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OzFuel Pre-Phase A Study

Australian Forest Fuel Monitoring from Space



OzFuel

OzFuel Pre-Phase A Study: Australian Forest Fuel Monitoring From Space

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Executive Summary

This document presents the results of a Pre-Phase A study for the OzFuel bushfire fuel monitoring mission in accordance with NASA system engineering standards.

The OzFuel Pre-Phase A Study (Australian Forest Fuel Monitoring from Space) report was developed by the Australian National University (ANU) Institute for Space for Geoscience Australia (GA) and CSIRO in support of their contribution to Australia's Satellite Cross-Calibration Radiometer (SCR) and AquaWatch missions (UNSW Canberra Space, 2021).

The OzFuel study conceptualises a multispectral bushfire fuel monitoring satellite mission to fulfil two major goals:

- To launch a dedicated science and research mission to mitigate the risk of future catastrophic bushfires; and
- To deliver an Australian designed and built pathfinder mission to de-risk the SCR program.

Key outcomes of the OzFuel mission are:

- Australian capability enables the forward-looking development of a fully operational satellite constellation for bushfire prevention, mitigation and resilience.
- ANU expertise in global fuel hazard spatial data augments international commercial and government fire detection initiatives.
- Space-proven Australian detector technology becomes available for national and commercial small satellite missions.

This report comprises two parts:

- Part 1: OzFuel Mission Requirements developed by Nicolas Younes and Marta Yebra from the ANU Fenner School of Environment & Society. The report introduces the OzFuel mission, the need for a dedicated fuel monitoring mission, and the remote sensing requirements for a pathfinder mission.
- Part 2: OzFuel Technical Overview developed by Rob Sharp from the ANU Advanced Instrumentation & Technology Centre. The overview outlines the technical design and payload options for the OzFuel-1 mission.

The climate crisis over the past decade culminated in the unprecedented 2019/2020 Australian bushfire conditions that were more catastrophic than expected or modelled. The risk of larger and more frequent mega-fires is only going to increase in future years. Allocating further ground resources to suppress fires is extremely costly and dangerous, and needs to be augmented with more effective prediction, prevention and mitigation strategies before an unforeseen ignition event burns out of control.

One of the most crucial aspects of fire prevention is understanding vegetative fuel state. The 2020 Royal Commission into National Natural Disasters highlights the need for whole-of-continent visibility of vegetative fuel state – how much fuel there is and how dry it is. Australia relies on foreign satellite data which is not optimised for measuring our unique bush landscape. The growing need for

sovereign satellites to remotely sense Australia’s unique vegetation has been supported by recommendations from government, agencies, industry and research institutions.

Royal Commission into National Natural Disasters
Recommendation 17.3 Classification, recording and sharing of fuel load data
Australian state and territory governments should develop consistent processes for the classification, recording and sharing of fuel load data.

The OzFuel mission aims to monitor fuel conditions via satellite remote sensing to deliver whole-of-continent fuel spatial data at the optimum spatial, temporal and spectral resolution. Conceptualised as a pathfinder to a national environmental monitoring constellation, the mission will provide critical bushfire Earth observation data to support government, frontline organisations and communities for enhanced bushfire situational awareness and preparedness.

OzFuel is being developed in parallel with the CHICO mission, a dual-use hyperspectral imager for water quality monitoring (ANU and partners). While each pathfinder has unique user requirements, both serve as a staged series of development missions to de-risk critical sovereign capabilities and enable larger, fully operational national satellite missions.

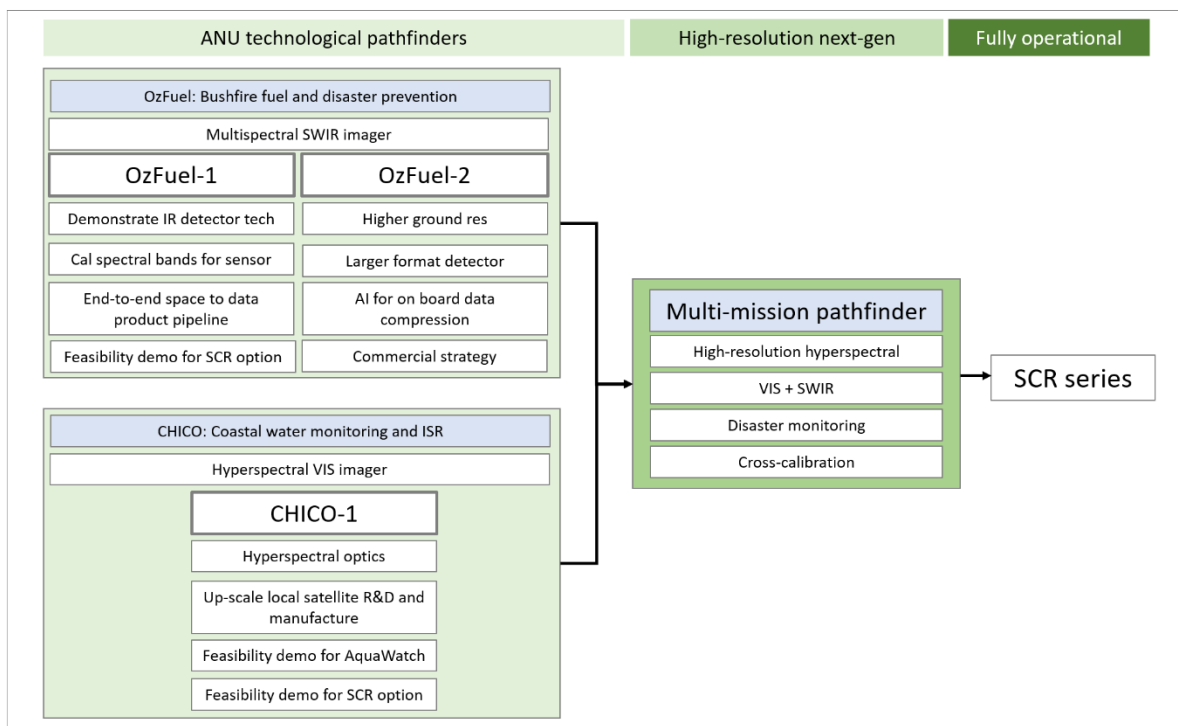


Figure 1. ANU small satellite mission roadmap in support of an Australian multi-mission small satellite launch program for Earth observation (Deloitte Access Economics, 2021). OzFuel and CHICO are Earth observation missions under development at the ANU. SCR refers to the Satellite Cross-Calibration Radiometer feasibility study undertaken by UNSW Canberra Space (2021).

Recommendations following this study include:

- Fieldwork to verify and validate the preliminary requirements identified for remote sensing of fuel conditions during the upcoming 2021/22 fire season.
- A follow-on Phase A concurrent engineering study and mission analysis for the OzFuel-1 pathfinder;
- Market analysis for OzFuel shortwave infrared data and potential distribution channels.

The results of **this study will inform the Australian Space Agency Earth Observation from Space Technology Roadmap** (“the Roadmap”) being developed by The Agency, in close partnership with the Bureau of Meteorology, CSIRO, the Department of Defence, Geoscience Australia and the Australian Earth observation community.

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Part I: OzFuel Mission Requirements

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1 Introduction

1.1 Background and Justification

Across Australia, bushfires consume millions of hectares of forests every year. They can cause millions of dollars in damage to infrastructure and can kill people and animals. Once ignition occurs, locating the fire, estimating its area and potential routes of spread are vital steps to ensure communities are safe and damage is kept to a minimum. Comprehensive fuel characterisation is a critical 'pre-fire' element for assessing bushfire risk, predicting fire behaviour, informing suppression efforts, and planning prescribed burns. A key determinant of successful fire ignition and spread is the amount of fuel that is dry enough to burn (i.e. fuel load).

Fuel Moisture Content (FMC) is a measure of the amount of water in the fuel available to a fire, and it is expressed as a per cent of the dry weight of that specific fuel (Equation 1). When the FMC is high, the energy required for a plant to burn is too high. The fuel will not ignite readily or at all (Yebra et al., 2018, 2013). In contrast, if the vegetation has low FMC, it can be easily ignited, making it more flammable and combustible. Knowing how much fuel there is in a given area allows us to estimate

the potential severity and sustainability of a bushfire. In general, if there is more fuel, flames can be larger, the fire becomes more intense, and it can burn for longer (Jolly et al., 2014; Jolly and Johnson, 2018).

$$FMC = \frac{EWT}{DMC} = \left(\frac{\frac{W_f - W_d}{A}}{\frac{W_d}{A}} \right) = \frac{W_f - W_d}{W_d}$$

Equation 1: Fuel Moisture Content formula, and its relationship with the Equivalent Water Thickness (EWT) and Dry Matter Content (DMC) (Yebra et al 2013). W_f , W_d , and A represent the fresh weight, dry weight, and area of the leaf samples, respectively.

Australian fuel conditions are currently tracked and quantified largely via ground assessments, broad-scale proxies (e.g. weather indices or time since fire), and occasional satellite data at regional and state levels. Imagery from the Sentinel 2, MODIS (Moderate Resolution Imaging Spectroradiometer), and Himawari 8 satellites, is increasingly being used to monitor fuel attributes such as FMC (Yebra et al., 2019, 2018), but some limitations remain. For example, the Australian Flammability Monitoring System (<http://anuwald.science/afms>, Figure 2) uses MODIS imagery to estimate FMC across Australia. Despite being a useful tool, the resolution of MODIS imagery (i.e. 500m) is too coarse for accurate field operations planning. Also, MODIS has already exceeded the expected lifetime and, at some point in the not-too-distant future, will become inoperative. Likewise, the Himawari 8 satellite provides satellite imagery of Australia every 10 minutes with the drawback that its pixel size is 2 km, making it even coarser than MODIS imagery. An alternative to MODIS and Himawari 8 satellites comes in the form of the Sentinel 2A and 2B satellites. With a pixel size between 10m – 20m, and a revisit time of ~5 days, the Sentinels provide exceptional spatial detail for operations planning, however the spectral bands are too wide to capture FMC variations in eucalypt forests. There is thus a critical scientific and technological gap in bushfire management that can be filled with a dedicated fuel monitoring mission.

Recently, the New South Wales Bushfire Enquiry, highlighted several limitations of the remote sensing tools used during the 2019-2020 bushfire season. These limitations included: (1) the lack of data regarding the characteristics and conditions of the fuel, (2) the low spatial resolution of the imagery available, and (3) untimely acquisition of high-resolution satellite imagery to inform and update firefighting efforts (NSW Government, 2021). Some of these limitations were also registered by the Australian Space Agency's Bushfire Earth Observation Taskforce report (ASA, 2021). The Taskforce concluded that one way in which Australia can overcome these limitations was by "*consider[ing] the development of its own capability [...] focused on supporting bushfire activities*".

The OzFuel mission is the first step in the creation of an EO early warning system, with high revisit, high spatial and spectral resolutions. This mission is unique as it will measure fuel properties as opposed to fire detection. By targeting the specific wavelengths related to dry matter and water content of eucalypts, OzFuel will provide a comprehensive characterisation of fuel loads at a continental scale. Its fire prevention function will be the first of its kind in the world, complementing an array of commercial and government initiatives for active fire detection.

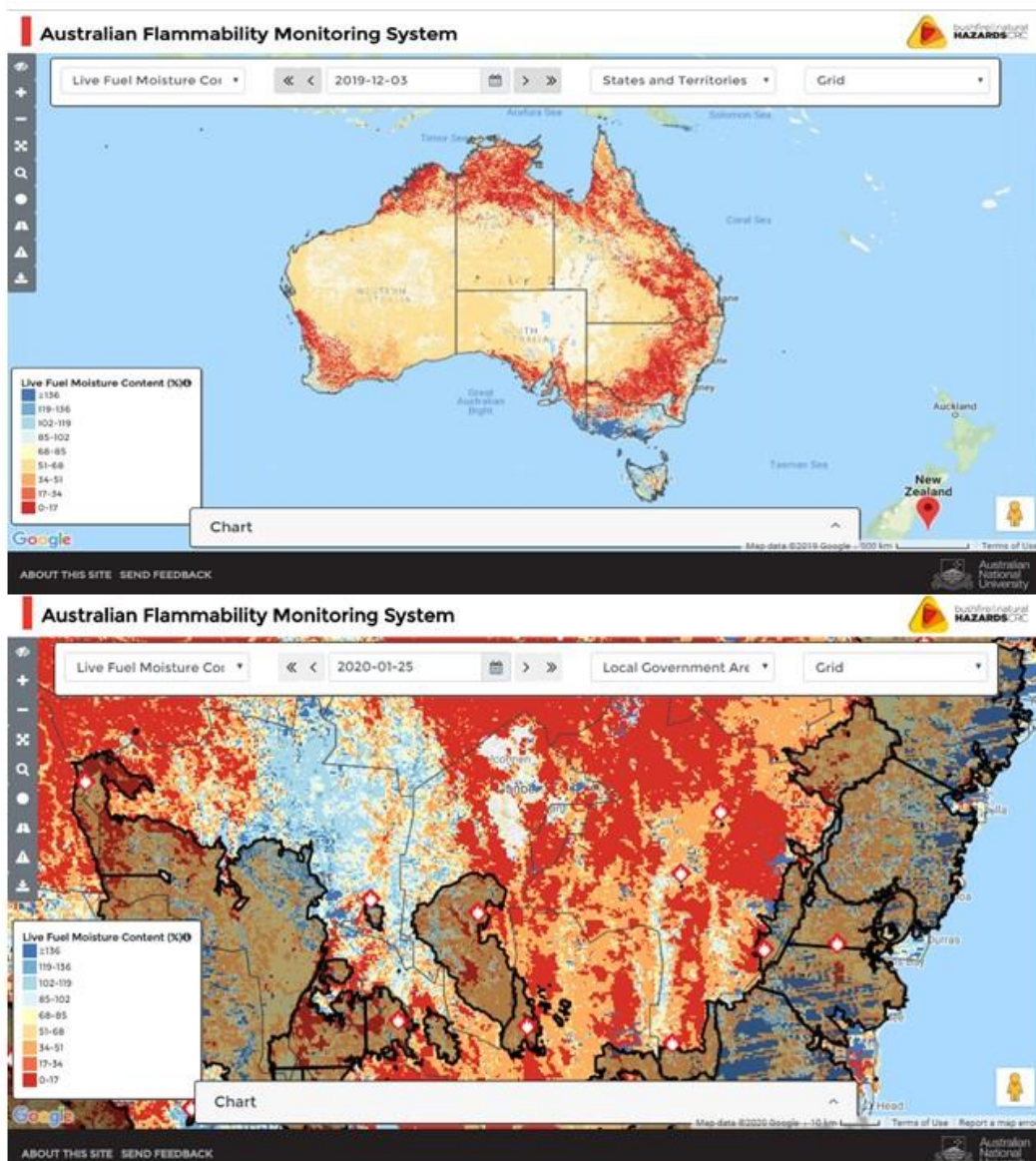


Figure 2. Screenshots of the Australian Flammability Monitoring System public website (AFMS, (<http://anuwald.science/afms>)). The AFMS is the first website in Australia that uses satellite data to collect information on live fuel moisture content (LFMC). It displays this information on an interactive map, which helps fire managers schedule and plan their prescribed burning efforts and preposition firefighting resources based on the flammability of the landscape. The bottom image displays the LFMC map during the Orroral Valley fire in the Canberra region on 25 January 2020. It reveals very dry fuel continuity on the fire ground. The black areas represent the total burned extent reported by the emergency authorities at the time and the red flames represent active fires. Dark blue stripes on areas in the east coast of the map represent artifacts due to thick smoke and poor quality reflectance data.

1.2 What is OzFuel

OzFuel is a satellite mission specifically designed to monitor fuel loads across Australia.

Eucalypt trees are known to be more flammable than other species. Considering that in Australia, approximately 77% of forested areas are comprised of eucalypts, it is important to constantly monitor these forests to detect the signs of imminent bushfires. OzFuel is specifically designed to

monitor the moisture content and fuel load of eucalypts, and it's the first of an envisioned constellation that aims to address the challenges of fuel load monitoring, bushfire hazard mapping, and resource allocation.

This proof-of-concept mission uses the Short-Wave Infrared (SWIR) region of the electromagnetic spectrum to monitor changes in fuel moisture and fuel load, thereby highlighting areas vulnerable to bushfires. OzFuel data will enhance existing flammability modelling and monitoring capabilities such as the Australian Flammability Monitoring System.

The long-term vision for OzFuel is to have one (or more) hyperspectral satellite(s) that provide(s) very detailed information on the flammability and fuel condition of eucalypt forests across Australia. This can be achieved through a staged approach. Here the user needs are defined for the first OzFuel-1 multispectral imager that will de-risk the development of later generation hyperspectral satellites.

1.3 Purpose of the OzFuel mission

The Australian National University (ANU) proposes a program of work beginning with the OzFuel demonstrator mission. The mission will deliver a bespoke sensor system to achieve high ground resolution, low-noise images, in a suite of pass bands dedicated to monitoring fuel moisture content and fuel load of Eucalypt trees.

The OzFuel mission was conceived to fulfil three important purposes:

1. Address the need for more efficient national monitoring of fuel conditions and bushfire prevention across the Australian mainland and Tasmania,
2. Deliver critical data to boots-on-ground resources as a proactive approach to reducing the likelihood of out-of-control bushfires, and
3. Promote the growth of the space industry while demonstrating Australia's capabilities to design and operate a satellite mission.

The expected outcomes of the OzFuel mission are:

- Demonstrated Australian capability to develop a fully operational satellite (or satellite constellation) for bushfire prevention, mitigation and resilience,
- Increased and demonstrated expertise of ANU for global fuel hazard monitoring and assessments,
- Contribution of geospatial data to national and international fuel characterisation and fire detection initiatives, and
- Availability of space-proven Australian detector technology for national and commercial small satellite missions.

1.4 Scope of the document

This document presents the Mission Requirements of the OzFuel mission. The current version of the document focuses solely on the pathfinder OzFuel mission and does not intend to describe or specify the requirements of the hyperspectral sensors.

Here we describe the user requirements and technological limitations that have been identified by potential users in terms of geographical coverage, revisit frequency and spectral sampling. We present them as specific, quantifiable, and traceable characteristics of the mission.

This is a living document and will be used in subsequent derivations of the mission requirements and for the mission implementation.

2 Mission requirements

2.1 Revisit frequency

The revisit frequency refers to the temporal resolution of the satellite. It refers to the time between when a satellite acquires data over a point on the Earth's surface and when it returns to that point again. This frequency does not consider cloud cover or other potential obstructions that impede the actual observation of a site or place.

Fuel loads in eucalypt forests are not expected to change suddenly (i.e. from one day to the next) but gradually (i.e. over a period of days or weeks). Therefore, end users would need updated Dry Fuel Load products and Fuel Moisture Content products on a weekly basis (approximately). For a single satellite, a temporal resolution of 6-8 days is acceptable. An ideal repeat coverage should be higher than that for Landsat sensors (i.e. every 16 days) and similar to that of the combined Sentinel 2A and 2B satellites (i.e. every three to five days). This may be accomplished with a constellation of two or more satellites.

For a single satellite, an imaging frequency of 6-8 days is acceptable.

2.2 Time of observation

The time of observation is the time of day at which an image is captured by the satellite. As a general principle, the design team should ensure that the time of observation is such that illumination and viewing directions remain identical (or similar) through time. The aim should be to maximise the number of images with identical or similar observation configurations.

Considering that FMC changes seasonally and throughout the day (Cheng et al., 2014; Nolan et al., 2020), it would be desirable to acquire data in the early hours of the afternoon, when vegetation is more stressed and can be more easily ignited. Images should be acquired, preferably, between 12h00 and 14h00. This schedule will depend on other factors such as cloud prevalence, potential 'hot spots' in images, and other considerations that could complicate image analysis.

2.3 Ground Sampling Distance

The Ground Sampling Distance (GSD) is the distance between the centre points of two consecutive pixels measured on the ground.

To determine an acceptable GSD for the mission, we performed an experiment whereby we used a Sentinel 2 image from the Canberra (ACT) region and resampled it to simulate different GSDs. We used the satellite image (captured on 25-01-2020) to compute FMC with an adapted version of the Yebra et al. (2018) algorithm. Importantly, we assumed that (1) the GSD of the Sentinel image was the same as the resampled pixel size of the image (i.e. 25 m), and (2) that the GSD did not vary over the study area. In Figure 3 we show the FMC at GSD = 25 m with resampled images at 50 m, 70 m, 100 m, 250 m, and 500 m (e.g. MODIS resolution). Visually, images with 25 m and 50 m pixels

provide a similar amount of information and allow easy identification of ridges, valleys, and places where potential soft containment lines (e.g. wetter patches of vegetation) could be located (Figure 3B/C). Additionally, studies suggest that some algorithms for species discrimination and phenology have similar accuracies when pixel sizes ranging between 20m and 60m are used (Roth et al., 2015; Younes et al., 2021).

Resolutions between 25-70 m provide superior quality information on the FMC gradients in the landscape at various levels of detail. Considering that FMC maps may be used for prescribed burning, firefighting efforts, and other fuel management activities, GSDs of 100 m or greater are too blurred and less informative, especially in terrains with high heterogeneity (Figure 3E/F/G).

As a result, a GSD greater or equal to 100 m is undesirable, but an acceptable GSD for the OzFuel sensor would be between 20 and 60 m. Keeping in mind that OzFuel’s aim is to deliver critical data to boots-on-ground (see Section 1.3), a GSD of 50 m would provide enough information for decision-making while reducing the size of the file and accommodating for a larger swath width (Section 2.4).

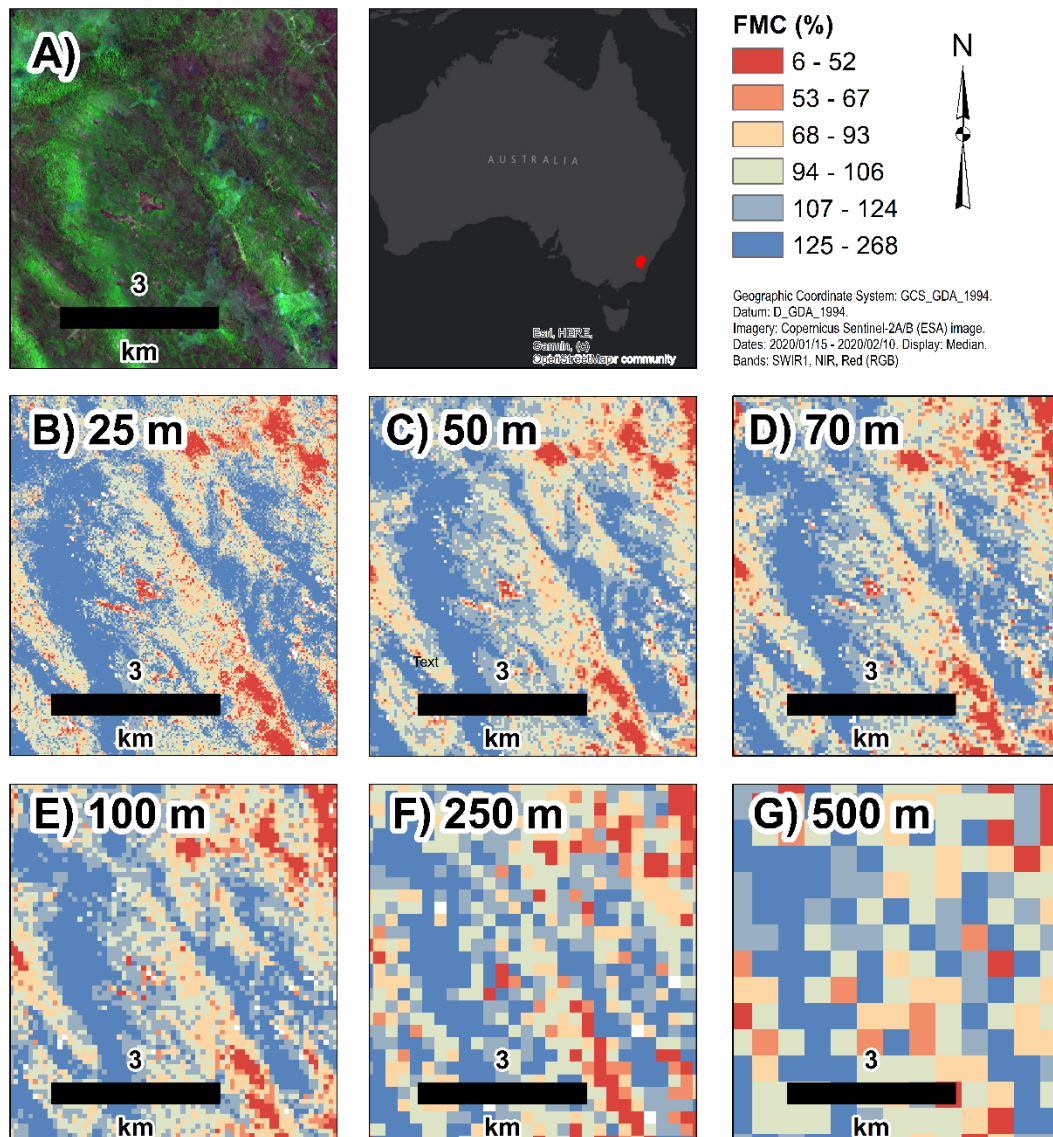


Figure 3: Fuel Moisture Content (FMC) represented at 25 m, 50 m, 70 m, 100 m, 250 m, and 500 m per pixel for an area in the Canberra (ACT) region in panels B-G respectively. Panel A) shows a false colour composite (SWIR, NIR, Red) Sentinel 2A/B image of the study area.

2.4 Swath width

For satellite sensors, the swath width is the strip of the surface of the Earth where data is captured. For operational purposes, a larger swath width is better, if the spatial resolution of the imagery is not compromised.

A swath width between 100 km and 150 km, would be desirable. However, given the constraints of the currently available sensor (i.e. 320 spatial pixels), achieving this swath width would compromise the GSD. The expected swath widths for different GSD, using the currently available sensor, are shown in

Table 1. A swath width of 16 km - 19.2 km is acceptable for the first generation OzFuel-1. Future versions of OzFuel should have larger swath widths without compromising the GSD.

Table 1: Expected swath width given a GSD

GSD (m)	No. of Pixels	Nominal swath width (m)
20	320	6,400
30	320	9,600
40	320	12,800
50	320	16,000
60	320	19,200

2.5 Suggested solar irradiance model

Solar irradiance refers to the amount of electromagnetic radiation emitted by the sun. It plays a significant role in the energy and flux changes between the atmosphere and the Earth's surface. Therefore, accurate measurements are essential (Huang et al., 2019). Solar irradiance can be measured by space-borne and land-based sensors, or it can be estimated numerically through modelling. Measurements of solar irradiance can have coarse spatial resolution (1-20km) in the case of satellites, or can be sparsely distributed in the case of land-based sensors. In contrast, numerical modelling can recreate different atmospheric conditions over wide areas with ease.

One of such numerical models, the Simple Model of the Atmospheric Radiative Transfer of Sunshine (SMARTS) model, is widely used and can be a starting point for the design of the OzFuel sensor. For example, the American Society for Testing and Materials (ASTM) adopted the reference spectra from a previous version of SMARTS (v 2.9.2) for two of their standards (G172-03, and G177-03), and the International Electrotechnical Commission (IEC) has also used SMARTS in their standard (IEC 60904-3:2016) for photovoltaic systems.

SMARTS was developed by Gueymard (1995), and it was recently updated to version 2.9.8 by Gueymard (2019). The model has a spectral range between 200-4000 nm, with 2002 spectral bands,

and estimates the irradiance at the surface of the Earth at 1361.10 W/m². The model can be downloaded from the NREL website (<https://www.nrel.gov/grid/solar-resource/smarts.html>), and is available for computers running Windows and Mac operating systems. The user manual is only available for version 2.9.5 and can be attained on the same website (<https://www.nrel.gov/grid/solar-resource/smarts-files.html>), free of charge. The model can provide simulations for: "Direct normal irradiance", "Diffuse tilted irradiance", "Global tilted irradiance", "Beam normal + circumsolar", "Diffuse horizontal-circumsolar", "Zonal ground reflectance", some of which are shown in Figure 4 (see Gueymard (2019) for details).

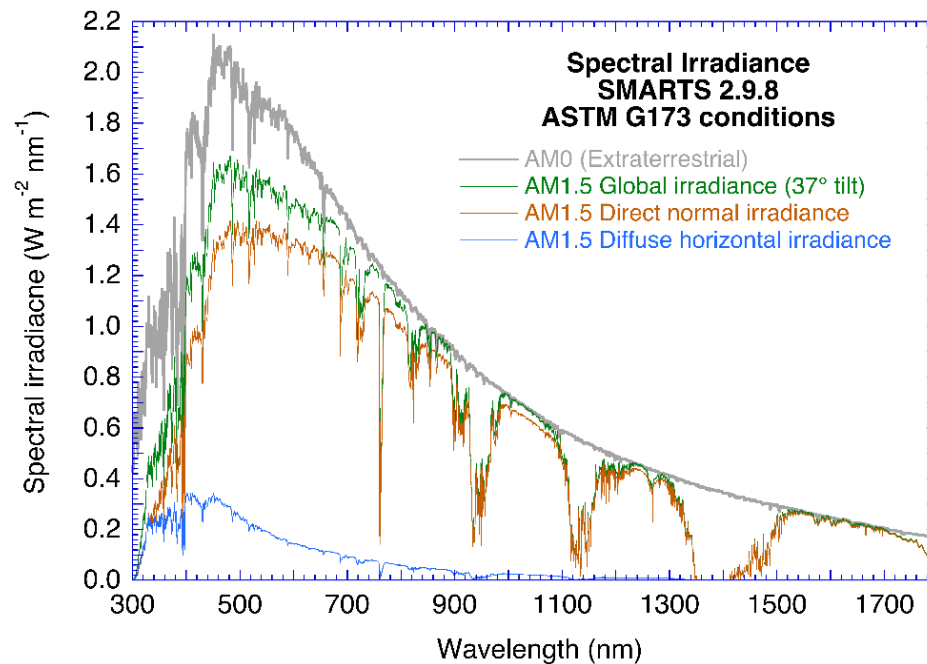


Figure 4: Spectral irradiance produced by the SMARTS model using the conditions established under U.S. standard ASTM G173 in the 300-1800 nm range. Source: Solar Consulting Services (<https://solarconsultingservices.com/smarts.php>)

According to Gueymard (2019), the latest version of the model includes an updated carbon dioxide concentration in the atmosphere (~410 ppm), as well as the ability to specify local conditions for water vapour, ozone and carbon dioxide, three major absorption gases (Figure 5). The ability to specify the local conditions of the atmosphere could be useful for the OzFuel project, where the 'local conditions' can refer to the atmospheric composition of the Australian continent or, more narrowly, to the average conditions of south-eastern Australia. Input parameters for the SMARTS model include pressure (mb), ground altitude (km), height above ground (km), relative humidity (%), precipitable water (cm), ozone (atm-cm), aerosol optical depth, and visibility (km).

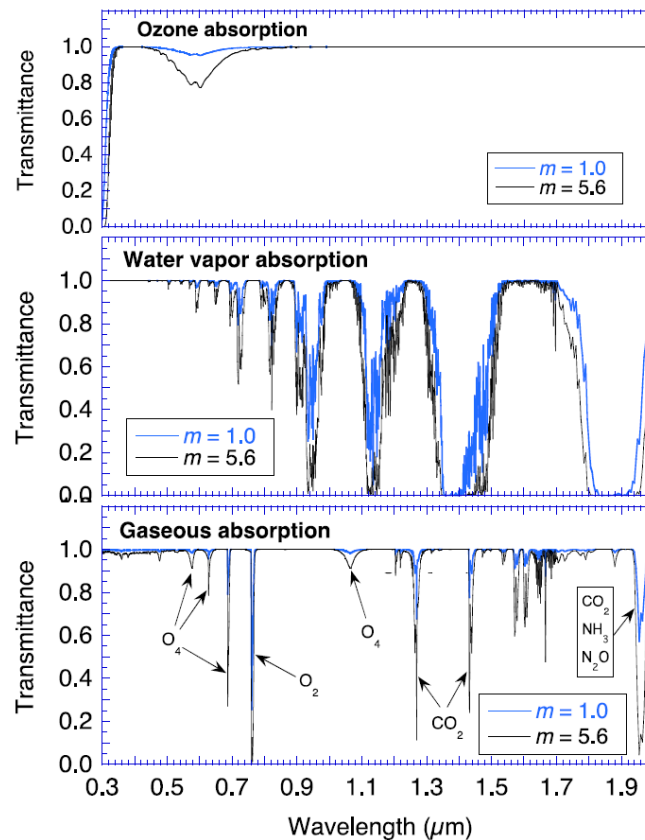


Figure 5: SMARTS transmittance of absorption gases. The figure shows the ozone absorption (Top), water vapour absorption (Middle), and the absorption of other gases (bottom) in the 300-2000 nm range. Source Gueymard (2019).

2.6 Albedo

Albedo varies with forest structure, canopy cover, tree height, and other biophysical and environmental parameters (Hovi et al., 2019). Albedo values for forested areas range between 10-20%, with eucalypt forests on the lower end of the range (Sharma, 1984).

The SMARTS model includes 66 albedo references for different vegetation types (e.g. conifers, oak), human-made materials (e.g. concrete, plywood), water, soils and rocks (e.g. clay, gravel) that can be used as a starting point for the OzFuel project.

In addition, albedo measurements can be obtained from the MODIS (Moderate Resolution Imaging Spectroradiometer) MCD43A3 Version 6 Albedo Model dataset (Schaaf and Wang, 2015). This dataset provides both Black-sky and White-sky albedo at a 500m resolution for the visible-NIR (460, 555, 659, and 865 nm) and in SWIR bands (1240, 1640 and 2130 nm).

2.7 Spectral characteristics of the OzFuel sensor

In this section, we describe the desired spectral characteristics of the OzFuel sensor, the regions of the spectrum that should be avoided, and the ones most useful to monitor changes in fuel moisture content.

2.7.1 Atmospheric absorption features

Experiments have found around 30 absorption features associated with atmospheric gases between the 500-2500 nm range (Cui et al., 2015). In wavelengths between 1000 – 2500 nm, there are three main regions where the incidental energy from the sun is absorbed by the atmosphere, mainly related to the presence of water (H₂O) and carbon dioxide (CO₂) (Figure 5). The absorption features of other gases (e.g. O₂, O₃) in this range of wavelengths (i.e. 1000 – 2500 nm) can be ignored for now.

Broadly, atmospheric absorptions features should be avoided by the OzFuel sensor to ensure enough light reaches the sensors and information can be gathered. Therefore, the following regions of the spectrum should be avoided: 1100-1162 nm, 1336-1492 nm, and 1742-2075 nm.

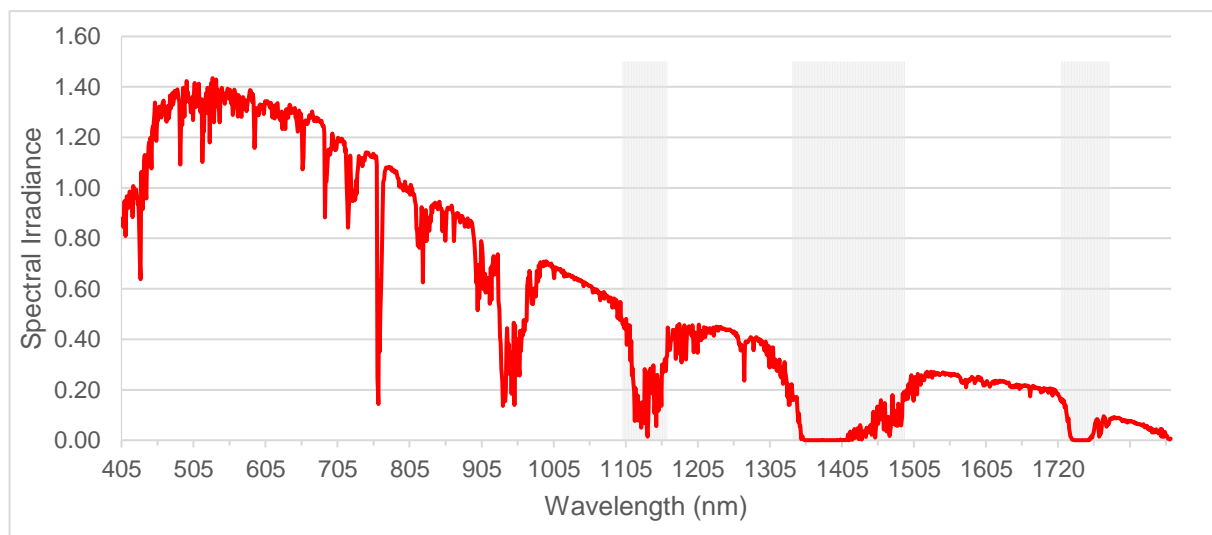


Figure 6: Solar irradiance derived from SMARTS v. 2.9.2 (red line). Atmospheric absorption features (shaded areas). Source: <https://www.nrel.gov/grid/solar-resource/spectra-am1.5.html>

2.7.2 Vegetation absorption features

Figure 7 shows how vegetation interacts with sunlight and how it is captured by a satellite sensor. The horizontal axis shows the wavelengths of light, and the vertical axis shows the amount of light reflected back to the sensor by the vegetation between 400 – 2500 nm. In the SWIR region (1100-2500 nm), healthy (i.e. hydrated) vegetation will display four troughs related to the amount of water in the leaves (Curran et al., 2001). The location and magnitude of these troughs vary with the health of the vegetation and the species. Some of these features seem to coincide (at least in part) with the location of the spectral bands of different existing satellites (Figure 8).

In Figure 8, we present the spectral signature of a eucalypt leaf, and the location of the spectral bands of 24 satellites that are commonly used for vegetation monitoring. These satellites were chosen as a source of comparison because they have spectral bands in the visible, NIR and SWIR regions of the spectrum. The OzFuel mission focuses specifically on the Short-Wave Infrared (SWIR)

region (1100-2500 nm) of the electromagnetic spectrum because that is the region where moisture, lignin, and cellulose content are more easily detected. Cellulose and lignin are the two main components of dry matter content (DMC, Equation 1) of leaves. Estimating the DMC is important because the mass of the leaves is related to their flammability. The more mass in the leaves, the more fuel there is to burn, and the longer a fire will last.

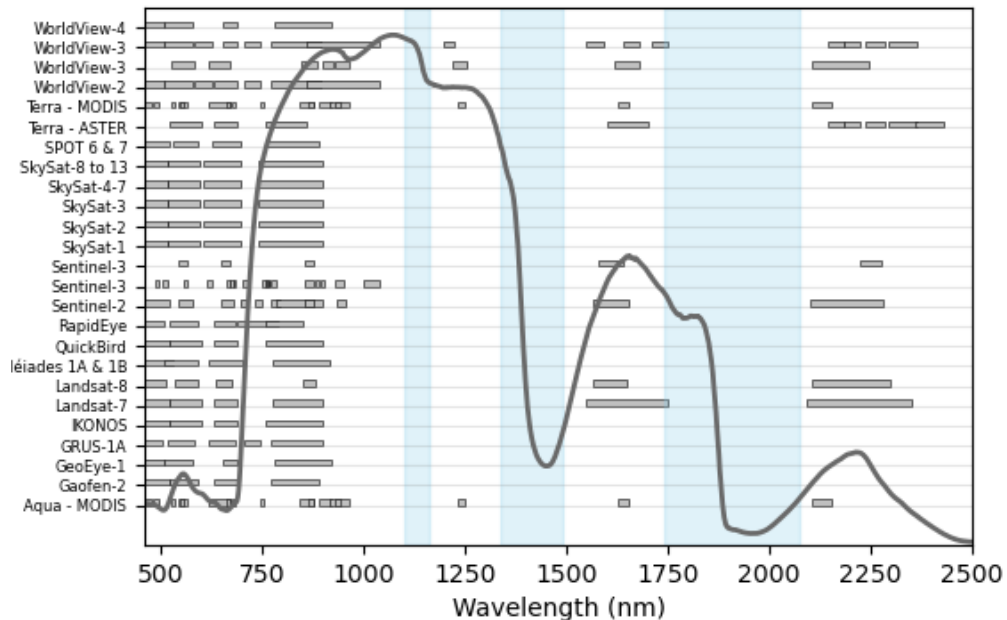


Figure 7: Location of the spectral bands of 25 Earth Observation satellites in the 400-2500 nm range (horizontal bars). The grey line represents the spectra of a leaf simulated in PROSPECT. Blue shaded regions represent water absorption bands.

In the SWIR region, water content in the leaves is what determines how much sunlight is absorbed, and how much sunlight is reflected back to the sensor. Here, the Equivalent Water Thickness (EWT, Equation 1) provides useful insights into the amount of water in the vegetation. Healthy vegetation will hold more water in their leaves and will reflect less SWIR radiation back to the sensor (e.g. $EWT=0.05$ in Figure 8). In contrast, dry vegetation will hold less water, and will reflect more SWIR radiation to the satellite (e.g. $EWT=0.02$ in Figure 8). This is important for monitoring bushfire risk because there is a higher risk of bushfires when the vegetation is dry (i.e. has low water content in the leaves). To provide an accurate characterization of the fuel loads, OzFuel will provide estimates of the amount of water (i.e. EWT), and the dry matter content (DMC, Equation 1) in eucalypt leaves.

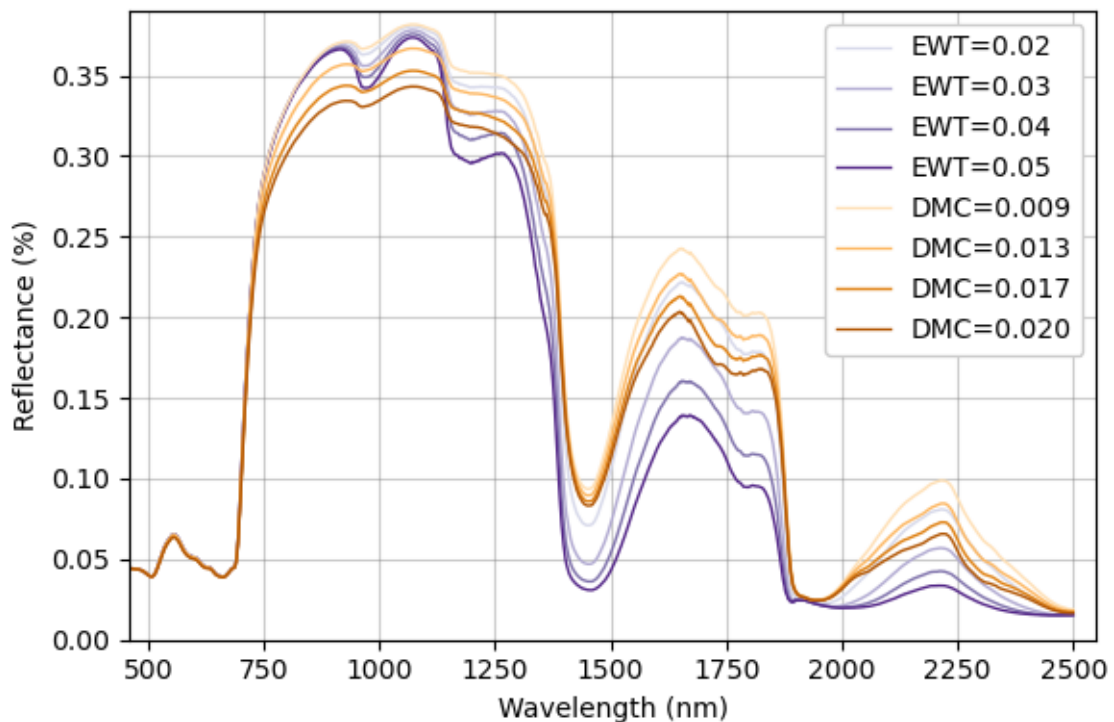


Figure 8: Leaf spectra with varying amounts of water (EWT, purple lines), and mass (DMC, brown lines). Spectra simulated in PROSPECT (<http://opticleaf.ipgp.fr/index.php?page=prospect>).

The chemical composition of leaves also plays a role in the reflectance in the SWIR region. For example, organic compounds such as cellulose, lignin, and waxes absorb and reflect energy in this region of the spectrum. However, these features may be weak and can be easily masked by the water content in the leaves (Varshney and Arora, 2004). To inform the state of vegetation and, thus, bushfire risk across Australia, OzFuel will focus on examining changes in the cellulose and lignin contents of live vegetation. More mass in the leaves means there is more combustible material (i.e. fuel). For example, leaves with higher DMC (DMC=0.020 in Figure 8) reflect light differently to leaves with low DMC (DMC=0.009 in Figure 8). Dry matter content is expressed as the ratio of the leaf's dry weight to its area ($DMC = \frac{W_d}{A}$) (Féret et al., 2019).

From Figure 8 it is clear that changes in EWT and DMC alter the spectral signature of leaves. The spectral bands for OzFuel should cover the wavelengths where these differences are greatest, but at the same time, in wavelengths that are specific for the three main target compounds: water, lignin, and cellulose.

Studies have found that the following wavelengths are useful for detecting lignin and cellulose in dry or dead vegetation: 2180 – 2222 nm, 2310-2380 nm, 2000–2050, 2080–2130, and 2190-2240 nm (Daughtry, 2001; Daughtry et al., 2001; Nagler et al., 2003). In Figure 9 there is a summary of the wavelengths that have been identified as important for detecting changes in lignin and cellulose.

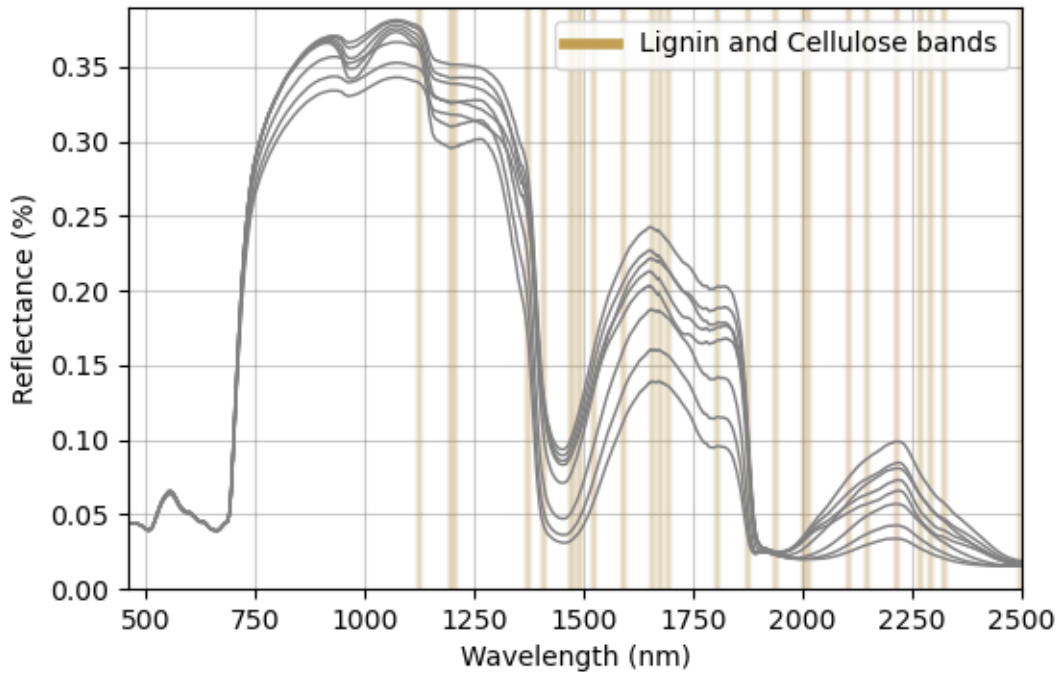


Figure 9: Spectral bands associated with leaf cellulose and lignin in the 1000-2500 nm range. Grey lines represent leaf spectra simulated in PROSPECT. Brown lines represent the spectral bands related to lignin and cellulose. Sources: (Curran et al., 2001; Daughtry et al., 2001; Jin et al., 2017; Nagler et al., 2003; Soukupova et al., 2002; Terdwongworakul et al., 2005; Thulin et al., 2014; Wessman et al., 1988).

2.7.3 Proposed spectral bands

For the first iteration of the OzFuel sensor, we propose the four spectral bands (Table 2). Because OzFuel aims to detect changes in FMC, it is important to target the wavelengths that provide information related to vegetation water content (EWT) and DMC.

In this case, we have selected four spectral bands linked to water, cellulose, and lignin. This data is the basic input for the proposed products (Section 3), and it is crucial for 'pre fire' management activities and for the characterisation of fuel loads across Australia. In addition, we propose very narrow spectral bands (10 nm) to specifically target FMC in eucalypt forests.

Table 2: proposed bands for the OzFuel sensor. Initial estimation of band centres and band widths

No.	Band Centre (nm)	Band width at FWHM (nm)
1	1205	10
2	1660	10
3	2100	10
4	2260	10

Later iterations of the OzFuel mission will include more spectral bands, with the potential for making OzFuel a multi-satellite hyperspectral mission.

The proposed bands are subject to change, depending on the results from field and laboratory experiments that we are currently performing to characterise the spectra signature of Eucalypt species in detail.

As shown in Figure 10 the selected spectral bands for OzFuel allow for good separability of leaves with varying moisture (i.e. Effective Water Thickness – EWT), and dry matter content (DMC). Here, we assume that EWT and DMC are proxies for Fuel Moisture Content and Dry Matter Content, respectively.

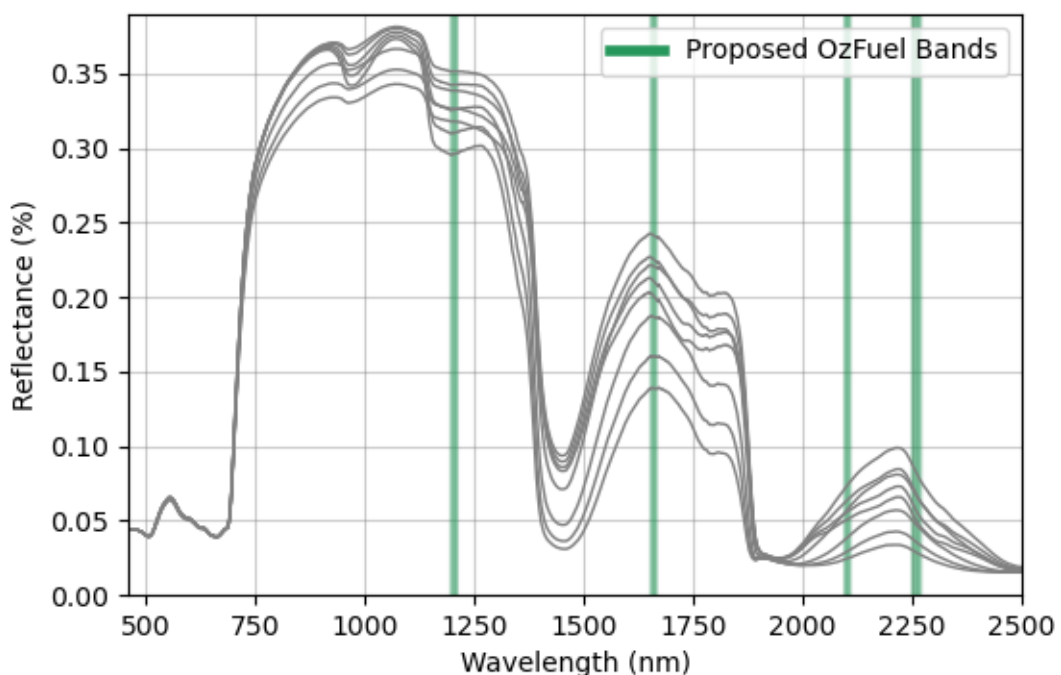


Figure 10: Spectral bands proposed for the OzFuel mission (green). Grey lines represent leaf spectra simulated in PROSPECT.

2.8 Radiometric resolution

The radiometric resolution of a sensor refers to its ability to discriminate changes in the incoming energy. Higher radiometric resolution means that the sensor can discriminate smaller changes in the energy that reaches the sensor, resulting in more information being captured. For the OzFuel sensor, a high radiometric resolution is desired to detect slight changes in FMC (EWT and DMC) in eucalypt forests.

To ensure proper sampling of the dry and wet properties of the vegetation, between 12 and 16 bits of radiometric resolution are needed.

2.9 Signal-to-noise ratio

The signal-to-noise ratio (SNR) refers to the relationship between the pixel values of the target feature (i.e. radiance), with the pixel values of the target feature plus elements that contribute to uncertainty in the signal level (Fiete and Tantaló, 2001). Some of the elements that cause noise include atmospheric scattering, fluctuations in the rate of arrival of photons to the sensor, variations in the voltage of the instrument (i.e. dark noise), and others. Importantly, (1) there are several ways of calculating the SNR (Fiete and Tantaló, 2001), making the comparison of SNR between sensors a complicated task, and (2) SNR varies between regions of the electromagnetic spectrum (Varshney and Arora, 2004).

For the purposes of this document, we will assume the same SNR as the Sentinel-2 to facilitate the comparability between OzFuel, Sentinel-2, and Landsat 8 sensors. In the 900-2500 nm wavelength range, SNR values for the Sentinel-2 MSI instrument are as shown in Table 4. These values do not necessarily coincide with the proposed spectral bands presented in section 2.7.3, however they serve as a reference point. Whenever possible, SNR values should be 100:1 or higher.

2.10 Geographical coverage

OzFuel aims to image all the Australian mainland and Tasmania.

2.11 Mission specifications summary

The contents of Part 1 of this report are subject to change depending on the field and laboratory experiments which are due to begin Q3/4 2021. We shall update the information of this document when new information is available. A summary of the remote sensing end user requirements from section 2 is provided below.

Table 3: Summary of user requirements for the OzFuel mission.

Characteristic	User requirement
Revisit time (temporal resolution):	6-8 days
Time of observation:	Diurnal observations, preferably between 12h00 and 14h00
Ground sampling distance:	50m
Swath width:	At least 16 km
Albedo	10-20% for eucalypt forests
Spectral range:	1200 – 2300 nm
Spectral band centre:	1205 nm
	1660 nm
	2100 nm
	2260 nm
Number of Spectral bands:	3 – 4 bands
Radiometric resolution:	12 to 16 bit
Signal-to-Noise ratio:	100:1 or better
Geographical coverage:	Australian mainland and Tasmania

3 Data products

The following products are intended to be generated from OzFuel:

Level 0 products: Raw data at full space/time resolution with all supplementary information (i.e. metadata) to be used for subsequent processing (e.g. orbital data, time conversion, state of the sensor, etc). Level 0 data will be time-tagged for ease of use.

Level 1A products: Level 0 product with the necessary geometric and radiometric corrections applied. Level 1A products annotated with satellite position and consists of Top of Atmosphere (TOA) radiance ($W \times m^{-2} \times sr^{-1} \times \mu m^{-1}$) data. Level 1A products are not quality-controlled.

Level 1B products: Level 1B product orthorectified, re-sampled to a specific grid and geo-located. Re-sampling can be performed using several methods including bi-cubic convolution interpolation or nearest neighbour.

Level 2 product: product 1B with atmospheric corrections. Level 2A product consists of surface reflectance (unitless) data.

Level 3 product: maps of Fuel Moisture Content and dry fuel loads. Level 3 products should be updated frequently to provide information to end users.



Table 4: Comparison between Sentinel-2 and Landsat 8 sensors. Source: (ESA and Agency, 2015; USGS, 2019).

Sensor	Central wavelength / wavelength range (nm)	Bandwidth (nm)	Reference radiance - Lref (W m ⁻² sr ⁻¹ μm ⁻¹)	SNR @ Lref	Reported SNR	GSD (m)	Radiometric resolution	Swath width (Km)
Sentinel 2	945	20	9	114		60	12 Bit	290
Sentinel 2	1375	30	6	50		60	12 Bit	290
Sentinel 2	1610	90	5	100		20	12 Bit	290
Sentinel 2	2190	180	1.5	100		20	12 Bit	290
Landsat 8	1363 - 1384				165	30	12 Bit	190
Landsat 8	1566 - 1651				265	30	12 Bit	190
Landsat 8	2107 - 2294				334	30	12 Bit	190



Part 2: OzFuel Technical Overview

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4. Introduction

OzFuel is being developed in parallel with the CHICO mission, a dual-use hyperspectral imager (ANU and partners). While each pathfinder has unique user requirements, both serve as a staged series of development missions to de-risk critical sovereign capabilities to enable larger, fully-operational national satellite missions (Figure 1).

This section identifies a staged development pathway focusing on delivery of high-value intermediate data products (relevant to bushfire hazard mitigation and the wider industry) while securing a future capability by de-risking technical development. The ideal OzFuel mission requires a challenging combination of high ground resolution, a wide field, and (cloud free) repeat imaging cadence that will be hard to deliver with a first-generation micro/smallSat mission. Indeed, a modest constellation of satellites will likely be required. However, a staged series of development missions will deliver key end-user value-added data products while demonstrating high Technology Readiness level (TRL9) for the critical components with an acceptable risk profile for each development stage.

5. OzFuel sensor overview

The OzFuel mission represents part of a staged solution to Low Earth Orbit (LEO) bushfire fuel and environmental monitoring. The OzFuel-1 sensor is a small form-factor multispectral imager operating at short-wave infrared (SWIR) wavelengths ($\lambda = 1\text{-}2.5\ \mu\text{m}$). A representative focal plane format is shown in Figure 11. It shares many operational design characteristics with the CHICO hyperspectral visible light satellite development also underway at ANU. CHICO, funded by the Defence Materials Technology Centre (DMTC) as part of the High Altitude Sensor System (HASS) program, is a partnership with CSIRO and Canberra-based space systems operator Skykraft. While the CHICO concept will operate at visible light wavelengths using silicon CMOS detectors, the CHICO project presents a logical conceptual evolution for future phases of the OzFuel mission to deploy shortwave infrared (SWIR) hyperspectral sensing. The details of the current OzFuel-1 specification are presented in Table 5 alongside those of the CHICO sensor system for reference.

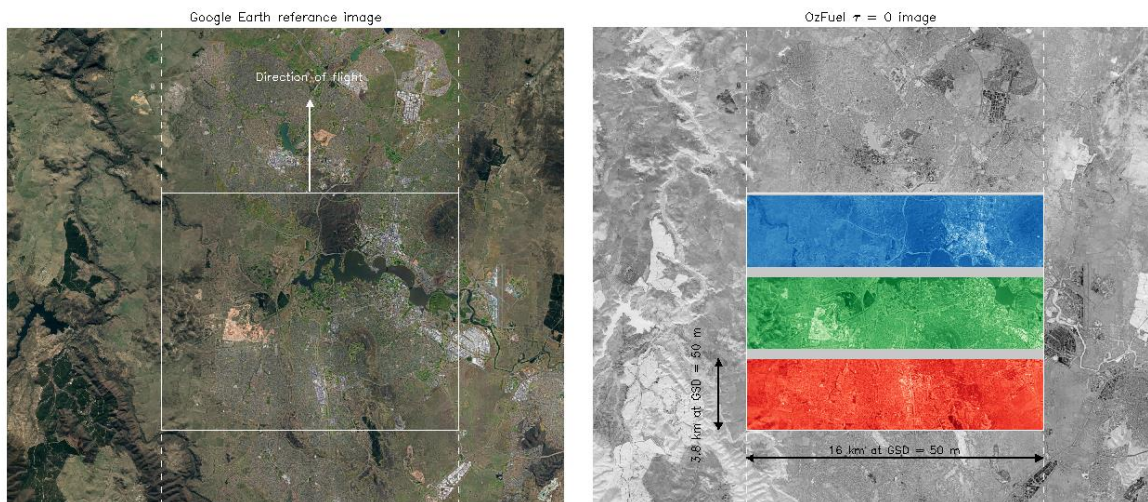


Figure 11: A representation of the OzFuel focal plane is shown alongside a reference (visible light) aerial photography image. The image to the left shows the hypothetical footprint of the OzFuel-1 sensor (single exposure) overlaid on Lake Burly Griffin (Canberra, ACT). The swath width and indicative direction of flight are shown. The right-hand image shows the OzFuel sensor focal plane, represented with independent SWIR filters (three are shown; OzFuel-1 will likely deploy four). Arrayed along the satellite line of flight, each filter sees part of a common swath and produces a long contiguous image track as the satellite passes over the scene.

Table 5: SmallSat sensor multi-mission specification

	Requirement	OzFuel-1	Target specification	CHICO parallel mission
Spatial	Spatial resolution – GSD			
	<i>Across-track (nadir)</i>	50 m	20 m	20 m
	<i>Along-track (nadir)</i>	50 m		
	Swath width (nadir)	16 km	20 km	20 km
Spectral	Spectral range	Multispectral	Hyperspectral	Hyperspectral

		$1 < \lambda < 2.5 \mu\text{m}$	$1 < \lambda < 2.5 \mu\text{m}$	$0.4 < \lambda < 0.82 \mu\text{m}$ Parallel glint channel $0.84 < \lambda < 0.9 \mu\text{m}$
	Number of bands	4	300	85
	Spectral resolution	15 nm	5nm	3-8 nm
	Spectral calibration accuracy (nm)	1 nm	0.5 nm	0.1 nm
Radiometric	Dynamic range	16 bit ADC	12 bit ADC	16 bit ADC
	Signal-to-noise ratio			
	<i>Day</i>	~250		300
	<i>Night</i>	> 10	n.a.	n.a.
Other	Orbit			
	<i>Type</i>	LEO	SSO	LEO
	<i>Altitude</i>	600 km	705 km	600 km
	Image Acquisition and data handling			
	<i>Frame rate</i>	150 Hz	325 Hz	325 Hz
	<i>Data compression</i>	n.a.	AI assisted value added data preprocessing	n.a.

5.1. Mission risk profile and key technology development stages

Table 6: Technology developments mitigated with each generation of OzFuel.

Item	Current TRL	OzFuel-1 – T0+ 18 months	OzFuel-2 – T0+36
Filter definition	Concept	TRL9	TRL9, larger filter or gradient filter hyperspectral
Bus system (12U)	TRL8	TRL9	n.a.
Bus system “larger sat”	TRL7	n.a.	TRL9
Telescope	Concept	TRL9	TRL9
Focal plane detector	TRL7	TRL9	TRL9, larger form factor higher ground resolution

Controller	TRL4	TRL9	TRL9 higher performance modes enabled
AI	TRL5-9 (depending on application and configuration)	TRL6 (lab testing only)	TRL9

6. OzFuel capabilities & sub-systems considerations

6.1. High ground resolution

Ground resolution is a central element of any remote sensing system. There are two critical aspects of mission design that dictate achievable ground resolutions: i) the diffraction limit of the optical system; and ii) the relative motion of the satellite platform with respect to the ground.

6.1.1. The diffraction limits

High ground resolution generates a number of program challenges. At shortwave infrared wavelengths, a small telescope system can become diffraction limited such that the fundamental ground resolution achievable is dictated by the diameter of the sensors' primary optics and the wavelength of observation. This follows the Airy diffraction limit:

$$\text{Diffraction limited angle, } \theta(\text{rad}) = 1.22 \times \frac{\lambda_{\text{obs}}}{D_{\text{Tel}}}$$

The implication for a range of observational wavelengths and sensor sizes is presented for a range of representative systems properties in Table 7. For a remote sensing system in a Low Earth Orbit altitude of around 600 km, a 50 m ground resolution can be delivered with a telescope of 85 mm diameter at a wavelength of 2.5 μm (OZFUEL-REQ-INST-0002; relevant documentation in Appendix A). This scales linearly with wavelength and hence at 1 μm the same sensor could in principle deliver imagery at a ground resolution of 20 m. Fundamental physics dictates that a larger telescope diameter is necessary for finer ground scale regardless of whether such light gathering power is required for sensitivity.

Table 7: Fundamental diffraction limited resolution (from 600 km Low Earth Orbit) - Airy disk Full Width at Half Maximum (FWHM). Many missions operate below the fundamental limit with a Ground Sampling Distance (GSD) limited by pixel sampling scale.

Fundamental Limiting GSD (m) from 600 km	Telescope effective diameter (m)					
	<i>OzFuel-1, CHICO</i>	<i>AquaWatch, Sentinel-2 (15 mm)</i>				<i>Hubble Space Telescope</i>
Wavelength (λ) (m)	0.1	0.2	0.3	0.5	1.0	2.5
0.4	2.9	1.5	1.0	0.6	0.3	0.1
0.6	4.4	2.2	1.5	0.9	0.4	0.2
0.8	5.9	2.9	2.0	1.2	0.6	0.2
1.0	7.3	3.7	2.4	1.5	0.7	0.3
1.5	11.0	5.5	3.7	2.2	1.1	0.4
2.2	16.1	8.1	5.4	3.2	1.6	0.6
2.5	18.3	9.2	6.1	3.7	1.8	0.7
3.0	22.0	11.0	7.3	4.4	2.2	0.9
5.0	36.6	18.3	12.2	7.3	3.7	1.5
10.0	73.2	36.6	24.4	14.6	7.3	2.9

6.1.2. Forward motion compensation

The second challenge for ground resolution is the relative ground motion of the satellite platform. For orbital altitudes of order 600 km, the relative ground speed for an overpassing satellite is of order 10 km s^{-1} . For a simple satellite imaging system, observing at nadir, this means the pixel crossing time (the time taken for any point on the ground to be blurred across one pixel in the image) is $\sim 1.3 \text{ msec}$ for 10 m (6.6 msec for 50 m; OZFUEL-SCI-OCD-0001; refer to Appendix A).

At the highest resolutions, pointing stability during an exposure will be a limiting factor for ultimate image resolution. However, for the resolution relevant to OzFuel (10–50 m), the most significant problem is platform forward motion relative to the ground. Counter rotation of the satellite platform as it passes over a region of interest, known as *forward motion compensation*, can reduce this effective transit speed, but this comes at the expense (technically and financially) of a much more challenging satellite attitude control system. Typically, the only method for providing the tracking control signal is a suite of star trackers with high astrometric precision and sensitivity. Once the pointing signal is generated by the star trackers, reaction wheels are typically needed to provide the torque required for platform motion control. Desaturation of the reaction wheels then typically requires a magnetorquer or similar to provide an efficient correction for the one-sided build-up of angular momentum. These systems all require power, take up payload volume, require controls, and add mission mass and system complexity (including single point failure or added system redundancy requirements).

A more appealing solution at first glance is to simply freeze-out this relative motion by reading the sensor system at a frame rate matched to the pixel crossing time of the ground resolution element. This will ensure that images are blurred only to the intrinsic pixelation limit of the sensor. This approach, related to the more general concept of Time-Delay Integration (TDI) imaging, trades demands on the bus systems pointing stability for complexity in the sensor system data rate, data volume, and frame to frame noise and integration time properties (OzFuel radiometry analysis and Operational Concept, OZFUEL-SENG-RANA-0001, OZFUEL-SCI-OCD-0001; refer to Appendix A). The challenge of TDI-like operations is that the necessary exposure rates (750 Hz for GSD = 10 m, 150 Hz for GSD = 50 m) generate large data volumes. This volume can be reduced by realising that not every image needs to be recorded (OZFUEL-SENG-RANA-0001), or through the use of onboard data processing and value-added data product generation with Artificial Intelligence (AI) which can reduce the volume of data that must be routinely downlinked.

6.1.3. OzFuel GSD

These issues considered together lead us to propose an 85 mm square telescope aperture for OzFuel-1. It delivers sufficient ground resolution (<50 m at all SWIR wavelengths) while also providing adequate image sensitivity. Furthermore, it conforms to the industry convention "1U" cross sectional form factor, as well as a "3U" length scale with the necessary effective focal length without the need for high-risk fast optical systems. This system will be well matched to performance specifications of a high-grade SWIR focal plane detector driven by a dedicated high-speed electronics package (such as the SAPHIRA eAPD detector from Leonardo UK coupled with the ANU Rosella controller; see Section 3.5).

6.2. Swath width

The swath width is the angular width of the field of view perpendicular to the direction of motion of the satellite sensor system. Maximizing the swath width provides the widest possible areal coverage on each satellite pass. This in turn increases the repeat observation rate achievable for any given point on the Earth's surface for any given mission orbital profile. However, wide swath width imposes two important technical difficulties on any sensor system.

6.2.1. Sensor opening angle

The field of view of any imaging system is restricted to the range of angles over which the sensor system can accept incoming light. For a remote sensing platform operating at a LEO altitude of ~600 km, a projected ground swath width of 10 km requires a range of acceptance angles for the telescope system of 1° (likely implemented as $\pm 0.5^\circ$ around the optical axis). This remains relatively linear out to $\sim 30^\circ$ (as $\pm 15^\circ$) for ~ 300 km swath width.

However, large opening angles are challenging for optical design. A common rule of thumb for an imaging system that is required to retain high image quality (i.e., one whose intrinsic resolution is dictated simply by pixelation from the chosen focal plane format and not be internal aberrations and distortions) should restrict the optical acceptance angle to 2 - 5° , with the range dictated by restrictions on the number of optical elements that can be employed, and the design risk considered acceptable in the adopted surface figures. Wider fields will suffer significant optical aberration unless complex aspherical surface figures, exotic glass choices, and large numbers of powered surfaces

(adding weight & volume while reducing transmission) can be tolerated in the design. In many cases, deployment of multiple sensors with narrower fields of view will provide a more satisfactory data outcome.

Wide field imaging systems present additional optical challenges at the focal plane. Trivially, a wider field of view requires a larger focal plane than a narrower one (assuming a common detector pixel-pitch and GSD). This larger focal plane must all remain “flat” with respect to the depth of focus tolerance for the optical system. There will also be significant optical design tension between preserving a flat focal plane (simple designs usually generate focal surfaces with unacceptable curvature leading to defocus at flat detectors) and retaining a (telecentric) optical design in which light-rays arrive perpendicular to the detector array. Camera designs without this telecentricity are viable but lead to image aberration and sensitivity variation due to the depth of photon penetration into the detector surface.

Furthermore, a wide field of view sensor by design observes a ground scene over a wide range of illumination and observation angles due to the variable geometry across a wide area. This dictates an increased complexity of image analysis to account for the variable atmospheric absorption path lengths, surface glint (particularly for aquatic systems) and shadowing. The angular variation may also introduce a considerable ground sampled variation due to foreshortening.

6.2.2. Focal plane array

Array size limitations

Wide swath width requires a large focal plane pixel array unless a very large GSD is to be tolerated (trivially, a 10 km swath width, sampled at a GSD of 10 m pixel size requires a 1,000-pixel detector width). Large format detector systems are routinely available; however there are limitations. High-performance devices have historically been available with modest form factors (1k×1k; 2k×2k; 2k×4k; 4k×4k). More recently, large format devices of order 10k×10k have emerged (OZFUEL-OZFUEL-TRS-0003; refer to Appendix A). However, the major detector vendors are largely restricted to the maximum possible size by availability of large format, high-quality silicon wafers. The industry standard is 200 mm (8 inches), meaning at 10 μm pixel-pitch, a 20k×20k device represents a maximum size. Such a device will also be costly due to the exposure of the device to a single point failure rendering the whole processed silicon wafer invalid. This is seen in the relative cost of devices such as the Teledyne H2RG SWIR detector series with 10 μm, 15 μm and 18 μm pixel pitches, with the smaller pitch devices delivering higher viable device yield per wafer due to the smaller footprint allowing more devices per processed wafer.

A larger pixel count can be achieved with a focal plane detector mosaic. A single detector focal plane array is preferable when possible as it provides the simplest solution with minimal overhead for control electronics and support systems such as cooling.

Focal plane array mosaics

When monolithic detectors of the required format cannot be sourced, a focal plane detector mosaic becomes the only solution (see Figure 12). Mosaic fabrication introduces additional optomechanical design challenges:

- The focal plane mosaic array must be flat with respect to the optical focal plane to avoid defocus.

- Independent detectors should be aligned to produce a common Cartesian pixel grid across the mosaic. This can be challenging as the pixel structure is typically not well aligned with the outer die of the detector.
- Each detector will require independent control electronics and will require an independent calibration solution to remove image artefacts. A sensitivity artefact that leads to a calibration requirement can be seen in the mosaic in Figure 12, with one of the mosaic elements showing a clear spectral response variation to reflected light in the photograph.
- Inter-detector mosaic gaps are unavoidable. Three/four-side buttable detectors are available, but an inter-detector gap corresponding to 4-10 pixel (20-200 μm depending on pixel pitch) is usually unavoidable. While there are strategies for ensuring complete coverage (see the Sentinel-2 VNIR array, Figure 13), most introduce data processing complexity and are susceptible to variable illumination/observation angle changes between the non-simultaneous observation regions.

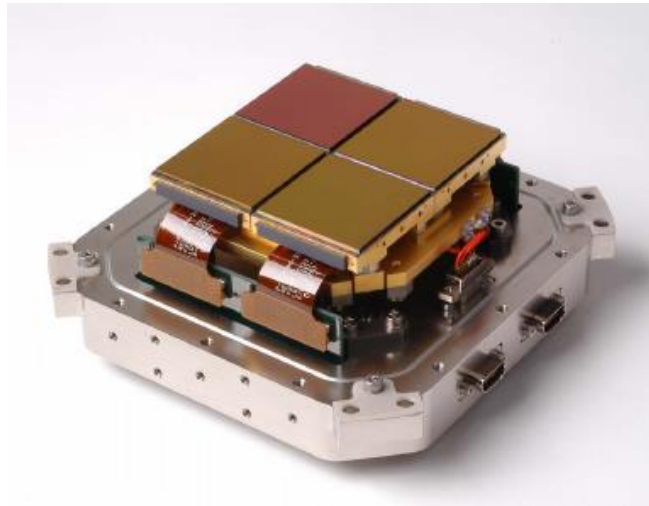


Figure 12: Based on the largest format SWIR detector available at the time of delivery, the focal plane array of the Gemini Observatory GeMS instrument McGregor et al. (2004) deploys a 2×2 mosaic of $2\text{k} \times 2\text{k}$ Teledyne Imaging systems HAWAII H2RG detectors with $18 \mu\text{m}$ pixels. The arrays are three-side buttable, leading to small caps (10 pixels wide) the active focal plane. The largest format science grade SWIR detector currently commercially available is the Teledyne H4RG, available in 10 and $15 \mu\text{m}$ pixel pitches.

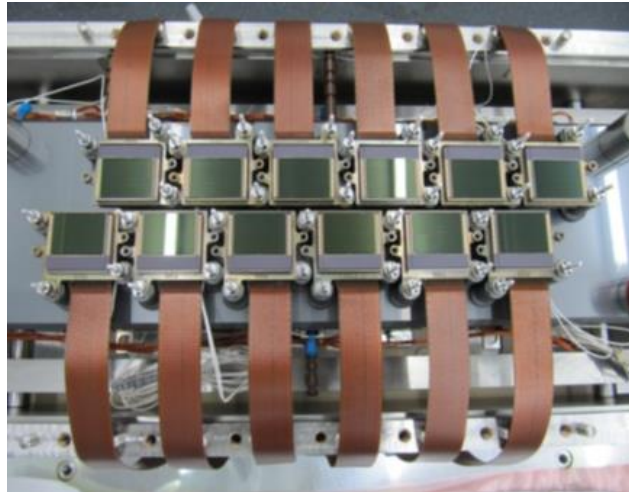


Figure 13: An exceptionally wide swath width was a design driver for the ESA Sentinel-2 mission. The large, 290 km projected ground distance, is not only optically demanding, but also required a large format offset mosaic focal plane (to provide contiguous pixel coverage) of 12 large format detectors. The VNIR is shown here. (image credit: <https://sentinels.copernicus.eu/web/sentinel/missions/sentinel-2/instrument-payload/>)

6.2.3. OzFuel Swath width and field of view

The initial OzFuel mission concept is baselined on the SAPHIRA SWIR detector from Leonardo UK due to ANU's current and ongoing experience with this device. The SAPHIRA device provides a modest form factor, 320×256 pixels, but is well suited to the frame rates necessary to provide high ground resolution via TDI-like observations. The short detector axis is sufficient to accommodate 3-4 independent filter pass bands while still providing significant 2D field of view for georeferencing and image alignment. The long axis provides a 16 km swath with a GSD of 50 m. This meets the basic specification outlined in Part 1 of this document.

A second generation OzFuel satellite (OzFuel-2) would seek to deploy larger form factor arrays (1k and 2k devices are available in the same family). The large array footprint would allow a wider swath width, or conversely a smaller GSD, once the control electronics architecture and thermal management system have been verified in the less demanding OzFuel-1 missions.

6.3. Satellite bus integration

The baseline model used to present likely OzFuel performance has been provided by Doug Griffin, Director and Chief Engineer of Canberra-based SME Skykraft. The design study presented is an evolution of a partnership between ANU, Skykraft, CSIRO and the Defence Materials Technology Centre (DMTC). The DMTC-funded CHICO project seeks to develop a visible light hyperspectral imaging system for coastal water monitoring applications. Material developed with the CHICO program is used here (by agreement of the CHICO partnership) to demonstrate how OzFuel could be deployed on a Skykraft platform either independently or alongside the CHICO sensor system. The trade study adopted the TheMIS (Thermal Management Integrated System) cooling and thermal control model from MSL (Section 6.4 Cooling systems). This system will be demonstrated in orbit (TRL9) as part of Skykraft operations in late 2021.

Launch and bus performance risks are common to any satellite missions and are not unique to the OzFuel mission concept. They are mitigated through careful selection of the correct partner(s) with the competing goals of: balancing the portfolio risk; controlling program costs; and stimulating growth, local capability and experience. The OzFuel concept as presented here has been developed in partnership with Skykraft (industry partners on the DMTC CHICO project) to present a viable roadmap for deployment of OzFuel (OZFUELOSENG-ICD-0002; refer to Appendix A).

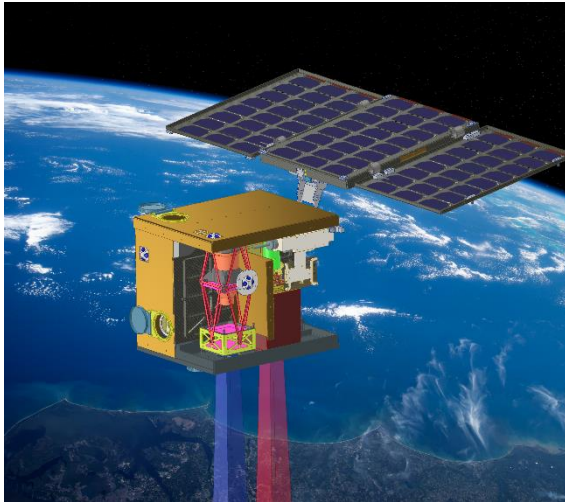


Figure 14: CAD rendering of the Skykraft ATM satellite platform is shown hosting the OzFuel SWIR multi-spectral sensor, mounted alongside the CHICO visible light hyperspectral sensor. The deployed solar array, and two of the internal star-trackers (for point control) are seen. The TheMIS cooler and thermal control system (from MSL) is obscured by the sensor payloads in this rendering.

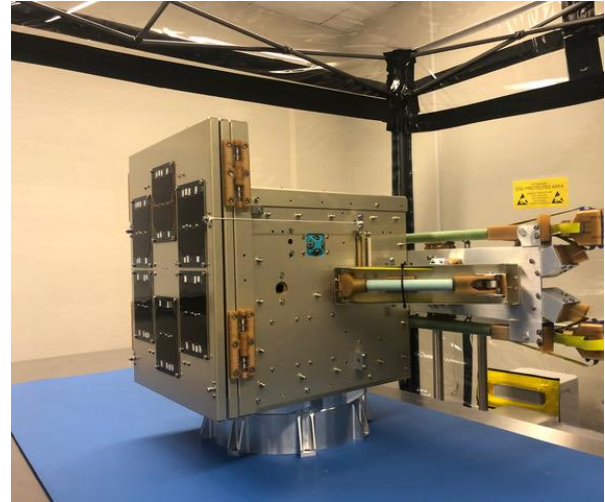


Figure 15: An example of the Skykraft ATM satellite platform is shown with stowed solar panel assembly.

The Skykraft small satellite platform technology (and related developments for space-based Air Traffic Management (ATM) system) is an ideal host for small scale remote sensing payloads providing a number of contemporary benefits:

- **Large size, weight and volume resources available to payload:** The Skykraft ATM platform departs from the CubeSat standard in order to host the large ATM surveillance and communications payloads. The availability of this sovereign spacecraft platform opens up the opportunity for ANU to design and operate innovative remote sensing payloads that bypass the Size, Weight and Power constraints imposed by CubeSat spacecraft.
- **Regular and economical access to space:** The development, operational deployment and ongoing maintenance of the Skykraft space-based ATM constellation provides regular (at least several times per year), opportunities to co-manifest spacecraft with remote sensing payloads with the Skykraft ATM spacecraft launches starting 2022 and then into the foreseeable future. This regular flight cadence and the economics of co-manifesting with the ATM spacecraft provides the right environment for innovation and rapid development of sovereign capability in this field.
- **Exploitation of Skykraft platform technology:** The Skykraft spacecraft platform, developed for its ATM business, provides the majority of critical capabilities needed to operate the remote sensing payloads. The economics of the development of the '210'

spacecraft for Skykraft's ATM constellation mean that NRE costs of adapting the platform to remote sensing applications are highly favourable. Indeed, collaboration between Skykraft and Melbourne Space Laboratory (MSL, Section 3.4) is using this model to retire program risk for the TheMIS cooling system, and in the process, providing a TRL9 solution for cooling for remote sensing payloads onboard the Skykraft ATM platform.

6.4. Cooling systems

Background information in this section, on COTS cooling systems and high TRL bespoke control systems, has been provided by Simon Barraclough (MSL) in collaboration with Douglas Griffin (Skykraft). – OzFuel Trade Study documents: "OZFUEL-OZFUEL-TRS-0001" & "OZFUEL-OZFUEL-TRS-0002" (refer to Appendix A).

The equilibrium temperature for a small satellite system in Low Earth Orbit is highly dependent on the specific geometry of the satellite system. However, the local ambient temperature within the satellite body would be expected to be in the range of 40-70°C.

Thermo-electric cooling is typically the option of choice for modest temperature reduction. It offers a mass and power efficient solution for visible light sensor systems as well as restricted wavelength SWIR systems (typically up to a wavelength of 1.7 microns but excluded from the 2-2.5 micron window due to limitations of InGaAs detector technology). Cooling to lower temperature using compact cryogenic coolers (such as the Thales Stirling cycle identified for OzFuel) is in principle readily achieved. However, performance of such systems on satellite platforms is compromised by the limited radiator area available which makes waste heat rejection challenging to operate high performance SWIR sensors at.

For SWIR observation in a TDI-like mode with pixels anywhere in the 10-50 m GSD range, the thermal load from the instrument and from the detector environment negligible (at least for daytime observations).

Thermal considerations are important for a number of reasons:

- Calibration stability, changing background loads at the few percent level, and variable thermal illumination across the field.
- The SWIR detectors need to operate reasonably cold, especially for wavelengths beyond 2.5 microns, at which the necessary sensor band gap becomes comparable to thermally excited electronics in an uncooled detector substrate, leading to significant dark current generation. The parasitic thermal load on a cooled focal plane array must be carefully controlled.

OzFuel is operating in the Short-Wave Infrared spectral region. This means that direct thermal emission from the low emissivity telescope optics is expected to be of limited concern at the operating temperature of 20-40 °C expected for a LEO smallSat in radiative equilibrium. However, high performance SWIR detectors capable of operating out to 2.5 μm required cooling to temperatures of ~100-200 K (-170 < T < -70 °C) in order to suppress excessive dark current to usable levels. Additionally, the detector enclosure – the high solid angle last surface seen directly by the detector which is not filled by the telescope pupil – is a unit emissivity surface that would flood the sensor with thermal background photons if not controlled. This leads to a requirement to implement three thermal zones for the OzFuel system:

- Warm Zone – Telescope and structure (20-40 °C)
 - This zone may be passively cooled and need only be stabilised, not actively controlled.
- Cool zone – Detector enclosure last scattering surface ($-70 < T < -20$ °C)
- Cold zone – ($-170 < T < -70$ °C)
 - Actively cooled region ensuring the detector temperature is cold enough for the required performance
 - Detector temperature must be stabilised ensure calibration stability.

This cooling regime is beyond that accessible with simple thermo-electric designs. Indeed, the most challenging element of cooling in this regime for a smallSat is the waste heat rejection due to the restricted size of radiator panels practical on a smallSat form factor.

It is proposed that the detector and its immediate environment for the OzFuel mission will adopt the thermal management strategy developed by the Melbourne Space Laboratory (MSL) team at the University of Melbourne. The MSL TheMIS control system (Figure 16), coupled to the Thales LSF9987 Stirling cycle cryogenic cooler (Figure 17), provides a COTS solution with current TRL6 heritage. This will be elevated to TRL9 in late 2022 as part of the ASA-funded SpIRIT mission managed by MSL.

An overview of the system has been provided to this OzFuel Pre-Phase A study by the SpIRIT Nanosatellite Technical Director, Simon Barraclough (MSL - "OZFUEL-OZFUEL-TRS-0001 – Cooling system"; refer to Appendix A). The ANU team has been collaborating with MSL on elements of the SpIRIT and SkyHopper missions. The MSL team's design heritage in satellite thermal systems management also informed the design evolution of the ANU 'Emu' space telescope (Gilbert et al., 2020, 2019; Mathew et al., 2020) which had adopted the previous generation cooling system recommended by MSL.

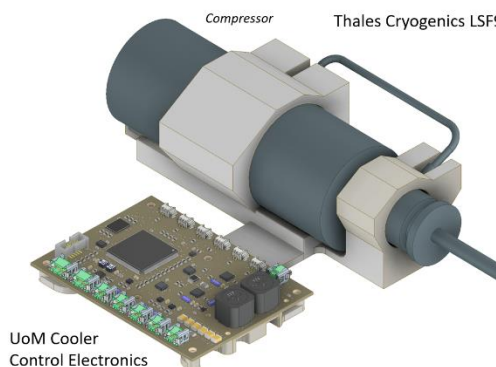


Figure 16: A CAD rendering of The MSL TheMIS system is shown.

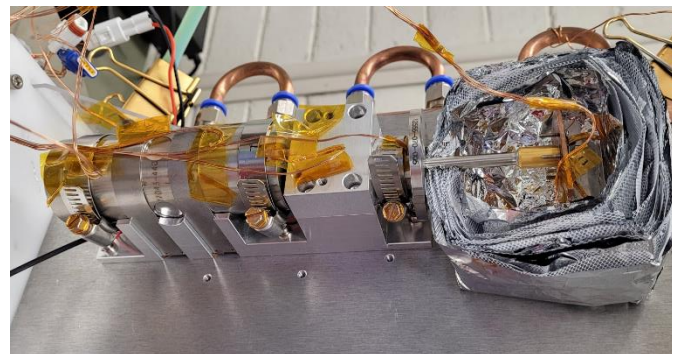


Figure 17: The Thales LSD9997 Stirling cycle cooler is shown in preparation for testing at MSL.

6.5. Focal plane array detectors and control systems

The OzFuel mission concept delivers high ground resolution (<50 m in the first instance but with a goal of 10-30 m using a larger format detector for OzFuel-2) via high frame rate imaging. This freezes out motion of the platform with respect to the ground, avoiding the need for costly (in terms of volume, weight, complexity and direct expense) attitude control systems that are challenging on a

smallSat platform. The necessary high frame rate places high demands on the associated control electronics driving the detector system. COTS control solutions typically cannot deliver the low-level detector control necessary to provide low latency data digitisation, particularly when interfacing with external on-board Artificial Intelligence (AI) processing solutions or when real-time data management is required for data compression via dropped redundant frames, or similar dynamic data manipulation is required.

ANU is developing the Rosella control system to address this problem. Based on Field Programmable Gate Array (FPGA) technology and building on laboratory developments for ground-based astronomical imaging camera systems, Rosella is a small form-factor (0.5 CubeSat U) control system capable of interfacing with any CMOS based visible/SWIR or longer wavelength detector technology, particularly those with no built-in pixel digitisation circuitry (i.e. most scientific grade devices). The modular control system is designed for high frame rate operations with parallel digitisation channels and the necessary clocking and power distribution systems (including filtering and stabilisation) to ensure the native sensitivity of the detector is preserved through the digitisation process.

Focal plane array detector choice for the OzFuel concept is based on the expediency of readily available technology during the initial development stage of the program. The stated requirement for OzFuel to image with at least one band in the 2-2.4 micron atmospheric window rules out low-cost Indium Gallium Arsenide (InGaAs) detectors due to their band-gap limitation restricting operations to below 1.8 microns. The preferred light-sensitive material for high-performance SWIR sensors is Mercury Cadmium Telluride (MCT, or HgCdTe), which is hybridised to a conventional silicon readout integrated circuit (ROIC). ANU has extensive experience with such devices from Teledyne imaging systems (the Hawaii detector array family). Other US and European vendors are available (e.g., Raytheon, Sofradir) and small formfactor devices are being actively fabricated at the University of Western Australia, providing a viable domestic solution.

OzFuel is built around the SAPHIRA MCT detector from vendor Leonardo UK. The SAPHIRA detector is an electron avalanche photodiode (eAPD) originally designed for low-noise and high-speed operations as an astronomical wavefront sensor. The current device is small, limited to 320×256 pixels, but specifically designed for high framerate with a large number of parallel readout channels. Large-format devices with similar pixel architecture are available from Leonardo, providing future upgrade paths for a larger format OzFuel mission, as well as next generation devices currently under development that promise even higher speeds.

6.6. Optics

The optical system for OzFuel is functionally identical to that under development at the ANU for the Emu astronomical survey telescope design for deployment on the International Space Station (Gilbert et al., 2020, 2019; Mathew et al., 2020). The small form factor of the telescope (~1 CubeSat U in cross-section) presents few optical challenges, with an on-axis catadioptric system providing a compact design with the correct focal length. The necessary sensitivity limits and diffraction performance for OzFuel-1, due to the 50 GSD, are achieved without the need for a bulky off-axis system. A more complex design for OzFuel-2, with larger optics, would be required for <20 m ground resolution, due to the demanding diffraction limit and decreased light return from a smaller ground source. A larger axis system would provide increased sensitivity due to the clear aperture. However, such systems require significant volume and common solutions. A three-mirror anastigmat (TMA) typically produces complex spatial distortion at the focal plane that introduces variable plate

scale (and pixel sizes), and requires significant post-processing. Such complexities are not warranted for OzFuel-1.

The suite of multispectral filters necessary for OzFuel is still under active development (see part 1 of this document). However, their specification is unlikely to be optically demanding, with a range of trusted international vendors available for fabrication as well as at the Australian National Fabrication Facility. Development of a graded-index filter for an OzFuel-2 mission, providing a transition to a hyperspectral capability, is more challenging, but this is largely a metrology and calibration problem rather than a fundamental roadblock.

6.7. Calibration

Any observational system is only as trustworthy as its underlying calibration. High-performance on-board calibration systems represent a significant parallel instrument development in their own right. Full in-flight calibration, via direct injection of carefully regulated calibration light sources, is a complex process. An accurate and repeatable system would likely be of comparable complexity, volume and mass to the sensor system to be calibrated. Furthermore, the necessity to insert/remove diffusing screens and ensure reliable operation of calibration lamps (dissipating heat, ensuring performance stability etc.) introduces significant risk and complexity into any remote sensing system.

At the opposite extreme, simply relying on pre-flight laboratory calibration (with or without in-flight validation via vicarious observations of well-understood test sites) places demanding stability tolerances on instrumentation. Even with calibration and testing facilities such as the ANU Space Detector Test Facility (recently enabled with supporting funding from the ACT Government Priority Investment Program) significant calibration drift might be expected between the laboratory testing and flight operations.

An intermediate solution is proposed for early OzFuel development. An extensive pre-flight test program will establish baseline performance. The OzFuel sensor will then be equipped with a deployable defusing element that covers the sensor entrance aperture. The screen can be engineered so that a thin form-factor device can be inserted and removed in front of the sensor, with relatively loose mechanical tolerances simplifying the necessary actuator without introducing calibration error. With the screen deployed, the sensor can be tasked to periodically (daily, weekly etc.) observe the Sun (or Moon) for a stable calibration reference source allowing confirmation and updating of the instrument calibration function as required. Such a calibration solution provides a reduced risk pathway to full in-flight calibration of a pathfinder mission such as OzFuel.

7. ROM COSTS

Element	Cost without any margin	Margin (locally applied)	ROM cost
OzFuel-1 Mission	AUD 6.3 M	44%	AUD 9.1 M
Ground Segment	AUD 0.4 M	50%	AUD 0.6 M
Launcher	AUD 1 M	10%	AUD 1.1 M
Mission Operations Centre	AUD 0.5 M	50%	AUD 0.8 M
Processing pipeline	AUD 0.3 M	100%	AUD 0.6 M
OzFuel Satellite	AUD 4.1 M	47%	AUD 6.0 M
- Environmental Qualification	AUD 0.2 M	50%	AUD 0.3 M
- Integration + System-level Tests	AUD 0.4 M	20%	AUD 0.5 M
- Payload	AUD 2.5 M	30%	AUD 3.3 M
- Platform / Bus	AUD 1 M	100%	AUD 2 M

8. Recommendations

The requirements identified for remote sensing of fuel conditions (Table 3) should be verified and validated via a dedicated field campaign during the Q4 2021/Q1 2022 fire season. The resulting spectral library will verify the spectral bands that are more sensitive to variations in fuel conditions and hence flammability. It will narrow down the preliminary spectral specification for OzFuel.

A follow-on Phase A study should be undertaken for mission analysis to detail the concept of operations, payload (sensor, onboard processing, onboard calibration), spacecraft requirements and the ground user segment. A concurrent engineering study would de-risk programmatic and technological challenges for the OzFuel-1 pathfinder.

Preliminary market research should be undertaken to identify the use and distribution of OzFuel spatial data beyond the Australian Flammability Monitoring System. ANU seeks to extend this engagement to the commercial sector to understand, for example:

- which data services would use or distribute the data for bushfire mitigation;
- how the data would be used;
- how the data would be delivered;
- what parallel applications in Earth observation the data would benefit.



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Acronyms and abbreviations

Abbreviation	Meaning
ASA	Australian Space Agency
ATM	Skykraft Air Traffic Management platform
BRDF	Bi-directional Reflectance Distribution Function
CAD	Computer-Aided Design
Cal/Val	Calibration/Validation
CHICO	Compact Hyperspectral Imager for Coastal Oceans mission
COTS	Commercial off-the-shelf
CSIRO	Commonwealth Scientific and Industrial Research Organisation
DMC	Dry Matter Content
DMTC	Defence Materials Technology Centre
DN	Digital Numbers
eAPD	Electron avalanche photodiode
ESA	European Space Agency
FMC	Fuel Moisture Content
FOV	Field of View
FPGA	Field Programmable Gate Array
FWHM	Full Width at Half Maximum
GA	Geoscience Australia
GSD	Ground Sampling Distance
HASS	High Altitude Sensor System
Hz	Hertz
InGaAs	Indium gallium arsenide
km	Kilometre
K	Kelvin
LEO	Low Earth Orbit
LFMC	Live Fuel Moisture Content
m	Metre
µm	Micron
msec	Milliseconds
MCT	Mercury cadmium telluride
MSL	Melbourne Space Laboratory
OzFuel	Australian Fuel Monitoring from Space
nm	Nanometre
NIR	Near Infrared
NRE	Non-recurring engineering

ROIC	Readout Integrated Circuit
ROM	Rough Order of Magnitude
SME	Small-Medium Enterprise
SNR	Signal-to-Noise Ratio
SSO	Sun-Synchronous Orbit
SWIR	Short Wavelength Infrared
TDI	Time Delay Integration
TheMIS	Thermal Management Integrated System
TMA	Three Mirror Anastigmat
TOA	Top of Atmosphere
TRL	Technology Readiness Level
UTC	Universal Time Code
UTM	Universal Transverse Mercator
VNIR	Visible and Near Infrared



Appendix A: Relevant documentation

Document ID	Title	Revision #
OZFUEL-SCI-SDD-0001	Mission Drivers Document	1
OZFUEL-SCI-SDD-0002	OzFuel Technical Overview	1
OZFUEL-SENG-FPRD-0001	External Reference Requirements	1
OZFUEL-SENG-FPRD-0002	Mission Requirements	1
OZFUEL-SENG-FPRD-0003	Instrument Requirements	1
OZFUEL-SCI-OCD-0001	Operational Concepts Document	1
OZFUEL-SENG-ICD-0001	Skykraft ATM SmallSat Platform Interface	1
OZFUEL-SENG-RANA-0001	Data Rates Analysis	1
OZFUEL-SENG-RANA-0002	Radiometric sensitivity analysis	1
OZFUEL-OZFUEL-TRD-0001	Cooling System Trade Study	1
OZFUEL-OZFUEL-TRD-0002	Skykraft Satellite Bus Trade Study	1
OZFUEL-MGT-PLAN-0001	Bill of Materials	1
OZFUEL-MGT-RISK-0001	Risk Register	1