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ABSTRACT

We report on the design, optimization and fabrication of a plasmon-assisted terahertz (THz) photoconductive antenna (PCA) for THz pulse generation at low-power optical pumps. The PCA features a high aspect ratio dielectric-embedded plasmonic Au grating placed into the photoconductive gap. Additionally, Si₃N₄-passivation of the photoconductor and the Al₂O₃-antireflection coating are used to further enhance antenna performance. For comparative analysis of the THz photocurrents, THz waveforms and THz power spectra we introduced the THz photocurrent δ_i and the THz power enhancement δ_{THz} factors, which are defined as ratios between the THz photocurrents and the THz power spectra for the plasmon-assisted and conventional PCAs. We demonstrated superior performance of the plasmon-assisted PCA $\delta_i=30$ and $\delta_{\text{THz}}=3 \cdot 10^3$ at the lowest optical pump power of $P=0.1$ mW. Nevertheless the increase to $P=10$ mW lead to monotonically decrease in the both values to $\delta_i=2$ and $\delta_{\text{THz}}=10^2$ due to screening effects. These results demonstrate a strong potential of the plasmonic PCA for operation with low-power lasers, thus, opening opportunities for the development of portable and cost-effective THz spectrometers and imaging systems.

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Existing THz sources do not meet many challenges posed by the rapidly-developing THz science and technology¹ and improving the efficiency of the THz emitters remains a

difficult problem. The photoconductive antennas (PCAs) based either on photoswitching^{2,3} or photomixing^{4,5} effects, are the prevalent THz emitters widely used in the THz spectroscopy

and imaging due to their reliability, cost effectiveness and a relative ease of fabrication. Since the first experimental observation of photo switching in semiconductors,⁶ rapid progress in the THz PCA technology has been achieved by using different materials and semiconductor technologies.⁷⁻⁹ Nevertheless, enhancement of the optical-to-THz-wave conversion efficiency and development of the THz PCAs operating with low-power optical pumps remain a challenge.

Recently, an approach for boosting the THz PCAs performance using plasmonic or dielectric nanoantennas incorporated into a photoconductive gap has been proposed.^{10,11} In such PCAs, strong confinement of the optical pump excitation at the semiconductor/nanoantenna interface leads to enhancement of the light-matter interaction, and to improvement of the antenna thermal efficiency.¹²⁻¹⁴ The PCA-emitters and PCA-detectors using different geometries of metal and dielectric nanoantennas, such as silver nano-islands or arrays of nanoscale apertures,¹⁵⁻¹⁷ fractal antennas,¹⁸ monopole or dipole plasmonic gratings with either low or high aspect ratios,^{10,11,19-24} plasmonic nanocavities based on Bragg reflectors,²⁵ metal colloidal particles deposited onto the photoconductive substrate,²⁶ or even all-dielectric gratings,²⁷ demonstrated impressive performance enhancement compared to the conventional PCAs.

In this paper, we report on a plasmon-assisted THz PCA that enhances the THz pulse generation and operates with low-power optical pumps. The THz wave generation enhancement is due to a favorable combination of a high aspect ratio dielectric-embedded plasmonic Au grating (resulting in a stronger optical field - photoconductor interaction), a Si₃N₄-passivation layer (that significantly reduces leakage currents and sustains thermal stability of the PCA), as well as an Al₂O₃-antireflection and protection coating (that reduces the Fresnel losses of the photoconductive gap and promotes the mechanical stability of the grating). For comparison, a conventional PCA was also fabricated. We demonstrated superior performance of the plasmon-assisted PCA which THz photocurrent and THz power spectrum were 30 and 3 · 10³ higher than those of a conventional PCA at the lowest optical pump power of P=0.1 mW, thus confirming that our plasmonic PCA is well suited for operation with low-power lasers. We believe that the plasmonic PCA reported in this work could become a key enabling component in the upcoming portable and cost-effective THz spectrometers and imaging systems.

Figures 1 (a) and (b) show the respective schematics of the studied plasmon-assisted PCA and the high-aspect-ratio dielectric-embedded Au-grating in the PCA's gap. The PCA features log-spiral Au-electrodes on a semi-insulating GaAs (SI-GaAs) photoconductive substrate. In order to significantly reduce the dark current, the photoconductor was passivated using a Si₃N₄-film with the windows for Ti/Au metallization etched prior to the plasmonic grating deposition. The plasmonic antenna is made of two physically spaced plasmonic gratings. In turn, each grating features an array of Au-nanoridges with rectangular cross-sections placed

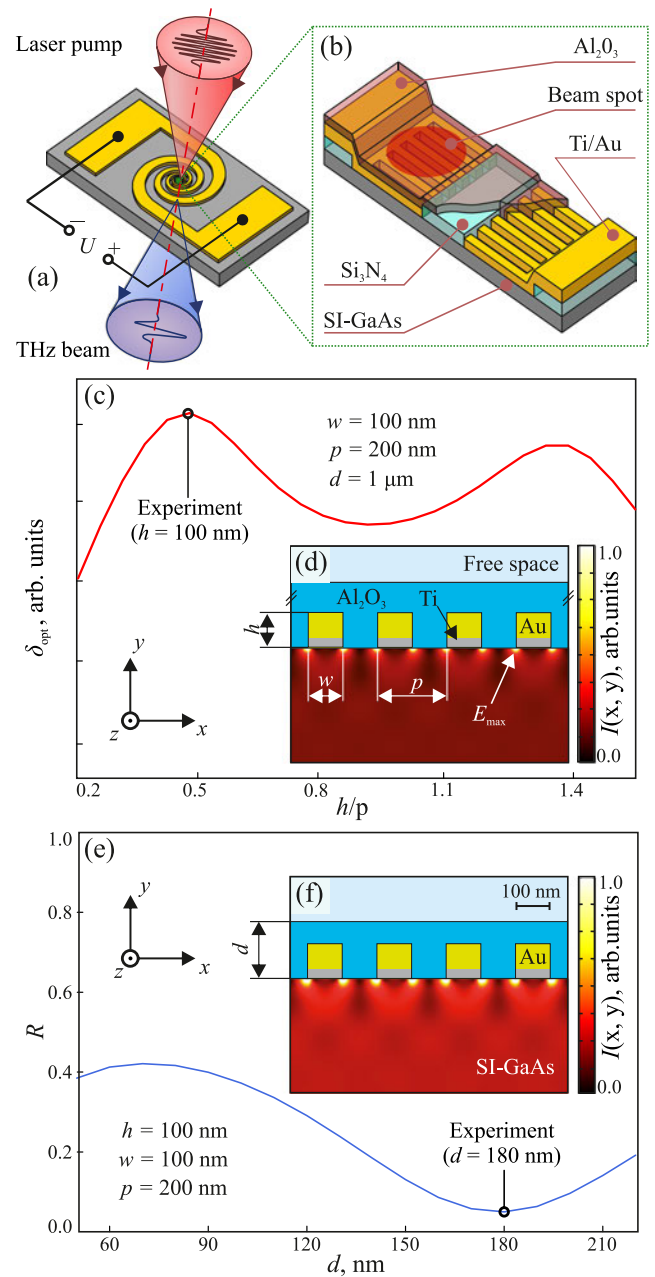


FIG. 1. Schematics of (a) the antenna design; (b) the gap region of a plasmonic PCA; (c) simulated local optical intensity enhancement factor δ_{opt} as a function of the Ti/Au-grating height-to-period with semi-infinite Al₂O₃-coating ($d=1 \mu\text{m}$ in simulation); (d) optical field intensity $I(x, y)$ in the photoconductor layer with semi-infinite Al₂O₃-coating and Ti/Au-grating height of $h=100 \text{ nm}$, width of $w=100 \text{ nm}$ and period of the grating $p=200 \text{ nm}$; (e) simulated PCA reflectivity R at $\lambda=0.78 \mu\text{m}$ as a function of the Al₂O₃-coating thickness d ; (f) optical field intensity $I(x, y)$ in the photoconductor layer for $h=100 \text{ nm}$, $w=100 \text{ nm}$, $p=200 \text{ nm}$ and $d=180 \text{ nm}$.

periodically onto the photoconductive substrate and brought in contact with the corresponding PCA electrodes. Finally, the antenna is covered with an Al₂O₃-coating, which infiltrates the

gaps between the Au-nanoridges. The PCA is pumped using a femtosecond laser beam focused onto the anode plasmonic grating (see Fig. 1 (b)).

The proposed plasmonic PCA enhances THz pulse generation due to strong field confinement at the interface between the plasmonic grating and the semiconductor material.¹⁴ In order to optimize PCA geometry, we performed numerical simulations using finite-element method of solving the Maxwell's equations by COMSOL Multiphysics.^{28,29} The values of the material optical parameters were taken from the existing literature - SI-GaAs,³⁰ Au,³¹ and Al₂O₃.³²

In our simulations, we used a monochromatic plane wave of $\lambda = 0.78\mu\text{m}$ incident normally at the PCA. To achieve an efficient excitation of the plasmonic modes of the metal grating, the incident plane wave polarization was chosen to be perpendicular to the Au-nanoridges.¹⁰ Furthermore, we used the semi-infinite SI-GaAs substrate, the individual nanoridge width of $w = 100\text{ nm}$, and the grating period of $p = 200\text{ nm}$, while the plasmonic grating height h and the Al₂O₃-coating thickness d were varied to achieve an optimal design. Figures 1 (d), (f) present the numerically simulated spatial distributions of the electromagnetic (EM) field intensity $I(x, y)$ in the photoconductor. These plots show that the antireflection coating leads to a significant enhancement of the field intensity in the plasmonic grating modes (the same scale is used for the two-color bars in Figs. 1 (d) and (f)).

Figure 1 (c) shows the local optical field intensity enhancement factor $\delta_{\text{opt}} = |E_{\text{max}}|^2/|E_0|^2$ as a function of the Au-nanoridge height h with the semi-infinite Al₂O₃-coating ($1\mu\text{m}$ in the simulation). Here E_{max} is the maximal local amplitude of the electric field at the shadow side of the plasmonic Ti/Au grating (we used the thickness of Ti equal to 18 nm) and E_0 is the amplitude of the homogeneous electric field formed in the photoconductive substrate without the Au-nanoridges. The higher is the value of δ_{opt} , the higher will be the absorbed local optical pump intensity, thus contributing to the generation of the electron-hole pairs and, therefore, to the THz photocurrent and to the THz pulse generation.¹⁴

Figure 1 (c) shows that, at first, δ_{opt} increases reaching its maximum at $h/p \sim 0.5$ nm. With a further increase of h/p , δ_{opt} varies periodically, which can be explained by the standing wave resonances in the finite-size parallel plate metallic waveguide formed by the Au-nanoridges.

Next, we optimized the thickness of an Al₂O₃-coating that entirely fills the gaps between the Au-nanoridges and serves as the antireflection coating. This coating ensures effective optical pump coupling into the photoconductor.³³ Figures 1 (e) and (f) show the results of this optimization and the EM field intensity distribution $I(x, y)$ for the optimal thickness of the Al₂O₃-antireflection coating of $d = 180\text{ nm}$, which reduces the Fresnel reflection down to $\sim 5\%$ thus allowing $\sim 95\%$ of the incident radiation to penetrate into the photoconductive substrate. With thus selected optimal parameters of the plasmonic grating ($h = 100\text{ nm}$, $w = 100\text{ nm}$, $p = 200\text{ nm}$, and $d = 180\text{ nm}$), we have

confirmed numerically a significant field enhancement behind the plasmonic grating.

Next, we fabricated the optimized plasmonic and conventional THz PCAs. The conventional PCA utilized the same photoconductive substrate, log-spiral Au-electrodes with the gap of $10\mu\text{m}$ and the Al₂O₃-coating but did not feature the plasmonic gratings. The fabrication technique was similar to that reported in Ref. 34. First, we passivated the surface of a SI-GaAs photoconductor with a 230 nm Si₃N₄ dielectric layer, then we etched two windows near the photoconductive gap for the antenna/semiconductor contact, and then deposited 50/450-nm-thick Ti/Au PCA electrodes using electron-beam evaporation. The plasmonic gratings were formed by the electron-beam lithography with 18/82-nm-thick Ti/Au metallization followed by the lift-off process. Finally, the $10 \times 10\mu\text{m}^2$ plasmonic grating was inscribed onto each of the two electrodes. Figure 2 shows the scanning electron microscopy (SEM) image illustrating the PCA structure, as well as the current-voltage characteristics demonstrating the reduction of the dark current i_d in the passivated PCA. As shown in Figs. 3 (a) and (b), the two arrays of Au-nanoridges are attached to the corresponding antenna electrodes and are separated by the $10\text{-}\mu\text{m}$ -wide gap. Finally, the resultant photoconductive antenna was coated with a 180-nm-thick Al₂O₃-coating using the atomic-layer deposition. Figure 3 (c) shows the SEM image of the PCA cross-section illustrating that the Al₂O₃-coating penetrated the voids between the Au-nanoridges, thus helping to maintain the mechanical stability of the grating,³³ and enhancing the optical pump coupling into the PCA.^{23,33} As seen from Fig. 3, the geometry of the fabricated plasmonic gratings corresponds to the one used in numerical modeling (see Fig. 1). It is also important to notice that the proposed passivation approach excludes mesa etching.³⁵ Therefore, it is suitable for any photoconductive material.

To experimentally characterize the fabricated PCAs, we used them as emitters in the THz-time-domain spectroscopy system (THz-TDS) measuring THz waveforms and THz power spectra P_{THz} . The THz-TDS is similar to the one used in our previous studies.^{36,37} It uses the compact femtosecond fiber laser Toptica FemtoFERb780 featuring the central

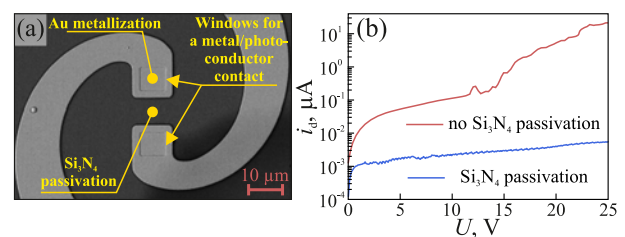


FIG. 2. Introduction of the passivation layer into PCA structure, and its impact on the dark current: (a) SEM image illustrating the photoconductive gap being passivated with a Si₃N₄-dielectric layer that features two windows to provide antenna/semiconductor contact; (b) dark current i_d versus bias voltage U for both passivated and non-passivated PCAs.

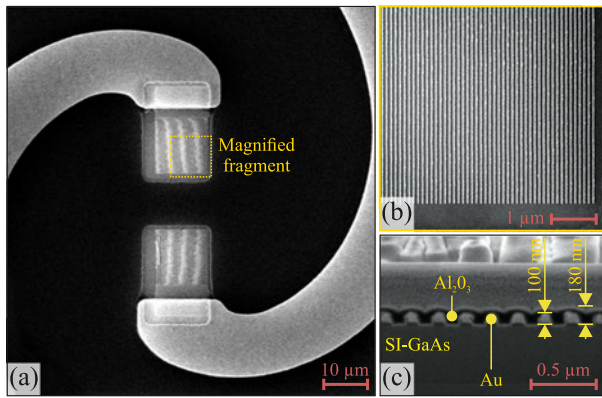


FIG. 3. Fabrication of the plasmon-assisted PCA: (a) SEM image of the passivated photoconductive gap, antenna metallization with the log-spiral Au-electrodes and two plasmonic gratings; (b) magnified image of the plasmonic grating; (c) SEM image of the plasmonic grating cross-section that shows the Al_2O_3 filling/coating, nanoridges, and their geometrical parameters.

wavelength of $\lambda = 0.78\mu\text{m}$, the pulse repetition rate of $f = 100$ MHz, and the pulse duration of $\tau = 95$ fs. In our experiments, we biased the PCA emitters with $U = 30$ Volts and varied the optical pump power in the range of $P_{\text{opt}} \approx 0.1$ to 10 mW using a set of attenuators. The emitted THz beam was collimated using a pair of the HRFZ-Si hemispheres and an off-axis gold parabolic mirror. The beam was then focused onto the PCA-detector (commercial THz receiver with a wrapped-dipole antenna topology, i.e. dipole with twisted bias lines) with the same optical components as used for the beam collimation. The PCA-emitter and the PCA-detector were placed in contact with the flat surfaces of the HRFZ-Si hemispheres. During comparative measurements, we only substituted and adjusted the PCA-emitters, while keeping the rest of the THz beam path unaltered. The time-independent THz photocurrent, i.e. the average photocurrent over THz pulse, was measured under fs laser illumination at bias voltage of 30 Volts for the plasmon-assisted (i_{pl}) and conventional PCAs (i_{c}), respectively.

Figure 4 (a) shows the normalized THz power spectra $P_{\text{THz}}/P_{\text{opt}}$ for both the plasmonic and conventional PCAs-emitters at high and low powers of the optical pump $P_{\text{opt}} = 10$ mW and 1.0 mW, respectively. Figures 4 (c) and (d) show the THz photocurrent enhancement factor δ_i and the THz power enhancement factor δ_{THz} as a function of the optical pump power P_{opt} , where δ_i is defined as a ratio of the THz photocurrents of the plasmonic and conventional PCAs, while δ_{THz} is a ratio of integrals over the THz power spectrum for the two PCAs in the frequency domain calculated as follows:

$$\delta_i = \frac{i_{\text{pl}}}{i_{\text{c}}}, \quad (1)$$

$$\delta_{\text{THz}} = \frac{\int P_{\text{THz}}^{\text{pl}}(\nu) d\nu}{\int P_{\text{THz}}^{\text{c}}(\nu) d\nu}.$$

where $P_{\text{THz}}^{\text{pl,c}}$ are the THz power spectra for the plasmon-assisted and conventional PCAs. We observe a strong

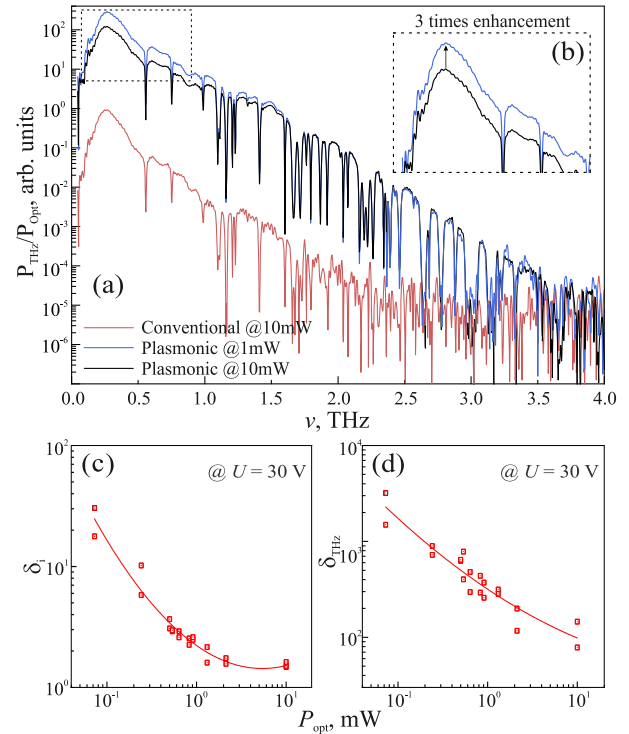


FIG. 4. Experimental comparison of the plasmon-assisted and conventional PCAs: (a) the normalized THz power spectra $P_{\text{THz}}/P_{\text{opt}}$ for various pump powers $P_{\text{opt}} = 1$ and 10 mW; (b) $P_{\text{THz}}/P_{\text{opt}}$ for the plasmonic PCA at various optical pump powers; (c), (d) the THz photocurrent enhancement factor δ_i and the THz power enhancement factor δ_{THz} as a function of the optical pump power P_{opt} .

enhancement in both the THz photocurrent and the THz power for the plasmon-assisted PCA compared to the conventional PCA. The highest THz power enhancement factor of $\delta_{\text{THz}} = 3 \times 10^3$ is observed at low powers of the optical pump $P_{\text{opt}} < 1.0$ mW. Figure 4 also shows the reduction in the THz generation enhancement when increasing the pump power P_{opt} . Namely, when increasing the optical pump power from 0.1 to 10 mW, the THz photocurrent enhancement decreases from $\delta_i = 30$ to 2 and the THz power enhancement decreases from $\delta_{\text{THz}} = 3 \times 10^3$ to 10^2 .

There could be a number of reasons for the observed reduction. First, with an increase in the pump power, we could expect broadening of the pump beam caustics formed behind the plasmonic nanoridges, thus, leading to an increase in the volume of the photoconductor occupied by the electron-hole plasma. Such an expansion of the electron-hole plasma volume could lead to a reduction in the efficiency of THz wave generation due to more pronounced charge screening effects.^{38,39} Moreover, the enhancement of the electron-hole pairs generation deep in the semiconductor volume reduces the efficiency of the optical-to-THz-wave conversion, since only the photocarriers in a close proximity to the plasmonic grating contribute to the THz pulse generation.⁴¹ A wide

bandgap semiconductor layer placed under the photo absorbing layer could reduce the electron-hole generation deeper into the semiconductor. The geometry and composition of such layer could be optimized by performing Monte Carlo simulations.⁴⁰ Additionally the increase of the PCA performance and its thermal stability can be reached by using short-carrier-lifetime semiconductors.⁴¹

In conclusion, we used the numerical simulations to optimize the plasmon-assisted PCA design, then fabricated and characterized the optimized plasmon-assisted PCA and confirmed a significant enhancement of the THz pulsed generation and its superior operation at low pump powers. The plasmon-assisted PCA uses the effect of the optical field confinement in the vicinity of the high-aspect-ratio dielectric-embedded Au-grating. Based on the achieved dynamic range of 70 dB, large spectral bandwidth of 4 THz, and low optical pump powers < 1 mW, we can claim that our plasmonic PCA competes well with the most advanced PCAs known to date based on optical nanoantennas, optical nanocavities, and other enhancement techniques.^{14,42} It is also important to note that other known plasmonic PCAs utilizing the same photoconductive substrate SI-GaAs with different metal adhesion layers⁴³ or polarization insensitive designs¹⁷ do not reach as high dynamic range or bandwidth as our antenna. A large 3×10^3 -times enhancement of the THz beam power generation at low optical pump powers reveals strong potential of the plasmonic PCA for operation with low-power lasers. The developed numerical simulation approach and plasmonic fabrication technology could be also applied for the development of the electrically driven THz plasmonic detectors and sources.⁴⁴

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