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Metastable microstructures containing zero valent iron for fast degradation of azo dyes

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Metastable Microstructures containing Zero Valent Iron for fast degradation of Azo Dyes --Manuscript Draft--

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Abstract:	<p>A novel iron powder obtained by ball milling ribbons of a rapidly solidified cast iron was tested for azo dye degradation in aqueous solution versus commercial Fe and a Fe-based metallic glass powders. The cast iron powders were at least as efficient in promoting the degradation reaction of ethyl orange and direct blue-6 as the ball milled metallic glass: dyes decomposition was complete in about a hour. The efficiency of alloy samples increases as a function of the decrease of particles size and does not appear to be strongly due to the structure of the phase containing Fe. The main reason for catalytic efficiency is the presence of metastable phases in the material. The Zero Valent Iron they contain is more prone to provide electrons for the degradation of N-N double bonds.</p> <p>The starting material is cheap and the sample preparation is straightforward. Therefore, it is believed these samples are suitable for fast degradation at room temperature of azo dyes compared with metallic glasses recently proposed in the literature.</p>
Funding Information:	

**UNIVERSITA' DEGLI
STUDI DI TORINO**



Dipartimento di Chimica

Torino, 27/04/2015

Dear Editor,

I am submitting a paper for publication in Journal of Materials Science by Federico Scaglione, Postdoc Fellow, and Livio Battezzati, Professor, on

Metastable Microstructures containing Zero Valent Iron for fast degradation of Azo Dyes

This is a research paper dealing with new materials for remediation of wastewaters, especially those containing dyes. During the current decade, there have been reports showing that the decomposition of azo-dyes can be substantially accelerated by employing Zero Valent Iron in the form of powders made from amorphous alloys. The reason for improved efficiency is not at all clear. The Authors think that the claimed change in local structure of the Fe in the alloy does not provide enough insight into the mechanism of action of the catalyst. By employing a widespread material, cast iron, but processed by rapid solidification and ball milling, the Authors show that the mechanism is essentially electrochemical: the less noble the material, the more efficient.

We declare that the work described has not been published before; it is not under consideration for publication anywhere else; and publication has been approved by all co-authors and the responsible authorities at the institute where the work has been carried out.

List of suitable referees:

1) Dr. Annette Gebert, Leibniz-Institute for Solid State and Materials Research (IFW-Dresden), P.O. Box 270016, D-01171 Dresden, Germany. a.gebert@ifw-dresden.de

Dr. Gebert is an expert in electrochemistry and corrosion.

2) Prof. A. Lindsay Greer, Department of Materials Science & Metallurgy, University of Cambridge. alg13@cam.ac.uk.

Prof. Greer is an expert in amorphous alloys, metastable phases and materials.

3) Prof. Jörg F. Löffler, ETH, Metal Physics and Technology, Zurich, Switzerland. joerg.loeffler@mat.ethz.ch

Prof. Löffler is an expert on the synthesis and characterization of novel nanostructured and amorphous materials and their interaction with organics.

Looking forward to hear from you, I remain

Sincerely yours

Dr. Federico Scaglione

Dear Editor,

the title of our paper has been amended to read "Metastable Microstructures containing Zero Valent Iron for fast degradation of Azo Dyes". A clean manuscript with highlighting removed has been uploaded.

Kind regards

Dr. Federico Scaglione

Metastable Microstructures containing Zero Valent Iron for fast degradation of Azo Dyes

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Keywords: ZeroValent Iron, catalysis, microstructure, azo dyes.

Abstract

A novel iron powder obtained by ball milling ribbons of a rapidly solidified cast iron was tested for azo dye degradation in aqueous solution versus commercial Fe and a Fe-based metallic glass powders. The cast iron powders were at least as efficient in promoting the degradation reaction of ethyl orange and direct blue-6 as the ball milled metallic glass: dyes decomposition was complete in about an hour. The efficiency of alloy samples increases as a function of the decrease of particles size and does not appear to be strongly due to the structure of the phase containing Fe. The main reason for catalytic efficiency is the presence of metastable phases in the material. The Zero Valent Iron that they contain is more prone to provide electrons for the degradation of N-N double bonds. The starting material is cheap and the sample preparation is straightforward. Therefore, it is believed these samples are suitable for fast degradation at room temperature of azo dyes compared with metallic glasses recently proposed in the literature.

1 Introduction

Zero valent metals are suggested for use in decomposition of organic molecules commonly employed in several industrial applications which cause waste water pollution [1-3]. The most common material employed so far is Zero Valent Iron (ZVI), commercially available in the form of a metal powder, displaying good efficiency although limited durability due to its corrosion

1 tendency. Various reports appeared recently showing that the decomposition of azo-dyes can be
2 substantially accelerated by employing iron in other forms, specifically powders of a Fe-based
3 metallic glass either atomized or obtained by ball milling glassy ribbons [4]. The latter material
4 proved much more efficient than the former indicating that the rough and kinked surface of ball
5 milled powders offers very likely much more active sites than the smooth surface of atomized
6 droplets of the same composition. Both materials decompose azo-dyes faster than commercially
7 pure Fe powders. On one hand, this is surprising since the Fe content of the metallic glasses is
8 typically of the order of 80 at % therefore it is expected that the number of surface active sites be
9 lower than that of pure Fe; on the other, the structural state of Fe atoms in the metastable
10 amorphous alloy differs markedly from that of crystalline Fe. This was suggested as a reason for
11 improved activity of surface Fe atoms. It is in any case difficult to quantify the actual active surface
12 area, and the consequent the Fe content of the surface of these powders, since the size of the
13 particles is of the order of microns if not tens of microns. There is still then uncertainty on the
14 reason for improved efficiency.

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34 With this scenario in mind we have devised two types of experiments. At first, the catalytic activity
35 of ZVI was tested for Fe-based materials of different composition and structure using bulk samples
36 having macroscopically the same surface area aiming at ranking their efficiency. Then, the
37 decomposition of dyes was attempted using fine powders obtained by ball milling of the more
38 efficient ones. The materials chosen are: a cube of iron having an edge of 1 cm, a $\text{Fe}_{82}\text{Si}_{13}\text{B}_9$
39 amorphous foil, and a cast iron foil equally obtained by rapid solidification (RS). The reason for
40 employing the RS cast iron is that it has a fine microstructure made of ferrite and cementite with
41 some amount of retained austenite, i. e. it contains metastable crystalline phases, and, in addition it
42 is definitely cheaper than the metallic glass.

53 54 55 56 57 58 **2 Experimental**

2.1 Materials and Methods

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Chemical grade azo dyes, Direct Blue 6 (C₃₂H₂₀N₆Na₄O₁₄S₄) and Ethyl-orange (C₁₆H₁₈N₃NaO₃S), and distilled water (Elix Millipore, resistivity 5.4 MΩ cm⁻¹ @ 25°C) have been used to prepare aqueous solution with concentration of 0.2 g l⁻¹. For each degradation experiment the ratio of grams of samples to volume of solution was kept constant at 13.4 g l⁻¹ for a comparison with other works in the literature [4]. Experiments have been collected in duplicates to check reproducibility.

Cubes having edge of 1 cm were machined from a sheet of mild steel and polished on all sides as for conventional metallography. Fe powder (99.9 % grade) was from Strem Chemicals, Newburyport, MA, USA (product n. 7439-89-6). Cast iron ribbons and powders were prepared as detailed in the next section. A commercial foil of Metglas® 2605SA1,[5] a magnetic materials employed in the core of distribution transformers of approximate composition Fe₈₂Si₉B₁₃, was purchased and cut in pieces of size comparable with those of the cast iron ribbons. Ribbons and powders have been characterized by X-ray diffraction (XRD) in Bragg–Brentano geometry with monochromatic Co Kα radiation and scanning electron microscopy (SEM).

The cubes, ribbons or powders were introduced in a test tube together with the dye solution and kept at room temperature without stirring the solution. Portions of 1 ml of solution were pipetted out, diluted appropriately and filtered to measure the ultraviolet-visible (UV) absorption spectrum as a function of reaction time.

Fourier Transform Infrared spectra (FTIR) of the azo dye and of the degraded insoluble products were obtained with a FTIR Bruker IFS 28 averaging 64 scans for each measurement. Degradation products were separated from the powder by dissolving them in ethanol. The solution was then pipetted out after powder settling. After waiting for ethanol evaporation, the product residue was recovered as a powder which was prepared for FTIR by mixing 10% (w/w) of specimen with KBr and pressing into a thin pellet. The control azo dye spectrum was collected in attenuated total

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2 reflectance (ATR), pressing the pure compound onto a diamond window. ATR measurement is
3 corrected for a direct comparison of the two spectra.

4 5 **2.2 Manufacture of cast iron samples**

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9 Lumps of a cast iron ingot of industrial production having Carbon equivalent of 4.31% i. e. 3.72
10 wt% C and 1.78 wt% Si, ($\text{Fe}_{82}\text{C}_{15}\text{Si}_3$ in at%) have been induction melted and rapidly solidified by
11 means of a melt spinning apparatus in the form of ribbons about 25 μm thick and 1 cm wide. An Ar
12 protective atmosphere was employed during the rapid solidification processing [6]. This resulted in
13 a white cast iron whose microstructure is made of equiaxed crystals of ferrite and cementite on the
14 side which was in contact with the spinning wheel (**Fig.1**). The crystals become then dendritic in the
15 central part of the ribbon up to the external side. They are some hundreds of nanometer in thickness
16 and several micrometers long with short lateral arms around a micron in size. The phase
17 constitution is made of ferrite, cementite, i. e. the expected eutectic mixture, and retained austenite
18 as indicated by XRD patterns taken on both sides of the ribbons (**Fig.2**). Here, the reflections have
19 varied intensity because of the oriented dendrites seen in **Fig.1**. The austenite is metastable at low
20 temperature and transforms into ferrite and cementite on heating above 400 °C [6]. The cementite is
21 obviously metastable in the Fe-C system, but the microstructure obtained by rapid solidification has
22 a further degree of metastability in that the ferrite is slightly super saturated in C and the cementite
23 off-stoichiometric [7]. Despite containing some austenite the ribbons are brittle. Therefore, portions
24 of them have been ball-milled for 8 or 24 hours in an agate cell to get powders of different size.
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51 **3 Results and discussion**

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56 Degradation of dyes is reported and discussed sequentially on bulk samples and ball milled cast
57 iron.
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59 60 61 **3.1 Bulk samples**

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2 Samples of different structure and composition but having the same geometrical external area are all
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4 active for dye degradation as shown in **Fig.3**. We confirm the finding in [4] and [8] that amorphous
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6 alloys, here $\text{Fe}_{82}\text{Si}_9\text{B}_{13}$, degrade faster the dye than iron. The RS cast iron appears on average as
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8 good as the metallic glass in view also of being produced with the same melt spinning technique,
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10 therefore the surfaces of the two materials are well comparable. It is well known, in fact, that melt
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12 spun ribbons display a dull surface, the one in contact with the spinning wheel, and a shiny surface,
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14 the opposite one. The difference is caused by asperities of the wheel which are replicated in the
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16 ribbon and by bubbles of protective gas entrapped between wheel and ribbon. Both RS materials
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18 have the same Fe content of 82 at % but different structure, therefore their activity should be due to
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20 a cause diverse from geometry of sample, composition and structural state.
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28 3.2 Ball-milled cast iron 29 30 31 32 33

34 For any application a high surface area is required and therefore the ribbons must be processed to
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36 obtain powders of fine grains. In [4] it was shown that ball-milled powders of an amorphous alloy
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38 are much more preferable than atomized powders, very likely because they are made of irregular,
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40 instead of smooth, rounded particles. The higher surface area was attributed to complex fracture
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42 surfaces. Analogously, cast iron powders were than made by ball-milling the ribbons.
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45 After ball-milling for 8 hours the ribbons are fragmented in fine pieces which, however, still retain
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47 mostly a plate-like shape (see inset of **Fig.4**). The aspect ratio of the platelets is of the order of 10.
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50 The absorbance of the ethyl-orange solution in contact with the BM-powder is shown in **Fig.4a**: it
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52 decreases steadily with time and practically vanishes after 26 hours as shown by the trend of the
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54 maximum of the absorbance in **Fig.4b**. Since the phase constitution of the material was not changed
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56 during the ball milling process as shown by the invariance of the angular position and number of
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58 reflections in XRD patterns of the powders with respect to those reported in **Fig.2**, the acceleration
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1 of dye degradation must be entirely attributed to the increased amount of active surface available
2 for the reaction. After ball milling for 24 h the aspect ratio of the particles was reduced by a factor
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4 of ten and their shape became roundish (inset in **Fig.5**). Still the phases in the powders remained as
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6 in the original ribbon but broadening of reflections due to the reduced size of scattering domains
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8 and loss of orientations have been observed especially for the more brittle phase, cementite (**Fig.2**)
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10 which is known to finely subdivide and eventually dissolve in ferrite as a consequence of heavy
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12 deformation [9, 10]. Their efficiency in degrading fast the dyes is demonstrated by the spectra in
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14 **Fig.5a**. The trend of the maximum of absorbance (both ethyl-orange and direct blue-6) as a function
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16 of time is given **Fig.5b**. The de-colouring is complete in less than one hour, a time well comparable
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18 with that of ball milled amorphous ribbons reported earlier with curves compatible with a first order
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20 exponential decay as well [4]. For countercheck we performed also the degradation of dyes by
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22 means of commercial Fe powders, 1 to 5 μm in size: it was much slower in that the absorbance was
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24 halved in about 50 hours confirming previous results [4]. After being dispersed in the solution the
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26 particles tend to aggregate being all ferromagnetic [11, 12], moreover with the advancement of
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28 degradation non soluble decomposition products sedimented together with the powders. However,
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30 the efficiency of powders is not hindered, indeed if a new portion of solution is added to the powder
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32 already used, without washing the sediment out, a second degradation cycle is possible with the
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34 same kinetics, i. e. no apparent passivation. Up to four consecutive degradation cycles the kinetics
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36 is only slightly slowed of 5 and 7 % respectively for the third and fourth cycle. This indicates the
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38 efficiency is maintained as long as Fe atoms in active sites are prone to oxidize to Fe^{2+} . In fact, the
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40 reduction mechanism of azo dyes is basically due to a redox reaction between Fe atoms and –
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42 (N=N)– azo dye bonds,[8] splitting the dye in aromatic amine [13] and other compounds such as
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44 aniline [14]. FTIR spectra of degraded products have been collected in the range of 500 – 4000 cm^{-1}
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46 and compared with that of the dye before treatment. In **Fig.6** the bands of spectrum a) are associated
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48 respectively: at 640 cm^{-1} and 977 cm^{-1} to S=O and C–O stretching, at 1044 cm^{-1} , 1186 cm^{-1} , 1340
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50 cm^{-1} to asymmetric and symmetric stretching of C–N, at 1492 cm^{-1} and 3421 cm^{-1} to symmetric
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1 stretching of N–H, at 1615 cm⁻¹ and 2924 cm⁻¹ to stretching of –N=N– and C–H [15]. In spectrum
2 b) the stretching of –N=N– has vanished, while new peaks associated to degraded products of the
3 dye appear: at 1631 cm⁻¹, 1730 cm⁻¹ and 1376 cm⁻¹ respectively scissor vibration of N–H and C–N
4 vibration in aromatic amines, at 1457 cm⁻¹ C=C stretching vibration of the aromatic ring [16]. This
5 confirms literature results showing that the breaking of the chromophore bond could probably form
6 anilines and benzenesulfonic acids [17]. It is reckoned that adsorption of dyes occurs on the iron
7 prior to degradation. However, this does not cause passivation of powders up to at least four
8 degradation cycles. The catalyzer was found to become exhausted due to formation of iron oxides
9 identified in XRD patterns. At this stage adsorption phenomena could still give rise to some
10 decoloring since the high adsorption properties of iron oxides particles has been recently proven
11 [18].
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26 In summary, both the as cast ribbons of cast iron and the ball milled powders obtained with them
27 are at least as active towards dye degradation as Fe-based amorphous alloys, being certainly much
28 cheaper. On a more fundamental ground, the results obtained in this work show that the structure of
29 the material does not appear the determining factor for its catalytic activity. Since the commercially
30 pure Fe is in any case less active, it is suggested that the occurrence of metastable phases is most
31 relevant being these more prone to provide electrons to break the N-N bonds of the dyes according
32 to the reaction mechanism outlined in [19, 20]. To this respect we recorded both the open circuit
33 voltage (OCV) and potentiodynamic behaviour of ribbons of cast iron and glassy Fe₈₂Si₉B₁₃. The
34 OCV is about 0.5 and 0.65 V respectively and the corrosion potential is 0.6 V and 0.7 V more
35 negative (**Fig.7**) with respect to those of a Fe foil. It is concluded that the catalytic effect on azo dye
36 degradation stems from the increased electrochemical activity of the material. It is worth noting that
37 an even faster reaction rate was recently reported for Mg-Zn-Ca metallic glasses,[21] i. e. a more
38 corrodible alloy, although definitely more expensive than cast iron. Finally, we note that the
39 corrosion products of white cast iron are well known and dealt with in water remediation, i. e. Fe
40 oxides, hydrocarbons or carbonates according to the pH of the solution and the eventual applied
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1 potential [22, 23]. The rapidly solidified and ball milled cast iron looks than more advantageous in
2 dye degradation than other forms of ZVI tested in this work, namely commercial pure Fe and a
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4 metallic glass.
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9 **4 Conclusion**

10 The present work shows that powders made by ball milling ribbons of rapidly solidified cast iron, a
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12 white cast iron containing ferrite, cementite and retained austenite, are good catalytic materials for
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14 the degradation of organic dyes. Rapid solidification is essential to obtain the above phase mixture
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16 and a fine size of crystals. The ribbons are brittle and, therefore, suited for ball milling which should
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18 be prolonged enough to reduce the particle aspect ratio to about one (24 hours with the working
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20 procedure used here) while keeping the phase constitution of the material unchanged. The cast iron
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22 powders are as effective as the best Fe-based materials proposed to date in the literature (i. e. ball
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24 milled amorphous alloys), although definitely cheaper, for the degradation of dyes. The increased
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26 reactivity proven also by electrochemical analyses will certainly also enhance the corrosion rate of
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28 the alloy powders since the oxidation of Fe is inherent to the process. Using this material will then
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30 be a matter of trade-off between the need for fast degradation and that for powder replacement
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32 although clear advantages are recognized, i.e. large availability and low price, fast degradation
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34 kinetics.
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60 **References**

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Captions

1
2 **Fig.1** SEM image of a cross section of a cast iron ribbon produced by rapidly solidification (wheel
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4 side on the right)
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9 **Fig.2** XRD patterns of the wheel (a) and external (b) sides of a cast iron ribbon produced by rapidly
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11 solidification, (c) after ball milling for 24 h
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17 **Fig.3** Normalized UV-visible absorption as a function of treatment time for bulk samples: C1 and
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19 C2 were white cast iron ribbons of the same composition, $\text{Fe}_{82}\text{Si}_9\text{B}_{13}$ was a glassy foil and Fe was in
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21 the form of polished cubes. All samples had the same geometrical external area. Experiments of
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23 ethyl orange degradation were performed at room temperature
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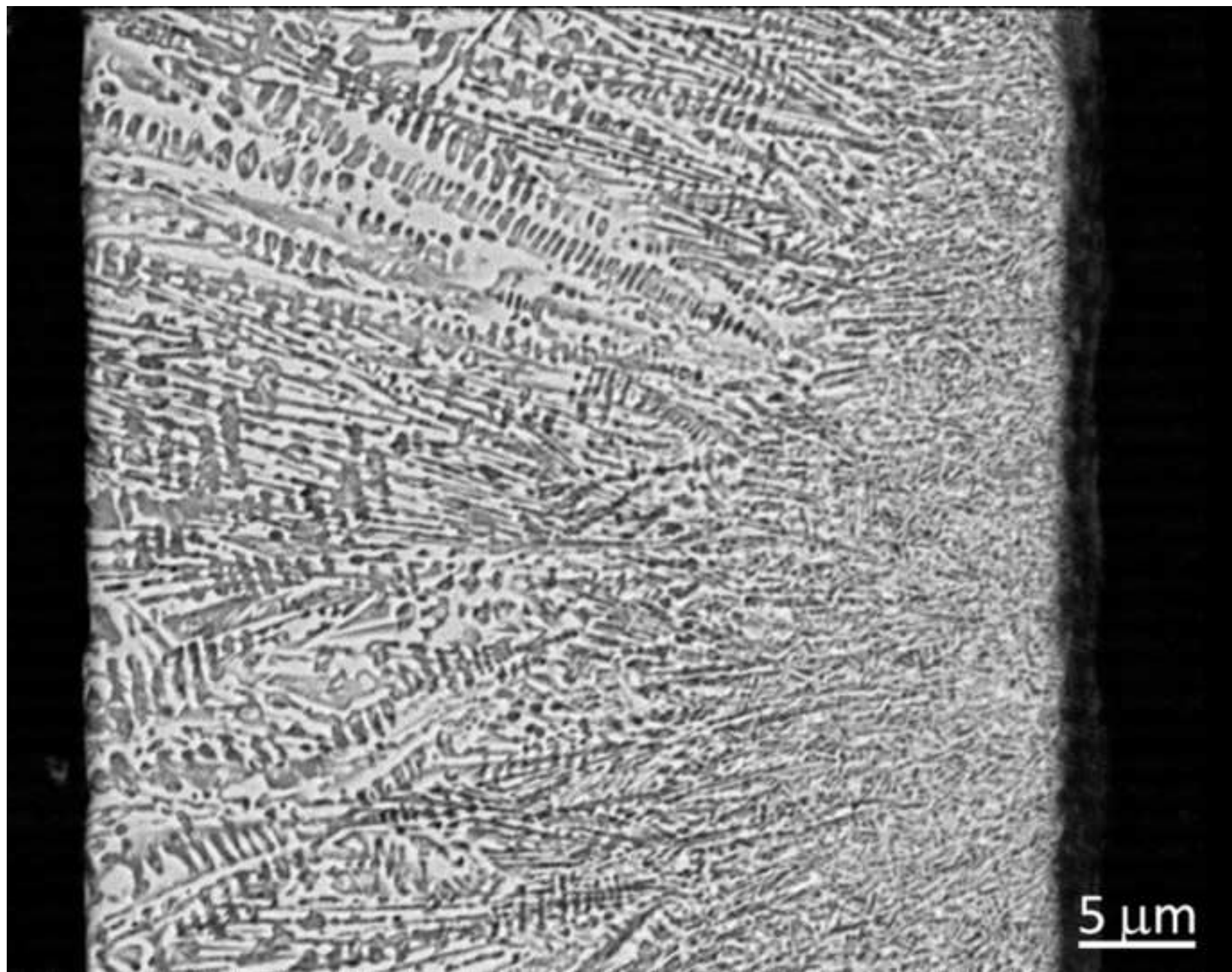
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29 **Fig.4 a)** UV-visible absorption of ethyl-orange solutions as a function of residence time on C1 and
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31 C2 white cast iron powders obtained by ball milling ribbon portions for 8 hours. **b)** The maximum
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33 of the absorbance as a function of residence time. The inset is the SEM image of the powder
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35 showing a plate-like shape
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40 **Fig.5 a)** UV-visible absorption of direct blue-6 solutions as a function of residence time on C1 and
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42 C2 white cast irons powder obtained by ball milling ribbon portions for 24 hours. **b)** The maximum
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44 of the absorbance as a function of residence time for both ethyl-orange and direct blue-6. The inset
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46 is the SEM image of the powder displaying roundish shape
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52 **Fig.6** FTIR spectra of **a)** Direct Blue 6 azo dye and **b)** degraded products after treatment with C1
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54 and C2 white cast irons powder obtained by ball milling portions of a ribbon for 24 hours
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58 **Fig.7** Potentiodynamic polarization curves in 0.2 g l^{-1} ethyl-orange azo-dye solution for samples
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60 listed in the legend. Experiments were performed at room temperature with a scan rate of 20 mV s^{-1}
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Figure

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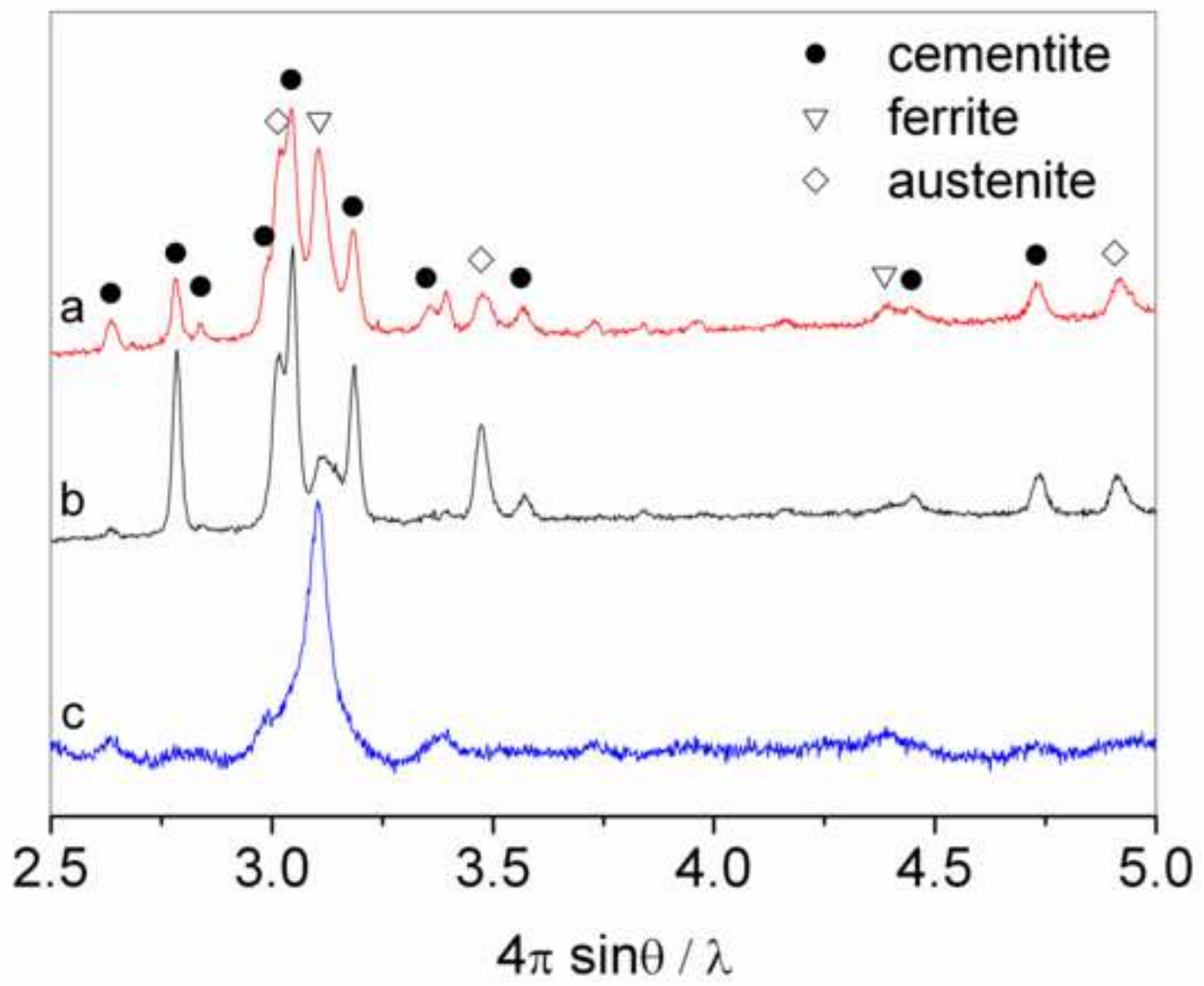
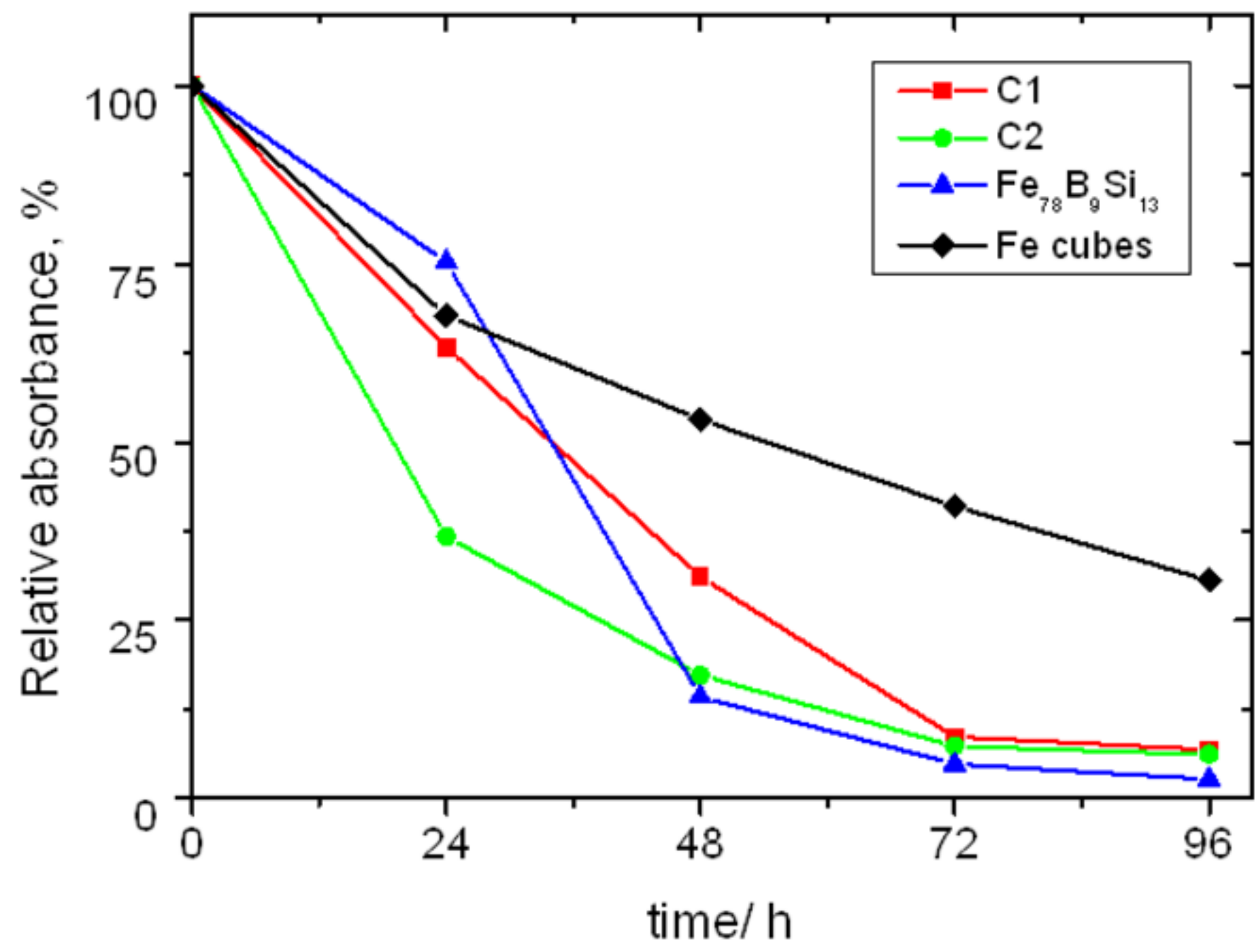
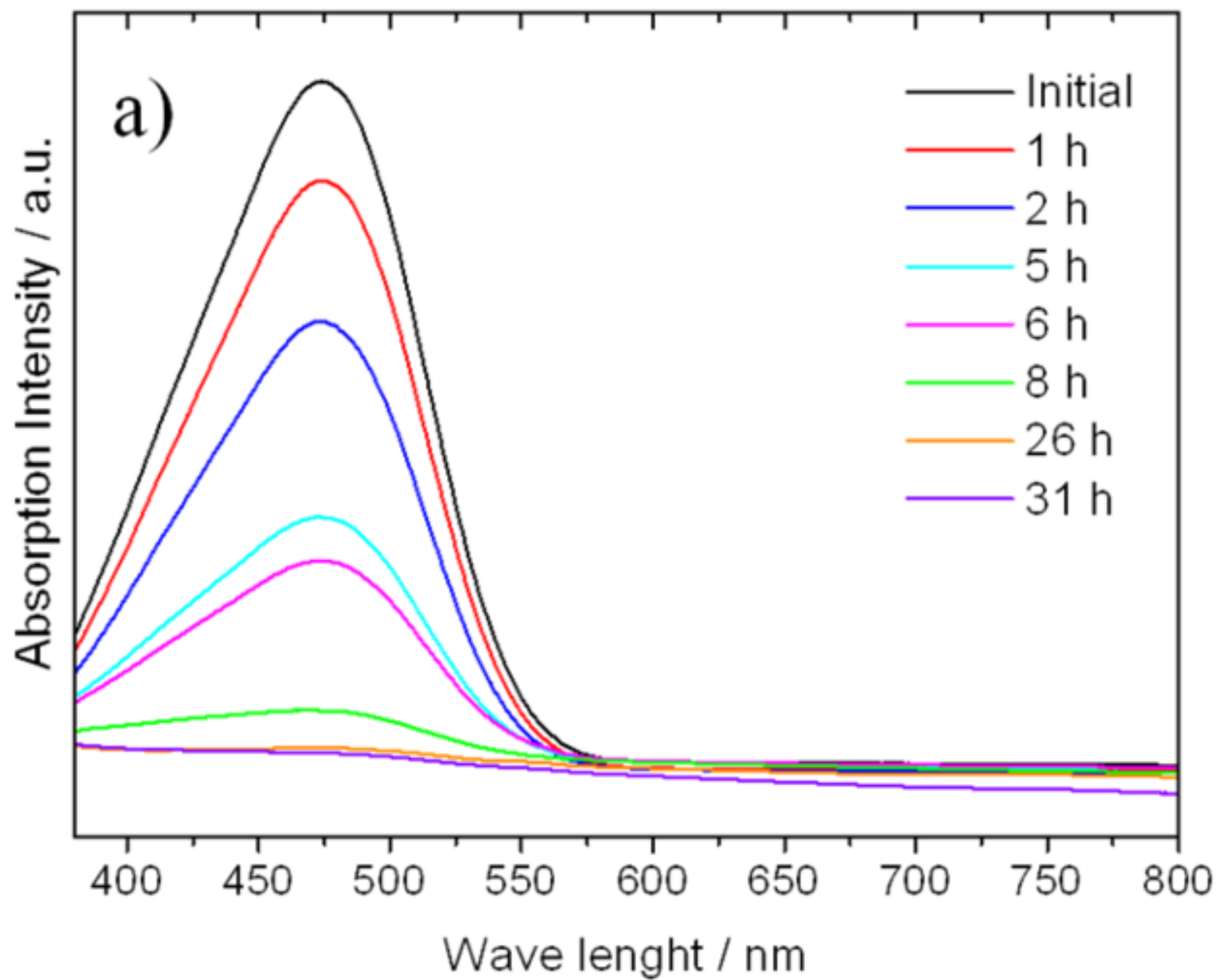
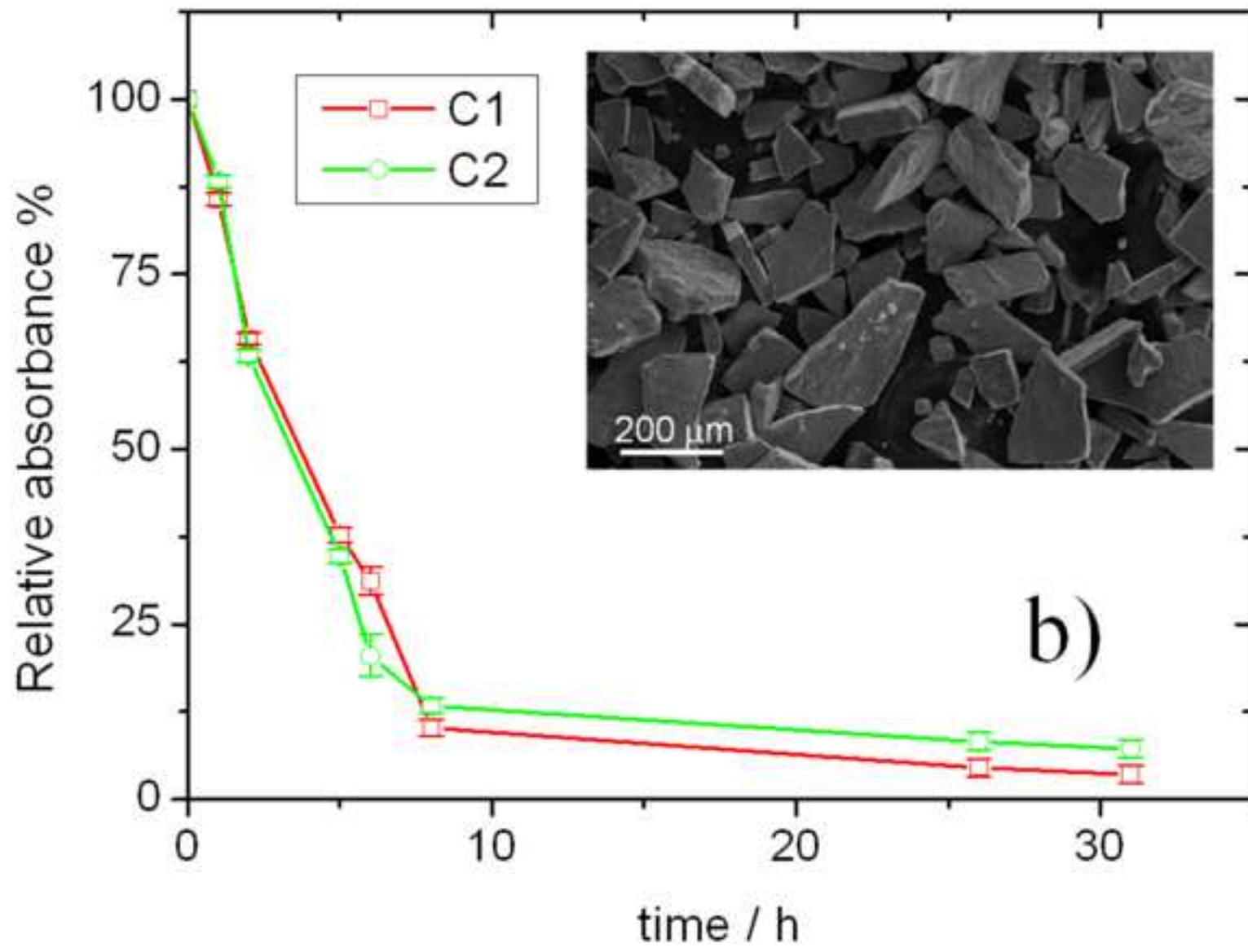
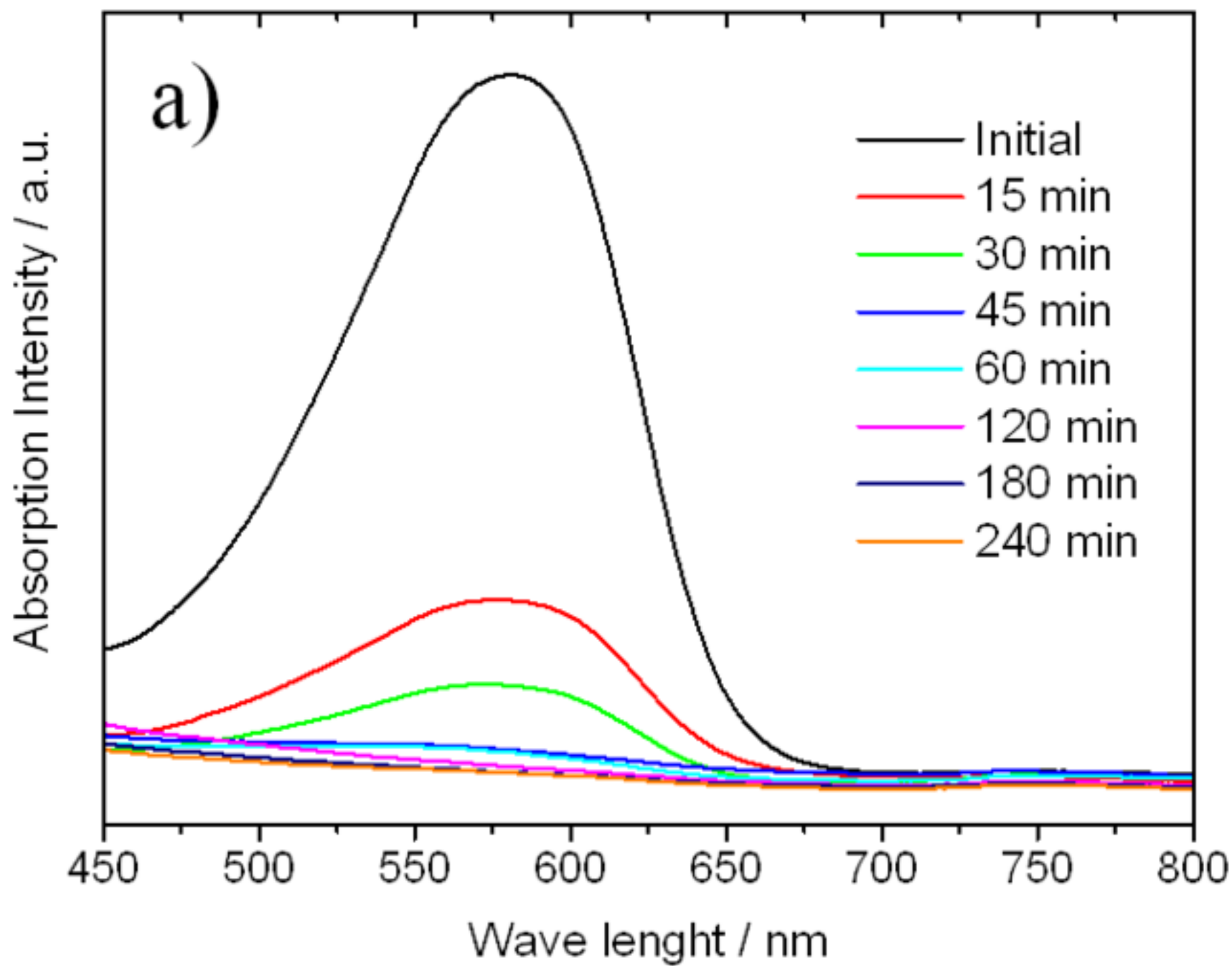


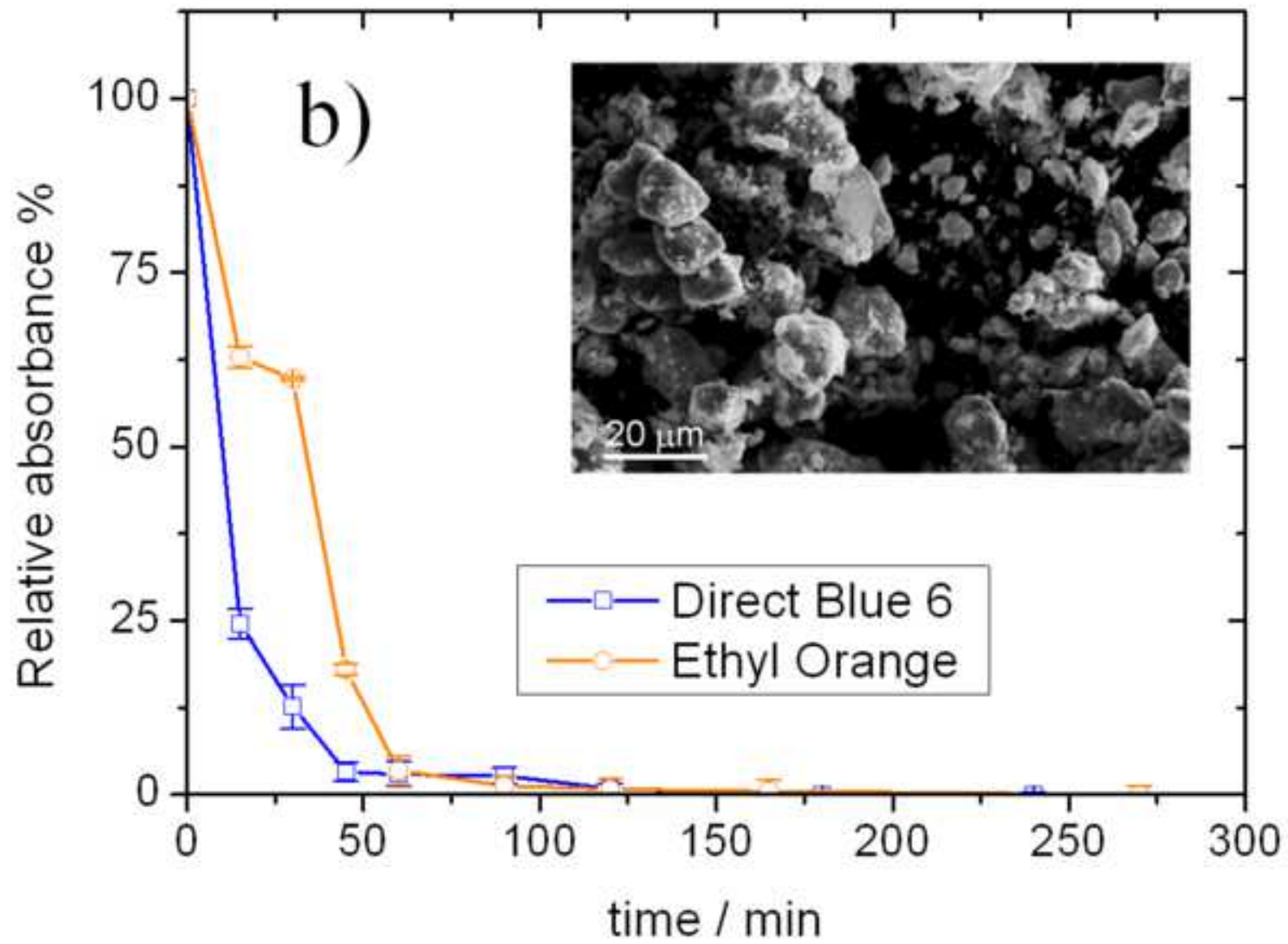
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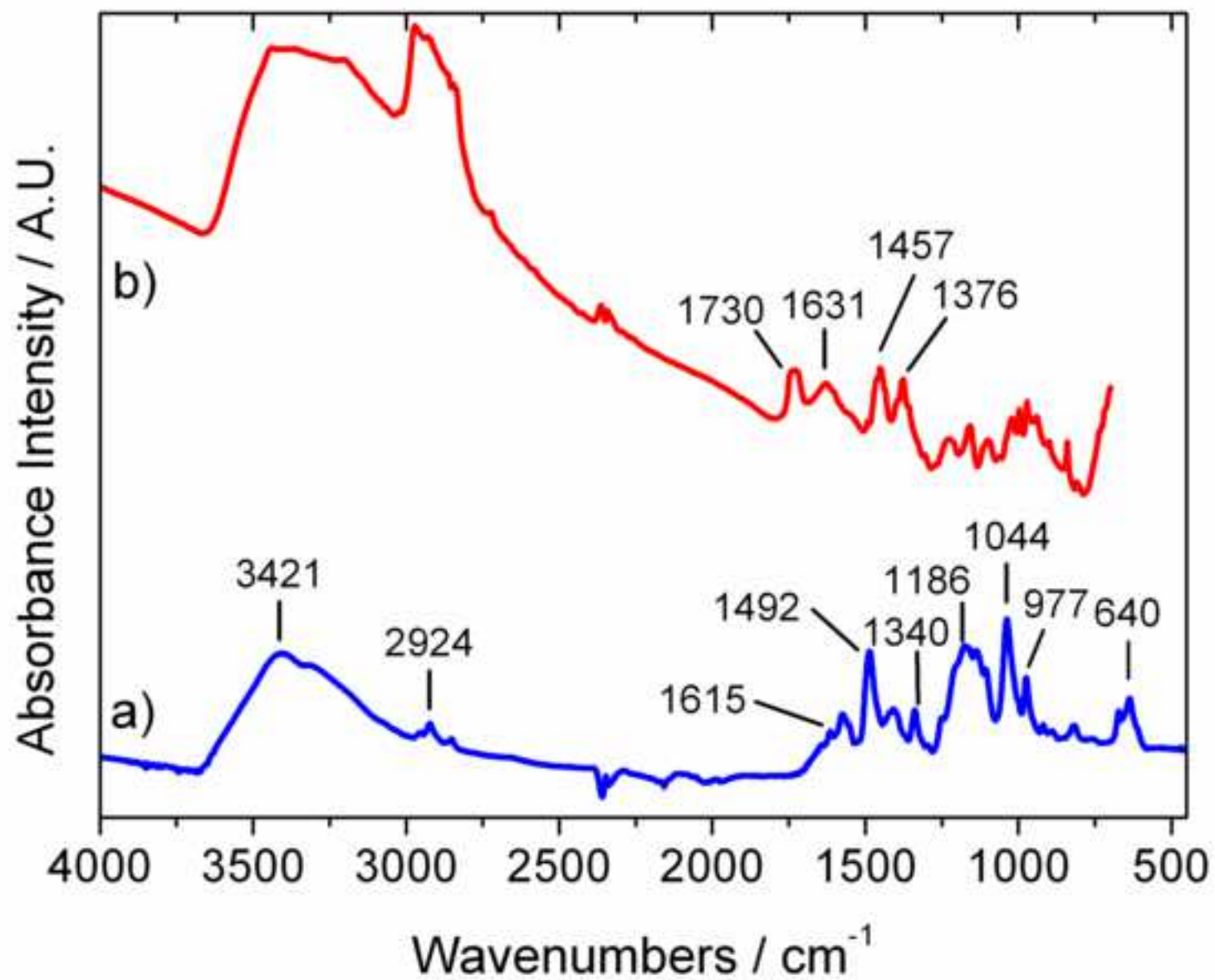


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