

1 **Assessing the viability of electro-absorption and photoelectro-** 2 **absorption for the treatment of gaseous perchloroethylene**

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15 **Abstract**

16 This work focuses on the development of electro-absorption and photoelectro-
17 absorption technologies to treat gases produced by a synthetic waste containing the
18 highly volatile perchloroethylene (PCE). To do this, a packed absorption column
19 coupled with a UV lamp and an undivided electrooxidation cell was used. Firstly, it was
20 confirmed that the absorption in a packed column is a viable method to achieve
21 retention of PCE into an absorbent-electrolyte liquid. It was observed that PCE does not
22 only absorb but it was also transformed into phosgene and other by-products. Later, it
23 was confirmed that the electro-absorption process influenced the PCE degradation,
24 favoring the transformation of phosgene into final products. Opposite to what expected,
25 carbon dioxide is not the main product obtained, but carbon tetrachloride and

26 trichloroacetic acid. Both species are also hazardous but their higher solubility in water
27 opens possibilities for successful and more environmental-friendly removal. The
28 coupling with UV-irradiation has a negative impact on the degradation of phosgene.
29 Finally, a reaction mechanism was proposed for the degradation of PCE based on the
30 experimental observations. Results were not as expected during the planning of the
31 experimental work but it is important to take in mind that PCE decomposition occurs in
32 wet conditions, regardless of the applied technology, and this work is a first approach to
33 try to solve the treatment problems associated to PCE gaseous waste flows in a realistic
34 way.

35

36 **Keywords**

37 VOCs removal; Perchloroethylene; Electro-absorption; UV irradiation

38

39 **Highlights**

- 40 • Absorption into electrolytes can help to retain PCE from gas effluents.
- 41 • Phosgene is produced by wet decomposition of PCE
- 42 • Electro-absorption favors transformation of phosgene into CCl₄ and TCA
- 43 • Almost no mineralization of gaseous streams was attained
- 44 • UV-irradiation does not have a significant influence.
- 45 • Reaction pathways with main liquid and gaseous by-products were proposed.

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50

51 **Introduction**

52 Over the last decades, electrochemical environmentalists have faced massively the
53 development of technologies for the remediation of liquids wastes and polluted soils,
54 sometimes developing applications with great interest (Abou Dalle et al., 2017; Moreira
55 FC 2017; Muñoz-Morales et al., 2019; Rodrigo et al., 2014; Sirés et al., 2014); others
56 only promising technologies with low TRLs (technology readiness level). However, the
57 treatment of gaseous pollutants has only been tackled rarely and, in this point (G et al.,
58 2016; Muthuraman and Moon, 2012) , there is a huge unexplored research field with
59 hundreds of applications still needed to be developed. In this line, some studies have
60 evaluated the degradation of volatile organic compounds (VOCs)(Liu et al., 2001;
61 Lugaresi et al., 2014;), degradation of environmental odor gases (Govindan and Moon,
62 2013) and hospital indoor air (Zadi et al., 2018).

63 Additionally treatment of gases can be carried out directly in gas phase using
64 electrochemical cells equipped with solids electrolytes (Barge and Vaidya, 2019;
65 Muthuraman et al., 2018), either polymer exchange membranes or solid oxides
66 (Monteiro et al., 2015; Yamazaki et al., 2001). Alternatively, it can be carried out in
67 liquid phase (Miao et al., 2015; Sáez et al., 2010; Sáez et al., 2009), following the
68 absorption (ABS) of the gas into a liquid, which is not only an absorbent of the
69 separation unit but also the electrolyte of the electrochemical cell (Muthuraman and
70 Moon, 2012). Hence, its formulation is a topic of the major importance, because it can
71 help to retain more efficiently the gas into the liquid or it can promote the
72 electrochemical generation of oxidants, which later are going to increase the efficiency
73 of the process (Chung and Moon, 2013; Muthuraman et al., 2017). In addition, the
74 combination of the absorber with the electrochemical cell is also a topic of great
75 significance.

76 Chlorinated hydrocarbons are extensively used, not only as solvents or degreasers but
77 also as pesticides, wood preservatives and in many other applications (Huang et al.,
78 2014; Mrema et al., 2014). Pollution associated to these molecules is typically persistent
79 and hazardous. High volatility of various of these pollutants brings up a case of special
80 interest, typically associated not only to environmental concerns but also, and more
81 importantly, directly related to health of humans (Basu et al., 1998). This is the case of
82 perchloroethylene, a product with many applications in industry and laundries,
83 nowadays with a decreasing use because of the problems associated to its volatility
84 (Nijhuis N, 2010). Anyway, it is still massively applied, and it is a topic of major
85 interest the search of a successful technology which can treat it. In the past, some
86 studies were carried out showing the removal of PCE from aqueous solutions using
87 ferrous ion catalyzed sodium percarbonate (Miao et al., 2015), Fenton process (Jho et
88 al., 2010) and/or applying different electrochemical (Sáez et al., 2009) and sono-
89 electrochemical degradation strategies (Sáez et al., 2010). In addition, previous works in
90 our research group evaluated the removal of PCE from spiked soils (Muñoz-Morales et
91 al., 2019), where it was found the importance of the amount of PCE that was partially
92 volatilized during the treatment, a key aspect that it is not considered in many other
93 works seem in the literature. Regarding to the removal of gaseous pollutants, electro-
94 reductive hydro-dehalogenation has been successful used to remove some volatile
95 organic halides (VOCs) (Lugaresi et al., 2014), following the promising results obtained
96 in the treatment of other gases (Govindan and Moon, 2013).

97 Considering this background, this work aims to use electro-absorption (EABS)
98 technology to treat gases produced in a synthetic waste containing perchloroethylene.
99 To do this, a packed absorption column, an undivided electrochemical cell and UV
100 lamps are going to be coupled in order to evaluate the retention and reactivity of the

101 pollutant by ABS, EABS and photoelectro-absorption technologies and to elucidate the
102 mechanisms involved in this process.

103

104 **Materials and methods**

105 **Chemicals.** All chemicals, including perchloroethylene ($C_2Cl_4 > 99\%$) (a.r., Sigma-
106 Aldrich), anhydrous sodium sulfate, phosphoric acid (85 %), sulfuric acid (98%),
107 sodium carbonate (a.r., Fluka, Spain), were analytical grade and they were used as
108 received. Hexane HPLC grade (a.r., Sigma-Aldrich, Spain) was used as mobile phase.
109 Helium and nitrogen (Al Air Liquide España, S.A) were used in gas chromatography
110 and helium was filtered by a Hydrocarbon Cartridge Filter (Thermo Fisher Scientific)
111 before its use. Double deionized water (Millipore Milli-Q system, resistivity = 18.2 M Ω
112 cm at 25 °C) was used to prepare all solutions. Na_2SO_4 at 0.04 M was previously
113 dissolved in Milli-Q water and perchloroethylene (PCE) was then added in a closed
114 volumetric flask and the solution was softly stirred with a magnetic bar overnight to
115 achieve complete dissolution.

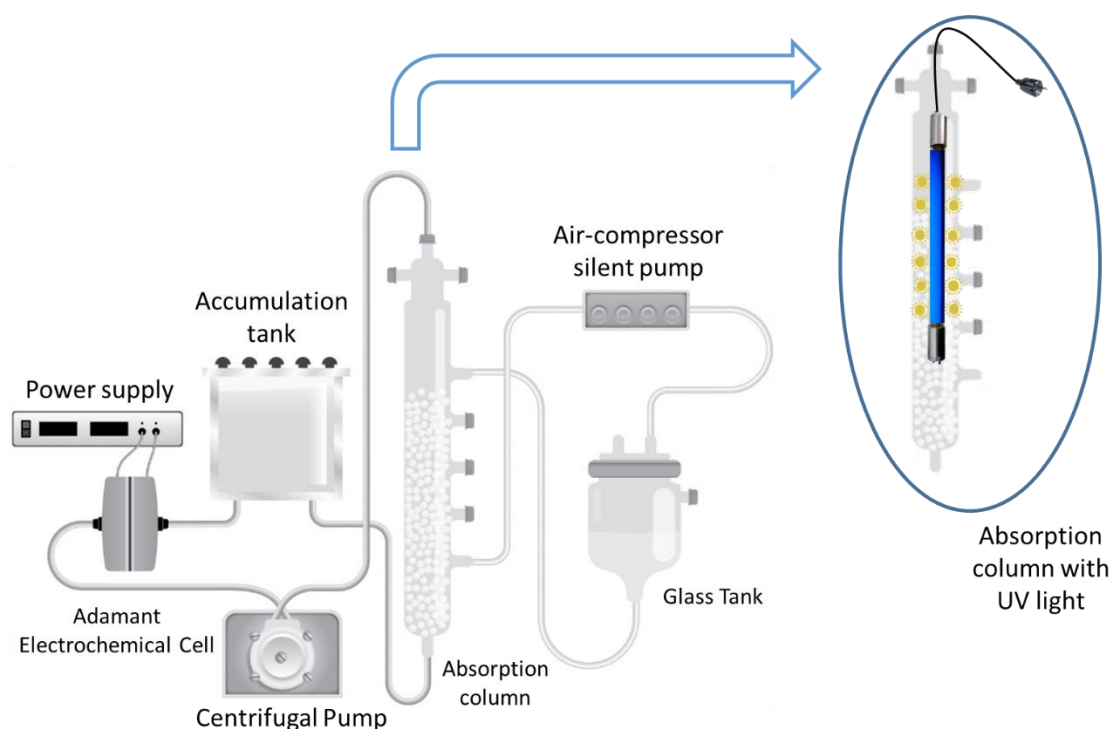
116 **Experimental setup.** The experimental set-up consisted of a wet absorption coupled
117 with an electrochemical cell. The system has four components as shown in Fig. 1: two
118 tanks, a packed absorption column and an electrochemical cell. The absorption column
119 (0.5 m long, inner diameter of 50 mm) was made of glass. A length of 0.4 m of the
120 column was packed with glass spheres (diameter 8mm). The gas liquid contact in the
121 packed column was continuous. The liquid flowed down the column over the packing
122 surface and the gas flowed up counter-currently. The first tank, which stored the
123 absorbent-electrolyte, was made of methacrylate and had a capacity of 2.5 dm³. It was
124 filled with a solution consisting of 0.1 mol dm⁻³ Na_2SO_4 used as supporting electrolyte.
125 A centrifugal pump was connected between the electrolyte storage tank and the top of

126 the absorption column. The second tank, that contains the synthetic waste polluted with
127 PCE (use to simulate in realistic conditions the generation of an PCE waste stream), was
128 a jacketed glass tank connected to a controlled thermostatic bath (Digiterm 100, JP
129 Selecta, Barcelona, Spain). This tank had a capacity of 1.2 dm³ and it was filled in with
130 a solution containing 150 mg dm⁻³ of PCE. To favor transfer of this pollutant to the gas
131 phase, the stripping was promoted by connecting an air-compressor Silent Pump model
132 SI6000 (ICA SA, Spain) with 3.8 W, flow 360 dm³ h⁻¹. Gas generated was flowed to
133 absorption column. To couple UV photolysis to the treatments, an UVC lamp of 11 W
134 (light path-length = 245 mm d_{ext} = 19 mm) was installed in the center of the absorption-
135 column. The photo-absorption column was covered with aluminum foil to avoid
136 exposure to UVC rays and during the collection of samples, the accumulation tank was
137 covered with ice gel packs. Then, temperature was monitored to make sure it keeps
138 practically constant during all processes (20±2 °C). Extreme care was taken to avoid
139 gaseous losses in all compartments by using tight-fitting ground-silicone stoppers and
140 by sealing with Teflon tape. Electrolyses were carried out in a single compartment
141 electrochemical flow cell DiaCell®, supplied by Adamant Technologies (Switzerland).
142 Conductive–Diamond Electrodes (p-Si–boron-doped diamond) were used as anode and
143 cathode. The BDD electrodes were subjected to cleaning procedure during 10 min in a 1
144 M Na₂SO₄ solution at 15 mA cm⁻² prior to electrolysis assays. All the processes were
145 conducted at atmospheric pressure conditions.

146 **Analysis procedures.** Liquid and gas samples were taken from the sampling ports of
147 the absorption column and from the PCE glass tank. To determine perchloroethylene
148 concentration in both gas and liquid phase, an L–L extraction process was employed
149 before the analysis: 1.0 mL of samples were taken using a syringe/ gas-tight (Hamilton,
150 Switzerland) following extraction with 3.0 mL of hexane using a glass vials with Cap

151 and PTFE Septa. Then, it was shaken in a vortex stirrer for 3 min at 4000 rpm for the
152 separation of the phases. Next organic phase was transferred to a GC vial. For by-
153 products analysis, different techniques such as HPLC, ionic chromatography, and
154 inorganic carbon analysis were used. Liquid samples were directly transferred to an
155 adequate vial to measure the parameters and for gaseous sample, 5 mL was drawn and
156 dissolved into 10 mL of Milli-Q water using a glass vials with cap and PTFE Septa to
157 guarantee that no losses of gas occur during the gas bubbling. Then, a vortex stirrer was
158 used during 3 min and the resulting samples were transferred to appropriate vials for
159 each analysis. All samples extracted from electrolyzed solution were filtered with 0.22
160 μm nylon filters before analysis.

161



162

163 **Figure 1.** Experimental setup for the EABS process couple to the UV irradiation
164 column.

165 The removal of perchloroethylene was quantified by Gas Chromatography Electron
166 Capture Detector (GC-ECD) (Thermo Fisher Scientific) using analytical column using a

167 TG-5MS capillary column (30m×0.25mm×0.25mm), Ni micro-electron capture
168 detector, a split/ splitless injector and ChromCard Software. Under the conditions used,
169 the quantification limit of the GC- ECD was 0.1 mg dm⁻³. The flow rate of gas He was
170 1.0 mL min⁻¹. The temperature of the oven was programmed as follows: kept at 60 °C
171 for 1 min increased to 140 °C at 10 °C min⁻¹ followed by another ramp at 10 °C min⁻¹
172 to reach 260 °C followed by 2 min hold. The temperature of the injector was 260 °C.

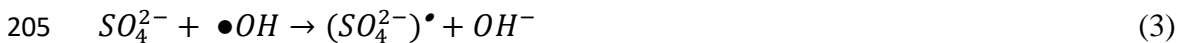
173 For the determination of degradation by-products originated in the ABS and EABS
174 treatments, two chromatographic methods were employed. The first was employed to
175 analyze tetrachloromethane by means of a Jasco HPLC LC-2000 with a PDA MD-2018
176 Detector (Jasco, Japan). The mobile phase consisted of 100 % of 0.1% phosphoric acid
177 (flow rate of 1 cm³ min⁻¹). The detection wavelength used was 280 nm and the
178 temperature oven was maintained at 25 °C. Volume injection was set to 20 µL

179 Trichloroacetic acid (TCA) was determined using a HPLC Agilent 1100 series (Agilent
180 Tech. USA) with a detection wavelength of 220 nm. The ion exchange column used
181 was SupercogelTM H Column with 30cm x 7.8mm ID. The mobile Phase was 1%
182 phosphoric acid (H₃PO₄), the column temperature was 30°C, the flow rate was 0.8 cm³
183 min⁻¹ and the injection volume was 20 µL.

184 Chloride concentration was determined by ion chromatography using a Metrohm 930
185 Compact IC Flex coupled to a conductivity detector. A Metrosep A Supp 7 column was
186 used to determine the anions using a eluent consisting of 85:15 v/v 3.6 mM
187 Na₂CO₃/acetone at a flow rate of 0.8 cm³ min⁻¹. Suppressor regeneration solution was
188 500 mmol dm⁻³ of sulfuric acid. The Inorganic Carbon concentration was monitored
189 using a Multi N/C 3100 Analytik Jena analyzer. Measurements of pH were carried out
190 with GLP 20 Crison pH-meter.

191 **Results and discussion**

192 **Absorption (ABS) and electro-absorption (EABS) of gases containing PCE.** Fig. 2
193 shows the changes in the amount of PCE as a function of the treatment time, measured
194 at the gas and liquid phases, in the tank containing the PCE liquid waste (PCE stripping
195 tank) and in the tank that stores the electrolyte that flows throughout the absorption
196 column, respectively, during the ABS and EABS treatments. Electrochemical
197 technology was coupled to the ABS system in order to increase the removal efficiency
198 of the PCE and its by-products by enhancing its reactivity, either by direct
199 electrochemical oxidation or reduction, or by mediated processes generated by the
200 oxidants and reductants produced on the electrode surfaces during the electrolytic
201 process (such as those shown in eqs (1-4)). The experiment shown in the Figure was
202 carried out at 8.0 A (102 mA cm⁻²) and at initial pH of 6.5.



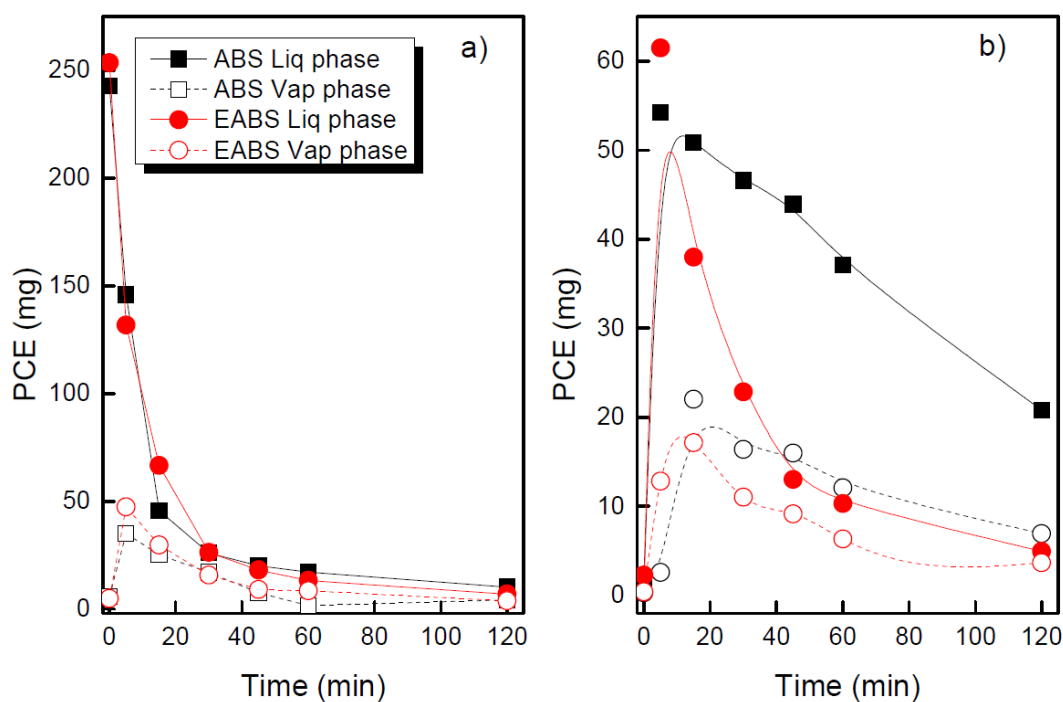
207 As expected, there are no important differences between the single ABS and the EABS
208 in the decay of PCE in the stripping tank containing the raw liquid waste (for both
209 phases). PCE contained in liquid phase decreased rapidly for both technologies during
210 the treatment time, reaching values lower than 50 mg within 15 min and attaining 95.8
211 % removal during the time span of 120 min (Henry's constant 0.02 atm m³ mol⁻¹). This
212 rapid removal indicates the importance of volatilization processes during the treatment
213 of liquid wastes containing PCE and the need of developing gas treatment technologies
214 or operate in non-opened to atmosphere systems.

215 In the gas phase, the quantity of PCE increased at the beginning of the tests, attaining its
216 maximum concentration just after 5 minutes of operation. This gas phase contacts with
217 the absorbent-electrolyte in the absorption column and this explains the transfer of the
218 PCE to the other circuit. The similar values obtained for the system with and without
219 the electrochemical cell indicates that volatilization of the PCE contained in the liquid
220 waste is almost not influenced by type of ABS treatment carried out (with or without
221 electrochemical reaction).

222 Part b shows the increase in the amounts of PCE in the absorption column/tank circuit
223 during the first 10 minutes in both liquid and gas phases. As seen, it reaches around 50
224 mg in the liquid phase and 20 mg in the vapor phase for both technologies, indicating
225 the success in the absorption of the gas generated into the stripping tank which
226 simulated the production of this gaseous stream. It also indicates that the ABS process is
227 very fast, meaning that the packing material used is very effective for the absorption of
228 PCE, which it can be related to the high specific area (which, in turn, provides intimate
229 contact between the gas and absorbing liquid).

230 After 10 min, it is observed that PCE decreased in both phases remaining around 20 mg
231 after 120 minutes for ABS process and only 8 mg in the liquid phase for the
232 electrochemically assisted process. This means that 97 % PCE is removed at 120 min in
233 the EABS technology which shows a higher mass-transfer coefficient (11.5 % higher in
234 the EABS process). Then, less gaseous PCE is observed in EABS, because of their
235 faster removal in liquid phase promoted by the electrochemical process. In addition, the
236 rate of PCE decay after 5 min (calculated fitting experimental data to a first-order
237 kinetic reaction model) in the column for EABS technology is three times faster than in
238 the ABS process ($3.85 \times 10^{-4} \text{ mol s}^{-1}$ for the EABS compared to $1.39 \times 10^{-4} \text{ mol s}^{-1}$ for
239 ABS process). This difference is indicative of the influence of the electrochemical

240 processes and it can be explained in terms of the high production of hydroxyl radicals
 241 and mediated electro-reagents, such as peroxosulfates generated by oxidation of the
 242 sulfate anions contained in the absorbent-electrolyte and also chlorine produced from
 243 the dehalogenation of the PCE. Other important remark is that at 5 min only 33% of
 244 PCE remains unreacted. This behavior can be explained in terms of the high PCE
 245 reactivity, which is not only electrochemical but also, and very importantly, chemical,
 246 as it can be suggested from the generation of by-products of reactions shown in Figure
 247 3.



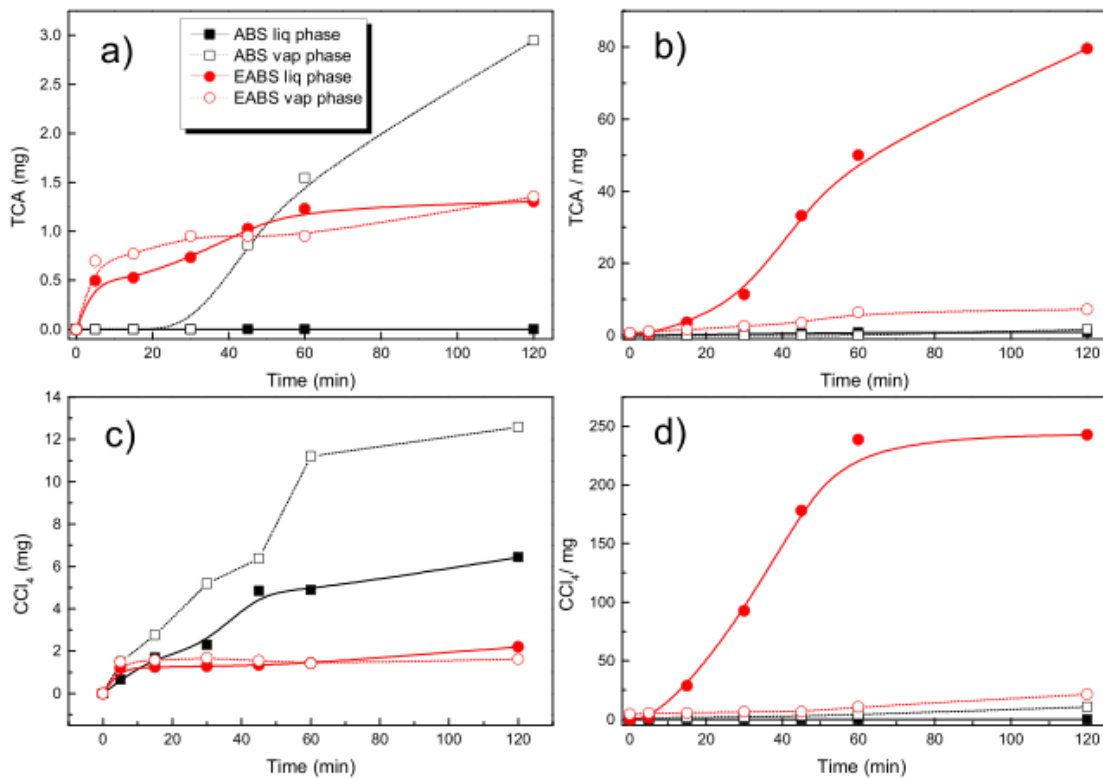
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249 **Figure 2.** Mass decay of Perchloroethylene during the scrubbing operation (■) and
 250 electro-absorption treatment (EABS) (●) as a function of the time. Samples analyzed in
 251 the a) PCE tank and b) Absorption (ABS) column. Full points: liquid phase and empty
 252 point: gas phase.

253 Thus, two important by-products were identified during the ABS and EABS in rather
 254 high amounts by High Performance Liquid Chromatography (HPLC): carbon

255 tetrachloride (CCl_4) and trichloroacetic acid (TCA). An important observation is that
256 both compounds are not only observed in the absorbent but also in the gases monitored
257 in both circuits. Thus, it can be seen the slight increase of the trichloroacetic acid and
258 carbon tetrachloride in the PCE stripping tank, especially in the vapor phase. These by-
259 products are not observed when the solution contained in the PCE stripping tank is not
260 stripped and passed throughout the column and this observation may indicate that their
261 production is carried out in the gas phase by wet decomposition of the PCE and, then, it
262 is transferred to the liquid phases. In addition, as both compounds are observed in the
263 system without the electrolyzer, their formation must be explained not by
264 electrochemical but by chemical processes. Anyhow, it is important to point out that the
265 amounts are very low in the single ABS process. However, they are very important in
266 the EABS and this observation indicates that decomposition of the PCE is accelerated
267 by the electrolytic processes produced in the electrochemical cell. In fact, it is important
268 to point out the very high concentration of both products in the liquid phase, which
269 suggest their generation by the electrochemical reaction of PCE in this phase. Anyway,
270 both compounds are also contained in the gas phase, which can be explained by the
271 liquid-gas transfer or by the previously commented wet chemical formation of both
272 species. CCl_4 seems to be the primary final product of degradation in the EABS process
273 and TCA is also a very important final product. This is not what it was initially
274 expected, because there is no mineralization but simply transformation into other
275 products with the only advantage of their lower volatility in the case of the TCA and the
276 higher solubility in water in the case of the CCl_4 and TCA respect to PCE (1160 mg/L
277 (CCl_4) and 54000 mg/L (TCA) vs 206 mg/L at 25°C (He, 2003; Schneider, 1983;
278 Verschueren, 2008). Moreover, it was observed an increase of pH in the column during

279 the EABS from 6.0 to 11.3 in the phase liquid. In the PCE stripping tank, no important
280 changes were observed, remaining around pH 6.0.

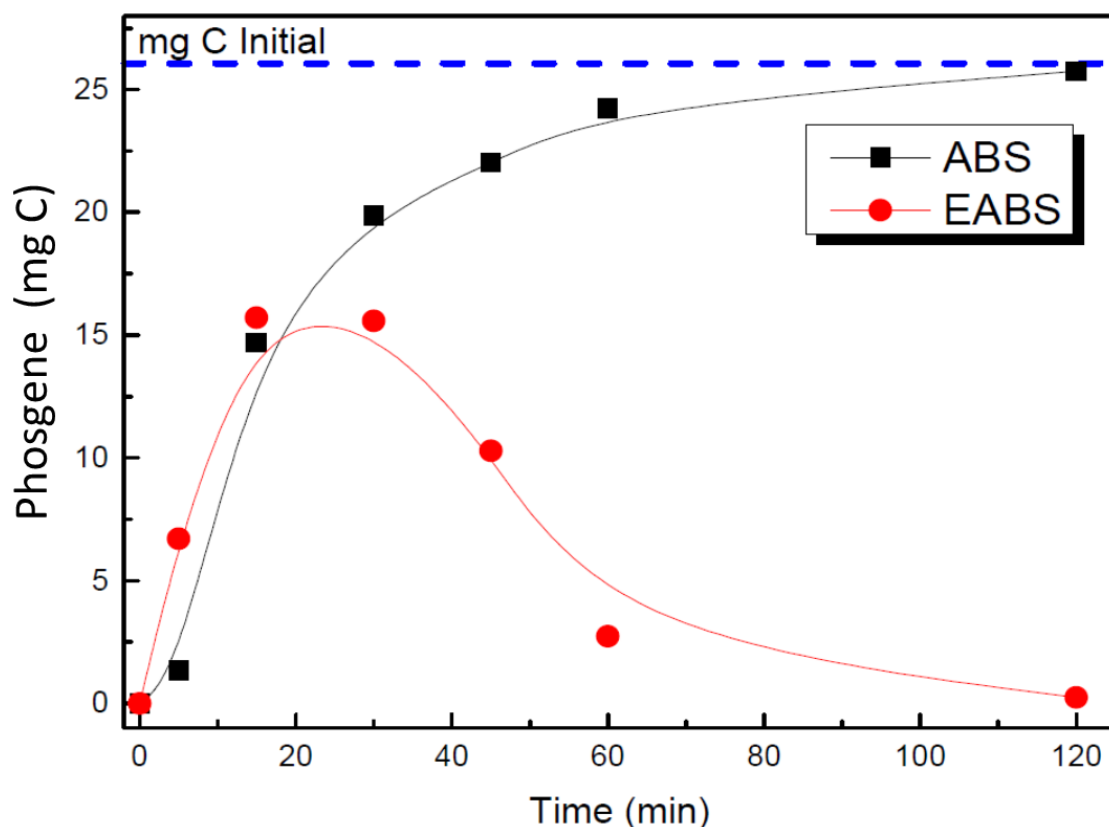


281

282 **Figure 3.** Mass decay of by-products generated during the (■) ABS process and EABS
283 treatment (●) as a function of the time. a) TCA mass in PCE tank b) TCA mass in ABS
284 column; c) CCl₄ mass in PCE tank; d) CCl₄ mass in ABS column. Full symbols
285 represent liquid samples and empty symbols are gas samples.

286 Another important point to be highlighted is that mass balances informs about the
287 formation of a third intermediate which is not detected by either HPLC or GC-ECD
288 chromatography. However, according to UV spectrum it absorbs light a 365 nm (Xie et
289 al., 2017), which is consistent with its identification as phosgene, a very volatile product
290 whose formation is promoted during the wet decomposition of PCE. Phosgene have
291 been related in literature as by-product of PCE promoted by hydrolysis reaction that
292 occur at humid medium. In this case, phosgene could not be detected as by-product due

293 to its decomposition during the gas chromatography processing. Thus, this compound
294 is known to easily decompose to TCA and carbon tetrachloride. Amounts of phosgene
295 produced are shown in Figure 4, where it can be seen that it has a behavior of
296 intermediate during EABS processes while it behaves almost as final product in the case
297 of the bare ABS. Anyway, the detection to TCA and CCl_4 indicates the partial
298 hydrolysis of these species, which is not favored when the current is not applied in the
299 electrolyzer.



300

301 **Figure 4.** Phosgene mass generated during the (■)ABS process and EABS treatment
302 (●) as a function of the time.

303 **Photo-electroabsorption.** It is known in the literature that PCE is capable to absorb
304 light especially with short UV wavelengths. Thus, direct photolysis of PCE with UVC
305 can leads to ionization resulting in removal of chlorine radicals from PCE molecules. In

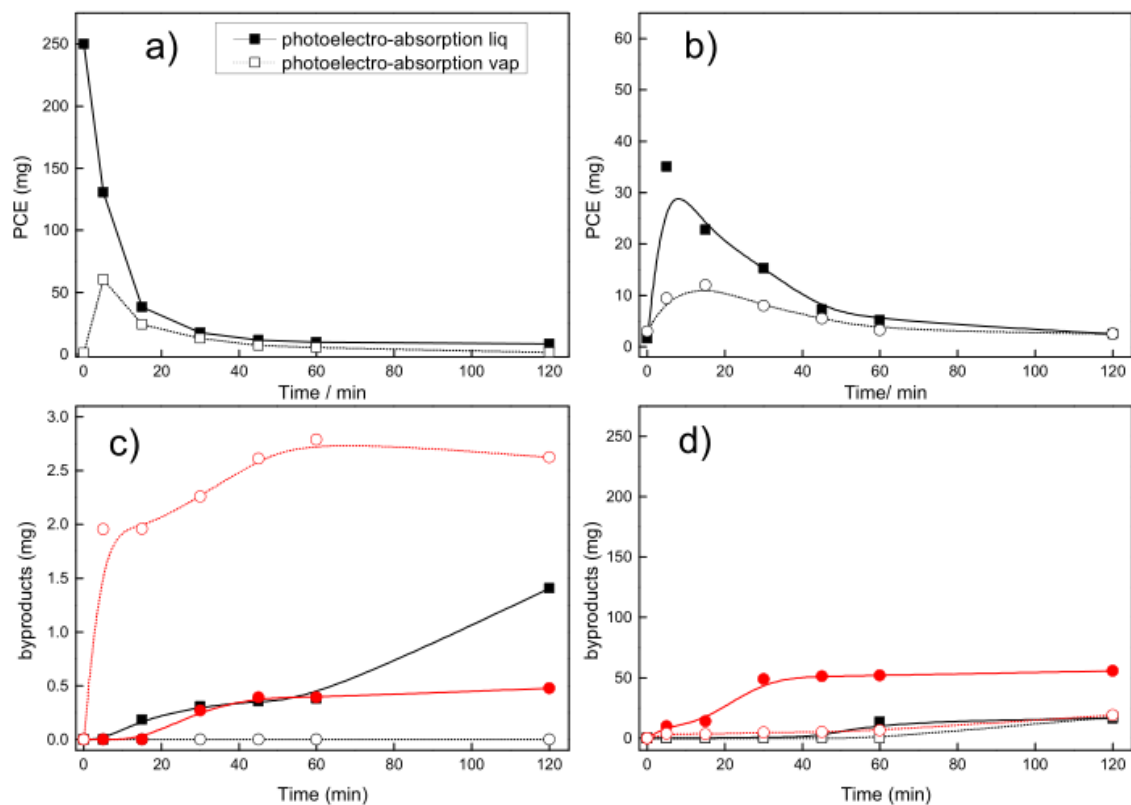
306 addition, it is well-known the formation of oxidants during electrolysis, such as
307 hydrogen peroxide, ozone and peroxosulfates, which can be activated by UVC light
308 irradiation, generating hydroxyl and sulfate radicals. Consequently, these radicals can
309 promote the oxidation of organics. In this way, in order to enhance the removal
310 efficiency of PCE and mainly its by-products removal, UV light was coupled to EABS
311 (no significant changes were observed with just ABS).

312 Part A of Fig. 5 shows that the PCE in the tank presents the same behavior for the non-
313 irradiated ABS and EABS processes. However, in the absorption column circuit (Fig.
314 5b) the maximum PCE found was 30 mg, almost the half of that obtained by non-
315 irradiated processes (first-order kinetic constant was $5.87 \cdot 10^{-4} \text{ mol s}^{-1}$). This indicates
316 the positive influence of the UVC light on the transformation of PCE. Additionally, to
317 compare the degradation carried out when two or more processes are combined, the
318 synergetic index was calculated from kinetics according to eq 5 obtaining a value of
319 1.12 ($k_{\text{ABS}} = k_{\text{photo-ABS}}$).

$$320 \text{ Synergetic index} = \frac{k_{\text{PHOTO-EABS}}}{K_{\text{photo-ABS}} + k_{\text{EABS}}} = \frac{5.87 \cdot 10^{-4}}{3.85 \cdot 10^{-4} + 1.39 \cdot 10^{-4}} = 1.12 \quad (5)$$

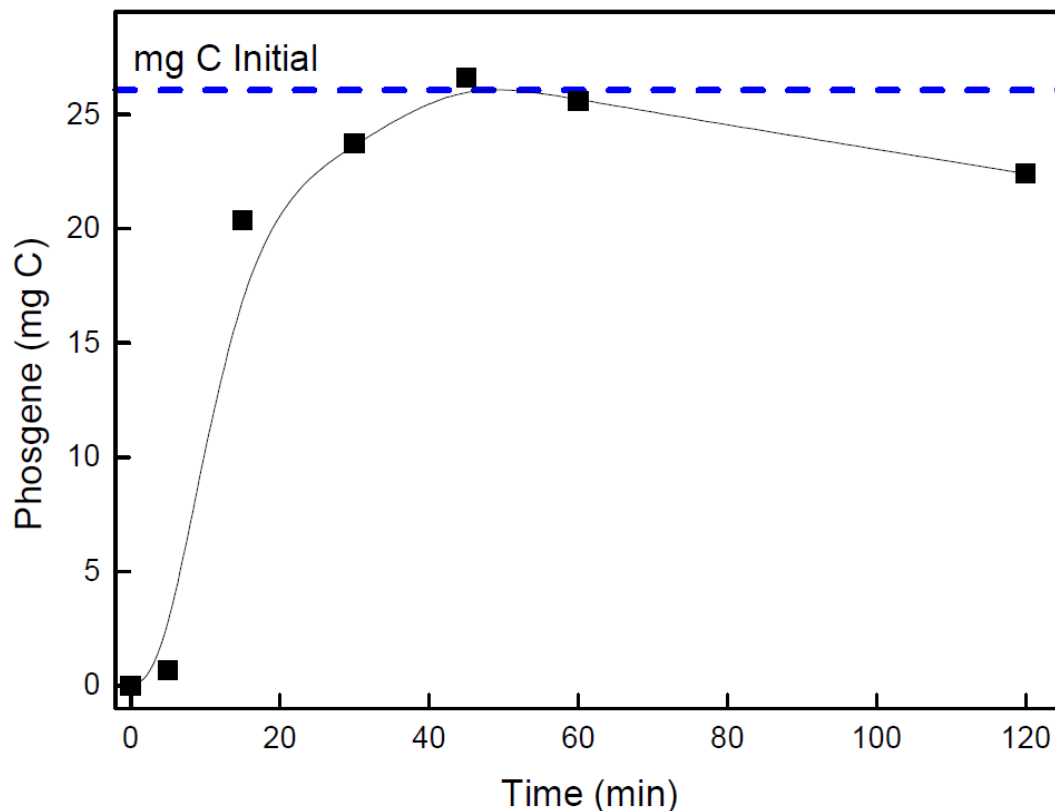
321 This value indicates that there is just a slight positive synergetic effect for the PCE
322 removal in the coupled process.

323 Regards to parts c and d of Fig 5., the main products generated shown by the HPLC
324 are, again, CCl_4 and TCA. Phosgene occurrence was also confirmed by UV spectra and
325 amounts formed are shown in Figure 6, where it can be seen a typical intermediated
326 profile, although the decomposition to final products is less favored than in the case of
327 the non-irradiated EABS process.



328

329 **Figure 5.** Changes in the amounts of PCE and intermediates in the photo-
 330 electroabsorption. a) and b) represents the mass decay of PCE; c) and d) by-products
 331 generated during the electro-scrubbing couple to UV treatment as a function of the time.
 332 a) and c) represents the samples analyzed in the PCE tank and b) and d) in the ABS
 333 column (■) TCA, (●) CCl₄; Full symbols represent liquid samples and empty symbols
 334 are gaseous samples.



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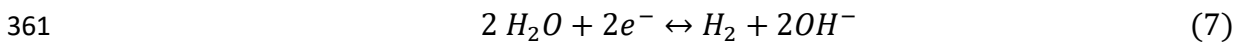
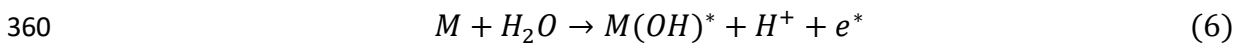
336 **Figure 6.** Phosgene mass generated during the photoelectro-absorption process.

337 Hence, the decomposition of oxidants into radical promoted by the UV irradiation does
 338 not seem to benefit the degradation of phosgene but to make it slower, indicating that
 339 the short lifetime of these radicals is negative in this case and pointing out that light
 340 irradiation does not have in this case a positive effect.

341 **Reaction mechanisms in the electro-absorption (EABS) of PCE.** The influence of
 342 current density and pH were studied by carrying out additional EABS tests at 0.8 A and
 343 8A at pH 6 (natural PCE solution) and pH 3.0. Fig. 7 shows the carbon mass balance for
 344 each compound in the end of the treatments. As can be observed, during the ABS
 345 process, only around 10 % in mass of PCE remains in solution being almost converted
 346 into phosgene, which is a bad news from the environmental point of view as this species
 347 is even more volatile than the PCE (vapor pressures of $1.6 \cdot 10^5$ vs $1.9 \cdot 10^3$ Pa at 20°C)

348 and even, it is considered more hazardous. It was reported that the production of
349 phosgene was inhibited when it is an increasing concentration of oxygen that does not
350 appear at single ABS process. However, this negative view has not been discussed in
351 previous works shown in the literature and it is a very important handicap to be
352 overcome, because the formation of these species does not depend on the treatment
353 technology proposed but it seems to occur naturally.

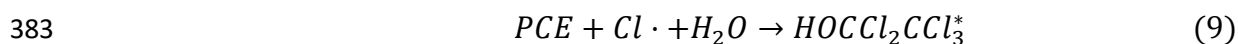
354 Comparing the EABS process at 0.8 A and 8.0 A, it is observed that at lower current
355 density the progress of the reaction of phosgene into CCl₄ and TCA is lower, and the
356 ratio of TCA formed seems to be higher. On the other hand, when higher current is
357 applied, it is promoted the destruction of phosgene because of the massive production of
358 hydroxyl radical and the local alkalization of the solution because of the hydroxyl
359 anions generated (eqs 6-7).



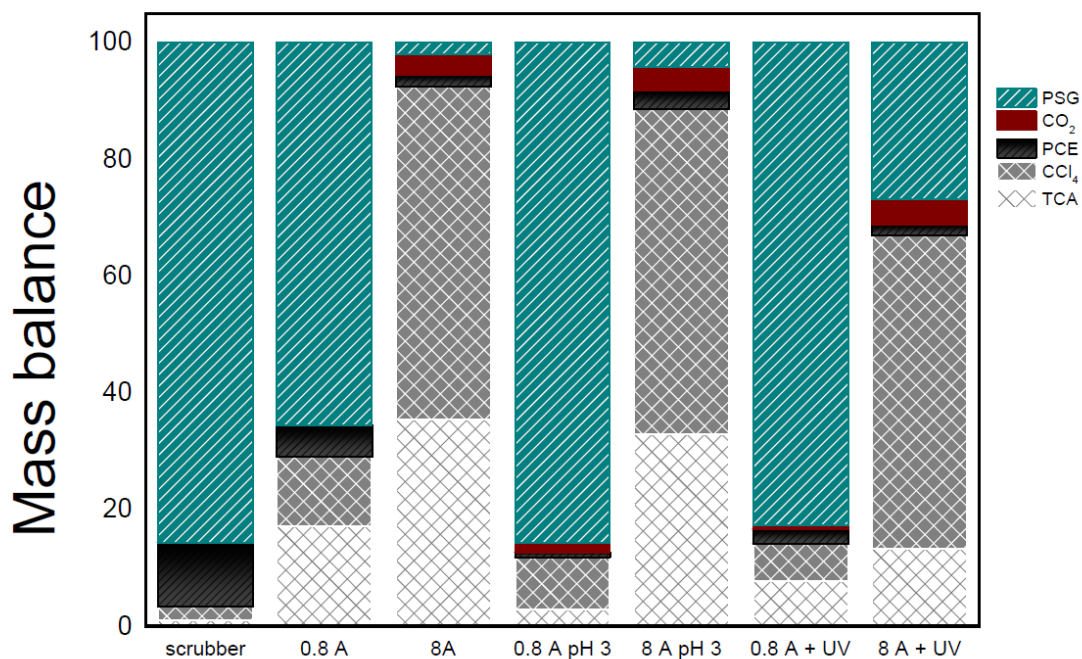
362 . Regarding to pH, it can be observed that acid medium contributed to PCE oxidation
363 and promote the increase of the phosgene generation at lower j. However, at higher
364 current densities, no significant differences were observed in terms of pH. Comparing
365 both current densities, when UV irradiation is coupled to the EABS, it is observed that
366 UVC light promotes the PCE photolysis decreasing its content in the end of the process
367 and favoring the phosgene generation. However, it does not favor the decomposition of
368 this compound.

369 These reaction products found in this work agree to those described in the literature and,
370 based on that, a mechanism can be proposed. So that, in Figure 8 it is proposed a
371 double pathway for the transformation of perchloroethylene. Thus, several studies have

372 demonstrated that the photochemical or photocatalytic conversion of PCE can occur
373 through two initiation steps: hydroxyl radical (HO•) and chlorine radical (Cl•) pathways
374 (Petit et al., 2007; Son-Jong Hwang, 1998; Yamazaki, 2001; Yamazaki, 2004).
375 Regarding the actions of these radicals, theoretical calculations indicates that HO•
376 addition to PCE is more exothermic than the addition of Cl• (43.8 and 9.2 kcal mol⁻¹,
377 respectively) (Yamazaki, 2001). Kinetic data point out that the reaction rate coefficient
378 for Cl• addition to PCE can be from 2.5 to several hundred times faster than the reaction
379 rate coefficient for addition of HO• to PCE (Nicovich, 1996; Petit et al., 2007; Thuner,
380 1999). This means that the addition of HO• to PCE can be expected to be negligible as
381 compared to the addition of Cl• (eq 8-9).



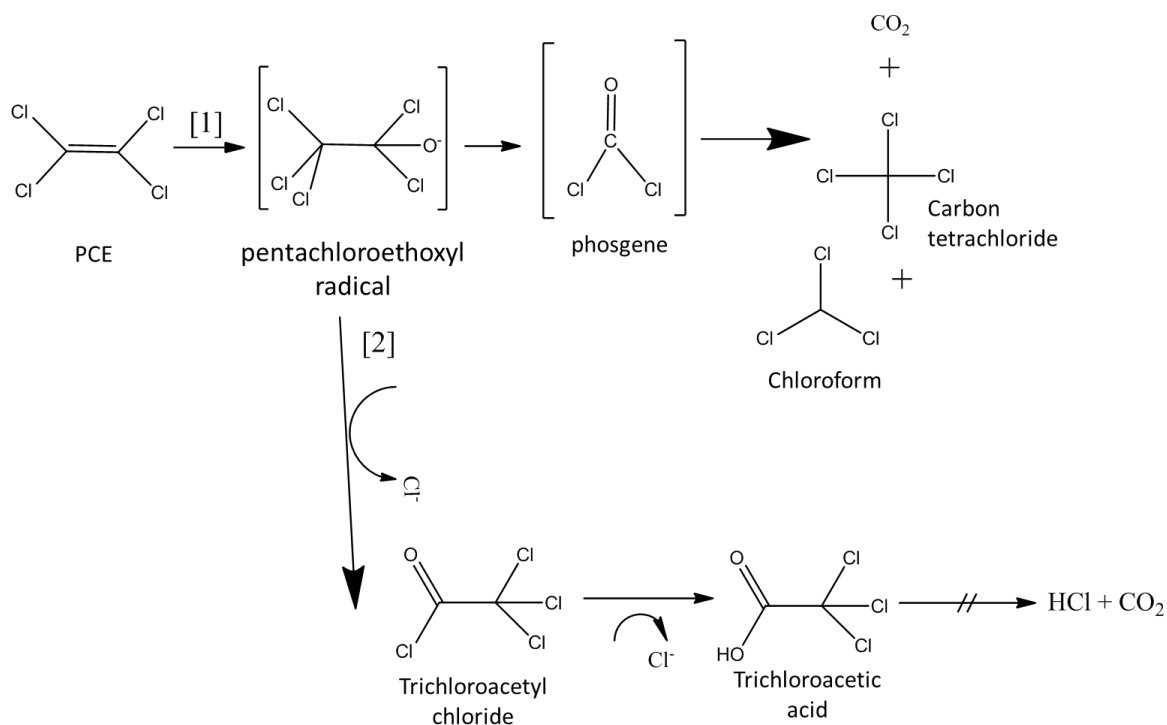
384 Thus, according to literature, PCE can suffer a reductive dechlorination under UV
385 radiation leading to the formation of trichloroethenyl radical, that reacts with water
386 generating trichloroethylene (C₂HCl₃). PCE can also react with Cl•, leading to the
387 formation of pentachloroethyl radical which, in turn, can react with O₂ generating
388 pentachloroethaneperoxy radical, followed by its dimerization, decomposing into
389 pentachloroethoxyl radical and oxygen. The cleavage of the C–C bond of the
390 pentachloroethoxyl radical yields to trichloromethyl radical and phosgene (CCl₂O)
391 formation (Feiyan, 2002; Yamazaki, 2004). The trichloromethyl radicals can react with
392 Cl• as well as with water, yielding to the by-products carbon tetrachloride (CCl₄) and
393 chloroform (CHCl₃), respectively.



394

395 **Figure 7.** Carbon mass balance calculated for PCE and its degradation subproducts
 396 generated during all process investigated ($\times\times\times$) TCA, (\square) CCl₄, (\square) Phosgene, (
 397 \square) PCE, (\square) CO₂.

398 On the other hand, the attack of chlorine radicals and the higher absorption efficiency
 399 promotes the generation of intermediates in the liquid phase with the formation of
 400 trichloroacetyl chloride that reacts very fast and synthesizes with chloride and hydroxyl
 401 radicals the trichloroacetic acid that mainly appears in the liquid phase where it is more
 402 stable. This route also was stimulated using an electrochemical process according with
 403 higher concentration observed in those experiments.



404

405 Figure 8. Proposed mechanism of reaction pathway for C_2Cl_4 degradation to different
 406 products considering the different adsorption processes evaluated.

407 Thus, according to the results shown, phosgene is produced always in ABS processes
 408 because of the wet hydrolysis of PCE (Meyer et al., 2001). Low current densities only
 409 attain a limited decomposition of this phosgene. Unexpected behavior occurs with UV
 410 irradiation which does not seem to favor the decomposition of this intermediate maybe
 411 because light does not promote the absorption process of PCE, so the high production of
 412 chlorine radicals are not effective to remove chlorine intermediates and just a trace
 413 amount of carbon dioxide was detected, showing an antagonist effect when an
 414 electrolysis at high current density and UV irradiation were combined. Anyhow, in the
 415 electrolysis, the ratio TCA/CCl_4 seems to be increased by working at these lower
 416 current densities which can be an interesting point for future work as TCA is a less
 417 hazardous and easier to degrade intermediate, with higher solubility and lower vapor
 418 pressure than parent PCE and the by-product CCl_4 . Opposite to what stated in other

419 works, mineralization of PCE is not favored and very low amounts of carbon dioxide
420 are detected, being more important when high current densities are applied.

421 **Conclusions**

422 From this work, the following conclusions can be drawn:

- 423 • The absorption in a packed column is a viable method to remove PCE from
424 gaseous streams. However, considerable concentration of phosgene is formed
425 during the process due to the promotion of wet hydrolysis of perchloroethylene.
- 426 • Electro-absorption using a non-divided BDD electrolytic cell is capable to
427 promote hard oxidation conditions leading to different reaction pathways. Lower
428 current densities favors the phosgene formation while higher current densities
429 promote the generation of CCl_4 (mainly in gas phase) and TCA as main reaction
430 by-products in the liquid phase. Mineralization obtained is very low and
431 treatment costs increased seriously with the total power applied.
- 432 • UV irradiation does not have a positive impact on the treatment, leading to a less
433 efficient decomposition of phosgene, which was explained in terms of the
434 transformation of the oxidant electrogenerated into radicals.
- 435 • Efforts have been done in order to better understand the possible pathway route
436 of PCE degradation and their influence on the speciation. Conversion of PCE
437 into phosgene is a non-electrochemical process which is promoted by wet
438 conditions. Phosgene is transformed into CCl_4 , and TCA during electrolysis,
439 being this later by-product promoted at low current densities.
- 440 • Results were not as expected during the planning of the experimental work in
441 terms of treatment of PCE but it is important to take in mind that PCE
442 decomposition occurs in wet conditions, regardless of the applied technology,

443 and this work is a first approach to try to solve the treatment problems
444 associated in a realistic way. Despite results are not positive from the viewpoint
445 of the treatment technology, it is important to state that the treatment of this
446 gaseous streams is more difficult than expected and it is a challenging aspect
447 worth to be faced by other researchers.

448

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