



#### BeWS-15 is organized under the auspices of the IEA Technology Collaboration Program on Fusion Materials (FM TCP

# Current design of the EU DEMO Helium Cooled Pebble Bed breeding blanket

Dr. Guangming Zhou (KIT) Lead Engineer of HCPB Breeding Blanket







This work has been carried out within the framework of the EUROfusion Consortium, funded by the European Union via the Euratom Research and Training Programme (Grant Agreement No 101052200 — EUROfusion). Views and opinions expressed are however those of the author(s) only and do not necessarily reflect those of the European Union or the European Commission. Neither the European Union nor the European Commission can be held responsible for them.

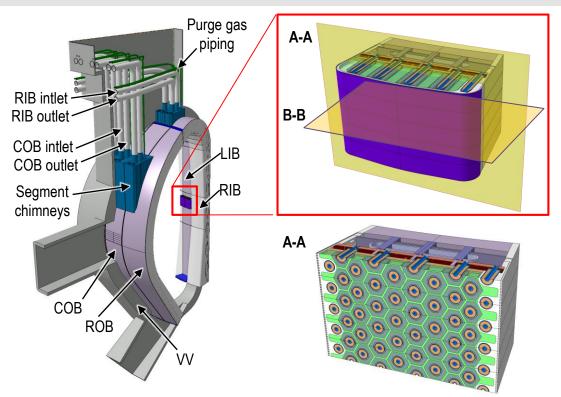
## Outline of content



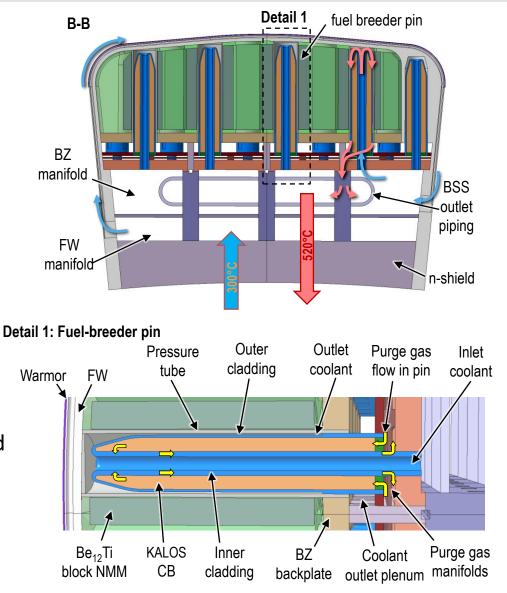
- Status at the end of Pre-Concept Design Phase (2014-2020)
- Identified risks
- Design activities to address the risks
- Outlook

#### Status at the end of Pre-Concept Design Phase (2014-2020)





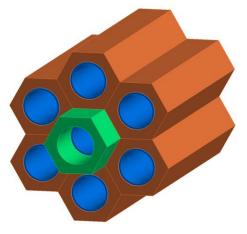
- Coolant: He @80 bar, 300-520°C
- Fuel-breeder pins containing advanced ceramic breeder (ACB) pebble bed
- Pins inserted into blocks of Be12Ti neutron multiplier
- Structural steel: Eurofer97
- Purge gas: He + 0.1vol% H<sub>2</sub> @2 bar
- Easier manufacturing, easier filling of pebbles
- NA, TH & TM; TBR = 1.20; Ppump per blower < 6 MW; satisfying shielding



# Identified risks related to HCPB BB

- 1. Low reliability of BB system under DEMO conditions [due to welds failure]
- 2. Loss of structural integrity of beryllide blocks
- 3. High pressure drops in coolant loop contributing to total high pumping power
- 4. Large tritium permeation rates at the interface of breeder-coolant loop
- 5. Low BB shielding capability
- 6. Degradation of Eurofer at contact with pebbles in purge gas environment
- 7. Reduction of structural integrity of blanket during shutdown due to Eurofer irradiation embrittlement

 $\rightarrow$ 



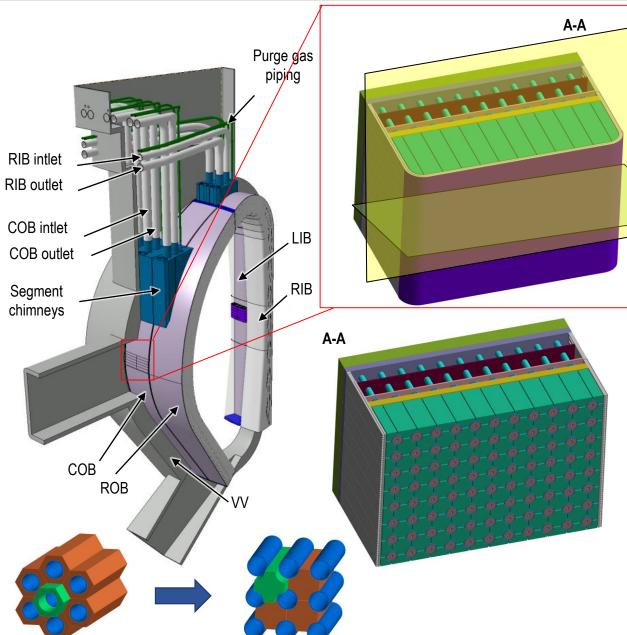
Fuel-breeder pin Pressure Outer Outlet Purge gas Inlet cladding flow in pin tube coolant coolant Warmor FW KALOS Purge gas Be<sub>12</sub>Ti Inner Coolant ΒZ CB block NMM outlet plenum manifolds cladding backplate

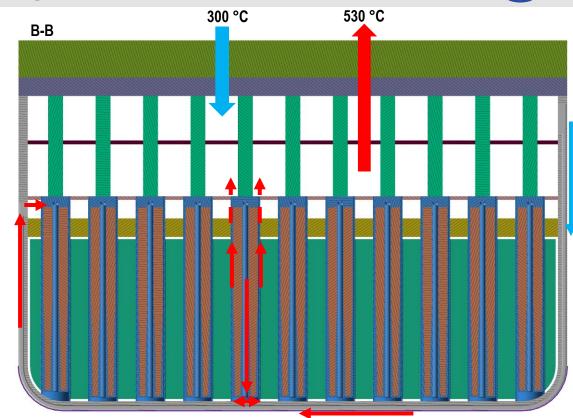
See Talk of S. Udartsev

Be<sub>12</sub>Ti block NMM

## Proposed design changes for improvements







- Equalize purge gas and coolant pressure to eliminate in-box LOCA welds to improve reliability
- Increase ΔT (300°C-530°C) to further reduce pressure drop
- Re-arrange flow scheme to cool key structure with fresh coolant
- Shape of Be12Ti block to square

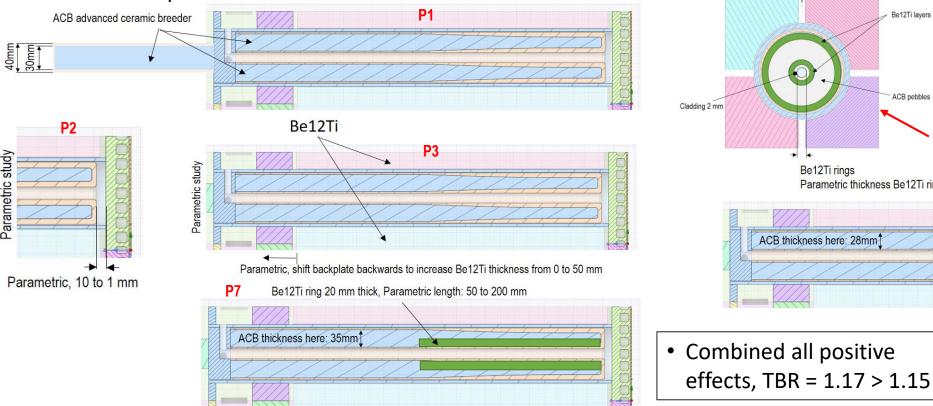
**₿-**В

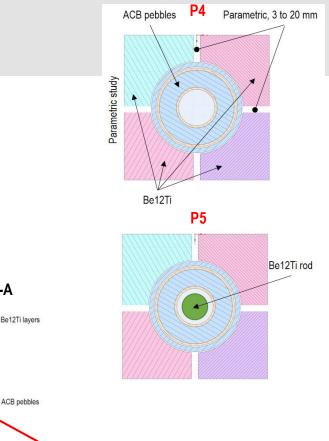
# Tritium breeding ratio (TBR) optimization

- P1. Study influence of ACB in back side of the pin (whole length of back side of pin)
- P2. Study reduction of the front pin cladding distance to FW
- P3. Study influence of Be12Ti radial length
- P4. Study influence of Be12Ti block gaps
- P5. Introduction of a Be12Ti rod in the inner tube
- P6. Introduce Be12Ti in ACB pebbles (on both sides)
- P7. Like P6, Introduce Be12Ti in ACB pebbles (only on inner side)

P8. Combined the positive effects

Parametric study





– A-A

Page 6

A-A

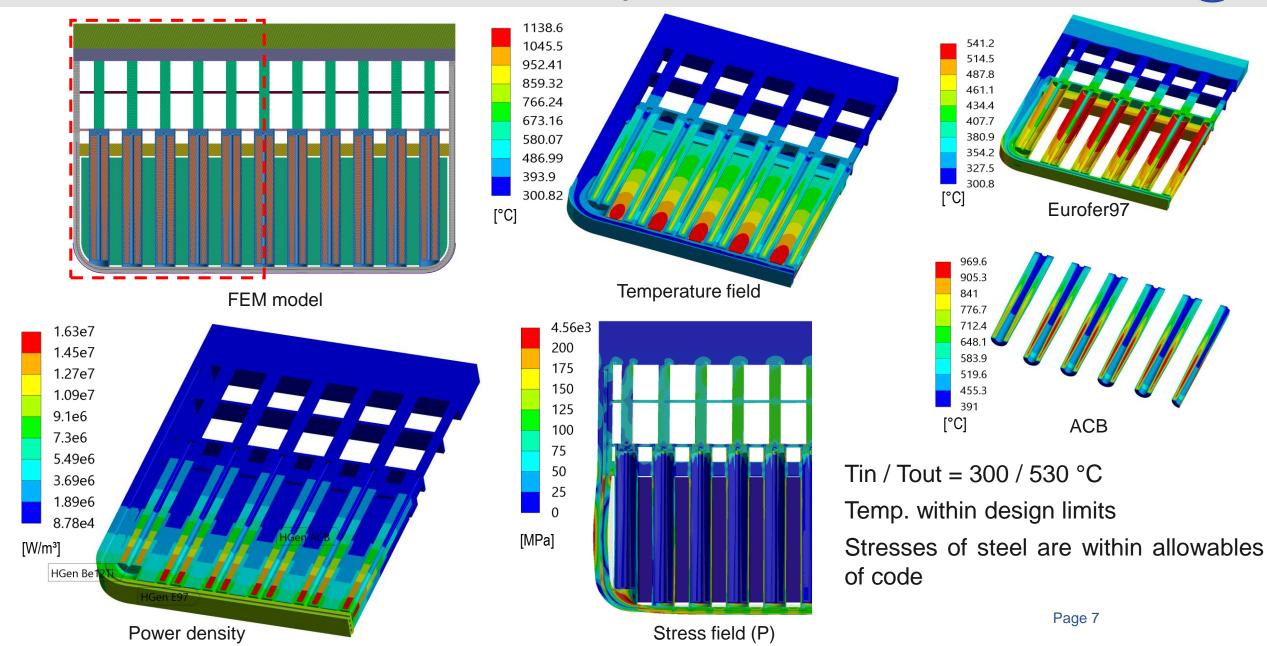
Be12Ti rings

**P6** 

Parametric thickness Be12Ti rings 1 to 10mm thick (keep total thickness 28mm)

#### Thermal and structural analysis





Page 7

Eurofer97

ACB

541.2

514.5

487.8

461.1

434.4

407.7 380.9

354.2

327.5

300.8

969.6 905.3

841

776.7

712.4

648.

583.9

519.6

455.3

391

# Assessment of pebble-Eurofer interaction

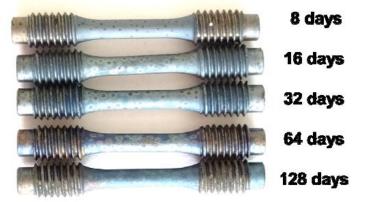


• Acc. to [1], the fatigue lifetime reduced due to interaction between pebbles and Eurofer97

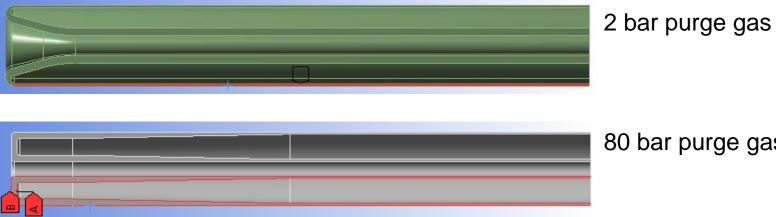


Interaction conditions:

T=550°C Atmosphere: purge gas flow (He+0.1%H<sub>2</sub>) Duration: 8, 16, 32, 64, 128 days



• Creep-Fatigue-Assessment tool [2] used to assess different design options (2 bar vs 80 bar purge gas)



• Along the indicated paths, most regions failed to withstand the required 7787 cycles

80 bar purge gas

• Along the indicated paths, most regions succeeded to withstand the required 7787 cycles

• New design able to improve lifetime.

# Shielding design (1/2)

 ${}^{10}_{5}B + {}^{1}_{0}n \rightarrow {}^{3}_{1}T + 2{}^{4}_{2}He$ 



Parametric neutronics analysis [3	3] 15 cm	Cases	Nuclear heating at 1st cm of TFC (limit: 5e-5)	Neutron flux at 1st cm of TFC (limit: 1e9)	dpa/fpy at 1st cm of TFC (limit: 1.6e-5)	dpa/fpy at 1st cm of VV (limit: 4.5e-1)	He production at 1st cm of VV (limit: 0.16)
3D MCNP model by SuperMC							(
- Baseline: 15 cm Eurofer			W/cm <sup>3</sup>	n/cm²/s			appm/fpy
- $v1$ : 1 cm B <sub>4</sub> C, 14 cm Eurofer		Baseline	8.69e-5	2.21e9	1.81e-5	1.53e-1	0.56
-		v1	7.36e-5	2.07e9	1.69e-5	1.28e-1	0.42
- $v2$ : 2 cm B <sub>4</sub> C, 13 cm Eurofer		v2	6.83e-5	2.29e9	1.24e-5	9.27e-2	0.35
т <i>г</i>		v3	5.37e-5	1.82e9	1.42e-5	9.43e-2	0.29
		v4	5.16e-5	1.74e9	1.50e-5	8.58e-2	0.27
- $v5$ : 5 cm B <sub>4</sub> C, 10 cm Eurofer		v5	4.72e-5	1.66e9	1.40e-5	7.70e-2	0.24
4-,		v6	4.16e-5	1.57e9	1.41e-5	6.94e-2	0.22
	B4C shield	v7	3.69e-5	1.47e9	1.41e-5	6.29e-2	0.18
<ul> <li>v10: 10 cm B₄C, 5 cm Eurofer</li> </ul>	Part of MCNP6 model	v8	3.32e-5	1.43e9	1.24e-5	5.76e-2	0.17
$v_1$ $v_2$ $v_3$ $v_4$ $v_4$ $v_5$ $v_4$ $v_6$ $v_4$ $v_6$ $v_4$ $v_6$ $v_4$ $v_6$		v9	3.30e-5	1.41e9	1.27e-5	5.52e-2	0.16
Tritium and helium production in B4C			3.24e-5	1.40e9	1.24e-5	5.27e-2	0.15
			4.06e-5	1.65e9	1.28e-5	7.46e-2	0.19
		v10 inverted	2.81e-5	1.33e9	1.16e-5	5.07e-2	0.14

Negligible, 120 kg T/fpy in EU-DEMO 1e-28 [Pa·m³/(s·m²)] << Outgassing limit 1e-11

Maximum T and He production is in v10, 1.84 mole (5.52 g) T per FPY, 500 mole (2 kg) He per FPY in EU-DEMO

Due to fragmentation of B4C, container of B4C is needed.

Nuclear heating in B4C and Eurofer used as input for structural design of the shield.

# Shielding design (2/2)

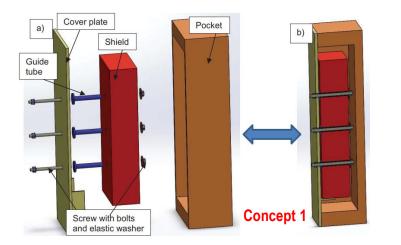
#### Structural design

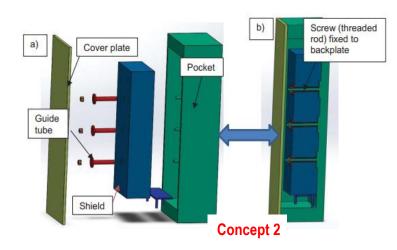
To confine the fragmentation, B4C is designed to be contained.

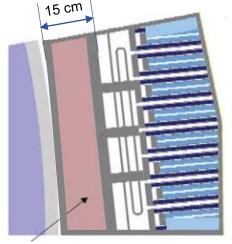
Concept 1: Radiation, shield fixed to cover plate

Concept 2: Contact, shield fixed to BSS backplate

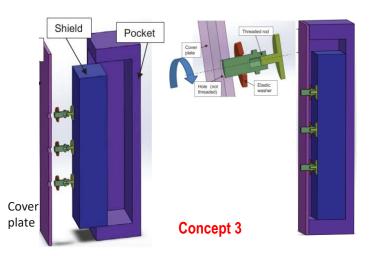
Concept 3: Contact, shield fixed to BSS backplate with external clamping



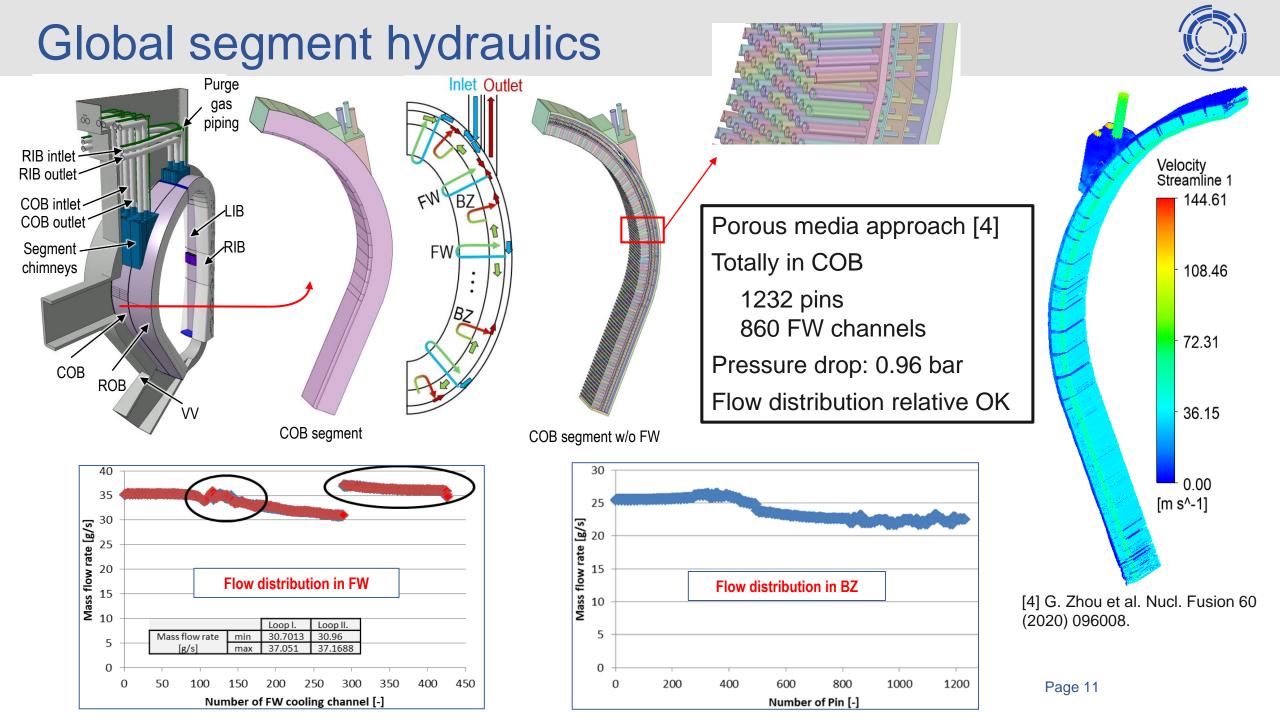




B4C shield







## Tritium Extraction and Removal (TER) system

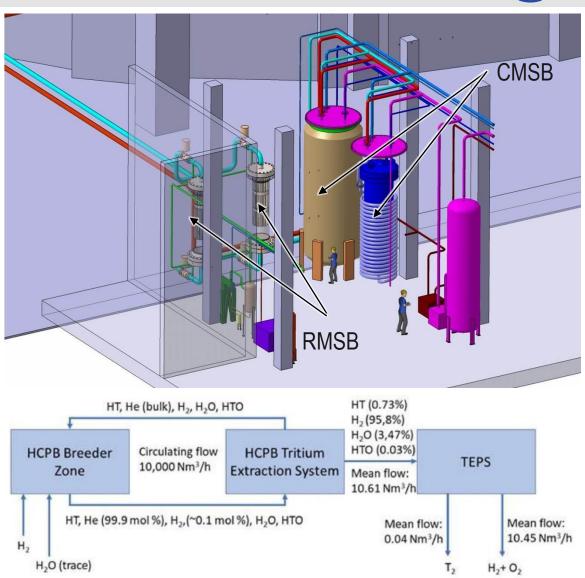


#### Reference design

➤ Two stages in series

First the adsorption of Q2O on the Reactive Molecular Sieve Bed (RMSB), thereafter the adsorption of Q2 on the Cryogenic Molecular Sieve Bed (CMSB) at 77 K. Q = H, D, T

- Tritium recovered via isotope exchange on RMSB and by heating-up of the CMSB.
- Extrapolated to DEMO scale is realized with industry.
- Outlook
- ➢ 80 bar purge gas, introduced to improve reliability of BB, results show that TER operating at 80 bar not a issue.
- CMSB requires large amount of liquid N2, getter bed is explored as alternative.
- Wetted purge gas to have a higher isotopic exchange rate compared to H2 and oxidized Q2, reducing permeation.



# **Tritium permeation analysis**



5

5

wall to coolant, 2 bar

breeder to wall. 2 bar

wall to coolant. 2 bar

interface mass flow (% of generation rate) 5 breeder to wall, 80 bar wall to coolant. 80 bar 3 breeder to wall. 2 bar 2 Open√FOAM The Open Source CFD Toolbox 0 1 2 3 Temp. field of 1/6 fuel-breeder pin 0 time (h) Permeation under equal volumetric flow 35 interface mass flow (% of generation rate) 30 25 breeder to wall, 80 bar 20 wall to coolant, 80 bar 15 10 5 1 2 3 0 time (h)

Permeation under equal mass flow

- 3D component level solver [6]
  - Developed based on the OpenFOAM and benchmarked with TMAP 7
  - > T release model

Grain surface release model based on irradiation T release experiment [7]

- T permeation analysis
- > T permeation analysis under 2 bar pressure purge gas vs 80 bar pressure purge gas, with same H2 partial pressure
- Wetted purge gas vs dry purge gas

Purge gas	Permeation to coolant	Wall T inventory
200Pa H2, no H2O	0.077% of T generation 290 mg/d	65 ng
200Pa H2 + 200Pa H2O	0.022% of T generation 83 mg/d	19.2 ng

[6] V. Pasler et al., Applied Sciences 11 (2021) 3481. [7] T. Kinjyo et al. Fusion Engineering and Design 81 (2006) 573-577.

### Outlook



- At end of 2022, the milestone of preliminary conceptual design of the HCPB blanket shall be reached.
- At second half of 2024, the milestone of reference conceptual design for the HCPB blanket shall be reached, together with R&D programme.
- At the end of 2024, the driver blanket for EU-DEMO will be selected from the HCPB and WCLL concepts.
- From 2025 to 2027, the selected blanket will be further consolidated and qualified via design and R&D activities.

# **Contributors & Acknowledgements**

Guangming Zhou<sup>1\*</sup>, Francisco A. Hernández<sup>1, 2</sup>, Jarir Aktaa<sup>1</sup>, David Alonso<sup>3</sup>, Frederik Arbeiter<sup>1</sup>, Lorenzo V. Boccaccini<sup>1</sup>, Ion Cristescu<sup>1</sup>, Antonio Froio<sup>4</sup>, Christophe Garnier<sup>5</sup>, Mathias Jetter<sup>1</sup>, Xue Zhou Jin<sup>1</sup>, Marc Kamlah<sup>1</sup>, Béla Kiss<sup>6</sup>, Christine Klein<sup>1</sup>, Christina Koehly<sup>1</sup>, Ivan Maione<sup>1</sup>, Luis Maqueda<sup>3</sup>, Carlos Moreno<sup>7</sup>, Ivo Moscato<sup>2,8</sup>, Iole Palermo<sup>7</sup>, Jin Hun Park<sup>1</sup>, Volker Pasler<sup>1</sup>, Dario Passafiume<sup>1</sup>, Pavel Pereslavtsev<sup>1</sup>, Anoop Retheesh<sup>1</sup>, Álvaro Yáñez<sup>3</sup>

<sup>1</sup>Karlsruhe Institute of Technology (KIT), Eggenstein-Leopoldshafen, Germany

<sup>2</sup>EUROfusion Programme Management Unit, Garching, Germany

<sup>3</sup>ESTEYCO, Madrid, Spain

<sup>4</sup>Dipartimento Energia, Politecnico di Torino, Turin, Italy

<sup>5</sup>French Alternative Energies and Atomic Energy Commission (CEA), Cadarache, France

<sup>6</sup>Budapest University of Technology and Economics (BME), Budapest, Hungary

<sup>7</sup>CIEMAT, Fusion Technology Division, Madrid, Spain

<sup>8</sup>University of Palermo, Palermo, Italy





This work has been carried out within the framework of the EUROfusion Consortium, funded by the European Union via the Euratom Research and Training Programme (Grant Agreement No 101052200 — EUROfusion). Views and opinions expressed are however those of the author(s) only and do not necessarily reflect those of the European Union or the European Commission. Neither the European Union nor the European Commission can be held responsible for them.



\*Guangming.Zhou@kit.edu



#### Thank you for your attention!