

Estimation of Reliability Parameters of a Complex Repairable System

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Abstract:-In this paper estimation of reliability parameters of a complex repairable system is considered and semi-markov process is used in analyzing various reliability parameters such as Transition Probabilities, Mean sojourn times, MTSF, Availability and Busy period of repairman in repairing the failed units. In the past, Arora et-al[2] has done reliability analysis of two unit standby redundant system with constrained repair time. Gupta et-al [6] has worked on a compound redundant system involving human failure. Rander et-al [2] has evaluated the cost analysis of two dissimilar cold standby systems with preventive maintenance and replacement of standby units. A pioneer work in this field was done by Gopalan [1] and Osaki [3] by performing analysis of warm standby system and parallel system with bivariate exponential life respectively. Earlier, Pathak et al [7&8] studied reliability parameters of a main unit with its supporting units and also compared the results with two different distributions. In this paper, Chapman-Kolmogorov equations are used to develop recursive relations. Also the involvement of preventive maintenance in the model increases the reliability of the functioning units. In the end a particular case is also taken for discussion.

Keywords: Regenerative Point, MTSF, Availability, Busy Period Subject Classification: 53A04, 53A05

System Description about the model:

The system consists of three units namely one main unit A and two associate units B & C. Here the associate unit B and C depends upon main units A and the system is operable when the main unit and at least one associate unit is in operable. Main unit are employed to rotate B and C. As soon as a job arrives, all the units work with load. It is assumed that only one job is taken for processing at a time. There is a single repairman who repairs the failed units on first come first served basis. Using regenerative point technique several system characteristics such as transition probabilities, mean sojourn times, availability and busy period of the repairman are evaluated. In the end the expected profit is also calculated.

Assumptions used in the model:

- a. The system consists of one main unit and two associate units.
- b. The associate unit A and B works with the help of main units.
- c. There is a single repairman which repairs the failed units on priority basis.
- d. After random period of time the whole system goes to preventive maintenance.
- e. All units work as new after repair.
- f. The failure rates of all the units are taken to be exponential whereas the repair time distributions are arbitrary.
- g. Switching devices are perfect and instantaneous.

Symbols and Notations:

$p_{i,j}$ = Transition probabilities from S_i to S_j

μ_i = Mean sojourn time at time t

E_0 = State of the system at epoch t=0

E=set of regenerative states

$q_{i,j}(t)$ = Probability density function of transition time from S_i to S_j

$Q_{i,j}(t)$ = Cumulative distribution function of transition time from S_i to S_j

$\pi_i(t)$ = Cdf of time to system failure when starting from state $E_0 = S_i \in E$

$\mu_i(t)$ = Mean Sojourn time in the state $E_0 = S_i \in E$

$B_i(t)$ = Repairman is busy in the repair at time t / $E_0 = S_i \in E$

$r_1 / r_2 / r_3 / r_4$ = Constant repair rate of Main unit A / Unit B / Unit C / Unit A&B or A&C

$\alpha / \beta / \gamma$ = Failure rate of Main unit A / Unit B / Unit C

$g_1 / g_2 / g_3 / g_4$ =Probability density function of repair time of Main unit A/Unit B/Unit C/Unit A&B or A&C

$\bar{G}_1 / \bar{G}_2 / \bar{G}_3 / \bar{G}_4$ =Cumulative distribution function of repair time of Main unit A/Unit B/Unit C/Unit A&B or A&C

$a(t)$ = Probability density function of preventive maintenance .

$b(t)$ = Probability density function of preventive maintenance completion time.

$\bar{A}(t)$ = Cumulative distribution functions of preventive maintenance.

$\bar{B}(t)$ = Cumulative distribution functions of preventive maintenance completion time.

\boxed{s} = Symbol for Laplace -stieltjes transforms.

\boxed{c} = Symbol for Laplace-convolution.

Symbols used for states of the system:

$A_0 / A_g / A_r$ -- Main unit ‘A’ under operation/good and non-operative mode/ repair mode

$B_0 / B_r / B_g$ -- Associate Unit ‘B’ under operation/repair/ good and non-operative mode

$C_0 / C_r / C_g$ -- Associate Unit ‘C’ under operation/repair/good and non-operative mode

P.M. -- System under preventive maintenance.

Up states: $S_0 = (A_0, B_0, C_0); S_2 = (A_0, B_r, C_0); S_3 = (A_0, B_0, C_r)$

Down States: $S_1 = (A_r, B_o, C_o); S_4 = (S.D.); S_5 = (P.M.)$

Transition Probabilities:

Simple probabilistic considerations yield the following non-zero transition probabilities:

1. $Q_{01}(t) = \int_0^t \alpha e^{-(\alpha+\beta+\gamma)t} \bar{A}(t) dt$

2. $Q_{02}(t) = \int_0^t \beta e^{-(\alpha+\beta+\gamma)t} \bar{A}(t) dt$

3. $Q_{03}(t) = \int_0^t \gamma e^{-(\alpha+\beta+\gamma)t} \bar{A}(t) dt$

4. $Q_{10}(t) = \int_0^t g_1(t) dt$

5. $Q_{20}(t) = \int_0^t e^{-(\alpha+\gamma)t} g_2(t) dt$

6. $Q_{24}(t) = \int_0^t (\alpha + \gamma) e^{-(\alpha+\gamma)t} \bar{G}_2(t) dt$

7. $Q_{30}(t) = \int_0^t e^{-(\alpha+\beta)t} g_3(t) dt$

8. $Q_{34}(t) = \int_0^t (\alpha + \beta) e^{-(\alpha+\beta)t} \bar{G}_2(t) dt$

9. $Q_{40}(t) = \int_0^t g_4(t) dt$

10. $Q_{50}(t) = \int_0^t b(t) dt$

11. $Q_{05}(t) = \int_0^t a(t) e^{-(\alpha+\beta+\gamma)t} dt$

Where $x_1 = \alpha + \beta + \gamma$, Now letting $t \rightarrow \infty$, we get $\lim_{t \rightarrow \infty} Q_{ij}(t) = p_{ij}$

12. $p_{01} = \int_0^\infty \alpha e^{-(\alpha+\beta+\gamma)t} \bar{A}(t) dt = \frac{\alpha}{x_1} [1 - a^*(x_1)]$, 13. $p_{02} = \int_0^\infty \beta e^{-(\alpha+\beta+\gamma)t} \bar{A}(t) dt = \frac{\beta}{x_1} [1 - a^*(x_1)]$

14. $p_{03} = \int_0^\infty \gamma e^{-(\alpha+\beta+\gamma)t} \bar{A}(t) dt = \frac{\gamma}{x_1} [1 - a^*(x_1)]$, 15. $p_{05} = \int_0^\infty a(t) e^{-(\alpha+\beta+\gamma)t} dt = a^*(x_1)$

16. $p_{10} = \int_0^\infty g_1(t) dt = 1$

17. $p_{20} = \int_0^\infty e^{-(\alpha+\gamma)t} g_2(t) dt = g_2^*(\alpha + \gamma)$

$$18. p_{24} = \int_0^{\infty} (\alpha + \gamma) e^{-(\alpha+\gamma)t} \bar{G}_2(t) dt = 1 - g_2^*(\alpha + \gamma) \quad 19. p_{30}(t) = \int_0^{\infty} e^{-(\alpha+\beta)t} g_3(t) dt = g_3^*(\alpha + \beta)$$

$$20. p_{34}(t) = \int_0^{\infty} (\alpha + \beta) e^{-(\alpha+\beta)t} \bar{G}_3(t) dt = 1 - g_3^*(\alpha + \beta)$$

$$21. p_{40}(t) = \int_0^{\infty} g_4(t) dt = 1$$

$$22. p_{50}(t) = \int_0^{\infty} b(t) dt = 1$$

$$23. p_{10} = p_{40} = p_{50} = 1$$

[6.1-6.23]

It is easy to see that

$$p_{01} + p_{02} + p_{03} + p_{05} = 1, \quad p_{20} + p_{24} = 1, \quad p_{30} + p_{34} = 1$$

[6.24-6.26]

And mean sojourn time are given by

$$27. \mu_0 = \frac{1}{x_1} [1 - a^*(x_1)], \quad 28. \mu_1 = \int_0^{\infty} \bar{G}_1(t) dt,$$

$$29. \mu_2 = \frac{1}{\alpha + \gamma} [1 - g_2^*(\alpha + \gamma)], \quad 30. \mu_3 = \frac{1}{\alpha + \beta} [1 - g_3^*(\alpha + \beta)]$$

$$31. \mu_4 = \int_0^{\infty} \bar{G}_4(t) dt$$

$$32. \mu_5 = \int_0^{\infty} \bar{B}(t) dt$$

[6.27-6.32]

We note that the Laplace-stieltjes transform of $Q_{ij}(t)$ is equal to Laplace transform of $q_{ij}(t)$ i.e.

$$\tilde{Q}_{ij}(s) = \int_0^{\infty} e^{-st} Q_{ij}(t) dt = L\{Q_{ij}(t)\} = q_{ij}^*(s)$$

[6.33]

$$34. \tilde{Q}_{01}(s) = \int_0^{\infty} \alpha e^{-(s+x_1)t} \bar{A}(t) dt = \frac{\alpha}{s + x_1} [1 - a^*(s + x_1)]$$

$$35. \tilde{Q}_{02}(s) = \int_0^{\infty} \beta e^{-(s+x_1)t} \bar{A}(t) dt = \frac{\beta}{s + x_1} [1 - a^*(s + x_1)]$$

$$36. \tilde{Q}_{03}(s) = \int_0^{\infty} \gamma e^{-(s+x_1)t} \bar{A}(t) dt = \frac{\gamma}{s + x_1} [1 - a^*(s + x_1)]$$

$$37. \tilde{Q}_{05}(s) = \int_0^{\infty} e^{-(s+x_1)t} a(t) dt = a^*(s + x_1)$$

$$38. \tilde{Q}_{10}(s) = \int_0^{\infty} e^{-st} g_1(t) dt = g_1^*(s)$$

$$39. \tilde{Q}_{20}(s) = \int_0^{\infty} e^{-(s+\alpha+\gamma)t} g_2(t) dt = g_2^*(s + \alpha + \gamma)$$

$$40. \tilde{Q}_{24}(s) = \int_0^{\infty} (\alpha + \gamma) e^{-(s+\alpha+\gamma)t} \bar{G}_2(t) dt = \frac{(\alpha + \gamma)}{s + \alpha + \gamma} [1 - g_2^*(s + \alpha + \gamma)]$$

$$41. \tilde{Q}_{30}(s) = \int_0^{\infty} e^{-(s+\alpha+\beta)t} g_3(t) dt = g_3^*(s + \alpha + \beta)$$

$$42. \tilde{Q}_{34}(s) = \int_0^{\infty} (\alpha + \beta) e^{-(s+\alpha+\beta)t} \bar{G}_3(t) dt = \frac{(\alpha + \beta)}{s + \alpha + \beta} [1 - g_3^*(s + \alpha + \beta)]$$

$$43. \tilde{Q}_{40}(s) = \int_0^{\infty} e^{-st} g_4(t) dt = g_4^*(s)$$

$$44. \tilde{Q}_{50}(s) = \int_0^{\infty} e^{-st} b(t) dt = b^*(s)$$

[6.34-6.44]

We define $m_{i,j}$ as follows:-

$$m_{i,j} = -\left[\frac{d}{ds} \tilde{Q}_{i,j}(s)\right]_{s=0} = -Q_{i,j}'(0) \tag{6.45}$$

It can to show that $m_{01} + m_{02} + m_{03} + m_{05} = \mu_0; m_{20} + m_{24} = \mu_2; m_{30} + m_{34} = \mu_3$

$$\text{Where } \alpha + \beta + \gamma = x_1 \tag{6.46-6.49}$$

7. Mean time to System failure-

Time to system failure can be regarded as the first passage time to the failed state. To obtain it we regard the down state as absorbing. Using the argument as for the regenerative process, we obtain the following recursive relations.

$$\begin{aligned} \pi_0(t) &= Q_{01}(t) + Q_{02}(t) \boxed{s} \pi_2(t) + Q_{03}(t) \boxed{s} \pi_3(t) + Q_{05}(t) \\ \pi_2(t) &= Q_{20}(t) \boxed{s} \pi_0(t) + Q_{24}(t) \\ \pi_3(t) &= Q_{30}(t) \boxed{s} \pi_0(t) + Q_{34}(t) \end{aligned} \tag{7.1-7.3}$$

Taking Laplace -stieltjes transform of above equations and writing in matrix form.

We get

$$\begin{bmatrix} 1 & -\tilde{Q}_{02} & -\tilde{Q}_{03} \\ -\tilde{Q}_{20} & 1 & 0 \\ -\tilde{Q}_{30} & 0 & 1 \end{bmatrix} \begin{bmatrix} \pi_0 \\ \pi_2 \\ \pi_3 \end{bmatrix} = \begin{bmatrix} \tilde{Q}_{01} + \tilde{Q}_{05} \\ \tilde{Q}_{24} \\ \tilde{Q}_{34} \end{bmatrix}$$

$$D_1(s) = \begin{vmatrix} 1 & -\tilde{Q}_{02} & -\tilde{Q}_{03} \\ -\tilde{Q}_{20} & 1 & 0 \\ -\tilde{Q}_{30} & 0 & 1 \end{vmatrix} = 1 - \tilde{Q}_{20}\tilde{Q}_{02} - \tilde{Q}_{03}\tilde{Q}_{30} \tag{7.4}$$

$$\text{And } N_1(s) = \begin{vmatrix} \tilde{Q}_{01} + \tilde{Q}_{05} & -\tilde{Q}_{02} & -\tilde{Q}_{03} \\ \tilde{Q}_{24} & 1 & 0 \\ \tilde{Q}_{34} & 0 & 1 \end{vmatrix} = (\tilde{Q}_{01} + \tilde{Q}_{05} + \tilde{Q}_{02}\tilde{Q}_{24} + \tilde{Q}_{03}\tilde{Q}_{34})$$

Now letting $s \rightarrow 0$ we get

[7.5]

$$D_1(0) = 1 - p_{02}p_{20} - p_{03}p_{30} \tag{7.6}$$

The mean time to system failure when the system starts from the state S_0 is given by

$$\text{MTSF} = E(T) = -\left[\frac{d}{ds} \tilde{\pi}_0(s)\right]_{s=0} = \frac{D_1'(0) - N_1'(0)}{D_1(0)} \tag{7.7}$$

To obtain the numerator of the above equation, we collect the coefficients of relevant of $m_{i,j}$ in $D_1'(0) - N_1'(0)$.

Coeff. of $(m_{01} = m_{02} = m_{03} = m_{05}) = 1$

Coeff. of $(m_{20}) = p_{02}$

Coeff. of $(m_{30} = m_{34}) = p_{03}$

[7.8-7.10]

From equation [7.7]

$$MTSF = E(T) = -\left[\frac{d}{ds} \tilde{\pi}_0(s)\right]_{s=0} = \frac{D_1'(0) - N_1'(0)}{D_1(0)} = \frac{\mu_0 + \mu_2 P_{02} + \mu_3 P_{03}}{1 - P_{02} P_{20} - P_{03} P_{30}}$$

[7.11]

8. Availability Analysis:

Let $M_i(t) (i = 0, 1, 2)$ denote the probability that system is initially in regenerative state $S_i \in E$ is up at time t without passing through any other regenerative state or returning to itself through one or more non regenerative states .i.e. either it continues to remain in regenerative S_i or a non regenerative state including itself . By probabilistic arguments, we have the following recursive relations

$$M_0(t) = e^{-(\alpha+\beta+\gamma)t} \bar{A}(t), \quad M_2(t) = e^{-(\alpha+\beta)t} \bar{G}_2(t), \quad M_3(t) = e^{-(\alpha+\gamma)t} \bar{G}_3(t),$$

[8.1-8.2]

Recursive relations giving point wise availability $A_i(t)$ given as follows:

$$\begin{aligned} A_0(t) &= M_0(t) + \sum_{i=1,2,3,5} q_{0i}(t) \boxed{c} A_i(t) ; & A_1(t) &= q_{10}(t) \boxed{c} A_0(t) ; \\ A_2(t) &= M_2(t) + \sum_{i=0,4} q_{2i}(t) \boxed{c} A_i(t) ; & A_3(t) &= M_3(t) + \sum_{i=0,4} q_{3i}(t) \boxed{c} A_i(t) ; \\ A_4(t) &= q_{40}(t) \boxed{c} A_0(t) ; & A_5(t) &= q_{50}(t) \boxed{c} A_0(t) ; \end{aligned}$$

[8.3-8.8]

Taking Laplace stieltjes transformation of above equations; and writing in matrix form, we get

$$q_{6 \times 6} [A_0^*, A_1^*, A_2^*, A_3^*, A_4^*, A_5^*]' = [M_0^*, 0, M_2^*, M_3^*, 0, 0]' \tag{8.9}$$

Where $q_{6 \times 6} = \begin{bmatrix} 1 & -q_{01}^* & -q_{02} & -q_{03}^* & 0 & -q_{05}^* \\ -q_{10}^* & 1 & 0 & 0 & 0 & 0 \\ -q_{20} & 0 & 1 & 0 & -q_{24}^* & 0 \\ -q_{30}^* & 0 & 0 & 1 & -q_{34}^* & 0 \\ -q_{40} & 0 & 0 & 0 & 1 & 0 \\ -q_{50}^* & 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{6 \times 6}$

Therefore $D_2(s) = \begin{bmatrix} 1 & -q_{01}^* & -q_{02} & -q_{03}^* & 0 & -q_{05}^* \\ -q_{10}^* & 1 & 0 & 0 & 0 & 0 \\ -q_{20} & 0 & 1 & 0 & -q_{24}^* & 0 \\ -q_{30}^* & 0 & 0 & 1 & -q_{34}^* & 0 \\ -q_{40} & 0 & 0 & 0 & 1 & 0 \\ -q_{50}^* & 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{6 \times 6}$

$$= 1 - q_{01}^* q_{10}^* - q_{02}^* (q_{20}^* + q_{24}^* q_{40}^*) - q_{03}^* (q_{30}^* + q_{34}^* q_{40}^*) - q_{05}^* q_{50}^*$$

If $s \rightarrow 0$ we get $D_2(0) = 0$ which is true [8.10]

$$\text{Now } N_2(s) = \begin{bmatrix} M_0^* & -q_{01}^* & -q_{02} & -q_{03}^* & 0 & -q_{05}^* \\ 0 & 1 & 0 & 0 & 0 & 0 \\ M_2^* & 0 & 1 & 0 & -q_{24}^* & 0 \\ M_3^* & 0 & 0 & 1 & -q_{34}^* & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{6 \times 6}$$

Solving this Determinant, we get

$$N_2(s) = M_0^* + M_2^* q_{02}^* + M_3^* q_{03}^* \quad [8.11]$$

If $s \rightarrow 0$ we get

$$N_2(0) = \mu_0 + \mu_2 p_{02} + \mu_3 p_{03} \quad [8.12]$$

To find the value of $D_2'(0)$ we collect the coefficient m_{ij} in $D_2(s)$ we get

$$\text{Coeff. of } (m_{01} = m_{02} = m_{03} = m_{05}) = 1 = L_0$$

$$\text{Coeff. of } (m_{10}) = p_{01} = L_1 \quad \text{Coeff. of } (m_{20} = m_{24}) = p_{02} = L_2$$

$$\text{Coeff. of } (m_{30} = m_{34}) = p_{03} = L_3 \quad \text{Coeff. of } m_{40} = p_{03} p_{34} + p_{03} p_{34} = L_4$$

$$\text{Coeff. of } m_{50} = p_{05} = L_5 \quad [8.13-8.18]$$

Thus the solution for the steady-state availability is given by

$$A_0^*(\infty) = \lim_{t \rightarrow \infty} A_0^*(t) = \lim_{s \rightarrow 0} s A_0^*(s) = \frac{N_2(0)}{D_2'(0)} = \frac{\mu_0 L_0 + \mu_2 L_2 + \mu_3 L_3}{\sum_{i=0,1,2,3,4,5} \mu_i L_i}$$

[8.19]

9. BUSY PERIOD ANALYSIS:

(a) Let $W_i(t)$ ($i = 1,2,3,4,5,6$) denote the probability that the repairman is busy initially with repair in regenerative state S_i and remain busy at epoch t without transiting to any other state or returning to itself through one or more regenerative states.

By probabilistic arguments we have

$$W_1(t) = \bar{G}_1(t), W_2(t) = \bar{G}_2(t), W_3(t) = \bar{G}_3(t) \quad [9.1-$$

9.3]

Developing similar recursive relations as in availability, we have

$$\begin{aligned} B_0(t) &= \sum_{i=1,2,3,5} q_{0i}(t) \boxed{c} B_i(t) & ; & \quad B_1(t) = W_1(t) + q_{10}(t) \boxed{c} B_0(t) ; \\ B_2(t) &= W_2(t) + \sum_{i=0,4} q_{2i}(t) \boxed{c} B_i(t) & ; & \quad B_3(t) = W_3(t) + \sum_{i=0,4} q_{3i}(t) \boxed{c} B_i(t) ; \\ B_4(t) &= q_{40}(t) \boxed{c} B_0(t) & ; & \quad B_5(t) = q_{50}(t) \boxed{c} B_0(t) ; \end{aligned}$$

[9.4-9.9]

Taking Laplace stieltjes transformation of above equations; and writing in matrix form, we get

$$q_{6 \times 6} [B_0^*, B_1^*, B_2^*, B_3^*, B_4^*, B_5^*]' = [0, W_1^*, W_2^*, W_3^*, 0, 0]' \quad [9.10]$$

Where $q_{6 \times 6}$ is denoted by [8.9] and therefore $D_2'(s)$ is obtained as in the expression of availability.

$$\text{Now } N_3(s) = \begin{bmatrix} 0 & -q_{01}^* & -q_{02} & -q_{03}^* & 0 & -q_{05}^* \\ W_1^* & 1 & 0 & 0 & 0 & 0 \\ W_2^* & 0 & 1 & 0 & -q_{24}^* & 0 \\ W_3^* & 0 & 0 & 1 & -q_{34}^* & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{6 \times 6}$$

Solving this Determinant, In the long run, we get the value of this determinant after putting $s \rightarrow 0$ is

$$\begin{aligned} N_3(0) &= (\mu_1 p_{01} + \mu_2 p_{02} + \mu_3 p_{03}) \\ &= \mu_1 L_1 + \mu_2 L_2 + \mu_3 L_3 = \sum_{i=1,2,3} \mu_i L_i \end{aligned} \quad [9.11]$$

Thus the fraction of time for which the repairman is busy with repair of the failed unit is given by:

$$B_0^{1*}(\infty) = \lim_{t \rightarrow \infty} B_0^{1*}(t) = \lim_{s \rightarrow 0} s B_0^{1*}(s) = \frac{N_3(0)}{D_2'(0)} = \frac{\sum_{i=1,2,3} \mu_i L_i}{\sum_{i=0,1,2,3,4,5} \mu_i L_i}$$

[9.12]

(b) Busy period of the Repairman in preventive maintenance in time (0, t], By probabilistic arguments we have

$$W_5(t) = \bar{B}(t) \quad [9.13]$$

Similarly developing similar recursive relations as in 9(a), we have

$$\begin{aligned} B_0(t) &= \sum_{i=1,2,3,5} q_{0i}(t) \boxed{c} B_i(t) & ; & & B_1(t) &= q_{10}(t) \boxed{c} B_0(t) & ; \\ B_2(t) &= \sum_{i=0,4} q_{2i}(t) \boxed{c} B_i(t) & ; & & B_3(t) &= \sum_{i=0,4} q_{3i}(t) \boxed{c} B_i(t) & ; \\ B_4(t) &= q_{40}(t) \boxed{c} B_0(t) & ; & & B_5(t) &= W_5(t) + q_{50}(t) \boxed{c}(t) & ; \end{aligned}$$

[9.14-9.19]

Taking Laplace stieltjes transformation of above equations; and writing in matrix form, we get

$$q_{6 \times 6} [B_0^*, B_1^*, B_2^*, B_3^*, B_4^*, B_5^*]' = [0, 0, 0, 0, 0, W_5^*]'$$

Where $q_{6 \times 6}$ is denoted by [8.9] and therefore $D_2'(s)$ is obtained as in the expression of availability.

$$\text{Now } N_4(s) = \begin{bmatrix} 0 & -q_{01}^* & -q_{02} & -q_{03}^* & 0 & -q_{05}^* \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & -q_{24}^* & 0 \\ 0^* & 0 & 0 & 1 & -q_{34}^* & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ W_5^* & 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{6 \times 6}$$

Solving this Determinant, In the long run, we get the value of this determinant after putting $s \rightarrow 0$ is

$$N_4(0) = \mu_5 p_{05} = \mu_5 L_5$$

[9.20]

Thus the fraction of time for which the system is under preventive maintenance is given by:

$$B_0^{2*}(\infty) = \lim_{t \rightarrow \infty} B_0^{2*}(t) = \lim_{s \rightarrow 0} s B_0^{2*}(s) = \frac{N_4(0)}{D_2'(0)} = \frac{\mu_5 L_5}{\sum_{i=0,1,2,3,4,5} \mu_i L_i} \quad [9.21]$$

(c) **Busy period of the Repairman in Shut Down repair in time (0, t]**, By probabilistic arguments we have

$$W_4(t) = \bar{G}_4(t) \quad [9.22]$$

Similarly developing similar recursive relations as in 9(b), we have

$$\begin{aligned} B_0(t) &= \sum_{i=1,2,3,5} q_{0i}(t) \boxed{c} B_i(t) \quad ; \quad B_1(t) = q_{10}(t) \boxed{c} B_0(t) \quad ; \\ B_2(t) &= \sum_{i=0,4} q_{2i}(t) \boxed{c} B_i(t) \quad ; \quad B_3(t) = \sum_{i=0,4} q_{3i}(t) \boxed{c} B_i(t) \quad ; \\ B_4(t) &= W_4(t) + q_{40}(t) \boxed{c} B_0(t) \quad ; \quad B_5(t) = q_{50}(t) \boxed{c} B_0(t) \quad ; \end{aligned} \quad [9.23-9.28]$$

Taking Laplace stieltjes transformation of above equations; and writing in matrix form, we get

$$q_{6 \times 6} [B_0^*, B_1^*, B_2^*, B_3^*, B_4^*, B_5^*]' = [0, 0, 0, 0, W_4^*, 0]'$$

Where $q_{6 \times 6}$ is denoted by [8.9] and therefore $D_2'(s)$ is obtained as in the expression of availability.

$$\text{Now } N_5(s) = \begin{bmatrix} 0 & -q_{01}^* & -q_{02} & -q_{03}^* & 0 & -q_{05}^* \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & -q_{24}^* & 0 \\ 0^* & 0 & 0 & 1 & -q_{34}^* & 0 \\ W_5^* & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{6 \times 6}$$

In the long run, we get the value of this determinant after putting $s \rightarrow 0$ is

$$N_5(0) = \mu_4(p_{02}p_{24} + p_{03}p_{30}) = \mu_4 L_4$$

[9.29]

Thus the fraction of time for which the system is under shut down is given by:

$$B_0^{3*}(\infty) = \lim_{t \rightarrow \infty} B_0^{3*}(t) = \lim_{s \rightarrow 0} s B_0^{3*}(s) = \frac{N_5(0)}{D_2'(0)} = \frac{\mu_4 L_4}{\sum_{i=0,1,2,3,4,5} \mu_i L_i} \quad [9.30]$$

10. Particular cases: When all repair time distributions are n-phase Erlangian distributions i.e.

$$\text{Density function } g_i(t) = \frac{nr_i(nr_i t)^{n-1} e^{-nr_i t}}{n-1!}$$

$$\text{And Survival function } \bar{G}_j(t) = \sum_{j=0}^{n-1} \frac{(nr_i t)^j e^{-nr_i t}}{j!} \quad [10.1-10.2]$$

And other distributions are negative exponential

$$a(t) = \theta e^{-\theta t}, b(t) = \eta e^{-\eta t}, \bar{A}(t) = e^{-\theta t}, \bar{B}(t) = e^{-\eta t} \quad [10.3-10.6]$$

For n=1 $g_i(t) = r_i e^{-r_i t}$, $\bar{G}_i(t) = e^{-r_i t}$ If i=1, 2, 3, 4

$$g_1(t) = r_1 e^{-r_1 t}, g_2(t) = r_2 e^{-r_2 t}, g_3(t) = r_3 e^{-r_3 t}, g_4(t) = r_4 e^{-r_4 t} \\ \bar{G}_1(t) = e^{-r_1 t}, \bar{G}_2(t) = e^{-r_2 t}, \bar{G}_3(t) = e^{-r_3 t}, \bar{G}_4(t) = e^{-r_4 t} \quad [10.7-10.14]$$

Also

$$p_{01} = \frac{\alpha}{x_1 + \theta}, p_{02} = \frac{\beta}{x_1 + \theta}, p_{03} = \frac{\gamma}{x_1 + \theta}, p_{05} = \frac{\theta}{x_1 + \theta}$$

$$\begin{aligned}
 p_{10} &= 1, p_{20} = \frac{r_2}{\alpha + \gamma + r_2}, p_{24} = \frac{\alpha + \gamma}{\alpha + \gamma + r_2}, \\
 p_{30} &= \frac{r_3}{\alpha + \beta + r_3}, p_{34} = \frac{\alpha + \beta}{\alpha + \beta + r_3}, \mu_0 = \frac{1}{x_1 + \theta}, \mu_1 = \frac{1}{r_1}, \\
 \mu_2 &= \frac{1}{\alpha + \beta + r_{2,4}}, \mu_3 = \frac{1}{\alpha + \gamma + r_3}, \mu_4 = \frac{1}{r_4}, \mu_5 = \frac{1}{\eta}
 \end{aligned}
 \tag{10.15-10.30}$$

$$\begin{aligned}
 \text{MTSF} &= \frac{\mu_0 + \mu_2 p_{02} + \mu_3 p_{03}}{1 - p_{02} p_{20} - p_{03} p_{30}}, A_0(\infty) = \frac{\mu_0 L_0 + \mu_2 L_2 + \mu_3 L_3}{\sum_{i=0,1,2,3,4,5} \mu_i L_i}, \\
 B_0^{1*}(\infty) &= \frac{\sum_{i=1,2,3} \mu_i L_i}{\sum_{i=0,1,2,3,4,5} \mu_i L_i}, B_0^{2*}(\infty) = \frac{\mu_5 L_5}{\sum_{i=0,1,2,3,4,5} \mu_i L_i}, B_0^{3*}(\infty) = \frac{\mu_4 L_4}{\sum_{i=0,1,2,3,4,5} \mu_i L_i}
 \end{aligned}
 \tag{10.31-10.35}$$

$$\text{Where } L_0 = 1; L_1 = p_{01}; L_2 = p_{02}; L_3 = p_{03}; L_4 = p_{02} p_{24} + p_{03} p_{34}; L_5 = p_{05};
 \tag{10.36-10.41}$$

11. Profit Analysis:-

The profit analysis of the system can be carried out by considering the expected busy period of the repairman in repair of the unit in (0,t].

Therefore, G(t) = Expected total revenue earned by the system in (0,t] -Expected repair cost of the failed units
 -Expected repair cost of the repairman in preventive maintenance -Expected repair cost of the Repairman in shut down

$$\begin{aligned}
 &= C_1 \mu_{up}(t) - C_2 \mu_{b1}(t) - C_3 \mu_{b2}(t) - C_4 \mu_{b3}(t) \\
 &= C_1 A_0 - C_2 B_0^1 - C_3 B_0^2 - C_4 B_0^3
 \end{aligned}
 \tag{11.1}$$

$$\text{Where } \mu_{up}(t) = \int_0^t A_0(t) dt; \mu_{b1}(t) = \int_0^t B_0^1(t) dt; \mu_{b2}(t) = \int_0^t B_0^2(t) dt; \mu_{b3}(t) = \int_0^t B_0^3(t) dt
 \tag{11.2-11.5}$$

C_1 is the revenue per unit time and C_2, C_3, C_4 are the cost per unit time for which the system is under simple repair, preventive maintenance and shut down repair respectively.

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Figure: state transition diagram

