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# Unit-cell for dual-circular polarisation reflectarrays

S. Mener<sup>1</sup>, R. Gillard<sup>1</sup>, R. Sauleau<sup>2</sup>, A. Bellion<sup>3</sup>, P. Potier<sup>4</sup>

<sup>1</sup>: European University of Brittany, INSA, IETR, UMR CNRS 6164, 35708 Rennes, simon.mener@insa-rennes.fr, raphael.gillard@insa-rennes.fr

<sup>2</sup>: University of Rennes 1, IETR, UMR CNRS 6164, 35042 Rennes, ronan.sauleau@univ-rennes1.fr

<sup>3</sup>: CNES, 31401, Toulouse CEDEX 9, France, Anthony.Bellion@cnes.fr

<sup>4</sup>: DGA Maîtrise de l'information, BP 57419, 35174, Bruz CEDEX, France, patrick.potier@dga.defense.gouv.fr

**Abstract**—A new unit-cell composed of two layers for dual-CP reflectarrays is proposed for the first time with the unique capability to reflect independently and simultaneously the two incident circular polarisations at the same frequency. The experimental results demonstrate that this unit-cell exhibits a 3.8% bandwidth around 8.4 GHz for a phase resolution better than 1.92 bits in LHCP and in RHCP. As a first step towards a reflectarray in dual-CP, this innovative unit-cell is studied in an array configuration. To increase the value of the maximum incidence angle up to 30°, a matching dielectric layer is placed over the cell.

**Index Terms**—reflectarray, dual-circular polarisation, circular polarisation selective surface, unit-cell

## I. INTRODUCTION

Reconfigurable reflectarrays are very attractive for beam scanning or beam-shaping in space applications such as Earth observations and satellite communications. In order to achieve higher data rate transmissions and prevent from losses due to polarisation misalignment, circular polarisation (CP) is usually preferred. Several circularly-polarised reflectarray unit-cells in frozen states have been proposed in the literature [1], [2], but they only operate with one single CP wave. To our best knowledge, dual-CP unit-cells with independent control of the reflected phases in both polarisations at the same frequency have never been reported so far.

A unit-cell based on a circular polarisation selective surface (CPSS) has been described in [3]-[5] as an attractive building block for dual-CP reconfigurable reflectarrays (Fig. 1a). The proposed unit-cell is made of two layers. The first layer (layer 1 in Fig. 1) is described in detail in [3] and is a Left-Hand CPSS (LH-CPSS) reflecting the incident LHCP with a controllable reflection phase; the incident RHCP is transmitted to the second layer (layer 2 in Fig. 1) that reflects it with an independent controllable reflection phase shift. As layer 2 operates in single polarisation, it only requires standard CP unit-cells (e.g. [6]).

The LH-CPSS has been validated experimentally in [3] and is derived from the Pierrot's cell [7]. This unit-cell provides a high isolation (20dB at 8.5 GHz) between the two incident circular polarisations and almost a 2-bit phase resolution [3]-[5].

Here, we firstly focus our attention on the whole unit-cell. A convenient co-design of both layers and an optimisation of

the distance  $d$  (Fig. 1b) separating them has thus been carried out to obtain simultaneously i) a good isolation between both polarisations, and ii) a 2-bit phase resolution in LHCP and RHCP. Secondly, in Section III, this whole unit-cell is studied in an array configuration to estimate the maximum acceptable incidence angle.

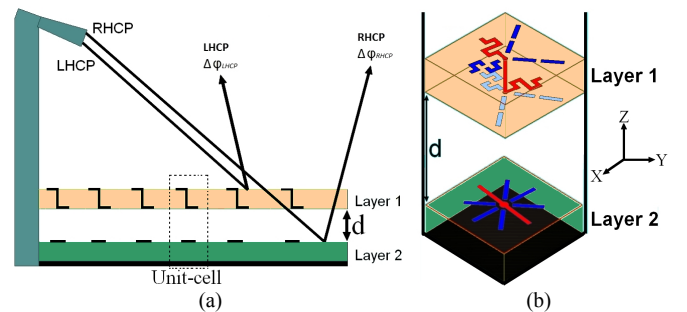


Fig. 1. (a) Schematic representation of a future reflectarray with independent control of both incident circular polarisations. (b) Unit-cell with dual circular polarisation control.

## II. DUAL-CIRCULARLY POLARISED UNIT-CELL

### A. Experimental validation of the second layer

As illustrated in Fig. 1, the second layer reflects the incident RHCP wave transmitted through the first layer (LH-CPSS). It is well known that, for an incident CP wave, the reflected phase can be tuned by varying the angular rotation of the reflecting element [8].

This principle has been implemented here around 8.5 GHz: 4 dipoles (Fig. 2) with an appropriate angle of rotation have been defined to reflect the RHCP incident wave with a nearly 2-bit phase resolution. As shown in Fig. 2, each configuration consists of one continuous dipole (in red in Fig. 2) and three non-connected dipoles (in blue in Fig. 2). Each continuous dipole is optimised to reflect totally the parallel component of the incident field while the orthogonal component is reflected by the ground plane. Fig. 2 represents the optimal geometry for the four states of the optimised cell. The main parameters to achieve the optimal geometry are  $h$ ,  $W$  and  $L$ . The four corresponding values of the rotation angles are the following:  $-45^\circ$  for State 2 ( $90^\circ$  phase shift),  $-90^\circ$  for State 3 ( $180^\circ$  phase shift), and  $-135^\circ$  for State 4 ( $270^\circ$  phase shift). Four breadboards, one per phase state, have been manufactured. The experimental results (not shown)

demonstrate that the RHCP incident wave is correctly reflected with insertion loss lower than 1 dB over the [8.2-8.8 GHz] range. Moreover, four 90°-spaced phase states are obtained with the same frequency dispersion.

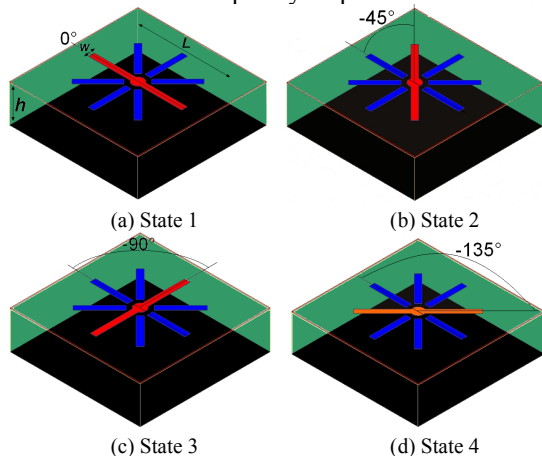


Fig. 2. Optimised states of the second layer of the unit-cell.  $L=16.6\text{mm}$ ,  $w=1\text{mm}$ ,  $h=6.5\text{mm}$ .

### B. Experimental results of the dual circularly polarised unit-cell

Layers 1 and 2 have been studied separately in [1] and in Section II.A respectively. They are now combined to form a complete unit-cell for dual-CP reflectarray applications. The sixteen possible configurations and the expected LHCP and RHCP reflected phases are summarized in Table I.

TABLE I

CHARACTERISTICS OF THE 16 CONFIGURATIONS OF THE WHOLE UNIT-CELL

Configuration	Layer 1 (LH-CPSS) in state $i$ ( $1 < i < 4$ )	Layer 2 (dipole) in state $j$ ( $1 < j < 4$ )	Expected LHCP reflected phase at resonance	Expected RHCP reflected phase at resonance
1	State 1	State 1	0°	0°
2	State 1	State 2	0°	90°
3	State 1	State 3	0°	180°
4	State 1	State 4	0°	270°
5	State 2	State 1	90°	0°
6	State 2	State 2	90°	90°
7	State 2	State 3	90°	180°
8	State 2	State 4	90°	270°
9	State 3	State 1	180°	0°
10	State 3	State 2	180°	90°
11	State 3	State 3	180°	180°
12	State 3	State 4	180°	270°
13	State 4	State 1	270°	0°
14	State 4	State 2	270°	90°
15	State 4	State 3	270°	180°
16	State 4	State 4	270°	270°

From [3], it can be seen that polarisation isolation of the LH-CPSS cell, although very good, is not perfect: approximately 3% of the power is not properly handled (the isolation coefficients  $\Gamma_{R-L}$ ,  $\Gamma_{L-R}$ ,  $T_{R-L}$  are around 15 dB at 8.5 GHz). As a result, parasitic uncontrolled waves with inappropriate polarisation may arise, thus disturbing the ideal operation described in Fig. 1. Fig. 3 represents the bandwidth of the whole unit-cell for several values of  $d$  which is the more prominent degree of freedom to minimize undesirable wave recombination. The optimal distance  $d$  is 20mm. Fig. 4

shows a 3D view of the fabricated prototype in configuration 5 (Table I).

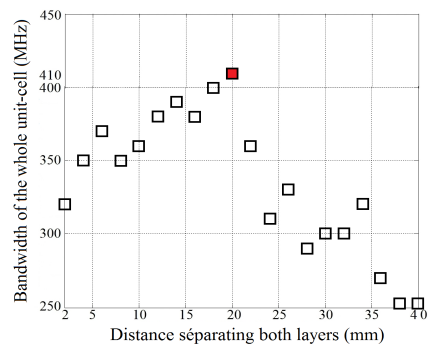


Fig. 3. Bandwidth of the whole unit-cell versus  $d$ .

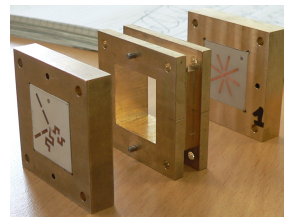


Fig. 4. One of the sixteen configurations of the complete unit-cell (here configuration 5).

The amplitudes of the measured reflection coefficients for the sixteen configurations are represented in LHCP and RHCP in Figs. 5a and 5b, respectively.

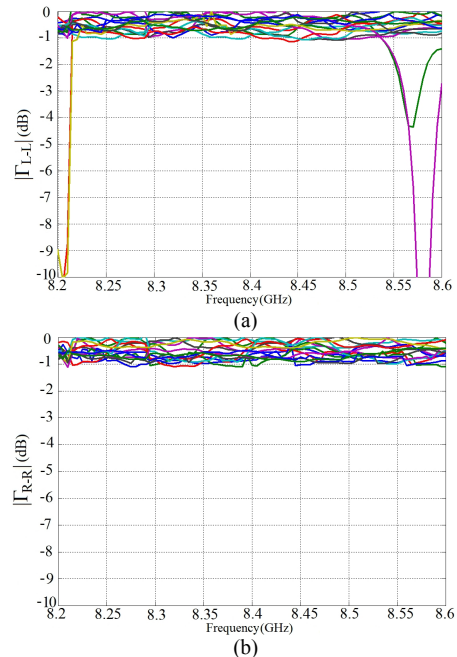


Fig. 5. Measured magnitude of the reflection coefficients for the 16 configurations of the complete unit-cell. (a) LHCP. (b) RHCP.

The complete unit-cell exhibits very attractive performances, with a 3.8% fractional bandwidth for insertion loss lower than 1dB in both polarisations. Fig. 6 represents the measured reflected phase for the 16 configurations of the

complete unit-cell, in LHCP (Fig. 6a) and in RHCP (Fig. 6b). Four 90°-spaced phase responses are obtained in reflection with almost the same frequency dispersion in LHCP and in RHCP, respectively for the four states of the first and second layers. Moreover, the phase states in one polarisation do not depend on the phase states of the other polarisation. The simulated and measured equivalent bit numbers are better than 1.92 bits over the [8.2-8.55 GHz] range for both incident polarisations.

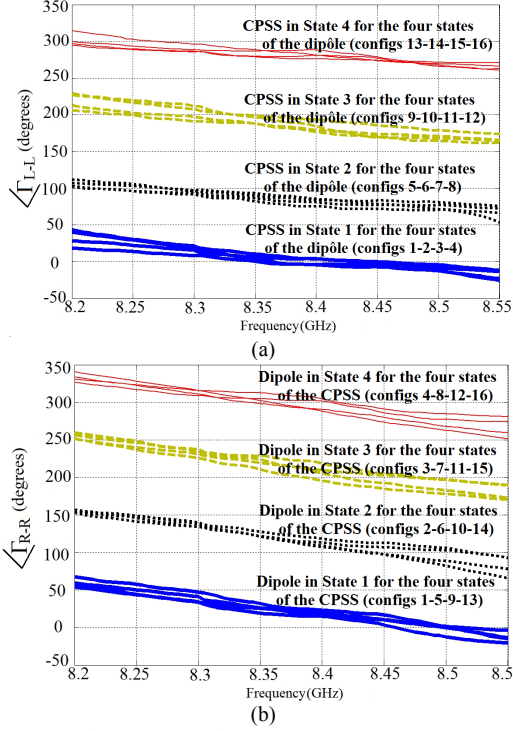


Fig. 6. Measured phase of the reflection coefficients for the 16 configurations of the complete unit-cell. (a) LHCP. (b) RHCP.

### III. STUDY OF THE UNIT-CELL IN A ARRAY CONFIGURATION

In the previous section, the unit-cell was studied in a waveguide simulator. Here the effect of incidence is studied using a more realistic configuration. As represented in Fig. 7, the unit-cell is embedded in a metallic cavity, and a metallic grid extends the cavity above the cell (height  $h_w$ ).

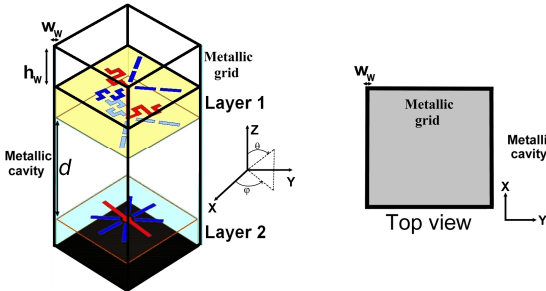


Fig. 7. Schematic representation of the square metallic cavity. The four edges of the cell are PEC walls forming a metallic cavity:  $w_w=0.1$ mm,  $h_w=20$ mm.

It is well known that Pierrot's cell [7] is very sensitive to incidence angle. For our configuration, the dependency to incidence angle is mainly governed by the reflection at the

waveguide mouth. To clarify this, the reflection coefficients for incident TE and TM modes on the mouth of a matched waveguide (same section as the metallic cavity containing our cell) have been computed for various incidence angles  $\theta$  (with  $\varphi=0^\circ$ ). They are represented in Fig. 8. This study demonstrates that the incidence angle should be limited to  $\theta=20^\circ$  (for  $|\Gamma_{TE-TE}|$  and  $|\Gamma_{TM-TM}| < -10$  dB). Note that total reflection at the waveguide mouth (e.g; for  $\theta=30^\circ$  and TM mode at 8.4 GHz, Fig. 8b) is caused by scan blindness, as for infinite phased arrays [9], [10].

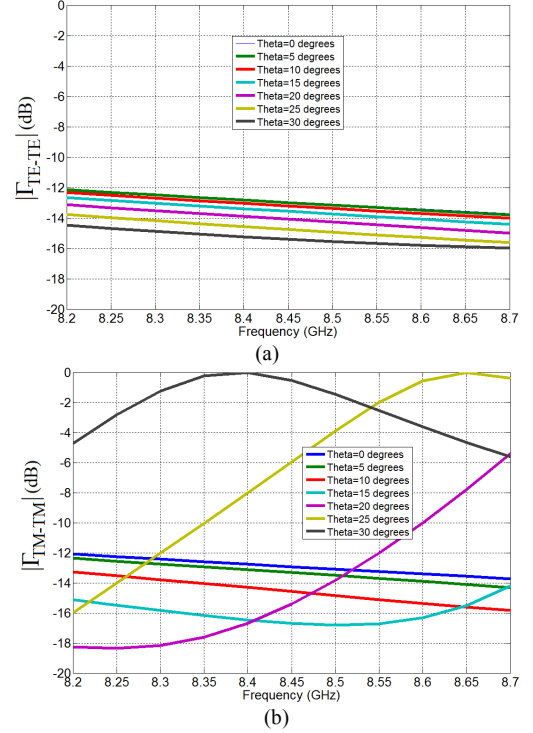


Fig. 8. Simulated reflection coefficient at the waveguide mouth for various incidence angle  $\theta$  (for  $\varphi=0^\circ$ ). (a): TE mode. (b): TM mode.

To shift the blind angle and thus increase the value of the maximum incidence angle, a matching dielectric layer has been placed over the cell so as to modify the surface impedance. Its dielectric permittivity is 1.65 and its thickness is 12mm (6mm above the waveguide interface, and 6mm inside, see Fig. 9). Fig. 10 represents the reflection coefficients for the incident TE and TM modes on the waveguide mouth for various incidence angles  $\theta$  (for  $\varphi=0^\circ$ ).

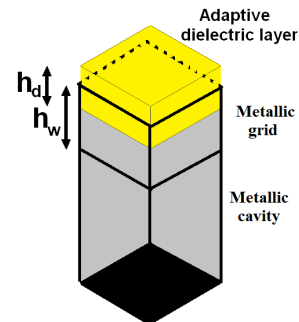


Fig. 9. Schematic representation of the square metallic waveguide with the matching dielectric layer.  $h_w=20$ mm,  $h_d=12$ mm.

This study demonstrates that the incidence angle should be now limited to  $\theta=30^\circ$  (for  $|\Gamma_{TE-TE}|$  and  $|\Gamma_{TM-TM}| < -10$  dB). Thus, the maximum acceptable angle of incidence has been increased by 10 degrees.

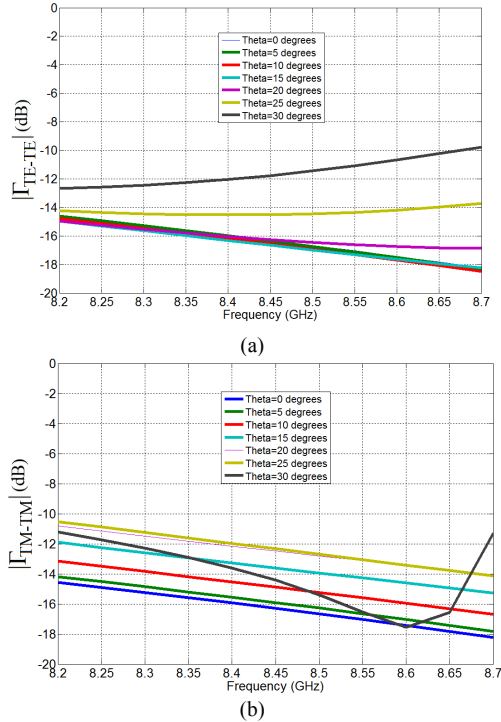


Fig. 10. Simulated reflection coefficients at the waveguide mouth for various incidence angles  $\theta$  (for  $\varphi=0^\circ$ ). (a): TE mode. (b): TM mode.

The performance of the whole unit-cell (including the cavity and its matching layer) has then been simulated for various incidence angles. The LHCP and RHCP incident waves are correctly reflected with loss lower than 1 dB over the full bandwidth, and the reflected phase for all configurations in LHCP and in RHCP are represented in Fig. 11 for the most critical case ( $\theta=30^\circ$  and  $\varphi=0^\circ$ ). This figure shows that, even in a quite critical configuration ( $\theta=30^\circ$  and  $\varphi=0^\circ$ ), the phase difference between two consecutive states is preserved over a large frequency bandwidth. Indeed, four  $90^\circ$ -spaced phase responses are obtained in reflection with almost the same frequency dispersion in LHCP and in RHCP, respectively for the four states of the first and second layers.

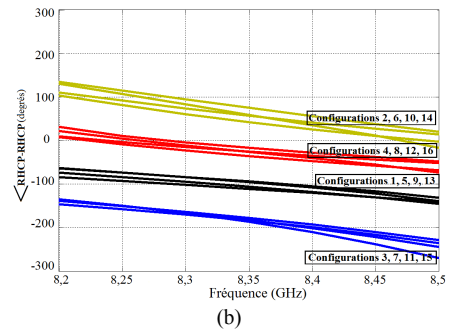
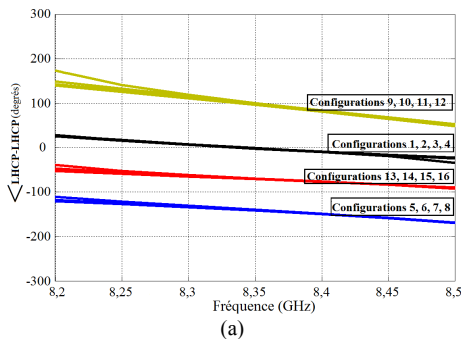


Fig. 11. Simulated phase of the reflection coefficients for all configurations of the complete unit-cell for  $\theta=30^\circ$  and  $\varphi=0^\circ$ . (a) LHCP. (b) RHCP.

#### IV. CONCLUSION

A unit-cell for dual-CP reflectarrays has been proposed for the first time with the unique capability to reflect independently and simultaneously the two incident circular polarisations at the same frequency. The experimental results demonstrate that this unit-cell exhibits a 3.8% bandwidth for a phase resolution better than 1.92 bits in LHCP and in RHCP. Then, as a first step towards a reflectarray in dual-CP, this innovative unit-cell has been studied in an array configuration. To increase the value of the maximum incidence angle up to  $30^\circ$ , a matching dielectric layer has been placed over the cell.

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