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2 **Modeling the impact of defects on the charge collection** 3 **efficiency of a Cadmium Telluride detector**

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18 **ABSTRACT:** Cadmium telluride is a favorable material for X-ray detection as it has an outstanding
19 characteristic for room temperature operation. It is a high-Z material with excellent photon radiation
20 absorption properties. However, CdTe single crystals may include a large number of extended
21 crystallographic defects, such as grain boundaries, twins, and tellurium (Te) inclusions, which can
22 have an impact on detector performance. A Technology Computer Aided Design (TCAD) local
23 defect model has been developed to investigate the effects of local defects on charge collection
24 efficiency (CCE). We studied a 1 mm thick Schottky-type CdTe radiation detector with transient-
25 current technique by using a red laser at room temperature. By raster scanning the detector surface
26 we were able to study signal shaping within the bulk, and to locate surface defects by observing
27 their impact on the CCE. In this paper we present our TCAD model with localized defect, and
28 compare the simulation results to TCT measurements. In the model an inclusion with a diameter
29 of 10 μm was assumed. The center of the defect was positioned at 6 μm distance from the surface.
30 We show that the defect has a notable effect on current transients, which in turn affect the CCE of
31 the CdTe detector. The simulated charge collection at the position of the defect decreases by 80 %
32 in comparison to the defect-free case. The simulations show that the defects give a characteristic
33 shape to TCT signal. This can further be used to detect defects in CdTe detectors and to estimate
34 the overall defect density in the material.

35 **KEYWORDS:** X-ray detectors, Detection of defects, Simulation methods and programs

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45 **1 Introduction**

46 Cadmium Telluride (CdTe) is a suitable material for room temperature detection of X-ray and
47 gamma-ray radiation. It has a relatively large band gap, 1.47 eV at 300 K, resulting in a small
48 thermal noise. Another outstanding characteristic of this semiconductor material is its high atomic
49 number that enables strong absorption and good detection efficiency for high-energy photons [1, 2].

50 At the same time, CdTe detectors suffer from the crystal impurities such as Te-inclusions,
51 dislocation networks, and twin and subgrain boundaries [3], which affect the detector performance
52 [4, 5]. Defects and impurities at the grain boundaries can trap charge carriers and also act as charge
53 drains, which can be seen as fluctuations in the collected signal and charge collection efficiency
54 (CCE) [6].

55 Laser Transient Current Technique (TCT) is a widely used and adopted method for the char-
56 acterisation of semiconductor radiation detectors. TCT reveals many material characteristics of a
57 detector, including defects and their influence on electric properties of the device [7, 8].

58 During a TCT measurement, a laser pulse generates charge carriers which pass through the
59 detector in the applied electric field. With red laser TCT, electron-hole pairs ($e-h$ pairs) are
60 generated close to the surface of the illuminated side of the device. One type of the charge carriers
61 is immediately collected by the nearest electrode. Thus, the induced current is an outcome of a
62 single carrier type drift, depending on the bias voltage. The collected signal is rich on information
63 about the detector: various parameters, such as rise time, charge collection efficiency (CCE), and
64 peaking amplitude can be extracted from the signal. By mounting the setup on a XYZ-stage and by
65 combining the signal output with the position information from the stage, the locations of the defects
66 and other non-uniformities can be mapped, and their effect on the charge collection efficiency (CCE)
67 can be studied [9].

68 In this paper, we studied the effects of defects in CdTe pad detectors by using red laser TCT.
69 In order to identify the impact of defects on the transient currents, simulations of a CdTe diode

70 structure with the defect inclusion has been performed. By combining measured results and TCAD
 71 simulations a detailed study of detector performance was obtained.

72 2 Materials and Methods

73 2.1 TCAD simulations

74 To better understand the impact of the defects on the detector performance, simulations were made
 75 using a Technology Computer Aided Design (TCAD) package from Synopsys [10]. The TCAD
 76 package provides the ability to simulate 2D or 3D CdTe structures with various electrode geometries
 77 and uses a drift diffusion model to simulate the detector response. At each point of the model, the
 78 Poisson and the charge carrier continuity equations are solved and the electrostatic potential and the
 79 carrier concentrations are calculated.

80 The simulated diode structure had dimensions of $A \times 3000 \times 1000 \mu\text{m}^3$ with a 50 nm thick
 81 AlN passivation layer, where A is an area factor to match the dimensions of the real diode. The
 82 thicknesses of the gold contacts on the front and backplanes were 500 nm. A work function of
 83 5 eV for Schottky-type contacts was assumed. In the simulation, CdTe bulk with a uniform charge
 84 carrier concentration of $1 \times 10^7 \text{ cm}^{-3}$ was used [11]. A bias voltage of -450 V from the backplane
 85 was utilised in the simulations and the front plane was set to ground. To consider the high defect
 86 concentrations in the CdTe bulk, two mid-gap levels (a deep acceptor and a donor level) were
 87 implemented with energies of 0.72 eV and with a concentration of $1 \times 10^{12} \text{ cm}^{-3}$ [12]. The electron
 88 and hole capture cross sections were found by fitting simulated transients to the measurement results.

89 As revealed by IR microscopy mid-sized Te inclusions are in 5 - 15 μm range [13, 14]. In
 90 the simulations, large-scale defects (grain boundaries, Te inclusions) in the detector bulk were
 91 reproduced by introducing a CdTe semiconductor material inclusion with high amount of traps into
 92 the detector body, as depicted in Fig. 1b. This approach was used since the conventional method of
 93 introducing energy levels into the CdTe bulk bandgap does not provide any physical localization of
 94 the defects. Due to this, a circular shaped inclusion with a diameter of 10 μm was considered as a
 95 local defect imitation. For the trap levels in the inclusion material, the same two mid-gap levels (a
 96 deep acceptor and a donor level) were implemented with energies of 0.72 eV.

97 The laser excitation was applied to the front opening. For the generation-recombination mech-
 98 anism of charge carriers in the CdTe, the doping-dependent Shockley-Read-Hall model (Scharfetter
 99 relation [10]) and impact ionization (van Overstraeten model [16]) were used in the simulation.
 100 The penetration depth of a red laser is about a few μm , so the red laser TCT signal displays holes
 101 drifting through the device, while electrons are immediately collected away by the front contact.
 102 The red laser current pulses can be described by the Ramo–Shockley theorem [17]:

$$I_{e,h}(t) = N_{e,h} \exp\left(\frac{-t}{\tau_{e,h}}\right) \vec{E}(\vec{r}) \vec{E}_w(\vec{r}), \quad (2.1)$$

103 where $N_{e,h}$ is effective doping concentration, \vec{r} the location of the charge, $\tau_{e,h}$ is effective
 104 carrier trapping time, $\vec{E}(\vec{r})$, the weighting field given by the electrode configuration in the detector
 105 [9]. To consider electric field variation near the surface, the laser beam was pointed at 3 different
 106 positions at the surface: the middle of the optical opening (0), the left and right edge of the opening
 107 (550 and -550).

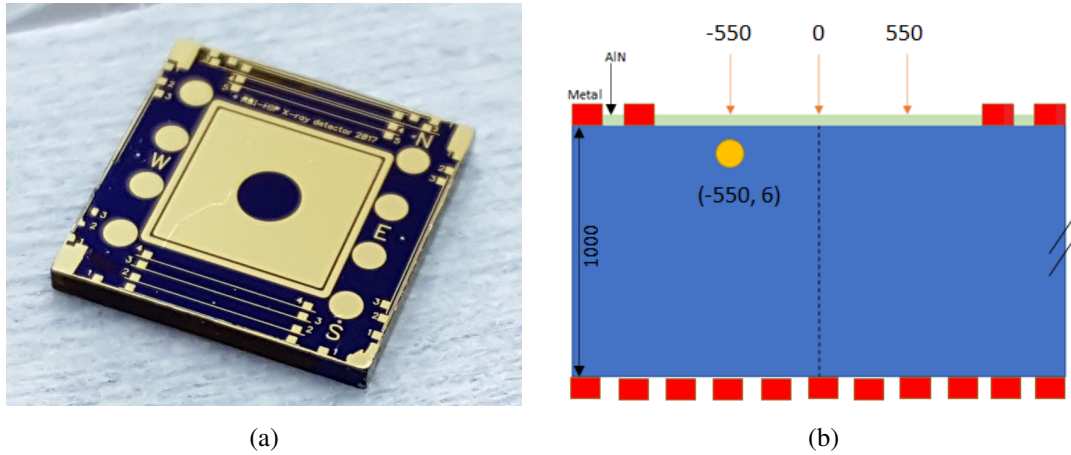


Figure 1: a) A pad detector with an optical opening in the middle [15] and b) a schematic of the simulated structure with the optical opening and a defect inclusion. All the dimensions are in μm . Optical opening is from $-1000 \mu\text{m}$ to $1000 \mu\text{m}$ and the defect inclusion center position is $(-550, 6)$. The laser beam was pointed at 3 different positions at the surface: the middle of the opening (0), the left and right edge of the opening (-550 and 550).

108 2.2 TCT measurements

109 The CdTe pad detectors discussed in this paper represent a simple structure of a CdTe single crystal
 110 with metal electrodes on both sides. Prior to metallization, CdTe was passivated with aluminium
 111 nitride (AlN) [15, 18]. The contacts for both sides of CdTe detector were formed by sputtering
 112 depositions resulting in Schottky barrier contacts. They consist of a 20 nm thick titanium tungsten
 113 (TiW) adhesion layer, and around 200 nm thick layer of gold. For TCT measurements, there is an
 114 optical opening on the front side with a diameter of 2 mm without any metallization (Fig. 1a).

115 The TCT-setup consists of a pulsed laser source, optics with an adjustable diaphragm collimator,
 116 and a XYZ-stage. The detectors were mounted to the XY-plane of the system by pressing the front
 117 anode with a wire. The wire was also used as a contact for the detector bias. The backside of the
 118 detectors was grounded through the metal frame of the sample holder.

119 The bias voltage of $+450 \text{ V}$ was provided with a Keithley 2410 SourceMeter through a bias-T
 120 to the front contact. The voltage supply was also used to monitor, and to limit, the leakage current
 121 of the system. The output signal was passed through the bias-T to a Particulars AM-01 A 53 dB RF-
 122 amplifier. The resulting signal pulses were read out with a Teledyne Lecroy WaveRunner 840M-MS,
 123 4 GHz, oscilloscope. The oscilloscope was operated in a sampling mode with a sampling frequency
 124 of 20 GS/s and a running average of 50 measurements, which was selected experimentally as a
 125 balance between noise suppression and response to changes in rise time. All measurements were
 126 made at room temperature.

127 A pulsed red-laser (wave length 660 nm, power 10 mW) with a Gaussian beam profile and
 128 pulse duration of 440 ps was used for $e-h$ pair creation. The repetition rate was set to 50 Hz and
 129 pulse power was cut to 60% of the maximum power, yielding pulse energy of about 4.4 pJ. The
 130 focal distance of the laser was set with a knife-edge technique [19].

131 In order to locate areas with non-uniformities, the optical opening of the detectors was raster

132 scanned. From the TCT signals, values of amplitude, charge collection efficiency, peaking time, and
 133 rise time, were extracted and mapped in 2D maps using the coordinate information from the stages.
 134 From the maps, areas with defects were identified [20]. The CCE is defined as an integral over the
 135 transient current signal with a time window of 900 ns. The resulting values are then normalized to
 136 the highest value in the measured area.

137 3 Results and discussion

138 3.1 Simulation results

139 In order to investigate the impact of the defect inclusion on the electrical field and the transient
 140 currents, a simulation of a reference diode detector with no bulk defects, no surface passivation
 141 layer on top of the optical opening and no incorporated defect inclusion was performed. This model
 142 is compared to the same structure with one defect inclusion inside.

143 In Fig. 2, the transverse distribution of the electrical field at the position of the defect is depicted
 144 for the abovementioned structure. The local defect introduction of a circular shape at the position
 145 of (-550, 6) gives us a fluctuation of the electric field due to charge accumulation as consequence of
 146 carrier trapping by the trap levels in the inclusion. In Fig. 2a one can see that the electric field starts
 147 increasing from the value of 1.7 kV/cm near the surface, while for the case without any defect,
 148 inclusion the value for the electric field near the surface is 2.1 kV/cm. Figure 2b shows that there is
 149 a disturbance of the electrical field at the position of the defect inclusion in the lateral distribution
 150 as well. This initial simulation indicates that the presence of a localised defect inclusion near the
 surface can cause fluctuations of the electric field, resulting in a change of the outcome signal.

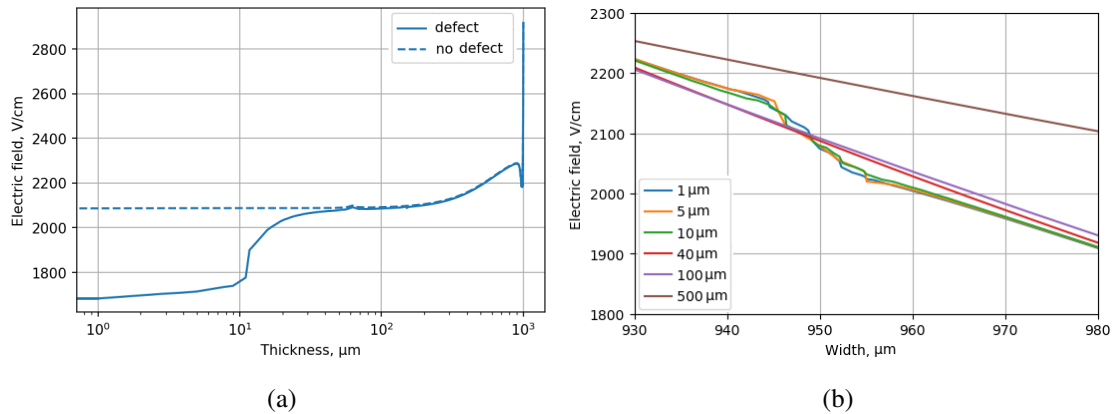


Figure 2: a) Comparison of the simulated transverse distribution of the electrical field at the position of the defect for the simulated diode with and without defect incorporation. No bulk traps and no surface passivation were considered. b) Simulated lateral electric field cuts with defect incorporated for different distances from the surface in μm in the proximity of the defect position.

151 The transient currents of the CdTe diode with and without defect are shown in Fig. 3. In the
 152 case of no inclusion, after generating $e - h$ pairs, fast electrons are collected on the front electrode
 153 in a short time that is demonstrated as a narrow peak, whereas slow holes travel long time through
 154 the sample to the back. When we are looking at the transient with the local defect, after the narrow
 155

156 peak produced by collected electrons the current rapidly decreases. In Fig. 3b the zoomed plot of
 157 the transient current is depicted. As the creation point of $e - h$ pairs is very close to the defect area
 158 with a very high concentration of traps, part of the free carriers were captured by the trap levels in
 159 the inclusion. As it is shown in Fig. 3, the current for the case with the defect is by 2 orders of
 160 magnitude less than the signal without any inclusion.

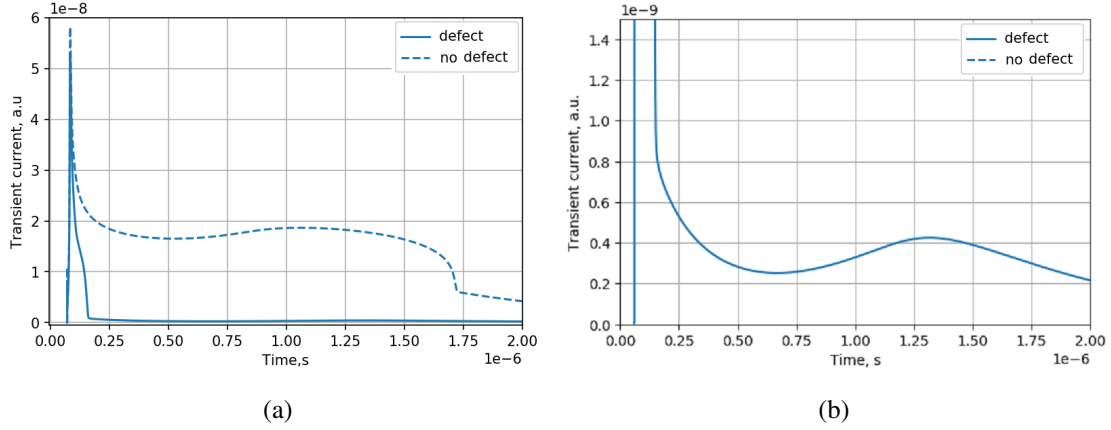


Figure 3: a) Comparison of the simulated transient current at the position of the defect for simulated diode with and without defect incorporation. No bulk traps and no surface passivation were considered. b) Zoom-in to the transient with defect inclusion.

161 In addition to bulk defects, surface recombination has a high impact on the device performance
 162 [21]. This can be reduced by passivating the surfaces of the crystal. To see how it affects the field
 163 strength, the AlN layer is added on top of the optical opening of the simulated structure. In Fig. 4a,
 164 the transverse distribution of the electrical field is compared for two cases: passivation on top of
 165 the opening and no passivation. Since the bias is applied through the metallization, the strength
 166 of the electric field for the structure with no dielectric is the lowest in the middle of the optical
 167 opening (Fig. 4a green solid curve represents "no AlN" case). However, one can notice that with
 168 AlN deposited on top of the optical opening this effect is negligible (Fig. 4a, green dashed curve
 169 represents AlN-passivated case). Figure 4b shows the lateral electric field profile of the simulated
 170 CdTe sensor with the defect inclusion and passivation layer along the optical opening for different
 171 distances from the surface. The field is uniform across the sample except for a local fluctuation
 172 of the field ascribed to the defect inclusion. For the field $1 \mu\text{m}$ below the surface the distribution
 173 reaches a peak at 4560 V/cm , then for $5 \mu\text{m}$ the peak height is decreasing, at $10 \mu\text{m}$ there is still
 174 some disturbance of the field and after $40 \mu\text{m}$ it becomes uniform. Also the electric field strength
 175 is almost two times higher for the detector with a dielectric on top of the optical opening. In the
 176 simulation, a positive fixed oxide charge was used with the absolute value of Q_f equal to 1×10^{12}
 177 cm^{-2} . With the AlN layer on top of the optical opening, the potential difference increases and
 178 the strength of the electric field changes to a higher value. In Fig. 5, a simulated transverse field
 179 distribution as well as corresponding transient currents are shown for different oxide charge values
 180 . It can be noticed that with the higher value of the interface oxide charge, the electric field strength
 181 has a higher value. For the corresponding current signals the higher value of the interface oxide
 182 charge gives a lower value of the amplitude of the signal.

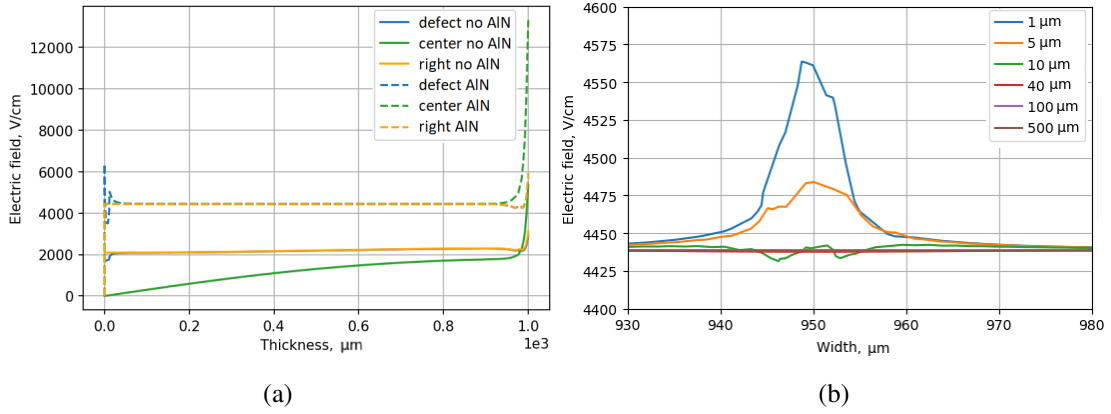


Figure 4: a) Simulated transverse distribution of electrical field for the diode with the defect inclusion, no bulk traps and with and without passivation on top of the optical opening and b) lateral electric field cuts with AIN on top of the optical opening for different distances from the surface in μm in the proximity of the defect position.

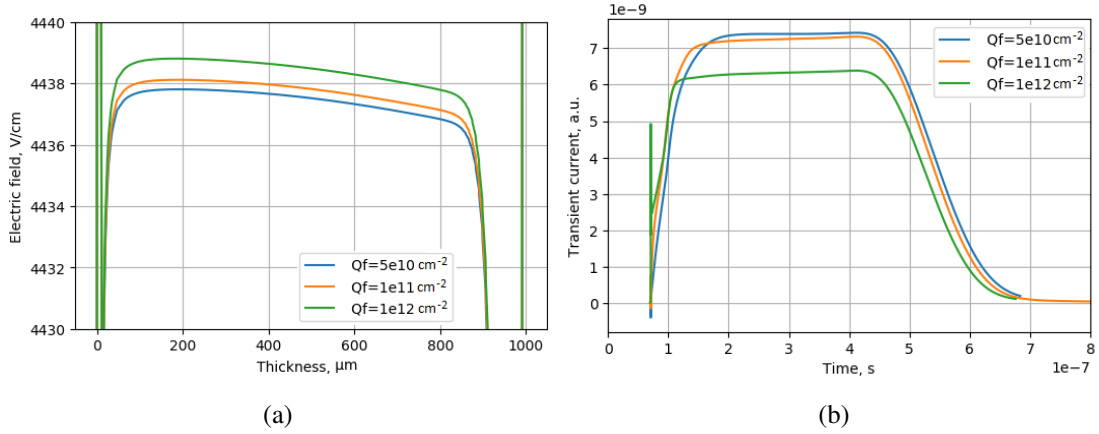


Figure 5: a) Simulated transverse electric field distribution and b) corresponding transient current at the position of defect inclusion with AIN on top of the optical opening for different oxide charges Q_f .

183 The waveforms corresponding to electric fields with and without passivation in Fig. 4a are
 184 shown in Fig. 6. When there is no AIN film on top of the optical opening, the electric field is small
 185 enough that the signal duration is much longer than $1 \mu\text{s}$. At the center of the opening without AIN
 186 film, the electric field near the surface is zero, so the charge carrier drift velocity slows in the low
 187 potential region and the signal evolves very slow. We see only the beginning of the signal with very
 188 low amplitude. On the right side of the opening, the current reproduces the signal with no defect in
 189 the Fig. 3a. The electric field strength at the center of the optical opening with the dielectric on top
 190 is almost the same as for the right side of the device, therefore the transient currents are identical
 191 as well. Comparing two transient signals at the position of the defect inclusion with and without
 192 passivation layer in Fig. 6, one can notice that the resulting current duration is 600 ns with the AIN
 193 deposited, while for the case without dielectric on the optical opening, the signal is longer than

194 1000 ns. The narrow peak in the beginning of the signal disappears with the passivation with the
 195 positive fixed charge, as the electric field strength increases, the electron drift velocity increased
 196 as well and the electrons are collected by the contact right away. It should be pointed out, that the
 197 shape of the signal with the defect inclusion and AlN on top of the opening has a characteristic form
 198 at the defect position, which can be easily identified from the surroundings.

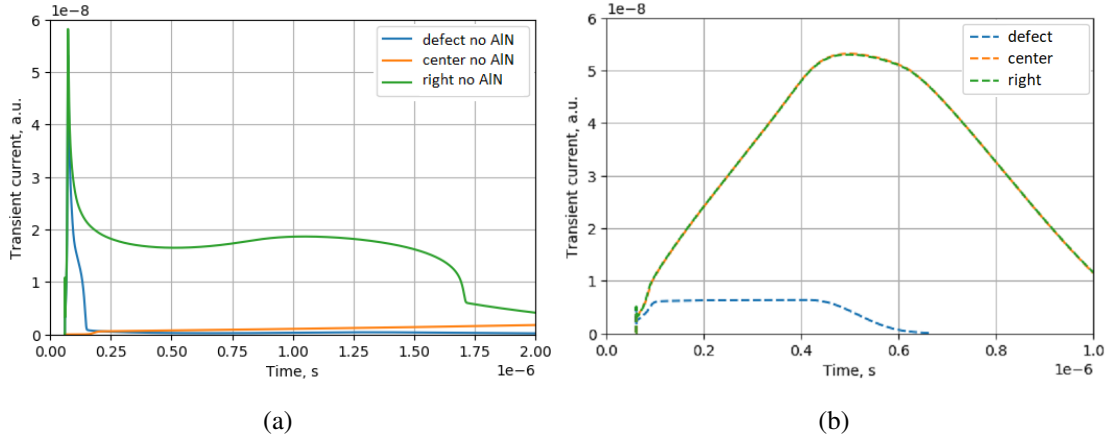


Figure 6: a) Simulated transient current for simulated diode with the defect inclusion, no surface passivation and no bulk traps. b) Simulated transient current for simulated diode with the defect inclusion, surface passivation and no bulk traps.

199 Finally, the bulk trap levels were implemented as to take into account the highly defected CdTe
 200 bulk material. In order to reproduce the measured double peak electric field distribution, a new defect
 201 model was created. In the upper half of the structure, the acceptor trap level was introduced with the
 202 energy 0.72 eV from conduction band and electron and hole capture cross section $\sigma_{e,h} = 2 \times 10^{-13}$
 203 cm^2 . For the bottom half of the created diode, the donor level was implemented with the same energy
 204 level and electron and hole capture cross section of $\sigma_{e,h} = 1 \times 10^{-16} \text{cm}^2$. The acceptor and donor
 205 concentration of $1 \times 10^{12} \text{cm}^{-3}$ was used. The electric field distributions of the abovementioned
 206 structure are shown in Fig. 7a. In Fig. 7b the simulated transients are plotted. One can notice that the
 207 electric field shape reproduced by the waveforms and the transient signal amplitude at the position
 208 of the defect inclusion is around 4 times smaller than the signal at other positions of the device.

209 In a real CdTe crystal, there are different types of defect complexes that can be spread all over
 210 the bulk of the device [22], but in the simulation we used only one defect inclusion to see its effect
 211 on the waveforms. As an illustration of the dependence of the position and radius of the defect,
 212 Fig. 8a shows charge collection for different defect positions. The closer the defect inclusion is
 213 located to the diode surface, the higher is the impact of it on the red laser induced transient current.
 214 After around $19 \mu\text{m}$ from the surface there is no impact of the defect to the charge collection. In
 215 Fig. 8b the effect of the defect diameter is depicted. In this simulation, the defect inclusion is placed
 216 at $8 \mu\text{m}$ below the surface and the defect radius is varied. It is shown that for the smaller sized
 217 defect, a larger fraction of charge carriers reaches the diode backplane and thus the influence of
 218 the defect on the CCE is less. All the above transient current simulations were performed at the
 219 center position of the inclusion. However, if the laser beam was directed on the optical opening a

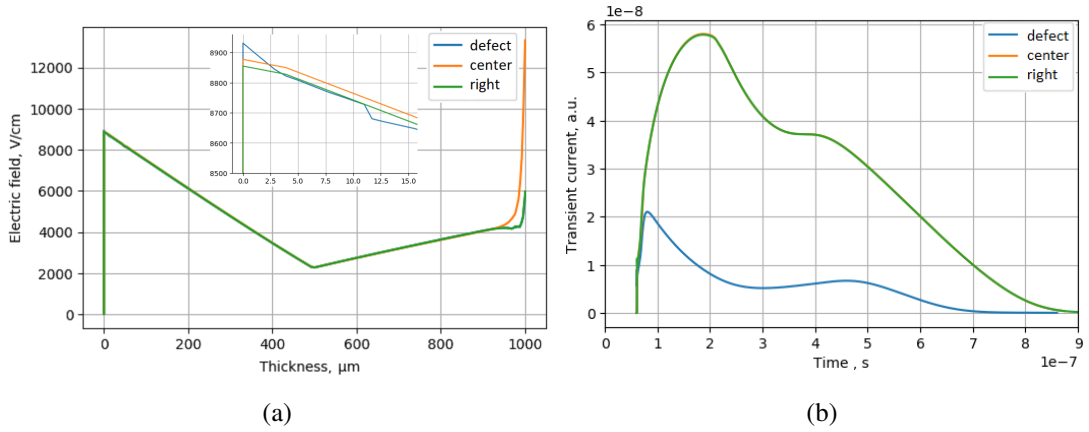


Figure 7: a) Simulated transverse electric field distribution for the diode with the defect inclusion, bulk traps and passivation layer and b) corresponding transient currents.

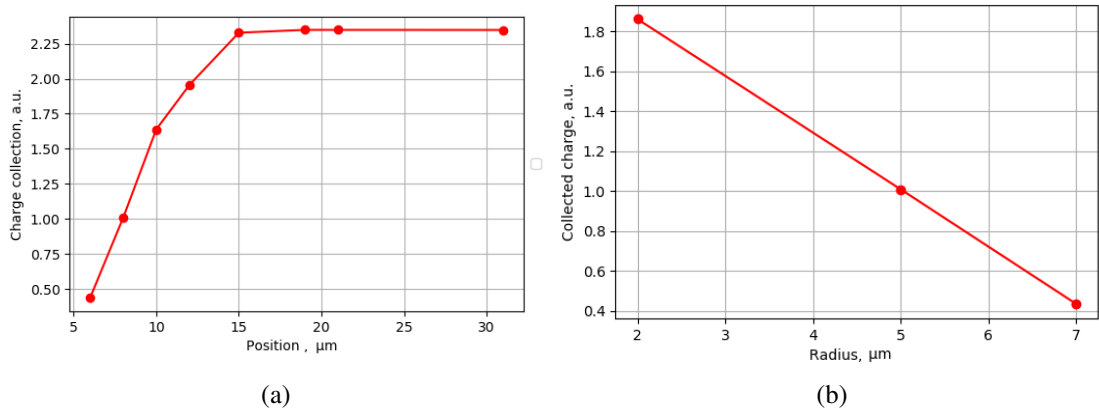


Figure 8: Simulated charge collection for different a) defect positions with the radius 5 μm and b) different defect radius of the inclusion with the defect position of 8 μm below the surface. The beam diameter is 10 μm for both cases.

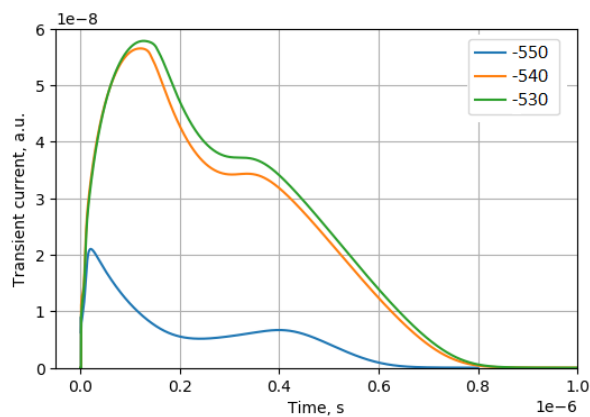


Figure 9: Simulated transient currents for the laser pointed at 3 different points at the optical opening where -550 is at the center of the defect.

220 bit shifted related to the defect center, the shape of the signal changes as well, as can be seen in
 221 Fig. 9. The closer the creation point of the charge carriers is to the center of the defect, the more
 222 impact it has on the waveform.

223 3.2 Experimental results

224 By raster scanning the area of the opening in the horizontal direction, the uniformity of the detector
 225 is analyzed. The resulting plot of the CCE in the optical opening is presented in Fig. 10a. In the
 226 plot, the CCE is normalized to the maximum value in the area. The fact that there is a passivation
 227 layer deposited in our sample can be an explanation why there is no minimum of charge collection
 228 in CCE map. From Fig. 10b we can also see that in the low-CCE region, the drift velocity is also
 229 lower than on the upper half of the opening. This could be resulting from trapping and de-trapping
 230 of the carriers [23].

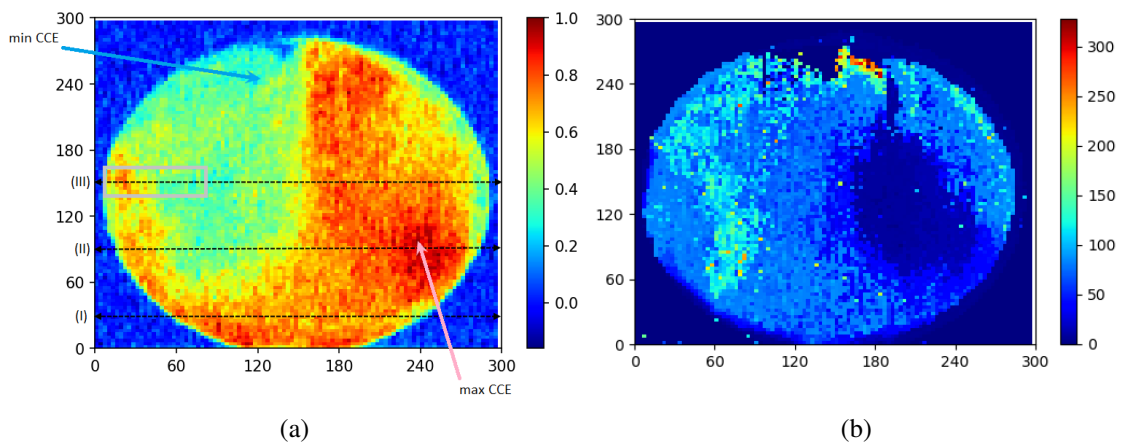


Figure 10: a) TCT area scan and b) the corresponding signal rise time at the optical opening of the CdTe detector at 660 nm. The area marked with a rectangle in (a) is discussed later in the paper.

231 The shape of the signals in the point with maximum and minimum CCE shown with the arrows
 232 in Fig. 10a and at the center of the optical opening are depicted in Fig. 11. The signal has a peak in
 233 the beginning and a long tail of the distributions that is produced both by the trapping-detrapping
 234 effects, and by the holes drifting to the sensor back-plane. The transient signal ends within 600 ns
 235 for the point with the lowest CCE, while the transient duration for the highest CCE is around 900 ns.
 236 The transient signal has a double peak shape [24]. Since the current is induced by charge moving
 237 in an electrical field, the shape of the signal is directly proportional to the electric field inside the
 238 sensor. The double peak signal gives us an evidence of the double peak electric field distribution
 239 through the bulk due to space charge build up at the contacts, probably in consequence of strongly
 240 trapped carriers in deep levels in the material [25].

241 In Fig. 12, the TCT signal cuts obtained from the oscilloscope at three different horizontal
 242 positions I, II and III of the TCT area scan map are depicted. These three horizontal cuts are shown
 243 in Fig. 10 with dashed lines and labeled. Each pixel represents a transient current amplitude where
 244 the x axis is a vertical position of the optical opening and y axis is a time of the waveforms. One
 245 can notice that from around 200 ns to 400 ns, the current signal has its minimum. For the TCT

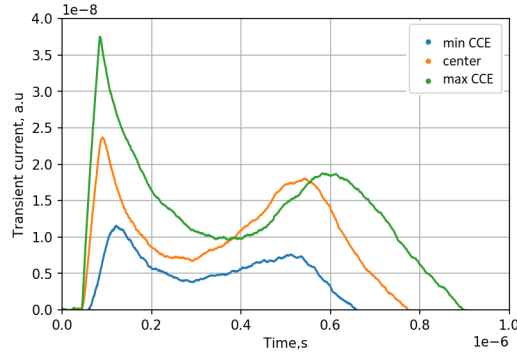


Figure 11: Transient currents for the point with maximum and minimum CEE shown with the arrows in Fig. 10a and at the centre of the optical opening .

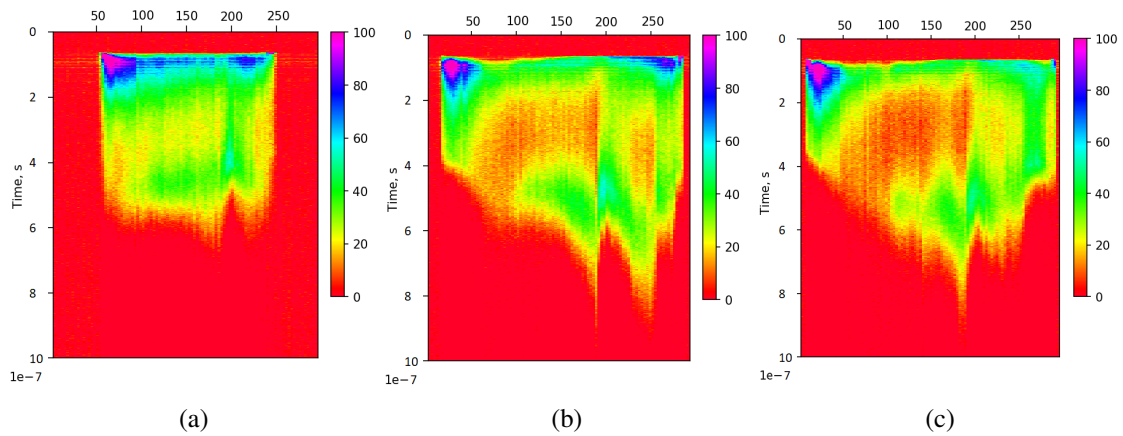


Figure 12: Transient current cuts at the I, II, and III horizontal position of the optical opening shown with dashed line in Fig. 10a.

246 signal cut at a horizontal position I, where we see a uniform distribution of charge collection in the
 247 CCE map, the waveform durations are almost equal comparing to the other cuts. Likewise there is
 248 a minimum of the signal height almost at the middle of the transient duration. For the cuts at the
 249 center of the optical opening line III and at the position II, the signal length is much more scattered
 250 and the minimum is more pronounced. The longer signal could be associated with a smaller value
 251 of electric field at this point. In contrary the shorter transient can indicate a higher field, or more
 252 likely a presence of some defect that can trap charge carriers or act as charge drains, again leading
 253 to charge loss.

254 Figure 13a shows a closeup of the rectangular area marked in Fig. 10a. In Fig. 13b the
 255 measured transient currents at two points, with higher and lower CCE, from this area are depicted.
 256 The simulated signals are plotted with dashed lines. One can notice that the transient signal for
 257 the point B with the minimum CCE is well reproduced by the simulation with the defect inclusion.
 258 However, the simulated currents at the position A where the higher charge collection has occurred,
 259 the simulation without any defect does not reproduce the measurement results precisely. This can
 260 be explained by the fact that in a real CdTe crystal, there are different types of defect complexes

261 and they can be spread all over the bulk of the device. The simulation model with one defect works
 262 well in areas with a high concentration of defects, but may not be fully representative for such areas
 263 where defects are more sparse. Nonetheless, simulations demonstrate the ability of the transient
 264 current technique to be used in distinguishing between areas with high and low concentration of
 265 defects.

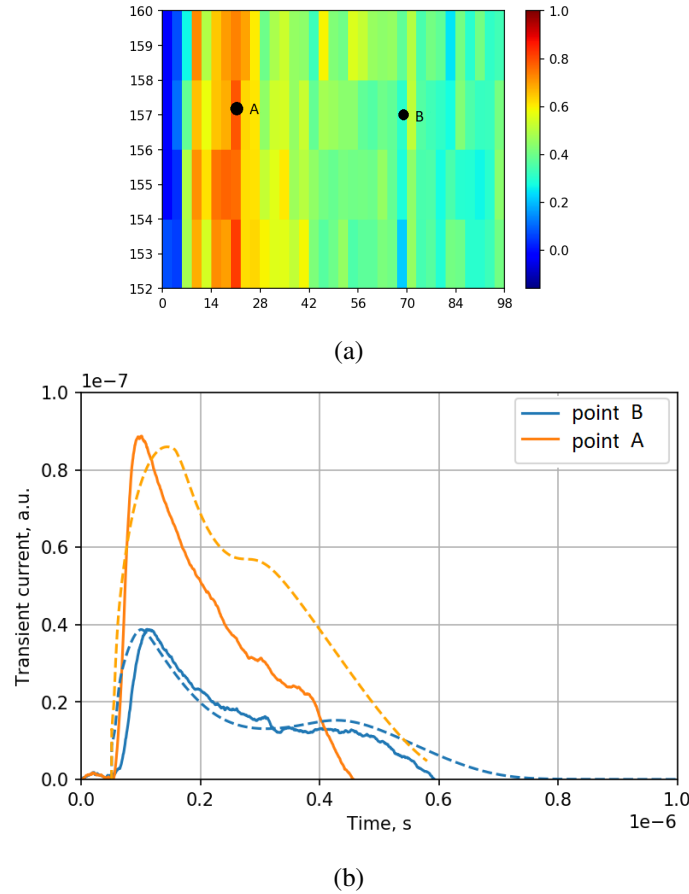


Figure 13: a) Zoomed part of the CCE map marked with rectangle in Fig. 10a. b) Simulated (dashed) and measured (solid) transient currents at the points A and B of the optical opening of the CdTe detector.

266 4 Conclusions

267 TCAD simulations are a powerful tool in aiding semiconductor detector design and understanding
 268 complex physical problems. Numerical simulations were used to create a model of a local bulk
 269 defect to better understand the effect of it on the transient current. This model shows that the
 270 presence of the local defect leads to a reduction in charge collection efficiency. Depending on
 271 the defect inclusion size, position and the position of the laser beam pointed on the surface of the
 272 optical opening, the transient current have different shapes. Defect inclusions that are closer to the
 273 surface and have a bigger diameter, if the trap level energies, trap concentration and electron and

274 hole capture cross sections are unchanged, have a higher impact to the charge collection by red laser
275 TCT. Shifted laser beam position from the center of the defect result in the fluctuations of the signal
276 form as well. The surface passivation, especially the fixed oxide charge value, plays an important
277 role in electric field formation and should be taken into account while designing the detector.

278 Simulation adds an evidence to the conclusion that the transient current has a characteristic
279 shape at a defect position, which can be clearly distinguished from the surroundings using transient
280 current technique. We were able to reproduce the measurement results adequately with a simple
281 simulation model with one defect inclusion.

282 CdTe has a large amount of extended crystallographic defects that deteriorate the device
283 performance. It is crucial to evaluate the quality of the material. A combination of the simulations,
284 TCT and three-dimensional (3D) infrared microscopy (IRM) would show the impact of the localised
285 defect of the raw material on the performance of the processed detector.

286 All measurements that were shown in this paper were made by using only one bias level, and
287 at room temperature. Further studies will involve, among others, analysis of effects of bias level,
288 impact of temperature variation, and changes in laser parameters.

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