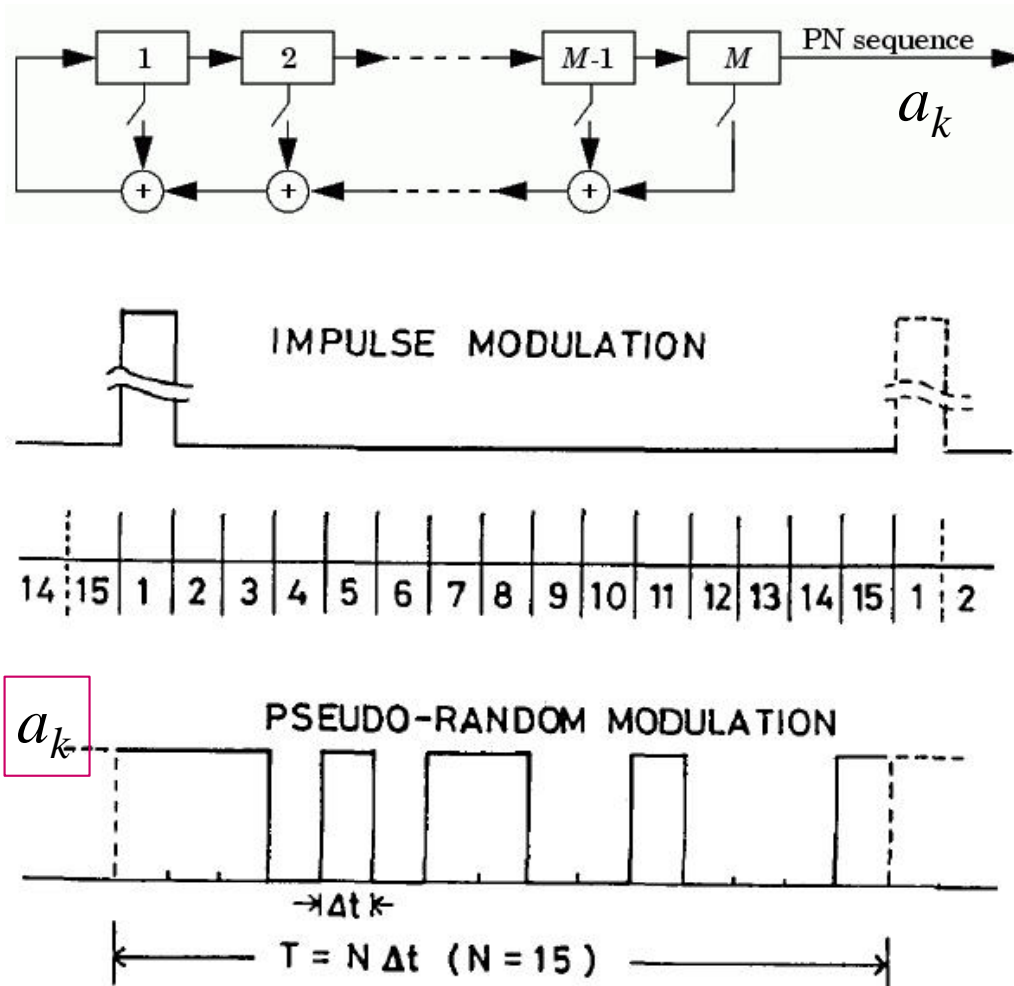


Fig. SOURCE: Takeuchi et al, "Random modulation CW lidar", Appl. Opt., 22(9), 1382-6 (1983).

KEYS:

1) A feedback **n-stage shift register** with non-zero initial state acts as a periodic seq. generator.

2) The PN (pseudo-noise) **sequence length** is

$$N = 2^n - 1$$

i.e., **period = NT_b**

3) Usually, the binary polar NRZ sequence is used,

$$a'_k = 2a_k - 1$$

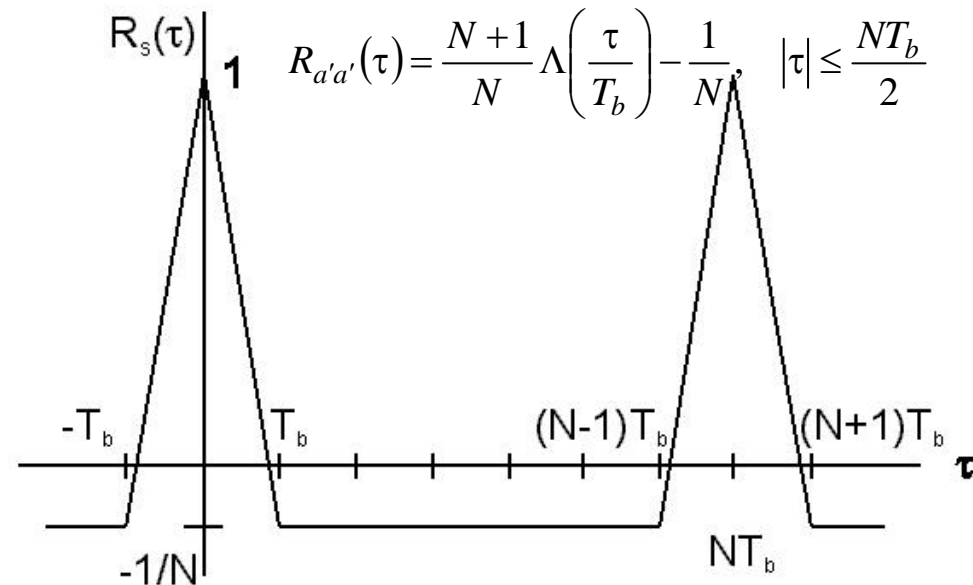
$$a'(t) = \sum_k (2a_k - 1) \Pi\left(\frac{t - kT_b}{T_b}\right)$$

PN SEQUENCES (II)

4) Periodic Autocorrelation

$$\tilde{R}_{a'a'}(j) = \begin{cases} 1 & j = 0 \\ -\frac{1}{N} & j \neq 0 \end{cases}$$

$$\tilde{R}_{aa'}(n) = \begin{cases} \frac{N+1}{2N} = \frac{l}{N} & j = 0 \\ 0 & j \neq 0 \end{cases}$$



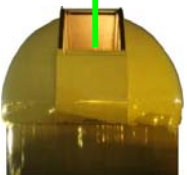
5) Reencounters the system (atmospheric) impulse response \rightarrow

- *System identification*
- *Demodulation is substituted by correlation*

$$g(t) = \frac{c}{2} A_r \frac{1}{R^2} \beta(R) T(R)^2 \xi(\lambda) \xi(R)$$

$$\begin{cases} \tilde{x}(t) = Ea(t) = P_0' T_b a(t) \\ \tilde{y}(t) = \tilde{x}(t) * g(t) \end{cases}$$

$$\tilde{\hat{g}}(t) = \tilde{y}(t) * a'(t) \approx g(t)$$



PSEUDO-RANDOM SYSTEMS

THE ATMOSPHERIC ID. PROBLEM

- The impulse excitation is substituted by

$$\tilde{R}_{ss}(t) = I E_b \delta(t)$$

SYSTEM LAYOUT

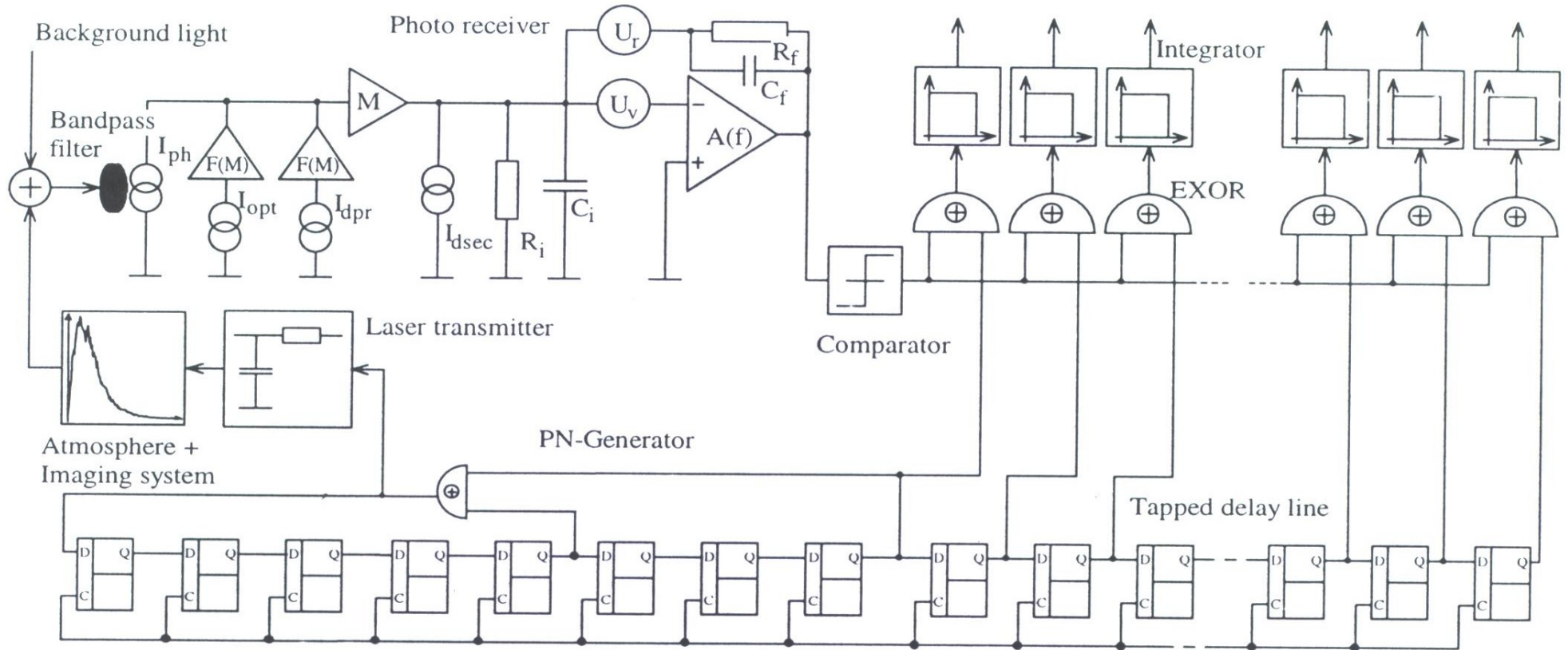
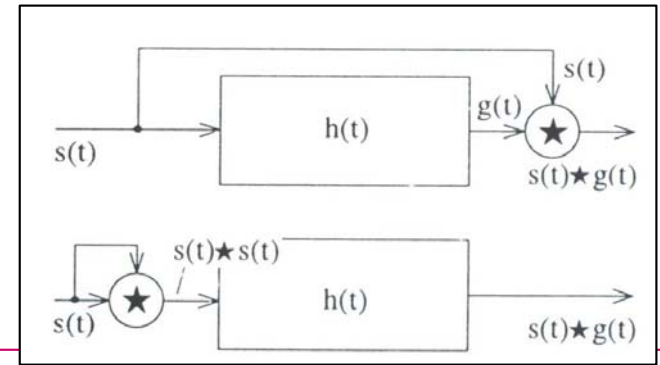


Fig. SOURCE: Bundschuh et al., "Feasibility study of a compact low cost correlation LIDAR using a pseudo-noise modulated diode laser and an APD in the current mode", IEEE (1996).

PSEUDO-RANDOM SYSTEMS

PROTOTYPE EXAMPLE

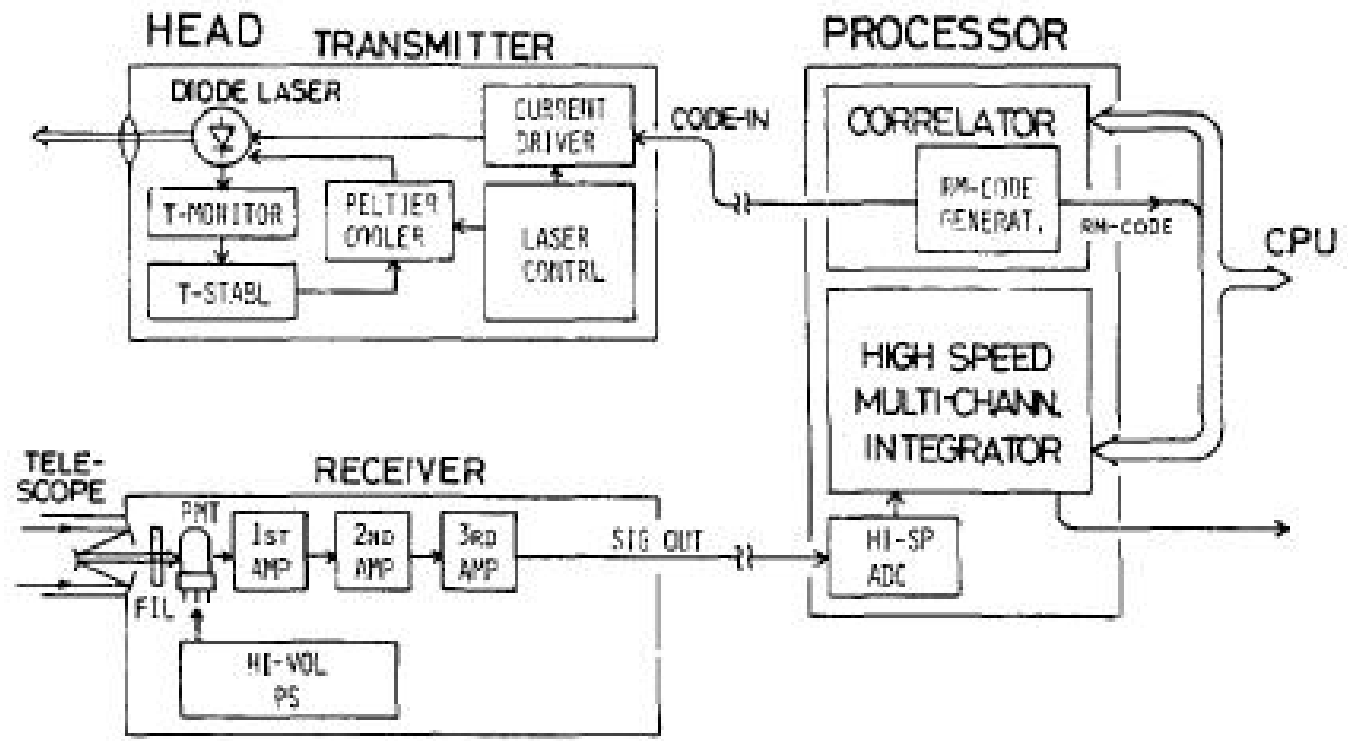
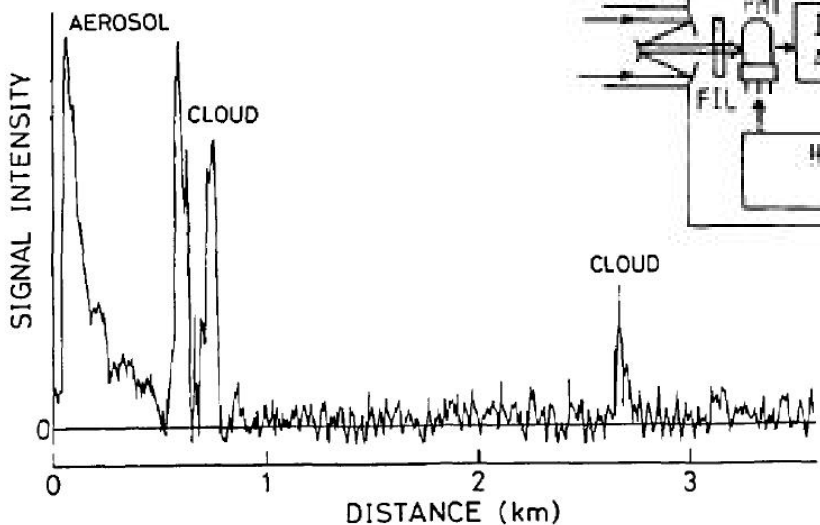
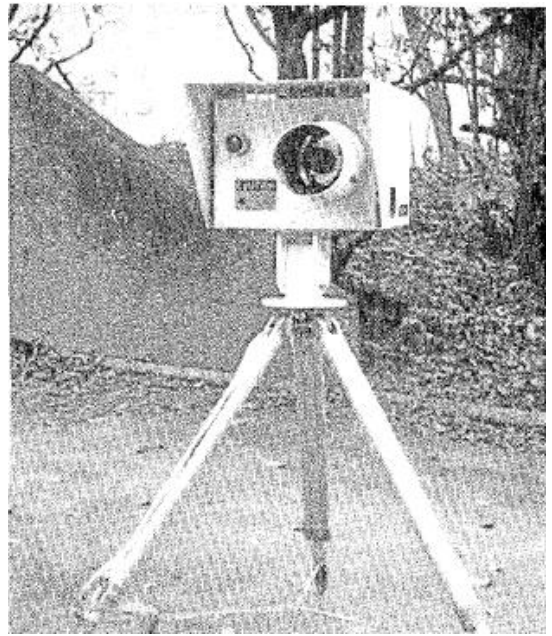


Fig. SOURCE: Takeuchi et al, "Diode-laser random-modulation CW lidar", Appl. Opt., 25(1), 63-7 (1986).