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Centrifugally spun mats based on biopolyesters/hydroxyapatite and their potential as bone scaffolds

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This is the author manuscript accepted for publication and has undergone full peer review but has not been through the copyediting, typesetting, pagination and proofreading process, which may lead to differences between this version and the Version of Record. Please cite this article as doi: [10.1002/app.50139](https://doi.org/10.1002/app.50139)

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Centrifugally spun mats based on biopolyesters/hydroxyapatite and their potential as bone scaffolds

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Abstract

This work studied the potential of centrifugal spinning for the production of fibrous materials based on poly(D,L-lactic acid) (PDLLA) and poly(3-hydroxybutyrate) (PHB) with hydroxyapatite nanoparticles (n-Hap). The influence of n-Hap concentration (5, 10 and 15 wt %) and spinneret angular speed on the final fiber morphology were analyzed. Further experimental evaluations were implemented to determine the effect of n-Hap on the thermal and mechanical performance. The optimum parameters that show a balance among high yield production of homogeneous fibers with the smallest fiber average diameter were found to be at 5 wt % of n-Hap processed at 7000 rpm for PDLLA, and 5, 10 and 15 wt % of n-Hap at 6000 rpm for PHB. The thermal stability, for both systems, was not significantly affected. The mechanical performance of PHB systems was improved with the addition of n-Hap. Osteoblast cell viability tests depicted a favorable cell response on the PDLLA systems.

1. Introduction

Hydroxyapatite nanoparticle (n-Hap) is a ceramic material mainly used in applications related to bone tissue, due to its resemblance to bone in structure and composition. Several recent studies reported that n-Hap contributes to important biological processes for bone tissue regeneration,

such as osteoconduction¹ (bone growth at the superficial level), osteoinduction² (pluripotent cells are stimulated to develop bone-forming cells, a process that induces osteogenesis) and osseointegration³ (stable anchorage of an implant, obtained by direct contact between the bone tissue and the implant). The major limitation in the use of n-Hap-based materials as bone implants is their poor mechanical behavior, increasing their fragility when they are manufactured in the form of scaffolds with high porosity to mimic the bone structure. Therefore, these ceramic compounds are commonly used as fillers or coatings in polymeric matrices.⁴

The design of polymeric scaffolds with n-Hap has been widely explored due to their effective regenerative characteristics, mainly those based on synthetic and natural biopolymers.⁵ In the biomedical area, the approach has been tilted in the production of polymer fiber scaffolds as they are systems that provide a structural morphology similar to the extracellular matrix of various tissues within the human body. The interest in this type of hybrid materials has promoted their study with different line cells, obtaining promising results for applications in tissue engineering.^{1,6-9}

Several research teams have worked on the design of fibrous materials based on PHB/Hap produced by electrospinning. Ramier *et al.*⁷ reported changes in the roughness of the fiber which resulted in improvements in the mechanical properties (Young's module, tensile strength), and increased adhesion and differentiation of human stromal mesenchymal cells (hMSc). Sadat-Shojai *et al.*⁶ results provided information that n-Hap have not a cytotoxic effect on mouse pre-osteoblast cells (MC3T3-E1) under *in vitro* conditions, thus suggesting further use for *in vivo* evaluation.

Poly(L-lactic acid) (PLLA) has also been explored for the design of n-Hap hybrid nanofiber membranes through the same technique than PHB/Hap. Morelli *et al.*¹ reported the influence of n-Hap on surface morphology and average fiber diameter and observed a decrease in mechanical performance (Young's modulus, tensile strength) by increasing the concentration of n-Hap to 50 wt %. On the other hand, Novotra *et al.*⁸ designed polymeric fibers containing 5 and 15 wt % of n-Hap, with similar tensile mechanical performance (stiffness and % of elongation at break);

furthermore, *in vitro* tests demonstrated good support for adhesion, growth and osteogenic differentiation. Recently, Sánchez-Arevalo *et al.*⁹ observed changes in the surface morphology and diameter of PLLA fibers obtained at concentrations of 2, 4 and 6 wt % of n-Hap; and found that at a concentration of 2 wt % there was a decrease in macro and micro tensile mechanical properties (Young's modulus).

Electrospinning has been the preferred method to produce the needed nanofiber membranes.¹⁰ However, this technique has certain limitations such as the need to use solvents with specific dielectric properties, high energy cost due to the required high voltage, and for lab scale single-needle electrospinning systems, low production rates (typically 10-100 mg·h⁻¹).¹¹ Alternative technologies have been developed with the purpose to overcome some of the electrospinning limitations. One of these technologies is the centrifugal spinning, a competitive option given its high production rate (50-100 g·h⁻¹)¹²⁻¹⁴ and lower operational cost since there is no need for electric fields and can easily be used for solvents or melts (further decreasing cost).

In this work, the process conditions for obtaining hybrid materials based on homogeneous PDLLA and PHB fibers with n-Hap are reported using the centrifugal spinning technique, Forcespinning®. In addition, an analysis of the influence of such nanoparticles on the morphological characteristics of the obtained fibers was established. Finally, aspects related to the influence of n-Hap on the thermal and mechanical performance as well as the interaction of the design materials with osteoblast cells were addressed to assess their potential application as bone scaffolds.

2. Experimental Methodology

2.1. Materials and reagents

Poly(D, L-lactic acid) (PDLLA) provided by NatureWorks LLC (Ingeo 6362D) with $M_w=160$ kg mol⁻¹ and $\bar{D} = 1.646$, and poly(3-hydroxybutyrate) (PHB) supplied by Goodfellow with $M_w=381$ kg mol⁻¹; $\bar{D} = 3.53$, were used as the polymer matrices. Chloroform, ACS grade, was purchased

from Fisher Scientific. Hydroxyapatite (Hap), $D_p \leq 200$ nm and 97% of purity, was obtained from Sigma-Aldrich.

2.2. Preparation of precursor solutions

Several dispersions with different n-Hap concentrations were prepared using chloroform as the liquid medium. The n-Hap was dispersed using an ultrasound bath (Cole-Parmer 8891) for 50 min. Once the dispersion process was finished, the polymer was added to the system in an amount corresponding to the established concentration. In the case of PDLLA, the solution was carried out under constant stirring for 22 h at room temperature, while for PHB the system was maintained at a temperature of 55 °C, during a stirring time which varied between 12-16 h.

The viscosities of the biopolyester solutions were determined using an Anton Paar rheometer, physical model MCR 301 with a cone-plate configuration (diameter 50 mm, angle of 2 ° and gap of 0.205) at 25 °C.

2.3. Centrifugal spinning process

The prepared solutions were subjected to a centrifugal spinning process in a Cyclone™ L-1000M (FiberRio Technology, Corp.), which consist of a cylindrical spinneret with two nozzles equipped with regular beveled needles (30-gauge length, Becton, Dickinson and Company) and 8 collectors in the form of metal bars arranged around the spinneret at a distance of 15 cm from the nozzles. For each run, 2 mL of polymer solution were added to the spinneret, and fiber spinning was carried out for 5 min at a temperature of $24.1 \text{ °C} \pm 1.5 \text{ °C}$ with a relative humidity of $54.3\% \pm 8.7\%$. It is important to mention that the fiber characterization in the optimization stage was determined from the fibers collected from a single run (5 min). Once proper parameters were established, the resultant mats were obtained by the collection of 7-runs (5 min each). The fibers were placed in a

vacuum oven at 30 °C for 24 h, to remove any residual solvent. Finally, the fibers were stored in plastic bags in the presence of a desiccant for moisture control.

2.4. Experimental design

Table 1 presents the precursor solution concentration and intervals of angular speed (ω) used in the production of the fiber-based mats.

Table 1.- Experimental conditions used during the centrifugal spinning process.

	C_p (wt %)	ω (rpm)	C_{Hap} (wt %)	Identification
PDLLA	10	6000-9000	5, 10, 15	PDLLA-Hap 5%
				PDLLA-Hap 10%
				PDLLA-Hap 15%
PHB	9			PHB-Hap 5%
				PHB-Hap 10%
				PHB-Hap 15%

* ω = angular speed, C_p = polymer concentration and C_{Hap} = Hap concentration

For the selection of the optimum ω , resultant fiber morphology, fiber diameter, and ultimate yield were considered. The yield/output of the process (η_p) was estimated by Equation 1.

$$\eta_p = \frac{M_{mf}}{ST} \times 100 \quad (1)$$

where M_{mf} and ST are the grams of fibers collected per run (5 min) and the total solids (polymer + NPs) contained in 2 mL of polymer solution, respectively.

2.5. Fibrous material characterization

The morphological analysis was carried out using a scanning electron microscope (Carl Zeiss, SigmaVP). The images obtained were analyzed with the Image J software (v. 1.48) to estimate

average fiber diameters ($\overline{D_f}$) and average pore size (interfibrillar spaces). Diameter distributions were obtained by measuring 100 fibers (20 fibers per micrograph) with three measurements per fiber, making a total of 300 measurements per sample. Obtained data was represented by means of box-bars charts, where the boxes reflect 50% of the population of values that located between quartile 1 ($Q_1 = 25\%$ of the population) and 3 ($Q_3 = 75\%$ of the population) and the bars represent the amplitude of the distribution according to the most probable values or those that appear more frequently.

The distribution and dispersion of the n-Hap within the fibers were determined using energy dispersive X-ray spectroscopy (EDS, EDAX Octane Super) and transmission electron microscopy (FEI, Titan 80-300).

For the calculation of the scaffold's porosity, an adjustment of the equation reported by Wang¹⁵ was used (Equation 2).

$$\phi = \left(1 - \frac{m}{Z \cdot A \cdot H \cdot \rho}\right) \cdot 100 \quad (2)$$

Where m , Z , A , H and ρ are the mass, thickness, width, and length of the scaffold and the density of the polymer with n-Hap in the corresponding case, respectively.

The thermal properties were evaluated through thermogravimetric analysis (TGA) (TA Instruments, Q400) and differential scanning calorimetry (DSC) (TA Instruments, Q200). To perform the TGA, the samples were heated from 30 °C to 600 °C under a nitrogen atmosphere, at a heating rate of 10 °C·min⁻¹. Regarding the DSC, the heating was carried out from -70 to 200 °C at a rate of 10 °C·min⁻¹, the samples were isothermally maintained at 200 °C for 2 minutes and then cooled down at the same rate to -70 °C. A second heating cycle under the same conditions was conducted. The crystallinity of the systems manufactured with PHB was determined using Equation 3:¹⁶

$$X_c = \frac{\Delta H_m}{\Delta H_m^\circ \times X_{PHB}} \times 100 \quad (3)$$

Where ΔH_m and ΔH_m° are the melting enthalpies of the PHB sample and a 100% crystalline PHB respectively, being $\Delta H_m^\circ = 146 \text{ J}\cdot\text{g}^{-1}$.¹⁷ The X_{PHB} is the PHB weight fraction in the sample.

The mechanical properties of the fibrous materials were determined by tensile tests using the universal testing machine (Tinius-Olsen, H10KS). The tensile testing was made using the paper frame method.^{18,19} To this end, test pieces of 30 mm long and 3 mm wide were cut and conditioned for 24 h at room temperature (23-25 °C). The tensile tests were carried out at a deformation speed of $2 \text{ mm}\cdot\text{min}^{-1}$ with a clamp separation of 27.5 mm, using a 50 N load cell (5 repetitions).

2.6. Cell viability test

Saos-2 (osteoblast like) cells were cultured in a flask with McCoy's culture media (Sigma, M4892-10X1L) containing $2.2\text{g}\cdot\text{L}^{-1}$ of NaHCO_3 , 15% of fetal bovine serum (Fisher Thermo Scientific, SH30396.03) and 1% of Penicillin-Streptomycin (Gibco, 15140-122). Culture media was changed after 24 h and then each 48 h until cell confluence. Third to fifth generation of cells were used to evaluate their interaction with the PDLLA or PHB surfaces. Cells were removed from the culture plates by rinsing in PBS and incubating in a trypsin solution. After trypsin inactivation, the cells were centrifuged for 5 min at 1200 rpm. The resulting pellet was resuspended in complete medium. 30000 cells in McCoy's culture media containing serum and penicillin-streptomycin were deposited on PDLLA and PHB samples of 1x1 cm, previously sterilized with UV light for 20 min, and incubated at 37 °C. After adhesion for the specified time, cells were rinsed with PBS in order to eliminate all the rests of culture medium. 300 mL of solution of resazurin (Aldrich, 1001140130) on culture medium (1:10) was then added to the samples and was allowed to react for 4 h. 150 μl were taken from each sample and fluorescence was measured at 570 nm using a spectrophotometer Elisa reader (BioRad mod.450).

3. Results and Discussion

3.1. Effect of n-Hap concentration on fiber formation

An optimization study was conducted for the PDLLA based systems using concentrations of n-Hap at 5, 10 and 15 wt % in an interval of ω between 5000 and 8000 rpm, in order to evaluate the influence of n-Hap on fiber formation (Figure S1, *Supplementary Information*). It was evidenced that the higher n-Hap concentration promotes the formation of defects within the fibers. This effect occurs more pronouncedly at 5000 rpm, whereas at a concentration of 15 wt % of n-Hap fibers exhibited a high level of ovoid defects. This fact produced a decrease in the amount of collectible material, affecting the process yield (η_p) ($\eta_p < 20\%$). The opposite occurred as ω increased, homogeneous fibers at a concentration of 5 wt % in the range of 7000 to 8000 rpm were obtained. In view of the difficulties presented with the incorporation of n-Hap, the criterion for selecting the best conditions was based on the fiber homogeneity and fiber yield. Therefore, the system obtained at 5 wt % of n-Hap and 7000 rpm was selected ($\eta_p = 67\%$, Q_1 - $Q_3 = 0.44$ - $1.70 \mu\text{m}$, $\bar{D}_f = 1.29 \pm 1.14 \mu\text{m}$) as one of the most suitable.

Figure 1 shows the influence of n-Hap concentration on fiber morphology and \bar{D}_f , it is compared to the system without n-Hap. Under the selected conditions, the incorporation of n-Hap did not have a pronounced effect on the material appearance, presenting a homogeneous morphology and a similar surface porosity. Regarding the \bar{D}_f values, the effect was more pronounced, at 5 wt % of n-Hap where a wider dispersion (0.10 to 3.58 μm) and an increase of \bar{D}_f from 1.03 to 1.29 μm was observed. This behavior was also observed by Morelli *et al.*¹ and Sanchez *et al.*⁹ The increase in the amplitude of the fiber diameter distribution could be related to the n-Hap particle diameter distribution. Although \bar{D}_p is around 44 nm, there is a small population with diameters ranging between 100 and 350 nm (Figure S2d, *Supplementary Information*), which could lead to the formation of thicker fibers.

The apparent viscosity of the polymer solutions was evaluated as a function of the shear rate with and without n-Hap (Figure 1d). As it can be observed, at 5wt % of n-Hap a decrease in viscosity was observed compared to the system without n-Hap.

The interaction among the Hap and PLA has been reported in several studies such as Neuendorf *et al.*²⁰ where they performed surface tension measurements to determine the work of adhesion between Hap and all stereochemical forms of PLA (-DL, -D and -L), they found that the adhesion strength between Hap and PDLLA (-DL) is 20% greater in comparison with the other stereochemical forms. The obtained value, 63 J/m², can be associated with physical bonding across the organic/inorganic interface. On the other hand, Zhou *et al.*²¹ reported the presence of hydrogen bond between the C=O group of the PDLLA and the OH groups present in the Hap. These studies, and taking into consideration that the size of the NPs (44.4 ± 36.3nm) is in the order of the radius of gyration of the polymer (30-40 nm),²² provide information to suggest that the incorporation of the n-Hap produced a conformational change in the polymer chains (the chains are adsorbed on the surface of the particles) leading to a lower proportion of free polymer chains interacting with the solvent.²³ This phenomenon could then explain the observed decrease in the viscosity for samples containing 5 wt % of n-Hap. Additionally, this particle-polymer interaction provides a faster rate of solvent evaporation during the fiber formation process therefore leading to larger fiber diameters.

In the case of PHB, the interval of ω selected for the optimization study was 6000-9000 rpm at the same n-Hap concentrations evaluated for the PDLLA systems (Figure S3, *Supplementary Information*). In contrast to the latter, the formation of mostly homogeneous fibers was presented in the selected interval. Considering the obtained results, it could be established that the best angular speed for the manufacture of PHB scaffolds is 6000 rpm. The developed systems present a narrower diameter distribution and a higher fiber yield (Figure S4, *Supplementary Information*) ($\eta_p > 70\%$, Q₁-Q₃ for 5, 10 and 15 wt % of n-Hap are 1.27-2.40, 1.07-1.74, 1.02-1.78 μm , and the corresponding \overline{D}_f are 1.96 ± 0.87, 1.44 ± 0.46, 1.44 ± 0.59 μm , respectively).

Figure 2 shows the effect of n-Hap concentration on the morphology and fiber diameter distribution for the PHB systems. The micrographs show small protrusions exclusively at 10 and 15 wt % of n-Hap, which could be associated with the formation of agglomerates, in a similar way to what was observed by Ramier *et al.*⁷ in electrospun fibers. On the other hand, at a concentration of 5 wt % of n-Hap, an increase in the Q_1 - Q_3 interval diameter and its dispersion was observed, in comparison with the system obtained without n-Hap, reflecting an increase of 0.92-1.76 μm to 1.27-2.40 μm . On the contrary, at 10 and 15 wt % there was a decrease in fiber diameter, maintaining a similar range to that of the reference system.

Based on the apparent viscosity of the polymer solutions (Figure 2f), PHB solutions showed an increase in viscosity for samples containing 10 wt % of n-Hap, while at 15 wt % a slight decrease was observed possibly due to the presence of agglomerates which prevented particle-polymer interaction. When the viscosity increases, the resistance to elongate the polymeric solution increases as well; therefore resulting in fibers with a larger diameter for the same angular speed.^{24,25} The results at 5 wt % of n-Hap described in the previous paragraph presented an increase in the \overline{D}_f . In the case of 10 and 15 wt % of n-Hap, the big agglomerates presence may have had an additional effect on fiber diameter. Due to the agglomerates the well dispersed concentration of n-Hap in the precursor solution is less than the initially established concentration. Consequently, the results of the fiber diameters will not necessarily reflect the expected influence with the increase in n-Hap concentration. The agglomerates were observed to act as thinning points resulting in fibers of smaller diameters.

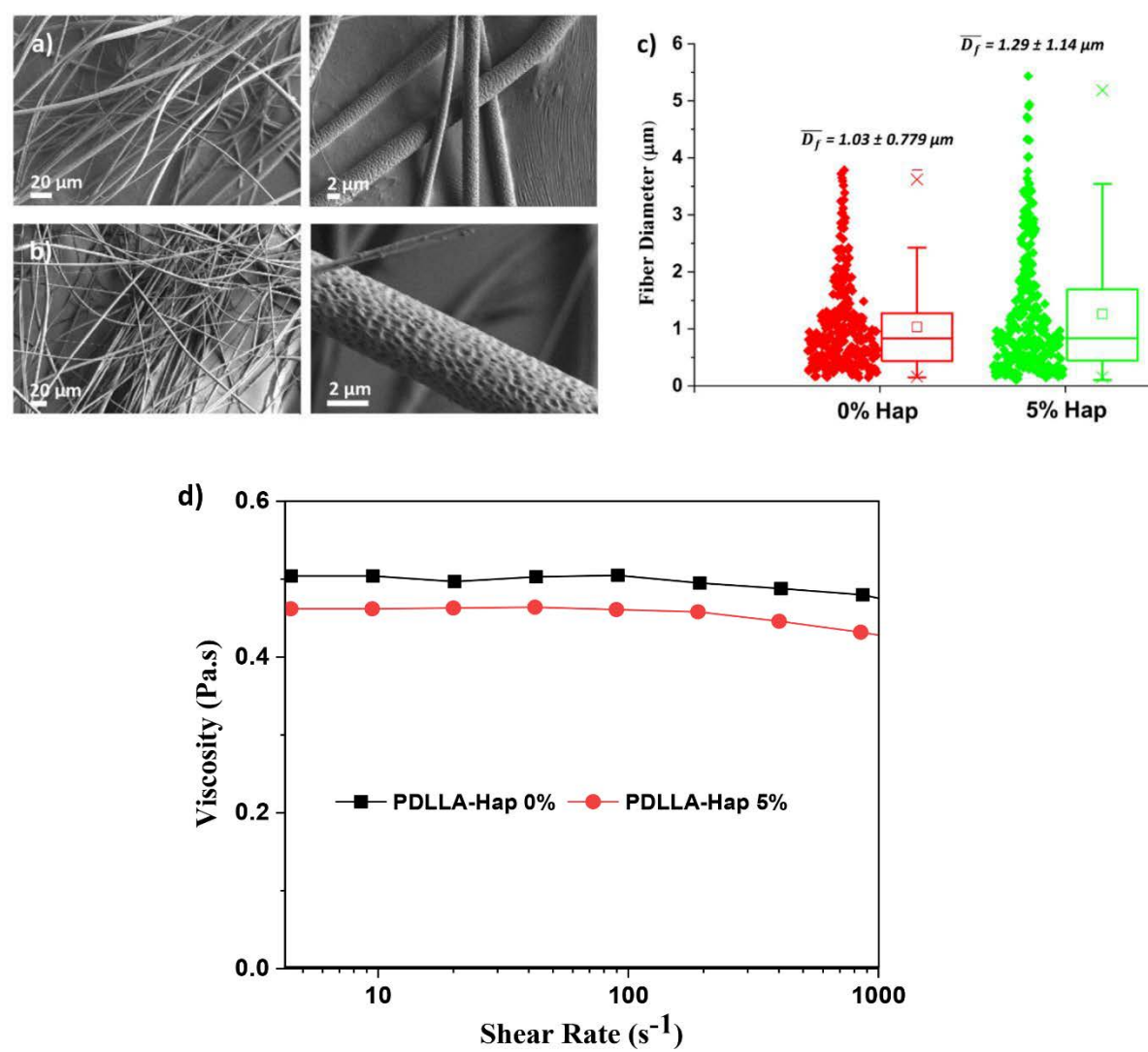


Figure 1. SEM images of PDLLA systems at 0 wt % (a) and 5 wt % (b) of n-Hap obtained at ω of 7000 rpm, box charts of fiber diameters for each system (c) and rheological behavior of PDLLA solutions at 0 and 5 wt % of n-Hap (d).

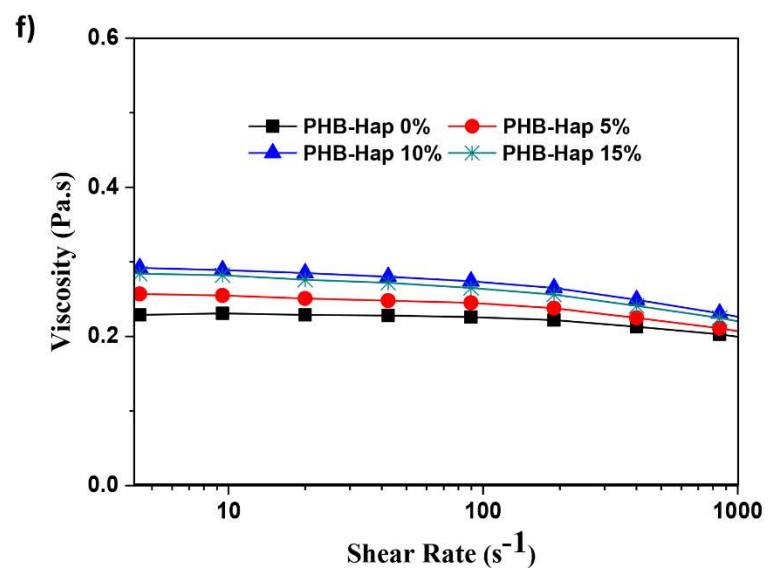
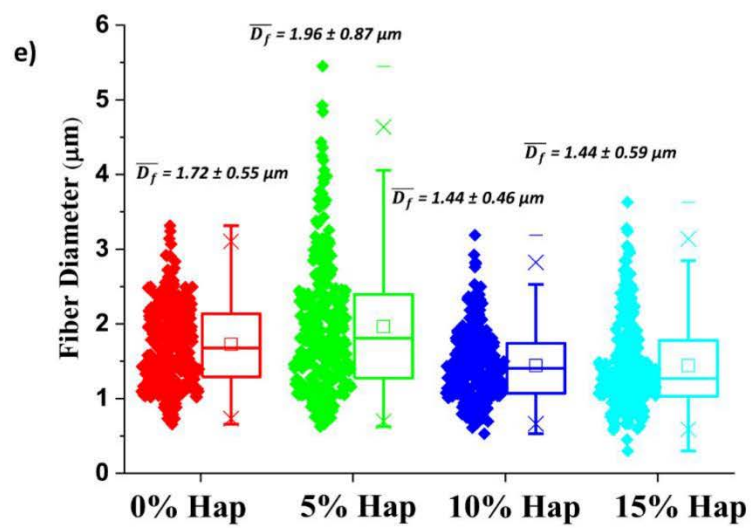
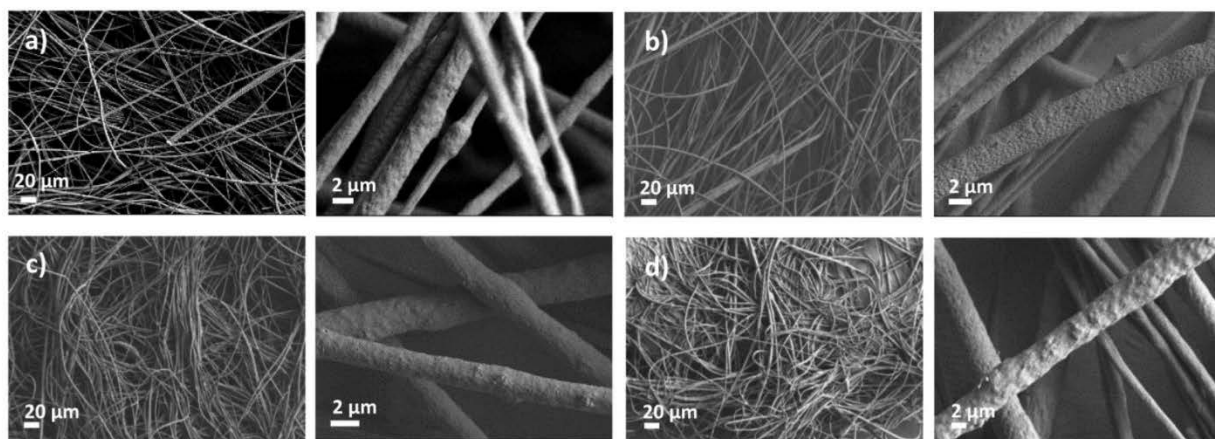


Figure 2.- SEM images of PHB systems at 0 wt % (a), 5 wt % (b), 10 wt % (c) and 15 wt % (d) of n-Hap obtained at ω of 6000 rpm, box charts of fiber diameters for each system (e) and rheological behavior of PHB solutions at 0, 5, 10 and 15 wt % of n-Hap (d).

3.2. Morphological characteristics of the designed hybrid materials

3.2.1. Centrifugally spun PDLA-Hap materials

The images of the materials obtained under the conditions selected in the optimization stage are presented in Figure 3. The fibers mostly show a homogeneous appearance over their entire length (Figures 3a and b). The diameters dispersion was wider and shifted towards larger diameters (0.29-4.69 μm) when compared to the optimized system (0.10-3.58 μm). Regarding the n-Hap distribution, the presence of phosphorus was observed throughout the analyzed area (green dots in Figure 3d), indicative of a good distribution of the nanoparticles. The dispersion of the NPs was moderate, with some agglomerates along the fiber (Figure 3e). In addition, Figure 3g shows that n-Hap is mostly embedded within the fibers, probably due to its interaction with the polymer (see previous section), and as such preventing nanoparticles from transferring out of the matrix. A similar behavior was reported by Rizzi *et al.*²⁶, where under the same procedure of incorporating n-Hap into polymeric films based on polycaprolactone (PCL) and PLLA, NPs were observed to be embedded in the PLLA films, which evidences the presence of strong interactions between n-Hap and the polymer.

Additionally, fibers show a rough surface along the entire length. This roughness occurs mainly when a very volatile solvent (in this case, CHCl_3) is used for the preparation of the precursor solution, in combination with the fiber production in a relatively high atmospheric humidity (54.3% \pm 8.7%).²⁷⁻²⁹ Although the aforementioned variables are highly relevant to the surface appearance of the fibers, there are other factors such as solvent interaction with atmospheric water, water diffusion coefficient, and solubility parameters that also play key roles in surface morphology.³⁰

The scaffold's porosity is above 90%, similar to fibers developed in our previously reported work.^{31,32} Figure S5, *Supplementary Information*, shows the estimated scaffold pore sizes (spaces

between fibers), specifically the 50% of the population which has an area above $30.52 \mu\text{m}^2$ with most of the distribution in the 5 to $200 \mu\text{m}^2$ range. These results pose promising potential for applications in tissue engineering.^{33,34}

3.2.2. Centrifugally spun PHB-Hap materials

Figure 4 shows the morphological characteristics of the PHB materials containing 5, 10 and 15 wt % of n-Hap, obtained at 6000 rpm. The fibers showed the expected behavior based on the previously performed morphological analysis; that is, mostly homogeneous fibers with a rough surface. The fiber diameter dispersion (Figures 4c, f, i) exhibited intervals similar to those observed in the optimization phase. However, in this case, the Q_1 - Q_3 interval did not show significant variations between the systems, ranging from 1.2 to $2.3 \mu\text{m}$.

Regarding the scaffolds' porosity, the values ranged from 93 to 96% (Figures 4c, f and i), while 50% of the pore population have an area above $31.8 \pm 8 \mu\text{m}^2$ and most of the population is distributed in a range from 2 to $200 \mu\text{m}^2$ (Figure S6, *Supplementary Information*). In Figures 5a, d and g, the presence of phosphorus in the samples is shown. Through these images, a good distribution of the n-Hap is evidenced with agglomeration points that vary as n-Hap concentration increases. These results are consistent with those observed in the TEM images (Figures 5b, e and h), and the particles are mostly embedded within the fibers (Figures 5c, f and i).

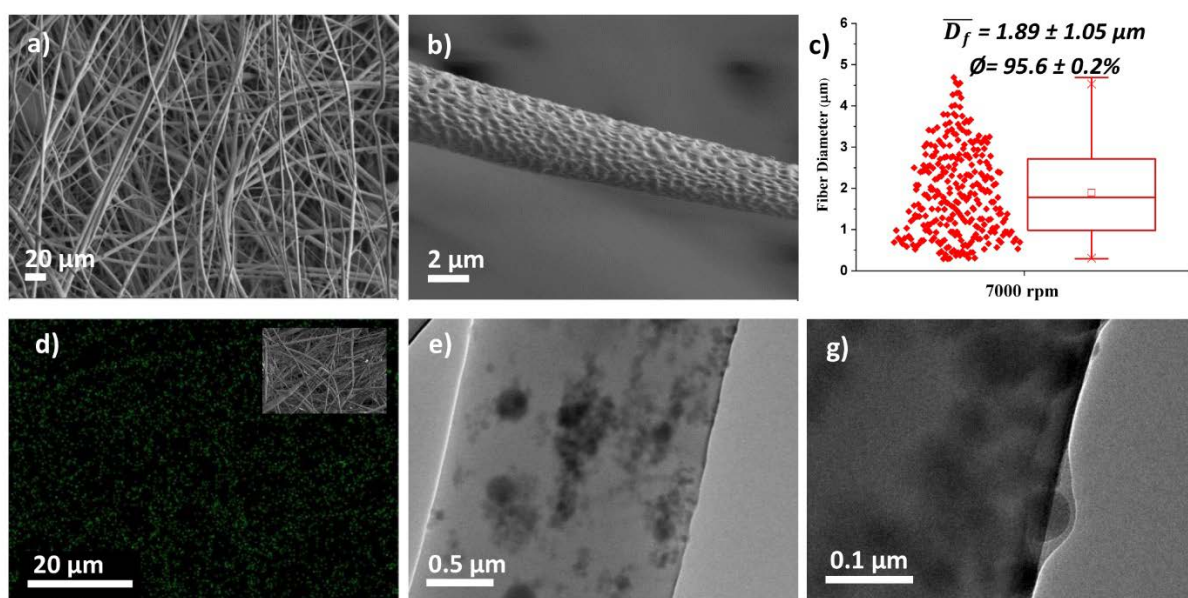


Figure 3. SEM images (a, b and d), TEM (f, g), box chart of fiber diameter (c) and mapping of element phosphorous obtained through EDS of PDLLA-Hap 5% system produced at ω 7000 rpm.

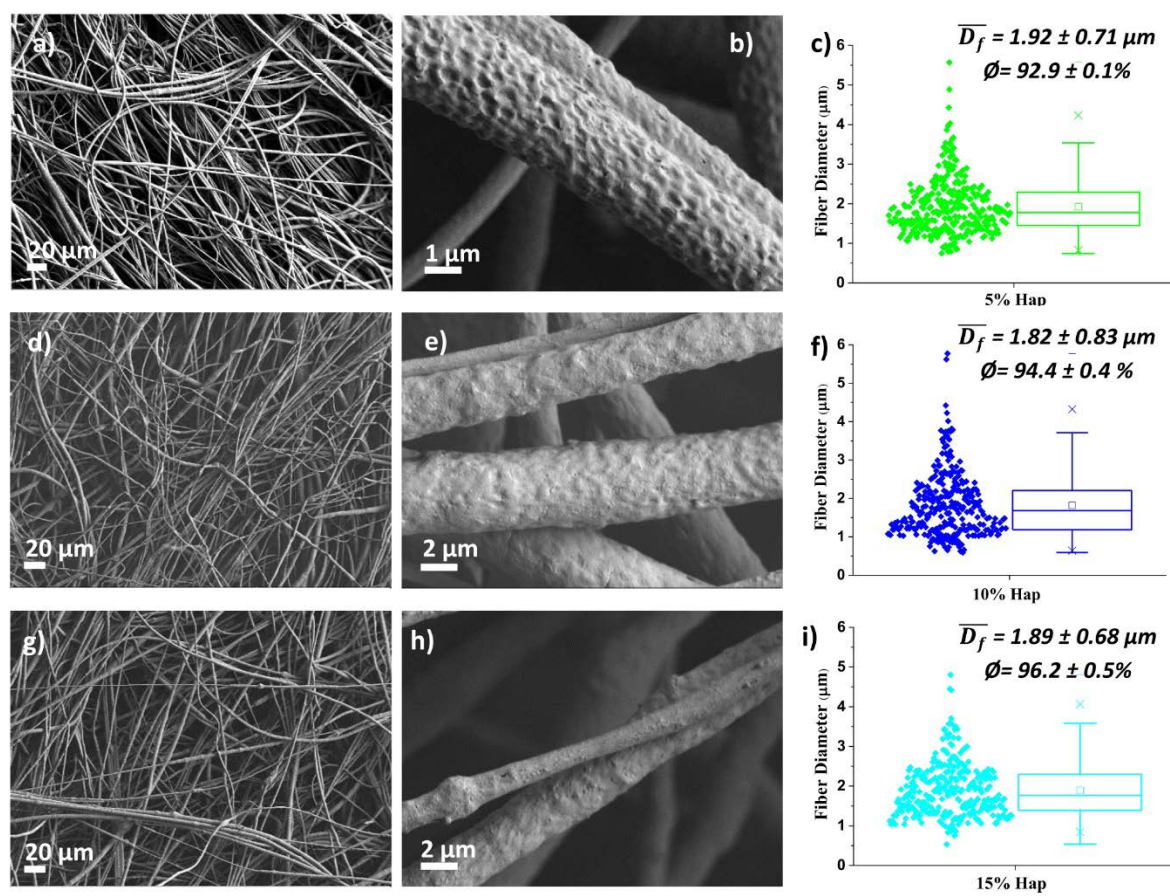


Figure 4.- SEM images (a, b, d, e, g, h) of PHB systems at 5 wt % (upper images), 10 wt % (middle images) and 15 wt % (lower images) of n-Hap, box charts of fiber diameters and their respective porosity (\emptyset) (c, f, i).

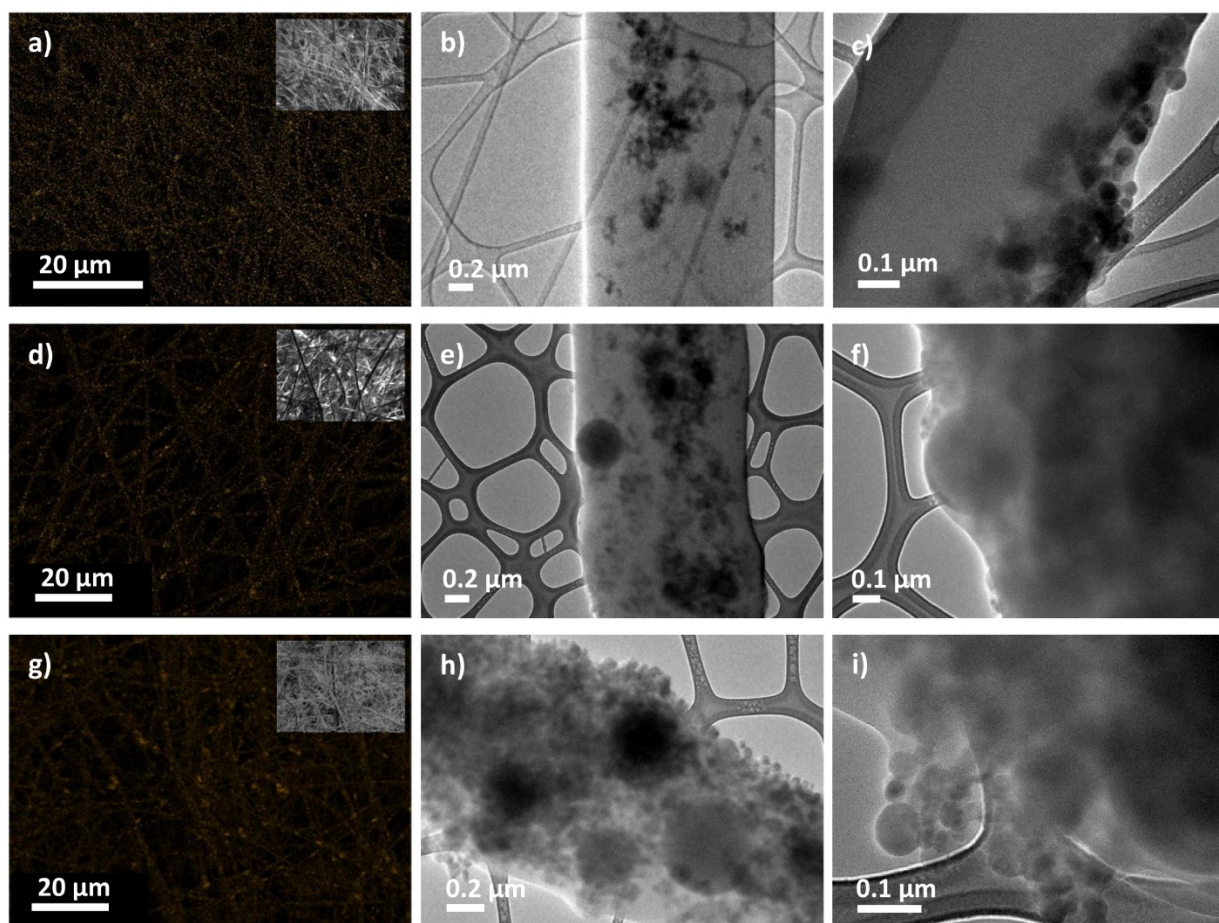


Figure 5.- Elemental mapping of phosphorous (a, b, g) and TEM images (d, c, e, f, h, i) of PHB systems at 5 wt % (upper images), 10 wt % (middle images) and 15 wt % (lower images) of n-Hap.

3.3. Thermal properties

From the thermo-degradation patterns of the scaffolds formulated with PDLLA (Figure 6a) and PHB (Figure 6b) at different n-Hap concentrations and at ω of 7000 and 6000 rpm, respectively, it was shown that the residues after heat treatment correspond to the theoretical concentration of n-Hap. Regarding the degradation of the materials, and taking into account the temperature at which the degradation rate reaches its maximum value (T_d) obtained by the derivative of the thermogram, it can be observed that the n-Hap did not produce a significant decrease in the thermal

stability of the materials. In the case of PDLLA, a T_d of 369 and 349 °C was obtained at 0 and 5% of n-Hap; respectively. On the other hand, the systems formulated with PHB showed a T_d of 272, 262, 262 and 260 °C at 0, 5, 10 and 15wt % n-Hap, respectively. This behavior could be attributed to the hydroxyl groups of the Hap that act as a catalyst in the decomposition reaction of the polymer.³⁵

Figure 7a shows the DSC thermograms of a heating-cooling-heating cycle of the PDLLA based scaffolds. In relation to the reference system (without n-Hap), in the first heating cycle an endothermic transition is observed at 62.5 °C with a relaxation enthalpy of 7,517 J·g⁻¹, which occurs followed by the glass transition temperature (T_g) of the PDLLA (51.2 °C) (Figure S7, *Supplementary Information*). This behavior denotes the presence of a certain order of the polymer chains formed by the uniaxial stretching experienced by the polymeric fluid in the spinning process, a characteristic that had already been observed in previously published articles.^{31,36,37} A similar behavior was observed at 5 wt % of n-Hap, but in this case the endothermic peak occurred at a higher temperature (63.3 °C) and enthalpy of relaxation (8.55 J·g⁻¹), which evidences some NPs-polymeric matrix interaction. On the other hand, during cooling and second heating, there was only a second order transition (T_g) typical of an amorphous polymer, as expected.

In the case of PHB systems (Figure 7b) during the first heating cycle similar transitions are observed in systems with and without n-Hap, with negligible modifications to the melting temperatures. PHB is composed of 95% poly(3-hydroxybutyrate) (3-PHB), 4% poly(4-hydroxybutyrate) (4-PHB) and 1% polyhydroxyvalerate (3-PHV), therefore, in the first heating two endothermic peaks at 48 °C and 170 °C are identified, corresponding to the melting of the 4-PHB and 3-PHB crystalline phases, respectively.³² Regarding the percentage of polymer crystallinity (X_c), the n-Hap caused a slight increase in X_c at a concentration of 5 wt % and from 10 wt % (with a greater impact to 15wt %) a decrease was observed, being 47.4, 49.2, 43.0 and 40.0% for 0, 5, 10 and 15 wt % of n-Hap, respectively. In the cooling stage, a reduction in temperature and enthalpy of crystallization was evidenced by increasing the n-Hap concentration,

similar to that described by Sánchez-Arévalo *et al.*⁹ This behavior indicates that NPs are slowing the polymer crystallization process, possibly due to their interference during the packing of polymer chains.

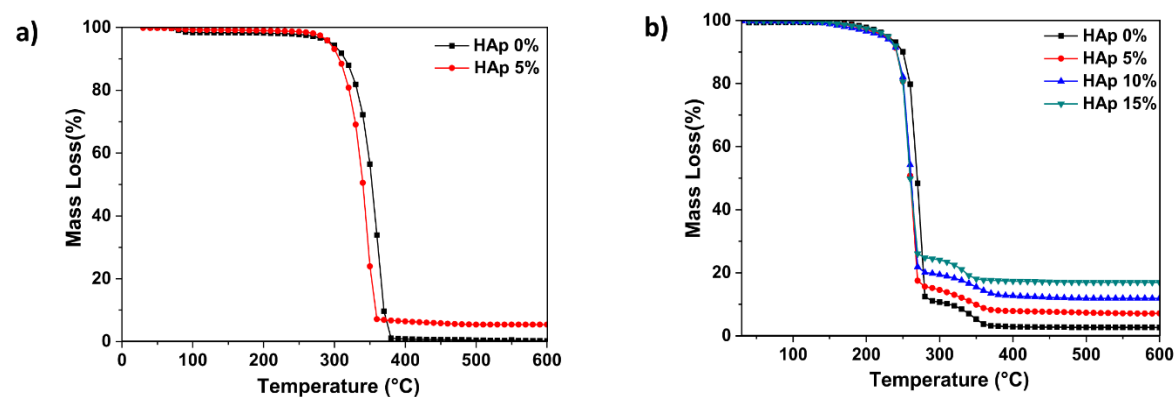


Figure 6. Degradation patterns derived from TGA of the centrifugally spun PDLLA (a) and PHB fibers (b) obtained at different concentrations of n-Hap.

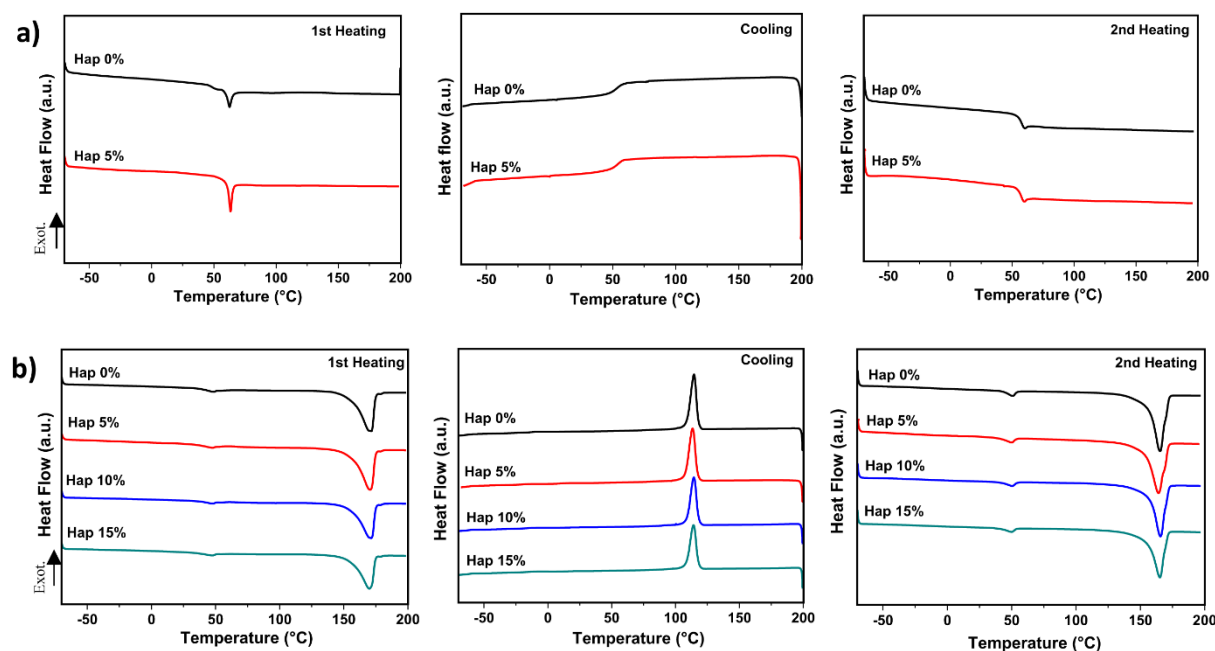


Figure 7. DSC thermograms derived from one cycle of heating-cooling-heating of PDLLA a) and PHB b) fibrous mats at different concentration of n-Hap.

3.4. Mechanical properties

Figure 8 shows the stress-strain curves obtained from PDLLA and PHB control and hybrid systems; the Young's modulus and the tensile strength are also shown. The fiber mats presented a linear elastic behavior in the first phase of deformation (elongation) and a maximum stress values before yielding at an elongation less than 10% and 20% for the PDLLA and PHB, respectively.

The selected fiber production method and chosen parameters significantly influence fiber orientation, polymer chain orientation, crystallinity, distribution of nanoparticles, as well as possible slipping between fibers, all of these factors then have an influence on the mechanical performance of the mats.^{38,39} In the case of the PDLLA, a significant decrease in the Young's modulus and tensile strength with the incorporation of n-Hap was observed, specifically the percentage of reduction was 66.6 and 68.7 %, respectively. Other studies have reported similar results using different concentrations of n-Hap;^{1,8,9} however, Gang Sui *et al.*,⁴⁰ reported an opposite result, adjudicating the behavior to the formation of strong surface bonding between the n-Hap and the polymer. In the case of PHB, the mechanical performance improved as the n-Hap concentration increased. Nevertheless, the decrease in the tensile strength presented at 15% could be due to the formation of n-Hap agglomerates that eventually acted as sites for crack propagation. In spite of this behavior, the tensile strength at 15% was higher than that one obtained without n-Hap. Ramier *et al.*⁴¹ also observed an increase in the mechanical properties of hybrid fibrous mats obtained by the electrospinning technique.

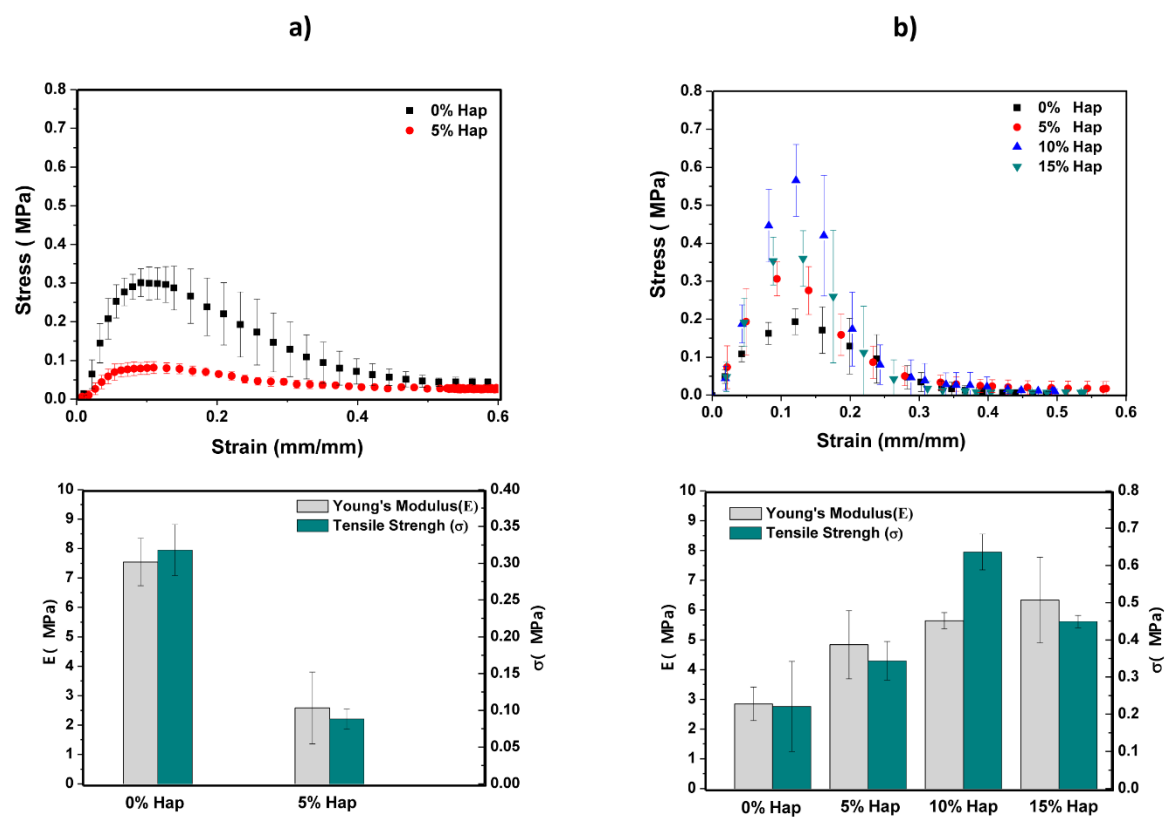


Figure 8. Stress-strain curves, Young's modulus (E) and tensile strength (σ) of the fiber mats obtained with PDLLA (a) and PHB (b) at different n-Hap concentrations.

3.5. Cell viability

Cell viability is a measure of the cell metabolic activity. The test was carried out through the fluorescence emitted by a redox indicator, known as resazurin, which is effectively reduced in cells mitochondria producing resorufin. This final product is excreted to the culture medium, making it a source to evaluate the cell mitochondrial metabolic activity.

It is important to highlight that for this test, only the systems obtained at 5% n-Hap and their corresponding references were evaluated for comparative purposes. In Figure 9, the influence of the designed materials on the behavior of Saos-2 (Osteoblast-like) cells can be observed. Regarding the polymer type, it is clear that PDLLA produced a better cellular response than PHB,

with a cell viability of around 60%. On the other hand, PDLLA-Hap 5% system promoted an increase of 10% in cell viability by day 7. The observed behavior could be attributed to the NPs disposition on the material, as they are mostly embedded in the fibers, avoiding the NPs direct interaction with the cells at first and third day of experimentation. With regard to the seventh day, it is likely that surface erosion (hydrolytic degradation)²⁷ of the fibers produced the exposure of a greater number of NPs, causing an increase in the cell metabolic activity. In addition, different authors have reported that n-Hap promote the superficial mineralization of apatite;^{42,43} which could have had an effect on the final result. In the case of PHB-Hap 5%, no significant changes in cell viability were observed when compared to the PHB without n-Hap. The decreased viability with days of interaction could indicate the presence of a certain cytotoxic effect in the cells. Different works have reported similar results regarding the lack of n-Hap effect on the viability and proliferation of osteoblast cells, while its influence on other mechanisms that allow its osteogenic evaluation in different cell lines, have shown a notable positive effect.^{6,8,40,41,44}

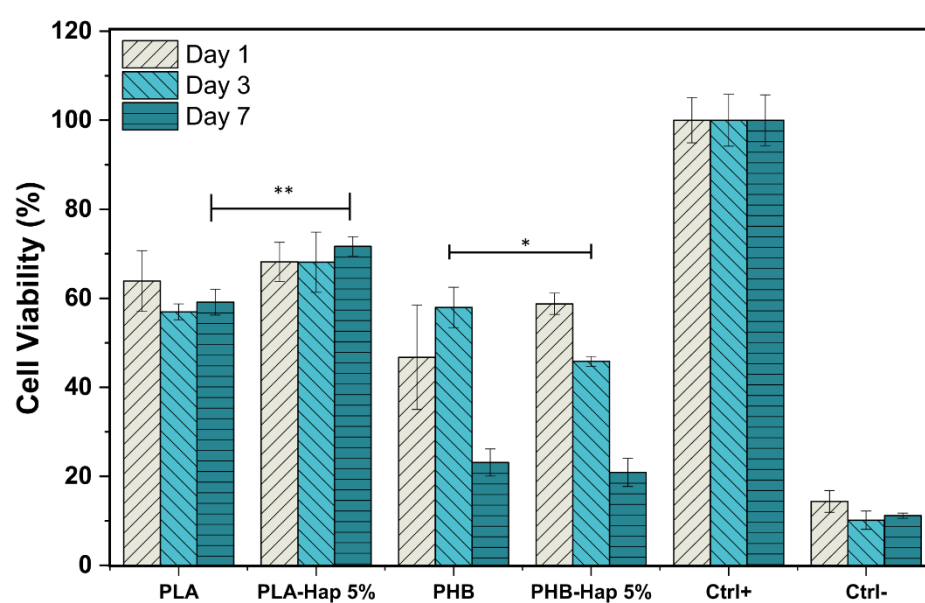


Figure 9. Osteoblast cell viability evaluated through days 1, 3, and 7 with resazurin. A statistical analysis is shown measuring the standard deviation of the mean, n= 3 trial experiment (* p <0.05, ** p <0.01).

4. Conclusions

PHB showed greater versatility for the production of homogeneous fibers at different n-Hap concentrations (5, 10 and 15 wt %) compared to PDLA (5 wt %). The hybrid systems obtained presented rough surfaces, and thermal stability similar to those of fibrous materials without n-Hap. In addition, n-Hap acted as a reinforcement for PHB systems, in which a better mechanical performance was observed at a concentration of 10 wt %; the contrary occurred in the PDLA based systems. Regarding cell viability, PDLA systems promoted higher cellular response than those formulated with PHB. Moreover, for PDLA systems, the incorporation of n-Hap produced a significant difference in the metabolic activity of Saos-2 cells by day seven of the assay. On the other hand, no significant changes were observed in PHB systems.

5. Acknowledgments

The authors thank CONACyT for the scholarship granted (429352) to Victoria Padilla Gainza, and for the support received by the National Science Foundation (NSF DMR 1523577). The authors also thank Anabel Ochoa, Alejandro Castillo, and Jesús G. Quiroz López for their technical assistance related to the evaluation of thermal properties, images by SEM and mechanical properties, respectively.

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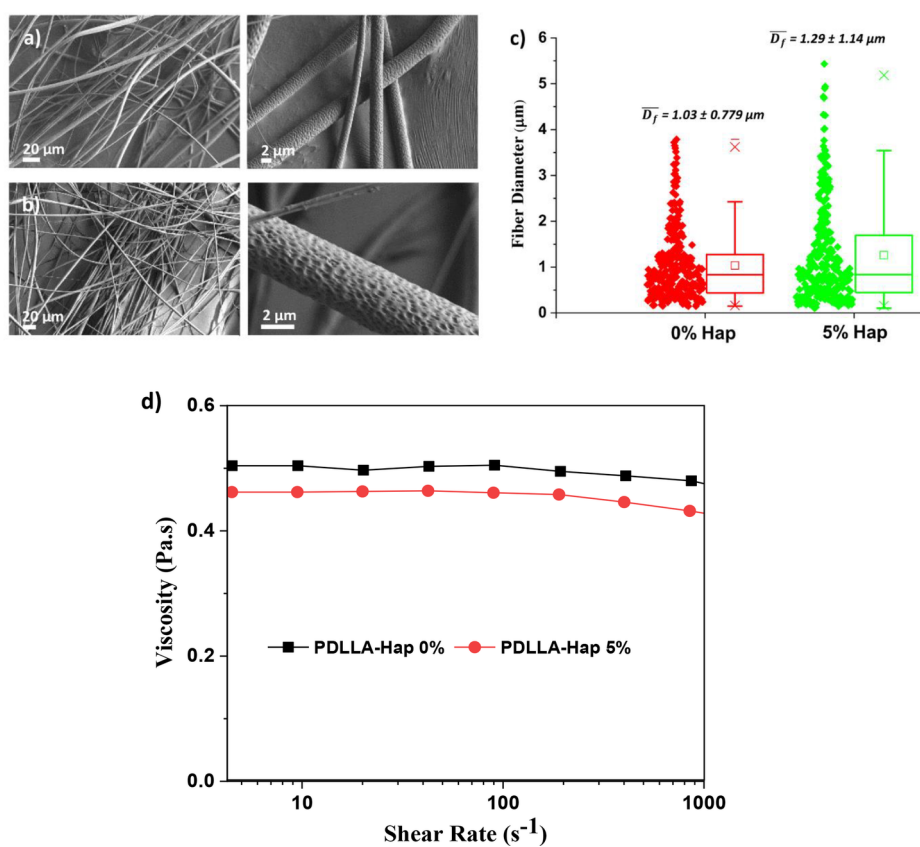
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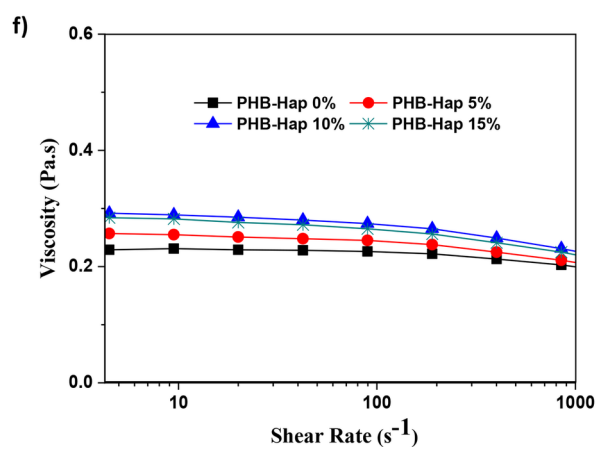
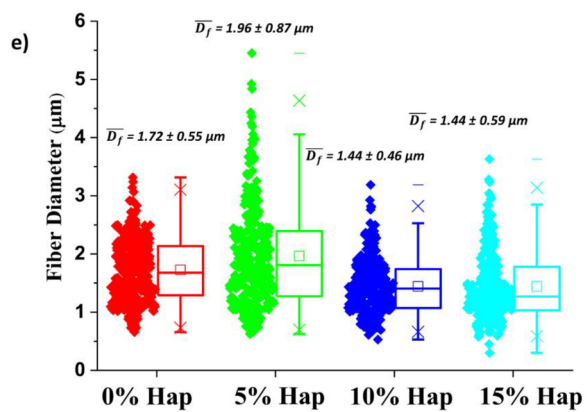
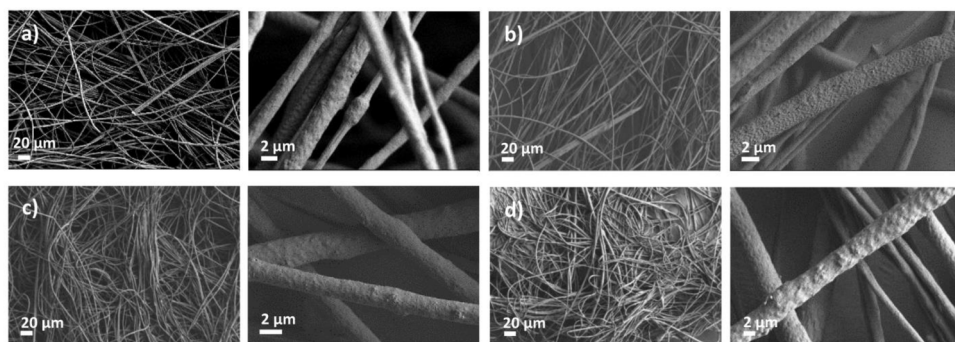
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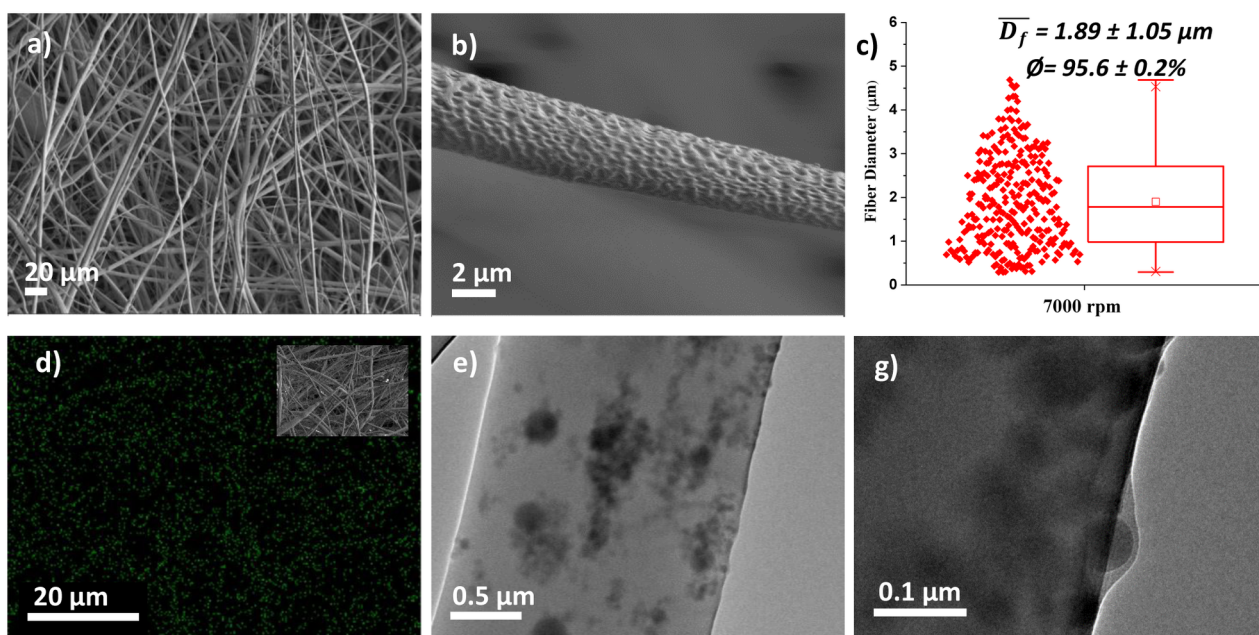
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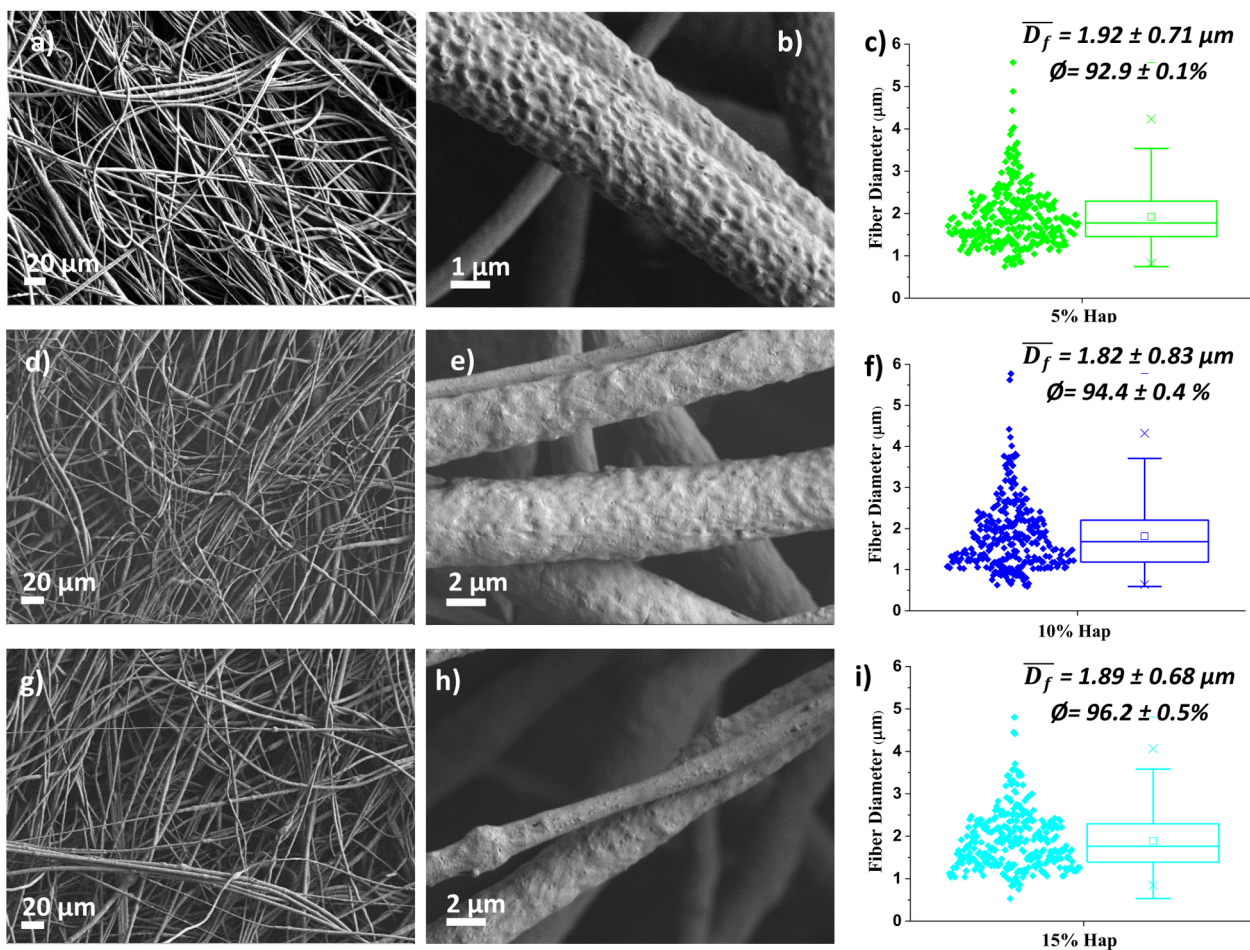
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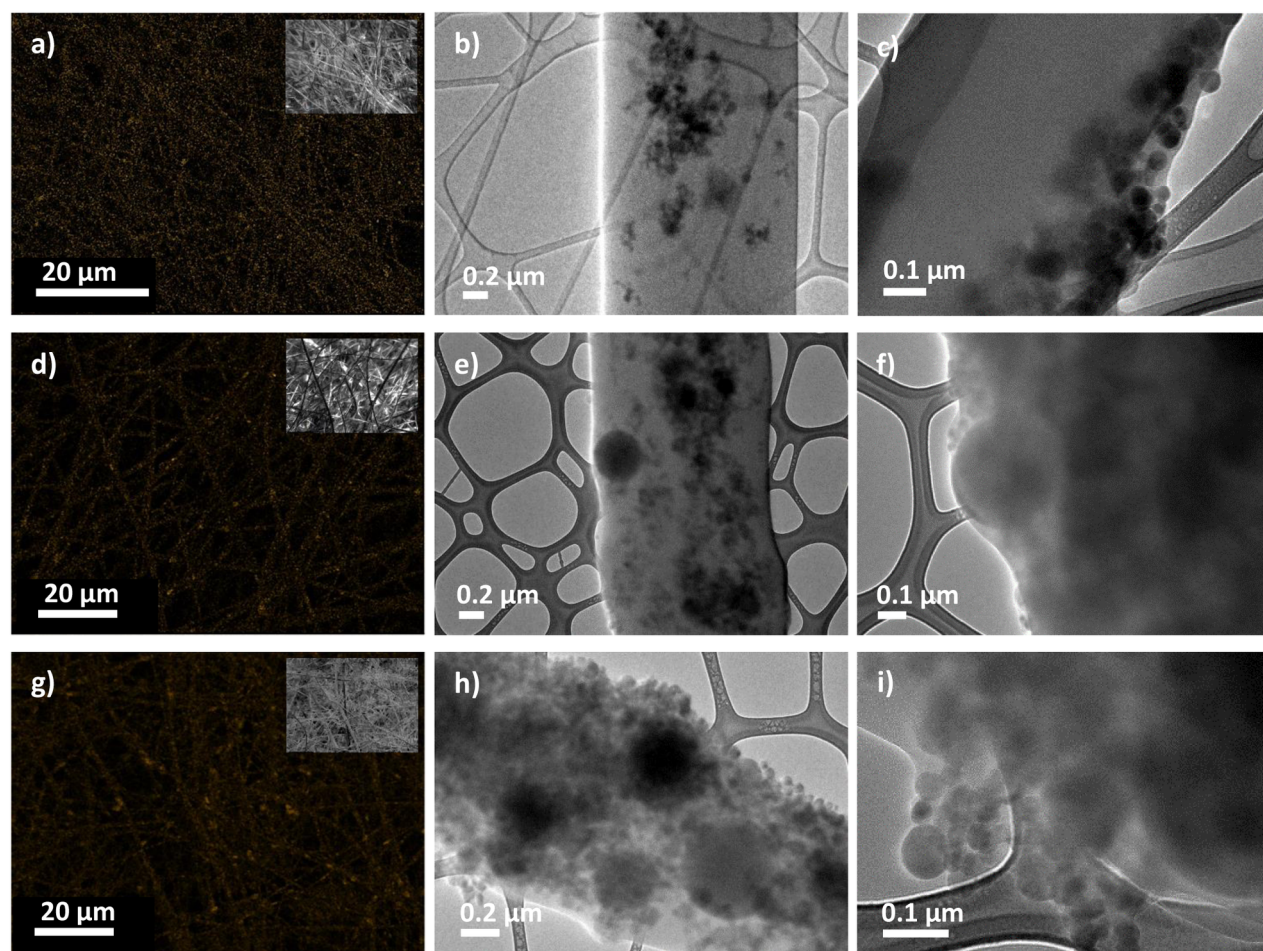
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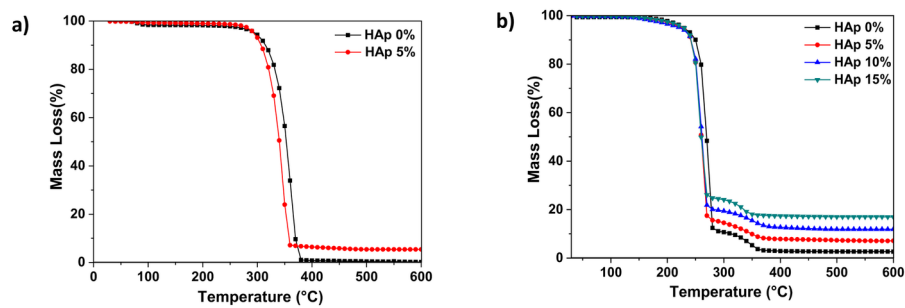
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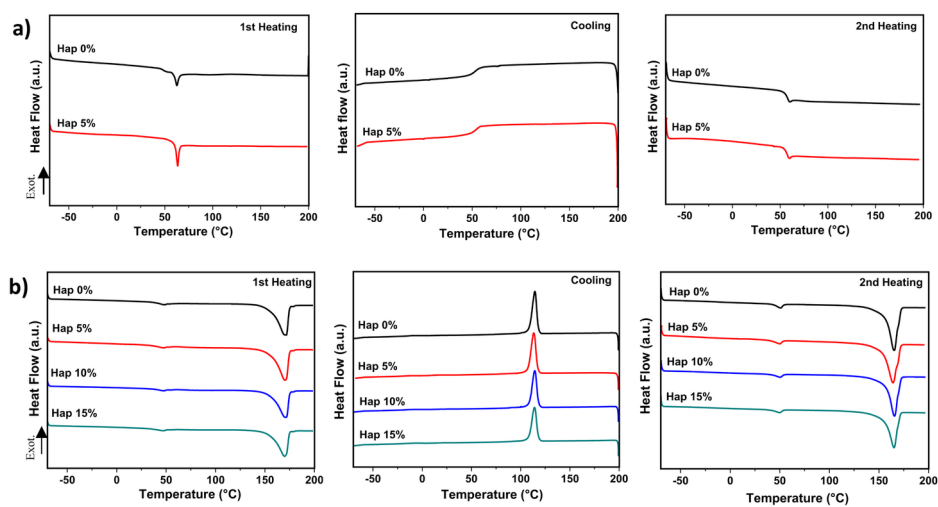
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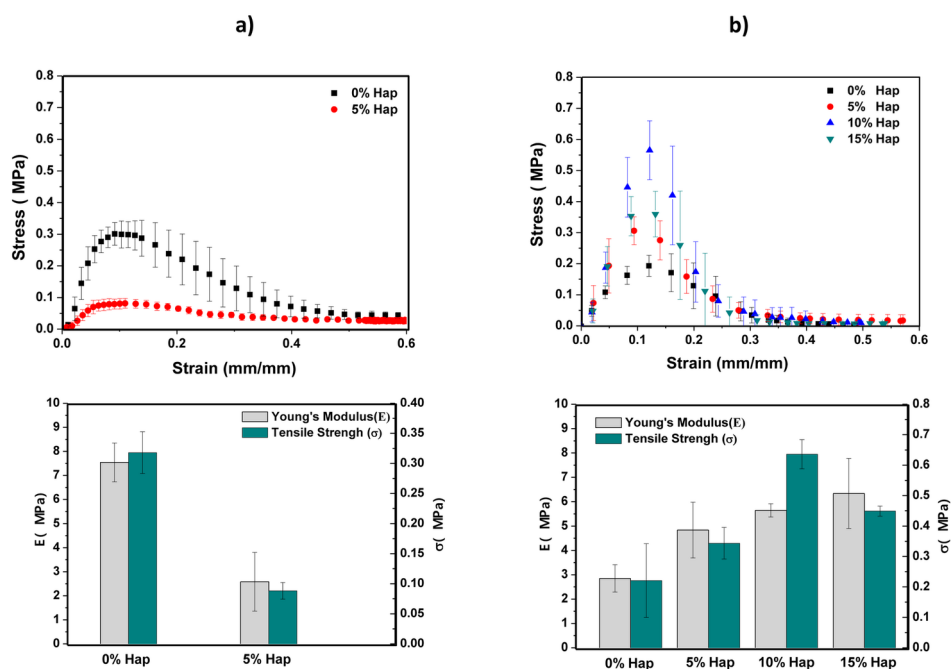
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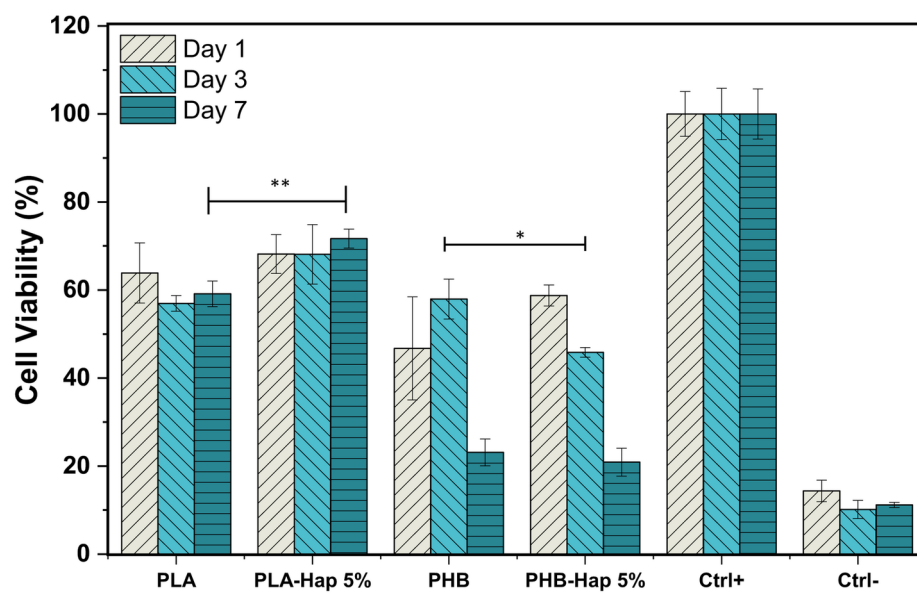
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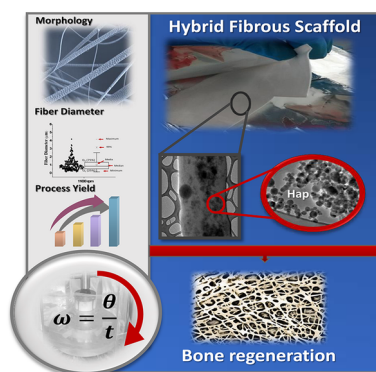
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