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1 **Evaluating the accuracy of the Distributed Activation Energy Model for**
2 **biomass devolatilization curves obtained at high heating rates**

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10
11 **ABSTRACT**

12 The characteristic parameters of devolatilization, the activation energy and the
13 frequency factor, can be obtained following different experimental approaches. In the
14 Distributed Activation Energy Model (DAEM), these parameters are derived from
15 several TGA curves that are typically obtained for constant, low heating rate
16 experiments. Then, the results are used to model high heating rate processes typical
17 of industrial combustors. In this work, a wide range of heating rates were employed
18 to obtain different TGA curves of the biomass pyrolysis, in order to analyse the
19 validity of DAEM when extrapolating the kinetic parameters obtained for low heating
20 rate curves used in the laboratory to higher heating rates present in industrial
21 applications. The TGA curves of the biomass pyrolysis employed in DAEM were
22 varied from low heating rates (around 10 K/min, values typically found in the literature

23 on DAEM), to high heating rates (up to 200 K/min). The differences in the activation
24 energy and the frequency factor obtained for different heating rates, were evaluated
25 and the validity of the model was discussed. The results show differences between
26 the activation energy and the frequency factor obtained using low and high heating
27 rates during the TGA tests. Therefore, if an accurate approximation is required when
28 extrapolating the data to high heating rates, the tests should be carried out at high
29 heating rates.

30 **KEYWORDS**

31 Distributed Activation Energy Model, devolatilization, pyrolysis, biomass conversion,
32 activation energy, heating rate.

33 **NOMENCLATURE**

34 a Heating rate [K/s].

35 E_a Activation energy for a determined devolatilization rate [J/mol].

36 k_0 Frequency factor for a determined devolatilization rate [s⁻¹].

37 R Universal constant [J/mol·K].

38 R^2 Determination coefficient of the linear fitting [-].

39 T Temperature [K].

40 V Volatile mass loss [%].

41 V^* Volatile content [%].

42 V/V^* Devolatilization rate [%].

43 ε Relative error [%].

44 **1. Introduction**

45 Biomass pyrolysis takes place during most of the processes related to biomass
46 thermochemical conversion, such as production of liquid biofuels [1], synthesis gas
47 [2], chemicals [3], or charcoal [4], becoming a key factor in most applications. The
48 characteristic parameters that control the kinetics of biomass devolatilization are the
49 activation energy (E_a) and the frequency factor (k_0). Several models are available in
50 literature to describe biomass pyrolysis [5], [6], [7], and between them the Distributed
51 Activation Energy Model (DAEM) proposed by Vand [8] has been widely used due to
52 its simplicity and accuracy. Miura and Maki [9] simplified the model to estimate the
53 activation energy and the corresponding frequency factor from three TGA curves
54 obtained for different heating rates. This simplification has been used to describe the
55 kinetics of pyrolysis for different types of biomass [10], [11], [12], [13], [14], coal [15],
56 [16], sewage sludge [17], [18], and waste [19], [20], [21].

57 The heating rates employed using DAEM are usually low, in the range of 3 to 30
58 K/min, due to the higher accuracy of TGA at reduced heating rates. Miura and Maki
59 [9] proposed the use of heating rates of 5, 10 and 20 K/min, but Sonobe et al. [10]
60 employed even lower heating rates 2, 4 and 10 K/min. Shen et al. [11] employed
61 heating rates between 5 and 40 K/min and Soria-Verdugo et al. [18] used heating
62 rates of 10, 15, 20 K/min. Despite of the variety of heating rates found in the literature
63 most of the authors used heating rates below 50 K/min. As an exception, Li et al. [15]
64 used heating rates of 20, 35, 50, 75 and 100 K/min during the devolatilization of coals
65 and biomass in a thermogravimetric analyzer, nevertheless there is no available data
66 for heating rates beyond 100 K/min.

67 In this work, a wider range of heating rates (3, 5, 10, 15, 20, 30, 50, 80, 100, 150 and
68 200 K/min) were employed to obtain different TGA curves, in order to analyse the
69 validity of the simplified Distributed Activation Energy Model, when extrapolating the
70 kinetic parameters obtained for low heating rate curves to higher heating rates. The
71 simplified DAEM process described by Miura and Maki [9] to obtain the pyrolysis
72 parameters was analyzed for the different heating rates, therefore the three TGA
73 curves employed were varied from very low heating rates (3, 5 and 10 K/min) to
74 higher heating rates (100, 150 and 200 K/min). The differences in the activation
75 energy and the frequency factor were evaluated and the validity of the model was
76 discussed.

77 **2. Experimental procedure**

78 The biomass employed during the tests was obtained from commercial pine pellets.
79 The biomass characterization results of a proximate and ultimate analysis are
80 presented in Table 1. The proximate analysis was performed in a TGA Q500 TA
81 Instruments, while the ultimate analysis was carried out in a LECO TruSpec CHN
82 and TruSpec S elemental analyzer. The moisture of the sample was obtained after
83 an isothermal process at 105°C under an inert atmosphere in the TGA, whereas the
84 volatile content was determined heating the sample up to 900°C under an inert
85 atmosphere, and maintaining the temperature until no difference in the mass of the
86 sample was observed. The ash content was measured as the constant mass of the
87 sample remaining after an isothermal process at 550°C under and oxidant
88 atmosphere. Finally, the fixed carbon of the sample was obtained by difference.

Proximate analysis ^a	
Moisture [%]	3.3
Volatiles [%]	76.3
Fixed carbon ^b [%]	17

Ash [%]	3.4
Ultimate analysis ^a	
C [%]	46.13
H [%]	6.51
N [%]	0.82
S [%]	0.07
O ^b [%]	46.47

89

90 Table 1. Thermochemical characterization of the biomass employed (^a wet basis, ^b
91 obtained by difference).

92 The devolatilization tests were carried out in the same thermogravimetric analyzer

93 TGA Q500 TA Instruments employed to obtain the biomass proximate analysis.

94 During the experiments, the TGA furnace was flushed with 60 ml/min of nitrogen to

95 maintain an inert atmosphere. The mass of the samples were 10±0.5 mg and they

96 were sieved under 100 μm to avoid heat transfer effects, according to Di Blasi et al.

97 [22]. A blank experiment was also run for any case studied to avoid buoyancy effects

98 [11], [12]. Each test was repeated five times to guarantee repeatability, obtaining

99 differences always lower than 3%.

100 Once the sample was introduced in the TGA, it was heated up to 105°C from room

101 temperature, and an isothermal process was maintained during 20 minutes to

102 eliminate all the moisture content. Then, the devolatilization process begins, and the

103 temperature increases with a constant heating rate *a* until 600°C. Fig. 1 shows the

104 weight loss and the temperature versus time for the TGA analysis using heating rates

105 *a* of 20 and 200 K/min during the devolatilization process. The drying process is the

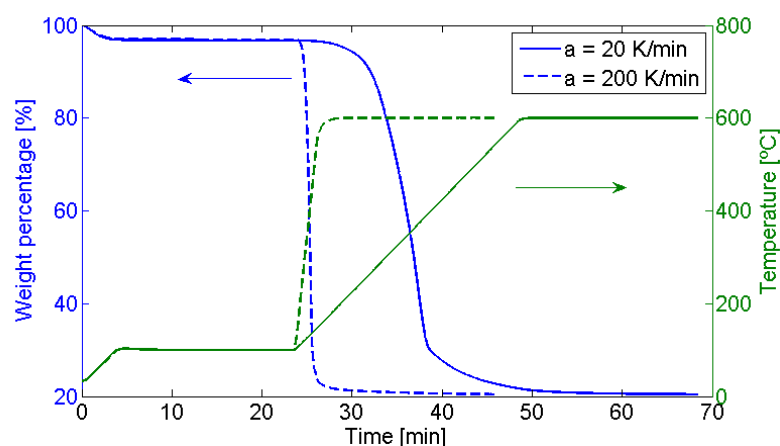
106 same for both tests so the weight loss curves collapsed during the first part of the

107 analysis, nevertheless the different heating rates employed in the devolatilization

108 process produced significant differences on the sample weight loss curves when the

109 pyrolysis occurred. Depending on the heating rate used during the devolatilization

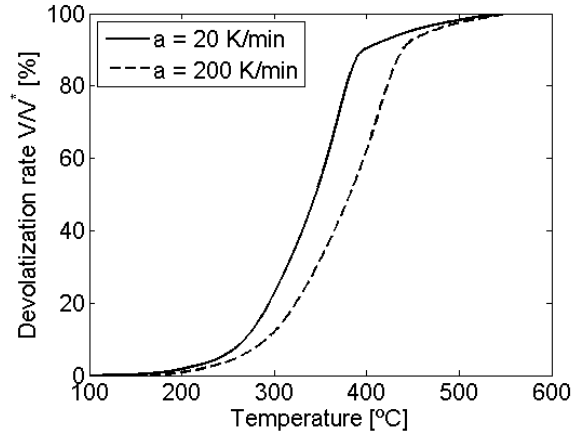
110 process, the time needed for the test can be very different, from 68 minutes for the
111 heating rate of 20 K/min to just 45 minutes when using 200 K/min, nonetheless the
112 weight percentage loss at the end of the devolatilization is independent of the heating
113 rate employed. During the experiments several heating rates were employed during
114 the devolatilization process, in a wide range: 3, 5, 10, 15, 20, 30, 50, 80, 100, 150,
115 and 200 K/min. In the case of a heating rate of 3 K/min, 210 minutes were needed to
116 perform the test.



117

118 Figure 1: Example of a thermogravimetric analysis ($a = 20 \text{ K/min}$ and 200 K/min)

119 Finally, since this work is not focused in the drying process but in the devolatilization
120 process, the range of devolatilization can be obtained from the TGA curve (Fig. 1),
121 defining a devolatilization rate of 0% at the end of the isothermal process at 105°C,
122 and 100% when the temperature is 550°C, ensuring a constant heating rate, a , for
123 the whole devolatilization process. Fig. 2 shows the devolatilization rate as a function
124 of temperature for the same heating rates depicted in Fig. 1. It can be observed that
125 most of the devolatilization process occurs between 300°C and 400°C, obtaining a
126 sharp devolatilization rate typical of cellulose.



127

128 Figure 2: Devolatilization rate against temperature ($a = 20 \text{ K/min}$, 200 K/min)

129 3. Simplified DAEM model

130 The Distributed Activation Energy Model has been proved to be an accurate method
 131 to describe the pyrolysis kinetics of biomass, obtaining a good agreement with the
 132 experimental data [10], [23], [24], and [25], when operating at low heating rates. The
 133 model assumes the existence of an infinite number of irreversible first order reactions
 134 occurring sequentially, with different associated activation energies, E_a . The
 135 devolatilization process can be described in the integral form by Eq. 1:

$$136 \quad 1 - \frac{V}{V^*} = \int_0^{\infty} \exp\left(-k_0 \int_0^t e^{-E/RT} dt\right) f(E) dE \quad (1)$$

137 where V/V^* is the devolatilization rate, R the universal constant, T the temperature for
 138 each devolatilization and $f(E)$ the distribution function of the activation energy. This
 139 equation was simplified to Eq. 2 by Miura et al. [26]

$$140 \quad V/V^* \cong 1 - \int_{E_a}^{\infty} f(E_a) dE_a = \int_0^{E_a} f(E_a) dE_a \quad (2)$$

141 The Arrhenius equation of the simplified DAEM model is:

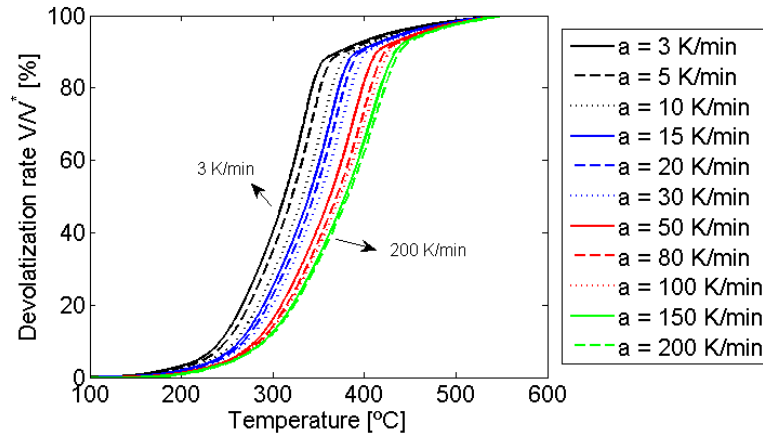
142
$$\ln\left(\frac{a}{T^2}\right) = \ln\left(\frac{k_0 R}{E_a}\right) + 0.6075 - \frac{E_a}{R} \frac{1}{T} \quad (3)$$

143 The values of the activation energy, E_a , and the corresponding frequency factor, k_0 ,
144 present in Eq. 3 can be obtained from three different thermogravimetric curves
145 obtained with different heating rates. Miura and Maki [9] proposed a procedure
146 following the next steps:

- 147 a) Measure and plot the devolatilization rate, V/V^* , as a function of the temperature,
148 T , for three different heating rates, a .
- 149 b) Plot $\ln(a/T^2)$ versus $1/T$ for the three different heating rates at each devolatilization
150 rate (Arrhenius plot).
- 151 c) For each V/V^* in the Arrhenius plot, linearize the data of the different heating rates
152 and obtain E_a and k_0 from the slope and the intercept respectively.

153 **4. Results and discussion**

154 Thermogravimetric tests were carried out for heating rates of 3, 5, 10, 15, 20, 30, 50,
155 80, 100, 150, and 200 K/min, obtaining the devolatilization rates plotted in Fig. 3 for
156 each heating rate. The devolatilization takes place at higher temperatures when
157 increasing the heating rate, a result previously reported in the literature that can be
158 attributed to non-isothermal pyrolysis processes [27], [28].



159

160

Figure 3: Devolatilization rate versus temperature for each heating rate.

161

Following the procedure proposed by Miura and Maki [9], the temperature at which

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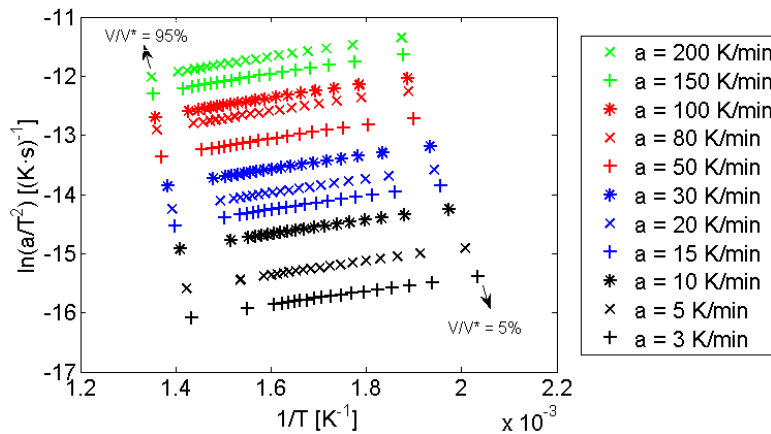
each devolatilization rate occurs can be obtained from Fig. 3, for each heating rate.

163

With these temperatures, an Arrhenius plot can be built, plotting $\ln(a/T^2)$ versus $1/T$,

164

as shown in Fig. 4 for each devolatilization rate, with variations of 5%.



165

166

Figure 4: Arrhenius plot for each devolatilization rate.

167

The next step in the procedure described by Miura and Maki [9] is the linearization of

168

the results shown in the Arrhenius plot for each devolatilization rate. Analysing Fig. 4

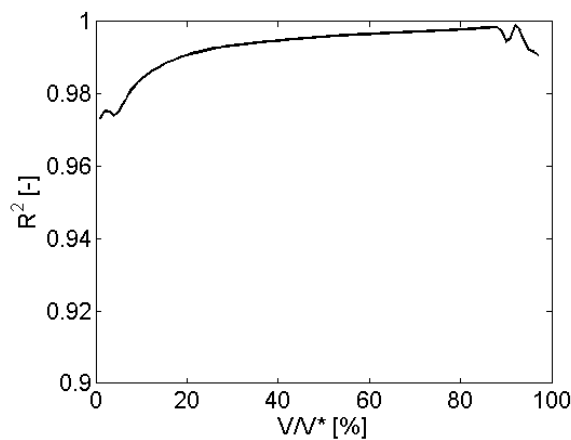
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for low devolatilization rates ($V/V^* = 5\%$), it can be observed that there is a change in

170

the slope of the linearization curve for heating rates over 50 K/min. For high

171 devolatilization rates this is not so evident. In order to quantify the goodness of a
172 linear fitting of the results considering all the heating rates, the determination
173 coefficient, R^2 , of the linear fitting is shown in Fig. 5, as a function of the
174 devolatilization rate. The determination coefficient is found to be lower at low
175 devolatilization rates informing of a poor linearity of the data in this zone, confirming
176 the idea that there is a change in slope for low devolatilization rates obtained from
177 the visual inspection of Fig. 4.



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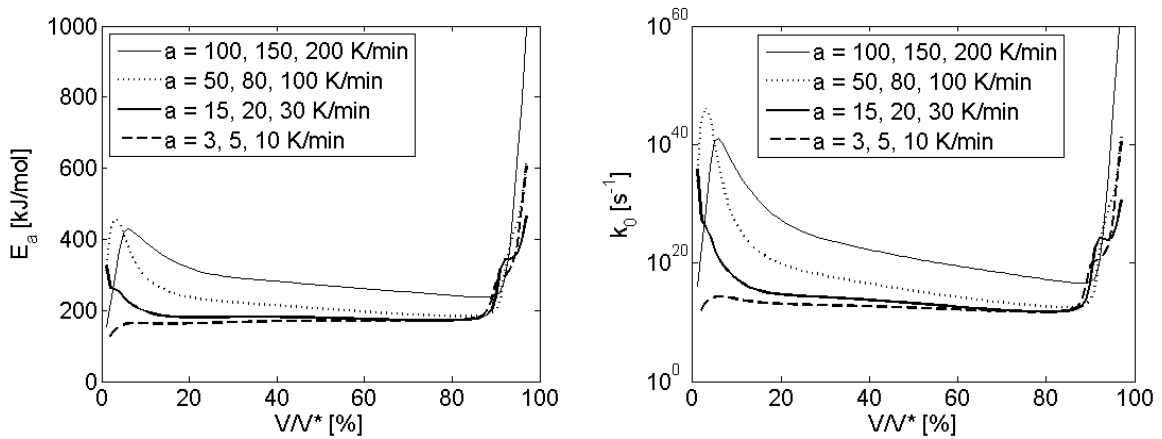
179 Figure 5: Determination coefficient of the linear fitting for all the heating rates as a
180 function of the devolatilization rate.

181 The linearization of the results shown in the Arrhenius plot (Fig. 4) was carried out
182 regrouping the data for three different heating rates as suggested by Miura and Maki
183 [9]. The experimental data allows to linearize the results for very low heating rates (a
184 = 3, 5, 10 K/min), low heating rates ($a = 15, 20, 30$ K/min), medium heating rates ($a =$
185 50, 80, 100 K/min) and high heating rates ($a = 100, 150, 200$ K/min), in order to
186 quantify the variation of slope stated above. The linearization of the results for each
187 group of heating rates provides an slope, m , and an intercept, n , from which the
188 activation energy, E_a , and the frequency factor, k_0 , can be easily obtained in view of
189 Eq. 3, obtaining Eq. 4 and 5.

190 $E_a = -m \cdot R$ (4)

191 $k_0 = -m \cdot e^{n-0.6075}$ (5)

192 The values of the activation energy and the frequency factor are presented in Fig. 6
 193 a) and b) respectively, as a function of the devolatilization rate for very low, low,
 194 medium and high heating rates. There is a clear difference in both the activation
 195 energy and the frequency factor when linearizing the results obtained for low and
 196 high heating rates. These parameters increase when higher heating rates are
 197 employed, confirming the existence of a higher slope in the linearization of the high
 198 heating rate TGA curves ($a = 100, 150, 200 \text{ K/min}$). The difference is larger at low
 199 devolatilization rates, as established in Fig. 5.



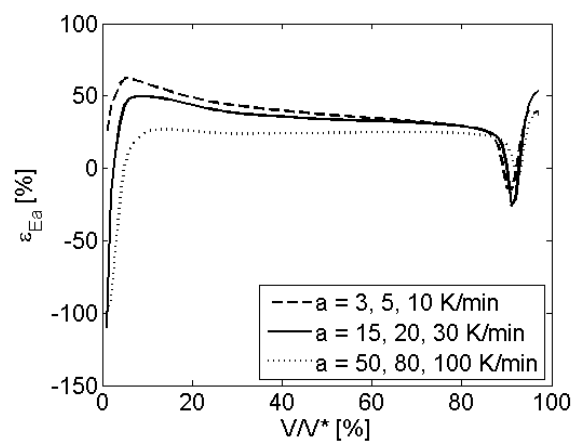
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201 Figure 6: a) Activation energy and b) frequency factor for each devolatilization rate.

202 The difference in activation energy obtained between each group of heating rates
 203 and the higher one can be analyzed by means of a relative error, ε , defined in Eq. 6.

204
$$\varepsilon = 100 \cdot \frac{E_{a_{i,j,k}} - E_{a_{100,150,200}}}{E_{a_{100,150,200}}} \quad (6)$$

205 The results of the relative error in activation energy can be observed in Fig. 7. A
206 relative error around 20% for the medium heating rates ($a = 50, 80, 100 \text{ K/min}$) and
207 around 40% for low ($a = 15, 20, 30 \text{ K/min}$) and very low heating rates ($a = 3, 5, 10$
208 K/min) is found for devolatilization rates between 20 and 80%, that is, for most of the
209 devolatilization process. Therefore, an error around 40% is made when determining
210 the activation energy with low heating rate TGA curves typically found in the literature
211 and extrapolating the results to high heating rates.



212

213 Figure 7: Relative error of the activation energy obtained from low and high heating
214 rates.

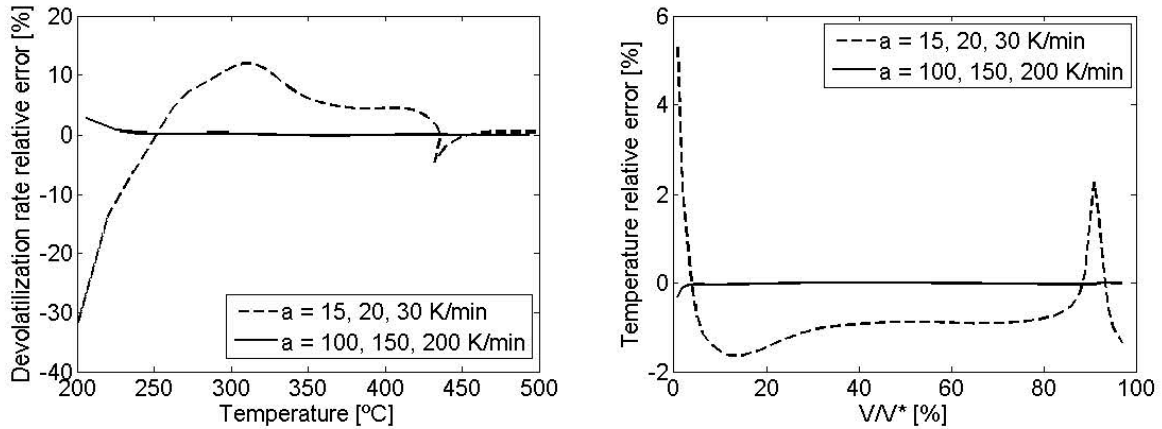
215 Finally, with the activation energy and the pre-exponential factor, the devolatilization
216 curve for a heating rate of 200 K/min can be recuperated and the differences
217 between the experimental curve obtained from the TGA and the curve recuperated
218 using DAEM can be evaluated. The recuperation could be carried out by solving the
219 temperature in Eq. 9 or linearizing the Arrhenius plot for each heating rate, as
220 described in [19], with negligible differences. The differences between the TGA curve
221 obtained for a heating rate of 200 K/min and the curve recuperated using the
222 Distributed Activation Energy Model with low ($a = 15, 20, 30 \text{ K/min}$) and high heating

223 rates ($a = 100, 150, 200 \text{ K/min}$) were analyzed by means of the devolatilization rate
224 error and the temperature error described in Eq. 7 and 8 respectively.

$$225 \quad \varepsilon_{V/V^*} = 100 \cdot \frac{V/V_{DAEM}^* - V/V_{TGA}^*}{V/V_{TGA}^*} \quad (7)$$

$$226 \quad \varepsilon_T = 100 \cdot \frac{T_{DAEM} - T_{TGA}}{T_{TGA}} \quad (8)$$

227 The error obtained for the devolatilization rate is plotted in Fig. 8 a). It can be
228 observed that the DAEM recuperated curve coincided with the experimental curve
229 when using the high heating rates ($a = 100, 150, 200 \text{ K/min}$), obtaining an error close
230 to zero. Nevertheless, when recuperating the curve with the activation energy and
231 pre-exponential factor obtained for low heating rates ($a = 15, 20, 30 \text{ K/min}$) the error
232 in devolatilization rate is not negligible. In this case a higher error is obtained for low
233 temperatures where the devolatilization rate is low, but for temperatures between
234 300°C and 400°C , where most of the devolatilization process occurs, the
235 devolatilization error is between 5 and 10%. In the case of the temperature error,
236 shown in Fig. 8 b), the value of the error is around 1% for devolatilization rates
237 between 20 and 80%. The higher error obtained for the devolatilization rate, in
238 comparison to that of the temperature, is motivated by the high slope shown in the
239 devolatilization rate curve (Fig. 2) for this type of biomass.



240

241 Figure 8: Error between the TGA curve for a heating rate of 200 K/min and the curve
 242 recuperated using DAEM, a) Devolatilization rate error b) Temperature error.

243 This result show a certain weakness of the standard process of obtaining the
 244 devolatilization parameters, E_a and k_0 , at low heating rates, as defined by Miura and
 245 Maki [9]. Even though the error obtained when extrapolating the activation energy
 246 obtained for low heating rates to higher rates can be as high as 50%, the final error
 247 obtained in the devolatilization curve is around 10% for V/V^* and just 1% for T . This
 248 error should be considered for and accurate description of the devolatilization
 249 process.

250 5. Conclusions

251 The Distributed Activation Energy Model (DAEM) was applied to study pine pellets
 252 devolatilization. The model is based on TGA curves obtained for several heating
 253 rates, from low heating rates usually found in literature (3, 5, 10, 15, 20, 30, 50
 254 K/min) to higher heating rates rarely reported (80, 100, 150, 200 K/min).

255 The Miura and Maki procedure was employed to obtain the activation energy and the
 256 frequency factor for each devolatilization rate. The procedure was repeated for very
 257 low heating rate curves (3, 5, 10 K/min), low heating rate curves (15, 20, 30 K/min),

258 medium values (50, 80, 100 K/min) and high heating rates (100, 150, 200 K/min) to
259 analyze the possible differences obtained. Such differences were quantified obtaining
260 a relative error for the activation energy around 40% when extrapolating the results of
261 low heating rates to higher ones. Nonetheless, when comparing the experimental
262 devolatilization curve for a heating rate of 200 K/min with the curve obtained applying
263 DAEM to low heating rates, the error in the devolatilization rate is under 10% and the
264 error in temperature is just 1%.

265 Therefore, care should be taken when employing DAEM from low heating rate TGA
266 curves and extrapolating the results to high heating rates typical of industrial
267 combustors.

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