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# Conversion of CO<sub>2</sub> to Fuels using Supported Cu Catalysts

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## Summary

Amid global warming concerns and skyrocketing CO<sub>2</sub> emissions in the atmosphere, mainly associated with the combustion of fossil fuels to produce energy, the research community has gained a large interest in CO<sub>2</sub> capture and reutilization to produce renewable fuels such as methanol (MeOH), dimethylether (DME) and additional hydrocarbons. MeOH is currently produced from syngas (H<sub>2</sub> + CO + CO<sub>2</sub>) over a Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalyst at mild temperature (200 - 270 °C) and high pressure (50 - 100 bar) and has a global demand exceeding 98 Mt/annum. Syngas is produced from the steam reforming of hydrocarbons, predominantly methane, and consequently the overall process has a great environmental cost (ca. 88 Mt GHG eq). Therefore, a more effective approach such as CO<sub>2</sub> hydrogenation to MeOH is required to enable the synthesis of CO<sub>2</sub>-neutral fuels whilst mitigating anthropogenic emissions. The catalytic conversion of CO<sub>2</sub> into methanol and DME bears a strong potential to transform large amounts of CO<sub>2</sub> in a short span of time due to the commonly reported high reaction rates. In order for the process to be sustainable in the light of the carbon cycle, H<sub>2</sub> should be produced in a greener way, e.g., photocatalytic water splitting and water electrolysis sourced by natural/renewable energy sources.

The literature surrounding the synthesis of methanol from CO<sub>2</sub> hydrogenation has predominately been based on Cu catalysts and this is due to its remarkable hydrogenation activity and abundance. Although many new active catalyst formulations have been developed, they still carry the problem of incorporating harmful/expensive elements, making them less valuable for commercial use. As such this thesis explores the use of various supported Cu catalysts; Chapter 3 investigates the effect of various supported Cu catalysts prepared via the oxalate gel synthesis method, with a particular focus on Cu/ZrO<sub>2</sub>, towards the conversion of CO<sub>2</sub> to MeOH. The role of various promoters (Pd, Pt, Ce, Ni and Ag) and the stability of these catalysts is also investigated. Chapter 4 explores the impact of varying the calcination temperature and reduction temperature of the Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel, towards their hydrogenation of carbon dioxide to methanol. The deposition of Cu onto the ZrO<sub>2</sub> polymorphs by oxalate gel and wet impregnation is also investigated to understand the effects of preparation method and support phase on catalytic activity. Finally, Chapter 5 investigates the synthesis of MeOH, DME and higher chain hydrocarbon between various CuZn or CuZr Zeolite integrated catalysts prepared *via* chemical vapour impregnation (CVI) and oxalate gel precipitation. Physical mixtures of the catalysts, as well as changes to the catalyst bed, are also explored in order to compare the catalyst activity.

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# Abbreviations and Units

At.%	Atomic percentage
Atm	Atmospheres
a.u.	Arbitrary units
BET	Brunauer-Emmett-Teller
cm	Centimetre
CP	Coprecipitation
CVI	Chemical vapour impregnation
DFT	Density functional theory
e-	Electron
Eq.	Equation
eV	Electron volts
FID	Flame ionisation detector
FTIR	Fourier-transform infrared
g	Gram
GC	Gas chromatography
GHG	Greenhouse gas
h	Hours
K	Kelvin
kg	Kilo gram
kJ	Kilo joule
L	Litre
mg	Milligram
MFC	Mass flow controller
min	Minute
ml	Millilitre
mmol	Millimoles
MPa	Megapascal

MS	Mass spectrometer
nm	Nanometre
OGP	Oxalate gel precipitation
PM	Physical mixing
RWG	Reverse water gas
TCD	Thermal conductivity detector
TEM	Transmission electron microscopy
TPR	Temperature programmed reduction
WI	Wet impregnation
wt %	Weight percent
XPS	X-ray photoelectron spectroscopy
XRD	X-ray powder diffraction
$\Delta G$	Change in Gibbs energy
$\Delta H$	Change in enthalpy
$\Delta S$	Change in entropy
$^{\circ}\text{C}$	Degrees celsius
$\mu\text{l}$	Microliter
$\mu\text{m}$	Micrometre

# Table of Contents

Summary.....	i
Acknowledgements .....	ii
Abbreviations and Units .....	iii
Chapter 1 .....	1
Introduction.....	1
1.1 – CO <sub>2</sub> Emissions and Utilisation .....	1
1.2 – Methanol Synthesis from Catalytic Hydrogenation of CO <sub>2</sub> .....	3
1.2.1 – Methanol Production in Industry .....	3
1.2.2 – Mechanism of Industrial Catalyst (Cu/ZnO/Al <sub>2</sub> O <sub>3</sub> ) .....	4
1.2.3 – Cu Catalysts for CO <sub>2</sub> hydrogenation to MeOH .....	7
1.3 – Indirect Conversion of CO <sub>2</sub> into Hydrocarbons.....	8
1.3.1 – Direct Vs Indirect Route.....	10
1.3.2 – Proposed Reaction Pathway .....	12
1.4 – Aims and Objectives.....	15
1.5 – References.....	16
Chapter 2 .....	23
Experimental.....	23
2.1 – Materials.....	23
2.2 – Catalyst Preparation.....	25
2.2.1 – Wet impregnation (WI).....	25
2.2.2 – Co-precipitation (CP) .....	25
2.2.3 – Oxalate Gel Precipitation (OGP).....	26
2.2.4 – Chemical Vapour Impregnation (CVI).....	26
2.2.5 – Physical Mixing (PM) .....	26
2.3 – Catalyst Testing.....	27
2.3.1 – Reactor Set-up .....	27
2.3.2 – Data Calculations.....	28
2.4 – Characterisation.....	30
2.4.1 – X-Ray Diffraction .....	30
2.4.2 – Brunauer–Emmett–Teller (BET) Surface Area Analysis .....	32
2.4.3 – N <sub>2</sub> O Pulse Titration to Determine Specific Metal Surface .....	33
2.4.4 – Temperature Programmed Desorption.....	34
2.4.5 – X-Ray Photoelectron Spectroscopy (XPS) .....	35

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2.4.6 – Transmission Electron Microscopy (TEM) .....	36
2.5 – References .....	37
Chapter 3 .....	39
Promoted Cu Catalysts Supported on ZrO <sub>2</sub> for the Hydrogenation of CO <sub>2</sub> to Methanol. ....	39
3.1 – Introduction .....	39
3.2 – Results and Discussion .....	45
3.2.1 – Effect of Support on Cu Catalysts Synthesised by Oxalate Gel Precipitation .....	45
3.2.3 – Pd Promoted Cu/ZrO <sub>2</sub> Catalysts .....	52
3.2.4 – Additional Promoters for Cu/ZrO <sub>2</sub> .....	58
3.2.5 – Catalyst Stability & Comparison between Cu/ZrO <sub>2</sub> and CZA catalysts .....	60
3.3 – Conclusions.....	65
3.4 – References .....	66
Chapter 4 .....	70
Phase Composition of Cu/ZrO <sub>2</sub> Catalysts and Their Impact on the Hydrogenation of CO <sub>2</sub> to MeOH..	70
4.1 – Introduction .....	70
4.2 – Results and Discussion .....	73
4.2.1 – Variation of Calcination Temperature .....	73
4.2.2 – Variation of Reduction Temperature .....	79
4.2.3 – Variation of Cu Deposition.....	81
4.3 – Conclusions.....	88
4.4 – References .....	89
Chapter 5 .....	91
Cu/Zn Zeolite Catalysts for the Indirect Conversion of CO <sub>2</sub> to hydrocarbons. ....	91
5.1 – Introduction.....	91
5.2 – Results and Discussion .....	94
5.2.1 – Cu/Zn Zeolite Catalysts Prepared by Chemical Vapour Impregnation (CVI).....	94
5.2.2 – Cu/Zn and Cu/Zr Zeolite Catalysts Prepared by Oxalate Gel Precipitation.....	99
5.2.3 – Physically Mixed Catalysts .....	112
5.3 – Conclusions.....	120
5.4 – References .....	122
Chapter 6 .....	124
Conclusions and Future Work.....	124

# Chapter 1

## Introduction.

### 1.1 – CO<sub>2</sub> Emissions and Utilisation

The combustion of carbon-based fossil fuels (oil, coal, and natural gas) for energy generation is accompanied by an enormous emission of anthropogenic greenhouse gases (GHGs) to the atmosphere, mostly in the form of CO<sub>2</sub>.<sup>(1)</sup> The impact of global warming and continued public and industrial interest globally has led to the drive in mitigation actions to reduce the global temperature rise and encourage the use of more sustainable and greener alternatives in the production of chemicals and the reduction of fossil fuel resources to reach the energy demand.<sup>(2-5)</sup> The annual global CO<sub>2</sub> emission in 2014 was recorded to be 39.25 Gt, of which fossil fuel emissions (including cement production) accounted for about 91% of the emissions from human sources. The distribution of the total emission comes from coal (42%), oil (33%), gas (19%), cement (6%), and gas flaring (1%). Consequently, the atmospheric CO<sub>2</sub> concentration increased from ~270 ppm in the pre-industrialization era to ~410 ppm in 2017, leading to serious climate change issues and detrimental ocean acidification.<sup>(6)</sup> As a result, various global initiatives like the Intergovernmental Panel on Climate Change and the United Nations Climate Change Conference (COP26, Glasgow, 2021; and COP21, Paris, 2015) have emphasized the urgency to mitigate CO<sub>2</sub> emissions by at least one-half of the current value by 2050, to limit the average global temperature increase to a maximum of 2 °C.<sup>(7, 8)</sup>

In the past decade, an immense amount of work has been done to reduce the impact of global warming and decrease GHG emissions, focusing on CO<sub>2</sub> sequestration and CO<sub>2</sub> utilization to synthesise valuable end products i.e. methanol, DME, formic acid, lower olefins, etc.<sup>(9)</sup> Carbon capture and storage (CCS), just as carbon capture and utilization (CCU), are believed to play a significant role in reducing the amount of released CO<sub>2</sub> in the atmosphere.<sup>(10, 11)</sup> In Europe the aim is for a 40% decrease in GHG emissions by 2030, compared to emission levels recorded in 1990.<sup>(12, 13)</sup> The technologies available for CCS and CCU continue to be developed every year, and there is an urgency to introduce a shift in the global energy base from fossil to renewable energy and greener fuels like hydrogen. These alternatives are considered important solutions to help reduce CO<sub>2</sub> emissions, but they do have a number of disadvantages: mainly the extensive changes that would need to be implemented in the energy infrastructure of the transportation sector, which could prove difficult and costly, as well as the political dilemma of introducing these changes in less developed geographic areas that rely on their abundant



fossil fuel deposits. The storage of CO<sub>2</sub> is also incredibly expensive and has high intensive energy requirements for separation and pumping, issues over the longevity and location of stored CO<sub>2</sub> in various sites, and an enlarged use of fossil C (from 20% to 60%) in the process.<sup>(14)</sup> For these reasons carbon utilization through CO<sub>2</sub> conversion is considered a more viable and practical option, as it is 20–40 times more efficient than sequestration over a span of 20 years.<sup>(15)</sup>

The catalytic conversion of CO<sub>2</sub> into methanol and DME bears a strong potential to transform large amounts of CO<sub>2</sub> in a short span of time, due to the commonly reported high reaction rates. In order for the process to be sustainable in the light of the carbon cycle (the process in which carbon atoms continually travel from the atmosphere to the Earth and then back into the atmosphere), H<sub>2</sub> should be produced in a greener way, e.g., photocatalytic water splitting and water electrolysis sourced by natural/renewable energy sources.

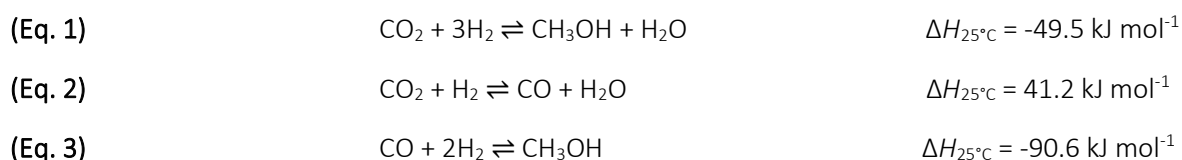
The production of methanol and its derivatives by alternative routes, and their use as fuels and chemicals, is the core of the methanol economy, a concept earlier proposed by Olah and co-workers.<sup>(16)</sup> In this conception, CO<sub>2</sub> is captured from any natural or industrial source, human activities or air by absorption and chemically transformed into methanol, dimethyl ether and varied products including synthetic hydrocarbons. According to Olah, methanol production from CO<sub>2</sub> is advantageous owing to the usage of non-fossil fuel sources (unlike syngas), avoidance of CO<sub>2</sub> sequestration (which is expensive) and the opportunity for mitigation of the greenhouse effect (by effective recycling of CO<sub>2</sub>).<sup>(17)</sup> Olah *et al.* emphasized that the chemical recycling of CO<sub>2</sub> to methanol (and dimethyl ether) provides a renewable, carbon-neutral, unlimited source for efficient transportation fuels, for storing and transporting energy, as well as convenient feedstock for producing ethylene and propylene and from them, synthetic hydrocarbons and their products. Thus, it essentially substitutes petroleum oil and natural gas. It allows the lasting use of carbon-containing fuels and materials and avoids excessive CO<sub>2</sub> emissions causing global warming.<sup>(18)</sup>

Recently, trends of R&D in methanol synthesis are shifting toward a greener process, where CO<sub>2</sub> is reduced by H<sub>2</sub> generated from the technology sourced by natural/renewable energies. Mitsui Chemicals and Carbon Recycling International (CRI) Inc. are the two well-known companies, among others, that have demonstrated such processes for production of methanol. The plant of the latter, CRI, located in Iceland, has a production capacity of around 5 million litres of methanol per year (4 kta). The H<sub>2</sub> for this reaction is produced by water electrolysis using energy produced from natural sources, mainly geothermal, hydro, and wind.<sup>(19)</sup>

## 1.2 – Methanol Synthesis from Catalytic Hydrogenation of CO<sub>2</sub>

### 1.2.1 – Methanol Production in Industry

MeOH is currently produced from syngas (H<sub>2</sub> + CO + CO<sub>2</sub>) over a Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalyst at mild temperature (200 - 270 °C) and high pressure (50 - 100 bar) and has a global demand exceeding 98 Mt/annum.<sup>(20, 21)</sup> Syngas is produced from the steam reforming of hydrocarbons, predominantly methane,<sup>(22)</sup> and consequently the overall process has a great environmental cost, (ca. 88 Mt GHG eq).<sup>(23)</sup> Small amounts of CO<sub>2</sub> (about 2–8%) are typically added to the CO/H<sub>2</sub> stream to balance the H/C ratio to the desired stoichiometry and to accelerate the reaction rate. Syngas production is not ideal if the aim is to prevent any further increases in CO<sub>2</sub> levels, therefore a more effective approach, such as CO<sub>2</sub> hydrogenation to MeOH, is required to enable the synthesis of CO<sub>2</sub>-neutral fuels whilst mitigating anthropogenic emissions.



The standard method adopted commercially to produce methanol via syngas is shown in Eq. 3; comparing this to methanol formation from CO<sub>2</sub> (Eq. 1), it can be seen that more hydrogen is required in order to remove the extra oxygen from CO<sub>2</sub> and subsequently form water as a by-product. Furthermore, methanol production from CO<sub>2</sub> is less thermodynamically favourable compared to CO, thus the one-pass methanol yield of the CO<sub>2</sub> based process is lower than that of the syngas based process.<sup>(24)</sup> Le Châtelier's principle states that if a dynamic equilibrium is disturbed by changing temperature, pressure, or concentrations of reactants in a system the position of equilibrium shifts in the opposite direction to offset the change.<sup>(25)</sup> According to Le Châtelier's principle, a combination of high pressure and low temperature is thermodynamically more favourable for the conversion of CO<sub>2</sub> to MeOH due to its exothermic nature and decrease in the number of molecules as the reaction proceeds forward; however, temperatures above 240 °C are utilised in order to activate CO<sub>2</sub> and provide a sufficient reaction rate.<sup>(26)</sup> As a consequence of the increased temperatures other unwanted side reactions occur, such as the reverse water gas shift (RWGS) shown in Eq.2, or formation of other hydrogenated products such as higher alcohols and hydrocarbons, resulting in reduced methanol yields.

Thermodynamic studies from Álvarez *et al.* showed that at 270 °C and H<sub>2</sub>: CO<sub>2</sub> ratios of 3:1, the equilibrium conversion (the highest conversion that can be achieved in a reversible reaction) increases from 18%, to 23% to 38% as the pressure is increased from 10, 30 and 100 bar respectively. The selectivity is also found to be influenced by the temperatures and pressures; the equilibrium methanol selectivity at 270 °C are 5%, 20%, and 80% at the same pressures listed above. Thus, promising methanol catalysts must be not only be active at relatively low temperatures (less than 270 °C) but they should also be stable and highly selective.<sup>(27)</sup>

As discussed, the maximum methanol yield is limited by the thermodynamic equilibrium; however, the equilibrium limitation on methanol yield can be overcome by several methods including the optimization of reaction conditions, the reactor designs, and innovations such as the recycling of the unconverted feed gas after product separation by condensation, and the *in situ* product removal (e.g. continuous water removal via distillation or membranes).<sup>(28)</sup>

### 1.2.2 – Mechanism of Industrial Catalyst (Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>)

Several researchers have probed into the mechanism of CO<sub>2</sub> hydrogenation to methanol over the years, in order to improve the process; despite this the mechanism on the molecular level is still widely debated. The importance of the active site during the reaction is well-understood, but the exact nature of this active site still remains unclear. Early literature has concluded that metallic copper (Cu<sup>0</sup>) is the major active site for the reaction, and have correlated the increased activity of the catalyst with an increase in copper surface area.<sup>(29-32)</sup>

Although a large emphasis has been placed on the active metal, it is important not to forget the role of the metal oxides present and their promoting effect. Indeed ZnO has shown to influence the chemical, structural, and electronic effects of Cu and hence improve the catalyst reactivity.<sup>(33)</sup> The Cu-Zn synergy is very unique and has shown to be essential towards explaining the catalyst activity; Arena and co-workers proposed that ZnO could act as a reservoir for atomic hydrogen and thus increase the rate of hydrogenation of the key intermediates. They also proposed that either ZnO could confer a peculiar morphology to the Cu particles, or ZnO was able to create additional active sites on the Cu surface.<sup>(9)</sup> These findings are in good agreement with Studt *et al.*, who showed how the presence or absence of the Zn drastically altered not only the activity but also the reaction mechanism. Based on DFT calculations, they concluded that the intermediates in CO<sub>2</sub> hydrogenation are bound to the surface through an oxygen atom and the addition of Zn acted as a promoter. In the case of the CO

hydrogenation, in contrast, the intermediates are bound to the surface through C atoms, and a full layer of Zn blocked these sites and hindered CO hydrogenation.<sup>(34)</sup>

There are mainly two models proposed to describe the Cu–Zn active site. The first one assumes the active site to be a fully Zn-decorated surface step of Cu,<sup>(34, 35)</sup> and the second one is an electron-deficient Cu<sup>δ+</sup> species dissolved across the ZnO promoter as the active site.<sup>(36-38)</sup> This first Zn-decorated model site was based on the experiments and theoretical studies, where the surface enrichment of Zn on the Cu particles was observed by XPS and HRTEM.<sup>(39)</sup> Kuld *et al.* found metallic Zn on the surface of reduced Cu–ZnO catalyst by Auger emission spectroscopy,<sup>(40)</sup> and Lunkenbein *et al.* showed clear evidence of the formation of metastable ZnO layer during reductive activation.<sup>(41)</sup> On the other hand, the electron-deficient Cu<sup>δ+</sup> species has been widely used to explain the differences in catalytic activity of the Cu–ZnO–ZrO<sub>2</sub> systems.<sup>(33, 42-45)</sup> This hypothesis has been supported by chemisorption and FTIR studies and proved that the interaction of Cu particles with ZnO and ZrO<sub>2</sub> phases leads to the stabilization of Cu<sup>δ+</sup> sites at the metal oxide interface.<sup>(46, 47)</sup>

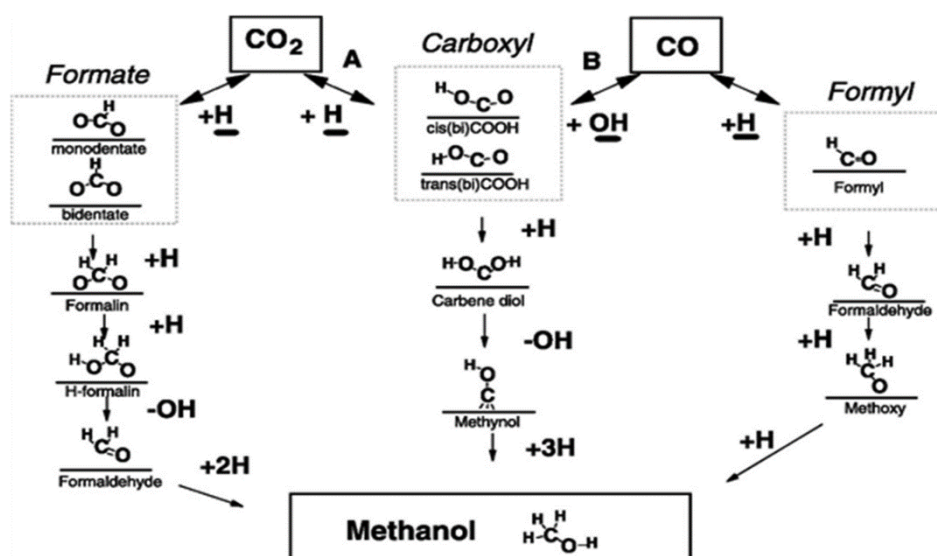
Besides the open discussion about the nature of the active site, the second point described above on the reaction pathway is also still a matter of active debate. The initial adsorption of CO<sub>2</sub> has been reported to occur in several ways. Some researchers claim that CO<sub>2</sub> can dissociatively adsorb over bare Cu<sup>0</sup>,<sup>(48, 49)</sup> while others report that pre-adsorbed H species are crucial to ensure CO<sub>2</sub> adsorption on Cu<sup>0</sup>.<sup>(50, 51)</sup> In addition, the type of species that are formed after the successful adsorption of CO<sub>2</sub> is also widely debated. Some researchers support the formation of formate species (HCOO\*) as the first hydrogenated species in the mechanism, whereas others propose the formation of hydrocarboxyl (COOH\*).

The very first studies supported the formate route via transformation to dioxymethylene (CH<sub>2</sub>O<sub>2</sub>\*), formaldehyde (CH<sub>2</sub>O\*), and then to methoxy. However, the only observable intermediates were formate and methoxy species.<sup>(52, 53)</sup> Grabow and Mavrikakis proposed a mean-field microkinetic model that fitted the experimental results obtained under realistic conditions on commercial Cu–ZnO–Al<sub>2</sub>O<sub>3</sub>. In their proposed mechanism, besides the formate (HCOO\*) and methoxy species, they also considered intermediates such as formic acid HCOOH\* and CH<sub>3</sub>O<sub>2</sub>\*. The DFT calculations showed that CO<sub>2</sub> hydrogenation goes through the formate route, where formate (HCOO\*) preferentially leads to the formation of formic acid rather than dioxymethylene (CH<sub>2</sub>O<sub>2</sub>\*). This formic acid would be further hydrogenated to CH<sub>3</sub>O<sub>2</sub>\*, which is subsequently transformed to CH<sub>2</sub>O\* by splitting off its OH group. In the final step, the hydrogenation of CH<sub>2</sub>O\* would yield methoxy.<sup>(53)</sup> As a favourable support of the formate route, Tabatabaei *et al.* reported the presence of formate species in the CO<sub>2</sub> hydrogenation by pulses and desorption analysis. They noted that the bidentate formate was an intermediate for the

RWGS reaction while a monodentate formate was the intermediate for  $\text{CH}_3\text{OH}$  synthesis on ZnO from  $\text{CO}_2/\text{H}_2$  feeds.<sup>(54)</sup> Yang *et al.* showed that methanol synthesis on Cu surfaces proceeds through a formate intermediate to formaldehyde, but in this case via a dioxomethylene intermediate.<sup>(50)</sup> The overall reaction rate was found limited by both formate and dioxomethylene hydrogenation. In a recent study, Kattel *et al.* reported the synergy of Cu–ZnO and the transformation of formate to methanol via  $^*\text{HCOOH}$ ,  $^*\text{H}_2\text{COOH}$ , and  $^*\text{CH}_3\text{O}$  intermediates.<sup>(55)</sup>

Furthermore, the synergistic effects of Cu– $\text{ZrO}_2$  were evidently reported recently by Larmier *et al.* using a tailored catalyst with highly dispersed Cu on  $\text{ZrO}_2$ . They have shown by NMR, DRIFTS, and DFT calculations that formate is an intermediate and its transformation to methanol is highly favoured at the interface of Cu and  $\text{ZrO}_2$  owing to lowered activation barrier by the interface. Interestingly, the unique interface of Cu and  $\text{ZrO}_2$  facilitated transformation of formate to an acetal-like species ( $\text{H}_2\text{C}(\text{O})_2^*$ ), which is further hydrogenated to methoxy and finally to methanol.<sup>(56)</sup>

Contrary to the formate route, Zhao *et al.* reported that formation of methanol from direct hydrogenation of formate ( $\text{HCOO}^*$ ) on Cu(111) is not feasible due to the high activation barriers in some of the elementary steps. Instead,  $\text{CO}_2$  hydrogenation to hydrocarboxyl (*trans*- $\text{COOH}$ ) is kinetically more favourable than formate in the presence of water via a unique hydrogen transfer mechanism.<sup>(57)</sup> In agreement with Zhao *et al.*, Yang *et al.* concluded that the direct hydrogenation of bidentate formate ( $\text{HCOO}^*$ ) on metallic Cu does not produce methanol. Interestingly, they found that a significant amount of methanol is formed if the Cu catalyst is pre-treated by  $\text{N}_2\text{O}$  or  $\text{O}_2$ , which implies that surface oxygen or possibly water-derived species may play a critical role in the reaction mechanism.<sup>(58)</sup> Figure 1.1 illustrates the different possible reaction intermediates and steps during the hydrogenation of CO and  $\text{CO}_2$  into  $\text{CH}_3\text{OH}$  over Cu.



**Figure 1.1** - Mechanistic pathways for conversion of CO and  $\text{CO}_2$  to  $\text{CH}_3\text{OH}$  over Cu.<sup>(32)</sup>

### 1.2.3 – Cu Catalysts for CO<sub>2</sub> hydrogenation to MeOH

The literature surrounding the synthesis of methanol from CO<sub>2</sub> hydrogenation has predominately been based on Cu catalysts and this is due to its remarkable hydrogenation activity and abundance.<sup>(59-61)</sup> CO<sub>2</sub> hydrogenation to methanol over Cu catalysts is generally known as a structure-sensitive reaction, in which the catalytic properties are closely associated with (i) metal dispersion and surface Cu metallic area, (ii) dimension, composition, and electronic properties of the Cu–ZnO interface, and (iii) capability of adsorption of reagents and mass transfer. Generally, these factors are tunable by means of promoter effect, support effect, preparation methods, and the incorporation of core-shell structure and hydrotalcite-like compounds.<sup>(53)</sup>

Although Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts have dominated in industry, their catalytic performance remains unsatisfactory. The poor performance is due to several factors including the formation of water as a by-product, which facilitates ZnO agglomeration and oxidation of active Cu species as a strong oxidant, leading to the serious deactivation of Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts.<sup>(62)</sup> Therefore, by considering the catalytic kinetics, the development of highly effective Cu-based catalysts in terms of activity, selectivity, water tolerance, and stability are feasible for the hydrogenation of CO<sub>2</sub> to methanol. A selection of Cu based catalysts are shown in Table 1.1.

**Table 1.1:** Summary of Cu based catalysts for the hydrogenation of CO<sub>2</sub> to MeOH from literature.

Catalyst	Preparation	H <sub>2</sub> /CO <sub>2</sub> ratio	Temperature (°C)	Pressure (MPa)	Con. (63)	Sel. (63)	STY (g <sub>MeOH</sub> kg <sub>cat</sub> <sup>-1</sup> )
Cu/Ga/ZnO <sup>(64)</sup>	Co-impregnation	3:1	270	2	6.0	88	378
Cu@ZnO <sub>x</sub> (core-shell) <sup>(65)</sup>	Surface modification precipitation	3:1	250	3	2.3	100	147.2
Cu/Zn/ZrO <sub>2</sub> <sup>(66)</sup>	Reverse coprecipitation	3:1	240	3	17.5	48.4	N/A
Cu/Zn/ZrO <sub>2</sub> <sup>(67)</sup>	Urea-nitrate combustion	3:1	240	3	17.0	56.2	N/A
Cu/ZnO/ZrO <sub>2</sub> /Ga <sub>2</sub> O <sub>3</sub> <sup>(68)</sup>	coprecipitation	3:1	250	8	N/A	75	324
Cu/ZnO/ZrO <sub>2</sub> /Ga <sub>2</sub> O <sub>3</sub> <sup>(68)</sup>	Citric complexing	3:1	250	8	N/A	70	382
Cu-ZnO/ZrO <sub>2</sub> <sup>(69)</sup>	Oxalate coprecipitation	3:1	240	3	9.0	N/A	1200
Cu/ZrO <sub>2</sub> <sup>(70)</sup>	Deposition precipitation	3:1	240	2	6.3	48.8	360

For CO<sub>2</sub> hydrogenation to methanol over Cu-based catalysts, formate (\*HCOO) produced by the reaction between CO<sub>2</sub> and dissociative H and CO generated from the RWGS are considered to be two major intermediates. For all catalysts, methanol selectivity is governed by the competition of the simultaneously catalyzed methanol synthesis and RWGS reactions. In both pathways, methanol is generated from the methoxy (\*CH<sub>3</sub>O) intermediate. In situ diffuse reflectance FT-IR studies reveals that CO<sub>2</sub> can be transformed into carbonate or bicarbonate, formate and methoxy, upon adsorption and hydrogenation on Cu/ZrO<sub>2</sub> particles.<sup>(71)</sup> The formate species is considered to be the most important reaction intermediate and that the Cu/ZrO<sub>2</sub> interface is crucial for the conversion of this intermediate to methanol. The rate-determining step for methanol synthesis is proposed to be the conversion of formate into formaldehyde or methoxy.<sup>(72)</sup> The ZrO<sub>2</sub> support is found to facilitate the conversion of adsorbed CO<sub>2</sub> to surface formate or hydroxycarbonyl entities.<sup>(73)</sup> DFT and kinetic Monte Carlo (KMC) simulations suggest that, on the oxygen-rich Cu/m-ZrO<sub>2</sub> interface, both methanol and CO are produced dominantly via the formate pathway, while the RWGS channel has only a minor contribution.<sup>(74)</sup>

In addition, the synthesis of methanol from CO<sub>2</sub> over Cu/ZrO<sub>2</sub> involves the spillover of H atoms formed on Cu to the surface of ZrO<sub>2</sub>, and the atomic H then participates in the hydrogenation of carbon-containing species (i.e., HCOO and HCO<sub>3</sub>) to methanol.<sup>(75)</sup> In general, a complete process of hydrogen spillover includes several steps, namely: (1) H<sub>2</sub> adsorption and dissociation on metal sites, (2) H atoms transfer from one surface to the other, (3) H atoms diffuse rapidly across the oxide surface and (4) H atoms react or exchange with other intermediates.<sup>(76)</sup> It should be highlighted that the -OH species on ZrO<sub>2</sub> is also involved in the spillover, because the exchange of atomically adsorbed H atoms and OH groups on the catalysts occurs, which would affect the spillover efficiency.

By combining DFT calculations, KMC simulations and in situ diffuse reflectance infrared Fourier transform spectroscopy (DRIFTS), Kattel et al. propose that the production of CH<sub>3</sub>OH via the formate pathway does not seem to be efficient over time due to the formate species being likely spectators and poison the active sites on the surface.<sup>(77)</sup> The CO<sub>2</sub> conversion is facilitated due to the fine-tuning capability of ZrO<sub>2</sub> (reduced Zr<sup>3+</sup> at the interface), being strong enough to stabilize \*CO<sub>2</sub>, \*CO, \*HCO, and \*H<sub>2</sub>CO at the Cu/ZrO<sub>2</sub> interface and therefore to promote its hydrogenation to CH<sub>3</sub>OH via the RWGS + CO-Hydro pathway. This pathway is summarised in Figure 1.2.



Figure 1.2 - Possible reaction pathways and active sites of CO<sub>2</sub> hydrogenation to CH<sub>3</sub>OH over the Cu/ZrO<sub>2</sub>.<sup>(78)</sup>



## 1.3 – Indirect Conversion of CO<sub>2</sub> into Hydrocarbons

### 1.3.1 – Direct Vs Indirect Route

Replacement of part of the fossil fuel consumption by renewable energy sources (solar, wind, biomass and so on) is a central strategy for resource and energy efficiency. When hydrogen originates directly from renewable energy, CO<sub>2</sub> hydrogenation can also provide an important approach for dealing with the intermittence of renewable sources by storing energy in chemicals and fuels. As such, methanol is an important raw material for the production of fuels. The Methanol to Gasoline (MTG)<sup>(79)</sup> process (C<sub>5</sub>–C<sub>11</sub>) was first commercialized in the 1980's and was soon adopted to produce lower olefins (ethylene, propylene and butylene, C<sub>2</sub>–C<sub>4</sub>) via the Methanol to Olefin (MTO)<sup>(80, 81)</sup> process, due to the higher added value of the olefins when compared with gasoline. These light olefins are important chemical building blocks for a variety of useful derivatives in the petrochemical industries.<sup>(82, 83)</sup> In particular, ethylene and propylene production in the petrochemical industries has shown significant growth in the global market during the past decades.<sup>(84)</sup> The global market demand for ethylene and propylene is predicted to reach 184 and 127 Mton, respectively, by 2022, corresponding to a 20% and 25% increase over 2017.<sup>(85)</sup> Conventionally, C<sub>2</sub>–C<sub>4</sub> hydrocarbons have primarily been produced using oil fractions from petroleum refineries and natural gas processing plants.<sup>(86-88)</sup> With the rapid depletion of petroleum sources,<sup>(89)</sup> many alternative feedstock (e.g. biomass-based)<sup>(90)</sup> and technological pathways (e.g. methanol-to-olefin<sup>(91)</sup> or coal-to-olefin routes<sup>(92, 93)</sup>) have been investigated to satisfy the demand growth of C<sub>2</sub>–C<sub>4</sub> hydrocarbons.

There are different possible routes to produce hydrocarbons from CO<sub>2</sub> hydrogenation. Two parallel reactions, the synthesis of methanol and reverse water-gas shift, RWGS), are typically present in the CO<sub>2</sub> hydrogenation process. The hydrocarbons could be directly produced from syngas (CO + H<sub>2</sub>) based on Fischer–Tropsch synthesis<sup>(86, 94)</sup> or indirectly via industrial methanol synthesis and then converting methanol to a range of hydrocarbons using the methanol-to-hydrocarbon process, including the methanol-to-olefin (MTO), methanol-to-propene<sup>(91)</sup>, and methanol-to-gasoline (MTG) processes. It had also been reported that aromatic or lower paraffin (LPG) hydrocarbons were synthesized from methanol or dimethyl ether (DME).<sup>(95-97)</sup> In addition, various hydrocarbons could be indirectly produced from CO<sub>2</sub> hydrogenation via CO<sub>2</sub> hydrogenation to methanol and methanol-to-hydrocarbon (MTH) reactions. Recently, the direct route of converting CO<sub>2</sub> into hydrocarbons has been developed based on Fischer-Tropsch synthesis (CO<sub>2</sub>-FTS), via a two-step process with an initial reduction of CO<sub>2</sub> to CO via the RWGS reaction followed by the conversion of CO to hydrocarbons via FTS.<sup>(98-101)</sup> The catalyst

used should be active in both RWGS and FTS reactions. The issue, however, with the direct approach is the maximum C<sub>5</sub>–C<sub>11</sub> hydrocarbon fraction is limited by the Anderson–Schulz–Flory distribution to ~48%, with an undesirable CH<sub>4</sub> fraction of ~6%.<sup>(102, 103)</sup> Furthermore, the heat of adsorption of CO<sub>2</sub> is lower than that of CO because of the thermodynamic stability of CO<sub>2</sub>, which leads to a much lower coverage of CO<sub>2</sub> over the catalyst, and thus a low CO<sub>2</sub> reactivity and high CH<sub>4</sub> selectivity. As an alternative it is possible to combine the catalysts for methanol and the zeolites for MTH to have a direct one-step formation of hydrocarbons from CO<sub>2</sub> hydrogenation.<sup>(104)</sup>

Dimethyl ether (DME), the dehydration product of methanol, can be used as a feed to produce several different classes of hydrocarbons, including lower olefins, gasoline-range hydrocarbons, branched alkanes, and aromatics. The selectivity to any of these classes of compounds is determined both by the zeolite topology and the operating conditions used. Direct transformation of CO<sub>2</sub> to DME involves a bifunctional catalyst capable of performing two reactions, methanol synthesis and methanol dehydration, simultaneously. These are known as hybrid catalysts; the active elements of these bifunctional catalysts inherently include a component active in the methanol synthesis, which is the preceding reaction in this process, while the methanol dehydration functionality of this hybrid catalyst relies on the solid acid catalyst component such as  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and H-ZSM-5. The use of hybrid catalysts was initially investigated and practiced for direct conversion of syngas to DME. Similar to the methanol synthesis reaction, the hybrid catalysts developed for the syngas-to-DME/gasoline conversion are also known to be active for CO<sub>2</sub> hydrogenation to DME.<sup>(63, 105, 106)</sup>

There has been rapid development in DME synthesis from CO<sub>2</sub> hydrogenation using CH<sub>3</sub>OH synthesis catalysts hybridized with CH<sub>3</sub>OH coupling catalysts.<sup>(107)</sup> The effect of promoters, supports, and synthesis conditions have been explored.<sup>(108-110)</sup> For example, the acidic sites on  $\gamma$ -alumina surfaces and the CuAl<sub>2</sub>O<sub>4</sub> spinel phase can be regulated by promoters like gallium or zinc oxides, resulting in higher stability for Cu NPs during CO<sub>2</sub>-to-DME.<sup>(110)</sup> To date, CO<sub>2</sub> conversion and DME selectivity mostly vary between 35–80% and 5–50%, respectively,<sup>(107)</sup> but CO<sub>2</sub> conversion can reach up to 97% at 280 °C over a Cu–Zn–Al/HZSM-5 catalyst by drastically increasing the reaction pressure (to 36 MPa).<sup>(111)</sup> In addition, interesting results have been reported on core–shell structured hybrid catalysts with the MeOH synthesis catalysts at the core and the MeOH dehydration catalysts forming the shell.<sup>(112, 113)</sup> Compared with traditional hybrid catalysts prepared by physically mixing the components, these novel core–shell catalysts have received much attention in the literature due to their unique structures and ability to valorise CO<sub>2</sub> by improving conversion and DME selectivity.

Selective synthesis of lower olefins from a CO<sub>2</sub> + H<sub>2</sub> mixture by one-pass conversion, via methanol synthesis, was investigated by Inui *et al.* The authors considered that, for the selective synthesis of

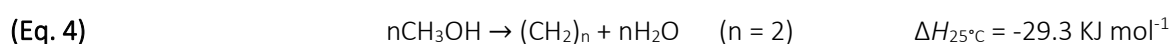
olefin, a weakly acidic and narrow pore microporous crystalline catalyst such as SAPO-34 was required. A bifunctional catalyst containing  $\text{In}_2\text{O}_3$  and SAPO-34 could realize the direct production of lower olefins from  $\text{CO}_2$  hydrogenation with excellent selectivity and high activity. The selectivity of  $\text{C}_2\text{--C}_4$  olefin reached up to around 76.9% with a much lower  $\text{CH}_4$  selectivity of 4.4%, and  $\text{CO}_2$  conversion was above 34%.<sup>(114)</sup>

Currently the indirect route is more developed and economical compared to the direct route; however, through optimisation of the catalyst, reactor designs, and reaction conditions, the product selectivity can be controlled and improvements to the catalytic stability can be made. Recently, the catalytic materials, mechanism, active intermediates and deactivation and commercial projects of MTH have been reviewed in detail.

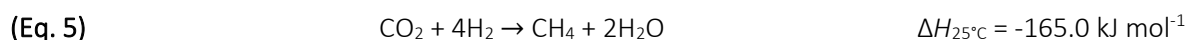
### 1.3.2 – Proposed Reaction Pathway

The methanol (MeOH) mediated route to form hydrocarbons consists of two consecutive processes, i.e.,  $\text{CO}_2$ -to-MeOH (Equation (1)) and a subsequent MeOH-to-olefins process (MTO) (Equation (4)). Additional competing reactions (i.e., Equation (5)) are also witnessed with the formation of light olefins. The control of the selectivity of the  $\text{CO}_2$  hydrogenation to the desired olefin product requires the design of catalysts for reaction pathways that are compatible with favourable thermodynamics and a good understanding of the reaction kinetics.<sup>(115)</sup> The thermodynamic values in the equations indicate that lower temperatures favour methanol (Equation (1)), and methane synthesis (Equation (5)), while higher temperatures are needed to activate  $\text{CO}_2$  for rapid reaction rates.<sup>(116)</sup>

Methanol to Olefins (MTO):



$\text{CO}_2$  methanation:



In reviewing the mechanistic details of light olefin formation, it is clear that controlling the active H to C ratio is of primary importance. The presence of too much  $\text{H}^*$  on the surface will result in excessive hydrogenation, and therefore methanation, while too little  $\text{H}^*$  on the surface will restrict the hydrogenation ability of the catalyst and therefore reduce the  $\text{CO}_2$  conversion activity. At its most fundamental, the pivotal steps of  $\text{CO}_2$  conversion to light olefins are the cleavage of the C–O bonds and the formation of C–C bonds.<sup>(117)</sup>

The reaction mechanism of the MTH process is highly complex. Researchers have reported multiple pathways since its discovery.<sup>(118, 119)</sup> Of the reaction pathways proposed, the most dominant are the oxonium ylide, carbene, carbocationic, free radical, and the hydrocarbon pool mechanism.

According to Li *et al.*, the mechanism of the first C–C bond formation over SAPO-34 occurs through the formation of the methoxymethyl cation intermediate ( $^+\text{CH}_2\text{OCH}_3$ ). The cation intermediate is formed from surface methoxy species and dimethyl ether. The methoxymethyl cation then reacts with another molecule of dimethyl ether or methanol to form 1,2-dimethoxyethane and 2-methoxyethanol, respectively, the compounds containing the first C–C bonds. The formation of the methyl cation was both theoretically and experimentally verified.<sup>(120)</sup>

Chowdhury *et al.* presented experimental magic-angle spinning nuclear magnetic resonance (MAS NMR) evidence for the involvement of acetate species in the first C–C bond formation over the SAPO-34 catalyst. In the proposed mechanism, the surface methoxy species undergo carbonylation (CO being derived via the decomposition of methanol) to form a surface-bound acetate species that, upon addition of a methanol molecule, generates a surface adsorbed methyl acetate species.<sup>(121)</sup>

The dual cycle mechanism deals with the formation of reaction products (selectivity) after the first C–C bond formation. According to Dessau *et al.*, various aliphatic and aromatic hydrocarbons in the MTH reaction can be considered to generate through the consecutive methylation by methanol (Figure 1.2). In principle, ethylene is methylated to form propylene. Further methylation of propylene yields butylene and the process carries on generating higher hydrocarbons. Cyclization of the  $\text{C}_6$  alkenes and further methylation produces various substituted aromatics.<sup>(122)</sup>

Dahl *et al.* used  $^{13}\text{C}$  labeled methanol and  $^{12}\text{C}$  labeled ethene over a SAPO-34 catalyst to verify the probable routes to higher hydrocarbon formation. The authors considered two mechanistic pathways; the first one was the previously suggested consecutive methylation path, and the second one was the “hydrocarbon pool” (HCP) type mechanism. The HCP is a pool of adsorbates having many characteristics similar to ordinary coke, represented as  $(\text{CH}_x)_n$  with  $0 < x < 2$ . In the latter mechanism, methanol is continuously added to the pool of  $(\text{CH}_x)_n$  species, causing their growth. The  $(\text{CH}_x)_n$  species also undergo splitting/cracking to generate the product molecules. According to the experimental results ( $^{13}\text{C}$  and  $^{12}\text{C}$ ), only a minor part of propylene was formed from ethene and methanol, indicating that the HCP mechanism is more prevalent than the consecutive mechanism.<sup>(123)</sup>

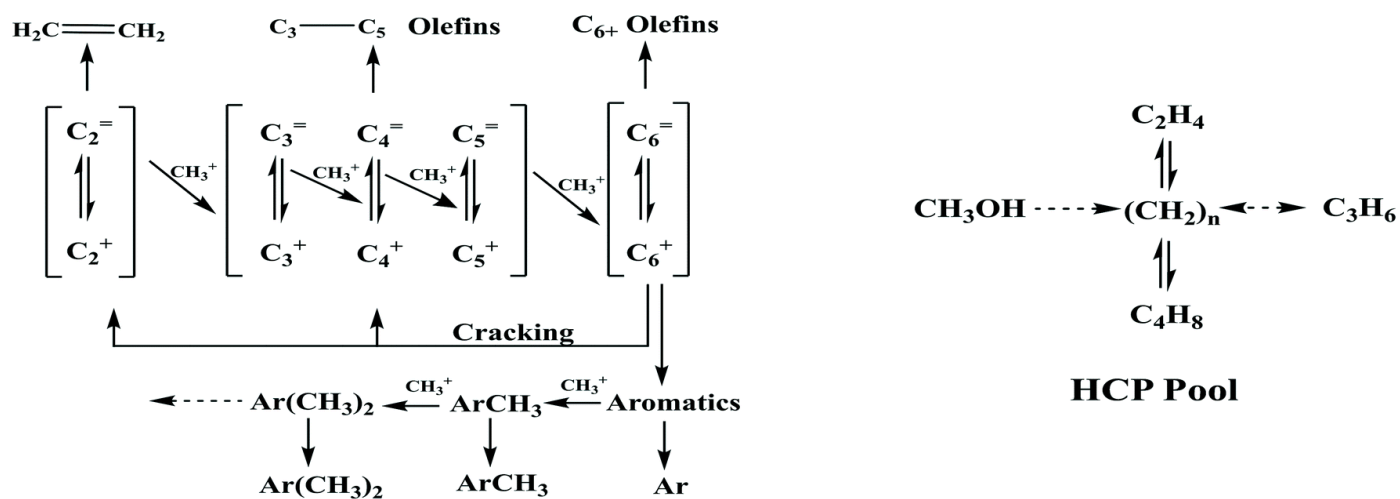


Figure 1.3 - Consecutive methylation scheme for higher hydrocarbons and hydrocarbon pool (HCP) pathway.<sup>(115)</sup>

## 1.4 – Aims and Objectives

The work presented in this thesis is part of a larger project (Flexible Routes to Liquid Fuels from CO<sub>2</sub>). The aims and vision of the wider project are to determine if routes to CO<sub>2</sub> valorisation with sustainable H<sub>2</sub> are potentially viable, with emphasis on upgrading solar hydrogen by reaction with CO<sub>2</sub> to afford drop-in replacements for current hydrocarbon fuels using existing distribution and FTS infrastructure; next-generation candidate fuel DME; and fuel vector methanol, which is a versatile precursor to DME and gasoline via established processes, a fuel additive, and in some scenarios a candidate fuel. The stored solar energy can also be used as a power source for remote locations, in closed cycle space heating and manufacturing applications and also as a supplement to the power grid.

One of the main themes of this project was the thermocatalytic conversion of CO<sub>2</sub> to fuels, and in this study the main focus was on the production of methanol and DME via thermocatalytic routes from CO<sub>2</sub> and H<sub>2</sub>, following this the catalyst design was adapted in order to produce additional hydrocarbons. The main aims of the project are summarised below:

- Identify catalysts that can operate under low temperatures (< 250 °C) for MeOH synthesis from CO<sub>2</sub>.
- Identify and develop active catalysts composed of earth-abundant materials for the hydrogenation of CO<sub>2</sub> to MeOH and DME.
- Investigate the formation of hydrocarbons via methanol formation using integrated catalysts (MeOH synthesis + zeolite).

Chapter 1 has given a brief insight into the impact of increasing CO<sub>2</sub> levels globally and the importance of alternative routes that are less environmentally damaging. Emphasis is placed on CO<sub>2</sub> hydrogenation to methanol, DME and hydrocarbons, with a particular focus on Cu based catalysts and their proposed mechanisms. Chapter 2 will give all the experimental details for the catalyst preparation techniques, characterisation techniques, reaction procedures, and the data analysis used throughout this thesis. A detailed investigation into the promotion of Cu catalysts supported on ZrO<sub>2</sub> is given in chapter 3. Chapter 4 explores the phase composition of Cu/ZrO<sub>2</sub> catalysts and their impact on the hydrogenation of CO<sub>2</sub> to MeOH. Finally, in chapter 5 the indirect conversion of CO<sub>2</sub> to hydrocarbons is explored using Cu/Zn and Cu/Zr zeolite catalysts. As indicated above this thesis initially looks into a variety of supported Cu catalysts, before attempting the catalyst optimisation through the addition of promoters and investigating the catalyst structure to understand its performance. Finally, this information is then used to help develop catalysts for the formation of hydrocarbons.

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## Chapter 2

### Experimental.

#### 2.1 – Materials

The chemicals, used throughout this work, including their supplier and purity, are presented in Table 2.1.

**Table 2.1:** List of all the materials and gases used throughout this thesis and their suppliers.

Material	Supplier
Copper (II) nitrate trihydrate - $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$	Merck
Zirconyl (IV) nitrate hydrate - $\text{ZrO}(\text{NO}_3)_2 \cdot x\text{H}_2\text{O}$	Acros Organics
Oxalic Acid - $\text{HO}_2\text{CCO}_2\text{H}$	Sigma Aldrich
Palladium (II) nitrate dihydrate - $\text{Pd}(\text{NO}_3)_2 \cdot 2\text{H}_2\text{O}$	Sigma Aldrich
Platinum (IV) nitrate solution, Pt 15% w/w - $\text{Pt}(\text{NO}_3)_4$	Alfa Aesar
Cerium (III) nitrate hexahydrate - $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$	Sigma Aldrich
Silver nitrate - $\text{Ag}(\text{NO}_3)_2$	Sigma Aldrich
Nickel (II) nitrate hexahydrate - $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$	Sigma Aldrich
Cerium (III) nitrate hexahydrate - $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$	Sigma Aldrich
Magnesium nitrate hexahydrate - $\text{Mg}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$	Sigma Aldrich
Lanthanum (III) nitrate hexahydrate - $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$	Sigma Aldrich
Manganese (II) nitrate tetrahydrate - $\text{Mn}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$	Sigma Aldrich
Aluminium nitrate nonahydrate - $\text{Al}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$	Sigma Aldrich

Copper (II) acetylacetonate - $\text{Cu}(\text{C}_5\text{H}_7\text{O}_2)_2$	Sigma Aldrich
Zinc acetylacetonate hydrate - $\text{Zn}(\text{C}_5\text{H}_7\text{O}_2)_2 \cdot x\text{H}_2\text{O}$	Sigma Aldrich
ZSM-5 (Si:Al 23; 30; 50 and 80)	Alfa Aesar
Mordenite (20:1)	Alfa Aesar
Zeolite Y	Alfa Aesar
Sodium carbonate - $\text{Na}_2\text{CO}_3$	Fischer
Absolute Ethanol	Sigma Aldrich
20 % $\text{CO}_2$ / 60 % $\text{H}_2$ / 20 % $\text{N}_2$	BOC
5% $\text{H}_2$ / Ar (99.99 %)	BOC
Helium, He (99.99 %)	BOC



## 2.2 – Catalyst Preparation

### 2.2.1 – *Wet impregnation (WI)*

Wet impregnation (WI) is the simplest method for catalyst preparation. In this method, a solution of the metal salt precursor is added to the support material and mixed so that the metal is distributed throughout the pores of the support.<sup>(1)</sup> The material is then dried in order to remove the solvent, but care must be taken that the drying is carried out in a way that the metal component does not migrate to the surface from the pores. After drying, calcination or elevated heat treatment may be carried out to decompose metal salt precursors or prepare the catalytic sites. Reduction treatment may also be employed. Incipient wetness impregnation is a variation of WI where the volume of the metal salt solution is equal to or smaller than the pore volume of the support. This process is simple, quick, reproducible, and ensures that all the metal is directly deposited onto the surface thereby reducing waste, which is especially important when expensive precious metals are used. Industries frequently use WI for the preparation of heterogeneous metal catalysts for these reasons.

Wet impregnation was used a method for Cu deposition onto ZrO<sub>2</sub> in Chapter 4. The Cu loading for all catalyst were fixed at 31 wt. %. The copper metal precursor was dissolved in deionised water (excess) and added dropwise to the ZrO<sub>2</sub> support with vigorous stirring until a paste was formed. The resulting wet solid was dried in the oven at 110 °C for 4 hours before calcining at under static air at 500 °C, 2 °C/min for 2 hours.

### 2.2.2 – *Co-precipitation (CP)*

Co-precipitation (CP) is a common catalyst preparation technique that involves the simultaneous precipitation of two or more metal components using a precipitant under a constant or a varied pH. There are many factors to consider in the synthesis of catalysts by CP including temperature, pH, flow rate of precipitating agent, ageing time, and washing. All of the preparation parameters must be controlled carefully in order to ensure that the catalysts are prepared reproducibly. Because catalysts can be prepared reproducibly by CP, this method has been applied for large scale production of heterogeneous catalysts.<sup>(2)</sup> The main drawback of this technique is that there can be large mass loss during the derivation of the final product. Calcination is often required to decompose the material to the active catalyst.

The following method was used to prepare the 31 wt. % Cu/ZrO<sub>2</sub> catalyst in Chapter 4. A 0.5 M mixed solution of Cu(NO<sub>3</sub>)<sub>2</sub>·3H<sub>2</sub>O and ZrO(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O was prepared. Na<sub>2</sub>CO<sub>3</sub> solution (0.5 M) was added



dropwise to the solution and a pH of 6.5 was maintained. The precipitate was aged in solution for 1 hour at room temperature. The precipitate was filtered under vacuum followed by washing with 6L of warm deionised water. The precipitate was dried in an oven at 110 °C for 16 hours and calcined at the 500 °C (heating rate 2 °C min<sup>-1</sup>) in static air for 2 hours.

### ***2.2.3 – Oxalate Gel Precipitation (OGP)***

Oxalate gel precipitation (OGP) is a variation of the CP procedure discussed in Section 2.2.3, so called because it uses oxalic acid as the precipitating agent, resulting in a sol-gel being formed in solution. The conditions of OGP must be carefully controlled in the same way as CP method.

The supported Cu catalysts and promoted Cu/ZrO<sub>2</sub> catalysts investigated in Chapter 3, Cu/ZrO<sub>2</sub> catalysts in Chapter 4 and CuZn/zeolite and CuZr/Zeolite catalysts in Chapter 5 were prepared by the OGP method. The appropriate metal nitrates were dissolved in 200 mL of ethanol. Solid oxalic acid (0.024 mol) was added into the metal solution, and the resulting precipitate was aged in solution at room temperature for 1 hour. The precipitate was then collected by centrifuge and filtered without a washing step. The material was dried in an oven at 110 °C for 16 hours, and the supported Cu catalysts were calcined at 500 °C (heating rate 2 °C min<sup>-1</sup>) in static air for 2 hours; for the zeolite catalysts calcination was at 550 °C (heating rate 10 °C min<sup>-1</sup>) in static air for 2 hours.

### ***2.2.4 – Chemical Vapour Impregnation (CVI)***

The chemical vapour impregnation (CVI) method was used in order to synthesise the 20 wt.% CuZnO/ZSM-5, CuZnO/H-Y and CuZnO/mordenite catalysts in Chapter 5, where Cu:Zn = 1. A mixture of Cu(acac)<sub>2</sub> (Sigma Aldrich), Zn(acac)<sub>2</sub> (Sigma Aldrich) and zeolite (H-ZSM-5 (Alfa Aesar), H-Y (Alfa Aesar) or mordenite (Alfa Aesar)) were mixed thoroughly before transferring to a 50 ml Schlenk flask. The flask was sealed and evacuated at room temperature on a vacuum line (~10<sup>-3</sup> mbar). The mixture was heated at 120 °C for 1 hour with magnetic stirring under continuous vacuum. The tube was then left to cool and brought to atmospheric pressure in air before collecting. The sample was then calcined at 500 °C (heating rate 2 °C min<sup>-1</sup>) in static air, for 16 hours) to allow complete decomposition of the acetylacetonate precursors.

### ***2.2.5 – Physical Mixing (PM)***

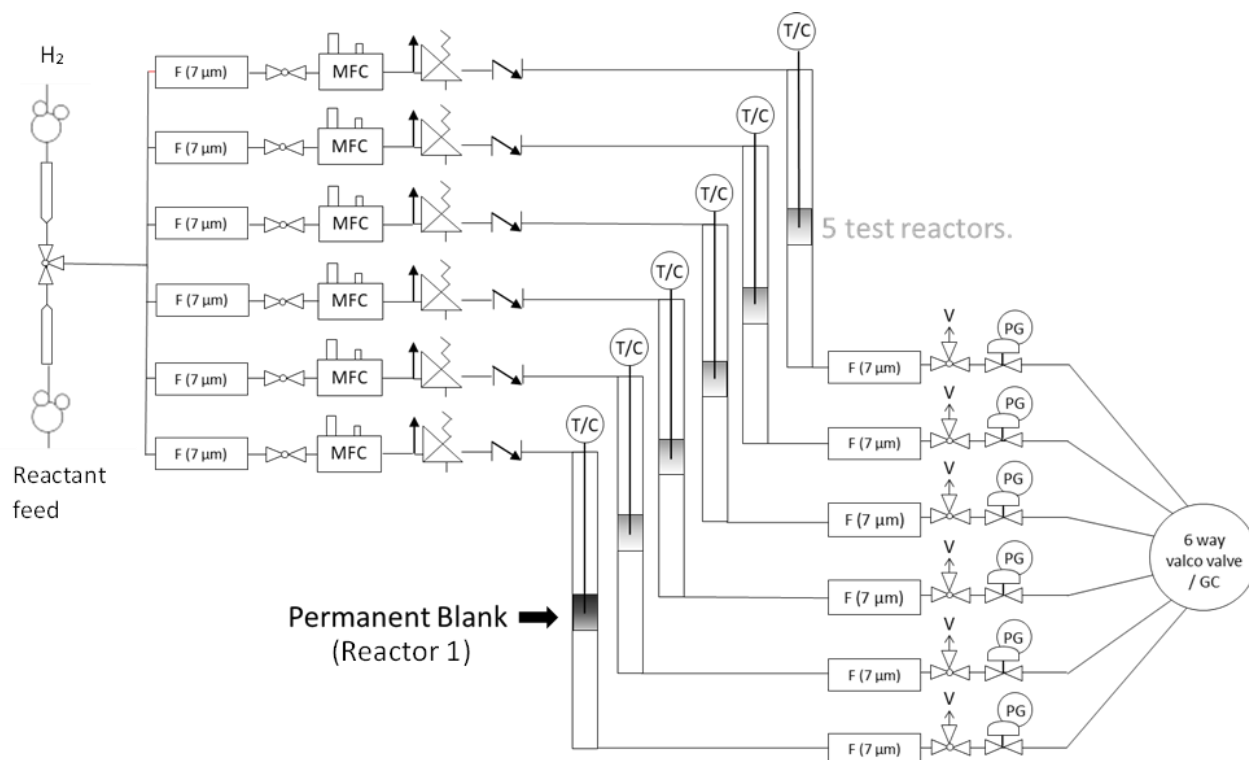
Catalysts prepared by physical mixing are presented in Chapter 5. Physical mixtures of 10% Cu/ZnO, prepared by the oxalate gel method, and commercial H-ZSM-5 (23:1) were made. Two methods of creating physical mixture were employed: the first involved shaking the two catalyst components; and

the second involved grinding the components together, using a pestle and mortar to give the final catalyst.

## 2.3 – Catalyst Testing

### 2.3.1 – Reactor Set-up

A custom-built six-bed flow reactor was used for the analysis of all the catalysts towards the CO<sub>2</sub> hydrogenation (250 °C, 20 bar, 30 ml·min<sup>-1</sup>, 60% H<sub>2</sub>, 20% CO<sub>2</sub>, 20% N<sub>2</sub>). Exhaust gas products were analysed online using a GC Agilent 7890 system fitted with a TCD and a FID detector, and an Agilent CP7557 column with He as the carrier gas. In order to avoid product condensation, post reactor lines and valves prior to the GC were wrapped with heating tape and kept at 130 °C. A thermocouple introduced inside a thermowell placed inside the reactor tube allowed control of the temperature inside the catalyst bed. Simultaneously, a reactor tube was always kept empty to measure the reaction blank activity. A schematic of this is shown below (Figure 2.1).



**Figure 2.1** – Schematic representation of the six-bed reactor used for CO<sub>2</sub> hydrogenation catalyst testing. Diagram produced by Dr. Robert D. Armstrong, Cardiff Catalysis Institute.

Prior to reactions, catalysts were pelleted (425 - 500 μm) and pre-reduced in situ using 5% H<sub>2</sub>/He (30 mL/min) for 1 hour at 220 °C at a ramp rate of 2 °C/min, under atmospheric pressure. Catalysts were placed in the middle of the reactor tube (stainless steel, 0.5 cm x 50 cm), which coincided with the

position of the thermowell, and held in place using quartz wool. Hydrocarbons produced during the reaction including methanol or methane were detected using a flame ionisation detector (FID), while non-hydrocarbon gases like CO, CO<sub>2</sub>, and N<sub>2</sub> were analysed using a thermal conductivity detector (TCD).

### 2.3.2 – Data Calculations

The following calculations (Equations 2.1 to 2.9) were used to determine the CO<sub>2</sub> conversion, product selectivity, and productivities.

Through the ideal gas law (Equation 2.1) where  $p$  is the pressure of the reaction mixture at the mass flow controller (MFC) (1 bar),  $R$  is the gas constant ( $83.15 \times 10^{-3} \text{ dm}^3 \text{ bar K}^{-1} \text{ mol}^{-1}$ ),  $T$  is the temperature (298.15 K) and  $V$  is the volume ( $0.03 \text{ dm}^3 \text{ min}^{-1}$  obtained from the flow gas used during the reaction of  $30 \text{ ml min}^{-1}$ ), the total molar gas ( $n$ ) flow was determined.

$$pV = nRT \quad n = 1.21 \times 10^{-3} \text{ CO}_2 \text{ mol min}^{-1} \quad (\text{Eq. 2.1})$$

Nitrogen gas was used as internal standard at a concentration of 20 vol. %. A blank reactor was analysed simultaneously to the CO<sub>2</sub> hydrogenation reaction, and CO<sub>2</sub> conversion was calculated according to Equation 2.2.

$$\text{CO}_2 \text{ conv. \%} = \frac{\left( \frac{\int \text{Blank CO}_2 / \text{area count}}{\int \text{Blank N}_2 / \text{area counts}} \right) - \left( \frac{\int \text{CO}_2 / \text{area count}}{\int \text{N}_2 / \text{area counts}} \right)}{\left( \frac{\int \text{Blank CO}_2 / \text{area count}}{\int \text{Blank N}_2 / \text{area counts}} \right)} \times 100 \quad (\text{Eq 2.2})$$

Because the number of moles in the gas phase change during the reaction, a compression factor (CF) was introduced (Equation 2.3).

$$\text{CF} = \frac{\int \text{N}_2 / \text{area counts}}{\int \text{Blank N}_2 / \text{area counts}} \quad (\text{Eq 2.3})$$

Non-reacted CO<sub>2</sub> was calculated according to Equation 2.4.

$$\text{Non-reacted CO}_2 \text{ mol min}^{-1} = \frac{\frac{\int \text{CO}_2 / \text{area counts}}{rF_{\text{CO}_2}} \times (\text{Total gas flow} / \text{mol min}^{-1})}{\text{CF}} \quad (\text{Eq 2.4})$$

Where  $rF$  is the response factor obtained from the calibration (area counts per mol<sup>-1</sup>). CH<sub>3</sub>OH productivity was calculated according to Equation 2.5.

$$\text{CH}_3\text{OH mol min}^{-1} = \frac{\left( \frac{\int \text{CH}_3\text{OH} / \text{area counts}}{rF_{\text{CH}_3\text{OH}}} \right) \times \left( \frac{\text{total gas flow/ml min}^{-1}}{0.25 \text{ ml loop volume}} \right)}{\text{CF}} \quad (\text{Eq. 2.5})$$

Productivity of remaining products was obtained following the next calculations (Equation 2.6 representative for CO productivity), where  $rF$  is the response factor obtained from the corresponding calibration (area counts per ppm<sup>-1</sup>).

$$\text{CO mol min}^{-1} = \frac{\frac{\int \text{CO} / \text{area counts}}{rF_{\text{CO}}} \times (\text{Total gas flow} / \text{mol min}^{-1})}{\text{CF}} \quad (\text{Eq. 2.6})$$

The product selectivity based on CO<sub>2</sub> hydrogenation was determined by dividing the productivity of each species times the number of carbons ( $nC$ ) by the productivities of all the products. For instance, CH<sub>3</sub>OH and DME selectivity was calculated following Equations 2.7 and 2.8, respectively.

$$\text{CH}_3\text{OH sel. \%} = \left( \frac{\text{CH}_3\text{OH productivity} \times 1C / \text{mol min}^{-1}}{\Sigma \text{productivities}} \right) \times 100 \quad (\text{Eq. 2.7})$$

$$\text{DME sel. \%} = \left( \frac{\text{DME productivity} \times 2C / \text{mol min}^{-1}}{\Sigma \text{productivities}} \right) \times 100 \quad (\text{Eq. 2.8})$$

Molar productivities, obtained in mol min<sup>-1</sup>, could be normalised to the mass of catalysts used during the reaction (0.5 g) and expressed as mol kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> according to Equation 2.9 as shown for methanol.

$$\text{CH}_3\text{OH prod mol kg}_{\text{cat}}^{-1} \text{ h}^{-1} = \left( \frac{\text{CH}_3\text{OH productivity} / \text{mol min}^{-1}}{(\text{catalyst mass g} / 1000)} \right) \times 60 \quad (\text{Eq. 2.9})$$

## 2.4 – Characterisation

### 2.4.1 – X-Ray Diffraction

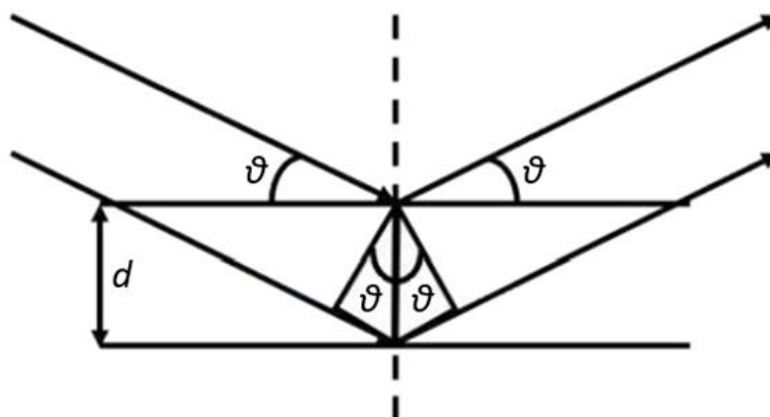
X-ray diffraction is a versatile non-destructive analytical technique for the identification and quantitative determination of the various crystalline forms, known as phases, of compounds present in powdered and solid samples. Identification is achieved by comparing the x-ray diffraction pattern (diffractogram) obtained from an unknown sample with an internationally recognised database containing reference patterns for more than 70, 000 phases. Modern computer-controlled diffractometer systems use automatic routines to measure, record, and interpret the unique diffractograms produced by individual constituents in even highly complex mixtures.

The widths of the peaks in a particular phase pattern provide an indication of the average crystallite size. Large crystallites give rise to sharp peaks, while the peak width increases as crystallite size reduces. Peak broadening also occurs as a result of variations in  $d$ -spacing caused by micro-strain. However, the relationship between broadening and diffraction angle  $2\theta$  is different from that of crystallite size effects, making it possible to differentiate between the two phenomena.

A crystal lattice is a regular three-dimensional distribution (cubic, rhombic, etc.) of atoms in space. These are arranged so that they form a series of parallel planes separated from one another by a distance  $d$ , which varies according to the nature of the material. For any crystal, planes exist in a number of different orientations – each with its own specific  $d$  spacing. When a monochromatic x-ray beam with wavelength  $\lambda$  is incident on lattice planes in a crystal at angle  $\vartheta$ , diffraction occurs only when the distance travelled by the rays reflected from successive planes differs by a complete number  $n$  of wavelengths.<sup>(3)</sup> This is described by Bragg's Law (Eq 2.10), and illustrated in Figure 2.2.

$$\text{(Eq. 2.10)} \quad n\lambda = 2d \sin \vartheta$$

By varying the angle  $\vartheta$ , the Bragg's Law conditions are satisfied by different  $d$ -spacings in polycrystalline materials. Plotting the angular positions and intensities of the resultant diffraction peaks produces a pattern that is characteristic of the sample. When a mixture of different phases is present, the diffractogram is formed by addition of the individual patterns.<sup>(4)</sup>



**Figure 2.2** – Illustration of x-ray beams interacting with a crystal, from which Bragg's Law is derived.

The average crystallite size of the material can be determined using Scherrer's equation (Equation 2.11). Scherrer's equation is only applicable to particles smaller than 100 nm. XRD reflections must be well defined as the full-width half-maximum (FWHM) is a parameter in the equation, meaning that poorly defined reflections (indicating small particles sizes) cannot always be used to determine the particle size using Scherrer's equation.<sup>(5)</sup>

$$\text{(Eq. 2.11)} \quad L = \frac{K\lambda}{\beta \cos \theta}$$

$L$  = measure of the crystallite size in the direction perpendicular to the reflecting plane;  $K$  = a constant based on crystallite shape (generally 0.9 – 1);  $\lambda$  = x-ray wavelength;  $\beta$  = the peak width (FWHM);  $\theta$  = Bragg angle (the angle between the beam and the normal on the reflecting plane).

Powder x-ray diffraction patterns (PXRD) were obtained using a PANalytical X'Pert Pro fitted with an X'Celerator detector and a CuK $\alpha$  x-ray source operated at 40 kV and 40 mA,  $2\theta = 10$ – $80^\circ$ . Each sample was scanned from  $2\theta = 10^\circ$  to  $80^\circ$  for 30 minutes at room temperature. All patterns were matched using the International Centre for Diffraction (ICDD) database. The Cu and Zn particle sizes were calculated using the Scherrer Equation; Cu (111) at  $2\theta = 43.3^\circ$  and Zn (101) at  $2\theta = 36.2^\circ$  respectfully.

### 2.4.2 – Brunauer–Emmett–Teller (BET) Surface Area Analysis

The Brunauer-Emmett-Teller (BET) method is the most widely used technique for surface area determination. The theory aims to explain the physical adsorption of gas molecules on a solid surface and serves as the basis for an important analysis technique for the measurement of the specific surface area of materials. BET theory applies to systems of multilayer adsorption, and usually utilizes probing gases that do not chemically react with material surfaces as adsorbates to quantify specific surface area. Nitrogen is the most commonly employed gaseous adsorbate used for surface probing by BET methods. For this reason, standard BET analysis is most often conducted at the boiling temperature of N<sub>2</sub>.<sup>(6,7)</sup> This method is an extension of the Langmuir model of monolayer adsorption to cover multilayer adsorption and relies on three key assumptions:

1. Gas molecules can adsorb on a solid in infinite layers
2. There is no interaction between each layer
3. The Langmuir model can be applied to each model

The determination of BET surface area is given by the BET equations show in Equations 2.12-2.14.<sup>(8)</sup>

$$\text{(Eq. 2.12)} \quad \frac{p}{V(p_0-p)} = \frac{1}{V_m C} + \frac{C-1}{V_m C} \cdot \frac{p}{p_0}$$

Where  $p$  = equilibrium pressure of the adsorbate at the adsorption temperature;  $p_0$  = saturation pressure of the adsorbate at the adsorption temperature;  $V$  = volume of gas adsorbed at pressure  $p$ ;  $V_m$  = volume of gas required to form a monolayer;  $C$  = BET constant, which is related to the heat of adsorption.

$$\text{(Eq. 2.13)} \quad S_{\text{total}} = \frac{V_m N_A \sigma}{22414}$$

$S_{\text{total}}$  = total surface area;  $N_A$  = Avogadro's constant;  $\sigma$  = the adsorption cross section of the adsorbing species; 22414 L mol<sup>-1</sup> is the molar volume of a gas

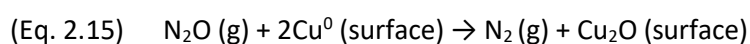
$$\text{(Eq. 2.14)} \quad S_{\text{BET}} = \frac{S_{\text{total}}}{m}$$

$S_{\text{BET}}$  = BET surface area;  $m$  = mass of the solid sample.

BET surface area measurements were performed on a Quantachrome Nova 2200 using a multipoint N<sub>2</sub> adsorption method. Prior to the analysis, samples were degassed for 3 hours at 120 °C under vacuum. The CuZn/Zeolite and CuZr/Zeolite catalyst surface areas were determined by multi-point N<sub>2</sub> adsorption at 77 K (BET range:  $P/P_0 = 0.0013-0.0079$ ) on a micromeritics 3-flex instrument according to the Brunauer-Emmett-Teller (BET) method; Prior to the analysis, samples were degassed at 350 °C, at a heating rate of 10°C/min for 9 hours.

### 2.4.3 – N<sub>2</sub>O Pulse Titration to Determine Specific Metal Surface

N<sub>2</sub>O titration is used for the determination of the metal surface area. N<sub>2</sub>O can oxidise surface metal particles while itself being reduced to N<sub>2</sub>, as shown in Equation 2.15 below.<sup>(9)</sup>



Any unreacted N<sub>2</sub>O used during the analysis is trapped before reaching the detector, in this instance a molecular sieve 5 Å (pelleted 1.6 mm, Sigma Aldrich) trap was used. The process relies on the oxidation of the Cu surface; thus the Cu surface area is determined using the amount of N<sub>2</sub> emitted and the catalyst mass (Equation 2.16).

$$\text{(Eq 2.16)} \quad \text{Cu surface area (m}^2 \text{ g}^{-1}\text{)} = \frac{\text{N}_2 \text{ volume (ml)} \times N_A \times 2}{\text{Catalyst mass (g)} \times 24000 \text{ (ml)} \times (1.0 \times 10^{19} \left(\frac{\text{atoms}}{\text{m}^2}\right))}$$

Whereby  $N_A$  = Avagadro's constant =  $6.022 \times 10^{23}$  (atoms)

The key assumptions are that the amount of N<sub>2</sub> emitted amounts to half a monolayer coverage of oxygen and that the surface density of Cu is  $1.47 \times 10^{-19}$  atoms/m<sup>2</sup>. The volume of N<sub>2</sub> produced was quantified using a thermal conductivity detector.

Cu surface area analysis was carried out by N<sub>2</sub>O pulse titration using a Quantachrome ChemBET. Catalysts were reduced under a flow of 10% H<sub>2</sub>/Ar at 220 °C (2 °C min<sup>-1</sup>, held for 60 min). This was followed by cooling under He. N<sub>2</sub>O titration was carried out at 65 °C with a programme of 13 pulses of 113 µl N<sub>2</sub>O followed by 3 pulses of N<sub>2</sub> for calibration.

Recent work has shown that if the catalyst is exposed to partial pressures of hydrogen exceeding 0.05 bar then partial reduction of ZnO at Cu interface can occur. This will effect copper surface area results, due to N<sub>2</sub>O oxidising both Cu and ZnO<sub>x</sub>. In these cases, alternative techniques, such as H<sub>2</sub> TPD, will give more accurate data with respect to copper surface area.<sup>(10, 11)</sup>



#### 2.4.4 – Temperature Programmed Desorption

Temperature programmed desorption involves monitoring the rate of desorption of chemisorbed molecules as a function of temperature. Adsorption, which can be defined as the enrichment of a fluid adsorbate at the surface of a solid (adsorbent) or the increase in fluid density in the vicinity of an interface,<sup>(12)</sup> can be categorised as physisorption or chemisorption. Physisorption arises as the result of weak intermolecular forces and is nonspecific, non-dissociative; it occurs only at reasonably low temperatures and is characterised by a low heat of adsorption ( $< 50 \text{ kJ mol}^{-1}$ ). Alternatively, chemisorption is characterised by a high heat of adsorption ( $> 50 \text{ kJ mol}^{-1}$ ) and can occur over a wide temperature range. Chemisorption is highly specific, monolayer forming and can take place associatively or dissociatively.<sup>(13)</sup>

TPD typically involves the saturation of a sample with a chemical species (adsorbate) and subsequently heating the sample at a controlled ramp rate to monitor the temperature(s) at which desorption occurs. Following pre-treatment of the adsorbent, the sample is exposed to the adsorbate, generally at ambient temperatures. Any physisorbed species are subsequently removed by flowing an inert gas over the sample before desorption of remaining chemisorbed species is performed. The adsorbent is heated under an inert gas with a constant heating rate ( $\beta = dT/dt = \text{constant}$ ) with any desorbed species monitored by an appropriate detector (generally TCD, FID or quadrupole mass spectrometer (QMS)).<sup>(14)</sup> The data generated from TPD experiments shows detector signal intensity as a function of time/temperature; since signal intensity is proportional to concentration of detected species as desorbed from the sample surface, it is proportional to the rate of desorption. Calibration of the detector by the direct admission of specific quantities of adsorbates, allows for quantitative measurements of desorbed species.

Acidic probe molecules, such as  $\text{CO}_2$  or  $\text{SO}_2$ , are used to investigate materials with basic sites; basic probe molecules, such as  $\text{NH}_3$ , pyridine or acetonitrile, are used to investigate materials containing acidic sites.  $\text{CO}_2$  and  $\text{NH}_3$  are the most widely probe molecules used for investigating the basic and acidic sites of materials, respectively.

Ammonia temperature-programmed desorption ( $\text{NH}_3$ -TPD) was carried out using a Quantachrome ChemBET TPR/TPD instrument equipped with a thermal conductivity detector (TCD). Each catalyst (0.15

g) underwent a pre-treatment at 400 °C (heating rate: 10 °C/min) for 1 hour under He, to remove any water. The catalysts were then saturated with 10% NH<sub>3</sub>/Ar for 15 mins. Physiosorbed NH<sub>3</sub> was removed by heating to 100 °C (heating rate: 10 °C/min) for 1 hour. Finally, NH<sub>3</sub> TPD profiles were recorded under a He flow, from 50 °C to 900 °C using a heating rate of 10 °C/min.

#### 2.4.5 – X-Ray Photoelectron Spectroscopy (XPS)

X-ray photoelectron spectroscopy (XPS) is a commonly used surface technique in catalysis research for the analysis of elemental composition, elemental oxidation state, and metal dispersion. The photoelectron effect is the basis of XPS. An atom absorbs a photon of energy ( $h\nu$ ) and ejects a electron with kinetic energy defined by Equation 2.17. The kinetic energy measured by XPS is used to determine the binding energy of the electron, which is characteristic for each element. Because the binding energy is not only characteristic of the element, but affected by the chemical state of the atom, chemical information can be obtained by XPS. XPS is considered surface sensitive, but x-rays can penetrate a sample to a depth of approximately 10 nm.<sup>(15)</sup>

$$\text{(Eq 2.17)} \quad E_k = h\nu - E_b - \varphi$$

$E_k$  = kinetic energy of the ejected photoelectron;  $h\nu$  = energy of the X-ray photon;  $E_b$  = binding energy of the photoelectron with respect to the fermi level;  $\varphi$  = work function of the spectrometer.

If the incident photon is sufficiently energetic, many different levels in the sample may be ionized and thus a spectrum is produced displaying all accessible energy levels as a distribution of photoelectrons with kinetic energies governed by Equation 2.17.<sup>(16)</sup>

Photoelectron peaks are labelled according to the quantum numbers of the level from which the electron originates. The electron is characterized by a total momentum number  $j=l+s$ , where  $l$  is the orbital momentum number, and  $s$  the spin momentum number, which is equal to 1/2 or -1/2. Therefore, whenever  $l>0$ , the peak is split into a doublet (according to quantum selection rules), with an energy difference called spin-orbit splitting which increases with  $Z$  roughly as  $Z^5$ .<sup>(17)</sup>

XPS was performed using a Kratos Axis Ultra-DLD photoelectron spectrometer, using monochromatic Al  $\kappa\alpha$  radiation, operating at 144 W power. High resolution and survey scans were performed at pass energies of 40 and 160 eV, respectively. Spectra were calibrated to the C (1s) signal at 284.8 eV and quantified using Casa XPS, using modified Wagner sensitivity factors supplied by the manufacturer.

### 2.4.6 – Transmission Electron Microscopy (TEM)

In Transmission electron microscopy (TEM) high energy electrons are accelerated onto a thin sample leading to a variety of interactions, these include elastic and inelastically scattered electrons. Elastic scattering occurs when there is no loss of energy of the incident primary electron. Inelastic scattering occurs when there is an interaction that causes loss of energy of the incident primary electron. Inelastically scattered electrons have a longer wavelength and can occur by many mechanisms; the energy is transferred to the specimen generating a range of useful signals that are exploited to characterize the material.<sup>(18)</sup> The electron beam is then transferred through the instrument's optics. The TEM has an electron gun and electromagnetic lenses that include condenser and objective lenses. The condenser lenses converge and control the electron beam and illuminate the sample, and the objective lens forms the image of the sample and diffraction. The images and diffractions are then magnified by other lenses in the system.

The accelerator voltages are high, to provide electrons with sufficiently high energy (100 – 400 keV) to penetrate the sample. In TEM, the beam is usually spread to encompass the whole sample and as a result does not need to be scanned across the material surface. In addition, the transmission of the electrons through the sample provides more information on the structure of the material, in contrast to scanning electron microscopy (SEM), where the poor depth penetration of the beam insists that only morphology and surface composition can be recorded. The electron beam is refocused after passing through the sample and projected onto a screen. TEM has been previously used to assess the structure and morphology of heterogeneous catalysts as atomic weight contrast, where the scattering increases with atomic number and thickness of the sample, allows for the determination of particle size for supported metal nanoparticles.<sup>(19, 20)</sup>

Samples are generally dispersed in alcohol and deposited on 3 mm carbon-filmed beryllium, copper or aluminium grids. If carbon or other support films are not desirable, freshly meshed metal grids can be used.

Transmission Electron Microscopy (TEM) images of the catalysts were taken using a JEOL JEM-2100 electron microscope operating at 200 kV.

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## Chapter 3

# Promoted Cu Catalysts Supported on ZrO<sub>2</sub> for the Hydrogenation of CO<sub>2</sub> to Methanol.

### 3.1 – Introduction

A wide range of Cu-based heterogeneous catalysts have been explored for the synthesis of MeOH from CO<sub>2</sub>, these include: Cu/ZnO/ZrO<sub>2</sub>,<sup>(1)</sup> Cu/CeO<sub>2</sub>,<sup>(2)</sup> CuZnGa,<sup>(3)</sup> Cu-ZnO<sup>(4)</sup> and Pd-Cu/SiO<sub>2</sub>.<sup>(5)</sup> ZrO<sub>2</sub> is a promising support for Cu catalysts because of its unique properties: high thermal and mechanical stability, high specific surface area, and amphoteric nature with acid sites to adsorb CO<sub>2</sub> and basic sites that facilitate the hydrogenation of intermediates.<sup>(6)</sup> Furthermore, ZrO<sub>2</sub> is less hydrophilic than Al<sub>2</sub>O<sub>3</sub>, which promotes water desorption, enhancing both the MeOH production rate and selectivity.<sup>(7)</sup>

Co-precipitation is the most common procedure for the synthesis of Cu-based catalysts for CO<sub>2</sub> hydrogenation to MeOH,<sup>(8-10)</sup> and is favoured over other synthetic procedures including; sol-gel,<sup>(11)</sup> impregnation<sup>(12)</sup> and citrate method<sup>(13)</sup> due to it being a well-established<sup>(14)</sup>, rapid, and economic method that has shown homogeneity in component distribution, uses mild reaction temperatures, and results in uniform particle sizes with weakly agglomerated particles.<sup>(15)</sup> However, co-precipitation is susceptible to reproducibility issues, since it relies on the precise control of various experimental parameters such as temperature, pH, precursors concentration, and stirring speed, which all highly influence structural and catalytic properties of the final material.<sup>(9)</sup> On the contrary, the oxalate gel synthesis allows for the reproducible synthesis of small and well dispersed Cu particles. Jingfa *et al.*<sup>(16)</sup> prepared Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts following several methods for the CO<sub>2</sub> hydrogenation to MeOH, and they reported that catalysts prepared through the oxalate gel method showed higher MeOH productivities compared to catalysts prepared by conventional precipitation routes. Following on from this study, Deng *et al.*<sup>(17)</sup> demonstrated that highly active and selective Cu/ZnO/ZrO<sub>2</sub> catalysts can be synthesised using this method to achieve finer (12 nm) and more well dispersed particles. It was established that the choice of solvent has a significant impact on the structure of the precipitates, precursors, and catalysts, and subsequently led to different activities; the solvent with the smallest surface tension and largest viscosity (ethanol) was the most beneficial, giving finer particle sizes, as well as more uniformly distributed metal oxides crystallites; this is attributed to the fast nucleation and slow nucleus growth from the more viscous ethanol and reduced shrinkage in volume of the precipitates' structures upon drying. Similar findings were also observed by Koeppel *et al.*<sup>(18)</sup> where Cu/ZrO<sub>2</sub> catalysts

were prepared via several methods including ion exchange, impregnation, deposition precipitation, and co-precipitation. Precipitation routes were the most effective for active catalyst preparation, compared to the other methods, as they resulted in a high interfacial area between the microcrystalline copper particles stabilised interacting with the amorphous zirconia matrix. From the information above, it can be seen that catalyst synthesis through precipitation, particularly oxalate gel, is highly beneficial and worth further investigation; one such possibility is through the use of different catalyst supports, as outlined in this chapter.

Copper has been one of the most common elements used for the hydrogenation of CO<sub>2</sub> to methanol reaction as it is both active and, more importantly, abundant in comparison to other noble metals such as Pd and Pt that are also active for CO<sub>2</sub> hydrogenation.<sup>(19, 20)</sup> Although many new active catalyst formulations have been developed, such as Pd/In<sub>2</sub>O<sub>3</sub>,<sup>(21)</sup> GaPd/SiO<sub>2</sub><sup>(22)</sup> and Ni/β-Ga<sub>2</sub>O<sub>3</sub>,<sup>(23)</sup> they still carry the problem of incorporating harmful/expensive elements, making them less suitable for commercial use. Instead, the inclusion of such elements (as promoters) is a much better solution. The addition of various promoters/additives to the catalyst are very beneficial towards increasing Cu dispersion, modifying the acid-base and redox properties, and enhancing the catalytic performance and stability. Such promoters may be in the form of oxides, an example being the industrial catalyst with the use of ZnO behaving as both a structural (geometric spacer between Cu nanoparticles) and electronic promoter (via metal-support interactions) for Cu based catalysts;<sup>(24)</sup> other forms include noble metals such as Au and Pd, where their promotion effects have been linked to a hydrogen spillover mechanism, whereby the reducibility of Cu sites and re-oxidation of the Cu surface is suppressed.<sup>(25, 26)</sup>

The literature surrounding the synthesis of methanol from CO<sub>2</sub> hydrogenation has predominately been based on Cu catalysts, and this is due to its remarkable hydrogenation activity and abundance. Although the catalyst support is typically viewed as being inert and involved in the dispersion of the active phase, this is far from the truth; indeed, the support has been shown to play an active role during the reaction for various systems. In certain circumstances it can provide thermal stability to the active phase, prevent sintering of metal particles under high reaction temperatures, and can be useful in tuning the surface interaction between the active components of a catalyst, an example of this being the strong metal-support interaction (SMSI), where in some instances the formation of hetero-interfaces between the metal particle and a semiconducting (oxidic) thin layer modifies the electronic structure, resulting in a change in the adsorptive properties of the system.<sup>(27, 28)</sup>

The synergy between certain metals and oxides can induce large electronic changes in the metal,<sup>(29)</sup> provide novel active sites<sup>(30)</sup> or induce variations in the structure or phase of the supported metal particles, which consequently affects the bonding properties and correspondingly the catalytic

performance.<sup>(31)</sup> The nature of the Cu/ZnO synergy has been studied in much detail with a number of phenomena discussed, such as: the reversible change in morphology of the Cu particles, which is dependent on the reaction conditions i.e. wetting/non-wetting behaviour;<sup>(32)</sup> and the formation of novel active sites associated with a Cu-Zn surface alloy via the migration of ZnO<sub>x</sub> species to the surface of Cu particles,<sup>(40)</sup> but this is still under debate. The importance of the Cu-ZnO interface in regards to the catalytic activity has been shown many times. For methanol synthesis catalysts, one of the key features is the specific Cu surface area ( $S_{Cu}$ ), and typically a linear relationship is seen between the Cu surface area and activity; however, deviations from this trend have been observed and can be associated with the synergy effect described above.<sup>(33)</sup> The potential of intrinsic or synergistic effects, which are responsible for different specific activities of Cu, is not easily determined because surface and interface area are interrelated by morphology and microstructure.

For CO<sub>2</sub> hydrogenation the support is necessary for the binding of CO<sub>2</sub> and intermediates, and the nature of the oxide support, i.e. acidic and basic properties, are crucial towards changing the reaction environment on the catalyst surface. In addition, the reducibility of an oxide is important as having the presence of an oxygen vacancy allows stronger binding of CO<sub>2</sub>, and therefore an increase in activity, which has been shown for a number of different supports including CeO<sub>2</sub>, where the increased methanol selectivity is associated with the formation of monodentate/bidentate carbonates that form from the reaction of CO<sub>2</sub> with coordinatively unsaturated O<sup>2-</sup> on CeO<sub>2</sub> in the presence of oxygen vacancies ( $V_O$ ).<sup>(34)</sup> Graciani *et al.* presented detailed theoretical and experimental evidence of a new site for the activation of CO<sub>2</sub> in the form of carboxylate (CO<sub>2</sub><sup>δ-</sup>) at the copper–ceria interface. The rate of methanol production on CeO<sub>x</sub>/Cu(111) was around 200 times greater than that on Cu(111), and about 14 times greater than that over traditional Cu/ZnO catalysts.<sup>(35)</sup>

A study by Kattel *et al.* looked at the use of bimetallic PtCo on various reducible supports including CeO<sub>2</sub>, ZrO<sub>2</sub> and TiO<sub>2</sub>, and revealed a remarkable difference in selectivity across the supports. The result has been attributed to both the different dominant reaction pathways and the role of the metal-oxide interface towards promoting the heterogeneity of the active sites. Unlike the binding of C-bound species, the binding of C,O-bound and O-bound species can be tuned selectively at the interface. Changing the support from TiO<sub>2</sub> to ZrO<sub>2</sub> did not affect the dominant RWGS and CO hydrogenation pathway; however, CO formation was hindered, and CH<sub>4</sub> was preferentially formed over ZrO<sub>2</sub>.<sup>(36)</sup>

Other studies have also shown the benefits of using reducible supports like CeO<sub>2</sub> and ZrO<sub>2</sub> and reveal similar results as above with Cu. Wang *et al.* found that the selectivity of the catalyst can be tuned via the metal-support interaction, and by combining the structural characterisations with in-situ DRIFTS it was concluded that the changes in reaction adsorption intermediates ultimately affected the



distribution of the final products, mainly CO and CH<sub>3</sub>OH. In order to improve on these results, the interaction of the Cu species with the support is essential as this will result in the formation of more Cu-support interfaces, which favour the binding and activation of CO<sub>2</sub>, and greater concentration of oxygen vacancies that can strengthen CO<sub>2</sub> adsorption and stabilisation of key carbon intermediates by promoting the charge accumulation and redistribution.<sup>(34)</sup>

To gain a deeper understanding of the support effect for the hydrogenation of CO<sub>2</sub> to methanol, a variety of different supports were investigated. The supports differed by their acid-base properties and include MgO, MnO, La<sub>2</sub>O<sub>3</sub>, ZnO, ZrO<sub>2</sub>, CeO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>. As shown by Tagawa *et al.*, the choice of support can have a major influence on the catalytic performance through CO<sub>2</sub> adsorption on the Cu surface and hydrogenation of intermediates, they showed that: the use of a basic support led to an increase in the concentration of the formate intermediate on Cu and therefore an increase in activity; using an acidic support allowed an increase in methanol selectivity due to increased reactivity of the reaction intermediate but low activity; and furthermore by choosing an amphoteric support such as Al<sub>2</sub>O<sub>3</sub> the combined effects mentioned above are observed resulting in even higher activity.<sup>(37)</sup>

Apart from varying the type of support, the addition of suitable promoters to the catalyst have been shown to be effective towards improving catalytic activity or stability. Palladium is a common dopant used for promoting higher MeOH rates during CO<sub>2</sub> hydrogenation. For example, Fujimoto *et al.* found that by doping a CuZnAl/SiO<sub>2</sub> catalyst with Pd, MeOH yield increased from 8.9 % to 11.2 % when assessed towards the CO<sub>2</sub> hydrogenation at (240 °C, CO<sub>2</sub>/H<sub>2</sub> = 9, 15 bar, W/F = 5g-cat.h/mol). Moreover, higher stability was observed for the Pd-doped counterpart. The activity for the Cu-Zn-Al catalyst dropped remarkably in the presence of steam and high temperatures (260 °C) due to catalyst oxidation; however, no change in activity was observed in the Pd-doped catalyst. The higher MeOH productivity was attributed to Pd hydrogen spill-over to adjacent Cu centres, which promotes the reduction of Cu<sup>2+</sup> to Cu<sup>+</sup> active sites for methanol formation.<sup>(38)</sup> Sahibzada *et al.* compared the effect of Pd doping on commercial Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts, prepared via a two-stage precipitation, under industrially relevant conditions (5 MPa, 250 °C), Pd was added into the Cu-Zn-Al catalyst by impregnation or by physically mixing Pd/Al with CZA, and promotion effect was observed for both Pd-doping methods compared to CZA (14 mol h<sup>-1</sup> g<sub>Cu</sub><sup>-1</sup> at 4 % CO<sub>2</sub> conversion); CO<sub>2</sub> conversion increases by almost double from increasing Pd concentration (4 wt.% and 12 wt.%) for physically mixed catalysts, whilst a higher promotion effect (35%) was observed when (4 wt. %) Pd was impregnated (14 mol h<sup>-1</sup> g<sub>Cu</sub><sup>-1</sup>) but no further rise in activity was observed with increasing Pd concentration (12 wt.%). Again, the promotion effect of Pd was assigned to hydrogen spillover and the formation of Cu<sup>+</sup> active sites. They also noted that the promotion effect was greater at higher flow rates (lower conversions).<sup>(39)</sup>

The addition of Pd not only promotes the formation of Cu<sup>+</sup> active sites, but it also alloys with Cu leading to active phases for MeOH production. For instance, Jiang and co-workers prepared a series of bimetallic Pd-Cu catalysts supported on amorphous and mesoporous silica. They concluded that the combination of Cu and Pd led to a strong synergistic promotion of CH<sub>3</sub>OH formation rate compared to the monometallic equivalents when the Pd/(Pd + Cu) atomic ratios were within 0.25–0.34 for amorphous silica supported Pd–Cu catalysts. Furthermore, XRD analysis suggested that alloy formation, specifically PdCu and PdCu<sub>3</sub>, are more favourable for methanol formation rather than CO formation.<sup>(5)</sup> From computational studies, it was concluded that the PdCu alloy was more active than the PdCu<sub>3</sub> alloy (based on (111) surface analysis); the higher activity of PdCu was attributed to under co-ordinated Pd atoms at the surface, which promoted both CO<sub>2</sub> and H<sub>2</sub> adsorption and activation. Overall, the Pd-Cu alloy structure has a major effect on the catalytic reaction pathway, and the presence of water can significantly influence the formation of CH<sub>3</sub>OH from CO<sub>2</sub> hydrogenation through acceleration of the CO<sub>2</sub> conversion by reducing the kinetic barriers, altering the rate-limiting step and enhancing the TOF.<sup>(99, 40)</sup>

Hu *et al.* prepared a series of Pd-doped Cu/ZnO catalysts *via* a polyol method with a Cu:Pd molar ratio of 0.005, 0.01, 0.02, 0.03, and 0.04. When tested for the CO<sub>2</sub> hydrogenation (CO<sub>2</sub>/H<sub>2</sub> = 1:3, 36 mL min<sup>-1</sup>, 45 bar and 230 – 290 °C) a volcano plot between methanol yield and Pd loading was obtained, with 1 wt. % Pd at the top. 1 wt. % Pd-doped Cu/ZnO catalyst showed an increase in the methanol space time yield (STY) by a factor of 2.5, and an increase of MeOH turnover frequency (TOF) by a factor of 3.5, compared to Cu/ZnO. The increase in MeOH productivity that was observed with increasing Pd concentration up to 1 wt. % was attributed to hydrogen spill over; however, excess of Pd translated in a decrease in surface Cu area and concomitant loss of activity.<sup>(41)</sup>

As well as Pd, other noble metals such as Pt and Ag are often a prime choice as promoters or additions to a catalyst. Tada *et al.* examined the effect of Ag as a promoter for Cu/ZrO<sub>2</sub> catalysts, by varying the loading from 0 – 5 wt %, and they found a monotonical increase in methanol selectivity from 39 % (Cu/ZrO<sub>2</sub>) to 65 % (5 wt% Ag/Cu/ZrO<sub>2</sub>). It was also noted that a strong synergy between the Cu and Ag, most likely through the formation of an alloy, contributes towards the differences in intrinsic activity between the promoted and unpromoted catalyst.<sup>(42)</sup> Zeng *et al.* prepared atomically dispersed Pt/MoS<sub>2</sub> catalysts with a Pt loading up to 7.5%, although not at promoter levels, they reported that the synergetic interaction between neighbouring Pt monomers reduces the activation energy and enhances the catalytic activity relative to isolated Pt monomers in CO<sub>2</sub> hydrogenation.<sup>(43)</sup> Other non-noble metal additions have also been investigated for CO<sub>2</sub> hydrogenation to MeOH, these include Ni and Ce; Frei and co-workers studied the in-depth promotion of Indium catalysts with Ni; interestingly, up to 10 wt% Ni resulted in the formation of InNi<sub>3</sub> patches along the oxide surface and this led to higher catalyst stability, increased methanol productivity and suppressed methane formation compared to

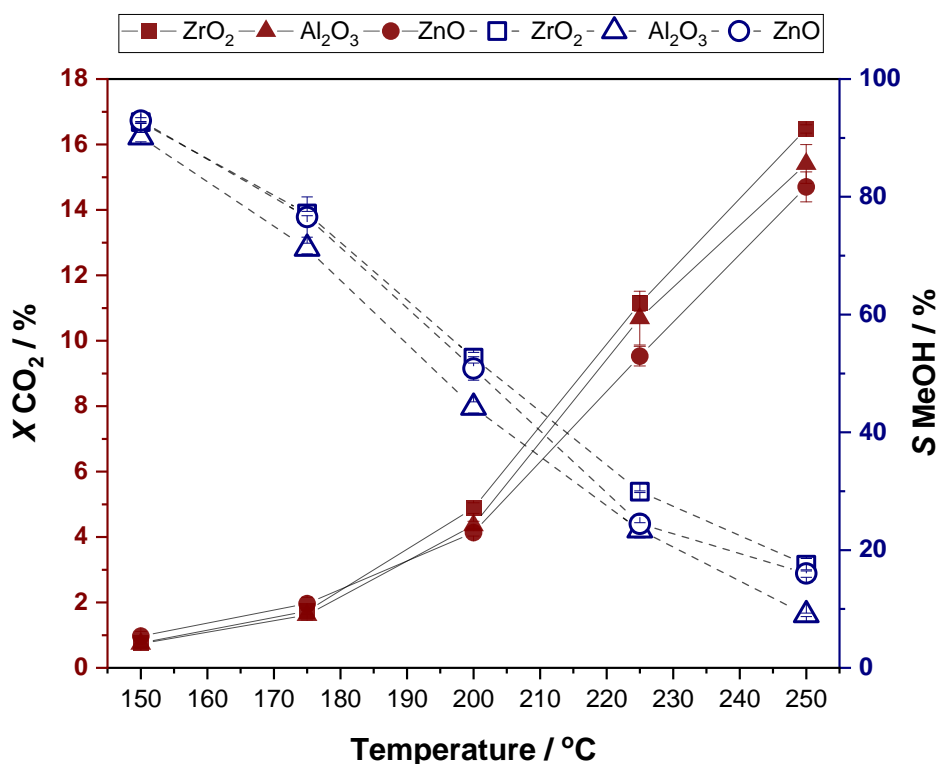
pure In<sub>2</sub>O<sub>3</sub>.<sup>(44)</sup> Gao *et al.* investigated the use of various rare earth metals, including ceria, as a promoter for Cu/Zn/Al catalysts and discovered that incorporating these promoters led to higher BET surface areas, Cu surface area, and Cu dispersion, and subsequently greater methanol productivity than the pure Cu/Zn/Al catalysts.<sup>(45)</sup> Seeing the benefits of introducing Pt, Ag, Ni and Ce to a catalyst it was decided that their addition as promoters would be investigated for Cu/ZrO<sub>2</sub>.

The work detailed in this chapter aims to explore various supported Cu catalysts prepared via the oxalate gel synthesis method, with a particular focus on Cu/ZrO<sub>2</sub>, towards the conversion of CO<sub>2</sub> to MeOH. The role of various promoters (Pd, Pt, Ce, Ni and Ag) and the stability of these catalysts is also investigated.

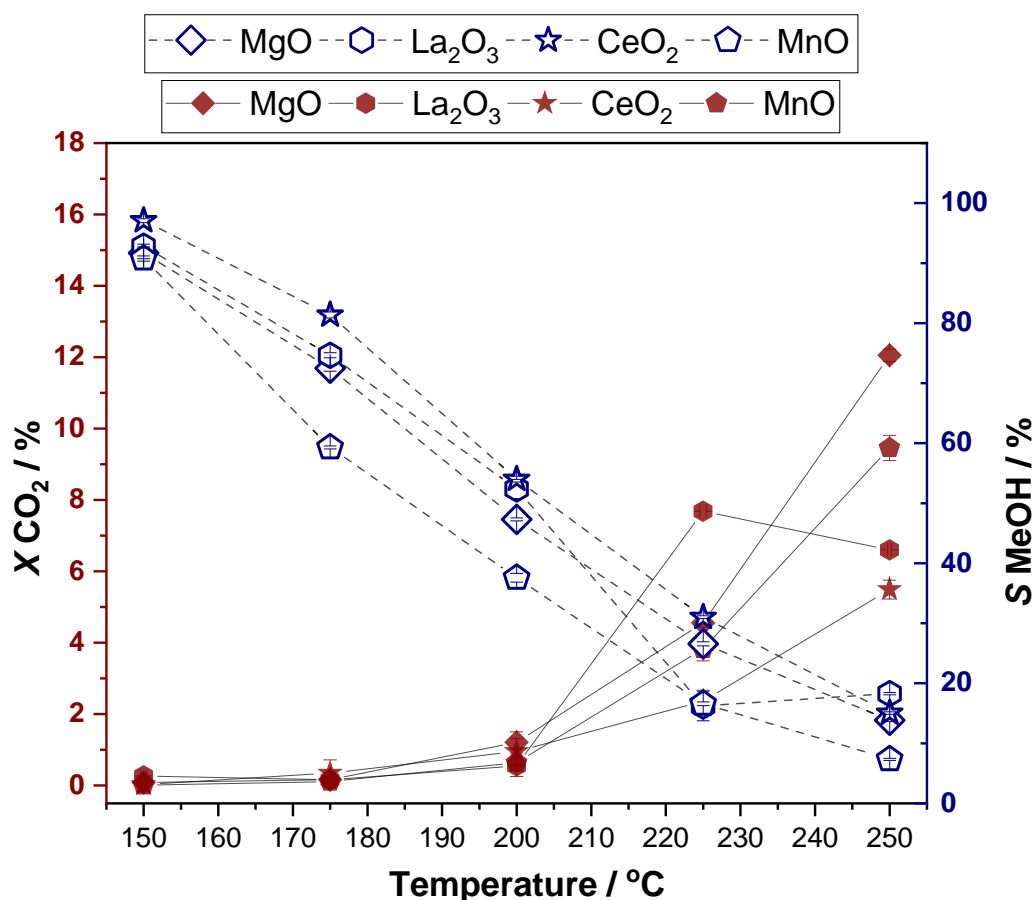
## 3.2 – Results and Discussion

### 3.2.1 – Effect of Support on Cu Catalysts Synthesised by Oxalate Gel Precipitation

As described previously, the support employed not only serves as a material where Cu nanoparticles are deposited but it also plays an important role in modifying the catalysts properties.<sup>(46)</sup> Hence, the first aim of this chapter was to prepare and study Cu catalysts on several supports (ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, ZnO, MgO, La<sub>2</sub>O<sub>3</sub>, CeO<sub>2</sub> and MnO) and study their catalytic activity for CO<sub>2</sub> hydrogenation to MeOH. Catalysts were prepared following the oxalate gel methodology described in the experimental section (Chapter 2, Section 2.3). The Cu loading for all the catalysts were fixed at 31 wt. % to allow comparison between the different supports; after preparation, catalysts were dried in static air at 500 °C for 2 h, 10 °C min<sup>-1</sup>. Prior to reaction, catalysts were pelleted (425–600 μm), and 0.5 g of pelleted catalyst was secured with quartz wool in the reactor tube and pre-reduced *in-situ* with 5 % H<sub>2</sub>/He (220 °C, 1 h, 2 °C min<sup>-1</sup>). After reduction, the reactor was allowed to cool to 50 °C, the gas flow was switched from 5 % H<sub>2</sub>/He to the reaction mixture (20 % CO<sub>2</sub>, 60 % H<sub>2</sub>, 20 % N<sub>2</sub>) and was pressurised to 20 bar at a flow rate of 30 ml min<sup>-1</sup>. Catalyst activity was assessed between 150 and 250 °C, for a total of 50 h.

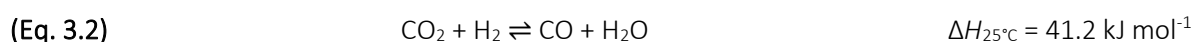
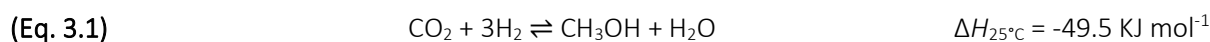


**Figure. 3.1a** - CO<sub>2</sub> conversion (left-red filled symbols) and methanol selectivity (right-blue open symbols) for Cu/ZrO<sub>2</sub>, Cu/Al<sub>2</sub>O<sub>3</sub> and Cu/ZnO catalysts. *In-situ reduction conditions*; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). *Reaction conditions*: 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.



**Figure. 3.1b** - CO<sub>2</sub> conversion (left-red filled symbols) and methanol selectivity (right-blue open symbols) for Cu/MgO, Cu/La<sub>2</sub>O<sub>3</sub>, Cu/CeO<sub>2</sub>, and Cu/MnO catalysts. *In-situ reduction conditions*; 1 h at 220 °C in 5%H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). *Reaction conditions*: 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

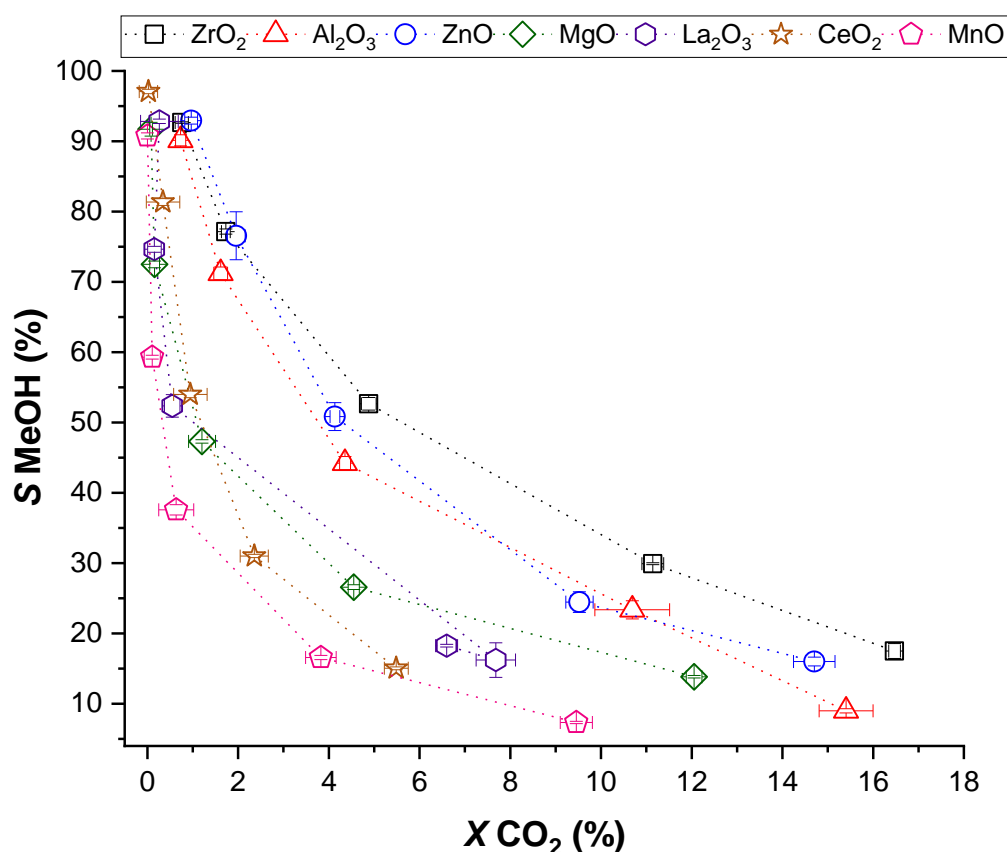
Energy input is necessary for the activation of CO<sub>2</sub>,<sup>(47)</sup> which is observed by the low CO<sub>2</sub> conversion (< 1 %) at low temperature for all catalysts (Figure 3.1). Increasing reaction temperature leads to an increase in the CO<sub>2</sub> conversion; however, this is at the expense of MeOH selectivity. The decrease in MeOH selectivity is explained by the reaction thermodynamics (Equation 3.1); MeOH synthesis is favoured at low temperature and high pressure,<sup>(48)</sup> whilst CO formation via reverse water gas shift (RWGS) is favoured at high temperatures (Equation 3.2). No other products (e.g., CH<sub>4</sub> or DME, which can originate from CO<sub>2</sub> methanation or MeOH dehydration, respectively) were detected.



The catalysts can be divided into two catalytic trends: the first group are Cu/ZnO, Cu/ZrO<sub>2</sub> and Cu/Al<sub>2</sub>O<sub>3</sub> (Figure 3.1a) and the second group are Cu/MgO, Cu/La<sub>2</sub>O<sub>3</sub>, Cu/CeO<sub>2</sub> and Cu/MnO (Figure 3.1b). Despite the variation in the supports used, there is little difference between the catalysts; the error bars show a good reproducibility between all the catalysts measured. The first group of catalysts (Cu-ZrO<sub>2</sub>, Cu-Al<sub>2</sub>O<sub>3</sub> and Cu-ZnO) show slightly higher activity compared to the other supports, and the MeOH selectivity falls within the same range across the temperatures, with the largest errors seen at the lowest temperatures and conversions. Al<sub>2</sub>O<sub>3</sub>, ZnO and ZrO<sub>2</sub> follow a similar trend for CO<sub>2</sub> conversion and MeOH selectivity up to 200 °C; at higher temperatures, the supports can be differentiated by their individual activity. At 250 °C CO<sub>2</sub> conversion for Cu/Al<sub>2</sub>O<sub>3</sub> and Cu/ZnO was 15.4 and 14.7 %, respectively, whilst MeOH selectivity was 9.0 and 16.0 %. In comparison, the Cu/ZrO<sub>2</sub> catalyst achieved the highest conversion (16.4 %) and MeOH selectivity (17.5 %) at 250°C.

Figure 3.1b shows CO<sub>2</sub> conversion and MeOH selectivity for the second group of catalysts (Cu/MgO, Cu/La<sub>2</sub>O<sub>3</sub>, Cu/CeO<sub>2</sub> and Cu/MnO). This group shows less activity and selectivity than the previous group of catalysts, with very low conversion observed below 200 °C. Cu-La<sub>2</sub>O<sub>3</sub> shows a rapid increase in CO<sub>2</sub> conversion from 0.5 % to 7.7 % when the reaction temperature is increased from 200 °C to 225 °C; however, the CO<sub>2</sub> conversion suddenly drops at a higher temperature, which might be associated with catalyst deactivation. The remaining supports show a steady increase in CO<sub>2</sub> conversion above 200 °C. Similar MeOH selectivity was observed for this group of catalysts; however, clear differences in CO<sub>2</sub> conversion were detected. The results most likely reflect a change in the basicity of the supports, where an increase in basicity results in an in higher CO<sub>2</sub> uptake and stronger adsorption of CO<sub>2</sub>.<sup>(49)</sup>

A comparison of the CO<sub>2</sub> conversion and MeOH selectivity between all the supports is shown in Figure 3.2. As discussed above, there is a noticeable difference between the two sets of supports, although all supports show near identical selectivity at the start with small changes over the course of the reaction. Differences between the conversion become apparent, with the maximum conversion of 12% for the second set of supports (MgO) and 16% for the first set of catalysts (ZrO<sub>2</sub>).



**Figure. 3.2** - Methanol selectivity and CO<sub>2</sub> conversion for Cu/ZrO<sub>2</sub>, Cu/Al<sub>2</sub>O<sub>3</sub>, Cu/ZnO, Cu/MgO, Cu/La<sub>2</sub>O<sub>3</sub>, Cu/CeO<sub>2</sub>, and Cu/MnO catalysts. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

The MeOH and CO productivities for the supported Cu catalysts at 250 °C are shown in Table 3.1. Of the supports tested, ZrO<sub>2</sub> achieved the highest MeOH productivity of 811 mmol<sub>MeOH</sub>Kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>, and MnO attained the lowest MeOH productivity of 215 mmol<sub>MeOH</sub>Kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>. ZnO is also a suitable support and the most comparable with ZrO<sub>2</sub> with regards to the methanol and CO productivity. These results support existing literature where the promoting effects of ZnO and ZrO<sub>2</sub> have been verified; the active sites in conventional Cu-ZnO catalysts are said to be a mixture of partial or completely reduced Cu,<sup>(50)</sup> with a strong synergistic contact with ZnO or partially reduced ZnO<sub>x</sub>.<sup>(51, 52)</sup> The presence of ZnO has been argued to contribute in a number of ways including; increased number of active sites by favouring the dispersion of reduced Cu, stabilising Cu<sup>+</sup> sites on the surface and reducibility of Cu<sup>2+</sup> species and catalysing the hydrogenation of carbon oxides via close contact between the basic sites available on ZnO and various Cu species.<sup>(53-55)</sup> In addition, the role of ZrO<sub>2</sub> in Cu based catalysts has also been emphasised, where its addition can tune the dissociation of H<sub>2</sub> and subsequent spillover of atomic hydrogen,<sup>(56-58)</sup> alter reaction pathways,<sup>(59)</sup> increase the metal dispersion and surface area, and enhance

the binding of key intermediates for further conversion,<sup>(60-62)</sup> as well as modifying key surface properties (e.g., basicity and defect concentration).<sup>(63, 64)</sup> The benefits listed above explain why the majority of mixed catalysts used for methanol production are based on ZnO and ZrO<sub>2</sub> in conjunction with Al<sub>2</sub>O<sub>3</sub>.

**Table 3.1:** Activity of supported Cu catalysts at 250 °C.

Catalyst	X CO <sub>2</sub> %	S MeOH %	S CO %	MeOH Productivity (mmol <sub>MeOH</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	CO Productivity (mmol <sub>CO</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )
Cu/ZnO	14.7	16.0	83.8	717	3753
Cu/ZrO <sub>2</sub>	16.5	17.5	82.2	811	3802
Cu/Al <sub>2</sub> O <sub>3</sub>	15.4	9.0	91.0	408	4133
Cu/MgO	12.1	13.8	86.2	501	3119
Cu/MnO	9.5	7.3	92.7	215	2716
Cu/La <sub>2</sub> O <sub>3</sub>	6.6	18.3	81.7	421	1884
Cu/CeO <sub>2</sub>	5.5	15.0	84.9	252	1422

As mentioned previously, the study by Tagawa *et al.* shows that the choice of support can have a major influence on the catalytic performance through CO<sub>2</sub> adsorption on the Cu surface and hydrogenation of intermediates. A range of supports were tested in their work; these include MgO (basic), SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> (acidic), SiO<sub>2</sub> (neutral) and TiO<sub>2</sub> and ZrO<sub>2</sub> (amphoteric). They showed that the use of a strong basic support (MgO) led to a destabilisation of the formate species preventing hydrogenation to MeOH and instead an increase in CO concentration via the RWGS reaction; similar findings were shown for the neutral support (SiO<sub>2</sub>) where the surface concentration of formate was small. Using an acidic support allowed an increase in methanol selectivity due to increased reactivity of the reaction intermediate; however, the acidic nature prevented the adsorption of CO<sub>2</sub> and consequently the conversion was low. Furthermore, by choosing an amphoteric support such as TiO<sub>2</sub> one can take advantage of both the basic sites to adsorb CO<sub>2</sub> to form the formate species and the acid sites to activate the formate species for hydrogenation to form methanol via a methoxy species. Differences between the amphoteric supports can be attributed to the increased concentration of formate and ease of hydrogenation to the methoxy species.<sup>(37)</sup> The results discussed in the literature above reflect the trends observed in Table 3.1, with the first group of catalysts (amphoteric) being the most active, and the more neutral and basic supports being the less active towards CO<sub>2</sub> hydrogenation to methanol.

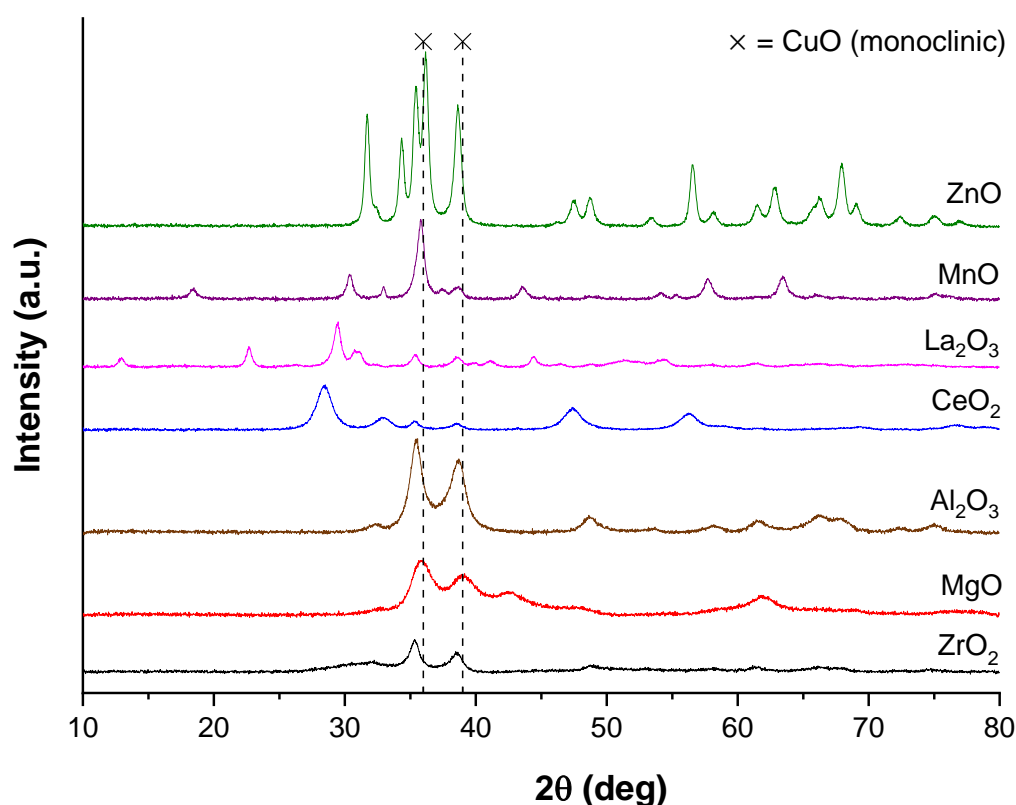


The physiochemical properties of the supported Cu catalysts (Table 3.2) were also characterised in order to investigate their influence on the catalytic activity observed above. The XRD data is shown in Figure 3.3.

**Table 3.2:** Physiochemical properties of supported Cu catalysts.

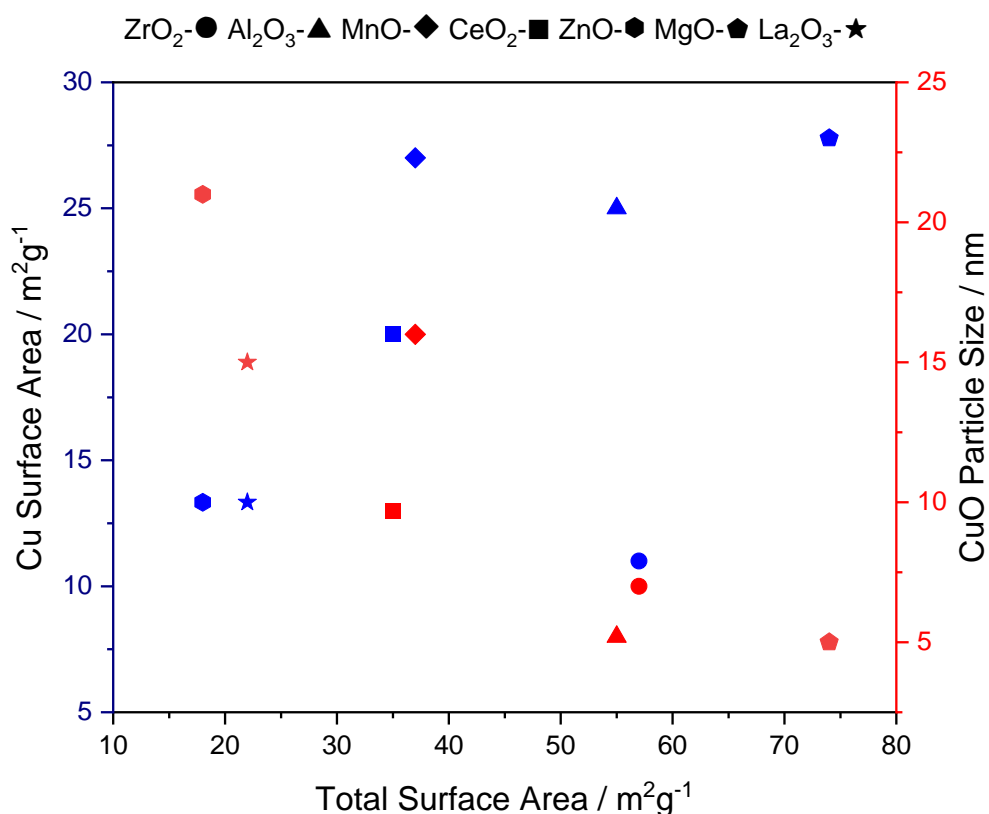
Catalyst	BET Surface area (m <sup>2</sup> /g)	Cu Surface area (m <sup>2</sup> /g)	CuO particle size (nm)*
Cu/ZnO	18	10	21
Cu/ZrO <sub>2</sub>	57	11	10
Cu/Al <sub>2</sub> O <sub>3</sub>	55	25	8
Cu/MgO	74	23	5
Cu/MnO	37	27	20
Cu/La <sub>2</sub> O <sub>3</sub>	22	10	15
Cu/CeO <sub>2</sub>	35	20	13

\*Calculated via Scherrer equation for CuO ( $\bar{1}11$ ) at 35.5°



**Figure 3.3** - XRD patterns for calcined supported Cu catalysts, the CuO (monoclinic) regions have been highlighted.

The XRD patterns above show the major peaks for CuO (monoclinic) at  $2\theta = 36^\circ$  and  $39^\circ$  for all the calcined catalysts, these however, vary in intensity and peak width suggesting a large variation in the CuO particle sizes between the supports. The reflections for the individual supports, particularly ZrO<sub>2</sub>, include peaks in close proximity to the CuO peaks ( $t\text{-ZrO}_2 = 31.5^\circ$ ). The variety is also reflected by the values calculated using the Scherrer equation CuO ( $\bar{1}11$ ) at  $35.5^\circ$ ; the first group of catalysts show some of the largest CuO particle sizes, with ZnO measuring 21 nm compared to the second group of catalysts such as MgO, giving a CuO particle size of 5 nm. The relationship between the overall surface area of the catalysts and the metal particle size and surface area are illustrated in Figure 3.4. Looking at the overall surface area of the supports, there is no specific trend in relation to the CuO particle size and Cu surface area; however, a fairly linear trend, with the exception of MnO, is established between the total surface area and CuO particle size, where an increase in the surface area shows a decrease in the size of the metal particles. Comparing with the specific Cu surface area, no clear trend is shown; despite ZrO<sub>2</sub> and ZnO belonging to the group of the most active supports, the specific metal surface areas are significantly lower compared to the other supports. This suggests that an increase in Cu surface area does not correlate with an increase in methanol activity as discussed previously.



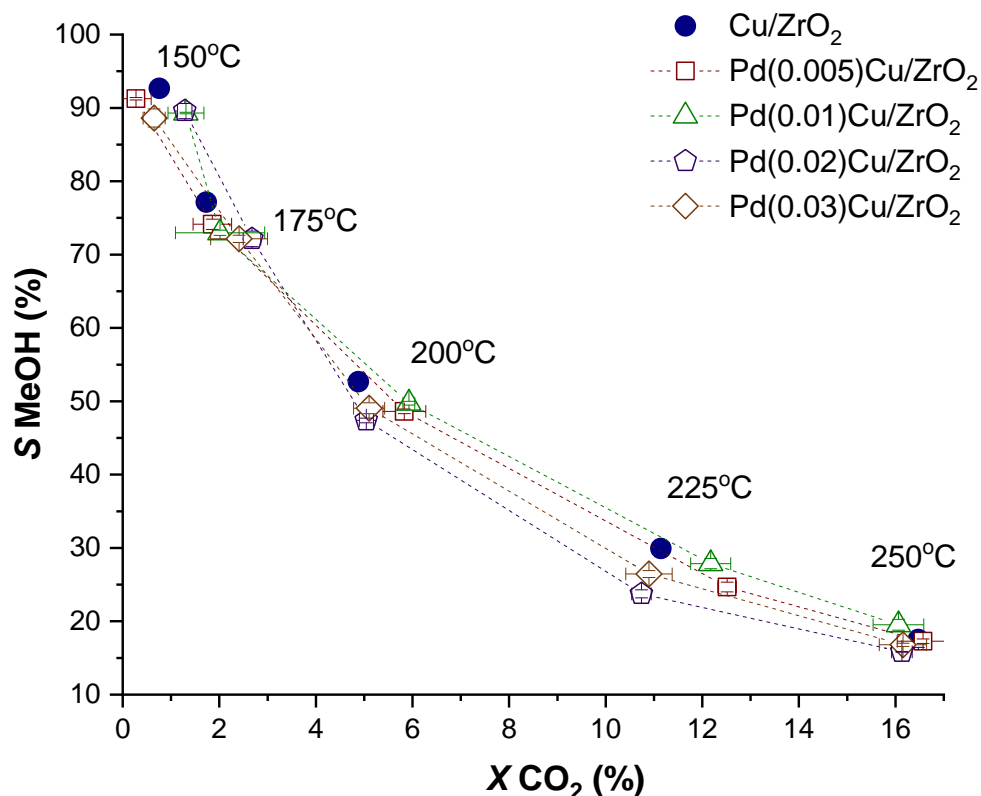
**Figure. 3.4** – Total surface area of supported Cu catalysts vs Cu surface area (blue symbols) and CuO particle size (red symbols).

### 3.2.3 – Pd Promoted Cu/ZrO<sub>2</sub> Catalysts

As the Cu/ZrO<sub>2</sub> catalyst showed promising results, with reasonable methanol productivities and CO<sub>2</sub> conversion compared to the other supports tested, it was decided that the catalyst would be optimised further through the addition of various promoters including Pd. The addition of Pd to the catalyst is beneficial as it can modify the structure and surface electronic properties, which will subsequently affect the stability of intermediates and transition states and thus alter the reaction path and modulate the selectivity. It is also crucial towards hydrogen activation and maintaining the Cu particles in a reduced state, by acting as the dissociation sites for H<sub>2</sub> and serving as an exit route for H<sub>2</sub> via inverse spillover during the desorption process, and therefore suppressing the re-oxidation of the Cu surface via a hydrogen spillover mechanism.

Based on the promoting effect of Pd-doping observed on several Cu-based catalysts for the CO<sub>2</sub> hydrogenation to MeOH,<sup>(25, 39, 65)</sup> a series of Pd-doped Cu/ZrO<sub>2</sub> catalysts (Pd:Cu molar ratio – 1 : 0.005, 1 : 0.01, 1 : 0.02 and 1 : 0.03) were prepared through the oxalate gel method. For the preparation of Pd-doped Cu/ZrO<sub>2</sub> catalysts via oxalate gel, the desired amount of Pd(NO<sub>3</sub>)<sub>2</sub> was added simultaneously with Cu(NO<sub>3</sub>)<sub>2</sub> and Zr(NO<sub>3</sub>)<sub>2</sub> precursors and precipitated with oxalic acid to induce its precipitation; further details of the synthetic process can be found in the experimental section (Chapter 2, Section 2.3). Catalysts are named as Pd(0.005)Cu/ZrO<sub>2</sub>, Pd(0.01)Cu/ZrO<sub>2</sub>, Pd(0.02)Cu/ZrO<sub>2</sub> and Pd(0.03)Cu/ZrO<sub>2</sub> following the order of Pd:Cu molar ratios listed above. Prior to reaction (150 – 250 °C, CO<sub>2</sub>/H<sub>2</sub>/N<sub>2</sub> – 1:3:1, 30 ml/min, 20 bar and total 50 h) catalysts were calcined, pelleted, and pre-reduced as described previously.

As observed in Figure 3.5, no significant promoting effect in terms of greater CO<sub>2</sub> conversion or improved MeOH selectivity was observed for Pd-promoted Cu/ZrO<sub>2</sub> catalysts compared to Cu/ZrO<sub>2</sub>. Slight differences observed between the catalysts fall within the experimental error with signs of deactivation observed for both Pd(0.02)Cu/ZrO<sub>2</sub> and Pd(0.03)Cu/ZrO<sub>2</sub> over the temperature range studied. Pd(0.005)Cu/ZrO<sub>2</sub> and Pd(0.01)Cu/ZrO<sub>2</sub> show a slight increase in CO<sub>2</sub> conversion in comparison to Cu/ZrO<sub>2</sub>, which is more apparent at 225°C where Cu/ZrO<sub>2</sub> achieves a conversion of 11% and Pd(0.005)Cu/ZrO<sub>2</sub> and Pd(0.01)Cu/ZrO<sub>2</sub> achieve a conversion of 13%; despite this difference, a decrease in methanol selectivity is also observed for these catalysts meaning any changes observed are within error and are not correlated to the addition of a promoter.



**Figure 3.5** - Activity of CuZrO<sub>2</sub> - Pd promoted catalysts (Cu:Pd = 1 : 0.005 – 1 : 0.03) vs unpromoted Cu/ZrO<sub>2</sub>. *In-situ* reduction conditions; 1 h at 220°C in 5% H<sub>2</sub>/He (2°C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: 150 - 250°C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3)(GHSV = 3,333 h<sup>-1</sup>), P(total) = 20 bar.

One hypothesis to explain the lack of promoting effect is the low concentration of Pd on the surface of the catalyst, and therefore limited interaction between the Pd and Cu species. Instead, Pd may be more concentrated in the bulk of the material and hence unable to perform H<sub>2</sub> spillover. One method to determine the concentration of species on the surface is XPS, as shown in Figure 3.7. Catalyst specific surface area was determined by N<sub>2</sub> adsorption (BET), while Cu surface area was determined by N<sub>2</sub>O adsorption. BET surface area and Cu surface area are shown in Table 3.3. BET surface area seems to greatly increase with the addition of Pd from 57 m<sup>2</sup> g<sup>-1</sup> for Cu/ZrO<sub>2</sub> to 82 m<sup>2</sup> g<sup>-1</sup> for Pd(0.03)Cu/ZrO<sub>2</sub>, suggesting the addition of the promoter during the oxalate gel method and subsequent calcination alters the porosity and catalyst structure. The same trend was observed for Cu surface area, which increased from 11.0 for Cu/ZrO<sub>2</sub> to 11.6 for Pd(0.03)Cu/ZrO<sub>2</sub> with increasing Pd loading. According to previous reports, higher Cu surface area would most likely have translated into higher activity; However, this was not reflected in our catalytic data. Based on results observed by Kapteijn<sup>(66)</sup> and Pachatouridou<sup>(67)</sup>, we can conclude that Pd is active for N<sub>2</sub>O decomposition even in small quantities, with the rate of decomposition reflected by an increase in metal loading, and hence, in this case N<sub>2</sub>O pulse titration is not a reliable technique to quantify the Cu surface area. In addition to Pd contributing

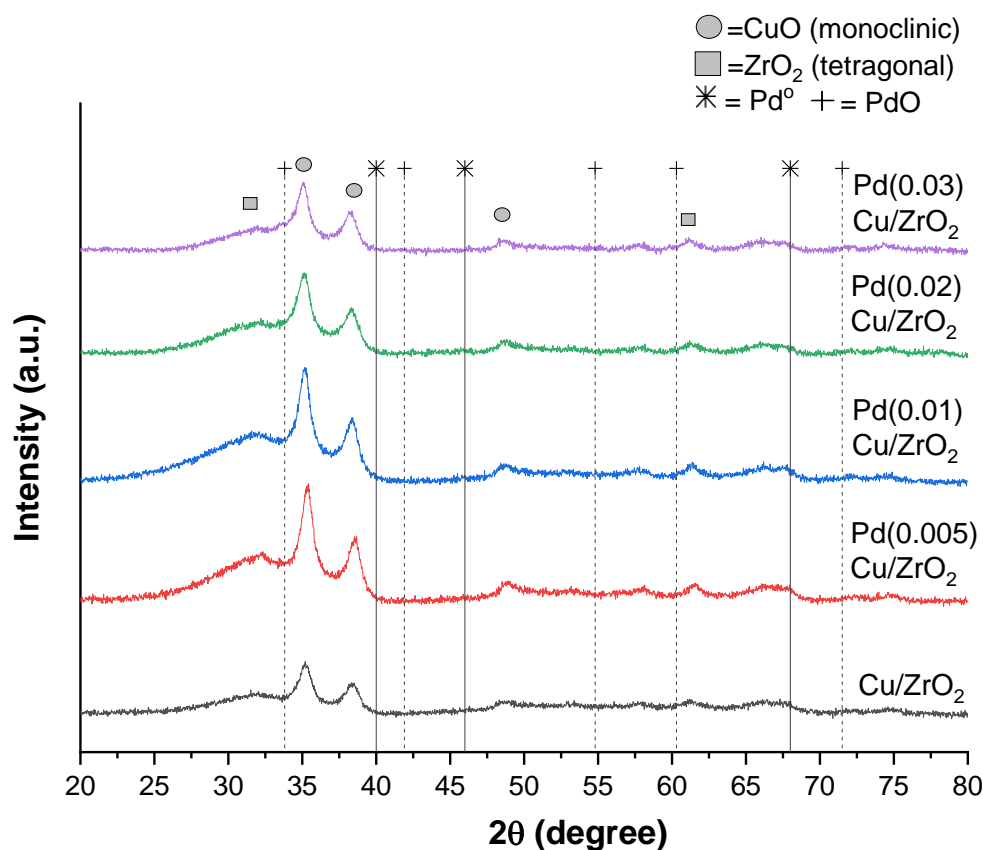
to the associated errors for the Cu surface area, Hinrichsen *et al.* found that N<sub>2</sub>O titration was indicative of both Cu surface area and oxygen defects present at the copper-zinc interface.<sup>(10)</sup> Moreover, Muhler and co-workers reported that N<sub>2</sub>O titration catalysts are prone to significant structural changes, which might lead to errors in the Cu surface area determination.<sup>(68)</sup> In our case, N<sub>2</sub>O titration was not conclusive to elucidate whether higher Cu surface area observed with increasing Pd concentration is related to surface Pd or to higher BET catalyst surface area. Nevertheless, it seems that neither the BET surface area nor the Cu surface area significantly affects the catalytic activity for MeOH formation.

**Table 3.3:** Physicochemical properties of Pd promoted catalysts and Cu/ZrO<sub>2</sub>.

Catalyst	Cu:Pd molar ratio	BET Surface area (m <sup>2</sup> /g)	*Cu Surface area (m <sup>2</sup> /g)
Cu/ZrO <sub>2</sub>	-	57	11.0
Pd (0.005)Cu/ZrO <sub>2</sub>	1 : 0.005	63	5.7
Pd (0.01)Cu/ZrO <sub>2</sub>	1 : 0.01	65	8.6
Pd (0.02)Cu/ZrO <sub>2</sub>	1 : 0.02	79	7.4
Pd (0.03)Cu/ZrO <sub>2</sub>	1 : 0.03	82	11.6

\*Pd (0) also catalytically active for N<sub>2</sub>O decomposition.

Phase differences between Pd-promoted catalysts were studied by XRD (Figure 3.6). The XRD pattern recorded for Cu/ZrO<sub>2</sub> shows characteristic peaks of monoclinic CuO at 36°, 39° and 49° corresponding to ( $\bar{1}$ 11), (111) and ( $\bar{2}$ 02) planes (PDF ref. 01-089-5896) and tetragonal zirconia (t-ZrO<sub>2</sub>) at 31.5° and 61° for (101) and (211) planes (PDF ref. 01-078-3194). Peaks corresponding to both crystallite phases, CuO and t-ZrO<sub>2</sub>, were broad and with low intensity, this indicates that the crystallites sizes were fairly small and that some amorphous material might be present. The addition of Pd seems to not affect the crystallite size of CuO and the peaks for the t-ZrO<sub>2</sub> phases are almost identical. No additional crystalline phases were observed for Pd-doped Cu/ZrO<sub>2</sub> catalysts, moreover, no Pd, PdO, CuPd or Cu<sub>3</sub>Pd were detected, with the exception of Pd(0.03)Cu/ZrO<sub>2</sub> catalyst, where the formation of PdO is observed as a very low intensity peak at 34° and 43°. The XRD results indicate that Pd is either well dispersed throughout the material or smaller than the XRD detection limit (clusters smaller than 2 nm).

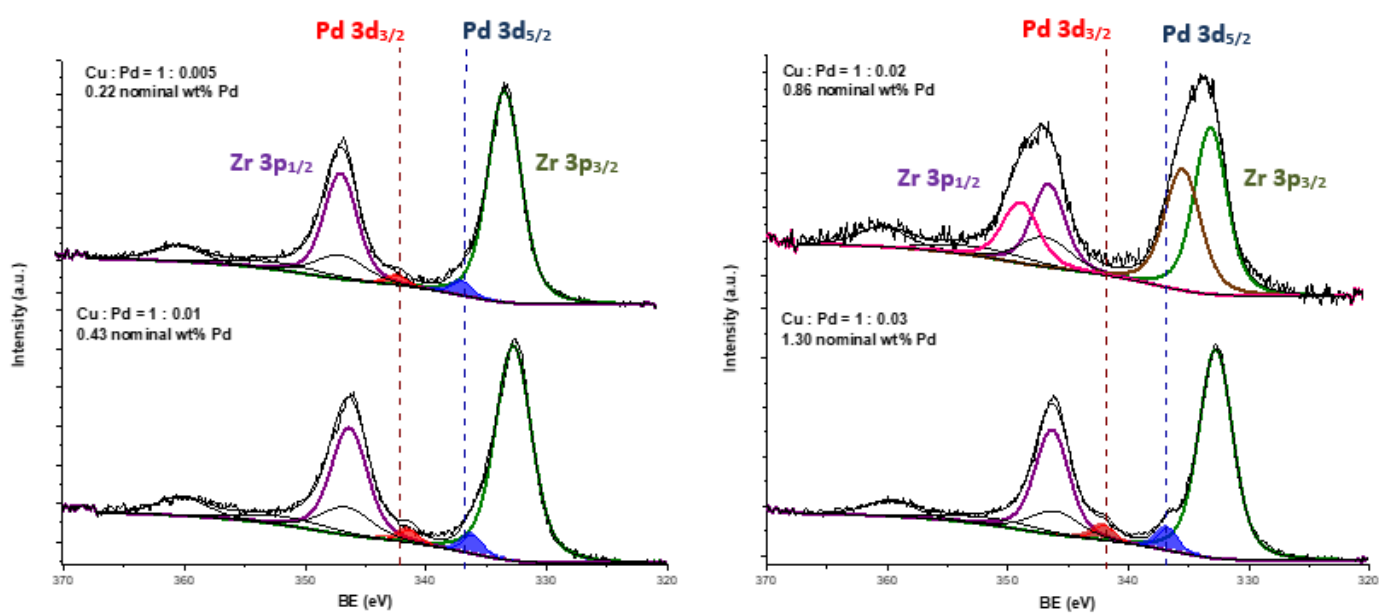


**Figure 3.6** - XRD patterns for Cu/ZrO<sub>2</sub> catalyst and series of Pd promoted catalysts in the range Cu : Pd molar ratio (1 : 0.005 – 1 : 0.03.)

XPS analysis was carried out on the samples in order to determine the quantity of surface Pd and any changes in oxidation state. The XPS data (Figure. 3.7) reveals changes in the Pd peaks between the different catalysts. Metallic Pd is reported to have a binding energy (BE) *ca.* 335 eV,<sup>(69)</sup> and the upward shift observed in the Pd peaks indicates the presence of PdO rather than Pd<sup>0</sup>. Due to the overlap of Pd and Zr 3p<sub>3/2</sub>, atomic percentages of the Pd were calculated from fits taken from bulk materials. The calculated concentrations of surface Pd, shown in Table 3.4, were significantly lower than expected, which can arise from Pd being present as large particles (poor dispersion) or the Pd being present within the bulk of the support or metal present (Cu). From the XRD data, it is most likely that the majority of the promoter remains trapped within the bulk of the support or present as a dilute alloy with Cu where it is unavailable for reaction. Hence, little change in activity is observed between the promoted catalysts compared to the unpromoted Cu/ZrO<sub>2</sub> catalyst.

**Table 3.4:** Summary of XPS data for Pd regions on Pd promoted catalysts.

Catalyst	BINDING ENERGY (eV) Pd		Total Atomic Percentage
	3d <sub>3/2</sub>	3d <sub>5/2</sub>	
Pd 1 (0.22 nominal wt% Pd)	341.5	336.2	1.9
Pd 2 (0.43 nominal wt% Pd)	341.4	336.1	2.3
Pd 3 (0.86 nominal wt% Pd)	341.4	336.1	0
Pd 4 (1.30 nominal wt% Pd)	342.0	336.7	2.8

**Figure 3.7** - XPS Spectra for Initial Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel with the addition of Pd promoters in the range Cu : Pd molar ratio (1 : 0.005 – 1 : 0.04). The Pd 3d<sub>5/2</sub> and Pd 3d<sub>3/2</sub> have been highlighted.

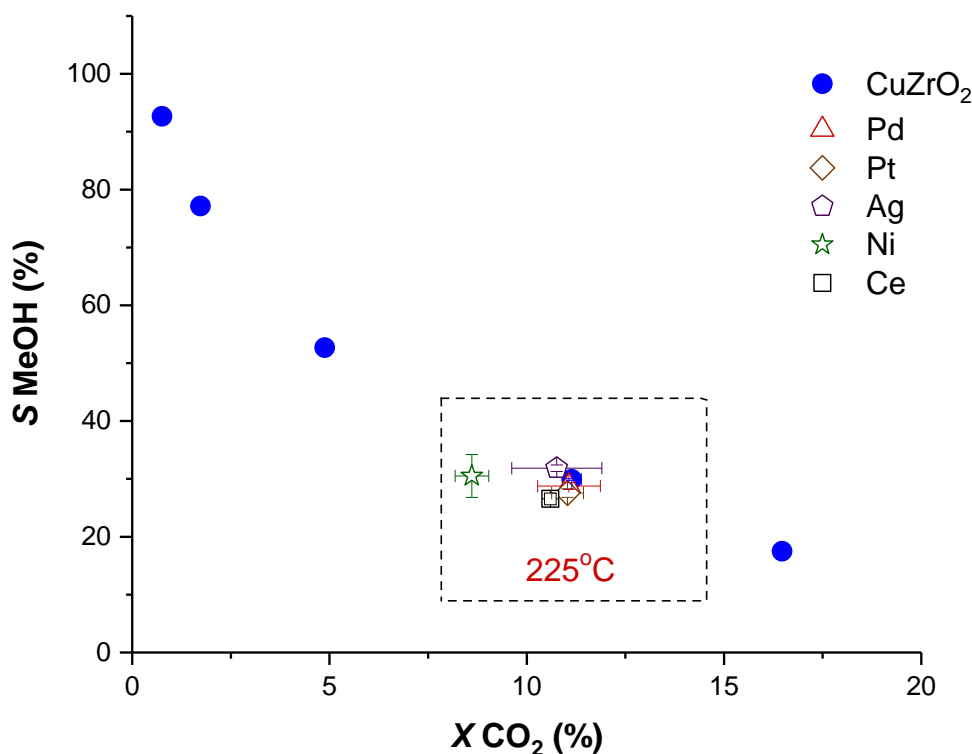
Based on our XRD results, it can be suggested that co-precipitation of Pd(NO<sub>3</sub>)<sub>2</sub>, Cu(NO<sub>3</sub>)<sub>2</sub> and Zr(NO<sub>3</sub>)<sub>2</sub> via oxalate gel led to well dispersed materials, broad and low intense CuO and t-ZrO<sub>2</sub> peaks were observed while no Pd related peaks were detected. Moreover, XPS characterisation suggests that Pd is homogeneously distributed throughout the material, and hence most of it is placed in the bulk of the material unable to significantly enhance MeOH rates via hydrogen spillover. This conclusion agrees with results observed by Melián-Cabrera *et al.*, where it was shown that the precipitation order for catalyst synthesis has a remarkable influence on the properties of the active phases and, consequently, on the catalytic performance for the hydrogenation of CO<sub>2</sub> to methanol ( $P = 60$  bar,  $CO_2/H_2 = 3$ , and  $T = 180$ – $240$  °C.) An enhanced methanol yield at 240 °C was observed for the Pd based Cu-ZnO catalyst prepared via sequential precipitation (11 mol MeOH/(h kg<sub>cat</sub>)) compared to the reference CuO-ZnO (9 mol MeOH/(h kg<sub>cat</sub>)) and this was attributed to a synergistic effect of Pd on the active Cu sites, which facilitated the H<sub>2</sub>-spillover mechanism. The catalyst prepared via co-precipitation resulted in very low methanol yields, almost inactive, compared to the reference Cu-ZnO catalyst which was due to significant changes in the bulk and surface properties of the catalyst: large CuO particle sizes, very low copper surface area, difficulty in CuO reduction, and greater instability towards sintering.<sup>(65, 70)</sup>



### 3.2.4 – Additional Promoters for Cu/ZrO<sub>2</sub>

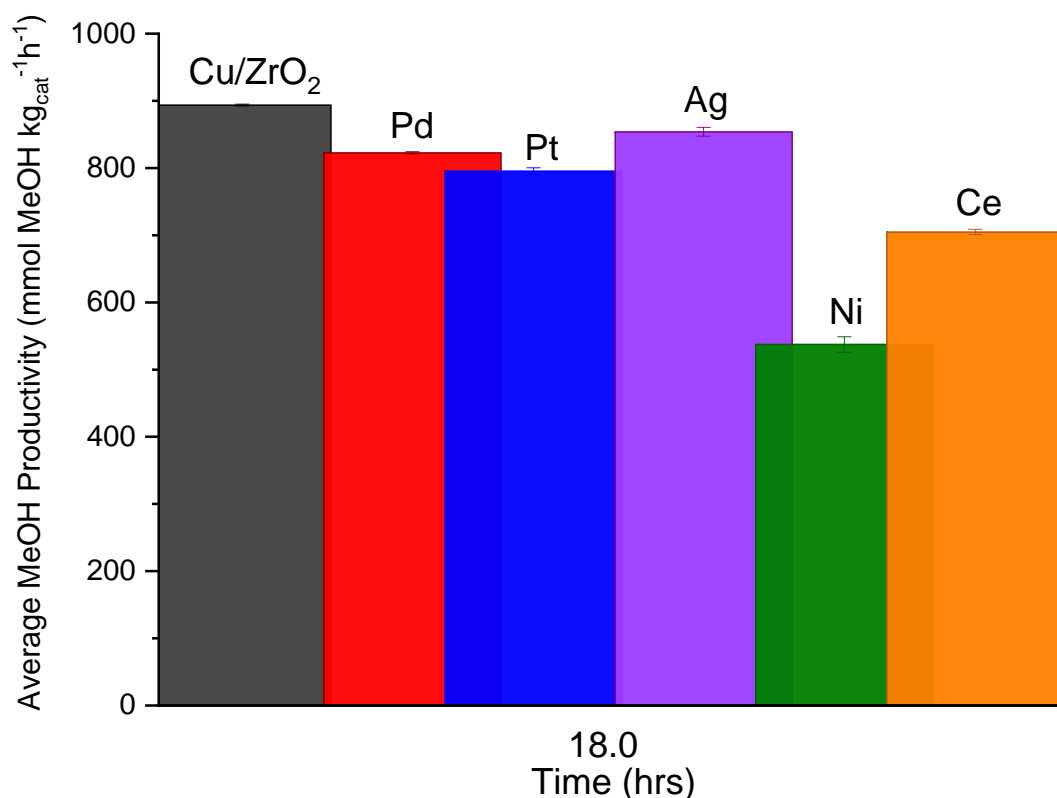
As shown in the previous section, the simultaneous co-precipitation of Pd(NO<sub>3</sub>)<sub>2</sub>, Cu(NO<sub>3</sub>)<sub>2</sub> and Zr(NO<sub>3</sub>)<sub>4</sub> during the oxalate gel synthesis resulted in a homogenous distribution of the three elements throughout the material and hence most of the Pd was not at the surface of the catalyst where required, resulting in no promoting effect. To concentrate promoters at the surface of the catalyst, Cu/ZrO<sub>2</sub> was prepared through the standard oxalate method, followed by promoter (Pd, Pt, Ag, Ni or Ce) post-impregnation, this is described in Section 2.21.

All promoted catalysts were prepared with a Cu to promoter molar ratio of 1:0.01. Prior to reaction, catalysts were dried (110 °C, 4 h), pelleted (425–600 μm) and pre-reduced *in situ* in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup>). CO<sub>2</sub> hydrogenation was assessed at 225 °C, 20 bar, 18 h, 30 ml min<sup>-1</sup>, 20 % CO<sub>2</sub>, 60 % H<sub>2</sub>, 20 % N<sub>2</sub>.



**Figure 3.8-** Activity of Cu/ZrO<sub>2</sub> catalyst vs various promoters at a Cu:X molar ratio of 1:0.01. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions:** Isothermal test at 225 °C, 18 h dwell, 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

As observed in Figure 3.8, no significant differences in CO<sub>2</sub> conversion or MeOH selectivity were observed between promoted and unpromoted Cu/ZrO<sub>2</sub> catalysts, with the exception of the NiCu/ZrO<sub>2</sub> which performs slightly worse, with lower CO<sub>2</sub> conversion (8.6 %) compared to Cu/ZrO<sub>2</sub> (11.1 %). When comparing MeOH productivity (Figure 3.9), it seems that the additions of Pd, Pt, Ag, Ni or Ce have a poisoning effect rather than a promoting one. The highest MeOH productivity of 890 mmol kg<sub>MeOH</sub><sup>-1</sup>h<sup>-1</sup> was recorded for Cu/ZrO<sub>2</sub> catalyst, and addition of a metal at low loadings seems to result in a lack of interaction between the active Cu sites, leading to lower MeOH productivity. The lowest MeOH productivity, observed for Ni-promoted Cu/ZrO<sub>2</sub> catalyst, can be attributed to a lower CO<sub>2</sub> conversion (8.7%) and slightly higher formation of CH<sub>4</sub> when compared with the other promoted catalysts, as shown in Table 3.5. Of the promoted catalysts tested, Pd and Pt resulted in the highest CO productivities, and the addition of Ag to Cu/ZrO<sub>2</sub> allows for an increase in DME and MeOH productivity at similar CO<sub>2</sub> conversions with a decrease in CO productivity.

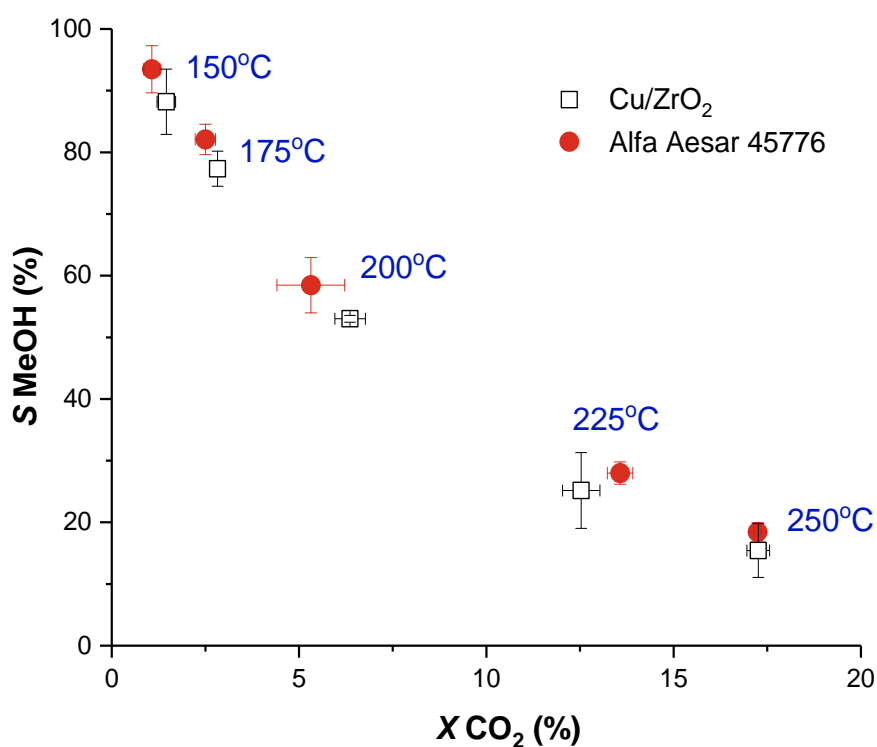


**Figure 3.9** – Methanol productivity data of Cu/ZrO<sub>2</sub> catalyst vs various promoters at a Cu:X molar ratio of 1:0.01. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: Isothermal test at 225 °C, 18 h dwell, 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

**Table 3.5:** productivity data for post-impregnation Cu/ZrO<sub>2</sub> promoted catalysts at 225 °C. Promoters at a Cu:X molar ratio of 1:0.01.

Catalyst	X CO <sub>2</sub> %	MeOH	DME	CH <sub>4</sub>	CO
		Productivity (mmol <sub>MeOH</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	Productivity (mmol <sub>DME</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	Productivity (mmol <sub>CO</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	Productivity (mmol <sub>CO</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )
Cu/ZrO <sub>2</sub>	11.13	881	2.59	0.08	2059
Cu/ZrO <sub>2</sub> - Pd	10.60	822	1.91	0.09	2052
Cu/ZrO <sub>2</sub> - Pt	11.10	795	2.23	0.09	2054
Cu/ZrO <sub>2</sub> - Ag	10.67	854	2.39	0.09	1844
Cu/ZrO <sub>2</sub> - Ni	8.70	537	1.78	0.13	1474
Cu/ZrO <sub>2</sub> - Ce	10.59	705	1.90	0.08	1979

### 3.2.5 – Catalyst Stability & Comparison between Cu/ZrO<sub>2</sub> and CZA catalysts



**Figure. 3.10** – MeOH selectivity and CO<sub>2</sub> conversion of Cu/ZrO<sub>2</sub> catalyst vs Commercial Alfa Aesar catalyst. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: 150 - 250 °C, 9 h dwells (total = 45 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3)(GHSV = 3,333 h<sup>-1</sup>), P(total) = 20 bar.

Once it was determined that the use of ZrO<sub>2</sub> as a support gave the best catalytic results, among a series of other supports (Section 3.2.1) employed for the synthesis of Cu-containing catalysts prepared via oxalate gel, we wanted to compare the Cu/ZrO<sub>2</sub> to a benchmark methanol synthesis CZA catalyst (Alfa Aesar, 45776). Catalysts were tested as previously described.

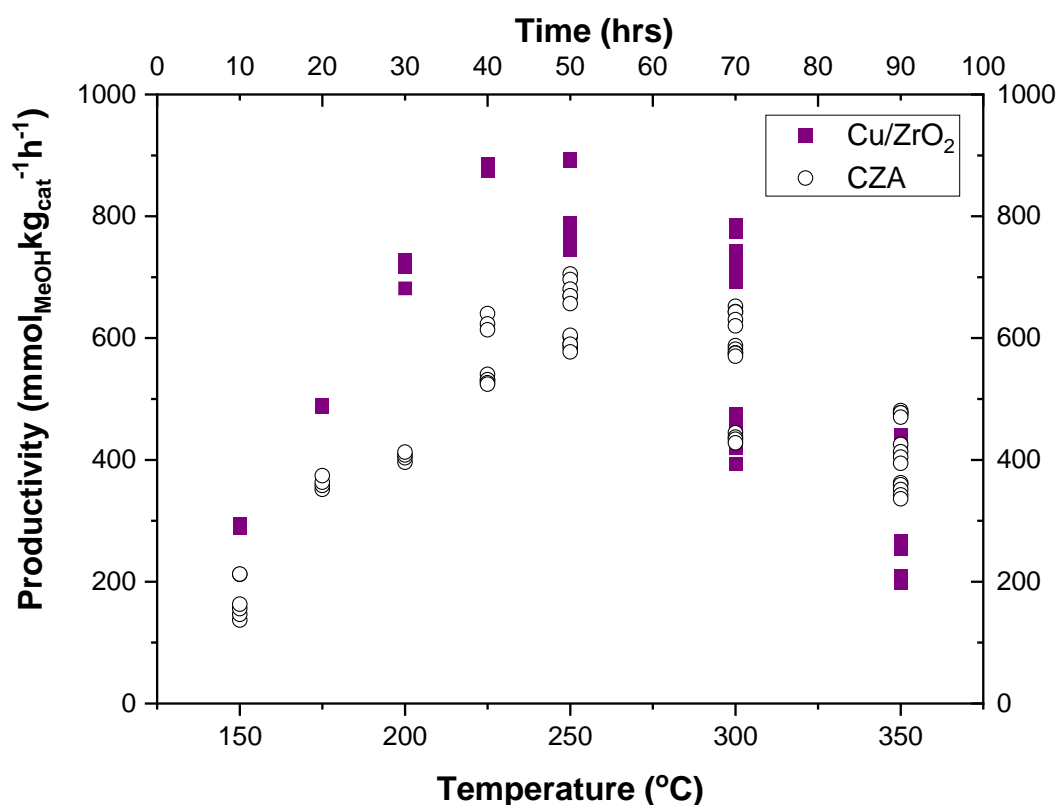
As observed in Figure 3.10, Cu/ZrO<sub>2</sub> prepared by the oxalate gel method presents comparable CO<sub>2</sub> conversion and MeOH selectivity to the commercial Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalyst over the temperature range studied, with an initial selectivity of 88% at 150 °C which then drops to 15.4% at 250 °C for Cu/ZrO<sub>2</sub> and a selectivity change of 93% to 18.4% for the commercial catalyst. A similar trend is seen for the conversion with Cu/ZrO<sub>2</sub>, increasing from 1.5 to 17.3% and the commercial catalyst increasing from 1.1 to 17.2%. Moreover, the trend line reflects an equilibrium limit where a decrease in methanol selectivity and an increase in CO<sub>2</sub> conversion are seen as the temperature is increased.

As important as CO<sub>2</sub> conversion and MeOH selectivity are when selecting an active catalyst, so is the catalyst stability. There are several pathways in which a solid catalyst can decay and they can be grouped into six intrinsic mechanisms. These include vapour formation; vapour-solid and/or solid-solid interactions; attrition/crushing; poisoning, which is the strong chemisorption (may be reversible) of reactants, products or impurities in the feed onto sites otherwise available for catalysis, and can potentially induce changes in the electronic or geometric structure;<sup>(71)</sup> fouling – the physical (mechanical) deposition of species from the fluid phase onto the catalyst surface, which results in activity loss due to blockage of sites and/or pores (e.g. coke and carbon deposition in porous catalysts); and thermal degradation and sintering – thermally induced deactivation of catalysts that results from sintering, which is the loss of catalytic surface area due to crystallite growth of the catalytic phase and loss of support area due to support collapse, which normally occurs at higher temperatures (> 500 °C) and are generally accelerated by the presence of water vapour. Understanding of these pathways allows for further optimisation of catalyst design and improved reaction conditions and thus increases the longevity of the catalyst during the process.<sup>(72)</sup>

In an industrial process catalysts are expected to remain stable under reaction conditions for as long as two years.<sup>(73 74)</sup> For example, in a methanol synthesis plant from a syngas feedstock (CO+CO<sub>2</sub>+H<sub>2</sub>), typical conditions adopted are 200–320 °C and 5–10 MPa, and variations in the synthesis gas phase composition have shown a close correlation between activity loss and loss of Cu surface area, suggesting that an important cause of deactivation is sintering, which may be promoted by over-reduction of Cu.<sup>(75)</sup> Studies have also indicated that when CO<sub>2</sub> is used as the feed, severe deactivation on Cu-based catalysts occur.<sup>(76)</sup> One of the major contributors to deactivation is the formation of water;

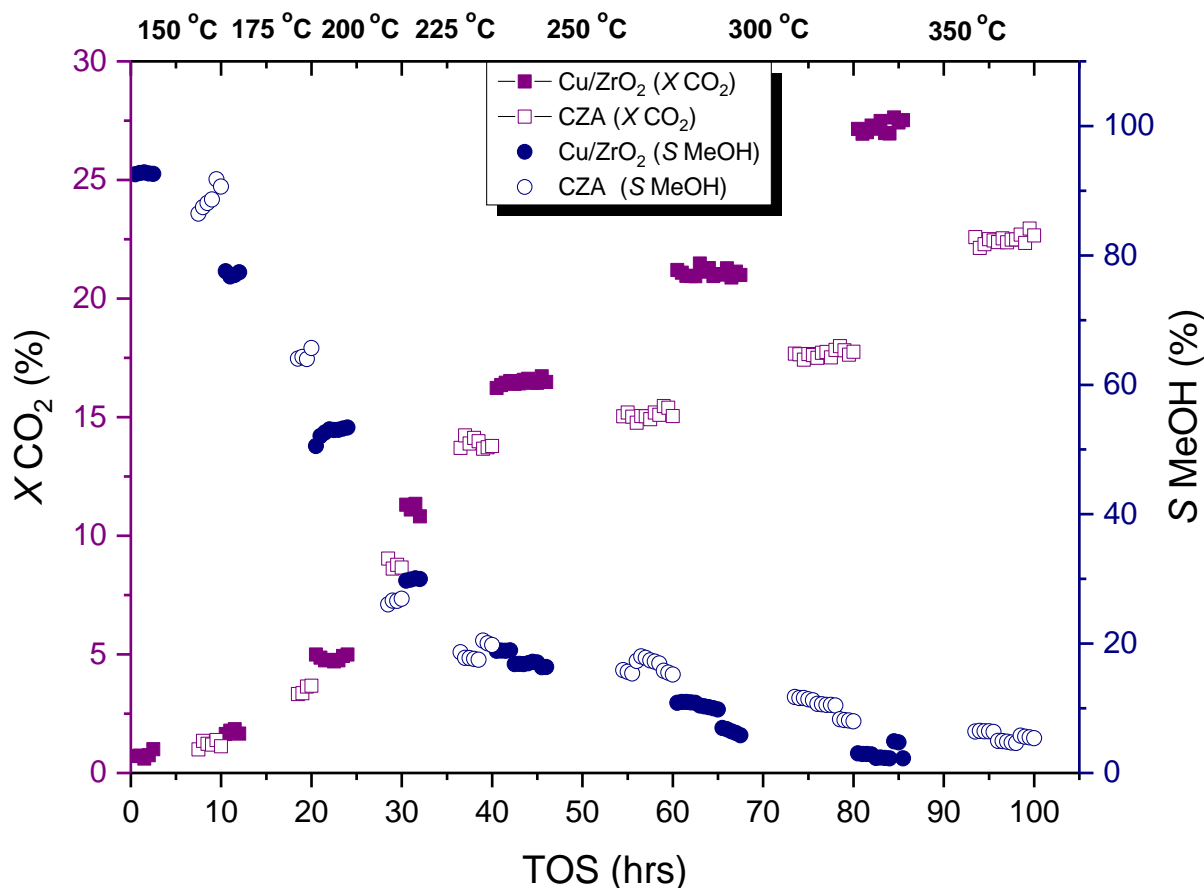
notably, one third of the H<sub>2</sub> is consumed to produce water, which is significantly wasteful compared to the commercial methanol production via synthesis gas.<sup>(77)</sup> Water is known to behave as a strong oxidant at elevated temperatures; under these conditions, the water oxidises the active Cu<sup>0</sup> to the less active Cu<sup>2+</sup> and thus reduces the number of active sites available for reaction. Wu *et al.* found that water produced during methanol synthesis from a CO<sub>2</sub>-rich feed (CO<sub>2</sub> (22%), CO (3%), H<sub>2</sub> (75%)) accelerated the crystallization of Cu and ZnO in a Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst, and led to the deactivation of the catalyst; they also showed that the addition of colloidal silica to the catalyst greatly improved the catalyst stability by suppressing the crystallization of Cu and ZnO.<sup>(78)</sup> Li *et al.* demonstrated that a Zr doped Cu-Zn-Zr-Al catalyst enhanced the stability for CO<sub>2</sub> hydrogenation by promoting the reduction of CuO, formed from the oxidation of Cu by water, in the presence of H<sub>2</sub>.<sup>(79)</sup>

The addition of CO into the gas feed, or gas recirculation, can improve the lifetime of Cu- based catalysts for the CO<sub>2</sub> hydrogenation to MeOH; however, we investigated catalysts stability using a 20 % CO<sub>2</sub>, 60 % H<sub>2</sub> and 20 % N<sub>2</sub> gas feed. The stability of Cu/ZrO<sub>2</sub> and the benchmark CZA catalysts was assessed at a reaction flow of 30 ml min<sup>-1</sup> and 20 bar pressure, 150 – 350 °C and total reaction time of 100 hrs. (Figure 3.11.)



**Figure 3.11** – Methanol productivity data over 100 hrs. for Cu/ZrO<sub>2</sub> and commercial Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalysts. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: temperature ramp study 150-225 °C, 10 hr dwell, 2 °C/min (total 40 hrs) then 250, 300 and 350 °C, 20 hr dwell, 2 °C/min (total 60 hrs); 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

Figure 3.11 above shows an increase in methanol productivity for both catalysts from 150 °C – 250 °C, with Cu/ZrO<sub>2</sub> achieving a maximum productivity of 894 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>, compared with 705 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> for the commercial catalyst. After 50 hrs, the productivity decreases for both catalysts, particularly for the Cu/ZrO<sub>2</sub> catalyst, which shows a drop in productivity of 78%, as the temperature increases up to 350 °C. However, when comparing the methanol selectivity and CO<sub>2</sub> conversion in Figure 3.12 (below), the catalysts remain fairly stable.



**Figure 3.12** – Methanol selectivity and CO<sub>2</sub> conversion data over 100 hrs for Cu/ZrO<sub>2</sub> and commercial Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalysts. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: temperature ramp study 150-225 °C, 10 hr dwell, 2 °C/min (total 40 hrs) then 250, 300 and 350 °C, 20 hr dwell, 2 °C/min (total 60 hrs); 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

As expected, an increase in CO<sub>2</sub> conversion and decrease in methanol selectivity is observed with increasing temperature, however there is a dramatic decrease in methanol selectivity for both catalysts as the temperature increases above 175 °C, the initial selectivity for both catalysts are around 90% and this falls to less than 5% by the end of the study. The methanol selectivity drops at a faster rate for the CZA catalyst compared to the Cu/ZrO<sub>2</sub> catalyst up until the reaction reaches 250°C after 40 hrs, where both catalysts achieve 18% methanol selectivity. The conversion and selectivity data across the

temperature range studied remains stable within the dwelling periods. The CZA catalyst shows a higher CO<sub>2</sub> conversion (9 %) than the Cu/ZrO<sub>2</sub> catalyst (5 %) after 30 hrs of reaction where the temperature reaches 200 °C; after increasing the temperature to 250 °C (50 hrs) the opposite is observed, and this difference is further increased as the reaction proceeds until the end (100 hrs) where there is a difference of 5% between the catalysts.

The significant change in CO<sub>2</sub> conversion and MeOH selectivity of the catalysts with increasing temperature can be associated with the increase in Cu particle size i.e., sintering as you approach higher temperatures, accompanied by the formation of water both from the reaction and the RWGS reaction leading to increased oxidation and deactivation of active sites.

Kurtz and co-workers conducted a rapid aging test where a selection of catalysts (Cu/ZnO, Cu/Al<sub>2</sub>O<sub>3</sub> and Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>) were tested under a 50 Nml min<sup>-1</sup> flow of synthesis gas (14% H<sub>2</sub>, 72% H<sub>2</sub>, 4% CO<sub>2</sub>, and 10% CO) and the temperature was gradually increased from 200 °C to 500 °C, with 50 °C increments and held for 8 h at each temperature, over a total of 125 hours. They concluded that the ZnO containing catalyst, that exhibited a pronounced deactivation behaviour compared to the other catalysts, was due to thermal sintering of the Cu crystallites. The addition of Al<sub>2</sub>O<sub>3</sub> was beneficial as a structural promoter and inhibited the thermal sintering of the Cu crystallites.<sup>(80)</sup> Spencer and Twigg also found that copper containing catalysts are susceptible to thermal sintering via a surface migration process, particularly at temperatures above 300 °C, and this is markedly accelerated by the presence of even traces of chloride.<sup>(81)</sup> Additional stabilisers and promoters such as alumina, alkaline earth oxides and other oxides were shown to play a number of important roles, including the inhibition of sintering and absorption of catalyst poisons.<sup>(82)</sup> These findings suggest that attention to catalyst design, particularly with the addition of promoters or oxides, can prove highly beneficial towards the stability of the catalyst; furthermore, control of other parameters such as the gas composition, temperature, and especially water removal are necessary to enhance the catalyst lifetime. One suggestion to alleviate H<sub>2</sub>O-induced catalyst sintering as well as increasing methanol selectivity and reducing the overall energy consumption is to optimise reactor design.

### 3.3 – Conclusions

Synthesis of catalysts for CO<sub>2</sub> hydrogenation to methanol via an oxalate gel precipitation method has been shown to be successful and reproducible. Comparing the activity of a number of supported Cu catalysts (Cu/ZnO, Cu/ZrO<sub>2</sub>, Cu/Al<sub>2</sub>O<sub>3</sub>, Cu/MgO, Cu/La<sub>2</sub>O<sub>3</sub>, Cu/CeO<sub>2</sub> and Cu/MnO) shows the influence the supports have on the catalyst. Ultimately, a change in the basicity or acidity of the supports results in changes to the catalyst performance most likely associated with changes to the intermediate species during the reaction, as reported in previous studies. Amphoteric supports were the most successful due to availability of basic sites to adsorb CO<sub>2</sub> and acid sites to activate formate species; ZrO<sub>2</sub> achieved the highest MeOH productivity of 811 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> of all the supports tested.

Addition of Pd to Cu/ZrO<sub>2</sub> catalysts at promoter levels (0.2 – 1.3 wt%) via the oxalate gel method proved unsuccessful, with no increase in methanol productivity, which is attributed to the homogeneous distribution of the Pd species within the bulk of the catalyst as opposed to the surface where it would be required for hydrogen spillover.

Addition of various promoters (Pd, Pt, Ag, Ni and Ce) to the Cu/ZrO<sub>2</sub> catalyst via post impregnation increased the concentration of surface metal species; however, no significant differences in CO<sub>2</sub> conversion or MeOH selectivity were observed between promoted and unpromoted Cu/ZrO<sub>2</sub> catalysts, with the exception of the NiCu/ZrO<sub>2</sub> with lower CO<sub>2</sub> conversion and higher methane selectivity. The lack of promotion effect observed for the promoted catalysts is likely due to the low metal loadings and proximity to the active Cu sites.

Cu/ZrO<sub>2</sub> prepared by the oxalate gel method presents comparable CO<sub>2</sub> conversion and MeOH selectivity to the commercial Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalyst over 150 – 250 °C. Comparing the stability of the catalysts over 100 hrs and increasing the temperature range from 150 – 350 °C, both Cu/ZrO<sub>2</sub> and the CZA catalyst remain fairly stable over time, but both catalysts show significant changes in CO<sub>2</sub> conversion and MeOH selectivity after 250 °C (total 60 hrs). The changes observed in the catalysts can be associated with an increase in Cu particle size i.e., sintering as you approach higher temperatures, accompanied by the formation of water from the RWGS reaction leading to increased oxidation and deactivation of active sites.

Recommendations for future work include; post-reaction characterization, particularly XRD, to determine the level of sintering and XPS to investigate any changes in surface oxidation. Also, the measurement of catalyst support basicity and acidity via CO<sub>2</sub> and NH<sub>3</sub>-TPD.



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## Chapter 4

# Phase Composition of Cu/ZrO<sub>2</sub> Catalysts and Their Impact on the Hydrogenation of CO<sub>2</sub> to MeOH.

### 4.1 – Introduction

As discussed previously the catalytic support has been shown to play an active and essential role in many systems including the hydrogenation of CO<sub>2</sub> to methanol. More recently, the interest towards the support composition of Cu/ZrO<sub>2</sub> catalysts has risen in order to gain a deeper understanding of the catalyst structure and possible reaction mechanisms.

ZrO<sub>2</sub> exists as three crystal forms: cubic, tetragonal and monoclinic; the isolation or mixture of these phases depends on the preparation method, particle size, defects and calcination temperature. The monoclinic phase is said to be the most stable at room temperature compared to the other two polymorphs, with the metastable tetragonal phase readily converted to the monoclinic phase at < 1170 °C and the cubic phase being stable >2370 °C.<sup>(1)</sup> The transition temperature, however, varies according to the defect degree of the crystallographic lattice and the existence of any additives.

The polymorphic nature of ZrO<sub>2</sub> has divided many researchers over its influence on the catalytic activity. A study by Bell and Jung looked at the effects of copper supported on monoclinic (*m*-ZrO<sub>2</sub>) and tetragonal zirconia (*t*-ZrO<sub>2</sub>) towards methanol synthesis using either CO or CO<sub>2</sub> as the feed. Their results showed that the catalyst supported by *m*-ZrO<sub>2</sub> was 4.5 times more active for methanol synthesis from CO<sub>2</sub>/H<sub>2</sub> than that supported by *t*-ZrO<sub>2</sub> (H<sub>2</sub>/CO<sub>x</sub> = 3, 60 mL/min, 275 °C, 7 bar), which is associated with a higher affinity of adsorbed intermediates to methanol. When using CO/H<sub>2</sub> as the feed, the *m*-ZrO<sub>2</sub> catalyst was found to be 7.5 times more active. The overall findings are a contribution of the ZrO<sub>2</sub> phase, where an increase in activity for *m*-ZrO<sub>2</sub> is expected with an increase in surface area, as well as the ratio of the surface area of Cu to that of ZrO<sub>2</sub>.<sup>(2)</sup> On the other hand, a number of studies have claimed that crystallisation of the zirconia (transformation from amorphous zirconia) is less catalytically active.<sup>(3)</sup> Early studies by Baiker *et al.*<sup>(4)</sup> showed that the lower Cu surface area combined with the crystallization of amorphous ZrO<sub>2</sub> (*am*-ZrO<sub>2</sub>) had a negative effect on the selectivity and activity of the Cu/ZrO<sub>2</sub> catalyst; the importance of a strong metal-support interaction was stressed. Sun and co-workers conducted studies on Cu supported onto different zirconia polymorphs, using CO feeds, and discovered



that the Cu/*t*-ZrO<sub>2</sub> catalyst, with a high Cu dispersion, showed greatest activity and selectivity to methanol compared to the two other catalysts. The CO conversion and space-time yield were only 11.30 %, 0.11 g/ml h<sup>-1</sup> and 9.28 %, 0.07 g/ml h<sup>-1</sup> for Cu/*am*-ZrO<sub>2</sub> and Cu/*m*-ZrO<sub>2</sub> catalysts, respectively, whereas the Cu/*t*-ZrO<sub>2</sub> catalyst was up to three times more active (13.96 %, 0.22 g/ml h<sup>-1</sup>) for methanol synthesis.<sup>(5)</sup> Recent studies by Tada *et al.* found that the interfacial sites on Cu/*am*-ZrO<sub>2</sub> that are obtained by reducing the prepared amorphous Cu–Zr–O oxides without forming crystalline CuO particles, are more active than those on Cu/*t*-ZrO<sub>2</sub> and Cu/*m*-ZrO<sub>2</sub>. Methanol adsorbs more weakly on *am*-ZrO<sub>2</sub> than on *m*-ZrO<sub>2</sub>, allowing the suppression of unwanted methanol decomposition and consequently a higher methanol selectivity.<sup>(6)</sup> Also, if the Cu loading of Cu/*am*-ZrO<sub>2</sub> decreases from 12 to 19 to 6–8 wt. % (the solubility limit of Cu species in *am*-ZrO<sub>2</sub>), the turnover frequencies (TOFs), methanol production per exposed Cu sites at weight/volume flow rate (W/F) of 430 g<sub>cat</sub> s L(STP)<sup>-1</sup>, increase from 16 to 18 to 29–39 h<sup>-1</sup> respectively.<sup>(7)</sup>

Although the differences in activity have been associated with support crystallographic structure, it is important to take into account the influence of catalyst preparation conditions, especially the acid-base environment as this can impact the surface hydroxylation and consequent activity. Indeed, a number of catalytic active sites can be found on the surface of zirconia, which include Brønsted acidic and basic hydroxyl groups, and coordinatively unsaturated Lewis acidic-base Zr<sup>4+</sup>O<sup>2-</sup> pairs.<sup>(8-12)</sup> It has been shown that all of these sites are crucial towards reactions involving CO and CO<sub>2</sub>.<sup>(4,7, 13)</sup> Differences in the methanol formation between the polymorphs are a reflection of the discrepancies in the concentration of these structural defects. Previous studies by Bell and co-workers found that the adsorption capacity of CO<sub>2</sub> is an order of magnitude higher for *m*-ZrO<sub>2</sub> (2–3 μmol/m<sup>2</sup>) compared to *t*-ZrO<sub>2</sub> (0.1 μmol/m<sup>2</sup>), which has been attributed to the increased concentration and basicity of hydroxyl groups as well as higher Lewis acidity/basicity of Zr<sup>4+</sup>/O<sup>2-</sup> pairs present on the *m*-ZrO<sub>2</sub> surface. The adsorption capacity of CO<sub>2</sub> on both *m*-ZrO<sub>2</sub> and *t*-ZrO<sub>2</sub> was shown to increase with surface area, suggesting that the surface density of adsorption sites increases with surface area. Furthermore, adsorption of CO<sub>2</sub> on monoclinic ZrO<sub>2</sub> produces bicarbonate and monodentate and bidentate carbonates, whereas bidentate and polydentate carbonates are formed on tetragonal ZrO<sub>2</sub>.<sup>(14)</sup>

An interesting study by Samson and co-workers looked at the effect of the various factors mentioned above for the activity of Cu/ZrO<sub>2</sub> catalysts in the synthesis of methanol from CO<sub>2</sub>. Their findings show that the methanol formation rate increases with increasing *t*-ZrO<sub>2</sub> phase in the catalyst, and the active centers are Cu<sup>+</sup> ions incorporated into the ZrO<sub>2</sub> lattice near oxygen vacancies. In addition, when investigating the acid sites formed, the addition of CuO onto the polymorphs resulted in an increase in Brønsted acid sites and an even larger increase (4-5 x) in the concentration of Lewis acid sites when

compared to those in the pure support; however, comparing the strength of the Lewis acid sites for the two polymorphs, the tetragonal zirconia was far greater than the monoclinic. A linear correlation was established between catalytic activity and acidity of the catalysts for both Brønsted and Lewis centres. In contrast to the previous studies, no correlation was found between the methanol formation rate and Cu surface area.<sup>(63)</sup>

Similar findings were also reported by Bueno and co-workers when studying copper catalysts supported on different ZrO<sub>2</sub> polymorphs for ethanol dehydrogenation to acetaldehyde and ethyl acetate. The catalytic properties of the Cu catalysts supported on *am*-, *m*-, or *t*-ZrO<sub>2</sub> phase were associated with the specific electron density of supported copper species (Cu<sup>0</sup> and Cu<sup>+</sup>) defined by the particle size and the interface at the copper metal oxide support. The active surface sites for the Cu/ *m*-ZrO<sub>2</sub> catalyst showed that greater ethyl acetate formation is determined by the high oxygen mobility from the bulk *m*-ZrO<sub>2</sub> phase to copper species, causing a high density of basic sites and a more heterogeneous distribution of the surface copper species (Cu<sup>0</sup> /Cu<sup>+</sup>).<sup>(15)</sup>

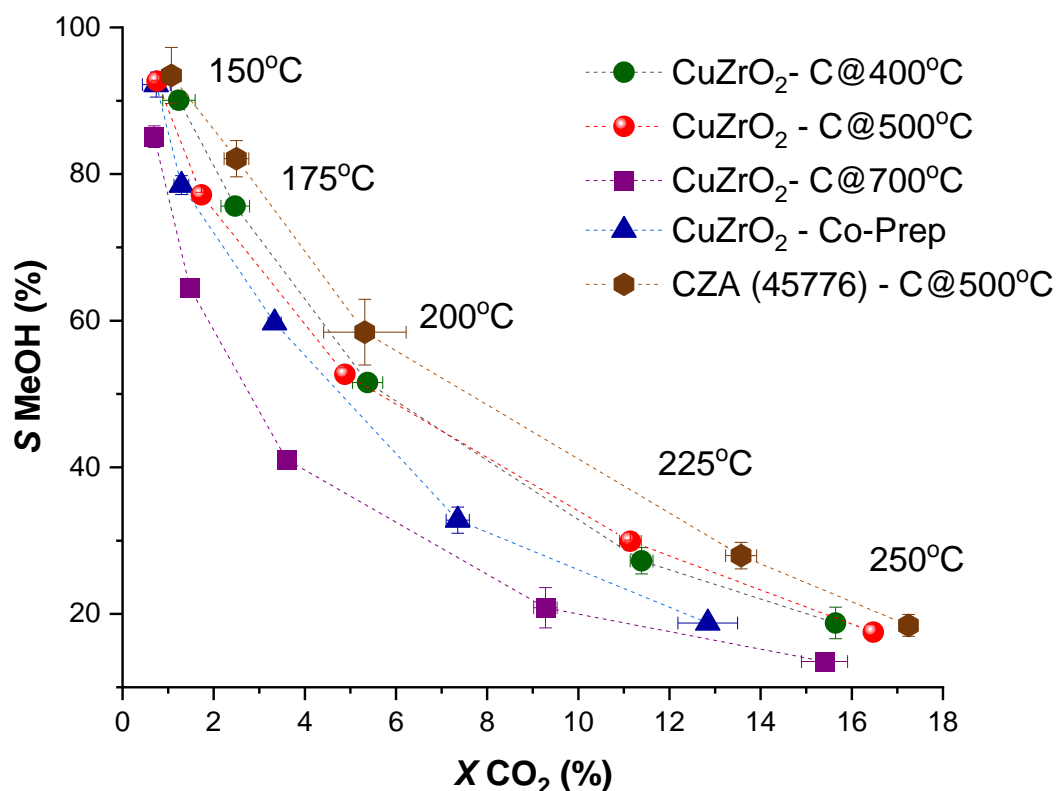
Lin *et al.* conducted a study on a unique catalyst with a ZrO<sub>2</sub>/Cu inverse configuration in which the domains of amorphous zirconia only covered a small fraction of the metallic copper surface. The catalysts were synthesised using a modified co-precipitation technique where oxalic acid was used for precipitation. The best ZrO<sub>2</sub>/Cu catalyst (ZrO<sub>2</sub>/Cu-0.1) displayed 3 times higher activity for the hydrogenation of CO<sub>2</sub> to methanol when compared with conventional Cu/ZrO<sub>2</sub> catalysts. (220 °C , CO<sub>2</sub>/H<sub>2</sub> = 1:3, 30 bar). AP-XPS and DRIFTS characterizations showed that the ZrO<sub>2</sub> species were in a highly reduced state and intermediates of formate and methoxy were formed and consumed on the inverse ZrO<sub>2</sub>/Cu much faster than on the Cu/ZrO<sub>2</sub> configuration. The high activity is mainly ascribed to the formation of a highly reactive HCOO-Cu intermediate adsorbed on the metallic Cu component of the inverse ZrO<sub>2</sub>/Cu catalyst.<sup>(16)</sup>

The work detailed in this chapter aims to explore the impact of varying the calcination temperature and reduction temperature of the Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel, towards their hydrogenation of carbon dioxide to methanol. The deposition of Cu onto the ZrO<sub>2</sub> polymorphs by oxalate gel and wet impregnation is also investigated to understand the effects of preparation method and support phase on catalytic activity.

## 4.2 – Results and Discussion

### 4.2.1 – Variation of Calcination Temperature

The effects of ZrO<sub>2</sub> phase transformation through varying the calcination temperature were explored using Cu/ZrO<sub>2</sub> catalysts prepared via the oxalate gel method. The catalysts were also compared against a Cu/ZrO<sub>2</sub> catalyst with the same metal loading (31 wt.%) prepared by a standard co-precipitation method. The catalysts were calcined at various temperatures (400, 500 and 700 °C) under static air with a ramp rate of 2 °C/min for 2 hrs. The catalysts were then tested for their activity towards CO<sub>2</sub> hydrogenation through a temperature ramp study (150–250 °C, with 10 h dwells at each temperature). at P(total) of 20 bar. The results are shown in Figure 4.1.

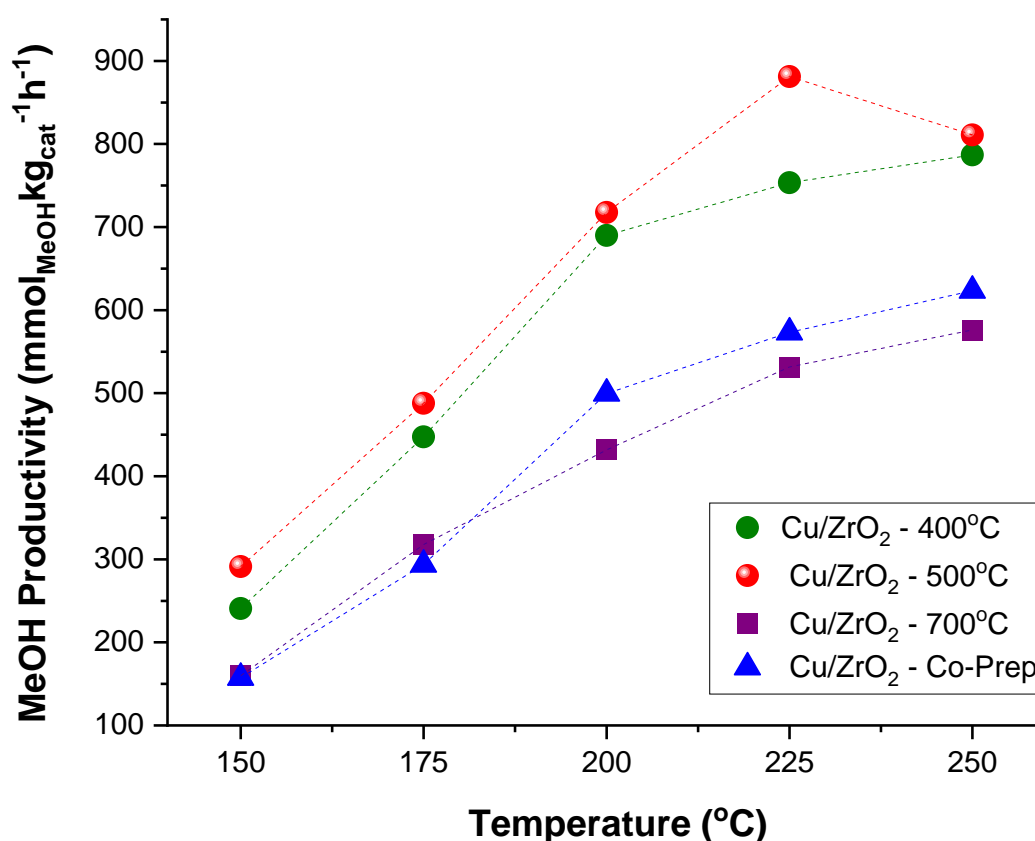


**Figure. 4.1** – CO<sub>2</sub> conversion vs MeOH selectivity of Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel and co-prep calcined at various temperatures (400, 500 & 700 °C) compared with Commercial Alfa Aesar Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> (CZA) catalyst. *In-situ* reduction conditions; 1 h at 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.



The methanol selectivity data for each catalyst in Figure 4.1 is shown to decrease, and CO<sub>2</sub> conversion increase, as the temperature is raised from 150 – 250 °C. Comparing the catalysts prepared via the oxalate gel method it can be seen that increasing the calcination temperature above 500 °C results in a loss in both the conversion and selectivity, which becomes more significant after 175 °C where the methanol selectivity drops to 41%. The catalysts calcined at 400 and 500 °C display very similar results, and are closest to the performance of the commercial CZA catalyst, which indicates that there are very small changes between the structure of the two calcined catalysts. The Cu/ZrO<sub>2</sub> catalyst prepared by a standard co-precipitation method is less active than the oxalate gel catalysts calcined at 400 and 500 °C. There is a clear change in the conversion data for all the catalysts, particularly after 200 °C, with a 5% difference between the co-prep catalyst and catalyst calcined at 500 °C, although there is little difference between the methanol selectivity of the catalysts calcined at the lower temperatures.

The differences between the calcined catalysts become more apparent when comparing the MeOH productivity over the different temperatures, as shown in Figure 4.2.



**Figure 4.2** – Methanol productivity of Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel and co-precipitation calcined at various temperatures (400, 500 & 700 °C).

The catalyst calcined at 500 °C achieves the highest MeOH productivity of 881 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 225 °C, followed closely by the catalyst calcined at 400 °C. The productivity for the catalyst calcined at 700 °C and catalyst prepared via co-precipitation remains level up to 175 °C at 300 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> before the co-prep catalyst overtakes the former at 200 °C. The Cu/ZrO<sub>2</sub> catalyst calcined at 700 °C displays the lowest productivity of 576 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> for all the catalysts tested. The general trend of an initial increase in productivity and decrease over higher catalytic temperatures is apparent in the majority of the catalysts tested, as expected with an increased rate of CO production from competing reactions.

The trends shown above suggest that the use of higher calcination temperatures cause a change in the structure of the catalyst and subsequently reduces the catalyst activity; the activity is also influenced by the catalyst preparation method. To investigate further, the catalysts were characterised using N<sub>2</sub>O pulse titration and standard BET method to compare the surface area in relation to the activity of the catalysts. The results for this are shown in Table 4.1.

**Table 4.1: Physiochemical properties of calcined Cu/ZrO<sub>2</sub> catalysts.**

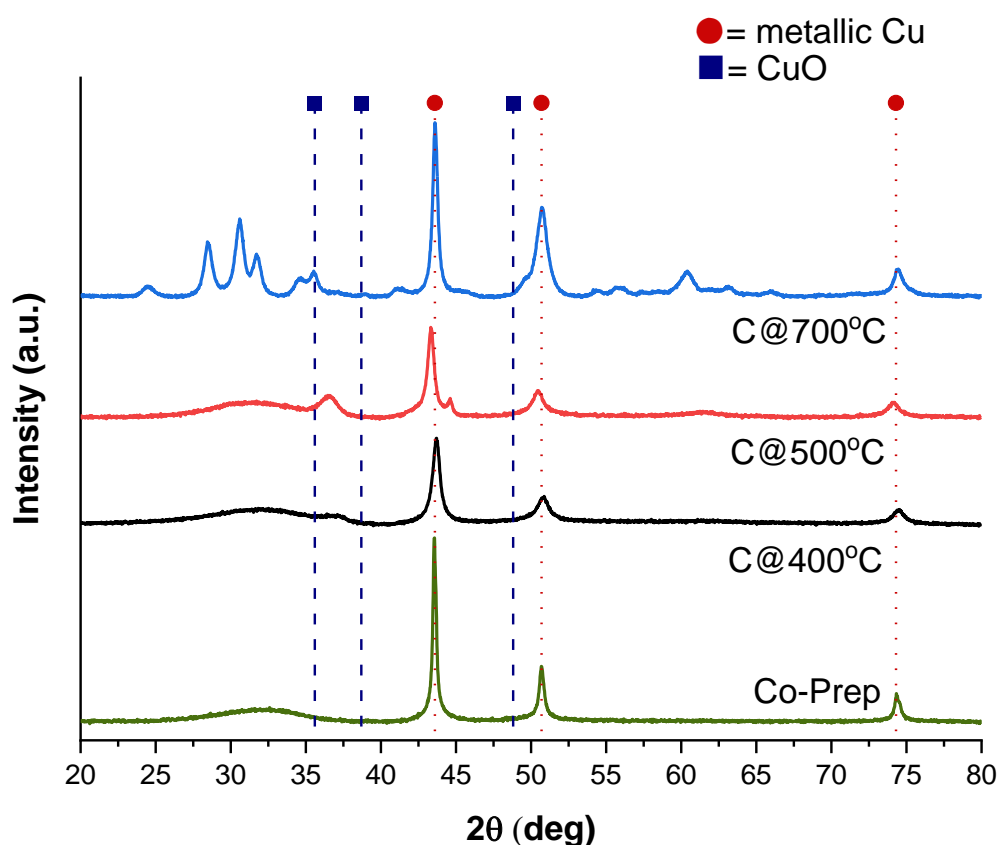
Catalyst	BET Surface area (m <sup>2</sup> /g)	Cu Surface area (m <sup>2</sup> /g)	Cu Particle Size (nm)*
Cu/ZrO <sub>2</sub> – C@400°C	53	11.4	11
Cu/ZrO <sub>2</sub> – C@500°C	57	10.8	11
Cu/ZrO <sub>2</sub> – C@700°C	22	11.5	17
Cu/ZrO <sub>2</sub> – Co-Prep	98	7.80	24
Alfa Aesar (45776)-CZA	72	20.2	11

\*Calculated via Scherrer equation for Cu (111) at 43.6°

Comparing the surface area data above, in Table 4.1 there are a range of surface areas between the catalysts. The catalysts calcined at 400 and 500 °C show identical Cu particle sizes (11 nm) and very similar surface area values; as mentioned previously, the work by Bell and co-workers established that the surface density of adsorption sites for CO<sub>2</sub> increases with an increase in surface area, particularly for *t*-ZrO<sub>2</sub>, and this reflects well with the activity data for the catalyst calcined at 500 °C. However, the least active catalysts (co-prep and Cu/ZrO<sub>2</sub> calcined at 700 °C) have BET surface area that vary significantly. The co-prep catalyst has the highest overall surface area (98 m<sup>2</sup>/g) but the specific Cu

surface area is marginally lower than the other catalysts, as well as containing larger Cu particles; but this catalyst performs slightly better than the catalyst calcined at 700°C, which has a very low BET surface area and most likely poor Cu dispersion and lack of CO<sub>2</sub> adsorption sites across the surface. These findings support the studies by Sun and co-workers, where greater Cu dispersion was linked to higher methanol activity and selectivity, and oppose the work of Bell and Jung where the most crystalline polymorph (*m*-ZrO<sub>2</sub>) was the most active. The commercial catalyst shows both high surface area (72 m<sup>2</sup>/g) and low Cu particle size (11 nm); the information suggests that the surface area and particle size may be a factor influencing the methanol activity but it is not the determining factor, and likely a combination of factors, such as the catalyst surface properties and metal-support interactions, as there is no clear trend in methanol productivity between the surface areas and Cu particle sizes displayed between the catalysts.

XRD analysis was performed on all of the catalysts and the resulting patterns are shown in Figure 4.3.

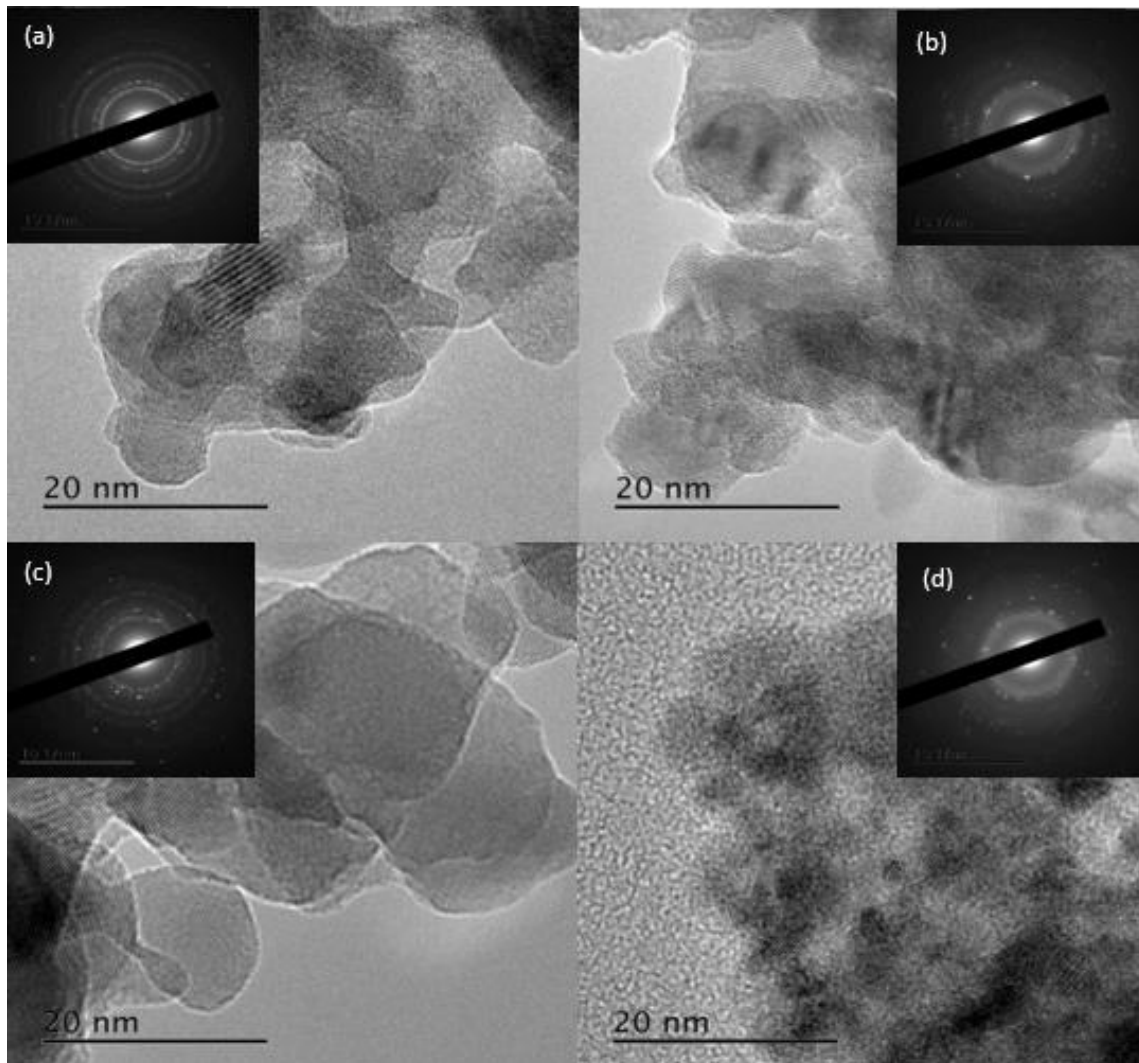


**Figure 4.3.** – XRD patterns for the reduced Cu/ZrO<sub>2</sub> catalysts calcined at 400, 500 and 700 °C and Cu/ZrO<sub>2</sub> prepared via co-precipitation. Peaks for metallic Cu have been highlighted with red circles and CuO with blue squares.

The XRD patterns show an increase in crystallinity as the calcination temperature is increased from 400 to 700°C. Comparing the two preparation methods, the co-precipitation catalyst is more crystalline than to the Cu/ZrO<sub>2</sub> catalysts prepared via the oxalate gel method. The most intense reflections observed at  $2\theta = 43.6^\circ$  are assigned to metallic Cu (111), which was used to estimate the Cu particle size using the Scherrer equation (Table 4.1); the remaining Cu<sup>0</sup> peaks are located at 50.7° and 74.3° and correspond to the (200) and (220) planes respectively (PDF ref. 01-071-4609). Peaks for CuO are also included, the major reflections are observed at  $2\theta = 35.6, 38.7$  and  $48.8^\circ$  and correspond to the ( $\bar{1}11$ ), (111) and ( $\bar{2}02$ ) planes respectively. Comparing the XRD patterns, the catalyst calcined at 700 °C shows low intensity peaks for CuO; no CuO peaks are found in the remaining catalysts. The increase peak width between the catalysts corresponds to an increase in the Cu particle size. Partial phase transformation of the ZrO<sub>2</sub> from tetragonal (*t*-ZrO<sub>2</sub>) to monoclinic (*m*-ZrO<sub>2</sub>) at 700°C is also observed, indicated by the formation of additional peaks at  $2\theta = 24.5, 28.5, 30.6$  and  $31.7^\circ$ ; only very small reflections were observed for tetragonal zirconia, with the majority being monoclinic. These phase transformations at the calcination temperatures used are well known for ZrO<sub>2</sub>, and the addition of elements such as Cu have little effect on the temperature, suggesting the incorporation of Cu into the matrix does not have a major impact on the phase transition temperatures of ZrO<sub>2</sub>.<sup>(17, 18)</sup>

The reflections for the most active catalyst (calcined at 500 °C) are very similar to those of the catalyst calcined at 400 °C; however, the peaks for tetragonal zirconia at  $2\theta = 36.5^\circ$  and  $60.3^\circ$  are more pronounced and there is the additional peak for monoclinic zirconia at  $44.6^\circ$ . The co-prep and catalyst calcined at 400 °C are more amorphous, with broad peaks around  $33^\circ$  assigned to tetragonal zirconia, and no signs of monoclinic zirconia are seen. The slight differences in the structure of the catalyst may be the cause for changes in the catalytic activity, with mixed phases of tetragonal and monoclinic zirconia being more favourable, as opposed to a complete transition to monoclinic zirconia that leads to larger Cu particles and hence a dramatic decrease in methanol activity.

In order to study this in more detail Selected Area Electron Diffraction (SAED) patterns were taken of the catalysts as shown in Figure 4.4.



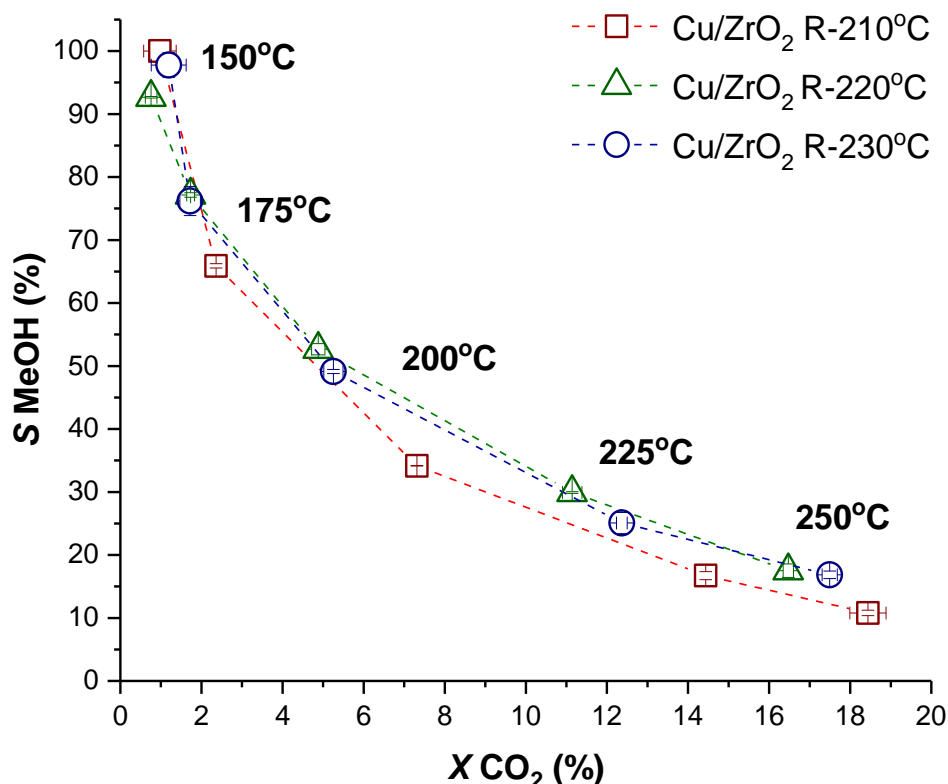
**Figure 4.4.** – TEM images with corresponding SAED patterns for (a): Cu/ZrO<sub>2</sub>-400 °C, (b): Cu/ZrO<sub>2</sub>-500 °C, (c): Cu/ZrO<sub>2</sub>-700 °C and (d): Cu/ZrO<sub>2</sub> – Co-Prep.

The SAED patterns show an increase in crystallinity with an increase in calcination temperature for the catalysts prepared via the oxalate gel method, as shown in the XRD patterns (Figure 4.3.). The crystallinity is evident by the rise in bright spots and disappearance of the diffuse rings corresponding to the amorphous layers. From Figure 4.4, the catalyst prepared via the co-precipitation method is most crystalline and the presence of multiple fringes shows the presence of larger CuO particles across the surface. The large lattice fringes in the remaining images are due to zirconia, and it is difficult to identify the presence of the CuO due to the inhomogeneity of the sample.

Combining the information above, it can be concluded that the increase in crystallinity and Cu particle size at higher temperatures, coupled with changes in the zirconia phase (transformation of tetragonal to monoclinic), lead to a decrease in methanol activity.

### 4.2.2 – Variation of Reduction Temperature

Changes in reduction temperature have been shown to impact the metal particle size and therefore increase the productivity of a catalyst. In this section, the changes in reduction temperature of the Cu/ZrO<sub>2</sub> catalysts will be explored and comparisons between the activity investigated.



**Figure. 4.5** - Activity of Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel and reduced at various temperatures (210, 220 & 230 °C). *In-situ* reduction conditions; 1 h in 5 %H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup>STP). **Reaction conditions:** 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

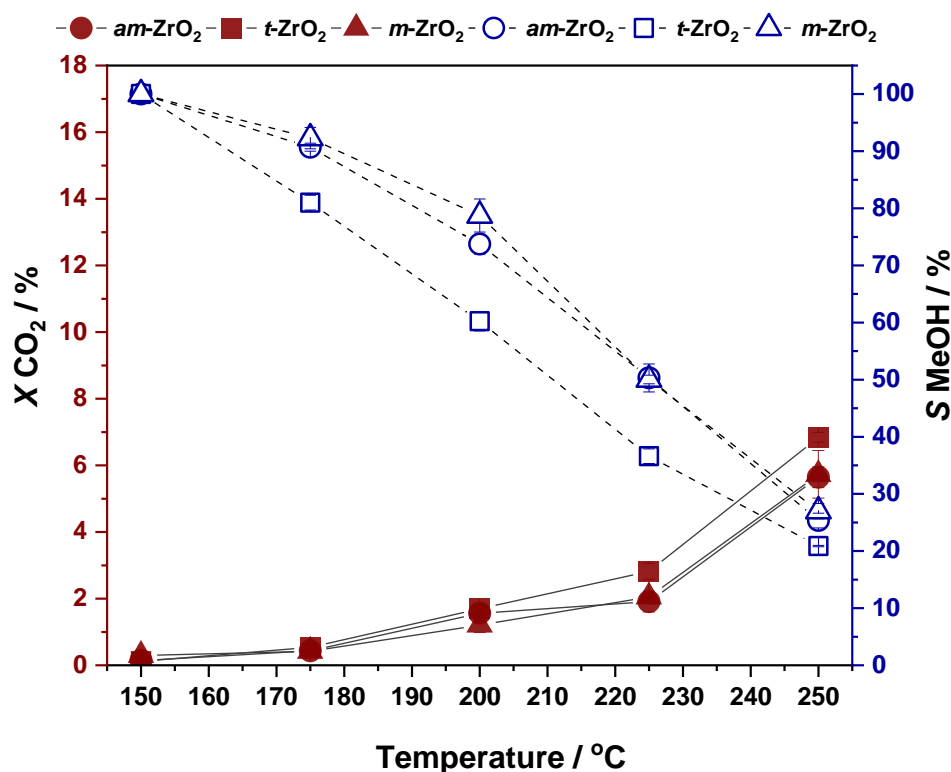
Figure 4.5 compares the methanol selectivity and CO<sub>2</sub> conversion between Cu/ZrO<sub>2</sub> catalysts pre-reduced *in-situ* with 5 % H<sub>2</sub>/He at three different temperatures – 210, 220 and 230 °C. A small temperature range was chosen for the reduction in order to prevent sintering of the Cu particles, and consequent loss of catalytic activity. The catalysts all have a high methanol selectivity (above 93 %), at the start, and this then drops with an increase in temperature and conversion. Although the catalyst reduced at the lower temperature (210 °C) shows the greatest decrease in methanol selectivity (66 %) above 200 °C, the CO<sub>2</sub> conversion remains greater than the other reduced catalysts. Very little difference is observed between the Cu/ZrO<sub>2</sub> catalysts reduced at 210 and 220 °C, at testing temperatures below 250 °C; the catalyst reduced at 220 °C slightly outperforms the other catalyst in

regard to the methanol selectivity between 175 – 225 °C, yet the CO<sub>2</sub> conversion remains somewhat greater for the catalyst calcined at 230 °C. The data suggests that a small change in the reduction temperature of the Cu/ZrO<sub>2</sub> catalysts has very little influence on the overall performance of the catalyst, which is most likely due to the Cu particles becoming fully reduced at temperatures  $\geq 220$  °C, as reflected in the XRD patterns (Figure 4.5). Any temperatures below this are likely to result in the presence of unreduced Cu species and consequently a reduction in methanol activity.

Work by Ramírez and co-workers looked at the influence of the calcination and reduction temperature over Cu/ZnO catalysts at atmospheric pressure. The best combination of calcination and reduction temperature was 10CuZnO-350-200 (ACuZnO-B-C: A, loading percentage; B, calcination temperature; C, reduction temperature), which gave the highest conversion to methanol. When they increased the calcination temperature more than 350 °C, the TPR showed that the  $\alpha$  and  $\beta$  peaks corresponding to the reduction of Cu(II) to Cu(I) and Cu(I) to Cu(0) merged together. This proved that the reduction became harsher and also there is an increase in particle size with calcination temperature. Interestingly, the influence of reduction temperature on particle size was the opposite. The size of Cu(0) decreased with reduction temperature. Studies on the methane–methanol selectivity of this catalyst proved the role of Cu oxidation states in governing the product selectivity. 10CuZnO-350-150 resulted in higher methane selectivity than methanol, which the authors attributed to the unreduced Cu(I) and Cu(II) because they observed these species in the XRD. Thus, for methanol, the best reduction temperature was identified as 200 °C, and it gave good conversion below 250 °C for methanol, where CO selectivity was less. A reduction temperature of 400 °C yielded CuZn alloy, which generated good selectivity to methanol only at  $>200$  °C. This study suggests a fine balance between the calcination and reduction temperatures is required to obtain the optimal Cu state and catalytic activity.<sup>(19)</sup>

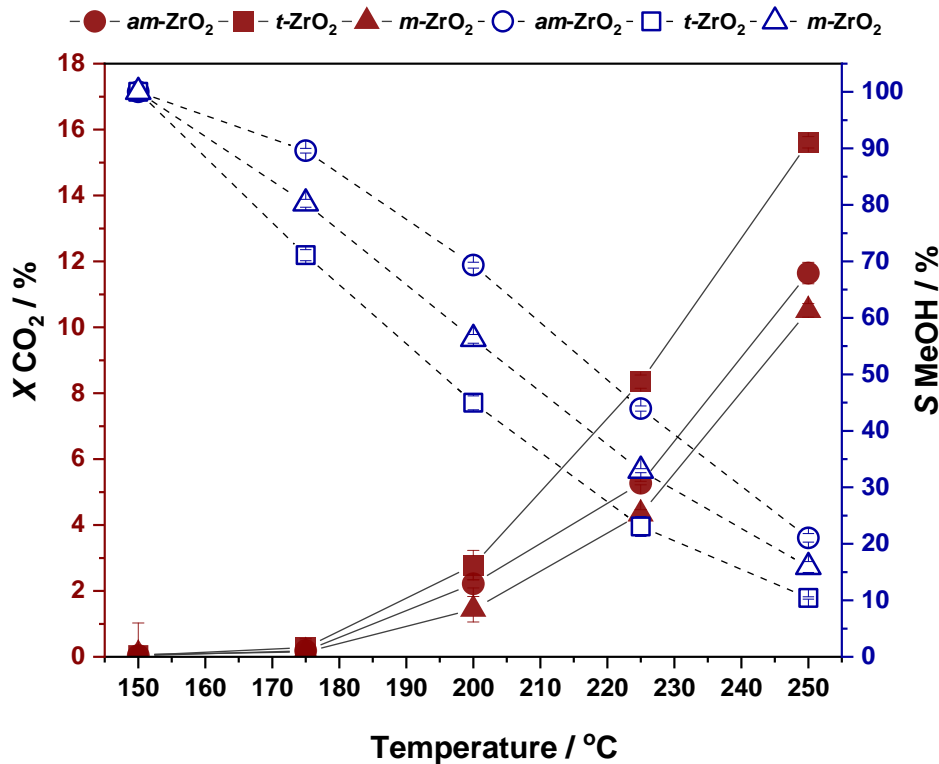
### 4.2.3 – Variation of Cu Deposition

As shown in the previous sections the variation of calcination and reduction parameters has marginal effect on the catalysts. In order to observe a more significant change and to establish the effect of changing the phase of the support without impacting the Cu particles, Cu was deposited onto different calcined ZrO<sub>2</sub> phases; amorphous (*am*-ZrO<sub>2</sub>), tetragonal (*t*-ZrO<sub>2</sub>) and monoclinic (*m*-ZrO<sub>2</sub>), all prepared via the oxalate gel method through two preparation methods. The first method was oxalate gel, and the second method was wet impregnation (WI). The Cu loading for all catalyst were fixed at 31 wt. %; after preparation catalysts were dried in static air at 500 °C for 2 h, 10 °C min<sup>-1</sup>. Prior to reaction catalysts were pelleted (425–600 μm), and 0.5 g of pelleted catalyst was secured with quartz wool in the reactor tube and pre-reduced *in-situ* with 5 % H<sub>2</sub>/He (220 °C, 1 h, 2 °C min<sup>-1</sup>). After reduction, the reactor was allowed to cool to 50 °C, the gas flow was switched from 5 % H<sub>2</sub>/He to the reaction mixture (20 % CO<sub>2</sub>, 60 % H<sub>2</sub>, 20 % N<sub>2</sub>) and was pressurised to 20 bar at a flow rate of 30 ml min<sup>-1</sup>. Catalyst activity was assessed between 150 and 250 °C, for a total of 50 h.



**Figure. 4.6a** - Activity of Cu/ZrO<sub>2</sub> catalysts with 3 different ZrO<sub>2</sub> phases- *am*-ZrO<sub>2</sub> (400-OG), *t*-ZrO<sub>2</sub> (500-OG) and *m*-ZrO<sub>2</sub> (700-OG) prepared via oxalate gel. *In-situ* reduction conditions; 1 h, 220 °C in 5% H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.





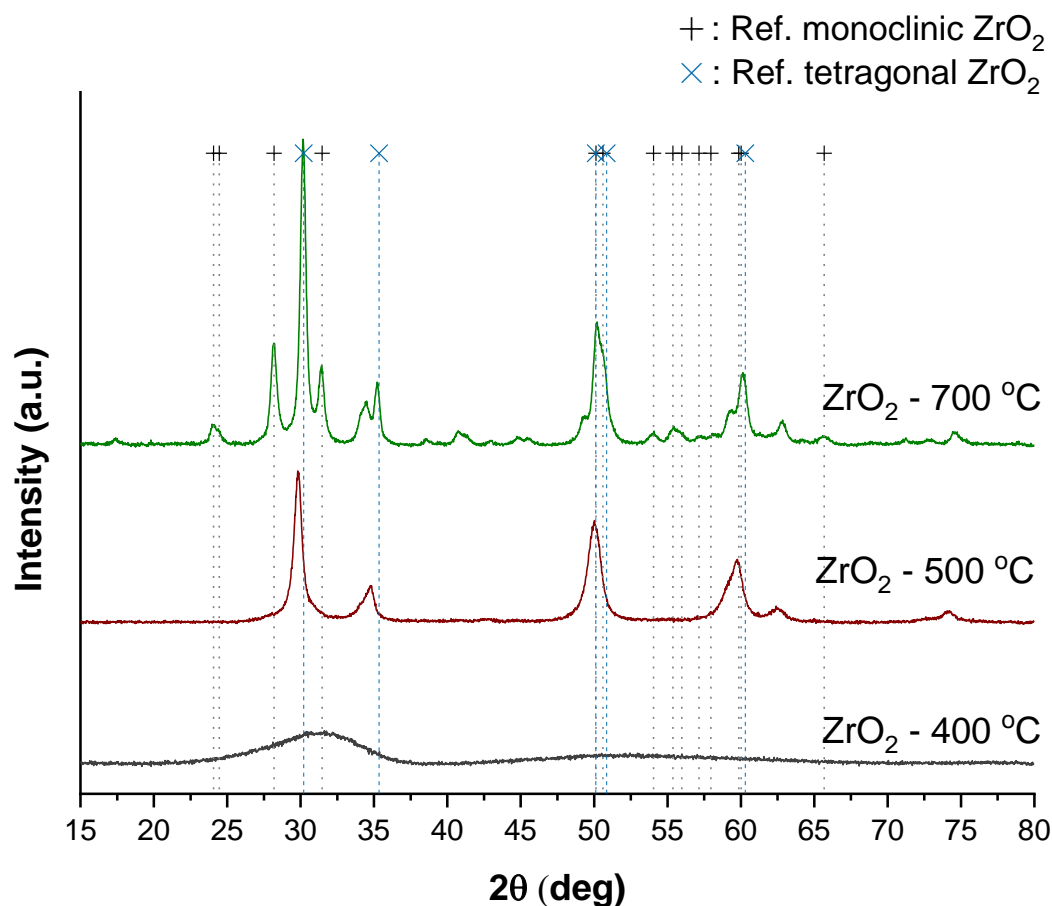
**Figure. 4.6b** - Activity of Cu/ZrO<sub>2</sub> catalysts with 3 different ZrO<sub>2</sub> phases- *am*-ZrO<sub>2</sub> (400-OG), *t*-ZrO<sub>2</sub> (500-OG) and *m*-ZrO<sub>2</sub> (700-OG) prepared via wet impregnation. *In-situ* reduction conditions; 1 h, 220 °C in 5 % H<sub>2</sub>/He (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Reaction conditions: 150 - 250 °C, 10 h dwells (total = 50 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

The catalysts can be split according to their Cu deposition methods: Figure 4.6a shows the catalysts prepared via oxalate gel; and Figure 4.6b shows the catalysts prepared via wet impregnation. As seen previously for Cu/ZrO<sub>2</sub>, the CO<sub>2</sub> conversion increases with temperature and the selectivity towards methanol decreases. The catalysts prepared via the oxalate gel show very similar conversions (1.6 %) up to 200 °C, and beyond this only a small increase (1 %) is observed for the tetragonal ZrO<sub>2</sub> catalyst (500-OG). On the other hand, Cu/*t*-ZrO<sub>2</sub> displays the lowest methanol selectivity across the temperature range studied, compared to the other catalysts, with a difference of up to 12%. Both the amorphous ZrO<sub>2</sub> (400-OG) and monoclinic ZrO<sub>2</sub> (700-OG) exhibit comparable methanol selectivities. In contrast, the catalysts prepared via wet impregnation can be distinguished more easily according to the crystallographic phases of ZrO<sub>2</sub>; noticeably, the conversions are higher and the methanol selectivities lower when compared to the oxalate gel catalysts. For the wet impregnation catalysts, clear differences are observed at 225 °C and above; the tetragonal ZrO<sub>2</sub> catalyst reaches a maximum CO<sub>2</sub> conversion of 16%, followed by 12% for amorphous ZrO<sub>2</sub> and 11% for monoclinic ZrO<sub>2</sub>. Differences in methanol selectivity can be observed from 175 °C onwards; amorphous ZrO<sub>2</sub> maintains the highest methanol selectivity across the temperature range falling to 21% at 250 °C, in contrast to monoclinic ZrO<sub>2</sub> at 16% and tetragonal ZrO<sub>2</sub> at 10%.

**Table 4.2:** Activity of Cu/ZrO<sub>2</sub> catalysts with varying ZrO<sub>2</sub> phases at 225 °C.

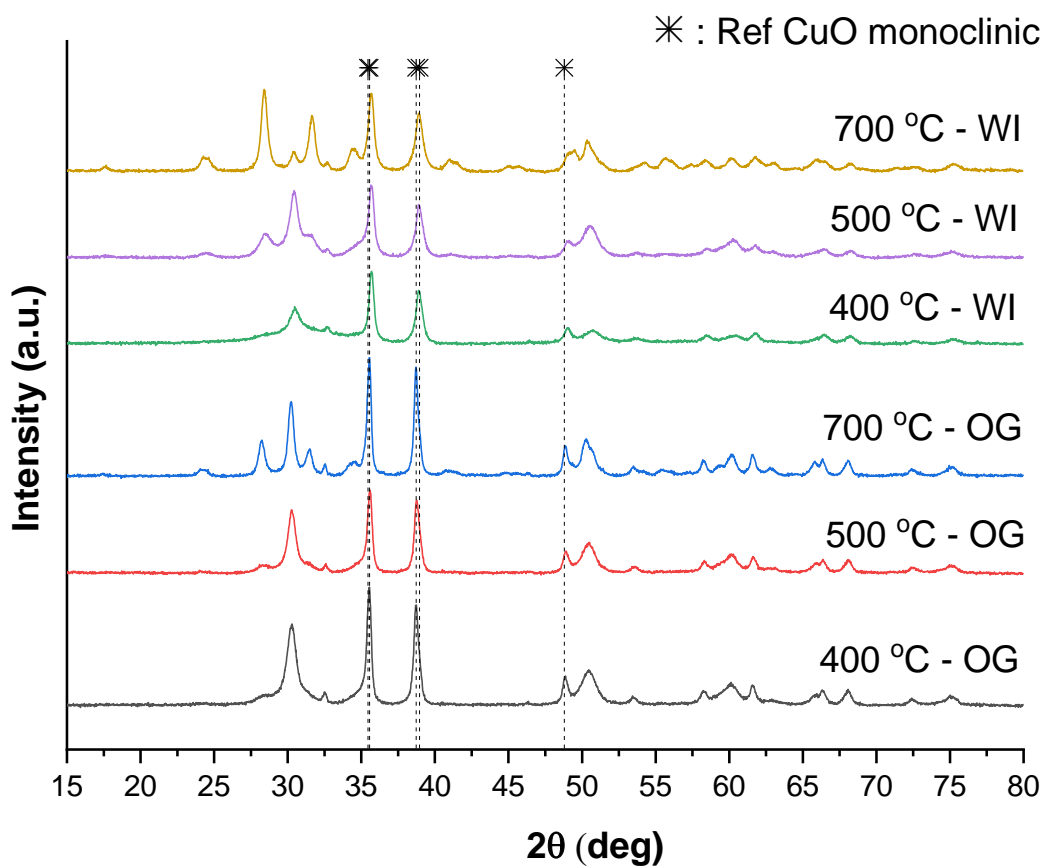
Catalyst	X CO <sub>2</sub> %	S MeOH %	S CO %	MeOH Productivity (mmol <sub>MeOH</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	CO Productivity (mmol <sub>CO</sub> kg <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )
Cu/ZrO <sub>2</sub> -400-OG	1.9	50.3	49.5	323	319
Cu/ZrO <sub>2</sub> -500-OG	2.8	36.6	63.4	226	392
Cu/ZrO <sub>2</sub> -700-OG	2.1	50.0	50.0	281	281
Cu/ZrO <sub>2</sub> -400-WI	5.3	43.9	55.9	521	662
Cu/ZrO <sub>2</sub> -500-WI	8.3	23.1	76.9	460	1531
Cu/ZrO <sub>2</sub> -700-WI	4.3	33.0	67.0	333	677

The difference in activity between the catalysts is highlighted in Table 4.2, where the reaction data is provided for 225 °C. As described above, the wet impregnation catalysts are more active compared to the oxalate gel catalysts. Interestingly, both sets the tetragonal ZrO<sub>2</sub> catalysts display a higher CO<sub>2</sub> conversion and significantly lower methanol selectivity. Furthermore, the amorphous Cu/ZrO<sub>2</sub> catalysts achieve the highest methanol productivity, when compared against the tetragonal and monoclinic phases, at 323 and 521 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>, respectively.



**Figure 4.7.** – XRD patterns for synthesised ZrO<sub>2</sub> catalysts calcined at 400, 500 and 700 °C; reference peaks for monoclinic ZrO<sub>2</sub> have been highlighted with + and reference peaks for tetragonal ZrO<sub>2</sub> have been highlighted with x in blue.

XRD analysis was performed on the synthesised ZrO<sub>2</sub> supports before Cu deposition, in order to determine if the calcination at the various temperatures formed the phases expected, and to identify any presence of mixed phases (Figure. 4.7). The crystallinity of the supports increases with an increase in the calcination temperature as expected; at 500 °C, a change from amorphous ZrO<sub>2</sub> to tetragonal ZrO<sub>2</sub> is observed, with characteristic peaks at 29.8°, 34.8°, 50.0°, 59.8°, 62.6° and 74.2° corresponding to (101), (002), (112), (211), (202) and (220) planes. As the temperature is increased further from 500 to 700 °C, a partial phase transition from tetragonal to monoclinic zirconia is seen. Reference data for monoclinic ZrO<sub>2</sub> (PDF ref num. 01-078-0047) and tetragonal ZrO<sub>2</sub> (PDF ref num. 01-078-3194) has been added for comparison; the most prominent peaks for the monoclinic ZrO<sub>2</sub> are 24.1°, 24.4°, 28.2°, 31.5° and 50.3° corresponding to (011), (110), ( $\bar{1}11$ ), (111) and (220) planes. To understand the potential changes in the support structure, additional XRD patterns were taken of the calcined catalysts after Cu deposition, via both the oxalate gel and wet impregnation (Figure 4.8).



**Figure 4.8.** – XRD patterns for calcined Cu/ZrO<sub>2</sub> catalysts, post Cu deposition onto ZrO<sub>2</sub> 400, 500 and 700 °C via oxalate gel and wet impregnation. Reference peaks for monoclinic CuO have been highlighted.

The XRD patterns in Figure 4.8 show an increase in crystallinity for both series of catalysts from 400 to 700 °C. Comparing the two preparation methods (wet impregnation and oxalate gel), the reflections observed for the ZrO<sub>2</sub> phases and CuO are very similar; differences are observed primarily in the peak intensities and widths, with the series of catalysts prepared via wet impregnation having less intense and more broad peaks, the series of catalysts prepared via oxalate gel displaying sharper and more intense peaks. The results suggest that the CuO particles deposited onto the Cu/ZrO<sub>2</sub> catalysts via wet impregnation are smaller than those deposited via the oxalate gel method.

The most intense reflections observed at  $2\theta = 35.6^\circ$  are assigned to monoclinic CuO ( $\bar{1}11$ ), which was used to estimate the CuO particle size using the Scherrer equation (Table 4.2). The remaining CuO peaks are located at  $38.9^\circ$  and  $48.8^\circ$  and correspond to the (100) and ( $\bar{2}02$ ) planes, respectively (PDF ref. 01-089-5896). The peaks for the various ZrO<sub>2</sub> phases are also shown for each catalyst, as was shown in Figure 4.7 for the supports before Cu deposition. The reflections expected for tetragonal and monoclinic zirconia are maintained, with Cu/ZrO<sub>2</sub>-500 °C exhibiting peaks for both monoclinic and

tetragonal zirconia and the Cu/ZrO<sub>2</sub>-700 °C exhibiting peaks for monoclinic zirconia; only this is true for both the wet impregnation and oxalate gel catalysts. The only exception was the Cu/ZrO<sub>2</sub>-400 °C system, where the amorphous support has now transformed, compared to no Cu, with reflections matching those of tetragonal zirconia; this is more pronounced for the oxalate gel catalyst.

**Table 4.2:** *Physiochemical properties of Cu/ZrO<sub>2</sub> catalysts calcined at 400, 500 and 700 °C and prepared via oxalate gel and wet impregnation.*

Catalyst	BET Surface area (m <sup>2</sup> /g)	Cu Surface area (m <sup>2</sup> /g)	CuO Particle Size (nm)*
Cu/ZrO <sub>2</sub> – C@400 °c-OG	94	5.11	34
Cu/ZrO <sub>2</sub> – C@500 °c- OG	50	4.58	31
Cu/ZrO <sub>2</sub> – C@700 °c- OG	20	5.04	37
Cu/ZrO <sub>2</sub> – C@400 °c-WI	41	9.00	29
Cu/ZrO <sub>2</sub> – C@500 °c-WI	33	7.94	25
Cu/ZrO <sub>2</sub> – C@700 °c-WI	17	8.30	23

\*Calculated via Scherrer equation for CuO ( $\bar{1}11$ ) at 35.6°

Comparing the two sets of catalysts, the BET surface areas vary according to the temperature used to calcine the support of the catalysts, with the monoclinic ZrO<sub>2</sub>-supported Cu catalyst calcined at the higher temperature of 700 °C giving the lowest BET surface area, in contrast to the less crystalline supported Cu catalyst calcined at 400 °C that gives the highest BET surface area. The CuO particle sizes remain fairly similar, as expected from the XRD patterns in Figure 4.8; the catalysts prepared by wet impregnation achieve smaller CuO particles than those prepared by the oxalate gel method. On the other hand, there are greater differences between the two sets of catalysts when comparing the Cu surface areas. The same trend is observed in both sets of catalysts; the Cu surface area increases as the calcination temperature of the catalyst support decreases. This trend correlates with the reaction data shown in Figures 4.6a and 4.6b, where the activity towards methanol production goes in the order 400 > 700 > 500 °C. Despite having higher CO<sub>2</sub> conversions, the methanol selectivity of the mixed ZrO<sub>2</sub> phase-supported Cu catalysts (500 °C) were lower than the other catalysts.

The results described above can be linked to both the type of method used to deposit the Cu in the support, and to the type of support phase present. Choosing a less crystalline support and adding Cu particles with larger surface areas, that are more well dispersed, is more favourable towards an increase in catalyst performance. The results match the work of Baiker *et al.*, as mentioned at the beginning, where the combination of an increase in support crystallinity and low Cu surface area results indicates a weakened metal-support interaction and subsequently lower activity. In addition, Bell and co-workers also emphasised the importance of acid-base sites on the support surface, this environment is influenced by the type of preparation method used, and from the data the deposition of the Cu onto the ZrO<sub>2</sub> supports through wet impregnation helped maintain the integrity of key structural defects compared to the catalysts where the Cu was deposited through the oxalate gel method. Furthermore, the adsorption capacity of CO<sub>2</sub> increases with surface area; therefore, the increased surface area of the Cu/ZrO<sub>2</sub>-400 catalysts can be linked to an increase in surface density of the adsorption sites and hence an increase in the adsorption capacity of CO<sub>2</sub>.

### 4.3 – Conclusions

The formation of the three zirconia phases – amorphous (*am*-ZrO<sub>2</sub>), tetragonal zirconia (*t*-ZrO<sub>2</sub>) and monoclinic zirconia (*m*-ZrO<sub>2</sub>) are possible through varying the calcination temperatures of the Cu/ZrO<sub>2</sub> catalysts prepared via the oxalate gel method. Temperatures  $\geq 700^\circ\text{C}$  afford more crystalline *m*-ZrO<sub>2</sub>, a temperature of  $500^\circ\text{C}$  results in a majority *t*-ZrO<sub>2</sub> phase, and temperatures  $\leq 400^\circ\text{C}$  achieves *am*-ZrO<sub>2</sub>. When comparing the catalysts with a co-precipitation catalyst of the same Cu loading (31 wt.%), increasing the calcination temperature above  $500^\circ\text{C}$  resulted in a loss in both the catalytic conversion and selectivity; the catalysts calcined at  $400^\circ\text{C}$  and  $500^\circ\text{C}$  displayed very similar results and were closest to the performance of the commercial CZA catalyst, which indicates that there are very small changes only between the structure of the two calcined catalysts. The Cu/ZrO<sub>2</sub> catalyst prepared by a standard co-precipitation method was more active than the oxalate gel catalyst when calcined at  $700^\circ\text{C}$ . The catalyst calcined at  $500^\circ\text{C}$  achieved the highest MeOH productivity of  $881 \text{ mmol}_{\text{MeOH}}\text{kg}_{\text{cat}}^{-1}\text{h}^{-1}$  and the Cu/ZrO<sub>2</sub> catalyst calcined at  $700^\circ\text{C}$  displayed the lowest productivity of  $576 \text{ mmol}_{\text{MeOH}}\text{kg}_{\text{cat}}^{-1}\text{h}^{-1}$ . These results reflect an increase in Cu surface area and Cu dispersion.

In addition, small change in the reduction temperature of the Cu/ZrO<sub>2</sub> catalysts had very little influence on the overall performance of the catalyst, which is most likely due to the Cu particles becoming fully reduced at temperatures  $\geq 220^\circ\text{C}$ , as reflected in the XRD patterns. Any temperatures below  $220^\circ\text{C}$  are likely to result in the presence of unreduced Cu species and consequently a reduction in methanol activity.

Cu was deposited onto the pre-synthesised ZrO<sub>2</sub> supports via wet impregnation and the oxalate gel method. The wet impregnation catalysts were more active than the oxalate gel catalysts, with the more amorphous Cu/ZrO<sub>2</sub> catalysts achieving the highest methanol productivity. Again, an increase in Cu surface area and Cu dispersion leads to an increase in activity, likely due to stronger metal-support interactions; in addition, increased surface area of the Cu/ZrO<sub>2</sub>-400 catalysts can be linked to an increase in surface density of the adsorption sites and hence an increase in the adsorption capacity of CO<sub>2</sub>. Overall, the type of preparation method used, as well as the ZrO<sub>2</sub> phase, Cu surface area and Cu dispersion, all play an important part towards the catalyst activity.

Future work recommendations include enhanced characterisation of catalysts, such as *in-situ* XRD to follow the changes in the support phases under reaction conditions. Also investigating additional methods to add Cu to the supports.

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## Chapter 5

# Cu/Zn Zeolite Catalysts for the Indirect Conversion of CO<sub>2</sub> to hydrocarbons.

### 5.1 – Introduction

We have already discussed in Chapter 3 the significance of methanol among the possible CO<sub>2</sub> hydrogenation products, not only because CH<sub>3</sub>OH is an essential product in its own right but it can also be blended with gasoline and used as an intermediate for the production of numerous important chemicals.<sup>(16)</sup> CH<sub>3</sub>OH is currently produced over Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts from syngas (CO + H<sub>2</sub> + CO<sub>2</sub>) at 200-300 °C and 80-120 bar.<sup>(1)</sup> Under laboratory testing conditions (20-50 bar), the CO<sub>2</sub> hydrogenation to CH<sub>3</sub>OH is limited to the 200-270 °C range, as at lower temperatures little CO<sub>2</sub> conversion is observed, whereas at higher temperatures CH<sub>3</sub>OH productivity is limited by the equilibrium due to the promotion of the reverse water gas shift (RWGS) reaction.<sup>(2)</sup>

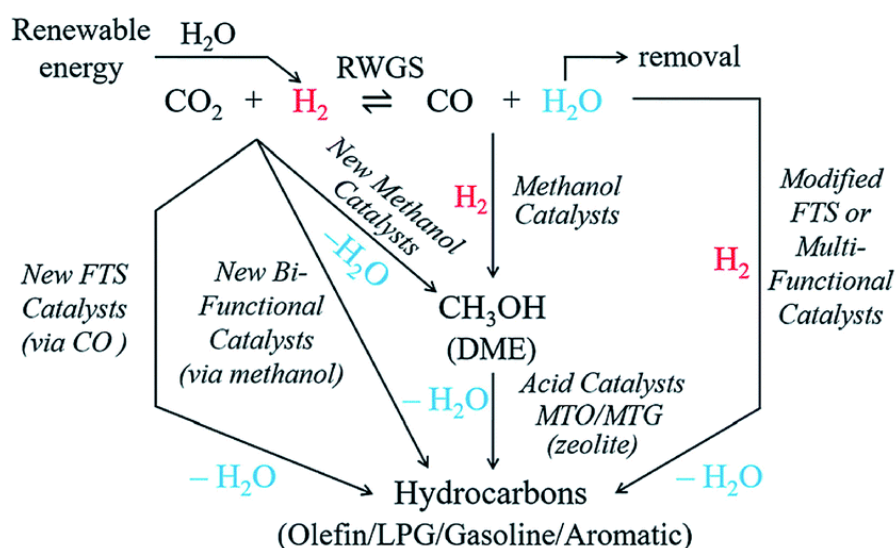
CH<sub>3</sub>OH productivity from CO<sub>2</sub> can be enhanced by simultaneously dehydrating CH<sub>3</sub>OH to dimethyl ether (DME). The simultaneous dehydration is achieved by combining a CH<sub>3</sub>OH synthesis catalyst with a solid acid catalyst, which is known as a hybrid catalyst. Like CH<sub>3</sub>OH, DME synthesis from CO<sub>2</sub> is favoured at low temperatures and high pressure; DME synthesis from CO<sub>2</sub> is also advantageous compared to CH<sub>3</sub>OH because of higher DME equilibrium selectivity. Moreover, DME is non-toxic; non-carcinogenic; can be employed as fuel in diesel engines because of its higher cetane number and lower auto-ignition temperature compared to diesel fuel (55-60 compared to 40-50, and 235 °C compared to 250 °C, respectively); and can be easily liquified at low pressure, hence it can be used as a liquified petroleum gas (LPG) substitute.<sup>(3, 4)</sup>

For the CH<sub>3</sub>OH dehydration to dimethyl ether (DME), ZSM-5 zeolites are preferred as acid catalysts because ZSM-5 zeolites contain Lewis and Brønsted acid sites, exhibit high resistance to water, and have excellent chemical and thermal stability.<sup>(27)</sup> For instance, Aguayo *et al.* compared Cu-ZnO-Al<sub>2</sub>O<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and Cu-ZnO-Al<sub>2</sub>O<sub>3</sub>/NaZSM-5 hybrid catalysts for CH<sub>3</sub>OH synthesis from the hydrogenation of CO and CO<sub>2</sub>, and observed competitive adsorption between H<sub>2</sub>O and CH<sub>3</sub>OH for acid sites on γ-Al<sub>2</sub>O<sub>3</sub>, leading to lower CO/CO<sub>2</sub> conversion and DME selectivity compared to ZSM-5. Moreover, catalyst

deactivation after regeneration was observed for  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>-containing hybrid catalyst, whilst good regeneration was observed for Cu-ZnO-Al<sub>2</sub>O<sub>3</sub>/ZSM-5 hybrid catalysts;<sup>(5)</sup> Similar conclusions were reported by Naik *et al.*<sup>(6)</sup> Bonura and co-workers studied the effect of water in the CH<sub>3</sub>OH dehydration activity over ZSM-5 zeolites; at low temperatures a decrease in CH<sub>3</sub>OH conversion was observed due to competition of H<sub>2</sub>O with the acid sites and at higher temperatures deactivation is observed, with increasing zeolite acidity. No appreciable decrease in CH<sub>3</sub>OH dehydration was observed above 180 °C.<sup>(7)</sup>

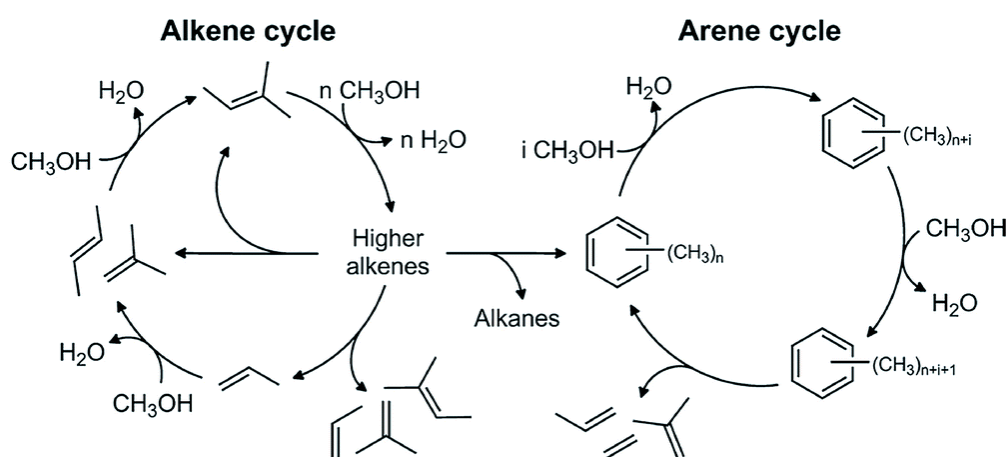
Frusteri *et al.* compared the activity of CuZnZr/ZSM-5 hybrid catalysts with CuZnZr supported over ZSM-5 by co-precipitation. Catalysts where the CH<sub>3</sub>OH synthesis catalyst is supported over the solid acid catalyst are known as integrated catalysts. Slightly higher CO<sub>2</sub> conversion and DME productivity was observed over the integrated catalyst, which was attributed to the spatial proximity between the two active functionalities. Other studies compare the hybrid and integrated catalyst configuration for the synthesis of DME from syngas,<sup>(8)</sup> but scarce literature comparing hybrid and integrated catalysts can be found for DME synthesis from CO<sub>2</sub>.

Typically, C<sub>2+</sub> products can be generated from CO<sub>2</sub> hydrogenation *via* two intermediate routes: CO intermediate route and CH<sub>3</sub>OH intermediate route (Figure 5.1a). In the CO intermediate route, CO<sub>2</sub> is first transformed into CO *via* the reverse water–gas shift (RWGS) reaction. As a result, the more reactive CO is subsequently hydrogenated to hydrocarbons (or oxygenates). For the latter route, the CH<sub>3</sub>OH intermediate can be obtained using a catalyst for methanol synthesis, which is further converted to hydrocarbons by methanol-to-hydrocarbon (MTH) catalysts.



**Figure 5.1a** – Schematic illustration of CO<sub>2</sub> hydrogenation to C<sub>2+</sub> products *via* the CO intermediate route and CH<sub>3</sub>OH intermediate route.<sup>(9)</sup>

Various mechanisms have been proposed for the formation of C<sub>2+</sub> products in the MTH processes, including the oxonium ylide mechanism, carbene mechanism, carbocationic mechanism, free radical mechanism and hydrocarbon pool mechanism. Among the mechanisms, the hydrocarbon pool mechanism in which aromatics and alkenes are important hydrocarbon pool compounds has been widely accepted. Larger hydrocarbons are formed after alkenes and aromatics are methylated with methanol (or dimethyl ether), and then crack or dealkylate to produce light alkenes and regenerate the starting compounds. The division between two classes of intermediates is usually referred to as the dual-cycle concept (Figure 5.1b). In such a mechanism, higher alkenes may be transformed into aromatics and alkanes through cyclisation and hydride transfer reactions, while light alkenes generated from aromatics may enter into the alkene cycle.



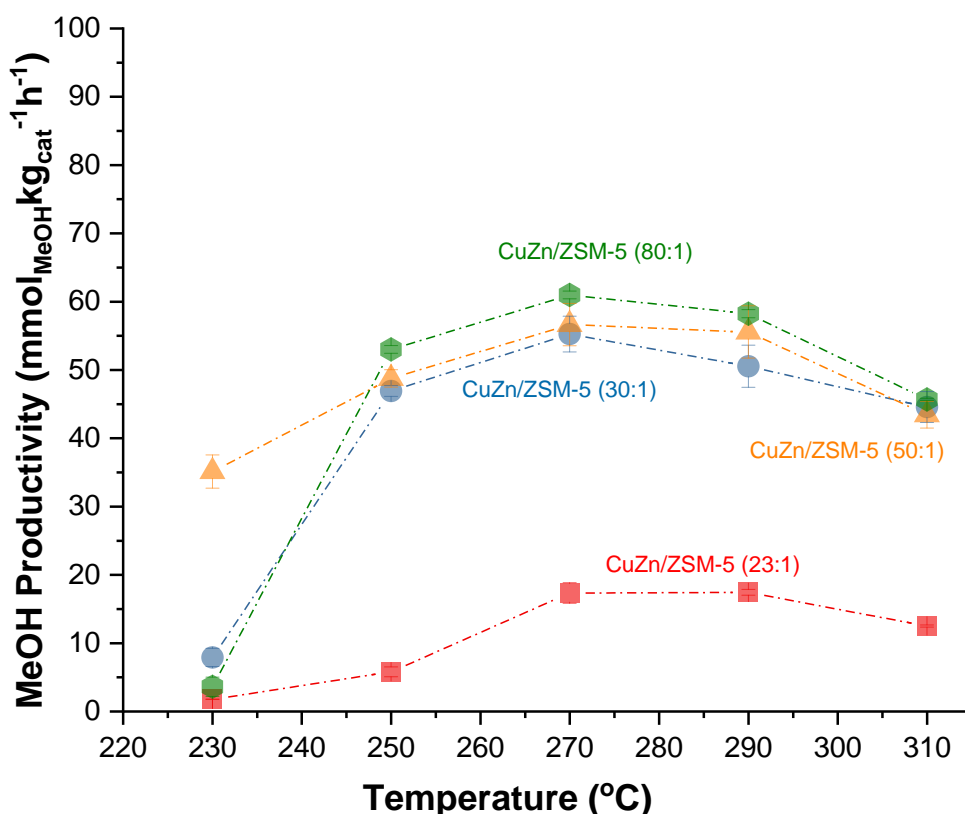
**Figure 5.1b** – Schematic illustration of the dual-cycle mechanism during the MTH process.<sup>(244)</sup>

The aim of this chapter is to compare MeOH, DME and higher chain hydrocarbon productivities between various CuZn- or CuZr-Zeolite integrated catalysts, where the zeolite is either commercially available H-ZSM-5 (Si:Al 23; 30; 50 and 80), mordenite (20:1) or zeolite Y, prepared *via* chemical vapour impregnation (CVI) and oxalate gel precipitation. Physical mixtures of the catalysts as well as changes to the catalyst bed are also explored in order to compare the catalyst activity. Cu-ZnO-based catalysts have been extensively studied for CO<sub>2</sub> hydrogenation to methanol,<sup>(11,12)</sup> variations of these catalysts by the addition of promoters/carrier oxides such as ZrO<sub>2</sub> and the combination of zeolites have allowed for the direct hydrogenation of CO<sub>2</sub> to methanol;<sup>(96)</sup> by starting with the Cu-ZnO based catalysts we can compare the existing data available in literature to gain a better understanding of the role of each of the catalyst components before introducing additional oxides to the catalyst.

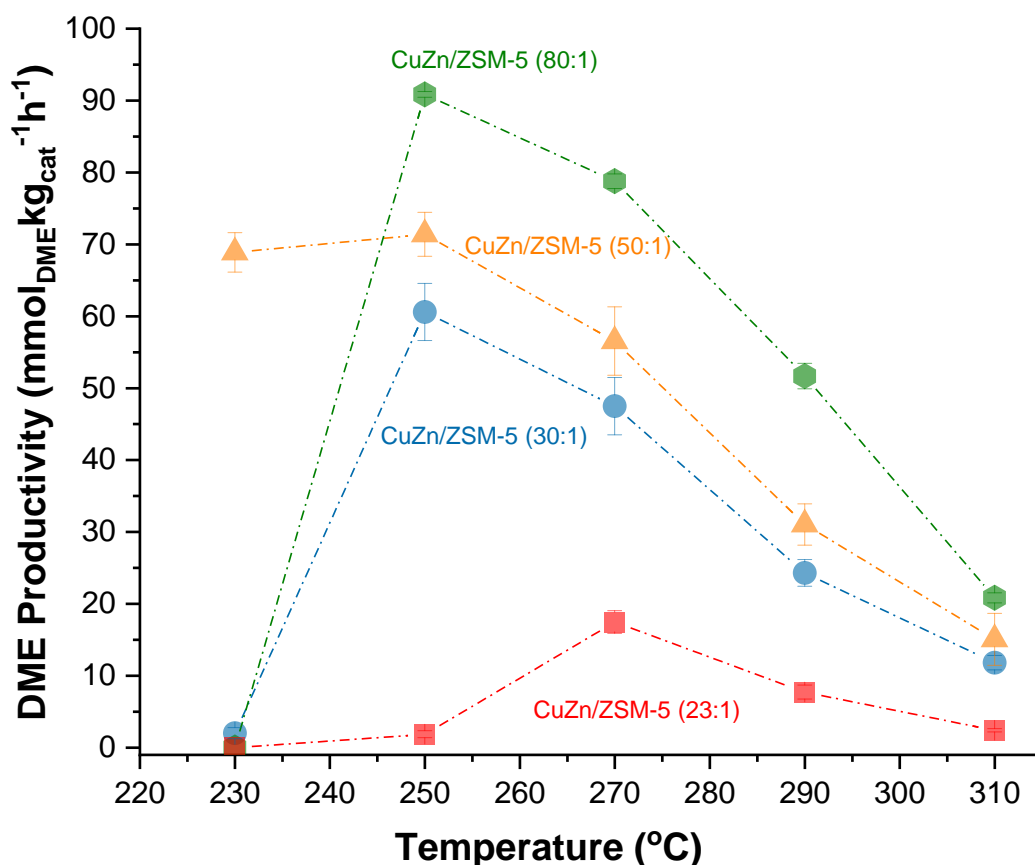
## 5.2 – Results and Discussion

### 5.2.1 – Cu/Zn Zeolite Catalysts Prepared by Chemical Vapour Impregnation (CVI)

A series of 20 wt.% CuZn (1:1) catalysts were prepared via Chemical Vapour Impregnation (CVI) on commercial ZSM-5 zeolites (Si:Al 23; 30; 50 and 80), the zeolites in their (NH<sub>4</sub><sup>+</sup>) form were activated to H-ZSM-5 via calcination (static air, 550 °C, 5 °C min<sup>-1</sup>, 4 h). Additional zeolites used include mordenite (20:1) and zeolite Y, these were investigated to determine if the variations in zeolite structures, particularly with pore sizes and acidity, had an impact on the methanol and DME productivities and hydrocarbon distributions. These catalysts were tested over a temperature range of 230 – 310°C; the higher temperatures for Cu/ZrO<sub>2</sub> were necessary for the production of any higher chain hydrocarbons. Hydrocarbons were identified after calibrating with an Agilent gas mixture and analysed via GC (Agilent 7890) fitted with an FID and TCD detectors; products eluted through a Agilent PoraPLOT Q-HTcolumn. The results are shown in Figures 5.2 and 5.3.



**Figure 5.2** – Methanol productivity of CuZn/ZSM-5 catalyst series with Si:Al range (23, 30, 50 and 80) prepared via CVI, reduced *in-situ*: 1 h at 220 °C in H<sub>2</sub> (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions:** 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.



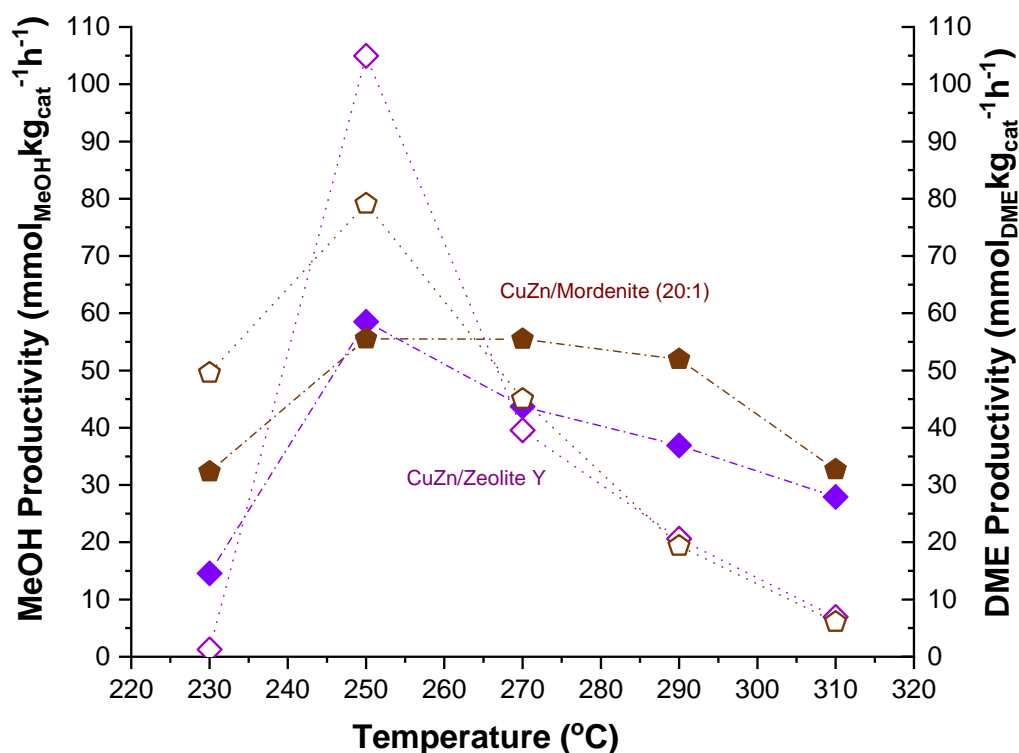
**Figure 5.3** – DME productivity of CuZn/ZSM-5 catalyst series with Si:Al range (23, 30, 50 and 80) prepared via CVI, **reduced in-situ**: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions**: 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

A clear trend can be observed where a higher Si:Al ratio results in an increase in both methanol and DME productivity across the temperature range studied. From 250°C upwards a 4x increase in methanol productivity is observed, with the exception of CuZn/ZSM-5 (50:1) with a methanol productivity of 35 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 230°C. Beyond 250°C, a drop in methanol productivity is observed; however, the catalysts, apart from CuZn/ZSM-5 (23:1), all fall within the same range. The maximum methanol productivity for the CuZn/ZSM-5 CVI series is 61 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 270°C for (80:1).

The differences in catalyst performance are more apparent in the DME productivities; the greatest DME productivity is 91 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 250°C for CuZn/ZSM-5 (80:1). The major difference between the catalysts in the series is the CuZn/ZSM-5 (23:1) catalyst; although the same trend of an initial increase in productivity and then decrease with increased temperature is seen, the values are much lower than other systems, giving MeOH and DME productivities of 17 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> and 18 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>, respectively. The change is attributed to the increased acidity of the catalyst, resulting in the formation

of other hydrocarbon products with increased temperature; additional products formed include: ethane and propane.

In addition to the ZSM-5 series of catalysts, CuZn catalysts on mordenite (20:1) and zeolite Y were also prepared via the CVI method and tested for methanol and DME productivity under the same conditions above. The results are given in Figure 5.4.



**Figure 5.4** – MeOH (filled symbols) and DME productivity (open symbols) of CuZn/mordenite (20:1) and CuZn/Zeolite Y prepared via CVI, **reduced *in-situ***: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions**: 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

From the results shown, both catalysts follow a similar trend as for the ZSM-5 series with regards to the MeOH productivity; an increase in productivity is observed up to 250°C before decreasing with increased temperature. The decrease in productivity is more rapid for the zeolite Y catalyst compared to the mordenite catalyst. The highest methanol productivity of 59 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> is achieved for the CuZn/zeolite Y catalyst, which is a slightly higher from the most active ZSM-5 catalyst (80:1), observed at 250°C. For the DME productivities, a substantial increase occurs at 250°C, with the CuZn/Zeolite Y achieving the highest DME productivity of 105 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> compared to 79 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> for mordenite. Again, comparing against the most active of the ZSM-5 series (80:1), there is a small increase. Increasing the temperature further results in a large drop in DME productivity

at a much faster rate than the ZSM-5 catalysts, with the exception of CuZn/ZSM-5 (23:1) which performs consistently poorly.

**Table 5.1:** Conversion and selectivity data for CuZn/Zeolite catalysts at 250°C

Catalyst	Temperature (°C)	X CO <sub>2</sub> (%)	S MeOH (%)	S DME (%)	S CO (%)
CuZn/ZSM-5 (23:1)	250	3.3	0.8	0.5	98.7
CuZn/ZSM-5 (30:1)	250	3.2	5.8	14.9	79.3
CuZn/ZSM-5 (50:1)	250	2.8	6.0	17.6	76.4
CuZn/ZSM-5 (80:1)	250	3.4	6.4	22.1	71.0
CuZn/Zeolite Y	250	1.4	10.1	36.0	53.9
CuZn/Mordenite (20:1)	250	2.7	6.4	18.2	75.4

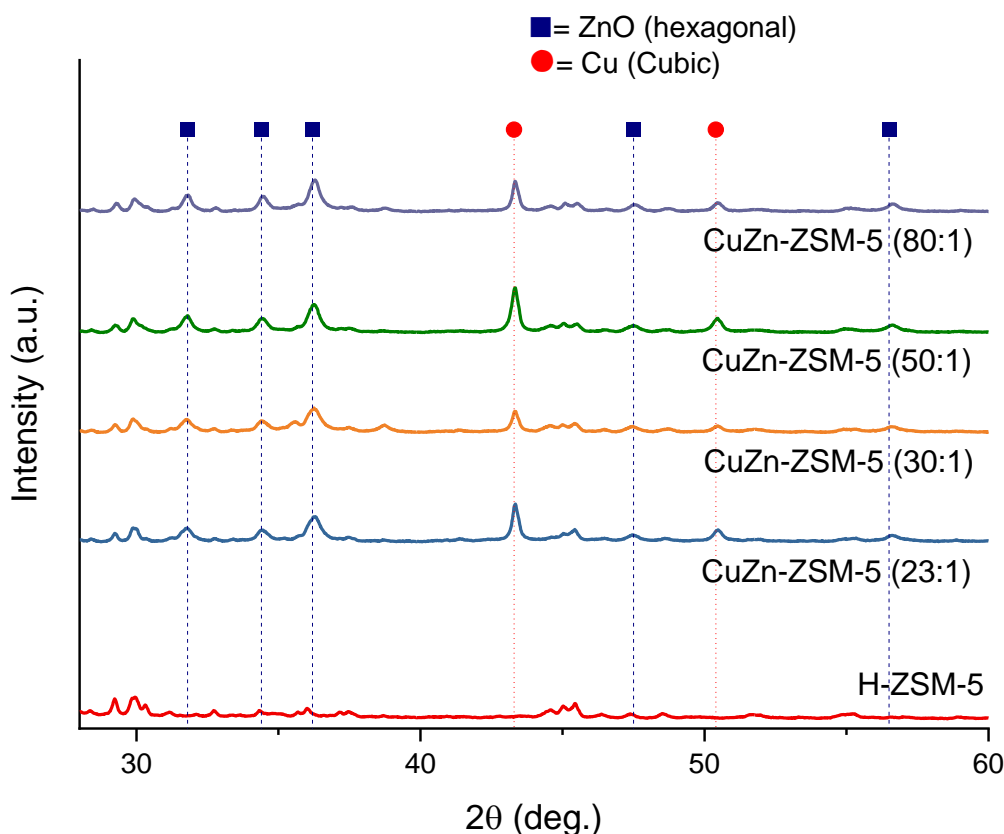
Comparing the data in Table 5.1 the ZSM-5 catalysts show an increase in selectivity towards MeOH and DME at 250°C as the Si:Al ratio increases, and a low CO<sub>2</sub> conversion of 3%. As explained previously, the selectivity data for CuZn/ZSM-5 (23:1) is lower than the other catalysts in the series due to the formation of additional hydrocarbons.

Although the additional zeolite catalysts achieve lower CO<sub>2</sub> conversions, the selectivities for CuZn/Zeolite Y are far greater than ZSM-5, with a MeOH selectivity of 10% and DME selectivity of 36% when compared with the ZSM-5 series; the CuZn/mordenite catalyst also performs similar to the most active of the ZSM-5 series (80:1). As the reaction proceeds, a decrease in selectivity is observed in all the catalysts as the temperature increases.

In order to understand the activity of the catalysts described here, characterisation using XRD and surface area analysis was conducted. The results are shown in Figure 5.5 and Table 5.2. From the XRD patterns, there are two distinct peaks at  $2\theta = 43.3^\circ$  and  $50.4^\circ$  assigned to metallic Cu (cubic) and correspond to the (111) and (200) planes respectively (PDF ref. 01-071-4609). Additional peaks observed at 31.8, 34.4, 36.2, 47.5 and 56.5° are associated with ZnO (hexagonal) and these correspond to the (100), (002), (101), (102) and (110) planes respectively (PDF ref. 01-074-9940). The sharpness and high intensity of the Cu peaks with an increase in Si:Al suggest larger particle sizes, as shown in Table 5.2 where the particle size was calculated using the Scherrer equation at  $2\theta = 43.3^\circ$ . The overall



surface areas and pore sizes are fairly similar amongst the ZSM-5 series, these were determined from the N<sub>2</sub> adsorption isotherms (- 196°C), and the Cu particle sizes are all large, particularly for the more active catalyst, suggesting additional factors, in addition to the Si:Al ratio, are influencing the activity of the catalysts.



**Figure 5.5** – XRD Patterns for reduced CuZn/ZSM-5 CVI series. Cu (○) and ZnO (□) regions have been highlighted.

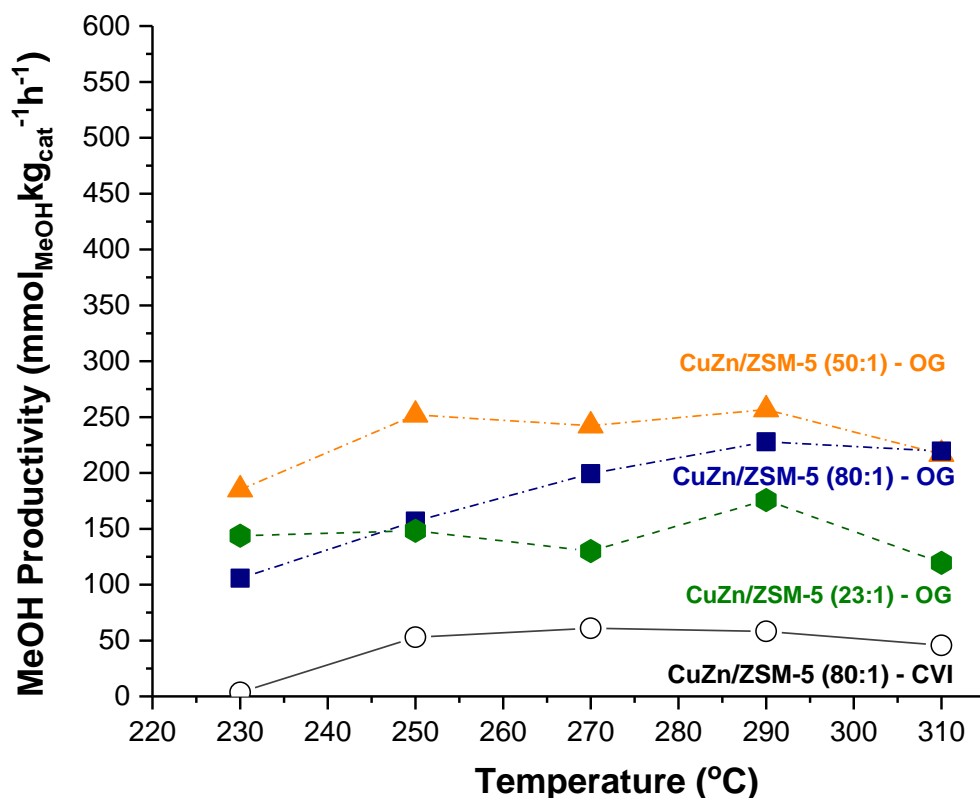
**Table 5.2:** Physiochemical properties of CuZn/zeolite CVI catalysts.

Catalyst	Cu Particle Size (nm)*	BET Surface area (m <sup>2</sup> /g)	Pore Width (Å)
CuZn/ZSM-5 (23:1)	51	258	4.8
CuZn/ZSM-5 (30:1)	71	279	4.9
CuZn/ZSM-5 (50:1)	54	273	4.9
CuZn/ZSM-5 (80:1)	76	297	4.8
CuZn/Mordenite	50	326	5.2 and 4.4
CuZn/Zeolite Y	55	467	5.0, 6.4 and 8.2

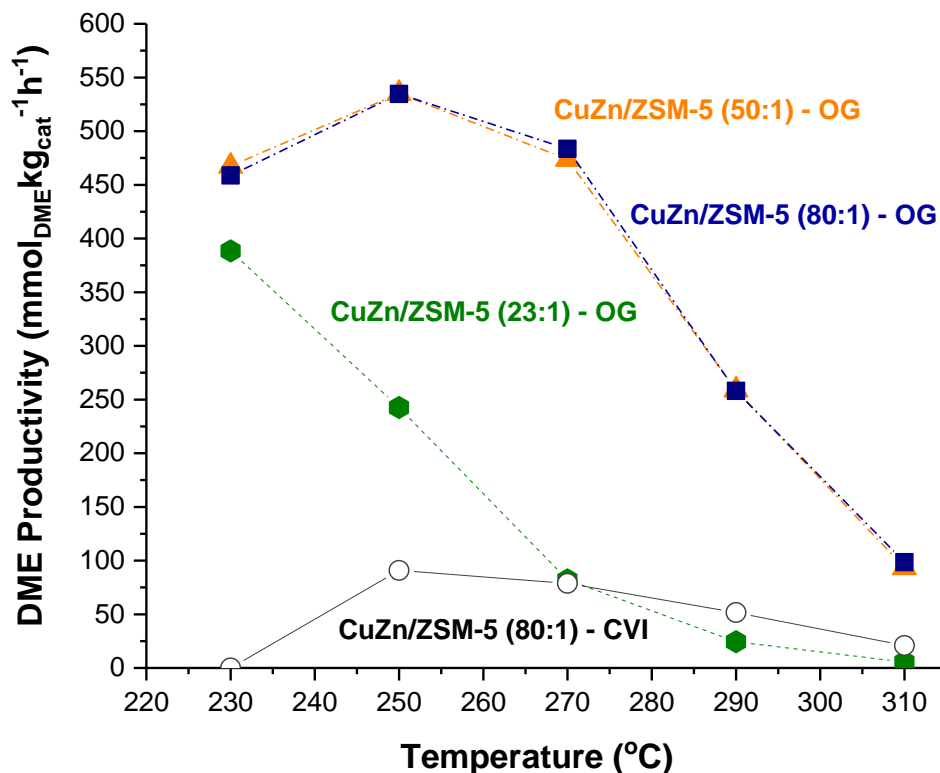
\*Calculated via Scherrer Equation for Cu (111) at 43.3°

### 5.2.2 – Cu/Zn and Cu/Zr Zeolite Catalysts Prepared by Oxalate Gel Precipitation

As established in Section 5.2.1, the preparation of CuZn/Zeolite catalysts via the chemical vapour impregnation method results in the formation of large Cu particles along the surface of the zeolite catalyst, rendering them relatively inactive. In order to improve, an alternative methodology must be adopted to reduce the particle size. Here, the oxalate gel method described in Section 2.2.3 is used as this is an effective and reproducible catalyst preparation technique in producing Cu/ZrO<sub>2</sub> catalysts with Cu particles around 11 nm. A series of 20 wt.% CuZn (1:1) catalysts were prepared on commercial ZSM-5 zeolites (Si:Al 23; 50 and 80) and on mordenite (20:1) and zeolite Y. These catalysts were tested for MeOH, DME and additional hydrocarbon synthesis over a temperature range of 230 – 310°C. The results for the ZSM-5 zeolites are shown in Figures 5.6 and 5.7, the Figures are scaled for ease of comparison.



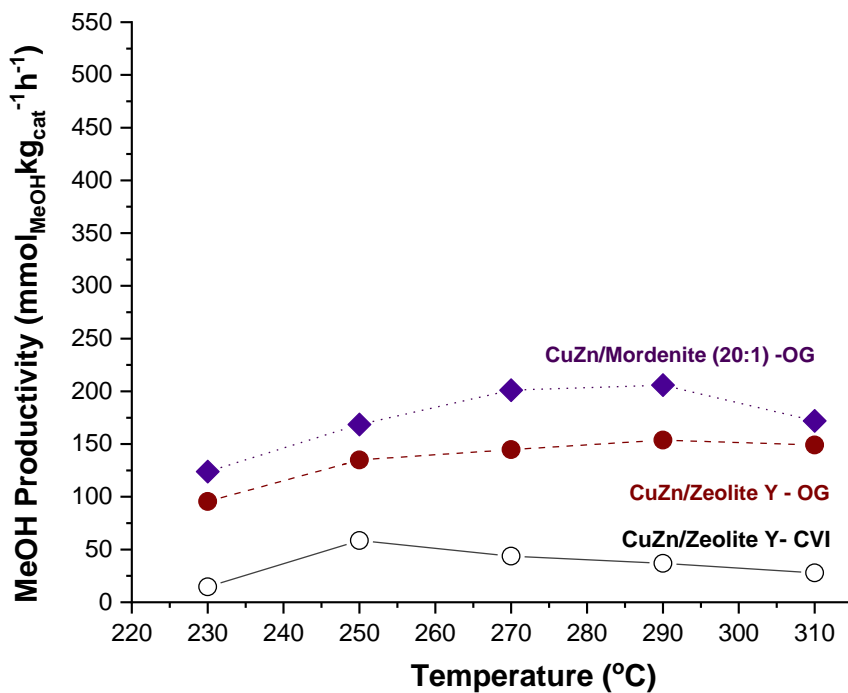
**Figure 5.6** – Methanol productivity of CuZn/ZSM-5 catalyst series with Si:Al range (23, 30, 50 and 80) prepared via oxalate gel, reduced *in-situ*: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). CuZn/ZSM-5 (80:1)-CVI is also plotted for comparison. **Reaction conditions:** 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.



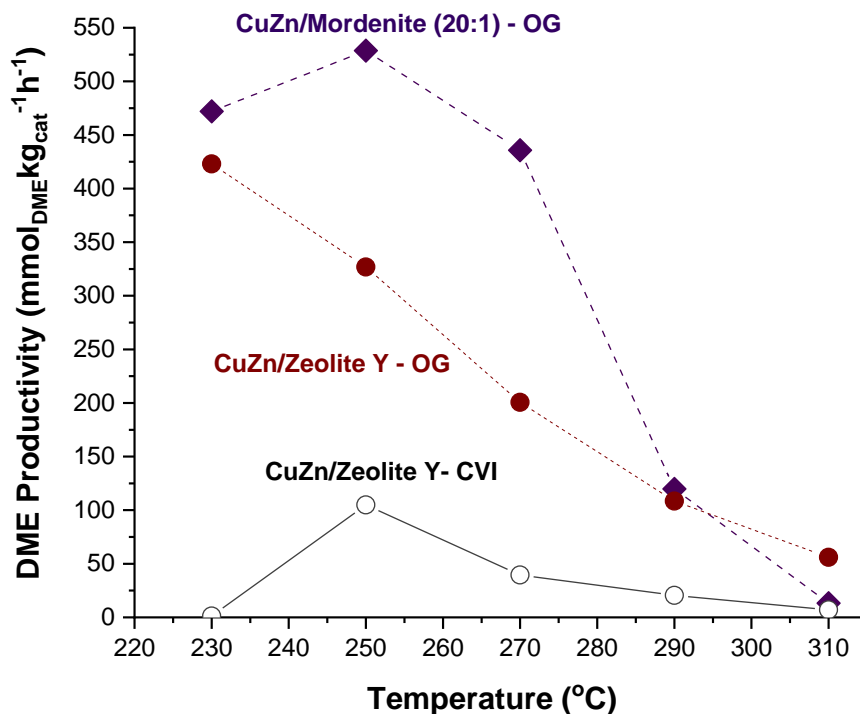
**Figure 5.7** – DME productivity of CuZn/ZSM-5 catalyst series with Si:Al range (23, 30, 50 and 80) prepared via oxalate gel, **reduced in-situ**: 1 h at 220 °C in H<sub>2</sub> (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). CuZn/ZSM-5 (80:1)-CVI is also plotted for comparison. **Reaction conditions**: 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

Comparing the results of the CuZn/ZSM-5 oxalate gel (OG) series against the most active of the CuZn/ZSM-5 CVI series (80:1), the catalysts produced via the oxalate gel method show almost 5x higher methanol and DME productivity, achieving a methanol productivity of 242 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> (against 61 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>) at 270°C and DME productivity of 535 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> (against 71 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>) at 250°C, respectively. Comparing the productivity profiles of the oxalate gel series against the CVI series, after a small drop in the methanol productivity at 270°C there is an increase at 290°C, for both CuZn/ZSM-5 (23:1) and (50:1), which is likely due to competing reactions as you approach equilibrium, and a continuous increase in methanol productivity with increased temperature for CuZn/ZSM-5 (80:1). These fluctuations are not observed in the CVI catalyst series.

The MeOH and DME productivities, unlike the CVI series, for the 50:1 and 80:1 catalysts are fairly similar; substantial differences are observed for the 23:1 catalyst, as reflected previously in the CVI series. Again, this is due to the formation of additional hydrocarbons (analysed using a GC where additional hydrocarbons were identified using an Agilent gas mix) as the reaction temperature increases, whereby the increase in acidity of the ZSM-5 support aids in the formation of longer chain hydrocarbons. Hydrocarbon products formed include ethane, propane, butane and Cis/trans-2-butene and 1-pentene.



**Figure 5.8** – MeOH productivity of CuZn/mordenite (20:1) and CuZn/Zeolite Y prepared via oxalate gel, *reduced in-situ*: 1 h at 220 °C in H<sub>2</sub> (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). CuZn/Zeolite Y-CVI is also plotted for comparison. **Reaction conditions:** 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.



**Figure 5.9** – DME productivity of CuZn/mordenite (20:1) and CuZn/Zeolite Y prepared via oxalate gel, *reduced in-situ*: 1 h at 220 °C in H<sub>2</sub> (2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). CuZn/Zeolite Y-CVI is also plotted for comparison. **Reaction conditions:** 230 - 310 °C, 6 h dwells (total = 30 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

In addition to the ZSM-5 series of catalysts, CuZn catalysts on mordenite (20:1) and zeolite Y were also prepared via the oxalate gel method and tested for methanol and DME productivity under the same conditions. The results are shown above in Figures 5.8 and 5.9.

Comparing the methanol productivity profiles of the CuZn/mordenite (20:1) and zeolite Y catalysts prepared by oxalate gel and CVI, the catalysts prepared via the oxalate gel method are almost 3x more active; the highest methanol productivity of 206 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> is achieved by CuZn/mordenite (20:1) at 290°C. The productivity falls slightly short of the CuZn/ZSM-5 (50:1) catalyst at the same temperature, with 257 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>. The oxalate gel catalysts show a more steady decline in methanol productivity in comparison to the CVI catalyst, as the temperature increases as was also seen for the CuZn/ZSM-5-OG series, suggesting the oxalate gel catalysts are less unstable.

Looking at the DME productivity data, a slightly different trend is seen; the CuZn/Zeolite Y catalyst starts with a DME productivity of 423 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 230°C, but this falls as the temperature is increased, which is the opposite to the equivalent CVI catalyst, which follows a similar trend to the mordenite catalyst. The result may be linked to a change in the zeolite or CuZn particles as the reaction proceeds. The CuZn/mordenite (20:1) catalyst achieves the highest DME productivity of 528 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 250°C, which is 5x higher than the CuZn/Zeolite Y catalyst prepared by CVI.

The results described above are in contrast to the CVI data shown in Figure 5.4, where the zeolite Y catalyst was more active. Comparing the methanol and DME productivities of the CuZn/mordenite (20:1) catalyst prepared by oxalate gel with the ZSM-5 series of catalysts prepared by the same method, it can be said that the mordenite catalyst performs very similarly to the CuZn/ZSM-5 (80:1) catalyst. The results suggest that changes in the catalyst are introduced when depositing the Cu and Zn onto the zeolites using the different preparation methods.

When comparing the CuZn/ZSM-5 series prepared by the oxalate gel method, the CuZn/ZSM-5 (50:1) is the most active catalyst, this is also true when compared to the mordenite and zeolite Y catalysts prepared by oxalate gel, and this may be linked to the individual structures of the zeolites used in the reaction.

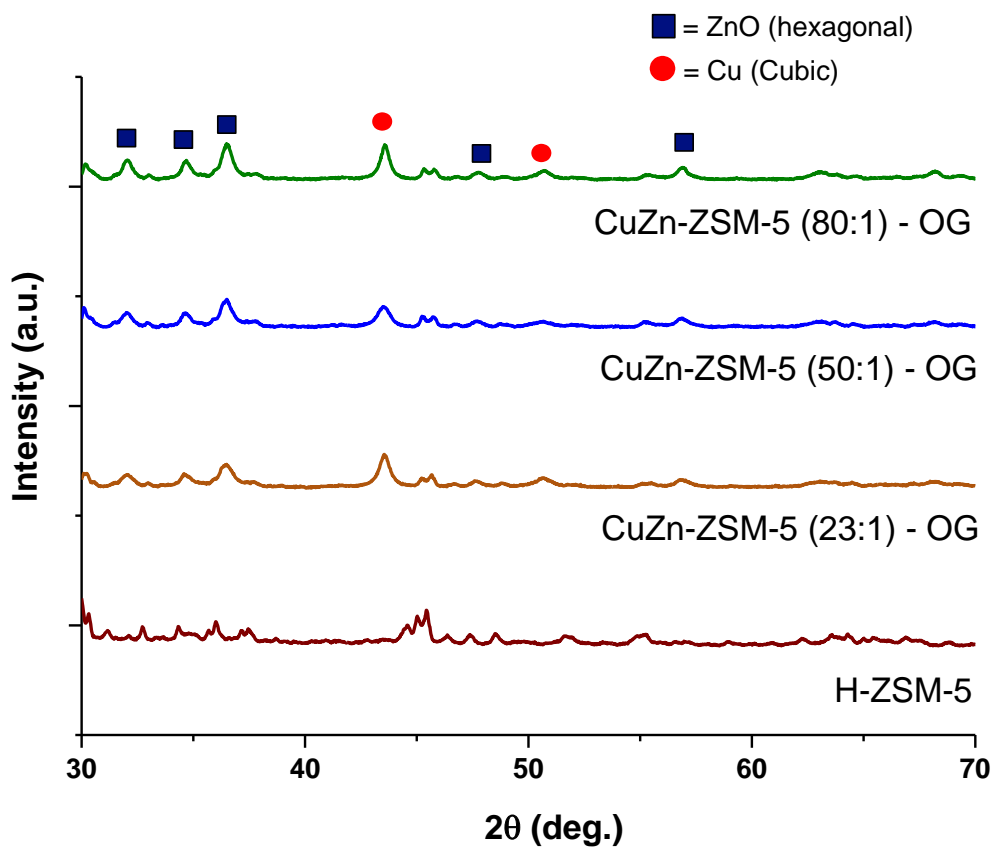


Figure 5.10 – XRD Patterns for reduced CuZn/ZSM-5 oxalate gel series. Cu (●) and ZnO (■) regions have been highlighted.

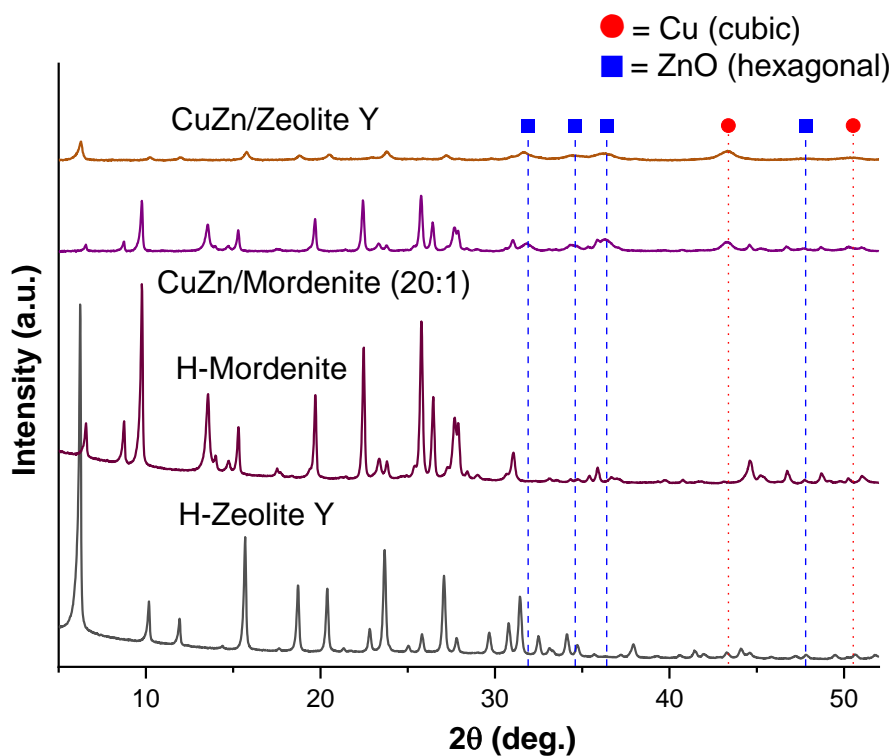


Figure 5.11 – XRD Patterns for reduced CuZn/Zeolite Y and mordenite (20:1) oxalate gel catalysts. Cu (●) and ZnO (■) regions have been highlighted.

**Table 5.3:** Physiochemical properties of CuZn/zeolite oxalate gel catalysts.

Catalyst	Cu Particle Size (nm) reduced and post- reaction*	BET Surface area (m <sup>2</sup> /g)	Pore Width (Å)
CuZn/ZSM-5 (23:1)	13 (23)	277	4.9
CuZn/ZSM-5 (50:1)	13 (14)	211	5.0
CuZn/ZSM-5 (80:1)	15 (20)	303	5.0
CuZn/Mordenite	9 (11)	253	4.0 & 5.1
CuZn/Zeolite Y	14 (17)	336	5.0, 6.4 & 7.9

\*Calculated via Scherrer Equation for Cu (111) at 43.3°, post-reaction particle size highlighted in red.

The catalysts were characterised using XRD and the Scherrer equation used to determine the Cu particle size before and after reaction using the Cu (111) at  $2\theta = 43.3^\circ$ , BET surface area measurements were made to monitor the changes from the fresh support to the support after the addition of Cu and Zn. The results are shown above in Figures 5.10 and 5.11, and Table 5.3. Comparing the XRD patterns for the oxalate gel series to those prepared via CVI in Figure 5.4, the distinct peaks at  $2\theta = 43.3^\circ$  and  $50.4^\circ$  assigned to metallic Cu (cubic) and corresponding to the (111) and (200) planes respectively (PDF ref. 01-071-4609) appear less intense and more broad; upon further analysis the particle sizes are reduced by up to 5x, and even after reaction there is a very small increase in particle size, which is unexpected due to the higher temperatures used during the reaction. Additional peaks observed at  $31.8^\circ$ ,  $34.4^\circ$ ,  $36.2^\circ$ ,  $47.5^\circ$  and  $56.5^\circ$  associated with ZnO (hexagonal) remain the same in both sets of catalysts, and these correspond to the (100), (002), (101), (102) and (110) planes respectively. (PDF ref. 01-074-9940).

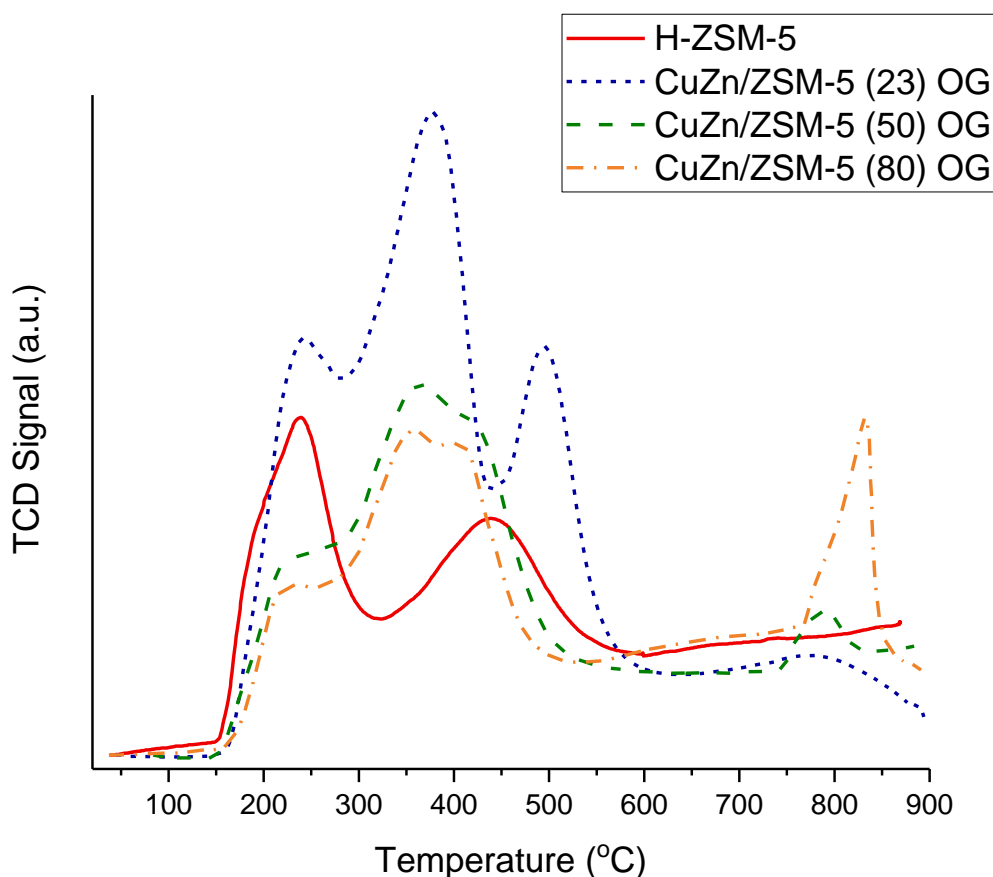
The peaks expected for metallic Cu and ZnO are also observed for the CuZn/zeolite Y and mordenite (20:1) catalysts; here, the metallic Cu peaks are less intense and broader, suggesting even smaller Cu particles, particularly for the mordenite (Table 5.3.) Interestingly only a small growth in Cu particle size is observed across all the catalysts post reaction.

Comparing the pore widths, the sizes remain the same, around 5 Å for the ZSM-5 catalysts, and for the mordenite and zeolite Y catalysts it differs slightly; although they are both large pore zeolites, zeolite Y displays a larger pore diameter of 7.9 for its main channel compared to 5.1 Å recorded for mordenite, the other pore sizes however, are of similar size suggesting the method of Cu and Zn deposition used

does not greatly impact the internal structure of the zeolites. However, the surface areas do change according to the type of preparation method used, with a decrease in the surface area observed for the oxalate gel series, which suggests that there are more Cu and Zn particles incorporated onto the zeolite and available for reaction.

Combining the information above it can be said that the choice of preparation method used to deposit the Cu and Zn onto the zeolite greatly influences the size of the resulting particles; here, the oxalate gel method is shown to produce smaller particles compared to CVI. In addition, the selection of zeolite, with regards to the Si:Al ratio, also impacts the activity, with a less acidic support (higher Si:Al) resulting in a more selective catalyst towards DME and MeOH.





**Figure 5.12**– NH<sub>3</sub>-TPD Patterns for CuZn/ZSM-5 series prepared via oxalate gel.

NH<sub>3</sub>-TPD measurements were taken for the CuZn/ZSM-5 catalysts prepared by the oxalate gel method and compared against the pure H-ZSM-5 zeolite in order to determine the acidity of the catalysts. From the figure, two major peaks are observed for H-ZSM-5: a lower temperature peak at 240°C, associated with the desorption of NH<sub>3</sub> from weak acid site (Lewis acid); and a higher temperature peak at 440°C, associated with the desorption of NH<sub>3</sub> from strong acid sites.<sup>(10)</sup> Additional peaks are also observed at lower temperatures between 355 and 410°C in the CuZn catalysts, and these are due to the formation of new medium-strength acid sites that arise from the Cu species interacting with the strong acid sites of the zeolite, making their acid strength weaker. As the Si:Al ratio increases, both the high and low temperature peaks shift to lower temperatures, indicating a decrease in the acid strength, this signifies the Al generates acidity; due to its valency, there is an overall negative charge (due to oxygen) on the zeolite which is balanced by a cation, for the ZSM-5 catalysts this charge is balanced by a proton to give a Brønsted acid.

To gain a deeper understanding of the acid sites on these catalysts, the acid sites were quantified via deconvolution of the peaks, by using individual peak areas of the NH<sub>3</sub>-TPD profiles and a reference

factor (10554) from NH<sub>3</sub> calibration on the Quantachrome ChemBET TPR/TPD, the μmol NH<sub>3</sub> could be calculated. Dividing the μmol NH<sub>3</sub> by the mass of each catalyst and dividing further to convert to mmol gave the final acidities for each catalyst in mmol/g. This information is shown in Table 5.4.

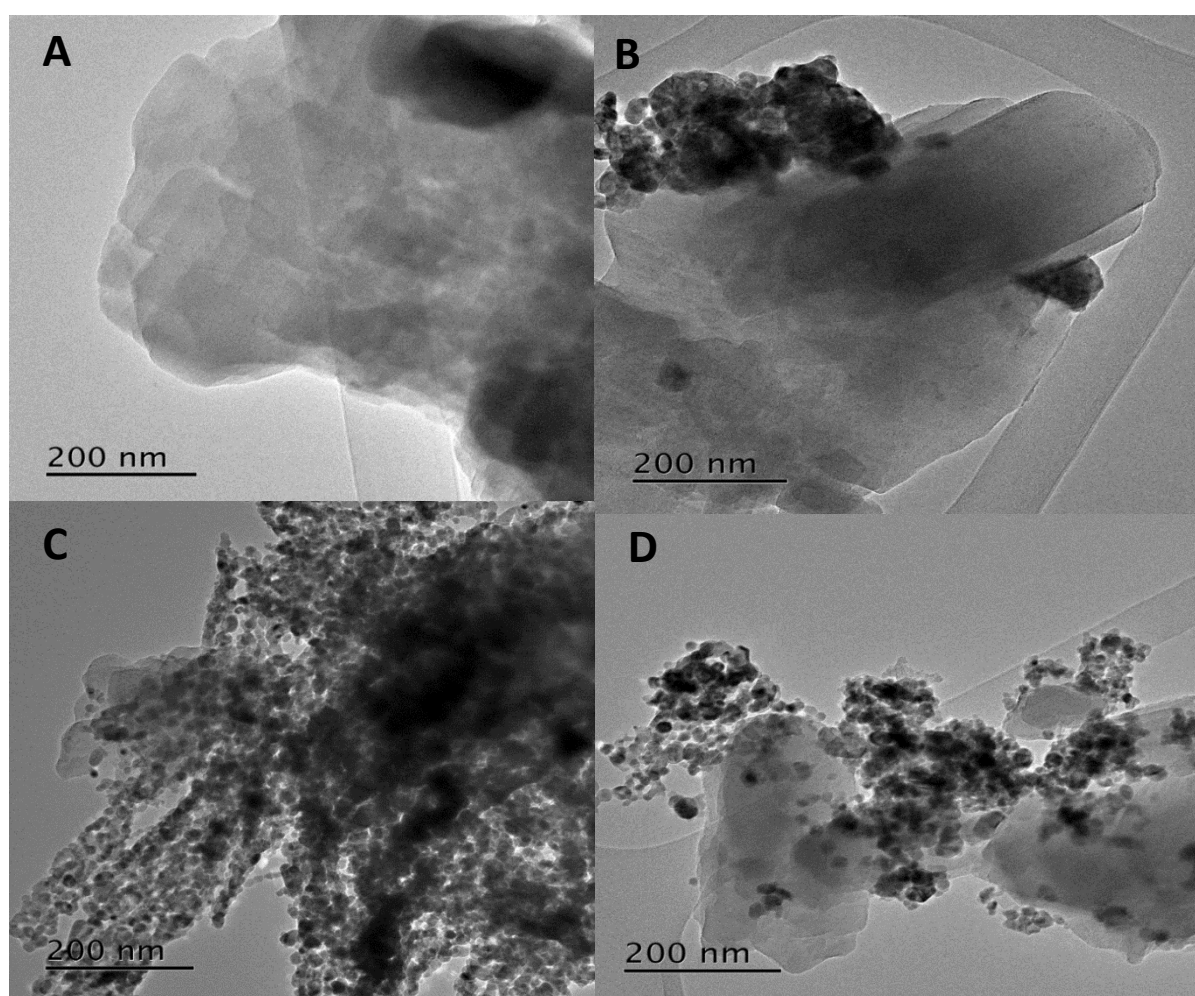
**Table 5.4:** Total number of acid sites for the CuZn/Zeolite catalysts prepared by oxalate gel.

Catalyst	Total Acid Sites (mmol/g)	Weak Acid Sites (mmol/g)	Medium Acid Sites (mmol/g)	Strong Acid Sites (mmol/g)
CuZn/ZSM-5 (23:1) - OG	0.04	0.01	0.02	0.01
CuZn/ZSM-5 (50:1) - OG	0.02	0.004	0.008	0.005
CuZn/ZSM-5 (80:1) - OG	0.01	0.002	0.007	0.005
CuZn/Zeolite Y - OG	0.05	0.02	0.02	0.005
CuZn/Mordenite (20:1) - OG	0.04	0.01	0.015	0.015

As reflected in the NH<sub>3</sub>-TPD profiles, an increase in the Si:Al ratio results in a decrease in the number of total acid sites available. CuZn/ZSM-5 (23) contains the highest amount of strong sites, compared to the other catalysts, as well as medium acid sites, suggesting these are essential towards the formation of higher hydrocarbons, likely through the stabilisation of key reaction intermediates over these sites, thus preventing them from further oxidation into CO and other undesired products. This can also relate back to the reactivity data shown in Figures 5.5 and 5.6, where the lower methanol and DME productivity can be correlated with a higher concentration of total acid sites, as well as the size of the particles. Comparing the zeolite Y and mordenite catalysts, it is clear that zeolite Y offers a greater number of acid sites but the mordenite catalyst contains more of the stronger acid sites, and this may be a factor towards the lower methanol and DME productivity observed in Figures 5.6 and 5.7.

Brønsted acid sites of zeolites act as catalytic sites for CH<sub>3</sub>OH conversion via HCP mechanisms. Sufficient Brønsted acid sites ensure successive and efficient reactions. However, an excess of Brønsted acid sites coupled with a high acid strength can cause deactivation by fast coke deposition. In addition, both aromatic and alkene-based mechanisms can occur simultaneously in ZSM-5 zeolites, with the density of the acid sites determining which mechanism is more dominant. Stronger Brønsted acid sites have been linked to the formation of aromatics.<sup>(13, 14)</sup> Recent work by Gao and co-workers have shown that using a bifunctional catalyst consisting of a zeolite (SAPO-34) and metal oxide (In<sub>2</sub>O<sub>3</sub>-ZnZrO<sub>x</sub>) are

effective for the direct hydrogenation of CO<sub>2</sub> to light olefins; the decreased quantity of Brønsted acid sites led to an increased selectivity in lower olefins, in addition, a reduced crystal size of the zeolite was shown to shorten the diffusion length from the surface to the acid sites inside the zeolite pores, thus favouring the mass transfer of intermediate species for efficient C–C coupling to generate lower olefins.<sup>(15)</sup> Work by Gascon et al. also supports this, interestingly they demonstrated that the incorporation of the alkaline earth metal Ca led to a higher selectivity of lighter olefins, this was attributed to a decrease in Brønsted acidity and formation of Lewis acidic sites. The decreased Brønsted acidity also inhibited the H-transfer reaction producing additional light olefins at the expense of longer chain hydrocarbons.<sup>(16)</sup>

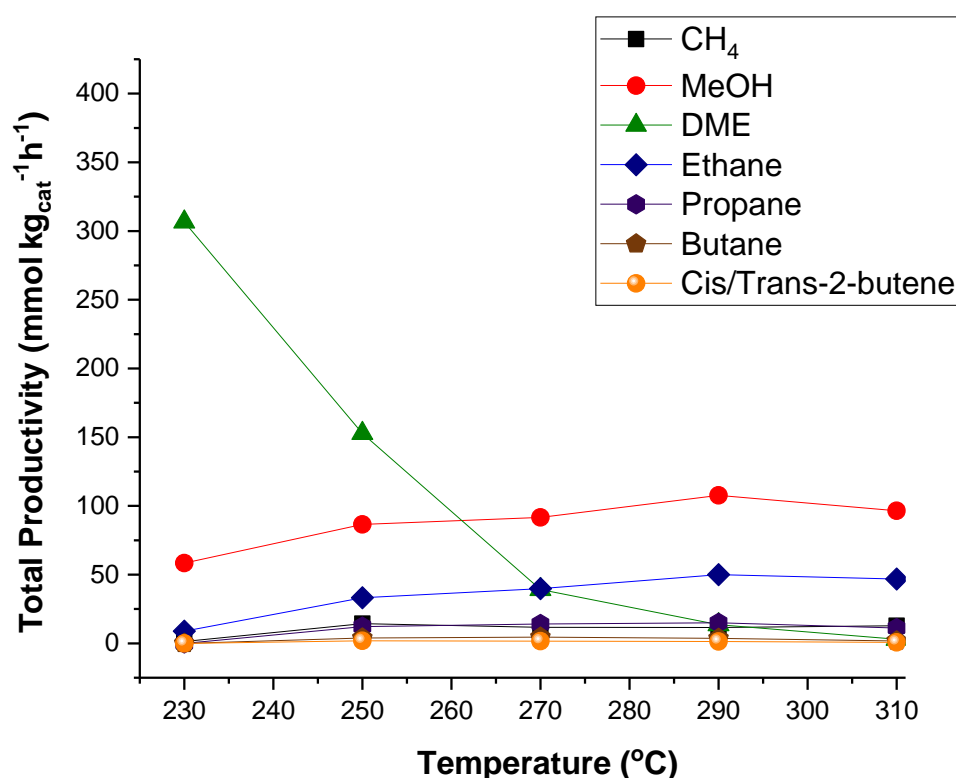


**Figure 5.13** – TEM images of CuZn/ZSM-5 (23:1) – CVI and oxalate gel catalysts. **A** = CuZn/ZSM-5 (23:1) CVI – Reduced **B** = CuZn/ZSM-5 (23:1) CVI after reaction **C** = CuZn/ZSM-5 (23:1) OG – Reduced **D** = CuZn/ZSM-5 (23) OG after reaction.

TEM images of the CuZn/ZSM-5 (23:1) catalysts prepared via CVI and oxalate gel were compared after reduction and post reaction (Figure 5.8). In image **A**, the surface is very smooth as CuZn is present as an epitaxial layer and when left under the beam the particle growth can be observed i.e. it is beam

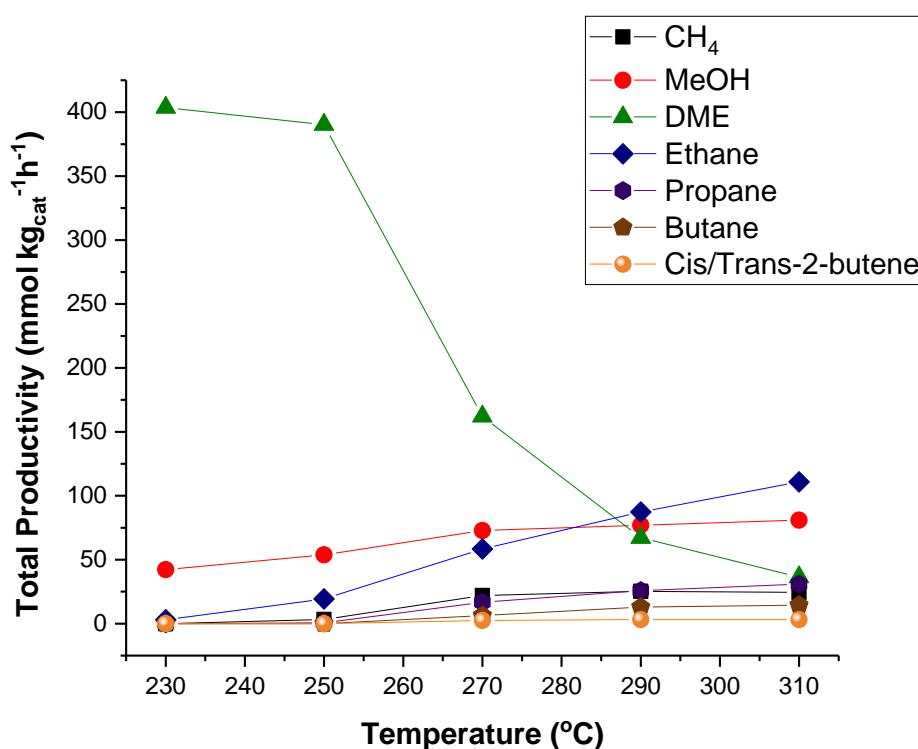
sensitive. After reaction (B), the particles begin to emerge on the surface as large agglomerates, and which is due to sintering during the reaction where the surface Cu is exposed to high temperatures. In contrast, the image for the CuZn/ZSM-5 catalyst prepared via oxalate gel after reduction (C) displays needles/strings of phase separated CuZn that are detached from the ZSM-5 support; after reaction (D), these are largely broken down and seen to accumulate as large clumps across various points on the ZSM-5 surface. Despite the lack of homogeneity and dispersion of the active metals on the surface of the zeolite, the oxalate gel catalyst still maintains its activity through the limited contact, suggesting the key intermediates formed have access to the channels of the zeolite necessary for the hydrocarbon formation. The large particles seen for the CVI catalyst, as supported by the XRD patterns, agglomerate to prevent access to the pores and result in poorly active nanoparticles.

As established in the previous experiments, the CuZn/ZSM-5 (23:1) catalyst was the most acidic of the ZSM-5 series, containing strong sites, and medium acid sites that are essential towards the formation of higher hydrocarbons. In an attempt to increase the hydrocarbon formation, the quantity of zeolite used during the preparation was doubled, whilst maintaining the loadings of Cu and Zn. The results are shown in Figure 5.14.



**Figure 5.14** – Total productivity of CuZn/ZSM-5 (23:1) prepared via oxalate gel with double mass of zeolite (1 g), reduced *in-situ*: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions:** 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

Looking at the data above, the productivity profiles for all the products follow a similar trend, with the exception of DME, which starts at 307 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> but drops significantly up to 270°C as the higher chain hydrocarbons start to form. Comparing with the previous CuZn/ZSM-5 (23:1) catalyst, the highest methanol productivity of 178 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> was achieved at 290°C and DME productivity of 388 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 230°C; in comparison, the methanol productivity for the catalyst with double the mass of zeolite was 108 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 290°C. Although a drop in productivity is observed for MeOH and DME, small amounts of additional products up to C<sub>4</sub> are produced, suggesting a greater concentration of the essential acid sites of the zeolite for hydrocarbon formation.



**Figure 5.15** – Total productivity of CuZr/ZSM-5 catalyst with Si:Al (23:1) prepared via oxalate gel, **reduced *in-situ***: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions:** 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

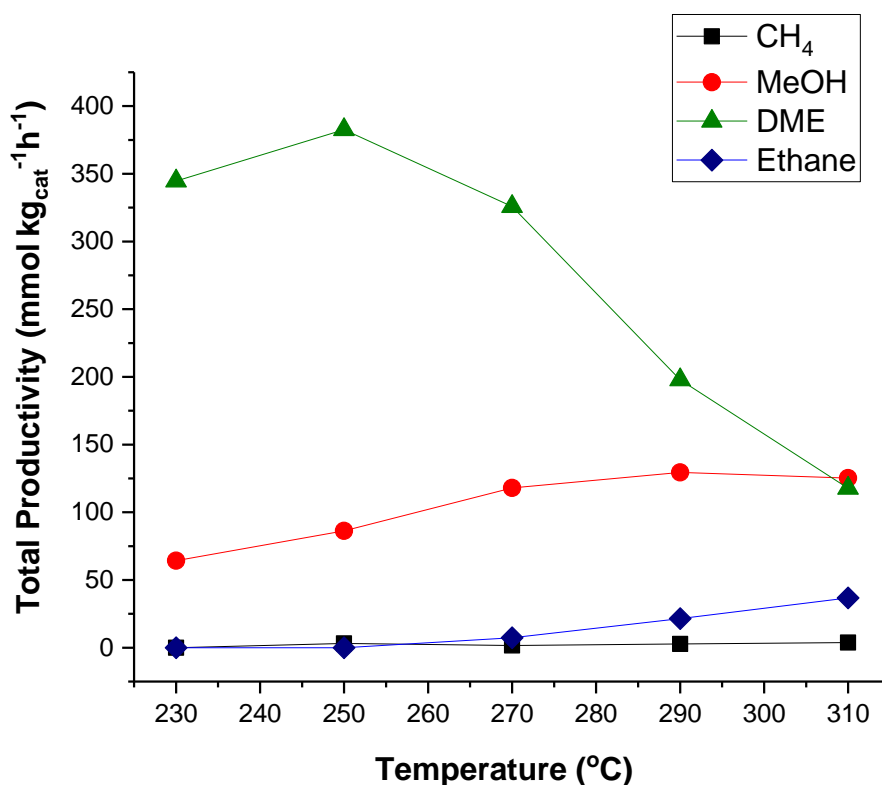
Although the combination of CuZn with a series of ZSM-5 zeolites was active towards the production of methanol, DME and higher hydrocarbons, a combination of several other copper-based catalysts could be used for the same reaction; indeed, in the previous chapters Cu/ZrO<sub>2</sub> prepared by the oxalate gel method is an active catalyst. Therefore, using the same method to prepare the CuZn/ZSM-5 (23:1) catalyst, an equivalent CuZr catalyst was made.

At the start of the reaction, results are shown in Figure 5.15, the DME productivity is at 408  $\text{mmol}_{\text{DME}}\text{kg}_{\text{cat}}^{-1}\text{h}^{-1}$ ; this then rapidly drops from 270°C as the additional hydrocarbons are formed. In comparison to the CuZn/ZSM-5 (23:1) catalyst, the DME productivity is much higher across the temperature range and the MeOH productivity is much lower, which shows that any methanol produced is quickly consumed to generate DME and this is then used in the formation of the higher hydrocarbons. From the data shown, the ethane productivity continuously increases from 250°C onwards and this is slowly followed by the generation of additional hydrocarbons up to C<sub>4</sub>.

Recent work by Gascon et al. investigated CO<sub>2</sub> hydrogenation to methanol and its conversion to hydrocarbons using ZrZnO<sub>x</sub> catalysts, prepared by co-precipitation, combined with H-ZSM-5 and H-SAPO-34 through mechanical mixing. The best performance was observed for the ZrZnO<sub>x</sub> sample with 30% Zn, combined with ZSM-5 at 350 °C, 30 bar and H<sub>2</sub>/CO<sub>2</sub>/N<sub>2</sub> = 6/2/1. Under these conditions, the equilibrium methanol yield was observed after 0.4 s g<sup>-1</sup> ml<sup>-1</sup> over ZrZnO<sub>x</sub> alone. Mixing with ZSM-5 in a 1:1 weight ratio, methanol was rapidly converted to hydrocarbons, with an optimum C<sub>3</sub> productivity of 1.5 mol kg<sup>-1</sup> h<sup>-1</sup> at 24 000 ml h<sup>-1</sup> g<sup>-1</sup>.<sup>(17)</sup> Wang and coworkers developed a bifunctional catalyst composed of ZnGa<sub>2</sub>O<sub>4</sub> and SAPO-34 which achieved 86% selectivity for C<sub>2</sub>–C<sub>4</sub> olefins at 13% conversion of CO<sub>2</sub> (370°C, H<sub>2</sub>/CO<sub>2</sub> = 3:1, 30 bar, 45 ml min<sup>-1</sup>). The oxygen vacancies on the surface of ZnGa<sub>2</sub>O<sub>4</sub> were responsible for CO<sub>2</sub> activation;<sup>(18)</sup> this is supported by Sun et al., where for the In<sub>2</sub>O<sub>3</sub>/H-ZSM-5 bifunctional catalyst, CO<sub>2</sub> was chemisorbed at the oxygen-vacancy sites on the surface of the reducible In<sub>2</sub>O<sub>3</sub> and hydrogenated to CH<sub>3</sub>OH through several intermediates. The CH<sub>3</sub>OH intermediate entered the HZSM-5 zeolite and was further converted to hydrocarbon products at the surface acidic sites of the zeolite via a hydrocarbon-pool mechanism. The proximity of the two components was important in suppressing the RWGS and to give a high selectivity for gasoline-range hydrocarbons.<sup>(19)</sup>

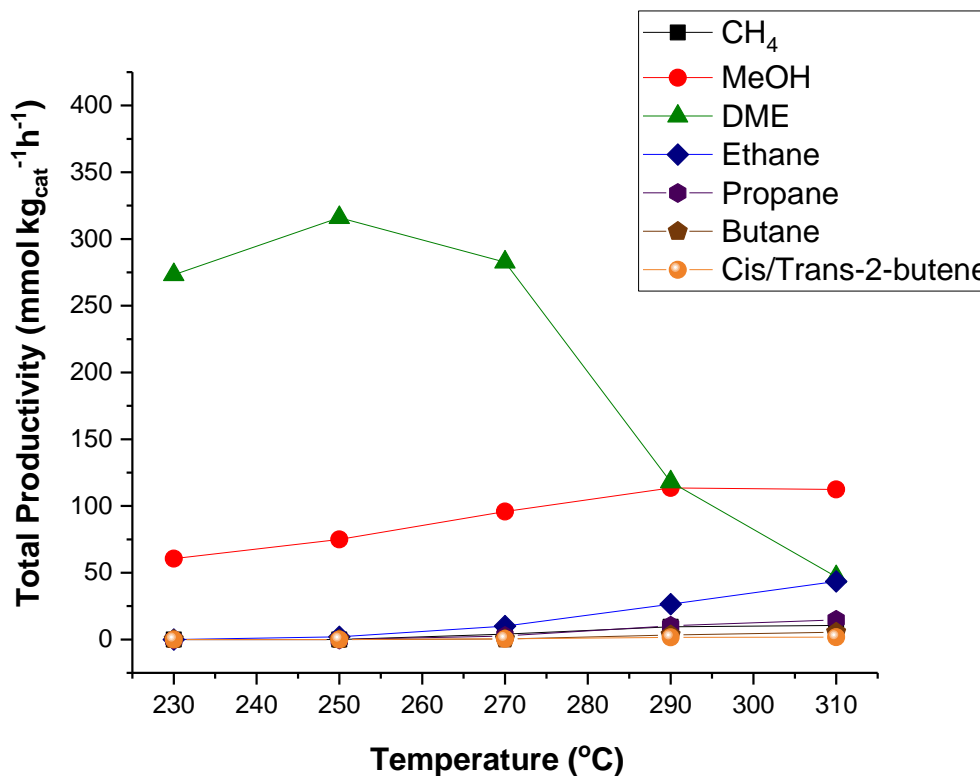
### 5.2.3 – Physically Mixed Catalysts

The preparation of 20 wt.% CuZn (1:1) catalysts on commercial ZSM-5 zeolites was successful previously by the oxalate gel method; however, from the TEM images not all of the Cu and Zn was homogeneously distributed across the zeolite surface. Instead, large phase segregated Cu and Zn detached from the surface; despite this, the catalysts still remained active and the more acidic CuZn/ZSM-5 (23:1) was able to produce high chain hydrocarbons. In order to examine the degree of contact between the active metals and zeolite support, a physical mixture of 10% Cu/ZnO, prepared by the oxalate gel method, and commercial H-ZSM-5 (23:1) was made. Two methods of physical mixture were employed: the first involved shaking the two catalyst components; and the second involved grinding the components together to give the final catalyst. The results for both catalysts are given below in Figures 5.16 and 5.17.



**Figure 5.16** – Total productivity of 10% Cu/ZnO + ZSM-5 (23:1) physically mixed catalyst (shaken), **reduced *in-situ***: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions**: 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.






**Figure 5.17** – Total productivity of 10% Cu/ZnO + ZSM-5 (23:1) physically mixed catalyst (254), *reduced in-situ*: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions:** 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

As expected, the DME productivity decreases after 250°C; the shaken catalyst achieved the highest DME productivity of 383 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 250°C, and the ground catalyst achieved a DME productivity of 316 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at the same temperature. The methanol productivity remains fairly level across the temperature range, starting below 65 mmol<sub>MeOH</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 230°C and ending at below 126 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> at 310°C, as there is very little hydrocarbon formation.

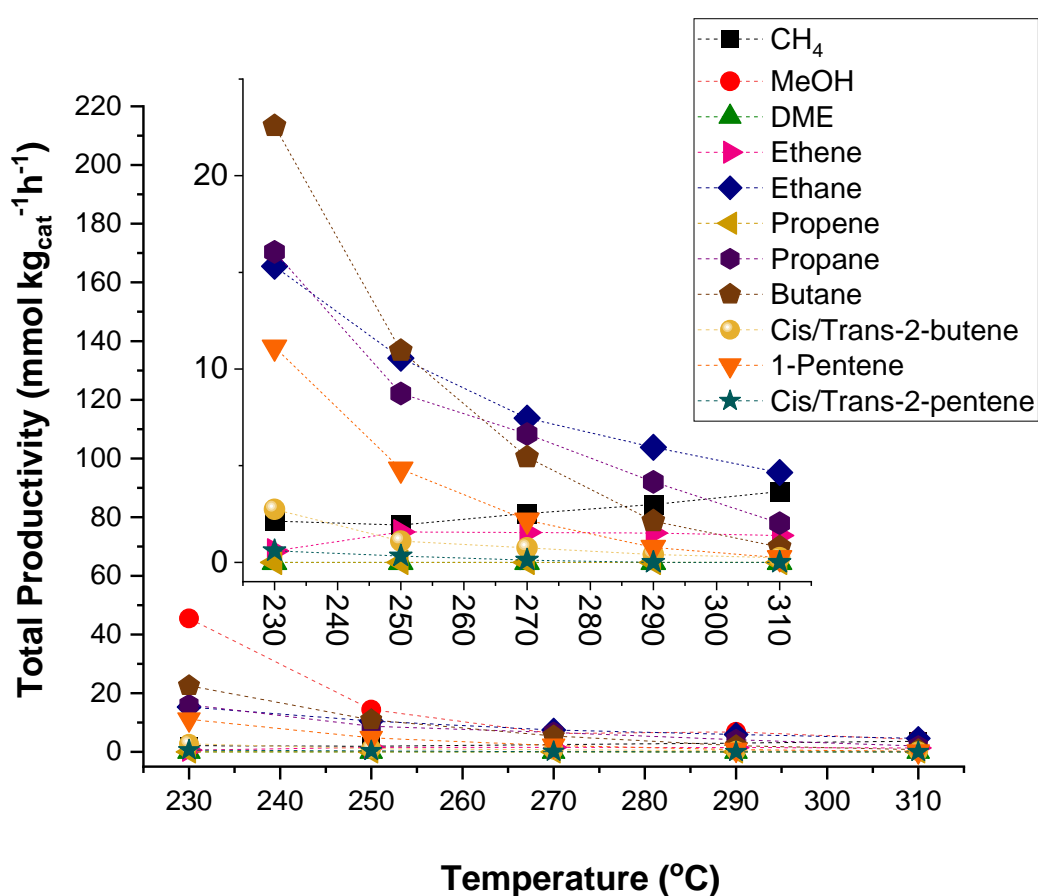
Comparing the graphs above, it can be seen that the method where the two components of the catalyst were shaken resulted in only the formation of ethane as an additional product, although at very low productivity; the ground 10% Cu/ZnO + ZSM-5 (23:1) catalyst is able to produce higher chain hydrocarbons up to C<sub>4</sub>. Although these productivities are low, the importance of the contact required between the strong acid sites of the zeolite and the active metals is demonstrated by revealing the changes in product distribution from the different physical preparation methods employed; also in contrast to previous results in this section, the methanol and DME productivities are lower, this shows the significance of the active metal sites in addition to the acid sites of the zeolite.



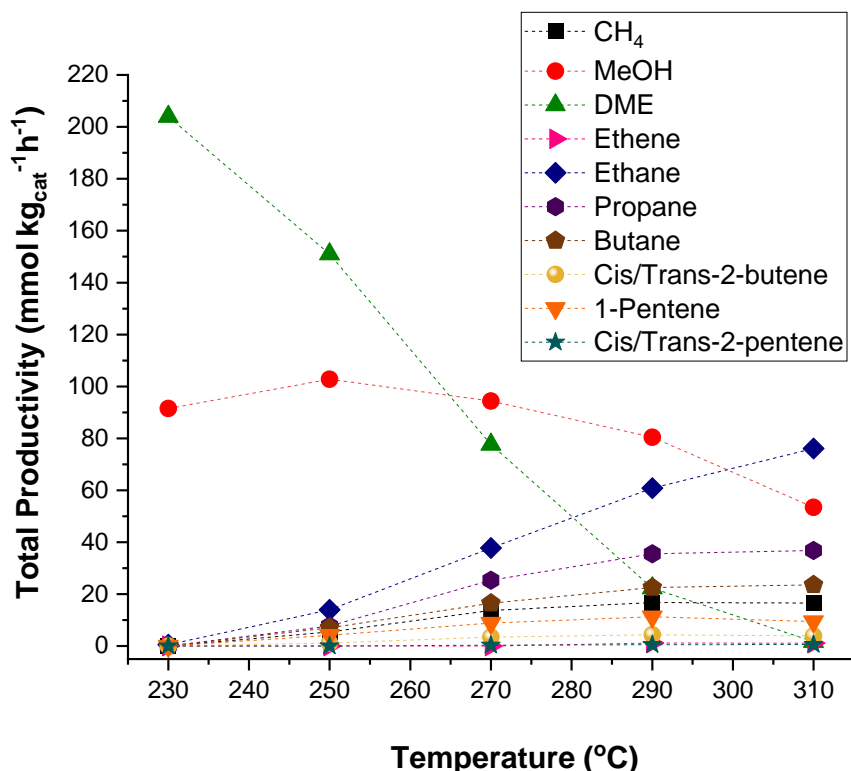


A recent study by Gohsh et. al proposed a kinetic model for the direct CO<sub>2</sub> hydrogenation to different hydrocarbon products over an In<sub>2</sub>O<sub>3</sub>/HZSM-5 bifunctional catalytic bed. The individual components were physically mixed in a mass ratio In<sub>2</sub>O<sub>3</sub>:HZSM-5 = 2:1 at a total of 1 g. The reaction was conducted at 20-40 bar, 250 - 400°C, H<sub>2</sub>:CO<sub>2</sub> – 1:1 to 4:1. Interestingly no DME was detected under any conditions in the effluent gas stream suggesting any DME formed is consumed quickly to form hydrocarbons. Compared with the singular indium catalyst the mixed bed catalyst resulted in lower CO selectivity through the suppression of the undesired RWGS and a higher methanol yield which was mostly converted to hydrocarbons. At a pressure of 40 bar and H<sub>2</sub>:CO<sub>2</sub> = 3:1 the mole fraction of methanol increases from 250°C to 350°C and then declines. The concentration of alkanes C<sub>2</sub>-C<sub>4</sub> increases above 250°C and at higher temperatures of 350°C there is a rapid increase in alkanes, particularly propane. As seen in the results above however, at much lower concentrations. The presence of alkenes is also observed initially, but this reduces at higher temperatures (> 350°C). The differences observed in this study show that under particular conditions (high partial pressure of H<sub>2</sub>, high temperatures, and catalyst mass ratio) the consumption of intermediates and hydrogenation of alkenes can result in higher hydrocarbon formation.<sup>(20)</sup>

From the information above, we have found that contact between the zeolite and active metals is important. The focus of the experiments conducted is to encourage the formation of DME through methanol dehydration and subsequent higher chain hydrocarbons at elevated temperatures. In order to maximise the efficiency of these reactions, changes to the catalyst bed were investigated. The changes involved either the pellets of the 10%Cu/ZnO and H-ZSM-5 (23:1) placed into separate beds, with the 10% Cu/ZnO placed at the end closest to the initial reaction feed followed by pellets of H-ZSM-5, or the pellets of both 10% Cu/ZnO and H-ZSM-5 were mixed and tested. The results are shown below in Figures 5.18 and 5.19.



**Figure 5.18** – Total productivity of 10% Cu/ZnO + H-ZSM-5 (23:1) pellets in separate beds, **reduced *in-situ***: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). Insert shows product distribution at an enlarged scale for clarity. **Reaction conditions:** 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.



**Figure 5.19** – Total productivity of 10% Cu/ZnO + H-ZSM-5 (23:1) pellets in mixed bed, **reduced *in-situ***: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions**: 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

From the graphs, the mixed bed has a fourfold increase in total productivity compared to the separate bed. No DME is observed in the separate bed, suggesting that it is either instantly consumed on formation or not formed at all, even at the lower temperatures, as presence of additional hydrocarbons up to C<sub>5</sub> are observed from 230 °C. The total productivity falls below 25 mmol kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> for the separate bed and as the temperature is increased the total productivity decreases, most likely due to the decomposition of methanol to CO which is more favourable at higher temperatures.

Comparing with the results from the mixed bed, we can see there is a complete contrast in the profiles. The product distributions are fairly similar; however, the addition of propene is seen in the separate bed, at a very low productivity. In the case of the mixed bed, the DME is produced at the start and is then slowly consumed with increased temperature, as shown in the catalysts tested previously; compared to the CuZn/ZSM-5 (23:1)-OG catalyst, both the methanol and DME productivities are lower. However, the product distribution is much broader; of the additional products, the highest productivity of 76 mmol<sub>C<sub>2</sub>H<sub>6</sub></sub> kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup> was achieved for ethane at 310 °C.

The results between the catalyst beds and data in Table 5.5 can be linked to the direct exposure of Cu/ZnO catalyst and the contact time between the formed products and zeolite. For the separate bed, the methanol and DME formed have a direct contact with the H-ZSM-5 zeolite across the bed; however, the increasing temperature is likely to impact the exposed Cu/ZnO required for the methanol formation. For the mixed bed the zeolite is more distributed and in good proximity to the Cu/ZnO pellets within the catalyst bed, allowing the rate of DME formation to increase at lower temperatures. As the temperature increases (> 250 °C), the conversion to hydrocarbons increases and DME decreases, which could be associated with the strong acid sites beginning to deactivate (increased water production).

Excessive water has been shown to deactivate surface acidic sites on zeolites, inhibiting C–C bond formation and leading to a low production of C<sub>2+</sub> products. Fujiwara et al. developed a composite catalyst consisting of a Cu–Zn–Al oxide and modified HB zeolite (addition of 1,4-bis(hydroxydimethylsilyl)benzene to the zeolite surface for hydrophobicity.), this significantly improved the yield of C<sub>2+</sub> hydrocarbons by suppressing the deactivation of strong acidic sites.<sup>(21)</sup>

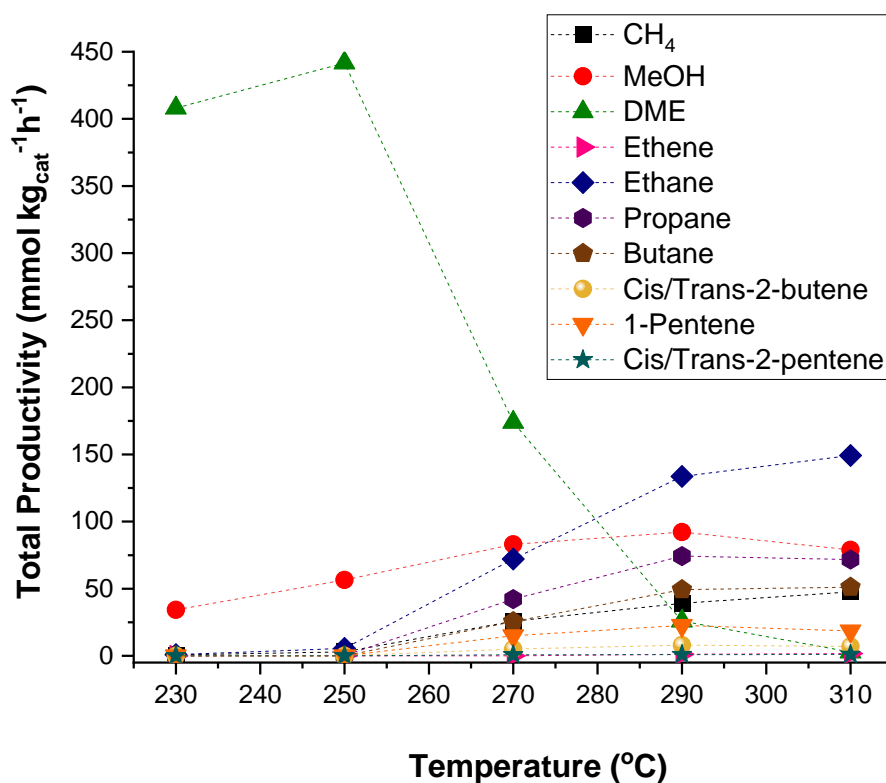
**Table 5.5:** Conversion and selectivity data for 10% Cu/ZnO + H-ZSM-5 (23) mixed and separate bed

10% Cu/ZnO + H-ZSM- 5 (23)	Temperature (°C)	X CO <sub>2</sub> (%)	S MeOH (%)	S DME (%)	S CH <sub>4</sub> (%)	S CO (%)	S Ethane (%)	S Propane (%)	S Butane (%)	S 1- Pentene (%)
<b>separate bed</b>										
	230	20.4	1.4	1.1	0.1	90.0	0.1	1.6	2.6	1.7
	250	24.0	0.4	0	0.06	95.8	0.6	0.8	1.3	0.7
	270	26.5	0.2	0	0.06	97.8	0.4	0.5	0.6	0.3
	290	29.7	0.1	0	0.06	98.9	0.3	0.3	0.2	0.1
	310	33.0	0.1	0	0.08	99.3	0.2	0.1	0.1	0
<b>mixed bed</b>										
	230	8.8	6.7	30.0	0	63.2	0.1	0	0	0
	250	15.6	4.7	13.3	0.3	76.2	1.5	1.3	1.5	1.1
	270	18.5	3.6	6.0	0.5	79.2	2.9	2.9	2.5	1.7
	290	20.5	2.8	2.0	0.6	79.4	4.6	4.1	3.4	2.1
	310	23.0	1.5	0.1	0.5	85.5	4.5	3.2	2.8	1.4

The table above compares the CO<sub>2</sub> conversion and product selectivity data for the separate bed and mixed bed. For the separate bed, as the temperature and CO<sub>2</sub> conversion increase the selectivity to MeOH and DME decreases, and selectivity to higher chain hydrocarbons increases, particularly for butane up to 270 °C; however, CO remains the major product of the reaction. For the mixed bed, the CO<sub>2</sub> conversions are slightly smaller in comparison but the selectivity towards the higher chain hydrocarbons increases greatly after 270 °C, achieving up to 5% selectivity to ethane at 290 °C, 15x higher than the separate bed.

Pérez and co-workers proposed an eleven-*lump* kinetic model for the reaction of DME to olefins over a HZSM-5 catalyst, considering as *lumps*: methanol, water, DME, ethylene, propylene, butenes, C<sub>2</sub>–C<sub>4</sub> paraffins, C<sub>5+</sub> aliphatic hydrocarbons, BTX, methane and CO. It was shown that slightly above atmospheric pressure DME reacts at a lower temperature to olefins compared to methanol (350°C vs 450°C), and at the same temperature DME reacts 20 times faster than methanol. This is reflected in the results above, in particularly for the mixed bed, where the DME is consumed much quicker as the reaction temperature increases when compared to methanol. <sup>(22)</sup>

The previous experiment involving the variation in the catalyst bed has shown very interesting results, this is attributed to the contact between the active metal sites and key acid sites of the zeolite, and this can be used in order to influence the product distribution. By preparing a mixed bed catalyst consisting of 31% Cu/ZrO<sub>2</sub> catalyst and commercial H-ZSM-5 (23:1), it was hoped that the catalyst would be more active than those tested previously. As the CuZr/ZSM-5 (23:1) catalyst prepared via the oxalate gel was able to show reasonable productivities towards the desired products (Figure 5.13), the introduction of the ZSM-5 (23:1) zeolite via a mixed bed, with the addition of a higher Cu loading was expected to aid in an increase in methanol productivity and DME productivity, and subsequently the productivities of the higher chain hydrocarbons. The results for this are shown in Figure 5.20.



**Figure 5.20** – Total productivity of 31% Cu/ZrO<sub>2</sub> + H-ZSM-5 (23:1) pellets in mixed bed, **reduced *in-situ***: 1 h at 220 °C in H<sub>2</sub> ( 2 °C min<sup>-1</sup>, 1 bar, 30 ml min<sup>-1</sup> STP). **Reaction conditions:** 230 - 310 °C, 8 h dwells (total = 40 h), 30 ml min<sup>-1</sup> (STP) of CO<sub>2</sub> : N<sub>2</sub> : H<sub>2</sub> (1:1:3), P(total) = 20 bar.

The DME productivity is high at the start of the reaction, and in this instance, rises to 442 mmol<sub>DME</sub>kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> for 250 °C, and falls as the temperature increases. The MeOH productivity on the other hand remains level across the temperature range. As anticipated, an increase in the higher chain hydrocarbon productivities is observed; the highest productivity is seen for ethane at 310 °C with 149 mmol<sub>C<sub>2</sub>H<sub>6</sub></sub> kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>, which is almost twice as much as that for the 10%CuZn + H-ZSM-5 mixed bed catalyst, suggesting increasing the metal loading of the catalyst in the mixed bed increases the DME productivity and resulting hydrocarbons.

### 5.3 – Conclusions

A series of 20 wt.% CuZn (1:1) catalysts were prepared via Chemical Vapour Impregnation (CVI) and oxalate gel method (OG) on commercial ZSM-5 zeolites (Si:Al 23; 30; 50 and 80). Additional zeolites used include mordenite (20:1) and zeolite Y. These catalysts were tested over a temperature range of 230 – 310 °C. The activity of the oxalate gel catalysts were far greater than those produced via CVI, with the CuZn/ZSM-5 (50:1) being most active, which is due to the choice of zeolite used and smaller size of the metal particles of the catalyst. From the TEM analysis, the presence of needles/strings of phase separated CuZn detached from the ZSM-5 support were detected; despite this lack of homogeneity and dispersion of the active metals on the surface of the zeolite, the oxalate gel catalyst still maintains its activity through the limited contact and hence access to the channels of the zeolite necessary for the hydrocarbon formation. The equivalent OG catalyst containing CuZr was also tested and found to be slightly more active than the CuZn.

Of the series of H-ZSM-5 catalysts tested, the lowest Si:Al was most acidic, as reflected in the NH<sub>3</sub>-TPD profiles where an increase in the Si:Al ratio resulted in a decrease in the number of total acid sites available. CuZn/ZSM-5 (23:1) contains the highest amount of strong sites, compared to the other catalysts, as well as medium acid sites. As higher chain hydrocarbon formation was seen only for the 23:1 catalyst, it is suggested that the acid sites described are essential towards the formation of higher hydrocarbons. Relating back to the reactivity data the lower methanol and DME productivity can be correlated with a higher concentration of total acid sites, as well as the decreased size of the Cu particles, as shown in the XRD patterns.

Physical mixtures of 10% Cu/ZnO, prepared by the oxalate gel method, and commercial H-ZSM-5 (23:1) were made. Two methods of physical mixture were employed: shaking and grinding, where the shaken resulted in only the formation of ethane as an additional product, although at very low productivity; and the ground 10% Cu/ZnO + ZSM-5 (23:1) catalyst, which was able to produce higher chain hydrocarbons up to C<sub>4</sub>. Although the productivities are low, it demonstrates the importance of the contact required between the strong acid sites of the zeolite and the active metals.

Pellets of the 10%Cu/ZnO and H-ZSM-5 (23:1) were placed into either a separate bed or mixed bed and tested. Differences in activity can be linked to the direct exposure of Cu/ZnO catalyst and the contact time between the formed products and zeolite. For the separate bed, the methanol and DME formed have a direct contact with the H-ZSM-5 zeolite across the bed; however, the increasing temperature is likely to impact the exposed Cu/ZnO required for the methanol formation. For the mixed bed, the zeolite is more distributed and in good proximity to the Cu/ZnO pellets within the catalyst bed, allowing

the rate of DME formation to increase at lower temperatures. As the temperature increases (> 250 °C) the conversion to hydrocarbons increases and DME decreases, which could be associated with the strong acid sites beginning to deactivate (increased water production).

A mixed bed catalyst consisting of 31% Cu/ZrO<sub>2</sub> catalyst and commercial H-ZSM-5 (23:1) was also prepared, and an increase in the higher chain hydrocarbon productivities observed. The highest productivity is seen for ethane at 310 °C with 149 mmol<sub>C<sub>2</sub>H<sub>6</sub></sub> kg<sub>cat</sub><sup>-1</sup>h<sup>-1</sup>, which is almost twice as much as that for the 10%CuZn + H-ZSM-5 mixed bed catalyst, suggesting that increasing the metal loading of the catalyst in the mixed bed increases the DME productivity and resulting hydrocarbons.

Future work recommended for this section includes the testing of the zeolites themselves and zeolites with the addition of only Cu to determine their potential activity towards the production of methanol, DME and hydrocarbons and compare to the results discussed in this section. Running experiments with an initial feed of DME, as opposed to CO<sub>2</sub>, for the conversion to hydrocarbons. This would allow a greater insight into the interaction of key intermediates with the zeolites. In addition, various experimental parameters such as total reaction pressure and H<sub>2</sub>/CO<sub>2</sub> ratio can be increased to enhance CO<sub>2</sub> conversion and reduce CO selectivity, thereby increasing the net yield of hydrocarbons over the bifunctional catalytic bed.



## 5.4 – References

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## Chapter 6

### Conclusions and Future Work.

Amid global warming concerns and skyrocketing CO<sub>2</sub> emissions in the atmosphere, mainly associated with the combustion of fossil fuels to produce energy, the research community has gained a large interest in CO<sub>2</sub> capture and reutilization to produce renewable fuels such as methanol (MeOH), dimethylether (DME) and additional hydrocarbons. By combining an integrated green hydrogen approach, whereby the H<sub>2</sub> is obtained using renewable sources, the synthesis of these fuels can become more sustainable in the light of the carbon cycle.

The main aims of the work for this project were:

- Identify catalysts that can operate under low temperatures (< 250 °C) for MeOH synthesis from CO<sub>2</sub>.
- Identify and develop active catalysts composed of earth-abundant materials for the hydrogenation of CO<sub>2</sub> to MeOH and DME.
- Investigate the formation of hydrocarbons via methanol formation using integrated catalysts (MeOH synthesis + zeolite).

The work in Chapter 3 explored the effect of various supported Cu catalysts prepared via the oxalate gel synthesis method, with a particular focus on Cu/ZrO<sub>2</sub>, towards the conversion of CO<sub>2</sub> to MeOH. The role of various promoters (Pd, Pt, Ce, Ni and Ag) and the stability of these catalysts was also investigated. It was found that at low temperatures the Cu/ZrO<sub>2</sub> catalyst is both active towards methanol production and stable. The introduction of promoters did not show any improvement to the catalyst performance; for future studies it would be beneficial to investigate further methods to introduce key promoters to the catalyst surface with an investigation into the loading effects.

The work in Chapter 4 explored the impact of varying the calcination temperature and reduction temperature of the Cu/ZrO<sub>2</sub> catalysts prepared via oxalate gel, towards their hydrogenation of carbon dioxide to methanol and DME. The deposition of Cu onto the ZrO<sub>2</sub> polymorphs by oxalate gel and wet impregnation was also investigated to understand the effects of preparation method and support phase on catalytic activity. It was shown that the type of preparation method used, as well as the ZrO<sub>2</sub> phase,

Cu surface area, and Cu dispersion, are all important factors towards the catalyst activity. Future work could involve the investigation of more refined preparation methods to deposit Cu onto the support; by doing this the main factors listed above can be targeted.

Work in chapter 5 looked at the production of MeOH, DME and higher chain hydrocarbon productivities between various CuZn or CuZr Zeolite integrated catalysts, where the zeolite is either commercially available H-ZSM-5 (Si:Al 23; 30; 50 and 80), mordenite (20:1) or zeolite Y, prepared via chemical vapour impregnation (CVI) and oxalate gel precipitation. Physical mixtures of the catalysts as well as changes to the catalyst bed were also explored in order to compare the catalyst activity. It was found that the preparation method used largely impacted the metal particle size, with oxalate gel forming smaller particles over CVI. Interesting results were seen with regards to hydrocarbon formation using the more acidic H-ZSM-5 (23) catalysts, as well as variation in the catalyst bed. Future studies could include the investigation of varying reaction conditions, such as the temperature, pressure, and gas feeds (start with DME), alongside a mixed bed catalyst to help improve on productivities, research into reactor design to investigate catalyst stability, and a look into using different metal loadings.