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The Resin Bond to High-Translucent Zirconia—A Systematic Review

Abstract

Objectives: Several systematic literature reviews have assessed the scientific evidence on resin bonding protocols to conventional 3 mol% yttria-stabilized zirconia (3Y-TZP) ceramics. It has been widely discussed, however, that the differing composition and physical properties of new high-translucent zirconia generations (4Y-TZP and 5Y-TZP) may require alternative bonding materials and procedures. This paper reviewed in vitro studies on the success and durability of bonding protocols to high-translucent zirconia. **Material and methods:** A systematic search of PubMed and Cochrane Library for in vitro studies on bonding to new zirconia generations published until November 2020 was conducted and complemented by a manual search. Studies selected for review fulfilled the applied inclusion and exclusion criteria. The quality of the included studies was assessed with the Cochrane risk-of-bias tool for randomized trials. **Results:** Of 629 screened articles, 18 were included in this review. They investigated different surface pretreatment methods, primers, resin cements, aging procedures, and bond strength test protocols. The limited number of the identified studies and the heterogeneity of the extracted data did not allow to conduct a meta-analysis. **Conclusions:** The available evidence suggests that resin bonding protocols successfully applied to conventional zirconia are also the most successful for high-translucent zirconia. Airborne particle abrasion and special phosphate monomer-containing primers or composite resin cements provide long-term durable resin bonds. **Clinical significance:** Durable bonds can be established between high-translucent zirconia and resin cements. The bonding materials and procedures applied do not compromise their physical properties. © 2022 Wiley Periodicals LLC.

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The resin bond to high-translucent zirconia—A systematic review

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Abstract

Objectives: Several systematic literature reviews have assessed the scientific evidence on resin bonding protocols to conventional 3 mol% yttria-stabilized zirconia (3Y-TZP) ceramics. It has been widely discussed, however, that the differing composition and physical properties of new high-translucent zirconia generations (4Y-TZP and 5Y-TZP) may require alternative bonding materials and procedures. This paper reviewed *in vitro* studies on the success and durability of bonding protocols to high-translucent zirconia.

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Results: Of 629 screened articles, 18 were included in this review. They investigated different surface pretreatment methods, primers, resin cements, aging procedures, and bond strength test protocols. The limited number of the identified studies and the heterogeneity of the extracted data did not allow to conduct a meta-analysis.

Conclusions: The available evidence suggests that resin bonding protocols successfully applied to conventional zirconia are also the most successful for high-translucent zirconia. Airborne particle abrasion and special phosphate monomer-containing primers or composite resin cements provide long-term durable resin bonds.

Clinical significance: Durable bonds can be established between high-translucent zirconia and resin cements. The bonding materials and procedures applied do not compromise their physical properties.

KEYWORDS

bonding, bonding protocols, *in vitro*, resin cements, translucent zirconia

1 | INTRODUCTION

Yttria-stabilized zirconium dioxide ceramics (Y-TZP or zirconia) have been increasingly used as an alternative to porcelain-fused-to-metal (PFM) restorations in daily dental practice, first as coping and framework materials to be veneered with layering porcelain and later to fabricate full-contour monolithic restorations.^{1,2} The rapid shift to

zirconia for all-ceramic restorations was due to their superior mechanical and biological properties,^{3,4} high-clinical success,^{5,6} accurate milling process,^{7,8} low-wear behavior of the antagonist dentition,^{9,10} and low material as well as fabrication costs.^{2,11} Zirconia is a polymorphic material that exists in several phases depending on the applied temperature.¹² The monoclinic phase is stable from room temperature to 1170°C, tetragonal at 1170–2370°C, and cubic over 2370°C.^{13,14}

Phase transformation from tetragonal to monoclinic goes along with a volumetric particle increase of approximately 4–5%.¹⁵ This phenomenon proves advantageous to limit crack propagation, also referred to as “transformation toughening.” Spontaneous transformation can be prevented by stabilizing the tetragonal phase at room temperature by adding certain oxides such as yttria, leading to high-fracture toughness.^{16–18}

The yttria content in zirconia largely defines its mechanical and optical properties. Different generations of zirconia can be classified according to their yttria content (mol%). The first generation contains 3 mol% yttria, known as 3Y-TZP or conventional zirconia. 3Y-TZP is partially stabilized in the tetragonal phase and has the highest fracture toughness and flexural strength among other generations.^{19,20} It is preferred for long-span fixed dental prostheses and in posterior areas with high-occlusal loads.^{21,22} However, due to its high opacity and compromised esthetic appearance, 3Y-TZP is predominantly used as a supporting coping and framework structure for bilayer all-ceramic restorations.^{23–25}

New generations of zirconia were developed to enhance esthetics appearance by increasing the yttria content to 4 and 5 mol% and apply them for full-contour monolithic restorations.²⁶ These generations contain approximately 30% to 50% cubic phase particles, which makes them more translucent and less susceptible to low-temperature degradation compared to conventional 3Y-TZP.^{27,28} Transformation toughening, key factor for the superior flexural strength, does not occur with these compositions. The reduced fracture toughness and flexural strength limits their clinical indication to single unit, partial coverage, and short-span fixed dental restorations in areas of limited occlusal load.^{26,29,30}

As with all brittle ceramic materials, resin bonding does not only provide adhesion of indirect ceramic restorations to teeth but also increases their flexural strength. This is especially true for silica-based ceramics and lower strength zirconia compositions with limited thickness. Conventional bonding protocols (i.e., hydrofluoric acid etching and silane coupling agents) applied to glass ceramics do not provide a durable chemical and micromechanical resin bonds to zirconia.^{31,32} Different mechanical, chemical, and combined chemical-mechanical surface pretreatment methods have been found to improve the zirconia-resin bonding.³³ These include airborne-particle abrasion (APA), tribochemical silica airborne-particle abrasion (TBS), low-fusion porcelain application, hot chemical etching solutions, selective infiltration etching (SIE), laser irradiation, plasma spraying, and zirconia ceramic powder coating.^{31,33–35}

Surface pretreatment methods aim to improve mechanical and chemical bonds.^{36,37} A combination of such surface pretreatment followed by 10-methacryloyloxydecyl dihydrogen phosphate (MDP) monomer or phosphate ester monomer-based primers and resin cements have resulted in superior and long-term durable zirconia-resin bonds.^{38–40} These functional monomers have proven to provide durable chemical bonds to the metal oxides in zirconia.^{41,42} Resin bonds to zirconia have been investigated for more than two decades now. Classic articles by Kern and coworkers have first demonstrated the effectiveness of APA and MDP-containing resin luting agents for long-term durable zirconia resin bonds.^{37,43} Other studies stressed

the importance of an MDP-containing primer, which provides better wettability, especially to the slightly rough computer-aided design/computer-aided manufacture (CAD/CAM) milled surfaces and can be used with conventional composite resin luting agents. This bonding protocol to 3Y-TZP consists of three main steps: air-particle abrasion with alumina or silica-coated alumina particles (step A), priming the air-abraded surfaces with an MDP or phosphate-monomer-based primer (step P), and cementation with dual or self-cure composite resin cement (step C), known as the “APC Zirconia Bonding Concept”.⁴⁴

Systematic reviews have also assessed both in vitro and clinical durability of different bonding protocols of 3Y-TZP to enamel, dentin, composite cores, titanium abutments and bases, zirconia abutments, and lithium disilicate crowns.^{45,46} They also concluded that 3Y-TZP surface pretreatment and chemically activating these surfaces with functional monomer-based primers and resin cements provide superior bond strengths.

Limited information is available about bonding to 4Y-TZP and 5Y-TZP zirconia. Concerns were expressed about surface pretreatment methods to new zirconia generations and the possibility of decreasing their flexural strength.^{47,48} It is unclear whether these treatments in combination with functional monomers would be also feasible. Therefore, the aim of this article is to systematically review in vitro studies on bonding protocols to new zirconia generations. The focused question was: Is the application of different surface pretreatment methods combined with an MDP monomer or phosphate monomer-based primer or resin cement a durable bonding protocol for new zirconia generations?

2 | MATERIAL AND METHODS

2.1 | Study selection criteria

This systematic review followed the PRISMA statement for reporting systematic reviews and meta-analysis.⁴⁹ The focused question was formulated according to the PICO strategy to develop the search strategy: **P**: 4Y and 5Y-TZP zirconia, **I**: MDP monomer or phosphate monomer-based primers/resin cements, **C**: Surface pretreatment methods, **O**: Durable bonding protocol.

One reviewer (A.A) conducted a search for English-language articles published in dental journals until 16 November 2020 of the following electronic data bases: PubMed and Cochrane Library. A manual search was also conducted. Searches used a combination of MeSH terms and free text words, as follows: ‘Zirconia’, ‘translucent zirconia’, ‘4Y-TZP’, ‘5Y-TZP’, ‘4Y-PSZ’, ‘5Y-PSZ’, ‘4Y’, ‘5Y’, ‘4Y-ZP’, ‘5Y-ZP’, ‘Primer’, ‘functional monomers’, ‘MDP’, ‘resin cement’, ‘adhesion’, ‘bonding’, ‘surface pretreatment methods’, ‘surface roughening’, ‘test’, ‘bond strength’, ‘in vitro’, and ‘laboratory’. References from different studies were included to identify relevant eligible studies. For the selection of studies, titles and abstracts of the studies were first reviewed independently by the two authors (A.A and M.B) according to the inclusion criteria. Second, final inclusion of studies

was based on screening and assessing full texts and with consensus of the authors. Table 1 gives a summary of all articles excluded in the second phase of the review along with reasons for exclusion.

2.2 | Inclusion criteria

1. In vitro studies reporting on the bond strength to new translucent zirconia generations.
2. Surface pretreatment methods applied to new translucent zirconia generations must be reported.
3. In vitro studies investigating the effect of surface pretreatment methods and adhesive bonding protocols on the bond strength outcomes.
4. In vitro studies including one of the artificial aging procedures: water storage, artificial saliva storage, thermocycling or mechanical load cycling.
5. Publications in the English-language dental literature.

2.3 | Exclusion criteria

1. In vitro studies reporting on the bond strength outcomes to conventional 3Y-TZP.
2. In vitro studies with a sample size of less than five test specimens in each subgroup.
3. Finite element analysis studies.
4. Clinical trials, case reports or animal studies.

Risk of bias assessment followed the Cochrane risk-of-bias tool for randomized trials (RoB 2).⁹⁴ The assessment of the quality of the studies was conducted according to a fixed set of domains of bias (selection bias, performance bias, attrition bias, reporting bias, and other bias). Within each domain, signaling questions were raised to extract information about features of the trial that are relevant to risk of bias, as follows: (1) random sequence generation, (2) allocation concealment, (3) blinding participants and personal, (4) blinding outcome assessment, (5) incomplete outcome data, (6) selective reporting, and (7) other resources of bias. The assessment of RoB was performed by categorizing each of the study features as 'low risk of bias', 'high-risk of bias', or 'unclear' (not possible to find the information). Both reviewers (A.A and M.B) conducted the assessment independently, and any uncertainty or disagreements were then resolved by discussion.

3 | RESULTS

Figure 1 depicts the study selection process according to the PRISMA checklist. The initial search revealed 629 papers, out of which 62 were selected for full-text assessment. Finally, 18 studies meet the inclusion criteria and were included in this systematic review. The studies identified were published between 2017 and 2020. Data from the

TABLE 1 In vitro studies excluded from the second phase of the review

Author (year)	Reasons for exclusion
Aung et.al 2019 ⁵⁰	Tested specimens were not subjected to an aging procedure
Cadore-Rodrigues et.al 2020 ⁵¹	Bond strength values was not evaluated
Elsayed et.al 2019 ⁵²	
Aboushelib et.al 2018 ⁵³	3Y-TZP zirconia were tested
Ali et.al 2019 ⁵⁴	
Asadzadeh et.al 2019 ⁵⁵	
Bhavana et.al 2019 ⁵⁶	
Cakirbay Tanis et.al 2019 ⁵⁷	
Carvalho et.al 2019 ⁵⁸	
Colombo et.al 2020 ⁵⁹	
Dantas et.al 2019 ⁶⁰	
Dantas et.al 2019 ⁶¹	
Ebeid et.al 2018 ⁶²	
Elsaka et.al 2016 ⁶³	
Flores-Ferreyra et.al 2019 ⁶⁴	
Hou et.al 2020 ⁶⁵	
Koko et.al 2020 ⁶⁶	
Kvam et.al 2019 ⁶⁷	
Lee et.al 2017 ⁶⁸	
Lee et.al 2019 ⁶⁹	
Le et.al 2019 ⁷⁰	
Li et.al 2020 ⁷¹	
Maciel et.al 2020 ⁷²	
Mendes et.al 2019 ⁷³	
Nagaoka et.al 2019 ⁷⁴	
Okada et.al 2017 ⁷⁵	
Okutan et.al 2020 ⁷⁶	
Omid et.al 2018 ⁷⁷	
Özdemir et.al 2019 ⁷⁸	
Petrauskas et.al 2018 ⁷⁹	
Ruyter et.al 2017 ⁸⁰	
Saade et.al 2019 ⁸¹	
Saade et.al 2020 ⁸²	
Saleh et.al 2019 ⁸³	
Salem et.al 2016 ⁸⁴	
Sathish et.al 2019 ⁸⁵	
Sharafeddin et.al 2018 ⁸⁶	
Skienhe et.al 2018 ⁸⁷	
Smielak et.al 2019 ⁸⁸	
Soltaninejad et.al 2018 ⁸⁹	
Tabatabaei et.al 2018 ⁹⁰	
Thammajaruk et.al 2020 ⁹¹	
Lümkemann et.al 2019 ⁹²	
Zahoui et.al 2020 ⁹³	

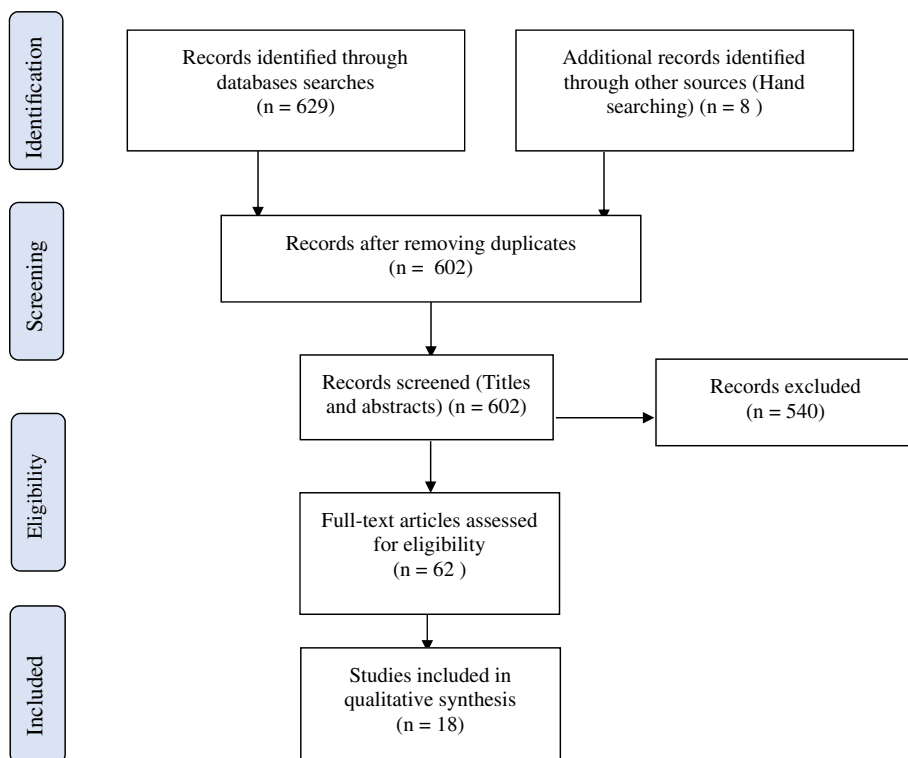


FIGURE 1 Flow chart of the study selection process

included studies were chronologically extracted in Table 2. Data extraction was performed using a predefined data extraction form as follows: author name, year of publication, zirconia generation, surface pretreatment method, primer, resin cement, aging procedure, bond strength values, and bonding failure mode analysis. Bonding failure modes were categorized as adhesive (failure along the interface between the resin cement and zirconia), cohesive (failure in the resin cement), or mixed (adhesive and cohesive).

3.1 | Bonding to 4Y-TZP

Three studies on bonding to 4Y-TZP zirconia were identified.⁹⁵⁻⁹⁷ The applied surface pretreatment methods in these studies were mechanical: alumina and glass-bead APA (Table 2). Alumina particles (50 μm) were applied at either 1 or 2 bar pressures. Glass-bead particles were 80 μm in size. Only one study included an MDP-based primer,⁹⁶ and two studies used MDP-based resin cements.^{95,97} All studies applied simulated aging in terms of water storage,⁹⁷ thermocycling,⁹⁵ and thermocycling combined with water storage.⁹⁶ Bond strength was tested with a shear test in all studies. Only one study provided results of failure mode analyses,⁹⁶ which were mainly adhesive with only a few categorized as mixed.

3.2 | Bonding to 5Y-TZP

The search revealed 18 studies on bonding to 5Y-TZP zirconia.^{86,95,96,98-111} The three types of surface pretreatment methods

were applied: mechanical, through alumina and glass-bead APA; chemical-mechanical, through TBS, lithium disilicate glass-ceramic coat, and plasma treatment; and chemical, through piranha acid etch solution and hot chemical etching (Table 2). Alumina APA particle sizes ranged between 40–110 μm at 1–6 bar pressure. Glass-bead particles were 80 μm in size. Most of the studies applied functional monomer-based primers and resin cements. All specimens in the identified studies underwent simulated aging, in terms of water storage,^{86,95,103,105,107,110} thermocycling,^{97,111} thermocycling combined with water storage,^{96,98,99,101,102,104,106,108,109} or thermocycling combined with water storage and mechanical load cycling.¹⁰⁰ Tensile, micro-tensile, shear, and pull-out tests were applied to test and measure bond strength. Most of the identified studies performed failure mode analyses, indicating adhesive, mixed or cohesive failure.

The risk of bias assessment of the 18 studies is shown in Table 3. The most common risk of bias was the absence of blinding the outcome assessment. Most of the identified studies did not provide any information about division of the tested specimens in a random manner (random sequence generation).

4 | DISCUSSION

Patient demand for dental restorations with a natural esthetic appearance has increased considerably over the past few decades. Translucency is considered as one of the primary parameters in controlling esthetics,^{112,113} which is a crucial step in the selection of restoration material. New zirconia generations have intermediate translucency to those of conventional zirconia and lithium disilicate glass-

TABLE 2 Identified in vitro studies

Author (year)	Zirconia generation	Surface pretreatment method	Primer	Functional monomers	Resin cement	Functional monomers	Pretest storage	Aging procedure	Bond strength test	Bond strength values	Failure mode analysis
Krifka et al 2017 ¹¹¹	5Y-TZP	Alumina APA 40 µm at 2 bar pressure	- Scotchbond Universal (3 M ESPE, Seefeld, Germany) - Monobond Plus (Ivoclar Vivadent, Shaan, Liechtenstein)	MDP MDP	RelyX Unicem 2 (3 M ESPE, Seefeld, Germany) RelyX Ultimate (3 M ESPE, Seefeld, Germany) Multilink Automix (Ivoclar Vivadent, Shaan, Liechtenstein)	Phosphoric acid -	-	12,000 TC (5°C/55°C)	Shear	67.6 ± 24 MPa (alumina APA 40 µm at 2 bar pressure + Monobond Plus + Multilink Automix) 57.6 ± 11 MPa (alumina APA 40 µm at 2 bar pressure + Scotchbond Universal + RelyX Ultimate) 54 ± 17.4 MPa (alumina APA 40 µm at 2 bar pressure + RelyX Unicem 2)	All test specimens experienced mainly adhesive failure modes
Kwon et al 2018 ¹⁰³	5Y-TZP	Alumina APA 50 µm at 2 bar pressure	Clearfil Ceramic Primer (Kuraray, Tokyo, Japan)	MDP	Panavia SA (Kuraray, Tokyo, Japan)	MDP	150-day WS	-	Shear	25.03 ± 6.44 MPa	NP
Yagawa et al 2018 ¹⁰⁴	5Y-TZP	Without surface pretreatment	- Alloy Primer (Kuraray, Tokyo, Japan) - Clearfil Ceramic Primer (Kuraray, Tokyo, Japan) - Meta Fast Bonding Liner (Sun Medical Co., Moriyama, Japan) - MR. bond (Tokuyama Dental Corp., Tokyo, Japan) Super-Bond PZ Primer (Sun Medical Co., Moriyama, Japan) V-Primer (Sun Medical Co., Moriyama, Japan)	MDP MDP - - - - -	- Panavia V5 Universal (Kuraray, Tokyo, Japan) - Panavia V5 Opaque (Kuraray, Tokyo, Japan)	- - - -	1-day WS 5000 TC (5°C/55°C)	Shear	42.3 ± 4.1 MPa (without surface pretreatment + Clearfil Ceramic Primer Plus + Panavia V5 Universal) 41.5 ± 3.7 MPa (without surface pretreatment + Alloy Primer + Panavia V5 Universal) 36.5 ± 2.7 MPa (without surface pretreatment + Clearfil Ceramic Primer Plus + Panavia V5 Opaque) 32.4 ± 2.2 MPa (without surface pretreatment + Alloy Primer + Panavia V5 Opaque) 14.9 ± 3.9 MPa (without surface pretreatment Meta Fast Bonding Liner + Panavia V5 Universal) 10.9 ± 3.4 MPa (without surface pretreatment + Meta Fast Bonding Liner + Panavia V5 Universal) 0.6 ± 0.3 MPa (without surface pretreatment + MR. bond + Panavia V5 Opaque) 0.6 ± 0.2 MPa (without surface pretreatment + Super-Bond PZ Primer + Panavia V5 Universal) 0.5 ± 0.2 MPa (without surface pretreatment + MR. bond + Panavia V5 Universal) 0.4 ± 0.2 MPa (without surface pretreatment + Super-Bond PZ Primer + Panavia V5 Opaque) 0.2 ± 0.1 MPa (without surface pretreatment + V-Primer + Panavia V5 Opaque)	Without surface pretreatment + Clearfil Ceramic Primer Plus + Panavia V5 Universal - Mainly adhesive - Few mixed Without surface pretreatment + Alloy Primer + Panavia V5 Universal - Mainly adhesive - Few mixed Without surface pretreatment + Clearfil Ceramic Primer Plus + Panavia V5 Opaque - Mainly adhesive - Few mixed Without surface pretreatment + Alloy Primer + Panavia V5 Opaque - Mainly adhesive - Few mixed Without surface pretreatment + Meta Fast Bonding Liner + Panavia V5 Universal Adhesive Without surface pretreatment + Meta Fast Bonding Liner + Panavia V5 Opaque Adhesive Without surface pretreatment + MR. bond + Panavia V5 Opaque Adhesive Without surface pretreatment + Super-Bond PZ Primer + Panavia V5 Universal Adhesive Without surface pretreatment + MR. bond + Panavia V5 Universal Adhesive Without surface pretreatment + Super-Bond PZ Primer + Panavia V5 Opaque Adhesive	

(Continues)

TABLE 2 (Continued)

Author (year)	Zirconia generation	Surface pretreatment method	Primer	Functional monomers	Resin cement	Functional monomers	Pretest storage	Aging procedure	Bond strength test	Bond strength values	Failure mode analysis
Sharafeddin et al 2018 ⁸⁶	5Y-TZP	Alumina APA 50 μm at 2 bar pressure	- All Bond Universal (Bisco, Schaumburg, USA) - Z-Prime Plus (Bisco, Schaumburg, USA)	MDP MDP	Variolink N (voclar Vivadent, Schaen, Liechtenstein)	-	1-day WS	-	Shear	22.45 \pm 3.60 MPa (alumina APA 50 μm at 2 bar pressure) + Z-Prime Plus + Variolink N) 17.51 \pm 1.34 MPa (alumina APA 50 μm at 2 bar pressure) + All Bond Universal + Variolink N) 7.57 \pm 1.62 MPa (alumina APA 50 μm at 2 bar pressure + Variolink N)	Without surface pretreatment + V-Primer + Panavia V5 Opaque Adhesive Without surface pretreatment + V-Primer + Panavia V5 Universal Adhesive Without surface pretreatment + Panavia V5 Universal Adhesive Without surface pretreatment + Panavia V5 Opaque Adhesive
Shimizu et al 2018 ⁸⁸	5Y-TZP	- Without surface pretreatment - Alumina APA 50 μm at 2 bar pressure - Plasma treatment	Super-Bond PZ Primer (Sun Medical Co., Moriyama, Japan)	MDP	Super-Bond (Sun Medical Co., Moriyama, Japan)	4-META	1-day WS	10,000 TC (5°C/55°C)	Tensile	36.7 MPa (without surface pretreatment + Super-Bond PZ Primer + Super-Bond) 35.5 MPa (alumina APA 50 μm at 2 bar pressure + Super-Bond) 32.6 MPa (Plasma treatment + Super-Bond PZ Primer + Super-Bond) 28.4 MPa (alumina APA 50 μm at 2 bar pressure + Super-Bond PZ Primer + Super-Bond) 11.1 MPa (without surface pretreatment + Super-Bond) 4.3 MPa (Plasma treatment + Super-Bond)	Without surface pretreatment + Super-Bond PZ Primer + Super-Bond - Mainly cohesive and mixed - Few adhesive Alumina APA 50 μm at 2 bar pressure + Super-Bond - Mainly cohesive and mixed - Few adhesive Plasma treatment + Super-Bond PZ Primer + Super-Bond - Mainly cohesive and mixed - Few adhesive and mixed Alumina APA 50 μm at 2 bar pressure + Super-Bond - Mainly cohesive and mixed - Few adhesive and mixed Plasma treatment + Super-Bond - Mainly adhesive - Few cohesive and mixed
Agren et al 2019 ¹⁰⁵	5Y-TZP	Alumina APA 110 μm at 3.5 bar pressure Lithium disilicate glass-ceramic coat	Monobond Plus (voclar Vivadent, Schaen, Liechtenstein)	MDP	Variolink Esthetic (voclar Vivadent, Schaen, Liechtenstein)	-	1-day WS	-	Shear	21.60 \pm 7.32 MPa (alumina APA 110 μm at 3.5 bar pressure + Variolink Esthetic) 16.56 \pm 11.09 MPa (Lithium disilicate glass-ceramic coat + Variolink Esthetic)	Alumina APA 110 μm at 3.5 bar pressure + Variolink Esthetic Adhesive Lithium disilicate glass-ceramic coat + Variolink Esthetic Adhesive

TABLE 2 (Continued)

Author (year)	Zirconia generation	Surface pretreatment method	Primer	Functional monomers	Resin cement	Functional monomers	Pretest storage	Aging procedure	Bond strength test	Bond strength values	Failure mode analysis
Franco-Tabares et al 2019 ¹⁰⁶	4Y-TZP 5Y-TZP	Alumina APA 50 μm at 1 bar pressure	—	—	Panavia F 2.0 (Kuraray, Tokyo, Japan)	MDP	—	TC	Shear	5.99 \pm 1.20 MPa (4Y-TZP) 5.13 \pm 1.21 MPa (5Y-TZP)	NP
Ruales-Carrera et al 2019 ¹⁰⁶	5Y-TZP	Without surface pretreatment Alumina APA 50 μm at 2.5 bar pressure TBS	Single Bond Universal (3 M ESPE, Seefeld, Germany)	MDP	RelyX Ultimate (3 M ESPE, Seefeld, Germany)	—	1-day WS	10,000 TC (5°C/55°C)	Micro-tensile	15.18 \pm 4.04 MPa (alumina APA 50 μm at 2.5 bar pressure + Single Bond Universal + RelyX Ultimate) 11.35 \pm 3.88 MPa (TBS + Single Bond Universal + RelyX Ultimate) 3.38 \pm 2.10 MPa (Without surface pretreatment + Single Bond Universal + RelyX Ultimate)	Alumina APA 50 μm at 2.5 bar pressure + Single Bond Universal + RelyX Ultimate Mixed TBS + Single Bond Universal + RelyX Ultimate - Mainly mixed - Few adhesive Without surface pretreatment + Single Bond Universal + RelyX Ultimate - Mainly adhesive - Few mixed
Zhao et al 2019 ¹⁰⁷	5Y-TZP	Without surface pretreatment Alumina APA 50 μm at 1 bar pressure for 10 s Alumina APA 50 μm at 1 bar pressure for 20 s Alumina APA 50 μm at 3 bar pressure for 10 s Alumina APA 50 μm at 3 bar pressure for 20 s - Alumina APA 50 μm at 6 bar pressure for 10 s - Alumina APA 50 μm at 6 bar pressure for 20 s - Alumina APA 110 μm at 1 bar pressure for 10 s - Alumina APA 110 μm at 1 bar pressure for 20 s - Alumina APA 110 μm at 3 bar pressure for 10 s - Alumina APA 110 μm at 3 bar pressure for 20 s - Alumina APA 110 μm at 6 bar pressure for 10 s - Alumina APA 110 μm at 6 bar pressure for 20 s	—	—	RelyX U200 (3 M ESPE, Seefeld, Germany)	Phosphoric acid	1-day WS	—	Shear	18.27 \pm 3.50 MPa (alumina APA 110 μm at 3 bar pressure for 20 s + RelyX U200) 12.42 \pm 3.32 MPa (alumina APA 110 μm at 6 bar pressure for 20 s + RelyX U200) 11.24 \pm 1.99 MPa (alumina APA 110 μm at 3 bar pressure for 10 s + RelyX U200) 10.96 \pm 3.26 MPa (alumina APA 50 μm at 1 bar pressure for 20 s + RelyX U200) 9.88 \pm 2.36 MPa (alumina APA 50 μm at 3 bar pressure for 10 s + RelyX U200) 9.80 \pm 3.13 MPa (alumina APA 110 μm at 1 bar pressure for 10 s + RelyX U200) 9.53 \pm 2.97 MPa (alumina APA 110 μm at 1 bar pressure for 20 s + RelyX U200) 8.70 \pm 3.42 MPa (alumina APA 50 μm at 6 bar pressure for 20 s + RelyX U200) 8.41 \pm 1.98 MPa (alumina APA 50 μm at 1 bar pressure for 10 s + RelyX U200) 7.34 \pm 2.64 MPa (alumina APA 50 μm at 3 bar pressure for 10 s + RelyX U200) 6.86 \pm 2.46 MPa (alumina APA 110 μm at 6 bar pressure for 10 s + RelyX U200) 5.98 \pm 2.95 MPa (alumina APA 50 μm at 3 bar pressure for 20 s + RelyX U200) 0.97 \pm 0.92 MPa (without surface pretreatment + RelyX U200)	Alumina APA 110 μm at 3 bar pressure for 20 s + RelyX U200 - Mainly adhesive - Some mixed Alumina APA 110 μm at 6 bar pressure for 20 s + RelyX U200 - Mainly adhesive - Few mixed Alumina APA 110 μm at 3 bar pressure for 10 s + RelyX U200 - Mainly mixed Alumina APA 110 μm at 3 bar pressure for 10 s + RelyX U200 - Mainly mixed Alumina APA 50 μm at 1 bar pressure for 20 s + RelyX U200 - Mainly mixed - Few adhesive Alumina APA 50 μm at 3 bar pressure for 10 s + RelyX U200 - Mainly mixed - Half adhesive Alumina APA 110 μm at 1 bar pressure for 20 s + RelyX U200 - Mainly mixed - Half adhesive Alumina APA 50 μm at 6 bar pressure for 20 s + RelyX U200 - Mainly mixed - Some adhesive Alumina APA 50 μm at 1 bar pressure for 10 s + RelyX U200 Mainly adhesive Alumina APA 50 μm at 3 bar pressure for 10 s + RelyX U200

(Continues)

TABLE 2 (Continued)

Author (year)	Zirconia generation	Surface pretreatment method	Primer	Functional monomers	Resin cement	Functional monomers	Pretest storage	Aging procedure	Bond strength test	Bond strength values	Failure mode analysis
Chen et al. 2020 ⁹⁹	5Y-TZP	Alumina APA 50 μm at 2.5 bar pressure TBS	Monobond N (Ivoclar Vivadent, Shaan, Liechtenstein)	Phosphoric acid	Variolink N (Ivoclar Vivadent, Shaan, Liechtenstein) Multilink Speed (Ivoclar Vivadent, Shaan, Liechtenstein)	- MDP	60-day WS	10,000 TC (5°C/55°C)	Shear	14.4 \pm 1.5 MPa (TBS + Monobond N + Variolink N) 13.2 \pm 1.5 MPa (alumina APA 50 μm at 2 bar pressure + Multilink Speed)	- Mainly mixed - Few adhesive - Few cohesive Alumina APA 110 μm at 6 bar pressure for 10 s \pm RelyX U200 - Mainly adhesive - Few mixed Alumina APA 50 μm at 3 bar pressure for 20 sec \pm RelyX U200 - Half mixed - Half adhesive Without surface pretreatment + RelyX U200 Mainly Adhesive
De Angelis et al. 2020 ¹⁰⁸	5Y-TZP	Alumina APA 50 μm at 2 bar pressure	Clearfil Ceramic Primer Plus (Kuraray, Tokyo, Japan)	MDP	Panavia V5 (Kuraray, Tokyo, Japan) Panavia SA (Kuraray, Tokyo, Japan) RelyX Unicem 2 Clicker (3 M ESPE, Seefeld, Germany)	- MDP Phosphoric acid	1-day WS	5000 TC (5°C/55°C)	Shear	21.1 \pm 3 MPa (alumina APA 50 μm at 2 bar pressure + Clearfil Ceramic Primer Plus + Panavia V5) 20.3 \pm 1.7 MPa (alumina APA 50 μm at 2 bar pressure + Panavia SA) 6.1 \pm 2.4 MPa (alumina APA 50 μm at 2 bar pressure + RelyX Unicem 2 Clicker)	Alumina APA 50 μm at 2 bar pressure \pm Clearfil Ceramic Primer Plus + Panavia V5 - Mainly mixed - Few adhesive Alumina APA 50 μm at 2 bar pressure \pm Panavia SA - Mainly mixed - Some adhesive Alumina APA 50 μm at 2 bar pressure \pm RelyX Unicem 2 Clicker - Mainly adhesive - Few mixed
Franco-Tabares et al. 2020 ⁹⁵	4Y-TZP 5Y-TZP	Without surface pretreatment	-	-	Panavia F 2.0 (Kuraray, Tokyo, Japan)	MDP	1-day WS	-	Shear	6.01 \pm 1.2 MPa (5Y-TZP) 4.81 \pm 1.2 MPa (4Y-TZP)	NP
Mehari et al. 2020 ⁹⁶	4Y-TZP 5Y-TZP	Without surface pretreatment Alumina APA 50 μm at 2 bar pressure 80 μm glass-bead APA	Z-Prime Plus (Bisco, Schaumburg, USA)	MDP	NX3 (Kerr, Rastatt, Germany)	-	1-day WS	2500 TC (5°C/55°C)	Shear	12.9 \pm 3.4 MPa (5Y-TZP + alumina APA 50 μm at 2 bar pressure + Z-Prime Plus + NX3) 11.8 \pm 4.1 MPa (4Y-TZP + alumina APA 50 μm at 2 bar pressure + Z-Prime Plus + NX3) 6.4 \pm 1.4 MPa (5Y-TZP + without surface pretreatment + Z-Prime Plus + NX3) 5.9 \pm 1.1 MPa (5Y-TZP + 80 μm glass-bead APA + Z-Prime Plus + NX3) 5.1 \pm 1.3 MPa	All tested specimens experienced mainly adhesive and some mixed failure modes

TABLE 2 (Continued)

Author (year)	Zirconia generation	Surface pretreatment method	Primer	Functional monomers	Resin cement	Functional monomers	Pretest storage	Aging procedure	Bond strength test	Bond strength values	Failure mode analysis
Monteiro et al 2020 ¹⁰⁰	5Y-TZP	Without surface pretreatment Alumina APA 50 µm at 2 bar pressure TBS	Scotchbond Universal (3 M ESPE, Seefeld, Germany)	MDP	RelyX Ultimate (3 M ESPE, Seefeld, Germany)	—	1-day WS	10,000 TC (5° C/55° C) + 240,000 MC (50 N)	Pull-out	(4Y-TZP + without surface pretreatment + Z-Prime Plus + NX3) 4.8 ± 1 MPa (4Y-TZP + 80 µm glass-bead APA + Z-Prime Plus + NX3)	Alumina APA 50 µm at 2 bar pressure ± Scotchbond Universal + RelyX Ultimate - Some adhesive - Few mixed - Few cohesive TBS + Scotchbond Universal + RelyX Ultimate - Mainly adhesive - Some mixed Without surface pretreatment + Scotchbond Universal + RelyX Ultimate Mainly adhesive
Sakrana et al 2020 ¹⁰¹	5Y-TZP	Alumina APA 50 µm at 2 bar pressure Alumina APA 50 µm at 2 bar pressure + Silane flame treatment Alumina APA 50 µm at 2 bar pressure + Piranha acid etch Alumina APA 50 µm at 2 bar pressure + Piranha acid etch + Silane flame treatment - Alumina APA 50 µm at 2 bar pressure + hot etching - Alumina APA 50 µm at 2 bar pressure + hot etching + Silane flame treatment	—	—	- Panavia SA Plus (Kuraray, Tokyo, Japan) - TheraCem (Bisco, Schaumburg, USA) - Panavia F2.0 (Kuraray, Tokyo, Japan)	MDP MDP MDP	1-day WS	10,000 TC (5° C/55° C)	Micro-tensile	25.1 ± 4.6 MPa (alumina APA 50 µm at 2 bar pressure + hot etching + Panavia SA) 23.2 ± 4.6 MPa (alumina APA 50 µm at 2 bar pressure + hot etching + Silane flame treatment + Panavia F2.0) 23.1 ± 5.1 MPa (alumina APA 50 µm at 2 bar pressure + Piranha acid etch + Panavia SA) 23 ± 3 MPa (alumina APA 50 µm at 2 bar pressure hot etching + Silane flame treatment + Panavia SA) 22.2 ± 6.9 MPa (alumina APA 50 µm at 2 bar pressure + hot etching + Panavia F2.0) 21.5 ± 7.3 MPa (alumina APA 50 µm at 2 bar pressure + Panavia SA) 20.8 ± 5.5 MPa (alumina APA 50 µm at 2 bar pressure + hot etching + Silane flame treatment + TheraCem) 20.6 ± 2.5 MPa (alumina APA 50 µm at 2 bar pressure + Panavia F2.0) 20.2 ± 4.2 MPa (alumina APA 50 µm at 2 bar pressure + Silane flame treatment + Panavia SA) 19.7 ± 7.1 MPa	All test specimens experienced predominantly adhesive and few cohesive failure modes

(Continues)

TABLE 2 (Continued)

Author (year)	Zirconia generation	Surface pretreatment method	Primer	Functional monomers	Resin cement	Functional monomers	Pretest storage	Aging procedure	Bond strength test	Bond strength values	Failure mode analysis
Khanlar et al. 2020 ¹¹⁶	5Y-TZP	Alumina APA 50 μm at 2 bar pressure	- Super-Bond Primer (Sun Medical Co., Moriyama, Japan) - Super-Bond PZ Primer + MMA (Sun Medical Co., Moriyama, Japan) - Super-Bond monomer (Sun Medical Co., Moriyama, Japan) - 4-MET experimental Primer (Sun Medical Co., Moriyama, Japan)	MDP 4-META 4-META	Super-Bond powder and Catalyst (Sun Medical Co., Moriyama, Japan)	-	150-day WS	-	Tensile	14.6 MPa (alumina APA 50 μm at 2 bar pressure + experimental 4-MET Primer + Super-Bond powder and Catalyst) 14.4 MPa (alumina APA 50 μm at 2 bar pressure + Super-Bond PZ Primer + MMA + Super-Bond powder and Catalyst) 10.8 MPa (alumina APA 50 μm at 2 bar pressure + Super-Bond monomer + Super-Bond powder and Catalyst) 10 MPa (alumina APA 50 μm at 2 bar pressure + PZ Primer + Super-Bond powder and Catalyst) 6.8 MPa (alumina APA 50 μm at 2 bar pressure + Super-Bond powder and Catalyst)	- Few mixed Alumina APA 50 μm at 1 bar pressure ± Z-Prime Plus + Duolink - Mainly adhesive - Few mixed Alumina APA 50 μm at 5 bar pressure ± Z-Prime Plus + Duolink Adhesive Without surface pretreatment + Z-Prime Plus + Duolink Adhesive

TABLE 3 Risk of bias assessment

Domain	Selection bias		Performance bias		Attrition bias Incomplete outcome data	Reporting bias Selective reporting	Other bias Other resources of bias
	Random sequence generation	Allocation concealment	Blinding participants and personal	Blinding outcome assessment			
Study							
Krifka et.al 2017 ¹¹¹	Unclear	NA	NA	High	Low	Low	Low
Kwon et.al 2018 ¹⁰³	High	NA	NA	High	High	Low	Low
Yagawa et.al 2018 ¹⁰⁴	Low	NA	NA	High	Low	Low	Low
Sharafeddin et.al 2018 ⁸⁶	Unclear	NA	NA	High	Low	Low	Low
Shimizu et.al 2018 ⁹⁸	Unclear	NA	NA	High	Low	Unclear	Low
Agren et.al 2019 ¹⁰⁵	Unclear	NA	NA	High	Low	Low	Low
Franco-Tabares et.al 2019 ⁹⁷	High	NA	NA	High	High	Low	Low
Ruales-Carrera et.al 2019 ¹⁰⁶	Low	NA	NA	High	Low	Low	Low
Zhao et.al 2019 ¹⁰⁷	Low	NA	NA	High	Low	Low	Low
Chen et.al 2020 ⁹⁹	Unclear	NA	NA	High	Low	Low	High
De Angelis et.al 2020 ¹⁰⁸	Low	NA	NA	High	Low	Low	Low
Franco-Tabares et.al 2020 ⁹⁵	High	NA	NA	High	High	Low	Low
Mehari et.al 2020 ⁹⁶	Unclear	NA	NA	High	Low	Low	Low
Monteiro et.al 2020 ¹⁰⁰	Unclear	NA	NA	High	Low	Low	Unclear
Sakrana et.al 2020 ¹⁰¹	Unclear	NA	NA	High	Low	Low	Low
Yoshida et.al 2020 ¹⁰²	Low	NA	NA	High	Low	Low	Low
Zhang et.al 2020 ¹⁰⁹	Low	NA	NA	High	Low	Low	Low
Khanlar et.al 2020 ¹¹⁰	Unclear	NA	NA	High	Low	Low	High

Abbreviations: 4-META, 4-methacryloyloxyethyl trimellitic acid; 4Y-TZP, 4 mol% yttria-stabilized tetragonal zirconia; 5Y-TZP, 5 mol% yttria-stabilized tetragonal zirconia; APA, airborne-particle abrasion; HT, hot treatment; MC, mechanical loading; MDP, methacryloyloxydecyl dihydrogen phosphate; MMA, methyl methacrylate; NP, not performed; TBS, tribochemical silica air-borne-particle abrasion; TC, thermocycling; WS, water storage.

ceramics,^{103,114} thereby increasing their potential use as esthetic monolithic restorations.¹¹⁵ Establishing a durable resin-bond to these new zirconia generations is crucial for their long-term clinical success. This systematic review aimed to review all in vitro studies investigated the durability of different bonding protocols applied in new zirconia generations. A meta-analysis was not performed due to the heterogeneity of the extracted data in terms of study design, surface pretreatment methods, resin cements, aging procedures utilized, laboratory tests, and the size of the sample. Therefore, a summary of the identified studies was made.

4.1 | Bonding to 4Y-TZP

APA surface pretreatment was tested in two of the identified studies.^{96,97} It cleans the zirconia surface, removes impurities, increases surface roughness, and modifies the surface energy and wettability.¹¹⁶ The effect of APA on the flexural strength of 3Y-TZP seems inconclusive as some studies report strengthening while others find a weakening effect.¹¹⁷⁻¹²⁰ These conflicting results may be due to the diverse

testing protocols and variations in particle type, size, and pressure. However, results from a meta-analysis showed that APA does actually strengthen 3Y-TZP, independent of particle size and air pressure.¹²¹ Included studies showed that APA in combination with an MDP monomer-based primer or resin cement resulted in durable resin-zirconia bonds. Bond strength values achieved with alumina APA were over twice as high than with other treatment methods (glass-bead APA) or no surface pretreatment (Table 2). Glass beads are typically used for APA of enamel, dentin, nickel-chromium alloys, and CAD/CAM composite materials.¹²²⁻¹²⁴ The particles are softer and may have less adverse effects on the mechanical properties of zirconia than alumina APA. However, bond strengths were similar to glass-bead-APA and nontreated zirconia surfaces. Additionally, failure mode analyses showed more mixed failures associated with alumina than glass-bead APA.⁹⁶

Nontreated zirconia surfaces showed reduced bond strength values and more adhesive failure modes compared to other surface pretreatment methods (Table 2).⁹⁶ Therefore, APA with alumina particles is essential for durable resin bonds to 4Y-TZP, even when functional monomer-based primers and resin cements are used.^{125,126}

Further *in vitro* investigations are required to test the effects of various sizes of alumina and glass-bead particles, different levels of air pressure, other surface pretreatment methods, primers, and resin cements when bonding to 4Y-TZP.

4.2 | Bonding to 5Y-TZP

APA with alumina was the most widely tested surface treatment in the identified studies (Table 2). Most of these focused on the effects of APA^{96–100,103,105,106,111} and found them to improve resin bonds to 5Y-TZP zirconia. Failure modes were either mixed or cohesive (Table 2), indicating strong resin bonds. Focused ion beam (FIB) microscopy showed that alumina APA, followed by MDP monomer-based primers, is necessary to optimize the adhesive bond interface between resin cements and zirconia.³² Resin cements and primers containing functional monomers such as MDP, other phosphate monomers, mixture of organophosphate and carboxylic monomers, and 4-methacryloxyethyl tri-mellitic anhydride (4-META) provide chemical bonds to pretreated 3Y-TZP surfaces.^{127,128} Outcomes of different types of functional monomer-based primers and resin cements to APA 5Y-TZP are inconsistent (Table 2). De Angelis and coworkers¹⁰⁸ found that MDP monomer-based primers and resin cements performed significantly better than phosphate monomer-based resin cements. Failure modes obtained with a phosphate monomer-based resin cement (RelyX Unicem 2 Clicker, 3 M ESPE, Seefeld, Germany) were mainly adhesive (Table 2). Conversely, Khanlar and coworkers¹¹⁰ and Shimizu and coworkers⁹⁸ found no significant difference between MDP and 4-META. Both types of functional monomers achieved comparable bond strengths to 5Y-TZP, and failure modes were mainly cohesive (Table 2).

Several alumina APA parameters influence the resin bond to zirconia, including particle size, air pressure, timing of abrasion, angle of abrasion, and the distance.^{116,129,130} The effect of particle size and air pressure on the 5Y-TZP zirconia-resin bond was investigated in two of the identified studies.^{107,109} Zhang and coworkers stated that APA with 50 μm alumina particles at 2 bar pressure is recommended for establishing durable resin bonds. This protocol did not achieve sufficient surface roughness in another study.¹⁰⁷ The authors found that an increase in particle size up to 110 μm and air pressure up to 3 bar provided a significant increase in bond strength (Table 2). Furthermore, the increase in particle size and air pressure did not induce tetragonal-monoclinic phase transformation. No decrease in flexural strength of the tested 5Y-TZP zirconia was observed.

Conventional 3Y-TZP zirconia undergoes transformation toughening, a tetragonal-monoclinic phase transformation that limits crack propagation.^{48,70,131} New zirconia generations with higher yttria content do not undergo transformation toughening, one of the reasons that limit their mechanical strength.¹³² However, the cited study did not include sufficient aging protocols, a clear limitation that negates any comment on bond durability over time (Table 2).¹⁰⁷

Additional heat treatment of air-abraded 5Y-TZP zirconia surfaces was investigated in one study (Table 2). This additional treatment

could recover any possible flexural strength reduction of the tested zirconia specimens after APA.¹⁰² However, a significant reduction in bond strength compared to the APA-only group was observed. Failure modes were mainly adhesive (Table 2). More specifically, APA created a conducive surface for durable bond strengths with an MDP-based resin cement. The significant reduction in bond strength after heat treatment suggests a decrease in surface roughness.¹⁰² Therefore, alumina APA and MDP-based resin cements provide superior and durable resin bonds to 5Y-TZP.¹⁰¹ Piranha and hot chemical etching solutions were applied after APA (Table 2). Piranha acid etching solution is a strong oxidizing corrosive agent.¹³³ It is a combination of hydrogen peroxide and sulfuric acid to remove organic impurities and hydroxylate surfaces.^{134,135} Hot chemical etching increases surface roughness and removes the superficial ceramic layer, creating a porous zirconia texture.¹³⁶ APA combined with hot etching solution resulted in greater bond strength values than piranha acid etching solution (Table 2). The additional heat treatment after hot acid etching improved the bond between MDP-based resin cements and zirconia. The authors reported that piranha solution hydroxylated and cleaned the zirconia surfaces, but failed to create a sufficiently rough surface.¹⁰¹ In addition, this method cannot be recommended for use in clinics.^{134,137} Furthermore, glass-bead surface pretreatment resulted in a smooth and less retentive zirconia surface than alumina APA.⁹⁶

Plasma surface treatment has been proposed as a chemical-mechanical surface treatment for zirconia bonding.³³ The goal is to increase the surface energy, improve wettability, and remove organic impurities.¹³⁸ Specimens that were plasma treated but not chemically activated with an MDP-based primer had significantly lower bond strength, while failure modes were mainly adhesive.⁹⁸ Besides plasma surface treatment, TBS has also been proposed for chemical-mechanical surface treatment.³³ It exerts dual functionality by increasing the silica content on the zirconia surface and roughening it, thereby creating a conducive surface for silanization that promotes chemical affinity to resin cements.^{50,139–141} Application of an MDP-based primer on TBS-treated zirconia resulted in durable bond strengths^{99,100,106} and failure modes were predominantly mixed (Table 2). All MDP primers in the identified studies incorporate silane molecules in their chemical composition (Table 2). Some studies have shown that utilizing a primer that contains both MDP and silane improved the resin-bond to TBS treated zirconia surfaces,^{142–144} while others suggested that these primers might reduce bonding to silica-enriched surfaces, due to silanol condensation.^{145,146} Moreover, SEM results showed that surface roughness generated by TBS was lower than after alumina APA.^{99,100,106} This is due to the inability of the silica-coated particles to be firmly embedded into the zirconia surface.^{42,147} Glass-ceramic lithium silicate coating has been also suggested in one of the studies (Table 2). It applies an etchable glass-ceramic coat on the zirconia surface,¹⁰⁵ which had varying results on 3Y-TZP.^{139,148–151} Concerns were raised regarding thickness control of that additional layer and its possible implications on restoration fit.^{148,152} SEM analyses revealed that the applied primer did not provide micromechanical interlocking to the HF-etched layer, either due to its specific composition or the glass-ceramic coating method.¹⁰⁵

Some studies stated that adhesive system selection is more important than surface treatment.^{153,154} However, the latter were found to be essential for durable resin-zirconia bonds in a recent systematic review.⁴⁵ The applied surface pretreatment methods changed the morphology of 5Y-TZP zirconia surfaces, created different levels of surface roughness, and improved the bond strength of resin cements to zirconia. Therefore, combined micromechanical and chemical surface treatment is key for strong and durable resin-zirconia bonds.

Further *in vitro* studies to test various bonding protocols to 5Y-TZP are necessary.

4.3 | Laboratory studies

Experimental designs and testing set ups varied greatly between studies. Several testing methods (i.e., shear, tensile, micro-tensile, and pull-out test) were applied to measure and compare bond strength of resin cements to new zirconia generations (Table 2), with the shear-bond strength test being the most common. This might be because its user-friendliness, simple specimen preparation, clear test protocol, and fast results.^{155,156} However, shear test has been criticized for the development of nonhomogenous stress distributions along the ceramic interface. Its fracture pattern may cause cohesive failures, leading to inaccurate interpretations of the results^{38,157,158} while failing to simulate clinical conditions.^{159,160} Tensile tests, on the other hand, provide more homogenous stress distribution. Fracture patterns occur within the adhesive interface, which seems more appropriate for evaluating bond strength values.^{158,161} Microtensile tests are claimed to be most suitable method.¹⁶² They offer better distribution of stresses and a more sensitive analysis. However, a major limitation is the demanding and technique sensitive specimen preparation.^{127,162-164} Pull-out tests may be the most adequate in terms of stress distribution, but their clinical relevance is not superior to the other tests mentioned.^{160,165} They are also technique sensitive and susceptible to additional influencing parameters.¹⁶⁰

Despite the variety of laboratory tests, their results are limited to the tested bonding protocols.¹⁶⁶ A microscopic analysis of the failure mode type is necessary to understand and properly interpret the obtained bond strength values.¹⁶⁶⁻¹⁶⁸ Another critical aspect is the inclusion of simulated aging parameters to evaluate the effects intraoral conditions in terms of temperature changes in a wet environment. It has long been demonstrated that long-term water storage and especially thermocycling considerably stress bonding interfaces and influence resin-zirconia bond strengths in a significant manner.^{169,170} Aging parameters such as water storage duration, temperature, number of thermal cycles, and their dwell times differed among almost all identified studies. To date, there is little consensus about the specific aging parameters. However, a combination of thermal and mechanical load cycling may best simulate intra-oral conditions.¹⁷¹ The mechanical loading mimics chewing forces while thermocycling subjects the test specimens to sudden changes in temperature, which causes repetitive contraction-expansion stresses to resin cements.^{172,173} And lastly, exposure in a wet environment subjects the applied materials to hydrolysis. Table 4 gives a summary of all abbreviated terms.

TABLE 4 List of abbreviations

APA	Airborne-particle abrasion
CAD/CAM	Computer-aided design/ Computer-aided manufacturing
FIB	Focused ion beam
HF-etched	Hydrofluoric etched
MDP	Methacryloyloxydecyl dihydrogen phosphate
PFM	Porcelain-fused-to-metal
Rob	Risk of bias
SEM	Scanning electron microscope
SIE	Selective infiltration etching
TBS	Tribochemical silica airborne-particle abrasion
Y-TZP	Yttria-stabilized tetragonal zirconia polycrystal
4-META	4-methacryloxyethyl tri-mellitic anhydride

The reviewed studies suggest that mechanical surface pretreatment in combination with an MDP monomer or phosphate monomer-based primer or resin cement are recommended for new zirconia generations. However, most of the studies did not use clinically relevant specimen geometries and flat discs or cylinders fail to reproduce actual stresses that occur at the zirconia-tooth interface.¹⁷⁴ There is also little information on the influence of the tested bonding protocols on the flexural strength and other physical properties of new zirconia generations.

Therefore, further studies that include clinically relevant test conditions, new and emerging bonding protocols, and their effect on various material properties are needed. And ultimately, their results must be confirmed in controlled clinical trials.

5 | CONCLUSIONS

Within the limitations of this review, the available evidence suggests that:

1. Resin bonding protocols successfully applied to conventional zirconia are also the most successful for high-translucent zirconia.
2. Airborne particle abrasion and special phosphate monomer-containing primers and/or composite resin cements provide long-term durable resin bonds.
3. Further *in vitro* studies applying clinically relevant geometry test specimens and aging procedures as well as clinical trials are necessary to further support these findings.

DATA AVAILABILITY STATEMENT

Data sharing is not applicable- the systematic review describes entirely theoretical research

DISCLOSURE

The authors declare that they do not have any financial interest in the companies whose materials are included in this article.

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