

Article

Harnessing of Different WECs to Harvest Wave Energy along the Galician Coast (NW Spain)

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Abstract: The wave power resource (WP) was calculated along the Galician coast (NW Spain) over the period 2014–2021 using high spatial resolution hourly data from the SWAN model. In addition, the electrical energy (P_E) that can be extracted for a particular wave energy converter (WEC) was analyzed for four different WECs (Oyster, Atargis, Aqua Buoy, and Pelamis). The performance of every WEC was also calculated attending to two parameters: the power load factor (ϵ) and the normalized capture width with respect to the WEC's geometry (efficiency). Results show that the WP resource is lower than 10 kWm^{-1} onshore, but it increases to about 50 kWm^{-1} offshore. Atargis obtained the highest P_E , and it is the most efficient device ($\epsilon \sim 40\%$ and efficiency $\sim 45\%$). Pelamis showed the lowest performance in offshore areas ($\epsilon \sim 15\%$, efficiency $< 10\%$). A different type of WEC should be considered for every location along the coast depending on its size, performance parameters, and coexistence with other socio-economic activities and protected environmental areas.

Keywords: wave power; wave energy converters (WECs); Galician coast; SWAN



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1. Introduction and Studied Area

More than 81% of the world's primary energy consumption comes from fossil fuels [1], which have a clear influence on the increase in greenhouse gases and global temperature [2]. In addition, global energy demand continues to rise, and fossil resources are increasingly scarce [3,4], highlighting the urgency of the energy transition. At the United Nations Conference on Climate Change (COP26), held in Glasgow in the autumn of 2021, many countries agreed upon a series of political action guidelines. Among them, the 1.5 °C scenario was maintained, for which it is necessary to reduce greenhouse gas emissions by 45%—with respect to 2010 levels—at the end of the current decade and reach zero emissions in 2050 [5]. One of the United Nations 2030 Agenda for Sustainable Development goals is to “increase substantially the share of renewable energy in the global energy mix” to mitigate global warming and ensure energy supply [6]. To achieve the necessary success in developing renewable energy, it is essential to use all available renewable sources, including marine energy.

Ocean waves continually form on the ocean surface and can travel thousands of miles with minimal energy loss [7]. A higher and more stable density power [7,8] makes wave energy a clear alternative to other “more conventional” renewable energies. In fact, the theoretical potential of wave power is 29,000 TWh per year, which is enough to meet the world's electricity demand [9]. In addition, wave energy has the advantage of having more predictability than solar or wind power and is less dependent on environmental

factors [10]. Unlike offshore wind power, the wave power resource is not yet being commercially exploited [9]. The survivability of the wave energy converters in the harsh marine environment, the lack of consensus on the choice of the most suitable device, and their economic costs have hindered their commercialization since the first patent in 1799 [11]. However, many of the wave energy converters can be scalable in size according to local wave characteristics to optimize their efficiency and make them economically profitable [10]. Another drawback is that wave energy devices have to coexist with other uses of the sea, such as shipping, fishing, or aquaculture. Nevertheless, these marine businesses—the so-called blue economy—can benefit from the installation of wave energy harvesting devices by not having to look for energy sources on land [9]. In addition, the installation of these devices in the vicinity of shellfishing areas could also protect them from waves by dissipating part of their energy.

The natural wave power (WP) resource depends on the sea state and is determined by the wave significant height (H_s) and the wave peak period (T_p). The WP resource is defined as the amount of energy per unit of time and length of the wave front (expressed in kWm^{-1}) transmitted in the direction of wave propagation [12]. Only a percentage of this resource will be transformed into electricity. This percentage depends on the wave energy converter (WEC) and its physical and technical characteristics (see [13–17] for more details). WECs can be classified attending to several factors. Depending on their operating principle, they can be oscillating water columns (OWS), oscillating bodies, wave-activated bodies, or cycloidal wave absorbers, among others (see [13,18–20] for more details). Regarding their optimal location, WECs are categorized into onshore, nearshore, and offshore devices [10,19–21]. They can also be classified as point absorbers, attenuators, and terminators according to their orientation with respect to the wavefront and their shape [20–23]. Attenuators and terminators have an elongated shape and are placed parallel and perpendicular to the direction of the wavefront, respectively, while point absorbers are similar to buoys. Attenuators and terminators must be larger than the predominant wavelength of the prevailing waves, while point absorbers have smaller dimensions than the main wavelength [21,24].

According to IRENA [25], in 2020, there was a total of 33 wave energy converters with a combined capacity of 2.3 MW distributed around the world. However, the European Commission aims to reach 1 GW of installed capacity by 2030 and 40 GW by 2050 [9]. Spain is the European country with the most R&D facilities in floating wind power and other marine energies [26,27]. For example, the experimental zone for the use of marine energy in Punta Langosteira (Galicia, Spain)—within the EnergyMare project—stands out. This site has the second-highest testbed wave energy density in the world, behind the south coast of Wales [27]. The Spanish government has set itself the goal of reaching 7 GW in floating wind power and between 40 and 60 MW of other marine energies—including wave power—by the end of this decade [27]. Galicia is the Spanish region with the highest wave energy potential ($40\text{--}45 \text{ kWm}^{-1}$), followed by the Cantabrian Sea (30 kWm^{-1}) and the north of the Canary Islands (20 kWm^{-1}) [27].

There are several studies on the wave power resource in large areas such as the Mediterranean Sea [28], the Black Sea [29], or along the western coast of the Iberian Peninsula [7,12]. However, regional studies allow the identification of local phenomena and areas of greatest interest in terms of the available wave energy. These regional studies are of vital importance to promote studies at a local scale in various areas of the planet and achieve a global energy transition. Regional studies require a high or very high spatial resolution. Thus, the Galician shelf was previously analyzed with a spatial resolution of $0.25^\circ \times 0.25^\circ$ and with a higher resolution of $200 \text{ m} \times 200 \text{ m}$ at the particular area between Cape San Adrián and Cape Ortegal [30]. In the same way, different locations in the north and west shelf of the Iberian Peninsula were analyzed with a nested grid of $0.5' \times 0.5'$ [31,32]. Apart from analyzing the WP resource, previous studies have analyzed the amount of energy that can be actually harnessed by particular WECs at different points of the Iberian Peninsula shelf [12,32,33]. In these previous studies, the performance of the

WECs is normally characterized by means of the capture width, which do not consider the dimensions of the different devices, making their comparison impossible.

The aim of this study is to analyze the wave power resource and the electrical power that could have been extracted from four WEC devices along the Galician coast between 2014 and 2021. Due to the narrowness of the continental shelf (Figure 1), the analysis of feasibility of the four WECs along the Galician coast makes it necessary to calculate the WP resource with a very high spatial resolution (a maximum of ~ 75 m) and also limits the type of device used. This very high spatial resolution makes it possible to calculate the wave power resource and the performance of these devices inside the estuaries. The performance of each WEC will be limited to the optimal depth range for the installation of the device and will be determined attending to two parameters: the power load factor (ϵ) and the normalized capture width according to the WEC's geometry (efficiency). At this point, it is important to mention that it was developed as a new metric that allows comparisons to be made between different WECs taking into account their dimensions.

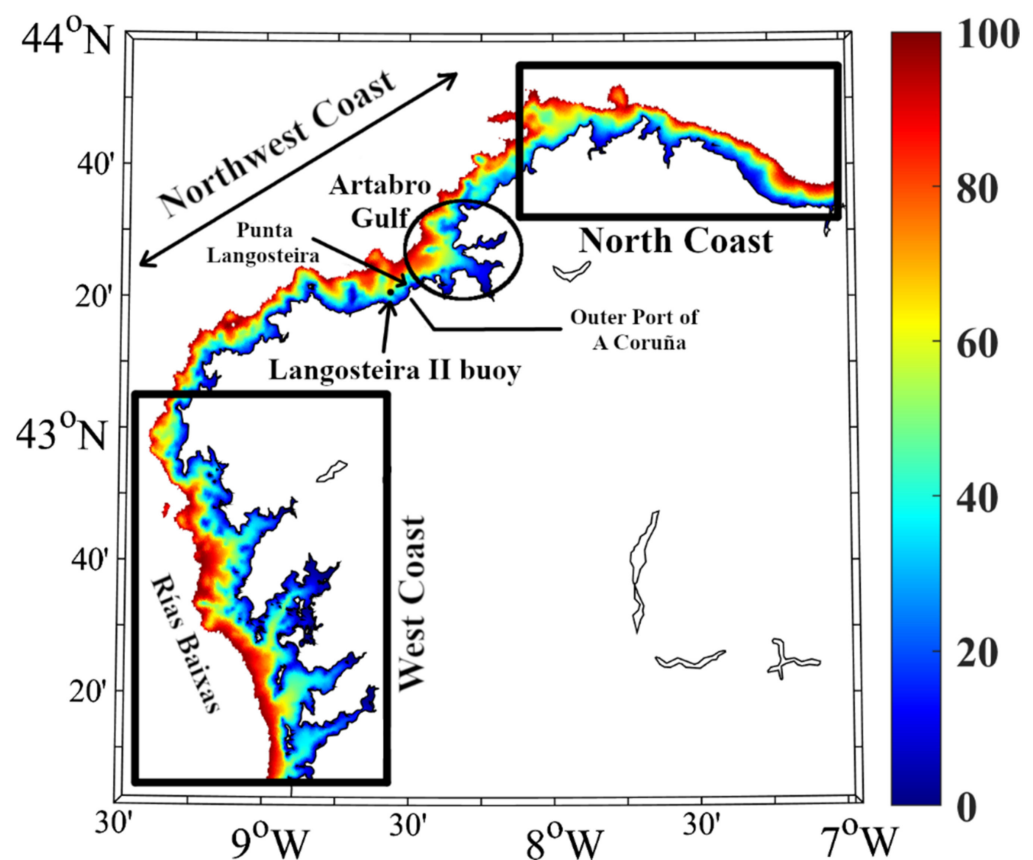


Figure 1. Study area. Colors represent the bathymetry (m).

2. Data and Methodology

2.1. Data

The wave parameters H_s and T_p were provided by MeteoGalicia, the regional administration in charge of weather forecast for Galicia, using simulations of the third-generation SWAN model developed by the Delft University of Technology [34–37]. SWAN solves the spectral action balance equations [34] (defined in [38]) and is the most adequate tool in order to simulate high-resolution coastal waves [34]. SWAN model uses an unstructured variable mesh, with a higher spatial resolution in coastal and estuarine areas—where it can reach 75 m resolution—than offshore [34]. Consequently, high-resolution wave data are obtained in the areas of interest without exceeding computational time. The SWAN model physics included bottom friction, shoaling, and depth-induced breaking, and the wave spectrum was discretized to a resolution of $\Delta f/f = 0.1$ between the frequency range of

0.0521–1 Hz and 36 directional bands. As boundary conditions, the implementation uses MeteoGalicia regional models for waves (WAVEWATCH III, with temporal and spatial resolution of 1 h and 2.5 arc minute, respectively), wind (WRF, with temporal and spatial resolution of 1 h and 4 km, respectively), and water level series (ROMS, with temporal and spatial resolution of 1 h and 4 km, respectively). These specifications are shown in Table 1.

Table 1. Main characteristics of the SWAN model set up in the present study.

Parameter	Value
<i>Computational grid</i>	
Spatial grid	Unstructured. Variable mesh step: 250 m–75 m
Frequency grid	Resolution: $\Delta f/f = 0.1$. Range: 0.0521 Hz–1 Hz
Directional grid	Resolution: 10°
<i>Processes activated</i>	
Local wave generation by wind	Yes (third-generation)
Limited depth processes	Yes (bottom friction, refraction, shoaling, depth-induced breaking)
Water level variations	Yes
Wave–current interactions	No
<i>Forcing</i>	
Boundary conditions	WaveWatch III. Temporal/Spatial resolution: 1 h/2.5 arc minutes
Wind	Meteogalicia WRF. Temporal/Spatial resolution: 1 h/4 km
Water level	Time series synthesis using the tidal solution of the MeteoGalicia ROMS model. Temporal/Spatial resolution: 1 h/4 km

Hourly time resolution data can be downloaded in daily folders from the THREDDS server (Thematic Realtime Environmental Distributed Data Service), http://mandeo.meteogalicia.gal/thredds/catalog/modelos/SWAN_HIST/galicia/catalog.html (accessed on 22 January 2022) [39]. Although each daily file contains data for a 4-day horizon, only the first 24 h of each file were selected to work in hindcast mode. Data series are available from 2014 onwards.

Simulation outputs were validated with Langosteira II buoy data, provided by Puertos del Estado (<https://www.puertos.es/es-es/oceanografia/Paginas/portus.aspx> (accessed on 22 January 2022), [40]), to assess the accuracy of the model results. This buoy is located in the Northwest Coast, at coordinates $8^\circ 33' W$, $43^\circ 22' N$ (Figure 1), being the only buoy that offers historical wave data on the Galician coast for the period considered in this study. Wave data have an hourly time resolution and are available from June 2013 to December 2021.

2.2. Methodology

Methods followed to validate the accuracy of SWAN model simulations to reproduce observed wave parameters (H_s and T_p) and to calculate the WP resource, and the WECs' efficiency are described below.

2.2.1. Validation

The validation process has been carried out by comparing H_s and T_p measured by the Langosteira II buoy and those calculated by the SWAN model at the point closest to the buoy for the period 2014–2021. This period was selected because it is the common period between both datasets. Four different statistics parameters have been used: normalized root mean square error (NRMSE), normalized bias error (NBias), Spearman's correlation coefficient (ρ_S), and the overlapping percentage (OP) between both series. RMSE is defined as the square root of the second sample moment of the differences between numerical and

observed values [41,42]. As the magnitude of RMSE depends on the actual values of the series, the NRMSE defined in Equation (1) is a better option to compare two series of data.

$$\text{NRMSE (\%)} = \frac{100}{\frac{1}{2}(\overline{x_i^{\text{num}}} + \overline{x_i^{\text{obs}}})} \cdot \sqrt{\frac{1}{N} \sum_{i=1}^N (x_i^{\text{num}} - x_i^{\text{obs}})^2}, \tag{1}$$

where N is the total number of elements in both the data series, x_i^{num} refers to numerical values from the SWAN model, and x_i^{obs} denotes the observed data series retrieved from the buoy. Barred variables $\overline{x_i^{\text{num}}}$ and $\overline{x_i^{\text{obs}}}$ correspond to mean values.

The normalized bias error (in percentage) [41] was calculated as

$$\text{NBias (\%)} = \frac{100}{\frac{1}{2}(\overline{x_i^{\text{num}}} + \overline{x_i^{\text{obs}}})} \cdot \frac{1}{N} \sum_{i=1}^N (x_i^{\text{num}} - x_i^{\text{obs}}). \tag{2}$$

The Spearman’s correlation coefficient was computed as

$$\rho_s = \frac{\text{cov}(R(x_i^{\text{num}}), R(x_i^{\text{obs}}))}{\sigma(R(x_i^{\text{num}})) \cdot \sigma(R(x_i^{\text{obs}}))}, \tag{3}$$

where $R(x_i)$ is the rank of the data series x_i , $\sigma(R(x_i))$ is its standard deviation, and $\text{cov}(R(x_i^{\text{num}}), R(x_i^{\text{obs}}))$ is the covariance between the rank variables [43].

The overlapping percentage was calculated as

$$\text{OP (\%)} = 100 \cdot \sum_{i=1}^n \min(f_i(x^{\text{num}}), f_i(x^{\text{obs}})), \tag{4}$$

where n is the number of bins in which series are classified, and $f_i(x)$ is the relative frequency of values in a given bin i. A number of 20 bins was used for H_s and 10 bins for T_p . An OP of 100% means that the model perfectly represents the observed data. The overlap test consists of calculating the OP between both series, and it has the advantage that the entire data distribution is considered. This method is based on the study of Perkins et al. [44] and has been used in previous studies [45].

2.2.2. Wave Power Resource

The WP resource is the wave power resource available in the natural environment. It is defined as the amount of wave energy flux per unit length of the wave front (expressed in kWm^{-1}) transmitted in the direction of wave propagation [12] and is represented by Equation (5):

$$\text{WP} = \frac{\rho g^2}{64\pi} H_s^2 T_e, \tag{5}$$

where ρ is the density of seawater (considered here as 1025 kgm^{-3}), g is the gravitational acceleration, H_s is the significant wave height, and T_e is the energy period. The latter can be expressed in terms of wave peak period, T_p , as follows:

$$T_e = \alpha T_p. \tag{6}$$

Factor α varies with the shape of the wave spectrum. A value of $\alpha = 0.9$ was assumed in the present study. This supposition is equivalent to assuming a standard JONSWAP spectrum with a peak enhancement factor of $\gamma = 3.3$ [7].

2.2.3. Parameters to Analyze WEC Performance

Total electric power depends on both the natural WP resource available and the performance of the WEC in extracting it. Every device operates in a different range of

depth, H_s and T_p . This means that if a sea state (H_s, T_p) does not belong to the WEC's operation range, no electric output will be generated. Operating intervals for H_s and T_p are included on the named "power matrix", which contains the electric power produced by the devices according to the sea state. In other words, each WEC obtains more energy with some sea states than with others so that each device is designed for certain wave conditions. The performance depends on this power matrix, which is provided by the manufacturer. Features such as WECs' geometric shape, size, and power take-off (PTO) parameters significantly influence the power matrix and thus the electric power output.

The expected average electric power (P_E , in kW) that can be extracted with a particular WEC is expressed by the Equation (7):

$$P_E = \frac{1}{100} \sum_{i=1}^{n_T} \sum_{j=1}^{n_H} p_{ij} P_{ij}, \tag{7}$$

where P_{ij} is the electric power obtained from an element ij of the power matrix of a particular WEC, p_{ij} is the probability of occurrence of a given sea state for this element of the power matrix (expressed in percentage), and n_T and n_H are the number of peak period and significant height bins considered, respectively. The methodology of [7,10,23,33,46] has been followed to compute P_E . Note that the power matrix is a matrix defined for a particular WEC, with specific geometric characteristics and a specific PTO principle. The same type of device with a different size, shape, or different PTO parameters would modify the power matrix and cause a change in the expected electrical power output. Additionally, if a sea state (H_s, T_p) is unlikely (small p_{ij}), the electrical power that can be extracted with that WEC will be smaller than if there is a more likely sea state.

Two parameters have been used to evaluate the performance of different devices to extract energy from waves: the power load factor (ϵ) and the efficiency. ϵ is defined as the relation between P_E and the maximum electric power that can produce a particular WEC (P_{max}), computed as the power matrix maximum value:

$$\epsilon (\%) = 100 \cdot \frac{P_E}{P_{max}}. \tag{8}$$

This dimensionless parameter reflects how far P_E is, which depends on the sea states at a particular location and the properties of the device, from the maximum power extractable from that device. Thus, a device well-fitted to the wave climate in the area would provide ϵ values close to 100%. Both P_E and P_{max} depend on the WEC size. Nevertheless, due to the fact that ϵ is defined as the ratio between the actual extracted power and the maximum extractable power, it can be used to compare devices with different geometries and sizes.

An additional parameter named efficiency was used to estimate the performance of the WECs in converting the wave energy into electricity. It is defined as the normalized capture width (C_w , in meters) with respect to the WEC's size [7,47]. In the literature, C_w is the width of the wave front that comprises the same amount of power as that absorbed by the WEC [47], and it is defined by Equation (9):

$$C_w = \frac{P_E}{WP}. \tag{9}$$

C_w is, like ϵ , one of the most common parameters to estimate WECs performances. However, as not all WECs have the same size, the new parameter efficiency has been introduced for this study. It is defined in the Equation (10):

$$\text{efficiency} (\%) = 100 \cdot \frac{P_E}{WP \cdot L} \tag{10}$$

where L is the WEC's length of the dimension by which the WEC captures the wave energy. The use of this parameter results in a dimensionless efficiency that allows the comparison among devices with different geometries and sizes.

Four different WECs have been considered: two point absorbers (Oyster and Aqua Buoy), an attenuator (Pelamis), and a terminator device (Atargis). Despite Oyster being classified on some occasions as an onshore terminator device [18,48], here, it is categorized as a point absorber due to its small size in comparison to the predominant wavelength. Although the development of the Oyster device was stopped a time ago [49], this device has been chosen as an example of a converter that operates at shallow depths since similar devices may be developed in the coming decades.

The technical properties of these devices can be found in [10,24,33,46,50–54] and summarized in Table 2. The different power matrices were obtained from [33,53].

Table 2. Type, maximum electric power, length opposite to the wave, and possible interval of depth for the installation of every analyzed WEC.

WEC	Type	P_{max} (kW)	L (m)	Depth (m)
Oyster	Point absorber	291	18	10–20
Atargis	Terminator	2530	60	40–100
Aqua Buoy	Point absorber	250	6	50–100
Pelamis	Attenuator	750	150	50–100

3. Results

3.1. Numerical Model Validation

The accuracy of the SWAN model to reproduce observed H_s and T_p measured by the Langosteira II buoy is shown in both Figure 2 and Table 3. Figure 2 represents the relative frequency of occurrence of a certain value of H_s (or T_p) contained in each bin. The red (blue) bars represent the relative frequency for the observed (numerical) data. The bars are plotted separately so that they can be properly differentiated. Blanks should not be interpreted as an absence of values, but rather the entire range of values on the x-axis is covered. Despite both data series being distributed over the same intervals, blue bars are drawn displaced with respect to the red ones for visualization purposes. Figure 2a shows that H_s data from MeteoGalicia are slightly underestimated for the smallest waves ($H_s < 1.575$ m) and overestimated for the largest ones. The comparison between the numerical and observed data is not clear for T_p . The SWAN model tends to overestimate T_p values in the intervals (7, 9), (9, 11), and (13, 15), and underestimates in the other bins (Figure 2b).

Table 3. Normalized root mean square error (NRMSE), normalized bias error (NBias), Spearman correlation coefficient (ρ_s), and overlapping percentage (OP) for significant wave height (H_s) and peak period (T_p).

Variable	NRMSE (%)	NBias (%)	ρ_s	OP (%)
H_s	20.10	8.72	0.94	92.26
T_p	14.82	−1.15	0.83	91.70

The NRMSE, the NBias error, the Spearman correlation coefficient (ρ_s), and the overlapping percentage (OP) between both series are shown in Table 3. The NRMSE and the NBias error show smaller values for H_s and similar values for T_p than those of Bento et al. in [32]. Values of ρ_s close to unity and an OP around 90% were obtained for both variables, which allow considering that the numerical simulations adequately reproduce the reality [45].

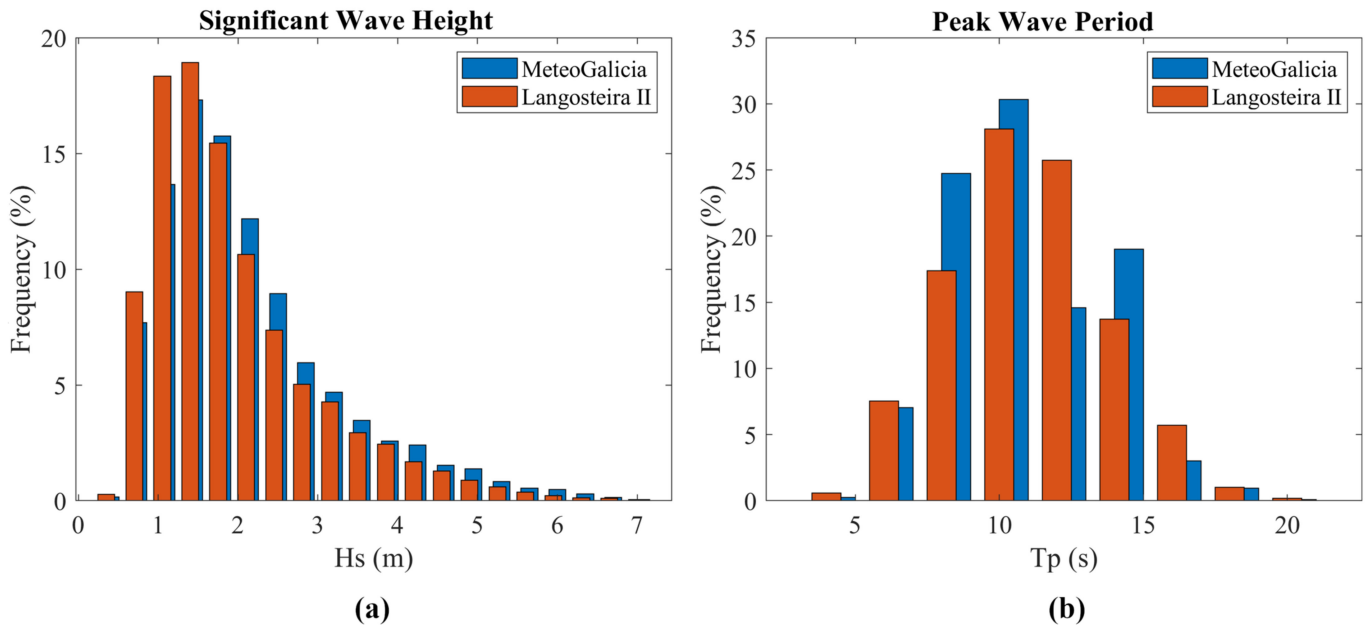


Figure 2. Histograms for (a) H_s and (b) T_p from the SWAN simulations (blue) and the Langosteira II buoy measures (red).

3.2. Wave Power Resource

First, the mean WP resource was calculated along the Galician coast from hourly data over the historical period (2014–2021). Figure 3 shows the WP resource for three regions: the West Coast (a), the Northwest Coast (b), and the North Coast (c). Overall, the WP resource is lower nearshore than offshore. Along the West Coast, WP increases from less than 10 kWm^{-1} inside the estuaries to around 50 kWm^{-1} at offshore (Figure 3a). As expected, the WP resource is related to the bathymetry—the shallowest areas are associated with the lowest WP resource. Spots of maximum WP resource ($\sim 60 \text{ kWm}^{-1}$) are found in submerged reef systems relatively far from the shore (Figure 3b,c). In the easternmost part of the North Coast, the resource is lower (around 20 kWm^{-1} at $\sim 10 \text{ km}$ from the coast, see Figure 3c) since waves usually come from NW, and that area is leeward.

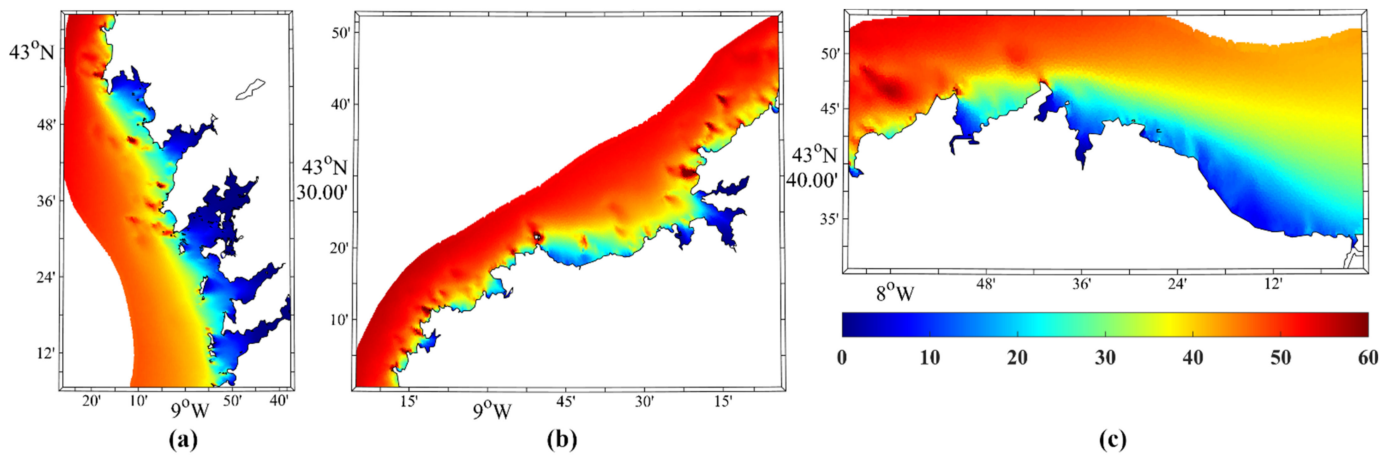


Figure 3. WP resource for (a) West Coast, (b) Northwest Coast, and (c) North Coast from 2014 to 2021.

3.3. Performance of WECs

Macroscopically, P_E patterns (Figure 4) are very similar for the three areas, decreasing landward, as previously observed for WP. The electric power that can be extracted from the Atargis device is greater compared to the other converters—an order of magnitude greater than Oyster and Pelamis and two orders greater than Aqua Buoy. These differences are justified by the disparities in the size of the devices, which result in the values of the WECs power matrices, and also by the fact that each device operates in a specific range of sea state (H_s , T_p). Similar values of P_E and their spatial distribution were found in [7] for the Aqua Buoy and Pelamis devices.

Along the West and Northwest Coast (Figure 5), the Atargis converter shows the most significant power load factor ($\varepsilon \sim 45\%$), followed by the Oyster converter ($\sim 40\%$ in shallow offshore areas) and Aqua Buoy with ε around 22%. Pelamis shows the most minor power load factor ($\sim 15\%$) in those regions. Note that the plotted area is different for each WEC, as each WEC works at different depth ranges. These results are consistent with those described in [7] for the Aqua Buoy and Pelamis devices, where P_E and ε show similar patterns. For example, along the North Coast the WECs performance decreases eastwards (right column). In this region, the power load factor for Atargis ranges between $\sim 30\%$ east of $8^\circ 36' W$ and $\sim 45\%$ north of the Northwest Coast. It ranges between $\sim 20\%$ east of $8^\circ 36' W$ and $\sim 40\%$ north of the Northwest Coast.

The efficiency percentage of WECs, represented in Figure 6, has a different distribution than the WP resource, P_E and ε , increasing landwards. Atargis shows the highest efficiency in the study area (more than 50% inside the estuaries and $\sim 35\%$ outside). For Oyster, efficiency around 35% is observed inside the estuaries (left column) and around 27% in the Artabro Gulf (middle column) and in the east part of the North Coast (right column). Aqua Buoy has a moderately homogeneous pattern of efficiency ($\sim 25\%$) in all regions. The Pelamis device shows a low efficiency ($< 10\%$) to exploit the WP resource in all the regions. Taking into account that the capture width is the efficiency multiplied by the length of the WEC, the Aqua Buoy and Pelamis efficiencies are consistent with the capture width (C_w) of 1.5 m and 3 m obtained by [7] for Aqua Buoy and Pelamis, respectively, along the North Coast for the period (1979–2005).

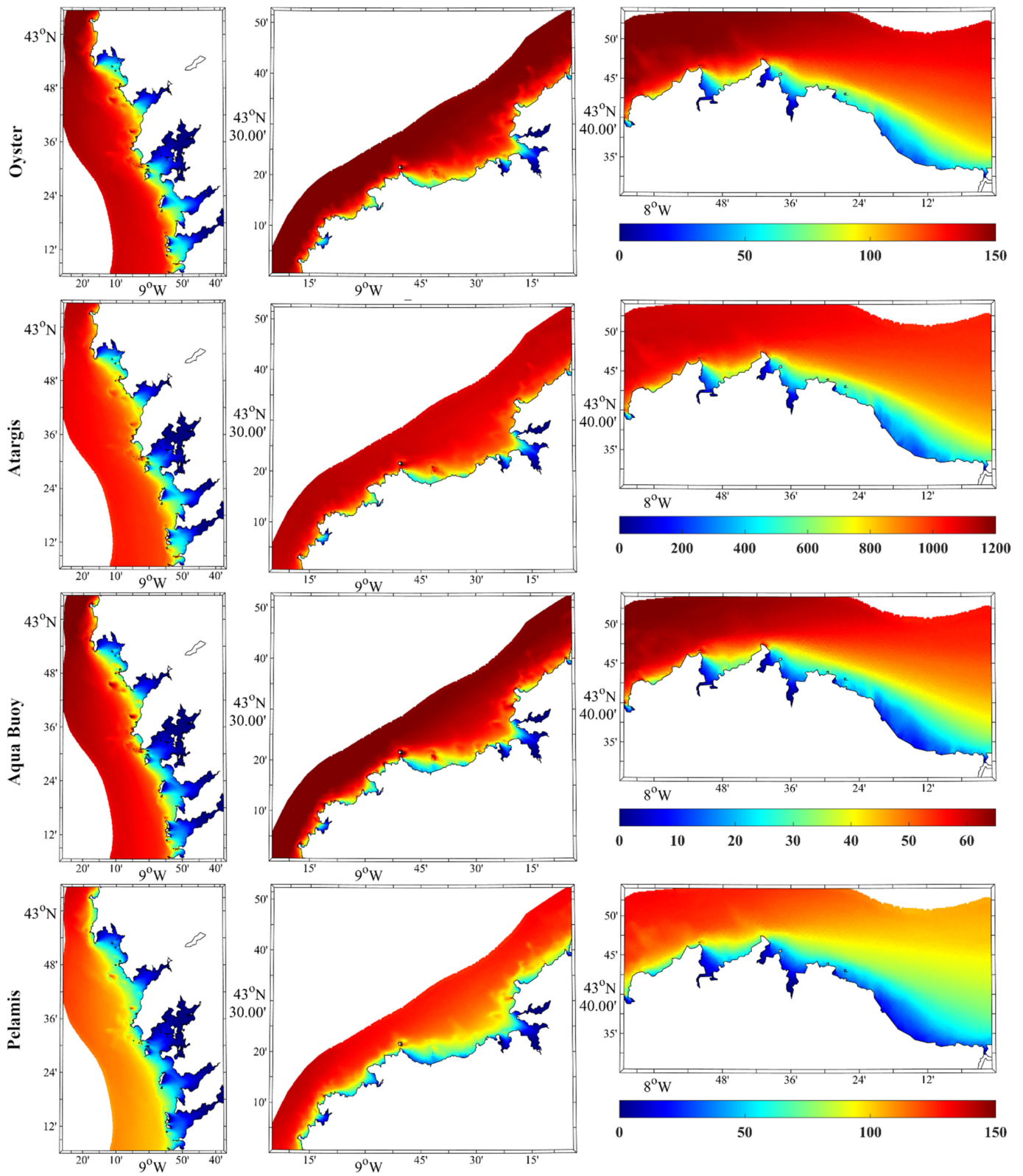


Figure 4. Electric power capacity (P_E , in kW) of the Oyster, Atargis, Aqua Buoy, and Pelamis devices for the West Coast (left column), the Northwest Coast (middle column), and the North Coast (right column) for the period (2014–2021).

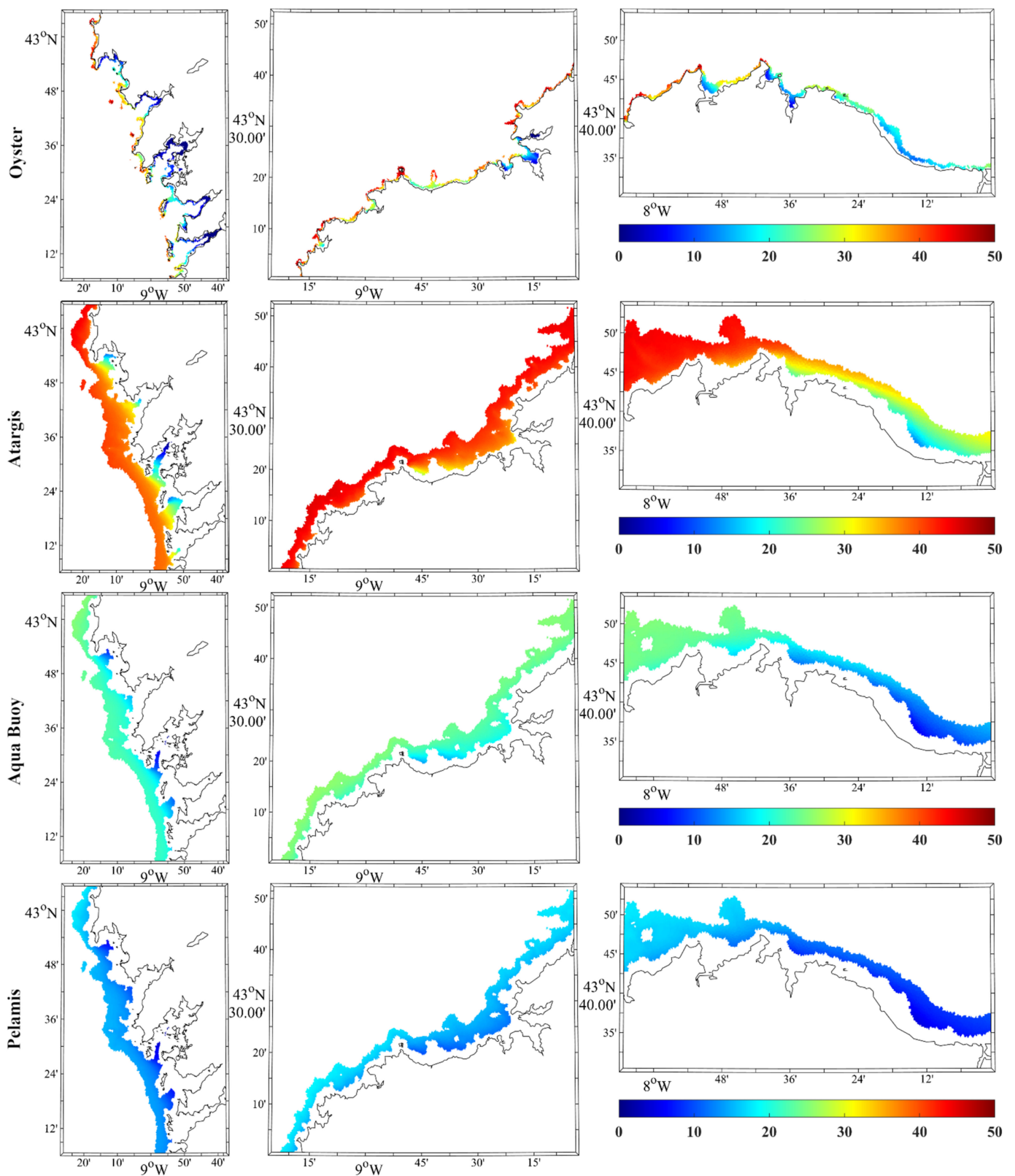


Figure 5. Power load factor (ϵ , in %) of the Oyster, Atargis, Aqua Buoy, and Pelamis devices for the West Coast (left column), the Northwest Coast (middle column), and the North Coast (right column) for the period (2014–2021).

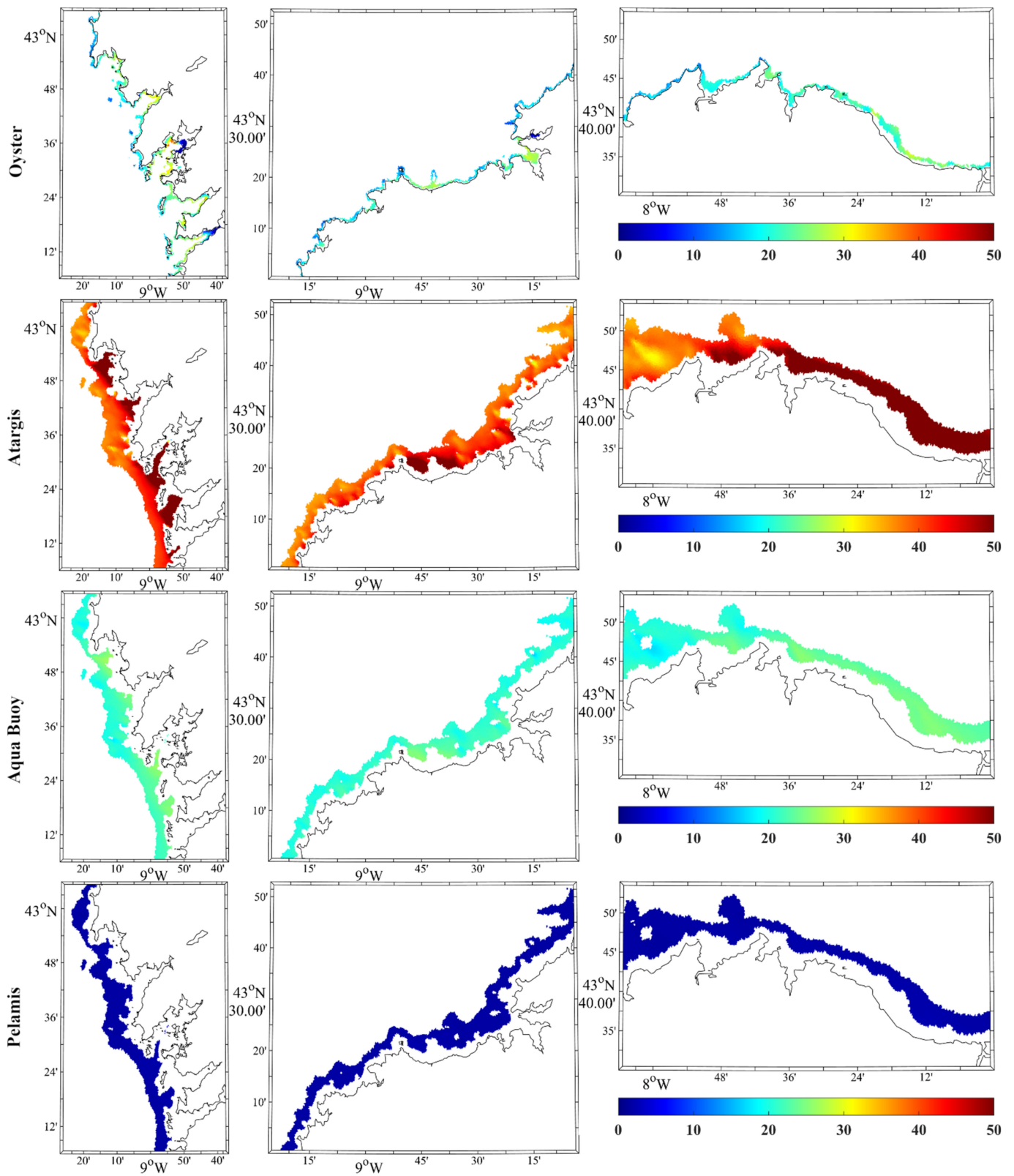


Figure 6. Efficiency (in %) of the Oyster, Atargis, Aqua Buoy, and Pelamis devices for the West Coast (left column), the Northwest (middle column), and the North Coast (right column) for the period (2014–2021).

4. Discussion

Although the implementation of renewable energies is a key factor in mitigating climate change, not all of them have reached the same level of maturity. Wave energy is an auspicious renewable energy due to its high stability, predictability, and power density. However, it has found many difficulties such as the lack of consensus between the best technology, the conflict with other socio-economic activities, and the high cost [11]. These uncertainties have delayed the development of this marine renewable energy. However, technological advances are expected to allow the installation of wave energy farms in the upcoming decades. As shown in this analysis, the use of high spatial resolution simulations containing wave data is crucial to discover the coastal areas with the best conditions for the future installation of wave energy farms. In addition, this approach is also helpful to know the WEC that best fits each area because it is possible to analyze its efficiency only in the depth range that can be installed. As a whole, this study highlights the great potential that Galicia has to become a wave energy-generating region.

Overall, the results have shown that the highest wave resource is found in the northernmost part of the West Coast, the Northwest Coast, and the westernmost part of the North Coast. This is mainly due to the fact that the swell has a north-western direction [34], and these areas are more exposed to waves, as previously pointed out in [30]. In the same way, the least WP resource is found in the easternmost part of the North Coast. This difference in values is possible because the swell is shielded by the northernmost part of Galicia. The spatial distribution of the WP resource and its values are very similar to those shown in [7,30,34] for other different periods.

The WECs use only part of the WP resource available to produce electricity. The electrical energy capable of producing the WEC depends on the power matrix and the probability of occurrence of the sea states. Looking at the power matrix for the four converters in [33], it is to be expected that the device capable of producing the highest electrical energy is Atargis since the elements in the power matrix are the highest. Pelamis has a high power output, especially for high waves (>6 m), while Aqua Buoy and Oyster have the smallest power elements. However, the probability of occurrence of a sea state (H_s , T_p) has to be also taken into account to estimate the P_E . Results have shown that the device capable of producing the most electricity in the three studied regions is undoubtedly Atargis. Oyster also gives high P_E values, especially along the Northwest Coast region (Figure 4). Installing Aqua Buoy seems not to be a good idea in terms of energy production because the lowest P_E has been obtained for that converter. The Pelamis device has not provided as much electrical power as expected when looking at the power matrix. This is because not as many optimal sea states have occurred for this converter. The P_E pattern observed in all WECs is very similar to the wave resource. As the P_E decreases towards the coast, it is possible to think that it is better to install wave energy farms away from the coast. However, installing offshore farms entails an increase in installation and maintenance costs, so a balance must be found between high energy production and proximity to the coast. The installation of a farm of Atargis devices seems to be the best option due to their P_E and the recommended depth. The Northwest Coast is likely to be the most suitable region for that installation.

The power load factor (ϵ) provides an approximation of how much the device is being availed because it compares the electrical energy obtained with the maximum energy it can produce. Atargis is the converter that showed the highest ϵ values in the study regions, followed by Oyster. Although Oyster and Pelamis had similar P_E , Pelamis shows the lowest ϵ due to the higher maximum electric power value (P_{max}).

The other parameter to estimate the performance of a WEC is efficiency. The efficiency represents the performance in harvesting the WP resource taking into account the dimensions of the WEC. The results have shown that the efficiency increases towards the coast. One possible explanation is that the WP resource is much larger than the observed offshore P_E because P_E depends on the WEC limitations and does not consider the most energetic wave states, whereas WP resource does. The similarity between the P_E and the WP resource

is also observable onshore. Regarding efficiency, Atargis has shown the best results in the study regions although Oyster and Aqua Buoy are acceptable. Size is another aspect to consider, especially in areas with insufficient space available for a large device such as Atargis. The installation of several Aqua Buoys can be considered in these areas to increase energy production. Pelamis is the least efficient device in WP resource harvesting because of its dimensions, being much larger than Oyster (Table 2), although both show similar P_E . The high efficiency of Atargis is explained due to its small dimensions and large P_E .

Environmental and human factors must also be considered to choose the best device and installation area. Although the analysis of legal concerns is out of the scope of the present analysis, it is important to mention that Galicia has a large number of ports distributed throughout the coast [55] and places with environmental and fishing interest, such as the Atlantic Islands National Park of Galicia and the Os Miñarzos marine reserve in the Rías Baixas [56,57] or the Costa da Morte Bird Protection Zone (ZEPA in Spanish) in the Northwest Coast [56]. In fact, it can be observed that practically the entire Galician coast is bathed in Natural and National Parks, Sites of Community Importance (LIC, in Spanish), marine reserves of fishing interest, and ZEPAs and RAMSAR wetlands [56,58,59]. Fortunately, WECs are barely above the sea level [21], so they do not have to negatively influence the flight paths of birds.

Aqua Buoy and Pelamis have the advantage that they can be installed far from other important socio-economic activities and environmental places—usually located near the coast. However, the installation far from the coast can lead to inflate the installation and maintenance costs. Instead, its installation can be considered to attract offshore blue economy business. The installation of Oyster could be complicated because the most suited areas are coastal waters, where most of the environmental interest sites are located. Possible locations would be near artificial structures, e.g., ports where visual impact and conflict with other activities are less significant. A possible site could be near the Outer Port of A Coruña at Punta Langosteira. Installation near harbors can reduce maintenance costs [30]. Atargis has the advantage that it can be located somewhat further from the coast, avoiding conflict with protected areas. In addition, Atargis is installed under the surface, nullifying the visual impact. For this, Atargis seems to be the better option for implementing wave energy on the Galician coast. However, its size makes it difficult to install within the estuaries where the Aqua Buoy device appears to be one of the most efficient due to its small size. The Atargis impact on the seabed could also be studied in the future.

5. Conclusions

This study analyzed the wave energy resource in three regions of the Galician coast over the period 2014–2021 and the expected electrical energy output from four wave energy converters—Oyster, Atargis, Aqua Buoy, and Pelamis. Their performance was also investigated attending to their power load factor and efficiency. To fulfil this task, high-resolution significant wave height and peak period data were obtained from simulations of the third-generation SWAN model. These data were validated with the measurements of a buoy located on the Northwest Coast, obtaining a high overlapping percentage. The main findings of this study can be summarized as follows:

- The wave power resource, the expected electrical energy output, and the power load factor decrease landward, while the efficiency increases landward.
- The highest wave power resource is found in the northernmost part of the West Coast, the Northwest Coast, and the westernmost part of the North Coast.
- Atargis is the device that shows the highest expected electrical energy output, followed by Oyster. Aqua Buoy is the device with the lowest electrical energy output.
- Attending to the power load factor, Atargis is the best-availed device, followed by Oyster. Pelamis has obtained the lowest performance in the three regions.
- The parameter efficiency could substitute capture width in future studies in order to estimate the WEC performance because it allows making comparisons between different WECs regarding their dimensions.

- Looking at the efficiency, Atargis is definitely the most efficient device, while Oyster and Aqua Buoy are quite efficient in harvesting the wave power resource in the three regions. Pelamis has shown a low efficiency in the whole area.
- Atargis seems to be the best device to be installed in the Galician coast—especially in the Northwest Coast region—due to its expected electrical output, performance, its location under the surface, and optimum depth, avoiding areas of environmental interest.

The present study showed the Galicia's great potential to become a wave energy-generating region. Regarding the parameters considered to determine the performance of the different types of WECs, and taking into account the size and location of WECs, Atargis is the most suitable to be installed in the Artabro Gulf, where it shows high values of P_E , load capacity factor, and efficiency. In addition, it can be located somewhat further from the coast than the others, avoiding conflicts with protected areas. The Aqua Buoy is shown to be the most suitable to be installed within estuaries, where the available space is limited and must coexist with other economic activities, such as raft aquaculture, restricting the installation of large devices such as Atargis or Oyster. The Aqua Buoy has high efficiency due to its small size, and the power output can be increased by considering various devices. The installation of these devices in the vicinity of shellfishing areas could also protect them from waves by dissipating part of their energy. The appropriate locations for the Oyster device, which shows high efficiency and capacity factor for the entire area, are in the vicinity of harbors such as the Outer Port of A Coruña to reduce costs and avoid conflicts with protected and shellfishing areas. Finally, it should be mentioned that future studies should estimate the economic profitability of the devices to fulfil a more comprehensive assessment of their economic viability of the wave power in the study areas.

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