



Second-order cone programming for rolling friction contact mechanics

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Minh-Hoang Nguyen, Vincent Acary, Paul Armand. Second-order cone programming for rolling friction contact mechanics. SMAI MODE 2022 - Journées du groupe MODE de la Société de Mathématiques Appliquées et Industrielles, May 2022, Limoges, France. pp.1-1. hal-03761228

HAL Id: hal-03761228

<https://hal.inria.fr/hal-03761228>

Submitted on 26 Aug 2022

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Second-order cone programming for rolling friction contact mechanics

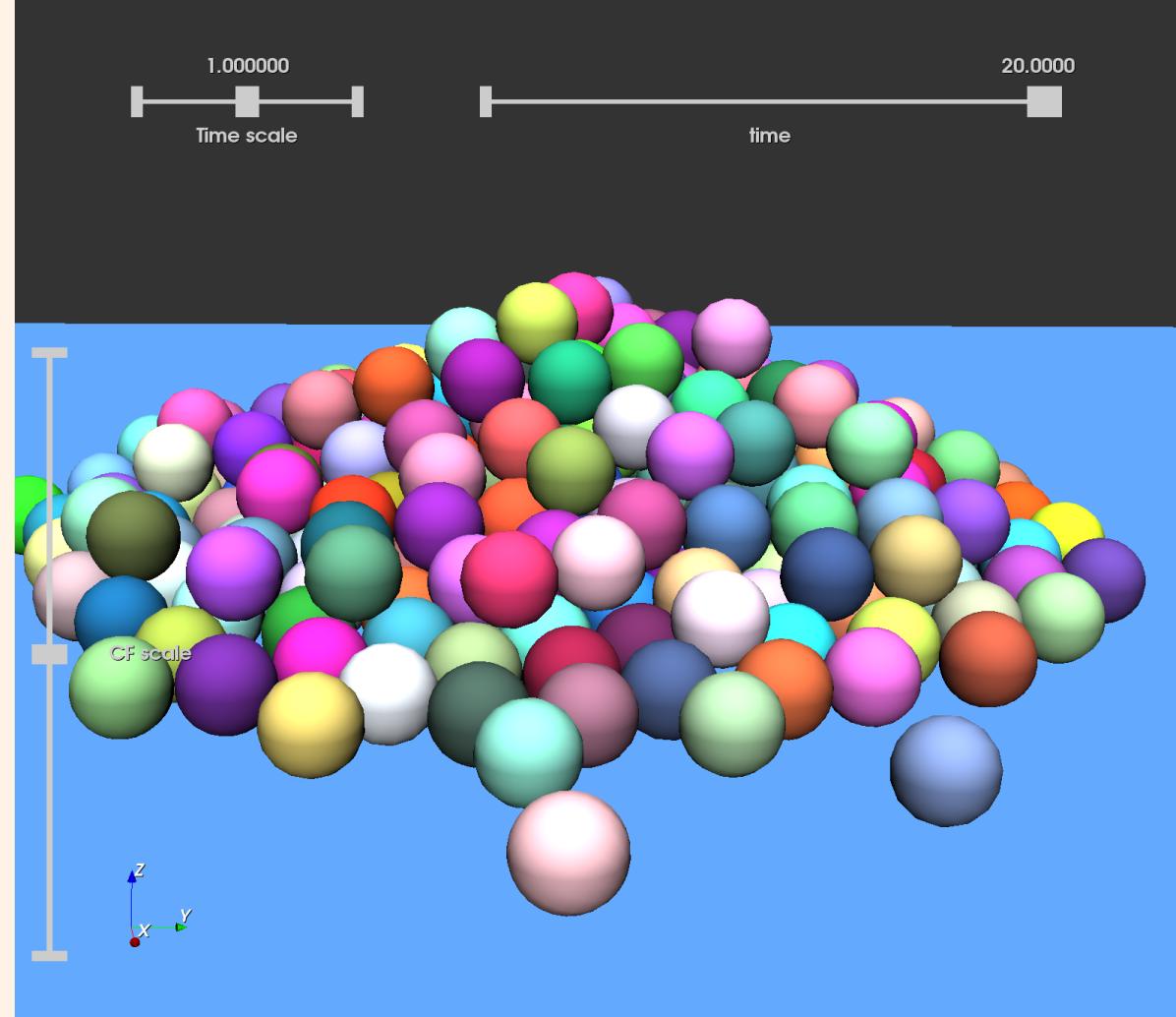
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GENERAL FRICTION CONTACT PROBLEM



$$\begin{aligned} Mv + f - H^\top r &= 0 \\ Hv + w &= u \\ \mathcal{F}^* \ni u &+ \Phi(u) \perp r \in \mathcal{F} \end{aligned}$$

ORIGINAL ROLLING FRICTION CONE

$$\mathcal{F} = \prod_{i=1}^n \mathcal{R}_i := \{r_i = (\bar{r}_i, \tilde{r}_i) \in \mathbb{R}^5 : \max\{\|\bar{r}_i\|_2, \|\tilde{r}_i\|_2\} \leq r_{i0}\}$$

$$\mathcal{F}^* = \prod_{i=1}^n \mathcal{R}_i^* := \{u_i = (u_{i0}, \bar{u}_i, \tilde{u}_i) \in \mathbb{R}^5 : \|\bar{u}_i\|_2 + \|\tilde{u}_i\|_2 \leq u_{i0}\}$$

$$\begin{array}{ll} \min_{v,u} \frac{1}{2}v^\top Mv + f^\top v & \max_{v,r} -\frac{1}{2}v^\top Mv - w^\top r \\ (\mathbf{P}) \quad \text{s.t. } Hv + w = u & (\mathbf{D}) \quad \text{s.t. } Mv + f - H^\top r = 0 \\ u \in \mathcal{F}^* & r \in \mathcal{F} \end{array}$$

Since \mathcal{F} is not self-dual, the Jordan algebra cannot be used as it is.

REFORMULATION WITH PRODUCT OF LORENTZ CONES

To simplify, set $n = 1$. By letting $u_0 = t + t'$, we obtain

$$\begin{array}{ll} \min_{v,z} \frac{1}{2}v^\top Mv + f^\top v & \max_{v,y} -\frac{1}{2}v^\top Mv - w^\top Ky \\ (\mathbf{P}') \quad \text{s.t. } Hv + w = Jz & (\mathbf{D}') \quad \text{s.t. } Mv + f - H^\top Ky = 0 \\ z \in \mathcal{L}^2 & y \in \mathcal{L}^2 \end{array}$$

where

$$J = \begin{pmatrix} 1 & 1 \\ I_2 & I_2 \end{pmatrix}, \quad K = \begin{pmatrix} 1 & 0 \\ I_2 & I_2 \end{pmatrix}, \quad z = \begin{pmatrix} t \\ \bar{u} \\ t' \\ \tilde{u} \end{pmatrix} \quad \text{and} \quad y = \begin{pmatrix} r_0 \\ \bar{r} \\ r_0 \\ \tilde{r} \end{pmatrix}.$$

Note that

- $Jz = u$, $Ky = r$ and $KJ^\top = I$,
- \mathcal{L}^2 is self-dual, then Jordan algebra can be used.

EQUAL STEPLENGTHS

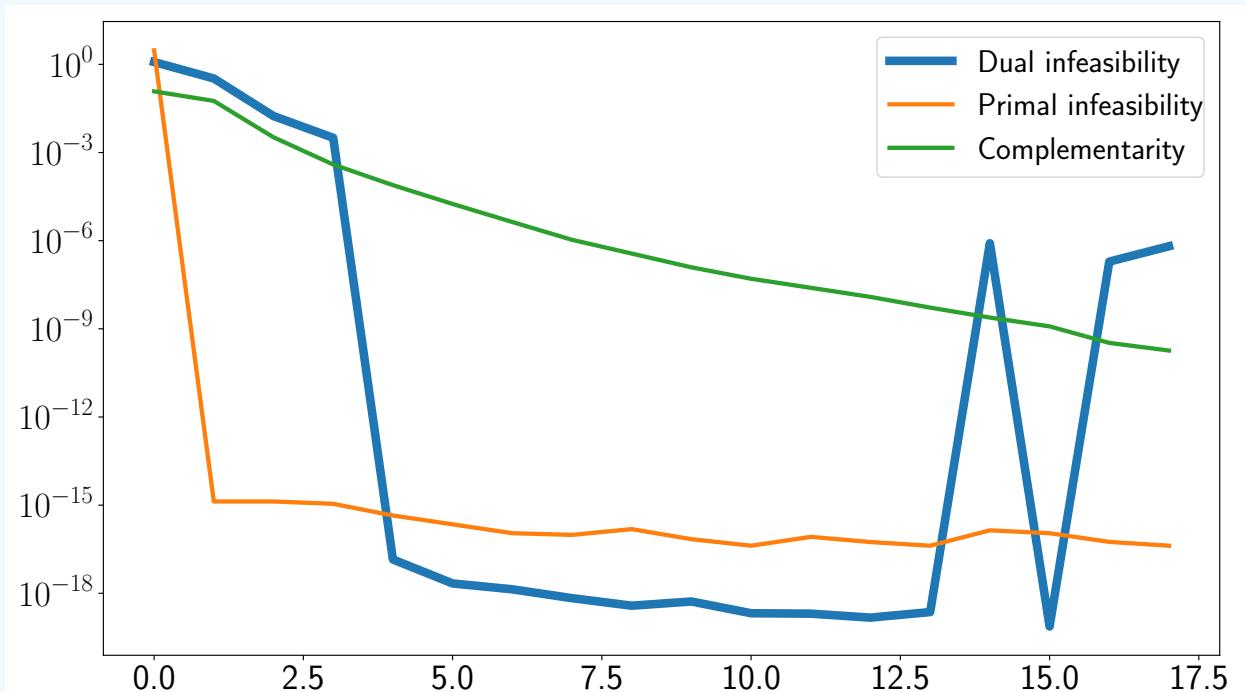


Figure 1. $n = 70$, steplengths $\alpha_p \neq \alpha_d$

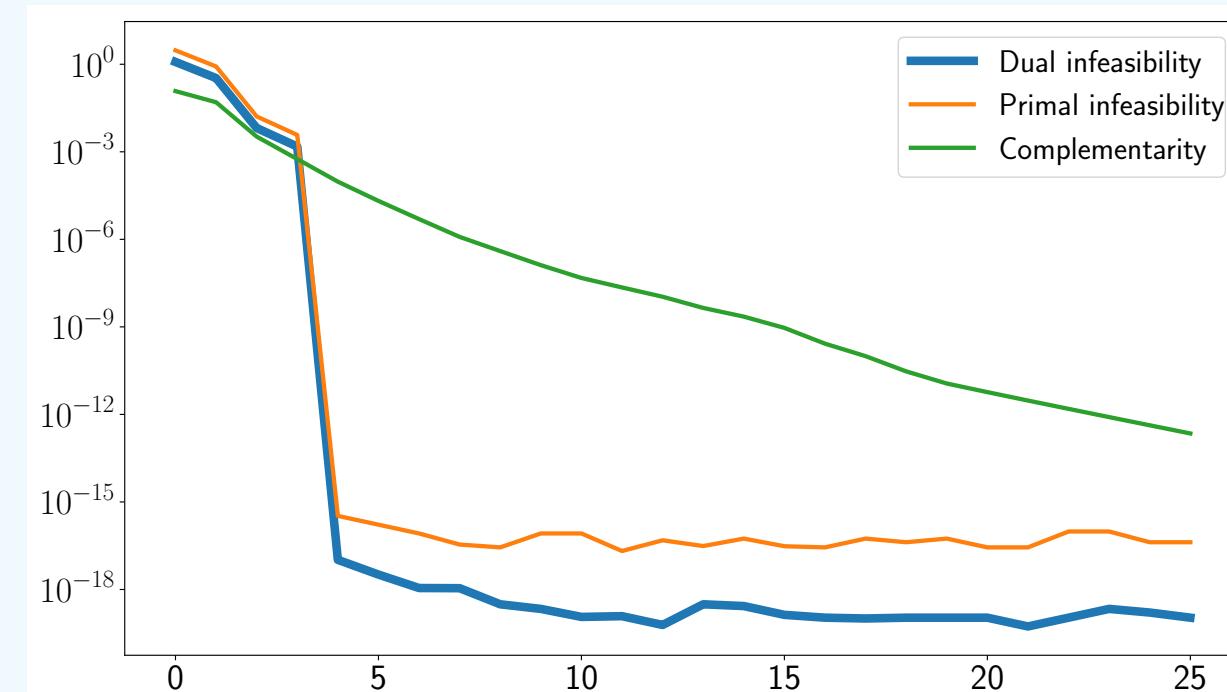


Figure 2. $n = 70$, steplengths $\alpha_p = \alpha_d$

Primal-dual infeasibilities

$$\text{pinfeas}^+ = (1 - \alpha_p)\text{pinfeas} + \alpha_p \xi_p$$

where

$$\text{dinefeas}^+ = (1 - \alpha_d)\text{dinefeas} + \alpha_d \xi_d + (\alpha_d - \alpha_p)Md^v$$

ξ_p, ξ_d are residual vectors.

THEORETICAL RESULT FOR FRICTION CONTACT MECHANICS WITHOUT ROLLING FRICTION

■ For the case without rolling friction, the original friction cone \mathcal{F} is the Lorentz cone \mathcal{L} . If (\mathbf{P}) is feasible, then it has a unique optimal solution (v^*, u^*) . It is not the case for (\mathbf{D}) , because H is rank deficient.

■ If the **Slater's conditions** and the **strict complementarity** hold, there are 3 possible cases:

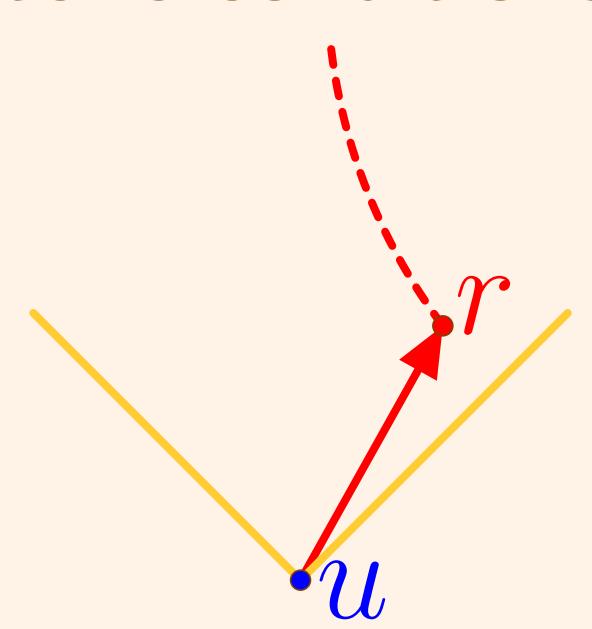


Figure 4. $u = 0, r \in \text{int}(\mathcal{L})$

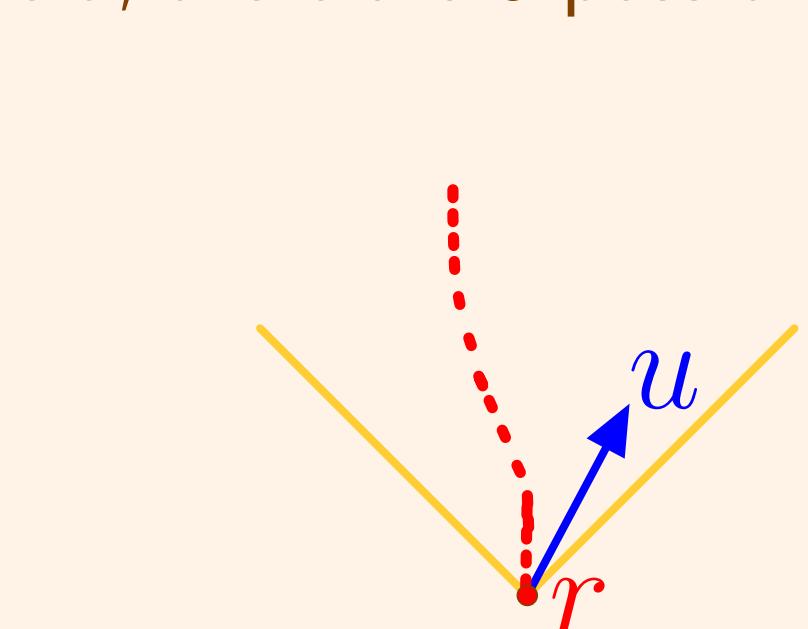


Figure 5. $u \in \text{int}(\mathcal{L}), r = 0$

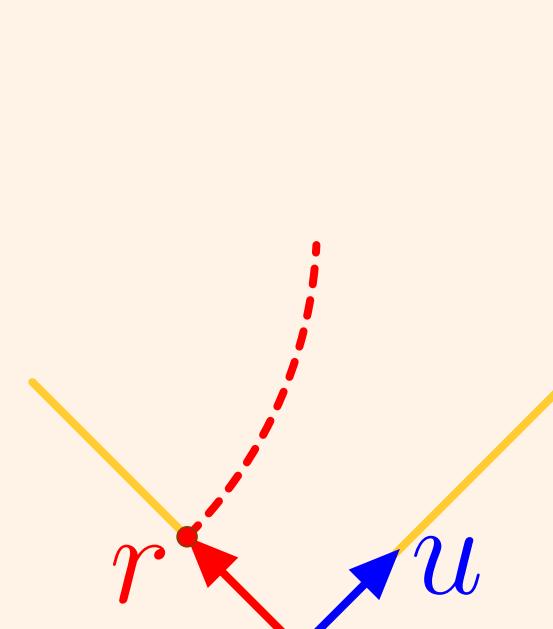


Figure 6. $u \in \text{bd}(\mathcal{L}), r \in \text{bd}(\mathcal{L})$

Then, the optimal solution r will converge to the **analytic center** of the optimal set \hat{R} which is the unique optimal solution of the problem

$$\min_{r \in \text{ri}(\hat{R})} \psi(r) := - \sum_{i \in B} \log \det r_i - \sum_{i \in N} \log r_{i,0},$$

where (B, N, R) is a partition of $\{1, \dots, n\}$.

■ This result can be extended to the case of rolling friction.