

1 High performance, large cross section S-bender for neutron polarization

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13 Abstract

14 An 80 mm long polarizing S-bender with a large cross section of 30 mm x 100 mm for the
15 instrument MIRA at the FRM II has been simulated, built and tested. The results of the
16 experiment show for the wavelength of 4.4 Å a homogenous polarization of more than 98%
17 across the bender cross section and a high transmission of above 65% of the spin up
18 component of the neutron beam. The bender design has the advantage of delivering the
19 polarized beam in the direction of the incoming beam.

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21 Keywords: Neutron polarizer, bender, S-shaped bender, supermirror

22

23 1. Introduction

24 The instrument MIRA [1] at the FRM II in Munich requires for several instrument options
25 like polarized small angle scattering, neutron reflection and quasi-elastic measurements with
26 the spin-echo method MIEZE [2,3] a highly polarized beam with a large beam cross section.
27 Due to the restricted space there are mainly two approaches to this goal: the ³He polarizing
28 gas cell [4] or a supermirror polarizer. The former has the advantage of providing a
29 homogenous polarization across the beam with very low small angle scattering while the main
30 disadvantage is the relative low transmission for a good polarization. A supermirror polarizer
31 provides a stable high polarization and a reasonable transmission but creates small angle
32 scattering at a significant order. Therefore the choice for a polarizer is the supermirror version
33 provided the instrument operates in the cold neutron range, while for an analyzer in small
34 angle scattering experiments the ³He polarizer is the preferred solution.

35 For MIRA additional requirements were to provide the polarized beam over the short distance
 36 of 8 cm and in the direction of the incoming beam. Three devices fulfilling these requirements
 37 were considered: the S-bender, a system of parallel V-shaped cavities (“V cavity”) and of
 38 cavities with two V cavities behind each other (“2V cavity”). The required wavelength range
 39 was 3 – 6 Å.

40 Monte-Carlo simulations were performed to compare these systems.

41

42 2. Simulations

43 McStas software [5] version 1.12c has been used to carry out simulations to investigate the
 44 performance of the three polarizing devices, each with a length of 8 cm. The cavities have
 45 purely absorbing walls. All other simulation parameters are shown in Table 1.

46

47 Table 1: Simulation parameters for the different polarizing devices for $m = 3$ supermirrors. d
 48 is the distance between the two V in the 2V cavity and r the radius of curvature of the S-
 49 bender.

	S-bender	V-cavity	2V-cavity
Length [mm]	80	80	80
d [mm]	-	-	20
r [mm]	2100	-	-
Wafer thickness [mm]	0.15	0.3	0.3
Channel width [mm]	0.15	3	3
Wafer angle to the walls	-	1.07°	1.43°
Absorbing wall width [mm]	-	0.3	0.3

50

51 For each of the three devices two different incoming angular and wavelength distributions
 52 were simulated to compare their angular acceptance: distributions at the end of a neutron
 53 guide behind the cold source of the Munich reactor coated with supermirrors with either
 54 $m=1.2$ or with $m=3$, where m is the multiple of the critical angle of natural Ni.

55 The value $m=1.2$ corresponds to the divergence distribution at the end of the neutron guide of
 56 MIRA. The value $m=3$ was chosen to show the transmission of the devices at the end of a
 57 neutron guide coated with $m=3$.

58 Figure 1 shows the simulated polarization for the three devices. The S-bender has for the
 59 wavelength range from 2 to 10 Å a very high polarization above 97.5%.

60 The cavities exhibit much worse polarizations values. They are very short and thus the angle
61 of the wafers is so large that a polarization above 95% is reached only for the small
62 divergence of $m=1.2$ and only at wavelengths above 7.5 \AA for the 2V cavity and 9.2 \AA for the
63 V cavity. For the large divergence of $m=3$ their polarization values stay below 70% (2V
64 cavity) and 60% (V cavity), even at 10 \AA . A smaller angle for the wafers would result in
65 smaller channel widths and increased absorption for the whole system which would lower the
66 quality factor (see below) as well.

67 The S-bender was found to clearly surpass the polarization of the two other devices in the
68 required wavelength range from 3 to 6 \AA .

69

70 **(Insert Figure 1 here)**

71

72 Figure 2 shows the simulated transmission values for the spin up component of the neutron
73 beam through the three devices, again for the two different divergence values. The cavities
74 show for wavelengths below 5 \AA a slightly larger transmission than the S-bender for the
75 $m=1.2$ divergence. For the $m=3$ divergence the same is true up to 3 \AA . However, the high
76 transmission of the cavities cannot be used since there the polarization is too small.

77

78 **(Insert Figure 2 here)**

79

80 The usefulness of a polarizer is often assessed by the quality factor $Q = P^2 * T_{up}/I_{up}$, where P
81 is the polarization of the transmitted beam and T_{up}/I_{up} the transmitted fraction of the spin up
82 component. Figure 3 shows the quality factor for the three devices, again for two different
83 divergence values. Here the S-bender shows the largest quality factors for all wavelengths;
84 especially for the large incoming divergence its performance is much better.

85 In conclusion, we found a clear advantage of the S-shaped bender over the other considered
86 systems. The tests of such a system, supplied by the company NOB, are described below.

87

88 **(Insert Figure 3 here)**

89

90

91 **3. The working principle of an S-bender**

92 An S-bender consists of a set of parallel S-shaped channels which are coated on both sides
93 first with a polarizing and then with an absorbing layer. A proof-of-principle was realized at
94 the ILL by Stunault et al. using a bender prototype with a cross section of 6 mm x 70 mm [6].
95 The system we report on here has a cross section of 30 mm x 100 mm and channels formed by
96 0.15 mm thick silicon wafers in which the neutrons propagate. The polarizing coating is
97 realized by Fe-Si supermirrors with $m=3$ which reflect only the spin up component of the
98 neutron beam. The supermirrors are magnetically saturated by permanent magnets creating a
99 field of 300 G. The absorbing coating is made from Gd and absorbs the unwanted spin down
100 state, which is transmitted through the supermirrors.

101 It is an important feature of the S-bender that the average direction of the transmitted
102 polarized beam is in the same direction as the incoming beam. This is advantageous compared
103 to a bender which deflects the beam and thus requires a readjustment of the instrument when
104 the polarizer is inserted. The conservation of the average flight direction is a result of
105 typically two reflections of the neutrons inside the S-bender. Simulations show that these
106 most often occur at a large and a small angle between neutron flight path and supermirror.
107 This results in a very high reflectivity for the low angle reflection. Furthermore the two
108 reflections lead to a multiplication of the flipping ratios and thus result in very high
109 polarization values.

110

111 **4. Polarization measurements**

112 First the S-Bender was adjusted at the instrument MIRA with the bender mounted at the
113 sample table of the instrument. A beam with the wavelength of 4.4 Å and a cross section of 5
114 x 5 mm² collimated to 0.5° hit the middle of the polarizer and was analyzed by a ³He polarizer
115 (99.9% polarization with 10% transmission) before being detected with a CSACADE 20 x 20
116 cm² boron GEM detector [7]. The polarizer bending was adjusted during a series of rocking
117 scans of the bender where the transmitted intensities of the two spin components were
118 measured. The transmission of the polarizer was determined from a comparison to the empty
119 beam. These values were determined at 12 positions across the polarizer showing a good
120 homogeneity of the system to within 6% in transmitted intensity and 0.4% in polarization.
121 The axes of incoming and transmitted beam coincided within less than 0.1°.

122 Figure 4 shows a rocking curve of the S-Bender in the beam, giving the values for the
123 transmitted spin up and spin down neutron beam intensities T_{up} and T_{down} together with the
124 flipping ratio $FR = T_{up}/T_{down}$, the polarization $P = (FR - 1)/(FR + 1)$ and the quality factor Q .
125 Due to the high polarization of the ³He cell no corrections were applied to the incoming

126 polarization. Background corrections were made due to detector noise in the order of 1% of
127 the direct beam.

128

129 **(Insert Figure 4 here)**

130

131 Polarization values above 98.7% at all angles where the transmission values were above 6%
132 of the spin up component indicate the excellent polarization capability of the S-bender. The
133 total transmission values were between 67% and 70% depending on the size of the beam.

134 The linear absorption length for neutrons at the wavelength of 4.4 Å is $\mu_1=0.03 \text{ cm}^{-1}$ [8] and
135 gives a transmission of 78.7% through 80 mm Si. Hence the losses due to incomplete
136 reflection at the supermirrors are in the order of 10%.

137 The FWHM amounts to 1.85° which corresponds to an m-value of ± 2.1 for the wavelength of
138 4.4 Å. Within this FWHM the average transmitted intensity is 58%, the average quality factor
139 is 57%.

140 Figure 5 shows a comparison of the experimental values to a simulation. The simulated
141 intensity reaches 70% in the maximum and is for all angles a few percent higher than the
142 experimental values. It should be noted that the simulated maximum value shown here is
143 higher than that in Figure 2. This is due to different incoming divergence values. In the
144 simulations for Figure 2 the full divergence at the end of a neutron guide with a nearly
145 rectangular distribution was used because the polarizing device will be applied at this
146 position. The experiment and the corresponding simulation were done with two slits which
147 transmit a triangular distribution. This favors angles close to 0° which have a higher
148 transmission probability through the S-bender.

149 The flipping ratio in the simulation is for most angles higher than in the experiment except for
150 a small dip below the experimental values in the interval from -0.4° to -0.9° . This is due to the
151 model for the spin down reflectivity, which uses the simulated reflectivity of the spin down
152 component of a neutron moving through Si and hitting a thick Fe layer. Obviously, this
153 underestimates the real reflectivity and thus only a qualitative agreement could be reached.

154

155 **(Insert Figure 5 here)**

156

157 After adjustment the polarizer was installed at the exit of the monochromator shielding of
158 MIRA. A black ^3He cell was used as analyzer to determine the total polarization of the beam.

159 At the same wavelength of 4.4 Å and the same set of slits, which were used for the
160 experiments, we found a transmission of the spin up component of the neutron beam of 68%
161 ±2% and a flipping ratio of 150 ±10.

162

163 **5. Conclusion**

164 The tested solid state S-bender with a length of 80 mm showed for neutrons with the
165 wavelength of 4.4 Å polarization values above 98.7%. The maximum transmission value was
166 above 65%, the average value within the FWHM 58% of the incoming spin up intensity. The
167 quality factor for the spin up component $P^2 \cdot T$ was 68% in the maximum, the average value
168 within the FWHM 57%. The polarized beam is delivered in the direction of the incoming
169 beam and the system is maintenance free. With these excellent features an S-bender can be
170 used to polarize and analyze cold neutrons beams in a broad range of applications.

171

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185

186 **Figure Captions:**

187

188 Figure 1: Simulated polarization performance of the three devices: S-bender (S), 2V-cavity
189 (2V) and V-cavity (V), each for two incoming divergence values of $m=3$ and $m=1.2$.

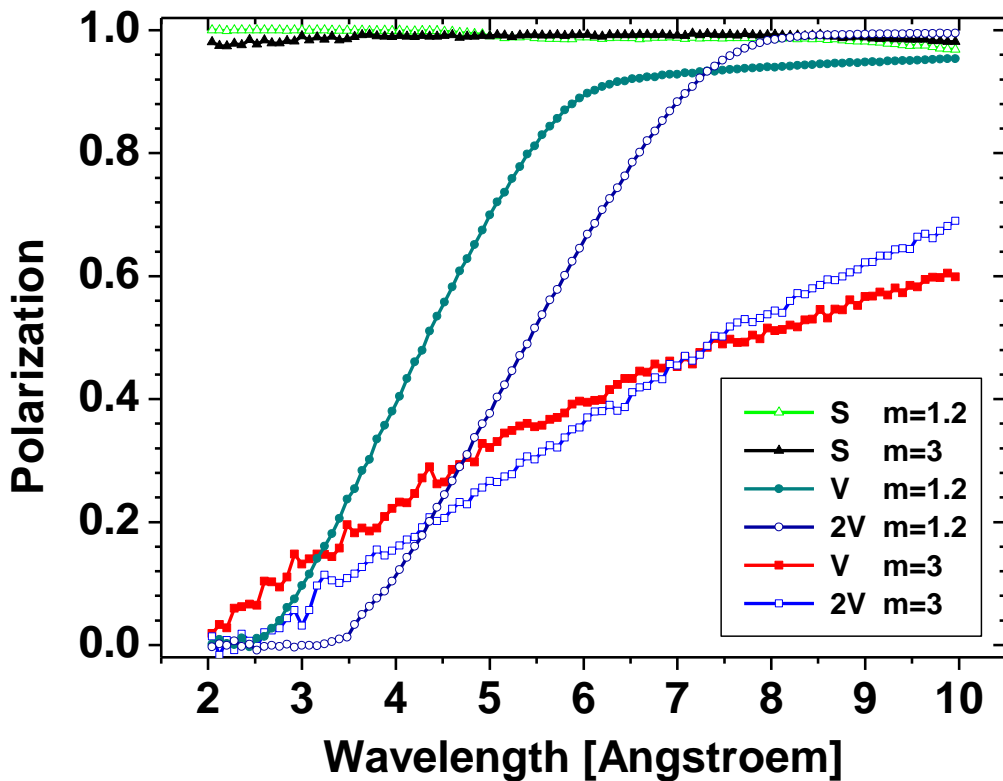
190 Figure 2: Simulated transmission of the spin up component through the three devices: S-
191 bender (S), 2V-cavity (2V) and V-cavity (V), each for two incoming divergence values of
192 $m=3$ and $m=1.2$.

193 Figure 3 Simulated quality factor $Q = P^2 * T_{up}/I_{up}$, where P is the polarization of the
194 transmitted beam and T_{up}/I_{up} the transmitted fraction of the spin up component for the three
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196 values of $m=3$ and $m=1.2$.

197 Figure 4 Experimental transmission through the S-bender of the two spin components of a
198 neutron beam with the wavelength of 4.4 \AA together with the quality factor Q, the polarization
199 P and the flipping ratio FR.

200 Figure 5 Comparison of experimental, Exp_{up} , Exp_{down} , and simulated, Sim_{up} , Sim_{down} ,
201 transmission values for the two spin components of a neutron beam with the wavelength of
202 4.4 \AA through the S-bender together with the flipping ratios FR_{exp} , FR_{sim} . Experimental values
203 as in Figure 4.

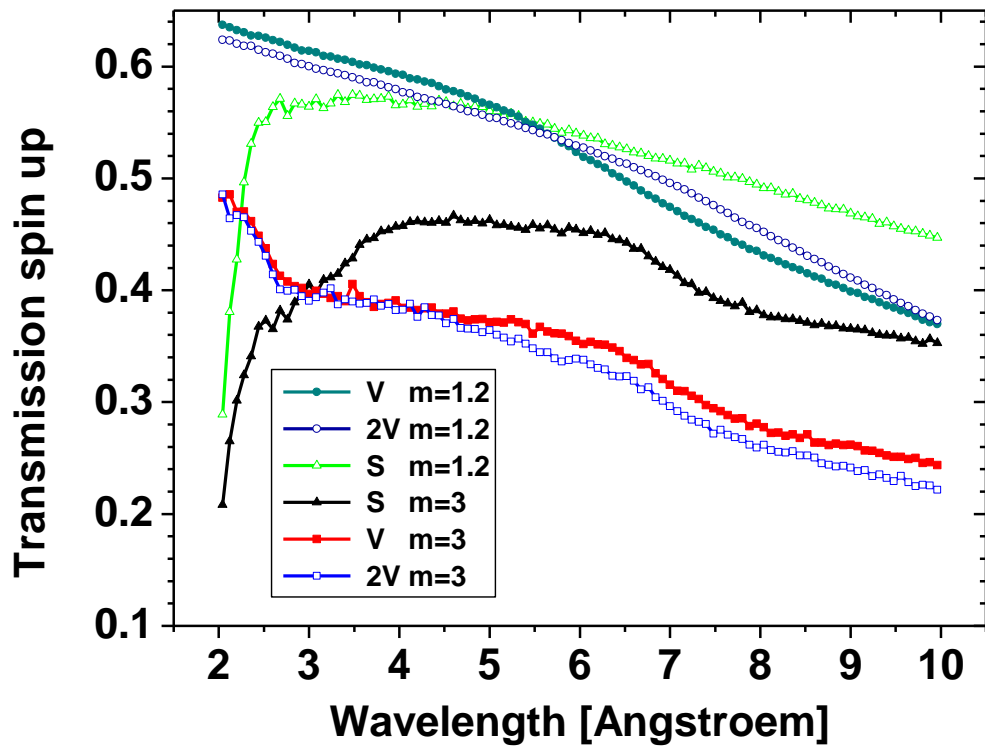
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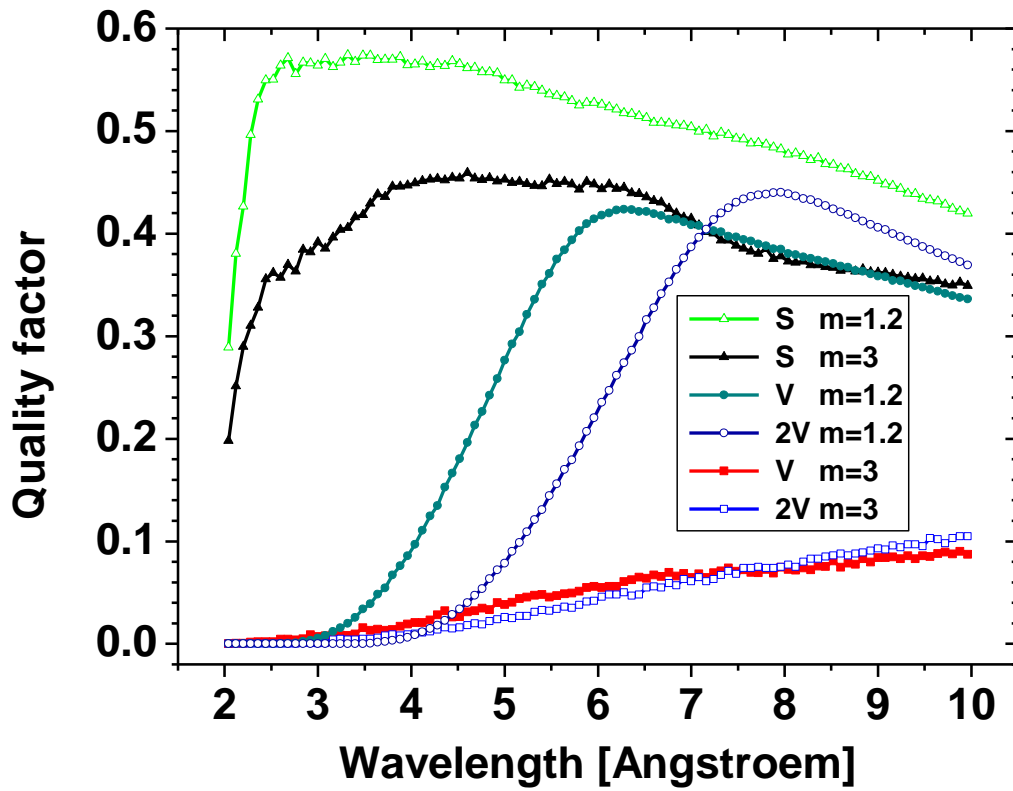


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 212 bender (S), 2V-cavity (2V) and V-cavity (V), each for two incoming divergence values of
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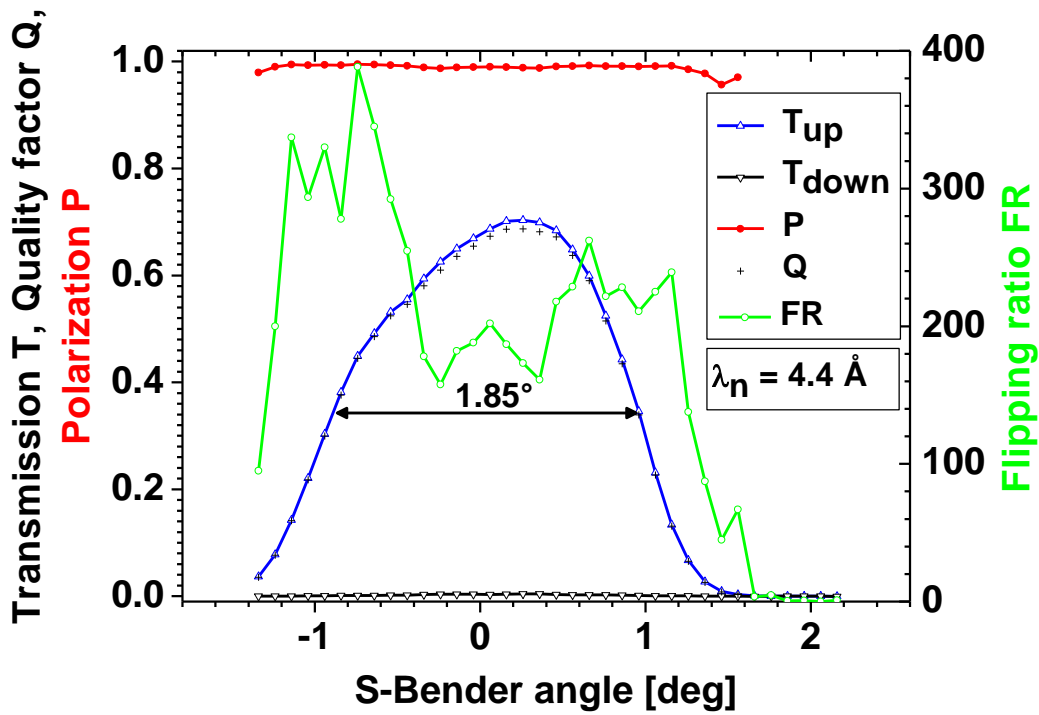
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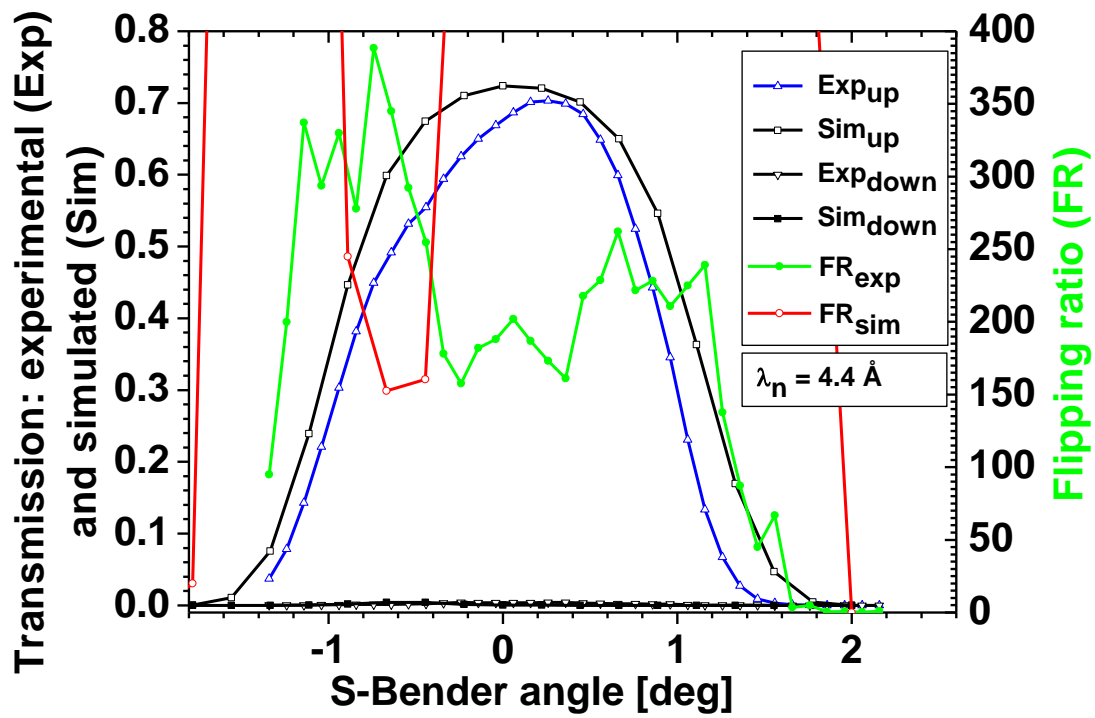
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