

An improved prism energy analyzer for neutrons

J. Schulz^{1a}, F. Ott^b, Th. Krist^a

^a*Helmholtz-Zentrum Berlin für Materialien und Energie, Hahn-Meitner-Platz 1, 14109
Berlin, Germany*

^b*Laboratoire Leon Brillouin, Bât 563 CEA Saclay, 91191 Gif sur Yvette Cedex, France*

Abstract

The effects of two improvements of an existing neutron energy analyzer consisting of stacked silicon prism rows are presented. Firstly we tested the effect of coating the back of the prism rows with an absorbing layer to suppress neutron scattering by total reflection and by refraction at small angles. Experiments at HZB showed that this works perfectly. Secondly the prism rows were bent to shift the transmitted wavelength band to larger wavelengths. At HZB we showed that bending increased the transmission of neutrons with a wavelength of 4.9 Å. Experiments with a white beam at the EROS reflectometer at LLB showed that bending of the energy analyzing device allows to shift the transmitted wavelength band from 0 to 9 Å to 2 to 16 Å.

Keywords: Neutron Optics, Energy analysis, Prisms

1. Introduction

1 The proposed neutron energy analyzer is used to measure at different
2 wavelengths at the same time and so to enhance the usable flux e.g. in a
3 reflectometer used in time-of-flight mode. In the last years several energy
4 analyzing devices had been developed, tested and improved (summarized in
5 [1],[2]) e.g. refraction based devices such as very flat prisms [3] and stacked
6 prism systems [5]. Flat prisms take advantage of the refraction at small
7 angles which are several orders of magnitude higher than the refraction at
8 angles around 45 deg [4]. For neutrons that are refracted at 0.2 deg the de-
9 flection is in the range of 10^{-1} deg whereas the refraction by a single prism
10

¹Corresponding author. Tel.: +49 30 8062 43048.
E-mail address: jennifer.schulz@helmholtz-berlin.de (J. Schulz)

11 with side walls at an angle of 54.7 deg is only $6 \cdot 10^{-4}$ deg for 4.9 Å neutrons.
12 Thus a large number of such prisms is necessary to achieve a good wave-
13 length resolution.

14 The advantage of such a prism system is its flexibility. More prisms can be
15 added to achieve higher deflections and to encode broader beams.

16 The disadvantages of a system with stacked prism layers are the total reflec-
17 tion and the refraction at small angles which occur when neutrons interact
18 with the back of the prisms in the next prism layer at an angle close to the
19 critical angle of the total reflection. Since in both cases the neutrons are scat-
20 tered in opposite direction compared to the one of the refraction at the sides
21 of the prisms these neutrons are lost for the energy analysis and are counted
22 as background. They lead at the detector to an intensity increase at small
23 wavelengths and make the use of the device in a reflectometry measurement
24 less useful [5]. These background neutrons can be removed by coating the
25 back of the prisms with an absorbing layer, cf. §3.

26

27 A flat prism row with 191 prisms and a height of 0.25 mm transmits neu-
28 trons in a wavelength band from 0 Å to 9 Å [5]. To increase the transmission
29 of neutrons with larger wavelengths a bending, which follows the deflection
30 of the neutrons inside the prism rows can be applied (see Fig.1). This way
31 neutrons with larger wavelengths can pass through the prism rows without
32 interacting with the back of the prisms in the next row. The intensity is max-
33 imal for neutrons with such a wavelength that their path follows the bending
34 of the prism stack. Neutrons outside a wavelength band around this ideal
35 wavelength get absorbed when they hit the coated back of the prisms below
36 or above their entry row. VITESS [6] simulations show that the wavelength
37 band can be shifted to longer wavelengths by increasing the bending angle
38 to values between 1 and 10 m (see Fig.2). This way the wavelength band
39 from 0 to 20 Å can be covered with 5 different bending angles. It should be
40 noted that the widths of the wavelength bands become smaller for increasing
41 wavelengths since the refraction angle is proportional to the square of the
42 neutron wavelength. The experimental verification of this idea is shown in
43 §4.

44 2. Theory

45 In this section we want to derive a formula for the attenuation of a neu-
46 tron beam in a bent prism energy analyzer where the backs of the prisms are

47 coated with an absorbing material.

48 For the prism rows the refraction angle and thus the wavelength resolution
49 increases with the number of prisms. The angular dispersion of the sys-
50 tem is the wavelength dependence of the refraction angle according to the
51 wavelength dependence in the index of refraction n , which is

$$n = 1 - \frac{\lambda^2}{2\pi} Nb, \quad (1)$$

52 where λ is the wavelength of the neutron and Nb the scattering length density
53 of the prism material. The refraction angle φ is given by Snells law

$$\varphi = \alpha - \sin^{-1}(n \sin \alpha), \quad (2)$$

54 where α is the incident angle.

55 The absorption in the material is given by the linear attenuation coefficient
56 μ and the material thickness:

$$d = \frac{b}{2} \cdot i, \quad (3)$$

57 where b is the base width and i the number of the prisms. For the whole
58 prism system this leads to a transmission of

$$T_{Abs.} = e^{-\mu \cdot \frac{b}{2} \cdot i} = e^{-\mu \cdot \frac{ih}{\tan(\Phi)}}, \quad (4)$$

59 where h is the constant height of the prisms and Φ is the angle between the
60 base and the sides of the prisms.

61 The absorption due to losses at the back of the prisms is given by the number
62 of neutrons which arrive at the back of the prisms in the next layer. This
63 is given by the geometry of the prism system and the refraction per prism.
64 For small wavelengths only neutrons close to the next prism layer will touch
65 it. For a fixed number of prisms the deflection in height, Δ_z , of the neutrons
66 inside the prism rows should be calculated here. Assuming the neutrons enter
67 the prism rows parallel to the prism bases, homogeneously distributed over
68 the whole height and without divergence the ratio of Δ_z/h gives the losses
69 due to absorption at the absorbing layer at the back of the prisms. For a
70 single prism the deflection is given by:

$$\Delta_{z1} = b \cdot \tan \Theta, \quad (5)$$

with the refraction angle $\Theta = \varphi_{out} + \varphi_{in}$ for a single prism and φ_{in} and φ_{out} the refraction angles of the neutrons when entering and leaving the prism according to eq.2.

At each prism the angle changes as well as the deflection. The total deflection for a prism row with i prisms is given by:

$$\Delta_z = \sum_{j=1}^i (jb \cdot \tan(\Theta_j)) \approx b \cdot \tan(\Theta_1) \sum_{j=1}^i j \quad (6)$$

$$= \frac{i^2 + i}{2} b \cdot \tan(\Theta_1). \quad (7)$$

71 For all practical cases this is a very good approximation since for $\alpha = 54.7$ deg
 72 and 1000 prisms the relative error is $3 \cdot 10^{-4}$ for 4.9 \AA and $2 \cdot 10^{-2}$ for 20 \AA .
 73 The fraction of neutrons that do not hit the back of the next prism row is:

$$T_{Refl.} = 1 - \frac{\Delta_z}{h}. \quad (8)$$

74 For curved prism rows the expression changes to:

$$T_{Refl.} = 1 - \frac{|\Delta_z - x|}{h}, \quad (9)$$

75 where x is the deflection of the prism row due to the bending. For $|\Delta_z - x| > h$
 76 all neutrons are absorbed.

77 The whole transmission is the product of both effects:

$$T = T_{Refl.} \cdot T_{Abs.} \quad (10)$$

78 The function T is given in Fig. 2 for prism rows of 191 prisms which are bent
 79 to different curving radii.

80 3. Back coating

81 To check the effect of an absorbing coating the back of the prisms was
 82 coated with Gadolinium. The effect of this coating was determined at the
 83 V14 reflectometer at the HZB by measuring two energy analyzers, one with
 84 and one without an absorption layer. We used a 20 mm x 0.3 mm neutron
 85 beam with a wavelength of 4.9 \AA . With a ^3He detector in 2 m distance the
 86 refraction by a stack of 4 prism rows each with 191 Si prisms was measured,

87 see Fig. 3. For both systems the position of the maximum of the deflected
88 intensity at 0.12 deg relative to the incoming beam is in good agreement
89 with the theoretical value. The small difference between the positions of the
90 maxima of 0.005 deg is due to small differences in the mechanical setup. For
91 the uncoated prisms the total reflection and the refraction at small angles of
92 the neutrons leads to an increased background at negative angles, see Fig.3.
93 This background is eliminated by using the Gd coated prism rows. Absorbing
94 back coating is thus a means to clear up the signal by avoiding total reflection
95 and refraction at small angles.

96 4. Bending the prism stack

97 First we measured the effect of the bending at a fixed wavelength of 4.9 Å
98 at the V14 reflectometer. For this purpose an energy analyzer consisting of a
99 stack of 4 Gd coated prism rows each with 191 Si prisms in a simple mechan-
100 ical bender had been adjusted parallel to the 20 mm x 0.3 mm neutron beam.
101 The divergence of the beam was limited to 7 mdeg. A 3 mm slit was put
102 in front of the detector, which was located 2 m behind the energy analyzer.
103 Thus it covers an angular range of 0.08 deg. The detector angle was set to
104 0.12 deg according to the refraction by the prisms for the chosen wavelength.
105 Then the intensity of the refracted beam was measured for different bending
106 radii of the energy analyzer between 19.8 m and 42.9 m.

107 Without bending the device the transmission is about 71 %. Bending the en-
108 ergy analyzer to a radius of 42.9 m leads to an increase of transmission (see
109 Fig.4) to 86 %. The maximum transmission is 87 % and was found at a bend-
110 ing radius of 32.4 m, for which the total refraction angle of about 0.12 deg
111 equals the total bending angle of the prism rows. The intensity decreases
112 again for radii smaller than 25.0 m due to the increased number of neutrons
113 that hit the coated base sides of the prisms.

114 This maximum of transmission is in good agreement with the attenuation
115 in the pure material, which is 88 % for a material thickness of 3.8 cm and a
116 wavelength of 4.9 Å [7].

117 Since this agreement can only be achieved when the bending angle equals
118 the angle of refraction this effect is strongly chromatic. Therefore another
119 measurement with a white neutron beam was performed at the EROS reflec-
120 tometer at LLB to get the wavelength depending transmission of the bent
121 device. The bending radius of the prism stack was 7.9 m which corresponds
122 to a bending angle of 0.5 deg. With such a small bending radius according

123 to VITESS simulations a wavelength band between 4 Å and 14 Å should be
124 transmitted. A 20 mm x 0.3 mm neutron beam with a collimation of 0.01 deg
125 was used and the detector was set 2 m behind the energy analyzer.

126

127 Compared to the unbent energy analyzer where the wavelength spectrum
128 ends at 9 Å the measured spectrum of the bent device shows a shift to the
129 intervall between 2 Å and 15 Å. Fig. 5 shows the wavelength distribution of
130 the neutron intensity transmitted through the bent analyzer normalized to
131 the incoming one. The maximum of transmission is 77 % for 9 Å neutrons.
132 The theoretical value for the transmission in the pure material is 81.5 %.

133 5. Conclusion

134 Coating the back of the prism rows with an absorbing layer removes the
135 totally reflected and at small angles refracted neutrons from the spectrum of
136 the refracted neutron beam. Additional bending of the prism rows increases
137 the transmission for specific wavelength bands. For neutrons at the central
138 wavelength and without divergence the remaining losses are resulting only
139 from the attenuation in the material.

140 6. References

- 141 [1] F. Ott, A. Menelle, Eur. Phys. J. Special Topics 167, 93 (2009)
142 [2] F. Ott, A. de Vismes, Physica B 397, 153 (2007)
143 [3] R. Cubitt, et al., Nucl. Instrum. Meth. A 558, 547 (2006)
144 [4] R. Cubitt, et al., Eur. Phys. L Plus 126, 111 (2011)
145 [5] J. Schulz, et al., Nucl. Instrum. Meth. A accepted manuscript (2013)
146 [6] VITESS web site: [http://www.helmholtz-](http://www.helmholtz-berlin.de/forschung/grossgeraete/neutronenstreuung/projekte/vitess/index_de.html)
147 [berlin.de/forschung/grossgeraete/neutronenstreuung/projekte/vitess/index_de.html](http://www.helmholtz-berlin.de/forschung/grossgeraete/neutronenstreuung/projekte/vitess/index_de.html)
148 HZB (2012)
149 [7] A. W. Freund, Nucl. Instrum. Methods, 213, 495-501 (1983)

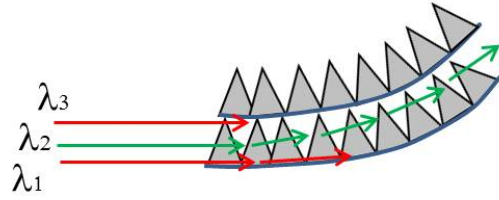


Figure 1: By bending the prism rows the transmission can be optimized for a wavelength band. Neutrons outside this wavelength band are removed by an absorbing coating at the back of the prisms.

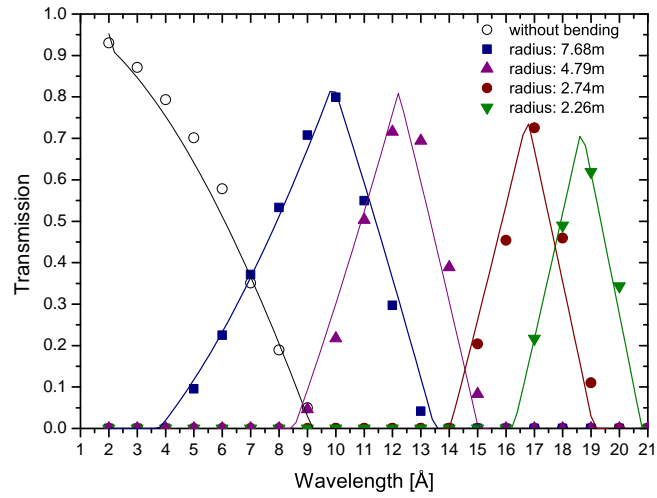


Figure 2: VITESS simulations (symbols) show that by bending prism rows with ^{191}Si prisms to smaller radii the transmitted wavelength band can be shifted to higher wavelengths. The curves are calculated with eq. 10.

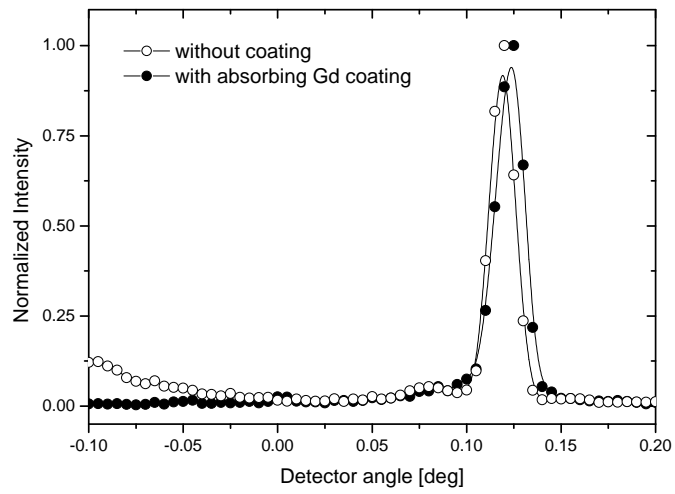


Figure 3: Measurement of the refraction of neutrons with a wavelength of 4.9 \AA by two energy analyzers consisting of 191 Si prisms, one with and one without an absorbing back coating. The intensity is normalized to the same maximum height of the intensity distribution due to the different experimental settings.

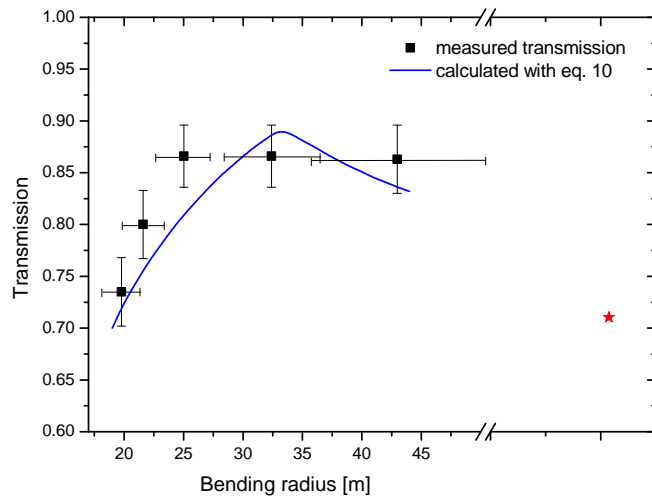


Figure 4: Measured and calculated transmission of neutrons with a wavelength of 4.9 \AA through an energy analyzer at different bending radii. At the maximum of transmission the bending angle of the prism rows equals the angle of refraction for ^{191}Si prisms. The measured transmission for the unbent energy analyzer is shown after the break in the x-axis as a red star.

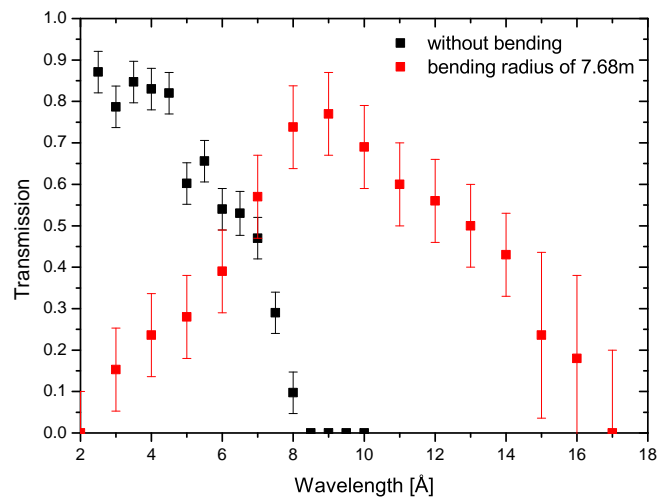


Figure 5: Measured wavelength depending transmission of a collimated white neutron beam through an analyzer without bending and with a bending radius of 7.9 m.