Review

An Old Technique with a Promising Future: Recent Advances in the Use of 2 **Electrodeposition for Metal Recovery** 3 Yelitza Delgado, Francisco J. Fernández-Morales and Javier Llanos * 4 Chemical Engineering Department, University of Castilla-La Mancha, Avenida Camilo José Cela s/n 13071, 5 Ciudad Real, Spain 6 Corresponding author e-mail: javier.llanos@uclm.es 7 Abstract: Although the first published works on electrodeposition dates from more than one cen-8 tury ago (1905), the uses of this technique in the recovery of metals are attracting an increasing 9 interest from the scientific community in the recent years. Moreover, the intense use of metals in 10 electronics and the necessity to assure a second life of these devices in a context of circular econ-11 omy, have increased the interest of the scientific community on electrodeposition, with almost 12 3,000 works published per year nowadays. In this review, we aim to revise the most relevant and 13 recent publications in the application of electrodeposition for metal recovery. These contribu-14 tions have been classified into four main groups of approaches: 1) treatment and reuse of 15 wastewater; 2) use of ionic liquids; 3) use of bio-electrochemical processes (microbial fuel cells 16 and microbial electrolysis cells) and 4) integration of electrodeposition with other processes (bi-17 oleaching, adsorption, membrane processes, etc.). This would increase the awareness about the 18 importance of the technology and would serve as a starting point for anyone that aims to start 19 working in the field. 20 Keywords: electrodeposition; metal recovery; ionic liquids; bioelectrochemistry; integration of tech-21 nologies 22

1. Introduction

Electrodeposition (ED) has been studied as one of the key electrochemical technolo-24 gies for more than one century. According to the Scopus database, the first article about 25 electrodeposition was published in 1905 [1] and studied the electrodeposition of copper 26 upon iron. Since then, the scientific community has added new materials, methods, con-27 ditions and many other elements in order to improve this technique and its results and to 28 widen the range of potential applications. This growing interest has caused an exponential 29 increase in the number of publications regarding electrodeposition. Thus, Figure 1 shows 30 the number of works published, according to the Scopus database, related to the terms 31 "electrodeposition" or "electrochemical deposition". 32

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Figure 1. Number of papers published related to "electrodeposition" appearing in either abstract, title or keywords

As it can be seen in Figure 1, there is an exponential increase in the number of articles published in this topic, reaching a total amount of almost 56,000 papers and 3,000 articles in the recent 2020 (1771 in 2021 until July 23rd). This evolution means that, although electrodeposition is a mature technology, the range of applications in which this technique can be applied is widening, increasing the interest of the scientific community on its development.

In order to focus on the topic of this review, the term "metal recovery" was included 44 to refine this search. The results of this refined search in the Scopus database were ana-45 lysed by the software VOSviewer, a free software developed by Nees Jan van Eck and Ludo 46 Waltman at Leiden University's Centre for Science and Technology Studies (CWTS). Two 47 figures were created in order to show the countries that have devoted more interest to this 48topic (Figure 2) and the most used keywords (Figure 3). Moreover, the connections be-49 tween papers are also shown in these figures. In the case of Figure 2, the Figure was re-50 stricted to countries with a minimum of 13 publications, meanwhile for Figure 3, a mini-51 mum number of occurrences of an author keyword of 13 was also used in order to limit the complexity of the figures. 53

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Figure 2. Publication density of countries by years including the term "electrodeposition" and 56 "metal recovery". Minimum number of publications by country: 13. Figure made with the software VOSviewer.



Figure 3. Keywords of papers published per year including the terms "electrodeposition" and "metal recovery". Minimum number of keyword occurrence: 13. Figure made with the software VOSviewer. 62

Almost 1300 papers were found for this topic. As it can be observed in Figure 2, China 63 appears as the country which has devoted the highest interest in the development of elec-64 trodeposition for metal recovery. It is followed by the United States, United Kingdom, 65 India and Japan. Regarding Figure 3, apart from electrodeposition and metal recovery 66 (terms included in the search restrictions), recycling, leaching, different metals, ionic liq-67 uids, microbial electrolysis cell, microbial fuel cell and wastewater treatment are among 68 the most common topics in this research field. 69

The use of electrodeposition for the recovery of metal ions is a topic closely related 71 to environmental applications, as the presence of heavy metals represents an environmen-72 tal issue of increasing concern, due to the massive use of metals in electronics and other 73 applications and its inherent bioaccumulation and potential risks for the human health 74 [2]–[6]. If this treatment is performed by electrodeposition, the removal of heavy metals is 75 performed together with its recovery, working on the field of circular economy, an essen-76 tial part of the main research programs worldwide including the Horizon Europe of the 77 European Commission. 78

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Based on this, the main aim of this paper is to review the most recent and relevant 79 applications of electrodeposition, focusing on the recovery of metals. According to the 80 most common topics of recent research work, the articles have been classified into four 81 different groups: 1) treatment and reuse of wastewater; 2) use of ionic liquids; 3) use of 82 bio-electrochemical processes (microbial fuel cells and microbial electrolysis cells) and 4) 83 integration of electrodeposition with other processes (bioleaching, adsorption, electrodialysis, etc.). 85

2. Treatment and reuse of wastewater by electrodeposition

Wastewater from industries, hospitals and domestic applications are an environmen-
tal issue of increasing concern nowadays [7]–[10]. As it is stated in several of the United
Nations Global Development Goals and it all the research programs worldwide, it is com-
pulsory to look for water treatments in order to obtain clean water without metals, plastics
and microplastics, pesticides and other pollutants [11]–[13].87

In this field, electrodeposition serves as a plausible technology to recover a wide spectrum of metals and to remove them from the target effluents to be treated. Table 1 gathers some of the most recent works in this field, including the main objective of the work, the effluent treated and the main conclusions obtained.

Generally, the articles published in the field are divided between those treating real wastewater [14]–[17] and those that elaborate a synthetic one [18]–[22] in order to simulate real effluents to set the material required for the installation, operational conditions, parameters to measure, elements to quantify and the equipment to use for it. 101

The common presence copper in both electronic or deplating wastewaters joined to 103 its high value of reduction potential (+0.34 V vs SHE) and its consequent facile electrodeposition. This metal is the most commonly studied in papers regarding the recovery of metals by electrodeposition, although the recovery of other metals as Co, Ni, Pd, Pb, Zn or Te 106 is also evaluated as it can be observed in Table 1. 107

In the recent papers published about metal recovery by electrodeposition, it is possi-109 ble to find several approaches to enhance the overall behaviour of the process. The first 110 interesting approach is coupling the cathodic recovery of target metals to the anodic oxi-111 dation of organic matter, as it is the case of the work of Gu et al. [14], who studied the 112 reduction of chemical oxygen demand (COD) by oxidation of plastic deplating 113 wastewater, obtaining a reduction of COD from 1360 mg L-1 to 378 mg L-1 after the elec-114 trochemical oxidation and a subsequent oxidation by H2O2. In the same line, Gu et al. [16] 115 evaluated the simultaneous removal of phenol and recovery of several heavy metals from 116 petrochemical wastewaters. 117

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Table 1. Most recent articles	published for treatment and reuse	e of wastewater (WW)	by electrodeposition for meta	al recovery

Objective	Water composition/process conditions	Conclusions	Ref.
Remove Ag ⁺ by precipitation, Cu ²⁺ by elec- trodeposition and reduce COD by oxidation of real wastewater from plastic deplating.	WW Composition: 5600 mg·L ⁻¹ Ag ⁺ ; 9069 mg·L ⁻¹ Cu ²⁺ ; 1360.00 mg·L ⁻¹ COD. Anode: Ruthenium- Iridium-Titanium (Ru-Ir-Ti) net. Cathode materials: copper sheet, titanium sheet, Ru-Ir-Ti net and graphite sheet. Current densities: from 35 to 95 mA/cm ² . Temperatures: from 15 to 45°C. Applied potential: 3.5-5.5 V.	Cu ²⁺ recover: up to 89.3% in 80 min; purity Cu ⁰ 98.34% by ICP. Optimal conditions: Copper sheet as cathode; cur- rent density: 75 mA/cm ² ; 1.5 cm electrode distance; 15 °C.	[14]
Compare Cu electrodeposition vs Cu pre- cipitation for treating the depleted solutions obtained in the biomachining of copper pieces.	WW composition: 9.0 g Fe ²⁺ L ⁻¹ ; 10.0 g Cu ²⁺ L ⁻¹ ; pH 1.8. Electrodes: Pt Winkler. Temperature: 24 ^o C Constant voltage (10 V) vs constant current (2 A) compared.	Both alternatives need previous Fe removal and al- lows Cu recovery (>98%) at reasonable cost. Constant voltage operation preferred with an esti- mated cost of 1.43 €·kg ⁻¹ Cu.	[18]
Removing Cu(II), Co(II), Ni(II) and Ag(I) from wastewater while generating high- power electric energy.	Synthetic WW: CuSO4 (0.0005-0.3 M); CoSO4 (0.01-0.1 M); NiSO4 (0.01-0.1 M; (NH4)2SO4 1M. Electrodes. Cathode: copper; Anode: zinc Cathode: stirred with an egg-shaped stir bar Temperature: 18-23°C. Applied potential: 0.13-0.32 V.	Cu recovery: >90% Optimal energy density of 4888 Whm ⁻³ Optimal power density of 546 Wm ⁻²	[19]
Study and optimization of copper recovery with pulsed electrodeposition.	Real WW from jewellery industry: 0.21 mg·L ⁻¹ silver, 0.79 mg·L ⁻¹ nickel, 430 mg·L ⁻¹ copper, <15 ppm gold and 8.3397 ± 0.66 g·L ⁻¹ cyanide; pH 1,74. pulsed electrodeposition (30 min) Rotating cathode, Pattern 616A – Princeton Applied Research Anode: hollow cylindrical platinum mesh	33.59% copper removal (with 10 ms pulse, 190 mA, 70 rpm, and 37 °C) with a deposition efficiency of 84.36% in 30 min.	[15]
Recovery of electric energy, water, and met- als through an autonomous electrochemical- osmotic system (EOS).	Synthetic WW from copper-laden: CuSO4. Electrode: Hydrophilic carbon fiber Anode: iron plate Cathode: carbon fiber Polyamide thin-film composite (TFC) FO, asymmetric TFC FO membrane and seawater reverse osmosis membrane. 10 mV at open circuit and variation of cell voltage from 0.2 to 0.8 V.	Maximum electric power density of 10.5 W·m ⁻² using a spontaneous Fe/Cu ²⁺ galvanic cell. 98,6% recovery Cu. Electric energy production of 3.3 kW·h using a 1.0 m ² area membrane produces 1 kg copper and 100 L of water in 122 h of operation.	[20]
Recovery of Cu with jet electrodeposition at high current density and efficiency.	Synthetic electroplating WW: 500 mg·L ⁻¹ Cu ²⁺ , 3.15 g·L ⁻¹ SO4 ²⁻ ; pH 1. Anode: RuO ₂ - coated Ti tube. Cathode: pure Ti sheet. Applied voltages: -1 to 0V.	97.4% recovery of Cu ²⁺ with current efficiency of 76.3% and current density of 12 A·dm ⁻² . Total energy consumption: 5.6 kW·h·kg ⁻¹ .	[21]
Recovery of heavy metals and simultaneous removal of phenol from multicomponent acidic media.	Real WW from petrochemical refinery. 500 mg·L ⁻¹ Cu ²⁺ ; 100 mg·L ⁻¹ Zn ²⁺ ; 200 mg·L ⁻¹ Pb ²⁺ ; 50 mg·L ⁻¹ Cd ²⁺ ; 50 mg·L ⁻¹ phenol Anode: IrO ₂ - Ta ₂ O ₅ coated Ti tube. Cathode: stainless steel. Cyclone electrochemical reactor system. Applied potential: -0.44 to -0.40 V	100% Cu recovery. Noticeable recovery of Zn, Pb and Cd and removal of phenol Energy consumption of 1.2·10 ⁻² kW·h for a 5 L batch	[16]

Electrochemical recovery of copper and nickel from acid pickling solutions at pilot scale.	Aqueous water acid pickling solutions: Ni (6-19 g·L ⁻¹); Cu (2-74.1 g·L ⁻¹); COD (1250- 40000 mg·L ⁻¹); H ₂ O ₂ (0-5 mg·L ⁻¹); pH (1-6); Conductivity (20.3-232 mS·cm ⁻¹) Anode materials: DSA®, graphite and lead. Cathode materials: Stainless steel and brass. Current density: 3-30 A·dm ⁻² . Temperature: 25-50°C. Applied potential: 0.1-0.89 V.	Optimal removal of Cu: 100 % laboratory; 40 % pilot. Very low Ni removal (<20 %). Optimum energy consumption: 2 kWh·kg ⁻¹ Cu. Promising results for Cu recovery from cost analysis.	[23]
Copper recovery from treated wood waste by sulfuric acid extraction and electrodepo- sition.	Real WW from wood waste: copper quaternary (1890 mg·kg ⁻¹ Cu) and copper az- ole (1890 mg·kg ⁻¹ Cu) Intensities from 1 to 10 A. Anode: titanium coated with iridium oxide (Ti/IrO ₂). Cathode: stainless steel or copper.	92% Cu deposition at 10 A for 90 min. 65 US\$ tn ⁻¹ of profit for wood waste treatment using electrodeposition according to an economic analysis.	[17]
Tellurium recovery from spent Te electro- lytes by cyclone electrowinning.	Composition of Te electrolytes: 40.02, 4.96, 4.64 and 0.52 g/L of Te, Sn, S and As, respectively and 39.00, 8.00, <1, <1 and 132.91 mg/L of Se, Mg, Pb, Cu and NaOH, respectively. Anode: IrO2–Ta2O5-coated titanium. Cathode: Titanium (Ti) sheet or stainless steel sheet (316L SS). Applied potential: 1.8-2.15 V.	82.89% of maximum. 99.90% purity of Te deposits, 95.61% of current effi- ciency and 1810.58 kWh·tn ⁻¹ energy consumption.	[24]
To recover Co and Ni through cementation (electrochemical deposition) with Al pow- der as electron donor.	Synthetic sulphate and chloride solutions: 1 mM Co/Ni; 4 pH. Process: 40 mm of shaking amplitude and 120 min ⁻¹ of shaking frequency at 25°C for 24 h of operation.	Recovery of 52-56% Co and 61-71% Ni from sulphate solutions. From chloride solutions: with 0.1 g AC dosage and adding Al a recovery of 61-70% Co and 70-99.9% Ni recovery from chloride solutions.	[22]
To recover palladium from spent hetero- genous catalyst from petrochemical indus- tries.	Acid solution (HCl/H2O2) with heterogeneous catalyst LD-265 (Pd/Al2O3). Three-electrode glass electrochemical cell. Electrodes: flat plate graphite.	99.07% Pd recovery with a purity of 94.02%	[25]
To recover copper by electro-electrodialysis (EED) from ammonia solutions.	Cu ⁺² concentrations from 0.01 to 0.1 mol·dm ⁻³ . Current density from 200 to 500 A·m ⁻² . Anode: titanium mesh coated with ruthenium oxide. Cathode: stainless steel. Applied potential: 2-4 V.	Almost 80% current efficiency in Cu recovery. Ammonia complexing agent can be reused.	[26]
To obtain high-purity copper deposits from complex mixtures by electrodeposition with a centrifuge electrode.	Synthetic WW: 2–9 g·L ⁻¹ Cu ²⁺ , 2–9 g·L ⁻¹ Ni ²⁺ , 5–40 g·L ⁻¹ H ₂ SO ₄ and 1.5 g·L ⁻¹ so- dium dodecylsulfonate (SDS). Bipolar centrifuge Ti electrode. Cathode face (Ti); anode face (IrO ₂ -Ta ₂ O ₅) Room temperature. Potential: 0.8-1.0 V.	99.9% copper purity obtained. The rest of metals can be also separated.	[27]
To recover uranium from aqueous solution into magnetite (Fe3O4) formed by iron anode dissolution and electrodeposition.	Synthetic WW: 0.5 to 10 mg·L ⁻¹ U; pH 1.6-10. Adsorbent: Fe ₃ O ₄ formed at the cathode (graphite) from iron (anode) dissolution. Sorption capacity: 53.6 mg·g ⁻¹ . Room temperature. Electrode gap from 4 to 19 cm. Potential: 10-30V.	Maximum removal of U (88%) at pH: 2.6, 30 V, 8-10 cm electrode gap.	[28]

To recover gold from cyanide solutions us- ing a static batch electrochemical reactor op- erating in an electrogenerative mode.	Cathode: three-dimensional cathodes: porous graphite and reticulated vitreous carbon (RVC) and two-dimensional cathode materials: copper and stainless steel plates). Anode: zinc. Synthetic WW: KAu(CN) ² with 500 mg·L ⁻¹ Au in 0.041 M sodium cyanide solu- tion. Anolyte: 0.10 M sodium cyanide solution. Cathode potential vs SHE: -0.1 - (-0.05) V.	 > 90% of gold can be recovered in 3 h of experiment for the cathodes studied. More than 99% gold was recovered in 1h of opera- tion using activated RVC. 	[29]
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The second way to improve the performance of electrodeposition is by proposing 121 novel reactor concepts with the aim of maximizing mass transfer or enhancing the reuse 122 of the treated effluents. One interesting approach is that used by Campenedo de Morais 123 Nepel and coworkers [15], who propose a pulsed electrodeposition with a rotating elec-124 trode in order to improve the removal of copper and the quality of the deposit. An addi-125 tional system was designed by Ning and coworkers [21], who proposed a jet design (jet 126 electrodeposition) that maximizes mass transfer by a direct injection of the solution on the 127 cathode surface or Wang et al., who propose a centrifuge electrode to enhance the recov-128 ery of copper into high-purity solids from complex matrixes [27]. With this approach, it is 129 possible to work at very high current densities (and thus at high recovery rates) maintain-130 ing also high recovery percentages and current efficiencies. A similar objective is obtained 131 with the design of cyclone cells, that promote high flow rate of electrolyte on the cathode 132 surface in order to enhance mass transfer of the process [24]. An additional interesting 133 approach is the so-called electro-electrodialysis (EED), that combines the proper use of 134 ion exchange membranes inside an electrochemical cell in order to allow the recovery of 135 the metal and the simultaneous reuse of a solution of interest [26]. Finally, Lu and cowork-136 ers proposed a system that promotes the adsorption of uranium on magnetite (Fe₃O₄), that 137 is produced on a graphite cathode from the Fe (II) dissolved from an iron anode [28]. Spe-138 cific details about the metal recovery percentages and efficiencies can be consulted in Ta-139 ble 1. 140

Additionally, a very recent approach to upgrade the potential uses of electrodeposi-142 tion for metal recovery is coupling this process with the generation of energy. This is the 143 case of the work of Wang et al. [19], who propose to apply the process called bimetallic 144 thermally regenerative electro-deposition battery (B-TREB), which uses waste heat to re-145 generate an ammonia solution that is used as the anolyte of a spontaneous galvanic cell 146 that produce energy by oxidation of zinc and electrodeposition of copper. The similar aim 147 is reached by using an electrochemical-osmotic system (EOS), that take advantage of the 148 high salinity of a copper containing wastewater to produce energy by promoting a spon-149 taneous electrochemical reaction involving the electrodeposition of copper and the oxida-150 tion or iron. Moreover, by placing an osmosis membrane between electrodes it is possible 151 to produce reclaimed water in the anodic compartment [20]. 152

3. Use of ionic liquids in electrodeposition

Ionic liquids (ILs) can be defined as organic ionic salts that are liquid at ambient or 154 near ambient temperature. Among its properties, it is worth noting their low or negligible 155 volatility, high thermal and chemical stability, high ionic conductivity, high solubility, low 156 flammability, moderate viscosity and high polarity [30]. This interesting combination of 157 properties have attracted an exponential increasing interest of the scientific community, 158 with a growing number or articles published and an increasing spectrum of potential ap-159 plications [31]. Among these applications, the low volatility and high electrical conductivity of ionic liquids, their potential applications electrochemical processes is continuously 161 increasing, including their use as electrolyte in batteries and fuel cells, electrode materials 162 for batteries/supercapacitors and carbon precursors for electrode catalysts [31]-[35]. 163

Electrodeposition is one of these potential applications of ionic liquids in electro-165 chemistry. The use of ILs in electrodeposition mainly tends to enhance the recovery yield 166 of heavy metals due to the high conductivity of ILs together with their wide electrochem-167 ical window, that prevent the concurrence of hydrogen evolution [36]. 168

Thus, Table 2 resumes the most recent and relevant papers published in the field, 170 including the main objective, the most relevant process conditions and conclusions 171 reached from these works and focusing mainly on those works devoted to the recovery of 172 metals. 173

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As it can be observed, ionic liquids are mainly used to replace aqueous environments 175 in order to enhance the recovery percentage of high value-added metals, as gold, palla-176 dium, copper or platinum and increasing current efficiency. In general terms, using a cer-177 tain percentage of ILs enhances the recovery of the target metal and allow to obtain this 178 metal as a power of a controlled size or morphology [37]-[40], including some works re-179 garding the formation of metal nanotubes [41]. It is also common to observe that the metal 180 recovery does not improve when the concentration of the IL increases above a given 181 threshold. 182

The use of ILs not only improves the recovery and morphology of the target metal but also increase the percentage of metal extracted from mineral ores or from electronic waste as waste printed circuits or used mobile phones [37], [38], [42]. In this line, an approach has been done when using mixtures of ILs to prepare a deep eutectic solvent mixture, which can be used to efficiently extract metals from mineral power and further recover them by electrodeposition [43].

Although the use of ILs in electrodeposition is gaining an increasing interest, some 191 issues should still be solved, as it is the case of the low thermal and chemical stability of 192 ILs, which hinders its reusability and thus increase its cost and environmental impact, and 193 the high viscosity of ILs, which may lead to low mass transfer coefficients and, consequently, to mass transfer limitations [44], [45].

The cost of ionic liquids is also an additional key aspect to consider for its use in the 197 recovering of metals by electrodeposition. Although there is not a comprehensive study 198 about the cost/benefit of using ionic liquids combined with electrodeposition, some works 199 have presented partial conclusions on this topic. Thus, Abbott et al. conclude that the high 200 cost and viscosity of ionic liquids make them better suited for the concentration of metals 201 from large volumes of aqueous metal solutions to reduced volumes of ionic liquids con-202 centrated in the target metals to be recovered [36]. Additionally, Magina et al. pointed out 203 in their recent review about the challenges and opportunities in the use of ionic liquids, 204 that the high cost of ionic liquids is one of the main drawbacks for the use of these group 205 of compounds [31]. In the same line, Parmentier et al. concluded that the use of 206 tetraoctylphosphonium oleate for cobalt concentration was more expensive in both 207 CAPEX and OPEX than a conventional process using ion exchange resins, although they 208 pointed out that it could be a promising alternative for the recovery of precious metals or 209 when the brine disposal is a matter of concern [46]. 210

To sum up, although the use of ionic liquids is a promising alternative, a detailed 212 study of the environmental and cost issues should be carefully performed for any appli-213 cation to be developed. 214

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Table 2. Use	f Ionic Liquids for metal recovery	

Objective	Process conditions	Conclusions	Ref.
Evaluating the properties of N,N,N-Dimethyl- butylammonium Methanesulfonate [DMBA][MS] for Pb electrodeposition from Pb-acid batteries.	Synthetic Pb solutions (from 0.025 M to 0.1 M Pb) with increasing water contents (from 20 to 60 %). Cathode: copper foil. Anode: lead wire. Stable electrode potential -0.510 vs SHE.	Electrochemical properties of IL strongly depend on water content and acid to base ratio. The morphology of the deposit depends on the poten- tial.	[47]
Studying the deposition of Ta nanotube arrays by porous anodic alumina (PAA) assisted electrodepo- sition using 1-butyl-1-methylpyrrolidinium bis(tri- fluoro-methylsulfonyl) imide ([BMP]Tf2N as sol- vent.	Cathodes: Sitall substrate with Ni/Cr adhesion layer and sputter-depos- ited gold layer on the top/ PAA template (100 nm wide/1 µm length pores). Anode: platinum wire. Potentiostatic deposition at -1.4 V at 200 °C.	The main component of nanotubes was tantalum pent- oxide. Synthesis of nanotubes up to 900–1000 nm long and diameters of 100 nm, characterized as semiconducting.	[41]
Comparing the efficiency of five new imidazolium ionic liquids for the extraction of Pt (IV) from mixed metal solutions and its further electrodeposition.	Pt extraction experiments from mixed metal solutions with Zn ²⁺ , Fe ³⁺ , Cu ²⁺ , Ni ²⁺ and Rh(III) (2 mM each). Cathode for electrodeposition: Cu film (10x10 mm). Potentiostatic deposition at -1.75 V.	ILs successfully extract Pt from mixed metal solutions. Pure Pt coating and Pt nanoparticles with diameters of 2–10 nm were identified as the electrolytic products.	[48]
Improving the recovery of copper from waste printed circuit boards (WPCBs) by replacing H2SO4 by the ionic liquid [BSO3HPy]· HSO4.	WPCBs powders dried and microwave-digested: 20.6% Cu; 4.55% Zn; 4.3% Al; 3.73% Fe; 2.36% Pb; 0.42% Sn. IL: [BSO ₃ HPy]·HSO ₄ . Slurry electrolytic system. Cathode: titanium net. Anode: graphite rod. Working conditions: 0.5 A for 3 h.	At the optimal conditions (10% H_2SO_4 was replaced by IL) the recovery rate, current efficiency, purity and particle size of copper powders were 90.94%, 70.68%, 81.69% and 2.30 μ m, respectively.	[37]
Enhancing the total metal recovery from waste printed circuit boards (WPCBs) by replacing H2SO4 by the ionic liquid [MIm]· HSO4.	WPCB metal-enriched scraps dried and microwave-digested: 71.96% Cu; 2.92% Pb; 2.43% Fe; 1.22% Al. IL: [MIm]HSO4. Slurry electrolysis system. Cathode: copper plate. Anode: ruthenium-plated titanium plate. Working conditions: 1.624 A (80 mA·cm ⁻²), for 4 h.	H ₂ SO ₄ substitution by IL increase recovery rate of Al, Fe, Sn and Zn but decreases that of Cu, Mg, Ni, Pb For 80% H ₂ SO ₄ replaced: total metal recovery: 85%; purity: 89%; current efficiency: 52%; particle size of cathode metal powder; 3.77 μ m.	[38]
To study copper leaching from waste mobile phones with different IIs and evaluate the influence of sev- eral operational variables.	Waste printed circuit boards (PCBs): 83.31% Cu; 3.35% Fe; 12.44% Zn. ILs: [Bmim]Cl; [Emim]Cl; [Bmin][BF4]; [Bmim][PF6]. Slurry electrolysis system. Cathode: titanium plate. Anode: carbon rod.	[Emim]Cl and [Bmim][PF6] are the best ILs for Cu leaching. Copper leaching efficiency was improved with the ad- dition of H ₂ O ₂ .Maximal Cu recovery of 92.65% with a current efficiency of 79.99%.	[42]
To improve the permeability of gold from aurocya- nide solutions with an ionic liquid-based polymer inclusion membrane (PIM) technology integrated with an electrodeposition unit.	[A336][SCN] as the extractant with PVDF as support. ED separated from the feed solution (50 ppm Au*) by a PIM. Cathode: copper. Anode: graphite.	98.6% Au transported and 96.4% deposited. A constant voltage (1.5 V) applied to the stripping so- lution enhances Au permeability. The PIM shows outstanding stability.	[49]
Extraction and recovery of neodymium from acidic medium using extraction by novel undiluted and non-fluorinated ILs and electrodeposition.	Nd acid solutions with concentrations between 5·10 ⁻⁴ and 5·10 ⁻² M. Ils: 1-octyl-1-methylpiperidinium octylphos-	Current efficiency higher than 83%. 48% purity in Nd deposits: crystallite rods of 3–70 μm in length and 0.5– 30 μm diameter.	[39]

	phitePip18-OP, 1-octyl-1 methylmorpholiniumoctylphosphiteMo r18-OP and 1-octyl-1-methylpyrrolidinium octylphosphitePyr18- OP. Potentiostatic electrolysis at -2 V. Cathode: copper disk electrode. Anode: neodymium rod.		
Extract gold from ore in bmmHS04.	Ore: Si0 ₂ (81%w/w), CaS0 ₄ (10%w/w), Fe ₂ 0 ₃ (6%w/w), Al ₂ 0 ₃ (2.5%w/w), Mn0 ₂ (0.3% w/w) and Ti0 ₂ (0.2%w/w); 42 g·tonne ⁻¹ Au. IL: 1 -butyl-3-methylimidazolium hydrogen sulfate (b _{mim} HS0 ₄). Current density: 5-200 mA·dm ⁻² . Cathode and anode: platinum.	Gold extraction in the presence of thiourea is high yielding (86%). Current efficiency of 30 % for the 20% bmmHS04 solu- tion at a current density of 5 mA·dm ⁻² .	[50]
Use ionic liquids as deep eutectic solvents (DES), for the recovery of different metals by electrodeposi- tion.	Dissolution of a mineral powder (multielemental: Cu, Fe, Pb, Ni, Zn, Al, Au, Co, Mn, Ag and Cr). IL: Choline chloride, malonic acid and ethylene glycol were used to make the hybrid DESs. Electrode: titanium. Anode: platinum.	With a small concentration of DES added, the recovery of Cu, Fe, Pb, Ni, Zn, Al, Au, Co and Mn increased. Ag and Cr recovery increases with a hight quantity of DES.	[51]
Removal of iron and boron by ionic liquid extrac- tion and recovery of neodymium by ED from voice coil motors (VCMs) waste.	Nd-Fe-B magnets from VCMs. ILs: phosphonium: tri-n-butyl phosphate (TBP) and triethylpen- tylphosphonium bis(trifluoromethylsulfonyl)amide ([P2225][TFSA]) Cathode: Cu substrate. Anode: prismatic Nd-Fe-B rod.	%recovery yield Fe: 95,1% with -1,75 V applied. %recovery yield Nd: 75% with -3,25 V applied 100% B removed.	[52]
To study gold(I) recovery from alkaline cyanide so- lutions by using hydrophobic imidazolium-based ionic liquids as extractants.	ILs: 1-butyl-3-methylimidazolium hexafluorophosphate ([C4mim][PF6]), 1-hexyl-3-methylimidazolium hexafluorophosphate ([C6mim][PF6]), 1-oc- tyl-3-methylimidazolium hexafluorophosphate ([C8mim][PF6]), and 1-oc- tyl-3-methyl-imidazolium bis(trifluoromethylsulfonyl)imide ([C8mim][Tf2N]). Cathode: copper. Anode: platinum foil. Potentiostatic electrodeposition at -1.2 V.	Recovery of 92% with 16 h electrolysis. Excellent stability of the IL	[53]
Recover palladium, ruthenium and rhodium by electrodeposition controlling the morphology and composition of the deposits.	IL: 1-butyl-3-methylimidazolium chloride (bmimCl). Electrodeposition of platinoids from bmimCl. Cathode: Stainless steel.	Recovery Pd: 51% with -1,2 V applied from bmimCl. Recovery Rh: 26,6% with -1,7 V applied from bmimCl. Recovery Ru: 10,1% with -1,0 V applied from bmimPF6.	[40]

4. Use of bio-electrochemical processes	217
The bio-electrochemical process is defined as a system where the electrochemical re-	218
actions are taking place with the contribution of a living system. In most of the cases, the	219
living systems are based on microorganisms, but also plants and higher organisms can be	220
used. In the bio-electrochemical processes, the living organisms mainly contribute to the	221
oxidation processes but also can contribute to the reduction processes.	222
	223
Depending on reaction spontaneity of the bio-electrochemical systems, these systems	224
can be defined as Microbial Fuel Cells (MFCs) or Microbial Electrolysis Cells (MECs). On	225
the one hand, MFCs carry out spontaneous oxidative and reductive half reactions, exert-	226
ing therefore a net energy flow. From the oxidative and the reductive processes chemicals	227
can be oxidized and reduced, leading to the removal of pollutants, the recovery of pre-	228
cious chemical, such as metals, etc. On the other hand, MECs carry out non spontaneous	229
oxidative and reductive half reactions, being necessary and energy supply to carry out the	230
reactions and causing, therefore, a net energy consumption [54], [55].	231
	232
When using bio-electrochemical systems for metal recovery, single, dual or multiple	233
electrochemical deposition cells can be used. The single configuration is the simplest. In	234
this configuration, the air acts as the final electron acceptor, being necessary its availability	235
on the cathode [56]. In the dual configuration, the anode and cathode are electrically con-	236
nected by an external conductor, whereas both compartments are separated by a mem-	237
brane [56]–[61]. Finally, the multiple configuration requires the participation of several	238
units electrically connected in series or parallel and hydraulically connected individual,	239
cascade, etc. With the multiple-cells configuration, a higher energy production and chem-	240
ical transformations can be obtained. Nevertheless, it has multiple electrical and hydraulic	241

In the literature, during the last years different new models or configurations have been developed with the aim to improve the performance of the bio-electrochemical systems. These modifications are very important because depending on the shape, (cylindrical, rectangular, etc.), the size, the superficial characteristics, and many other parameters, the mass transfer can be enhanced leading to an increase in the performance yields.

connections, so this can hinder the assembly [56], [62], [63].

In Table 3, the most relevant publications related to the metal recovery by using bioelectrochemical processes are presented. In these publications the main operational pa-251 rameters and performance of the biolectrochemical systems have been studied. 252

4. Use of bi

Table 3. Bio-electrochemical	processes for metal recovery

Objective	Process conditions	Conclusions	Ref.
Treating smelting wastewater by a biolectrochemical system (BES) coupled with a thermoelectric gen- eration (TEG), which uses the sim- ulated heat potentially available in the smelting factories.	Cathode fed with synthetic smelting WW: 267.59 mg·L ⁻¹ Cu ²⁺ ; 140.88 mg·L ⁻¹ Cd ²⁺ ; 130.16 mg·L ⁻¹ Co ²⁺ ; pH 1.8. Anode fed with simulated organic WW. BES operated sequentially as MFC and MEC (at 1 and 2 V). BES coupled with thermoe- lectric generator.	Cu ²⁺ , Cd ²⁺ and Co ²⁺ in smelting wastewater were sequentially (Cu-Cd-Co) recovered at a rate of 121.17, 158.20 and 193.87 mg L ⁻¹ d ⁻¹ , respectively. Cu ²⁺ recovered as Cu ⁰ , Cd ²⁺ recovered as Cd(OH) ² and CdCO ₃ , Co ²⁺ recovered as Co(OH) ² . COD removal of 60.55 \pm 1.22 %.	[64]
Co-treatment of municipal wastewater (anode) and acid mine drainage (cathode) by dual-cham- ber microbial fuel cells (DC-MFC).	Anode fed with a 50% municipal WW and 50% sewage sludge. Cathode fed with an industrial acid mine drainage: 42.53 mg L ⁻¹ Fe; 412.38 mg L ⁻¹ Zn; 51.50 mg L ⁻¹ Al; 248.00 mg L ⁻¹ Mg; 2.91 mg L ⁻¹ Cd; 1.34 mg L ⁻¹ Cu; 2.90 mg L ⁻¹ As; 36.48 mg L ⁻¹ Mn; pH 2.50. Two cells operated, one with a 100 Ω external resistance and other at open circuit potential. Electrodes: graphite rods. MFC voltage: 100-500 mV.	Both effluents simultaneously treated by the DC-MFC system 15% COD removal from municipal WW and 42, 84, 71, 77 and 55% removal of Cd, Cu, Fe, Al and Pb, respectively. Maximum volumetric power of 14,000 mW m ⁻³ with a MFC volt- age of 300 mV.	[65]
Observe the results in the start-up, maximum voltage output, power density, coulombic efficiency and microbial communities due to the different energy substrates used.	Synthetic AMD 348.87 mg·L ⁻¹ Cu ²⁺ , 45.06 mg·L ⁻¹ Fe ³⁺ , and 7.03 mg·L ⁻¹ Fe ²⁺ ; pH 1.8. MFC reactor (28 mL); resistance of 1000 Ω Anode: Carbon brush has the biofilm. Cathode: Carbon cloth treats the AMD. Membrane: Anion exchange membrane Anodic substrates: glucose, acetate, ethanol and lactate. Voltage output: 0-212 mV.	Acetate-fed-MFC showed the highest power density (195.07 mW·m ⁻²). All Cu ²⁺ ion (349 mg·L ⁻¹) was reduced as Cu ⁰ in 53 h. 100% re- cover Cu ²⁺ with lactate and ethanol. >90% recover Fe with abiotic, glucose, acetate, ethanol and lac- tate.	[66]
Elaborate a bioelectrochemically- assisted electrodeposition system for the removal and recovery of Pb and Zn.	Synthetic smelting WW: 115 mg L ⁻¹ Pb ²⁺ , 150 mg L ⁻¹ Zn ²⁺ , and small amounts of Cd ²⁺ and Cu ²⁺ (less than 1 mg L ⁻¹ each); pH 5. Bioelectrochemically-assisted electrodeposition system. Anode: carbon brush; 200 mL; inoculated with sludge fed with MWW (NaAc, 0.2; NH4Cl, 0.15; NaCl, 0.5; MgSO4, 0.015; CaCl ₂ , 0.02; NaHCO ₃ , 0.1; KH ₂ PO4, 0.53; K ₂ HPO4, 1.07; 1 mL trace element per litre). Catholyte: graphite rod; 200 mL simulated smelting WW. Membrane: anion exchange membrane (AEM). Temperature: 25°C.	Electrodeposition equilibrium constant $k_0 = 3.76 \text{ cm} \cdot \text{s}^{-1}$. Zn recovery: 98.7 ± 0.7 % in 6h with -1.2 V. Pb recovery: 98.5 ± 1.4 % in 10h with -0.75 V vs. Ag/AgCl. COD removal efficiency in the anode of 76.6% at 20h.	[67]
To demonstrate the feasibility of chloramphenicol (CAP) removal and Ag recovery.	 WW: 5 mS·cm⁻¹ conductivity. In MFC 300, 400 and 500 mg·L⁻¹ Ag (I); pH 1 and in MEC 20, 25 and 30 mg·L⁻¹ CAP. MFC (to recover Ag) and MEC [to convert CAP; copper foam as cathode electrode]. Electrode: several graphite fiber connected by titanium wire. Anode and cathode: graphitic carbon rod. Cation exchange membrane. Room temperature and pH maintained: 2. Applied voltage to MEC: 0.1-0.9 V. 	The optimum condition was 99.8% of Ag(I) in MFC and 98.8% of CAP in MEC. Process of 15 days. One control experiment was also carried out. The system was also operated under open circuit conditions (OCCs). 478.88 W·h·m ⁻³ energy saved.	[68]

To compare the efficiency of mi- crobial fuel cells (MFCs) with dual chamber and electrocoagulation (EC) for pH increase and Fe re- moval.	Synthetic Fe-rich AMD: 500 mg/L Fe; 2.4-2.5 pH. Both in batch reactors, Bioanode inoculated from municipal WW, AMD as cathode, an- ion exchange membrane (AMI7001), at room temperature, initial pH catholyte at 2.4-2.5. EC testing: electrode materials (Fe and Al), reaction times (15–90 min), current intensi- ties (100–500 mA) and at 6 V. Total volume of 500 mL Rotational speed of 200 rpm. Electrode: materials (Fe and Al), plates. Final pH catholyte: 7.3-7.4. MFC at open and closed circuit: total volume of 650 mL. Electrode: Graphite bars with a smooth surface. Final pH catholyte: 7.7-7.8. Initial pH anolyte: 6.3-7.1. Final pH anolyte: 6.2-7.5.	EC: The Fe recovery of >94% was at 500 mA and 60 min. EC in its optimal conditions (Fe-electrodes, 400 mA and 60 min) was found to be more cost effective than MFC and more suitability for large-scale use. EC energy consumption is 9.6 and 3.6 kWhm ⁻³ for Fe and Al, re- spectively. Operating cost for EC is 0.56 and 0.81 \$-m ⁻³ for Fe and Al, respec- tively. MFC: Power density between 2 and 20 W·m ⁻³ . The Fe removal of >99% was achieved thanks to a 1000 mg·L ⁻¹ acetate at the begin- ning. Total cost of consumables for MFC 2,731 \$-m ⁻³ .	[69]
Study applied cell potential, initial cobalt concentration, pH of the catholyte, and the mesh size of the cathode on the performance of a new design of flow-by fixed bed bio-electrochemical reactor.	Synthetic WW: CoCl ₂ solution adjusting the pH by addition of NaOH or HCl. Anolyte: prepared solution with soil. Anode: rectangular porous UHP graphite with 20-26% porosity. Cathode: stainless steel screen (316-AISI) with mesh size 30, 40, and 60 in ⁻¹ . Cation exchange membrane (IONIC-64LMR). Temperature: 25±2°C. Initial concentration studied: 25; 50; 75; 100 and 125 ppm. pH studied: 1; 3; 5; 7 and 9. Voltages studied: 0.6; 0.9; 1.2; 1.5 and 1.8 V.	The best removal efficiency of cobalt is >99% with 1,8 V; 50 ppm initial concentration; pH of 7; a tack of stainless no. 30 steel mesh as a packed bed cathode; energy consumption 1,564 kWh·kg ⁻¹ co- balt.	[70]
Use of polyaniline coated elec- trodes to recover cadmium in sem- iconductor processing WW.	WW from semiconductor processing from a middle process: 400 mg L ⁻¹ Cd ions; 85 mg L ⁻¹ COD; pH 5.8. Electrodes: Polyaniline coated on carbon-base material (PAC). Temperature: 30-55°C. Initial pH: 7. Voltage: 5-20 V. Cadmium concentration: 200-800 mg L ⁻¹ .	92% turbidity removal, 89% of TSS; 90% Cd recovery and 72% of water reclaimed in 40 min. Polyaniline coated electrodes exhibit high capability for the elec- trochemical recovery of cadmium.	[60]
Study the effect on copper elec- trowinning of the cyanide/copper molar ratio, the potential applied to the electrolytic cell, the temper- ature and circulation rate of the so- lution, and the use of synthetic so- lutions using electrolytic reactors in discontinuous, discontinuous with recirculation, and continuous flow regimes.	Synthetic WW from mining company: [CN]/[Cu] 3, 4 and 5 molar ratios; pH 10.9 and 6.8 mS·cm ⁻¹ . Copper electrowinning (1 h) in discontinuous regime (stirred at 600 rpm) and Copper electrowinning in discontinuous regime with recirculation (stirred by recirculating): electrode spacing of 3 cm, graphite anode, 304 stainless steel cathode. Copper electrowinning in continuous regime with recirculation: three plate electrodes, graphite anode, two stainless steel cathodes. Applied voltages: 3; 4; 5 and 6 V. Temperatures: 25; 40; 60°C.	The best option, according to them, is 50% copper removal ap- plying 4V. But they achieve 79% Cu removal with 4V, [CN]/ [Cu] of 3, an 1h of electrowinning and 25°C. And 99,90% Cu removal with 6V, 60°C, 1h of electrowinning and recirculation rate of 160 cm·min ⁻¹ .	[71]
Recovery of copper in-situ in an enhanced microbial copper recov- ery cell varying voltages, run it in	Synthetic WW from low-strength copper-laden water (0.4 g·L ⁻¹ sodium acetate, 4.28 g·L ⁻¹ Na ₂ HPO ₄ , 2.45 g·L ⁻¹ NaH ₂ PO ₄ ·H ₂ O, 0.31 g·L ⁻¹ NH ₄ Cl, 0.13 g·L ⁻¹ KCl, 5 mL vitamins and 12.5 mL minerals). Electrically enhanced microbial copper recovery cell (MCRC).	Maximum current density: $1.62 \pm 0.01 \text{ A} \cdot \text{m}^{-2}$. The maximum copper removal efficiency of 95.4 ± 0.9 % was obtained thanks to maximum current density, initial concentration of copper of 5 mg·L ⁻¹ and 0.8 V applied.	[72]

open circuit mode and doing one abiotic	Anolyte: Inoculated with domestic wastewater. Anode: Heat-treated carbon fiber brushes. Cathode: Graphite sheets. Voltages studied: 0; 0.4; 0.8 V. Anion and cation exchange membrane.		
Recover copper with two control strategies: maximum power point tracking (MPPT) and the applica- tion of 0.5 V doing 3 experiments with different WW.	Temperature: 23 ± 3°C. Real and synthetic WW from distillery effluent: 20 L copper sulphate varying the concentration (1000 and 50 mg·L ⁻¹) and real WW, 1.5 g·L ⁻¹ NaCl; pH 4 and 2.5 mS·cm ⁻¹ conductivity. Two hydraulically cells connected. Anode: Four previously enriched helical. Cathode: copper foil. Anaerobic cathodes separated by polypropylene separator. Tube anion exchange membrane AEM and a cation Exchange Membrane (CEM) tube. Temperature: 23-25°C. 0.5 V applied voltage.	The recovery percentage depends on the starting concentration. Recovery of Cu 60-95%. The recovery was low when the anode was supplied with cop- per depleted distillery waste.	[73]
Recover platinum through char- ring biofilms in MFCs, studying its distribution and generating Pt/C catalyst.	Synthetic WW: 32.92 g·L ⁻¹ K ₃ [Fe(CN) ₆], 5.46 g·L ⁻¹ Na ₂ HPO ₄ ·12H ₂ O and 1.22 g·L ⁻¹ NaH ₂ PO ₄ ·2H ₂ O; 7.0–7.2 pH. 5 rectors, one of them was the abiotic. The reactors differ from Pt initial concentration. Electrodes: graphite plate. Anolyte: inoculated with the anaerobic sludge. Cation exchange membrane (CEM, 13 cm ² , CMI7000, Dupont, USA). Temperature: 25 ± 1°C. Voltage: 0-0.8 V.	Around 40% Pt was recovered. Each batch process worked for 24h. Maximum power density of 844.0 mW·m ⁻² , having 2.11 mg·L ⁻¹ Pt(IV).	[74]

Nowadays, the bio-electrochemical systems seem to be a very interesting option of metal 255 recovery from effluents. This is because these systems allow to reach simultaneously two 256 objectives: on the one hand, the metal recovery and on the other hand, the energy gener-257 ation. The bioelectrochemical processes can be coupled with other technologies or pro-258 cesses, like coupling with a thermoelectric generation [64] or electrocoagulation to in-259 crease the pH and remove iron [64], [69]. With the last, more than 94 and 99% Fe was 260 recovered by electrocoagulation and MFC, respectively. Both obtained great results, but 261 the MFC configuration yielded better results [69]. 262

In the scientific studies, different substrates were fed to the microbial culture of the anodic 264 chamber, being the most biodegradable those presenting higher yield in terms of electric-265 ity generation and metal recovery [66], [74]. In other cases, real wastewaters have been 266 coupled with the metals recovery in both synthetic and real AMD effluents [60] obtaining 267 high recovery yields of the metals presenting the highest reduction potentials, mainly Cd, 268 Cu, Fe, Al, Zn and Pb [65], [67]. The coupling between anode and cathode has been also 269 implemented with the objective of the antibiotic removal from hospital wastewater saving 270 478.88 W·h·m⁻³ of energy [68]. 271

When using electrically enhanced systems, microbial electrolysis cells, higher metal recovery yields were obtained. These systems has the advantage that it can be done *in situ* [72]. Novel flow-by fixed bed bio-electrochemical reactors are also under development, allowing to reach higher metal recoveries and energy generation efficiencies [70], [71].

In conclusion, to obtain better removals and recovers of metal is necessary to continue 278 studying the initial concentration, molar ratios of elements from wastewaters, pH of catholyte, applied cell potential, flow regimes, inter alia as it can be proved with the scientific articles mentioned above [63]–[73]. 281

5. Integration of electrodeposition with other processes

The last approach that will be covered in this review is the combination of electrodeposition with other technologies. In general terms, the main aim of combining other technologies with electrodeposition is either transferring the metal from a solid to a liquid phase or improving the process of metal recovery by a previous stage of concentration/purification. Table 4 shows a selection of recent combination of electrodeposition with other technologies for metal recovery. 287

As it can be observed, the use of leaching or bioleaching to extract the metal from a 290 solid to a liquid phase and thus allowing its recovery by electrodeposition is a common 291 approach. Bioleaching consists in the extraction of metals from their ores using living or-292 ganisms [75]. This technology has been extensively studied in order to enhance the metal 293 recovery from many different solid matrixes polluted with metals [76]-[82]. Therefore, the 294 coupling of bioleaching with electrodeposition has been extensively evaluated to recover 295 copper from printed circuit boards, obtaining very high copper purities in the final depos-296 its and metal recoveries ranging from 75.8% to 92.85% [83]-[85]. Additionally, this leach-297 ing can be also performed chemically, as it is the case of the work published by Wang et 298 al., who propose the combination of chemical leaching (by a combination of acid and H2O2 299 addition) to obtain ultra-pure Ag deposits from spent silver oxide button batteries [86]. 300

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Objective	Process conditions (regarding electrodeposition stage)	Conclusions (regarding electrodeposition stage)	Ref.
To extract copper from Printed Circuit Boards (PDBs) waste by using bioleaching and electro- deposition sequentially.	Bioleaching solution (mg·L ⁻¹): Cu: 2903; Ni:17; Fe: 400; Zn: 19; Mn: 6; Al: 180; Mg: 56; Na: 17 Cathode: 316 stainless steel sheet. Anode: titanium coated with mixed metal oxide (IrO ₂ -Ta ₂ O ₅). Current density: 10 mA·cm ⁻² . Electrowinning at 2 V cell voltage on average.	75.8% copper from PCBs (highest pulp density) was recov- ered with more than 99% purity as copper foil with a current efficiency of 80.6%. The optimum time for electrodeposition operation is 3h.	[83]
To recover metals (Zn, Pb and Cu) from PCDs of cell phone chargers by bioleaching and elec- trodeposition.	PCBs: 10.8, 68.0, and 710.9 mg·L ⁻¹ of Zn, Pb, and Cu, respectively. Cathode: steel plate. Anode: copper plate. Potential: 2.6-2.9 V; Intensity: 0.19-0.25 A; Time 2-3 h.	92.85% recovery of Cu. The use of non-pulverized PCBs for bioleaching of metals is recommended.	[84]
To recover high-purity copper from PCBs by bioleaching, sol- vent extraction and electrodepo- sition.	Bioleaching solution (g·L ⁻¹): Cu: 2.196; Fe: 2.791; Mn, Pb, Sn, Zn, Al, Ni:<0.012 Cathode: stainless steel. Anode: lead–calcium–tin. Potential: 1.9-2.0 V; current density: 200-250 A·m ⁻² ; Time: 24 h	Specific energy consumption 1.8-1.9 kWh·kg ⁻¹ Cu Current efficiency of 93%. >99.83% copper metal purity.	[85]
To recover silver from spent sil- ver oxide batteries by acid leach- ing and electrodeposition.	Raw material: spent silver oxide button batteries (SR44). Cathode and anode: glassy carbon. Potentiostatic ED: -0.6 to -0.05 V.	Ultra-pure silver (>99.98% wt.) is obtained. 98.5% metal recovery with 98.7% energy efficiency.	[86]
Recover Ni(II) ions from real nickel plating wastewater, with a pilot-scale fixed-bed ion ex- change resin and subsequent electrodeposition.	Real WW from nickel electroplating: 500 mg·L ⁻¹ Ni(II). Anode: RuO ₂ /IrO ₂ titanium plate. Cathode: titanium plate. Current density: 50–500 A·m ⁻² . Temperature: 30-70°C. pH: 1-5. Time: 8 h.	Ni recovery: 95.6%. Current efficiency: 95.8%. Energy consumption: 25.05 kWh per ton electroplating wastewater. Total cost: ¥ 80000 per ton electroplating wastewater.	[87]
To develop a membrane capaci- tive deionization (MCDI) system for water desalination and metal recovery.	Real saltwater: 500 mg·L ⁻¹ CuCl ₂ and ZnCl ₂ . Anode and cathode: activated carbon fiber attached onto the graphite sheet. Voltages: 0.4, 0.8. 1.0 and 1.2 V for desalination.	Recovery Cu ²⁺ : 42.8%. Adsorption capacity: 108.7 mg·g ⁻¹ Cu ²⁺ ; 122.6 mg·g ⁻¹ Zn ²⁺ . Current efficiency: From 24.1% to 36.5%. Energy consumption: from 1.24 W·h·g ⁻¹ to 1.65 W·h·g ⁻¹	[88]
To recover Cu(II) from wastewater through an ion ex- change process coupled with electrodeposition.	Wastewater: from 98 to 266 mg·L ⁻¹ Cu (II). Room temperature. Anode: platinum wire. Cathode: copper plates. Scanning potential: -0.7 to -0.5 V vs Ag/AgCl.	Energy consumption: 0.6 kWhkg ⁻¹ in electrolysis. Copper purity (96.38%). Cu recovery: 65% as electrolyzed copper.	[89]
To study the recovery of Cu(II) by a combination of polymer en- hanced ultrafiltration (PEUF) and electrodeposition.	Synthetic nitrate solution: 160 mg·L ⁻¹ Cu for PEUF stage; 800 mg·L ⁻¹ for electrodeposition. Rotating graphite cathode (60x60 mm square size; 10 mm thickness). Anode: Cylindrical porous graphite. Intensity: 0.15 A; pH: 2.	Electrodeposition is a viable via for polymer regeneration in PEUF. 100% copper recovery. Polymer used in PEUF is not affected by electrodeposition.	[90]

Other process that results interesting for enhancing the efficiency of electrodeposi-305 tion technique is ion exchange. The main aim of using an ion exchange resin is to increase 306 the concentration of the metal to be recovered in order to increase the efficiency of the 307 subsequent electrodeposition stage. Thus, when using an ion exchange, it works in cycles 308 of operation (production of a treated solution)-regeneration. This latter regeneration stage 309 is performed by adding an acid stream and it produces a concentrated metal solution that 310 is further treated by electrodeposition. With this approach, it is possible to recover nickel 311 with very high current efficiency (95.6%) [87] and to recover Cu from wastewater with 312 high purity (96.38%) and low energy consumption (0.6 kWh·kg⁻¹ Cu) [89]. 313

Further approaches have been done including the combination of membrane pro-314 cesses with electrodeposition. In this group, it is worth noting the combination of a mem-315 brane capacitive deionization with electrodeposition in order to simultaneously promote 316 the desalination of a water stream with the recovery of copper, concluding that the recov-317 ery of copper is possible by the combination of technologies proposed [88]. Another ex-318 ample of combination of membrane technologies and electrodeposition was proposed by 319 Camarillo et al., who combined the so-called polymer enhanced ultrafiltration technique 320 (PEUF) with electrodeposition as an efficient process for efficient copper recovery [90]. In 321 this latter work, PEUF uses a water-soluble polymer to recover and concentrate Cu(II) by 322 an ultrafiltration membrane. This concentrated is further treated by electrodeposition, a 323 technology that allows to recover copper and to simultaneously regenerate the polymer, 324 that can be used in a further PEUF stage. 325

To sum up, great recovering percentages, acceptable energy consumption and high327metal purities can be obtained from both solid and liquid wastes by properly combining328electrodeposition with leaching or concentration techniques.329

6. Conclusions

This review covers the most relevant and recent uses of electrodeposition for metal 331 recovery. From the information included in this this review, the following conclusions can be deduced: 333

- The scientific interest in the use of electrodeposition is continuously growing 335 since it was firstly reported in 1904. 336
- The use of electrodeposition in water treatment and reuse is probably the most important topic regarding the use of the technology for metal recovery, with the most recent works mainly devoted to the development of novel reactor configurations of enhanced mass transfer characteristics.
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- When using electrodeposition combined with ionic liquids, it is possible to obtain an elevated yield of value-added metals recovery and a controlled morphology and size of the deposits. The cost, stability and reusability of ILs is a matter of improvement for the development of the technology.
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- The attention devoted to the use of bio-electrodeposition systems is increasing 345 within the last years, being selection of the reactor configuration, operational 346 conditions and source of the inoculum are critical in order to obtain the best 347 performance of these systems. 348
- Electrodeposition is commonly coupled to other technologies that allows either to extract the metals from a solid phase or concentrate them in the liquid phase, leading to an upgrade of the metal recovering while saving energy.

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