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School of Architecture

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Lincoln-Juarez Land Port of Entry Vehicle Processing Facility

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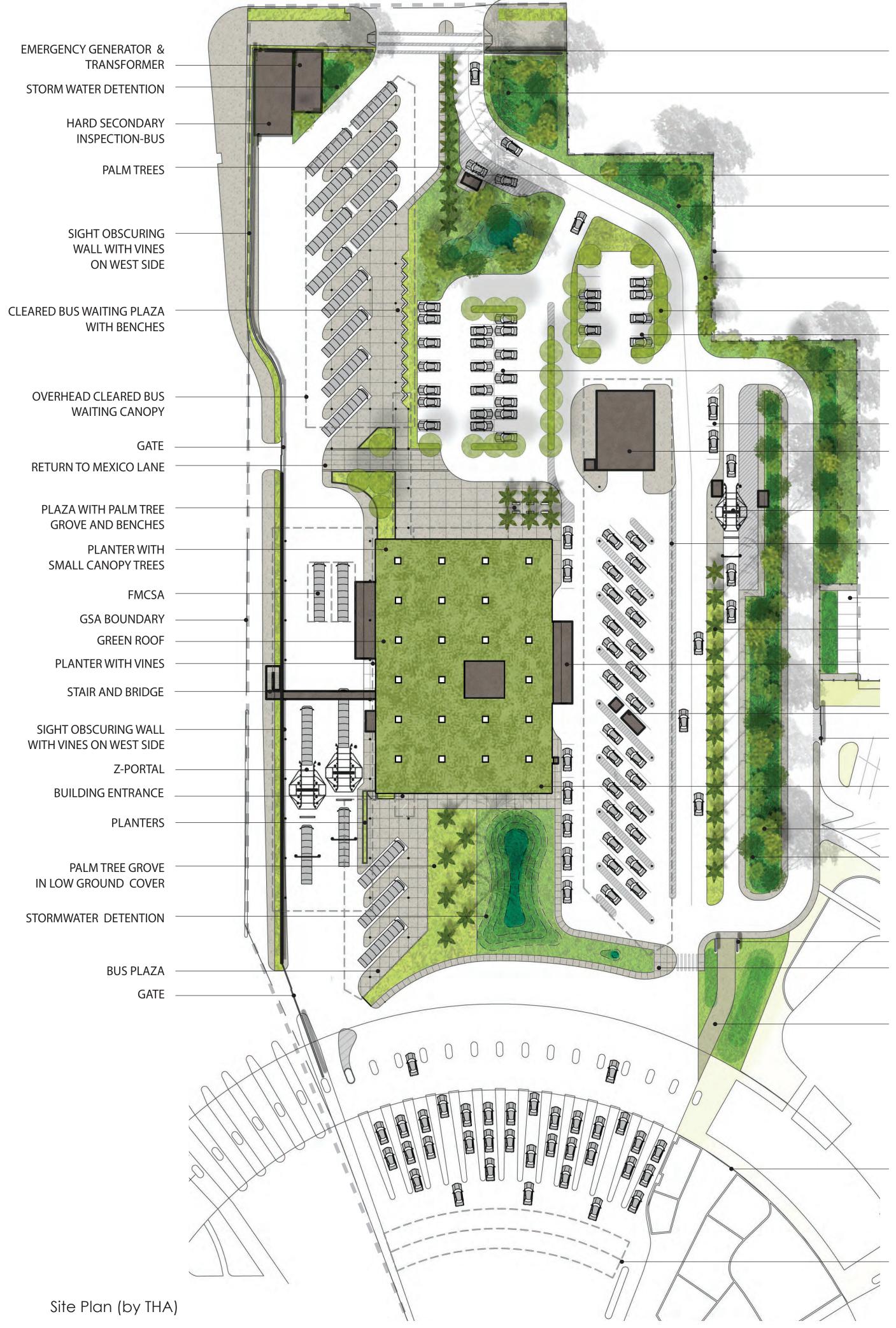
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Authors

Nathan Clifford, Dylan Morgan, Chad Norvell, Chris Kline, Raul Bayoan Cal, Matthew S. Melius, and THA Architecture

HIDALGO STREET



WALL WITH VINES ON NORTH SIDE

STORM WATER DETENTION

TABC BOOTH

STORM WATER DETENTION

PERIMETER FENCE

NATIVE OAK TREES

OVERHEAD CANOPY TREES **GOV PARKING**

REFERRAL PARKING

PURSUIT VEHICLES

HARD SECONDARY **INSPECTION-BUS**

Z-PORTAL

OVERHEAD SECONDARY **INSPECTION CANOPY**

SENTRI PARKING

PALM TREES

SALLY PORT

SUPER BOOTH

GATE

COMMAND CENTER

NATIVE OAK TREES STORM WATER DETENTION

RPM CONTROL POINT

RPM ALERT PULL OUT

EXISTING CANOPY

PRE-PRIMARY CANOPY

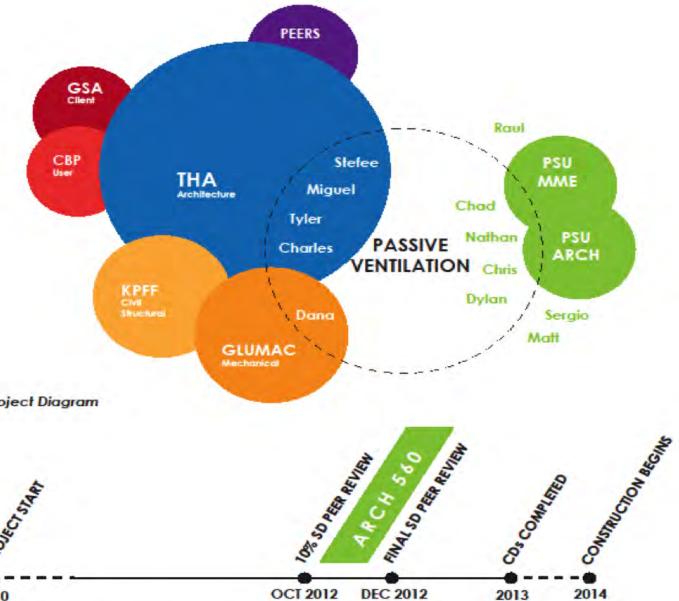


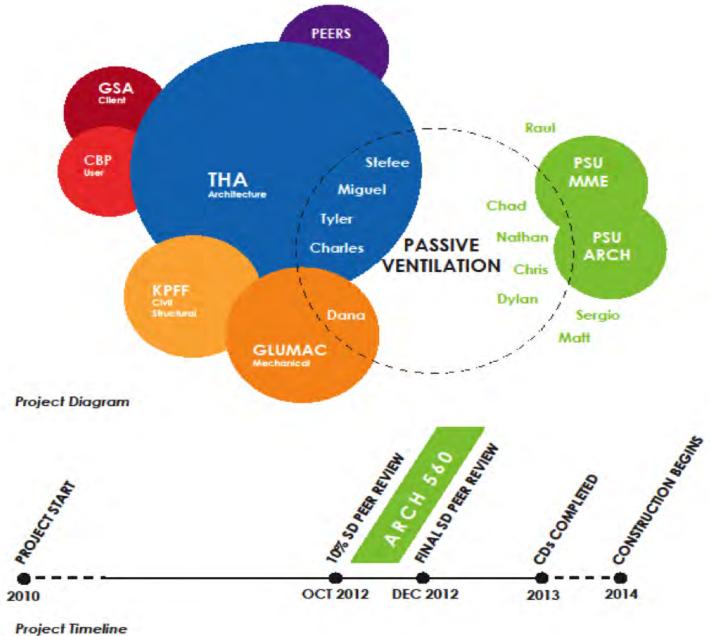


SITE OVERVIEW

The Lincoln-Juarez Land Port of Entry (LPOE) in Laredo is a unique and complex operation. Today, this port is one of the busiest in the nation. It is one of the few surrounded by an urban context, adjacent to a historic downtown commercial center and a historic barrio. The Lincoln-Juarez LPOE was built in 1976. Since then, the operations of the Port and the organizations that operate it have changed significantly.







Lincoln-Juarez Land Port of Entry Vehicle Processing Facility

Aerial View and Perspectives (by THA)



PROJECT OVERVIEW

The indoor environmental quality of a building has a significant impact on occupant health, comfort, and productivity. Exposure to the exhaust fumes of idling vehicles is a dangerous but avoidable toxic hazard. Proper ventilation of vehicle inspection areas is essential, and to the maximum possible means, should be accomplished by natural ventilation. We intend to research the extent to which it is possible to use passive ventilation strategies to alleviate the auto exhaust exposure of officers and travelers using the Port of Laredo entry.



THA Architecture

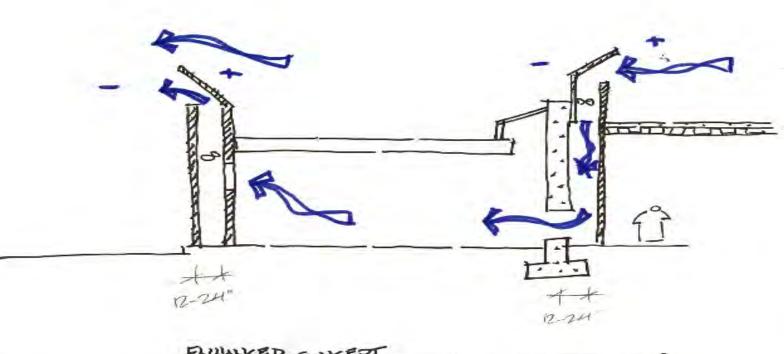
Thomas Hacker Charles Dorn Stefee Knudson Miguel Hidalgo Amanda Petretti Tyler Nishitani

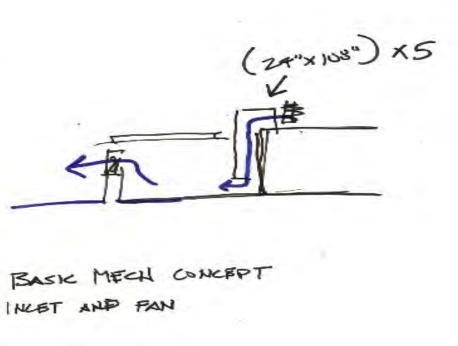
PSU Graduate Students

Nathan Clifford Dylan Morgan Chad Norvell Chris Kline

Collaborators

Raul Bayoan Cal Matt Melius Nicholas



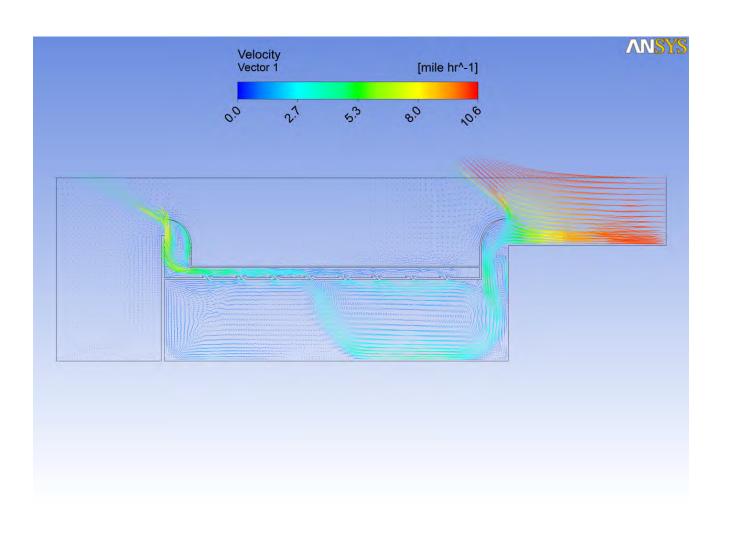


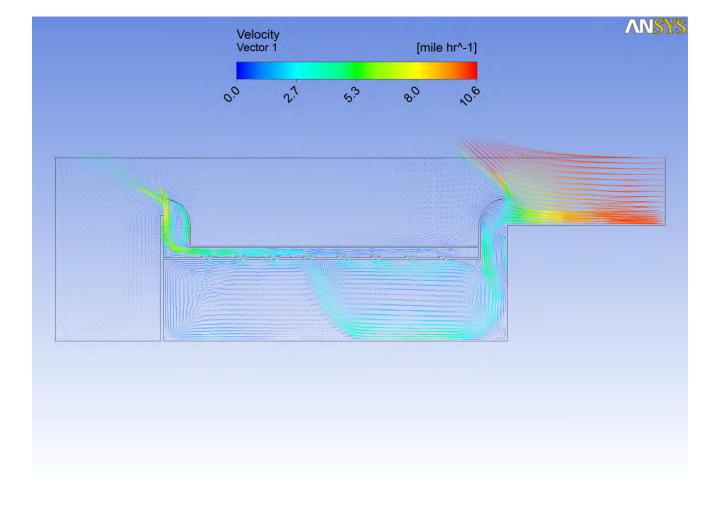
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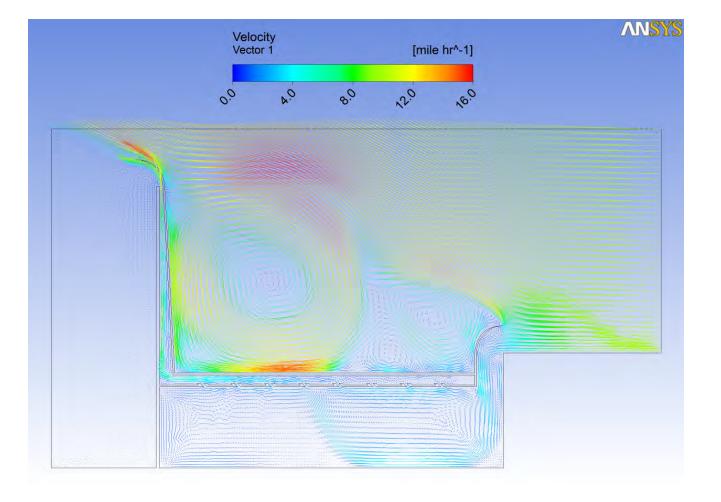
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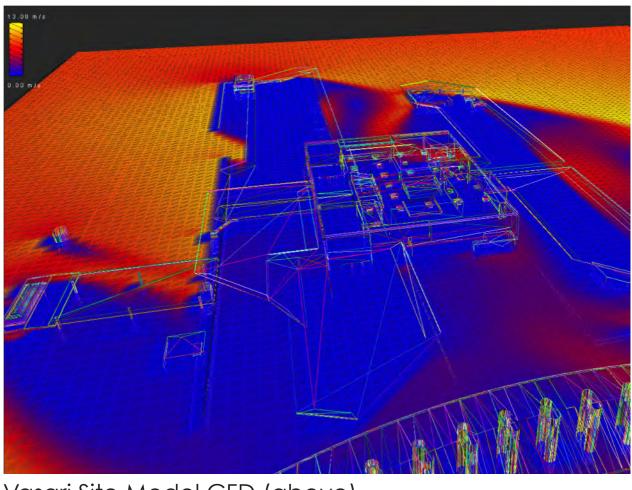
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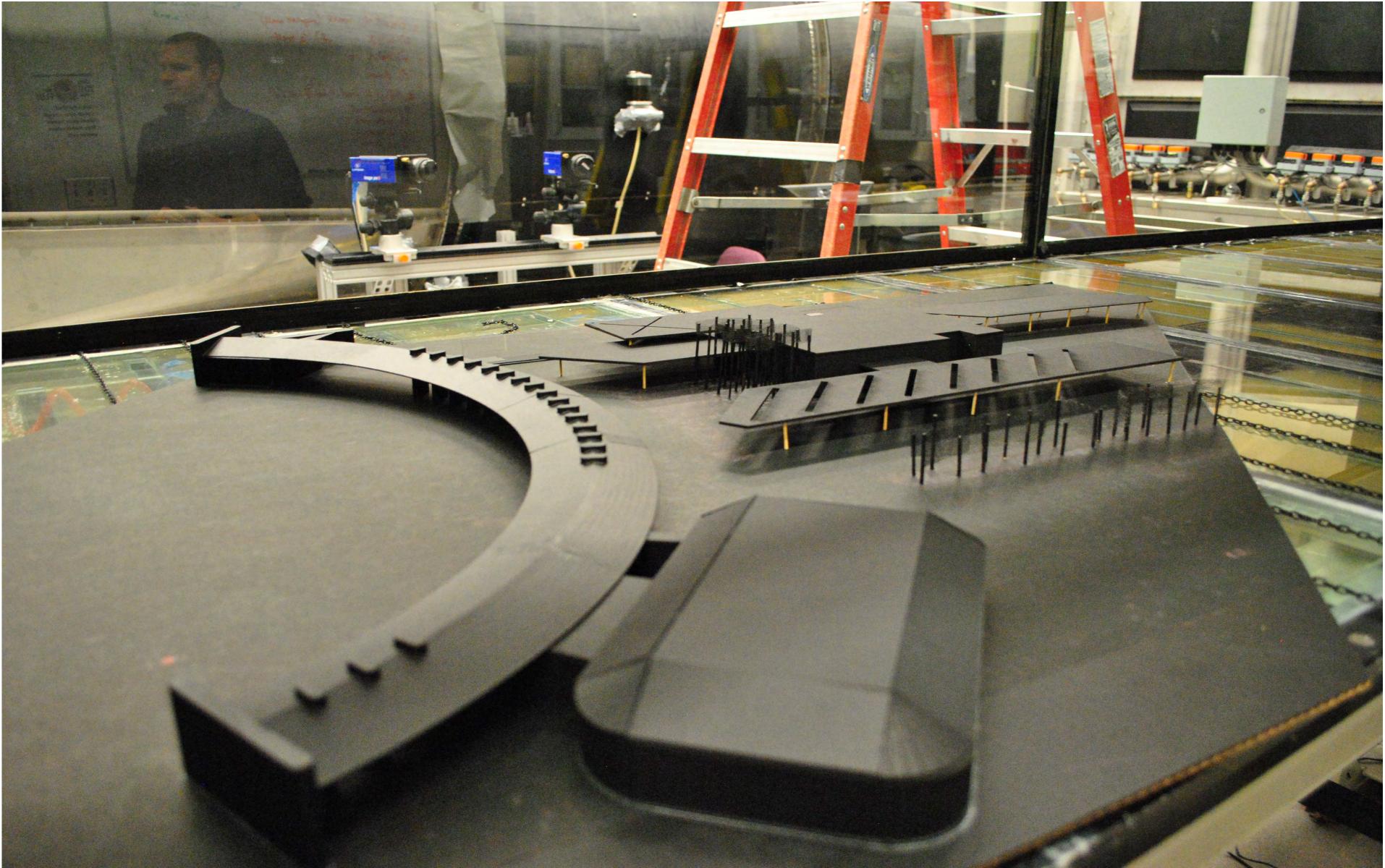


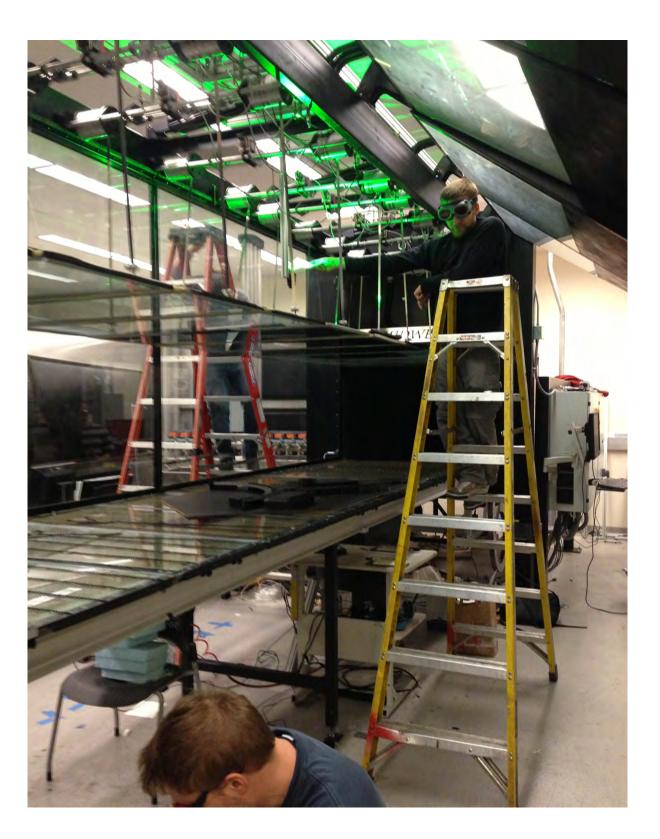
Computational Fluid Dynamics Testing Examining the passive stratigies needed to remove particulate from underneath the canopy and the wind conditions in the Laredo area, we were able to start with a concept sketch and import these sections into Ansys, a CFD modeler. Using these studies we could start to get an idea about what geometries started to give us the vectors that would become the best strategies for the space. These East-West sections looked directly at a 2D set of variables, in which one of our larger scale model is base off of. We were able to look at the whole site and a 3D model using Vasari, but finding more success in the physical wind tunnel testing.

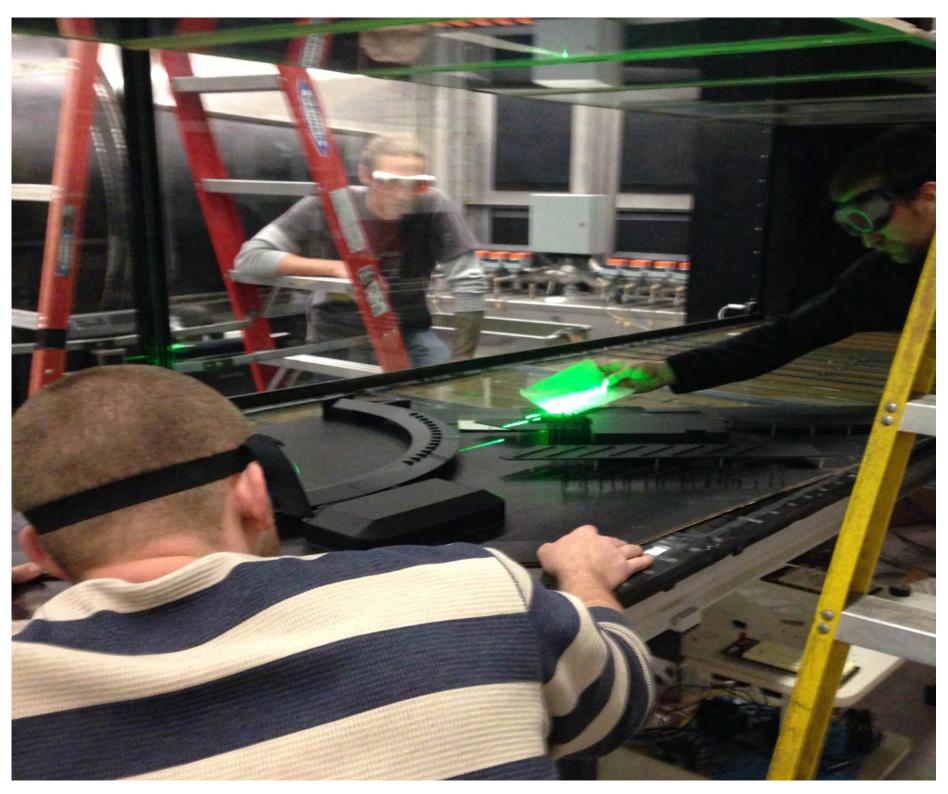


Vasari Site Model CFD (above)









Methodology for Testing Boundry Layer Wind Tunnel & CFD Modeling

Site Model in Wind Tunnel (above)

Boundry Layer Wind Tunnel Building off of our East-West section studies and site modeling, we were able to move forward by creating physical models that could be tested in the Boundary Layer Wind Tunnel in the Engineering Building, headed up by Assistant Professor Raul Bayoan Cal. The wind tunnel uses a laser sheet as a backdrop in the area to be tested, particles travel along the wind passage and are photographed by specific camera equipment. These photographs then are processed through the computer and produce valuable and highly accurate wind data.

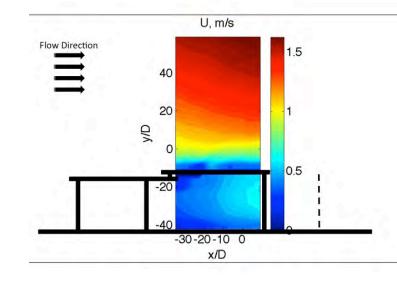
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Overall Model

- Significant increase of velocity close to the exit wall.
- High turbulence intensity above the canopy. • Flow ejected atop canopy.
- Investigation downstream of canopy is required.



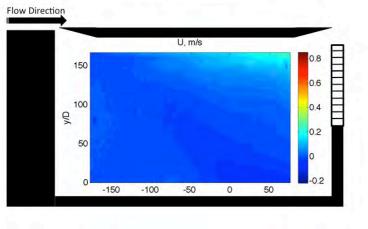
Streamwise Mean Velocity

- Straight wall: Flow not convected outward. Flow passage minimal.
- Strong component of flow in streamwise direction due to single scoop.
- Injections due to the perforations on roof occur although not remediated.

Wall-normal Mean Velocity

• Straight roof: Flow trapped in the enclosure. • Single scoop roof: Strong component of wall-

normal velocity outwards.



Solid Roof Upper-Perforated Wall

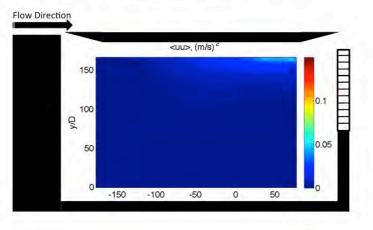




100 -50 0

Solid Roof Upper-Perforated Wall

Solid Roof Upper-Perforated Wall









Streamwise Reynolds normal stress

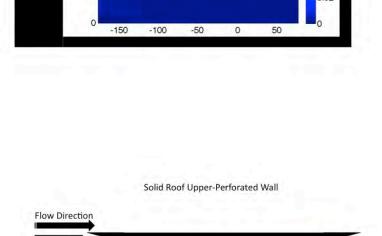
- Straight roof: No turbulence intensity in
- Single scoop roof: strong component of turbulence which will create mixing.
- attenuated while still transporting the flow outwards from the canopy.
- Perforated scoop roof: Not efficient.

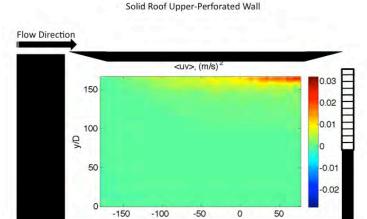
Vertical Reynolds Normal Stress

- Straight roof: No turbulence intensity in canopy due to low flow passage.
- Single Scoop roof: Mixing in center of canopy. Double Scoop roof: Mixing attenuated in the
- vertical direction. Perforated scoop roof: Not efficient.

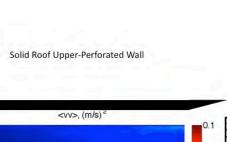
Reynolds Shear Stress

- Straight roof: No turbulence intensity in canopy due to low flow passage.
- Single/Double Scoop roof: Strong shear stress component. Could be non-negligible if buses are stationed in canopy.
- Perforated scoop roof: Not efficient.

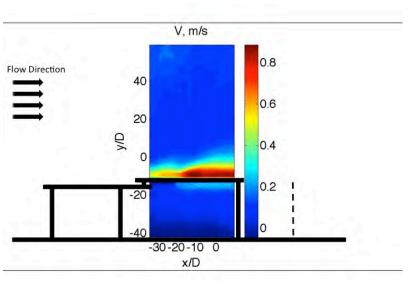


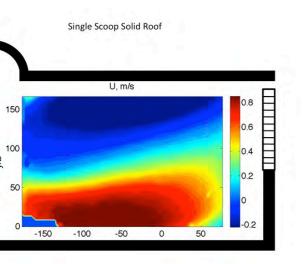


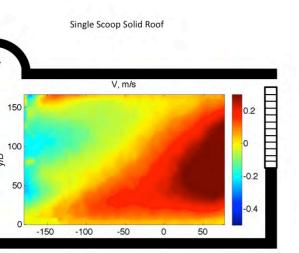
- canopy due to low flow passage.
- Double scoop roof: Mixing could be

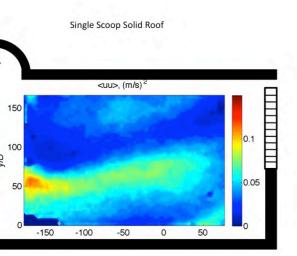


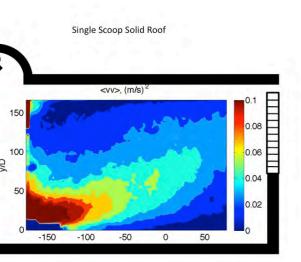


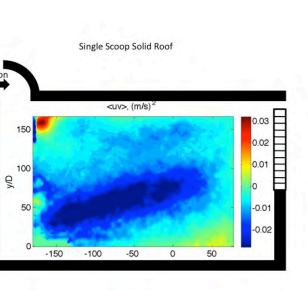


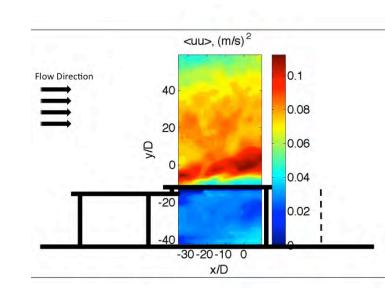


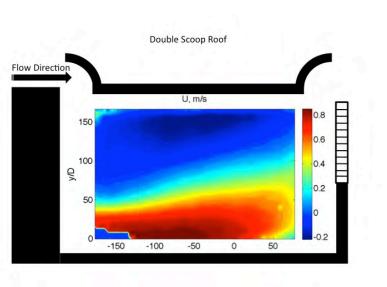


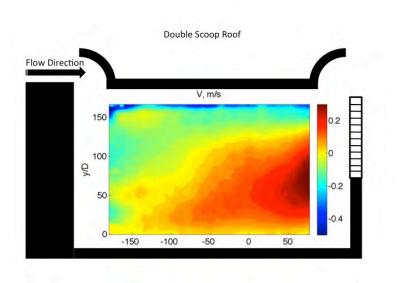


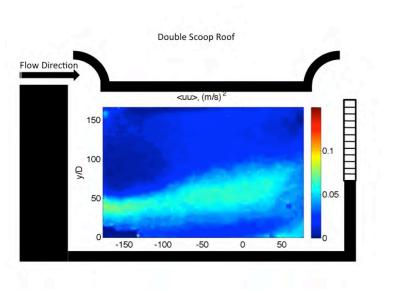


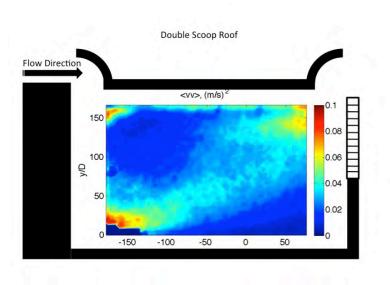


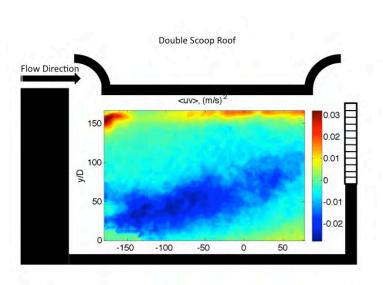


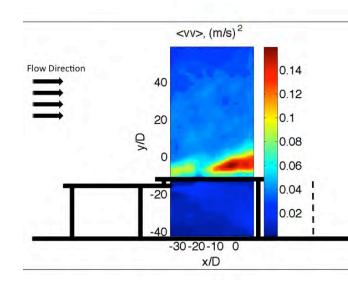


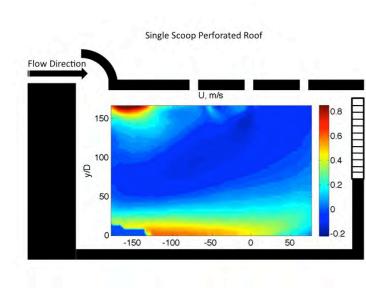


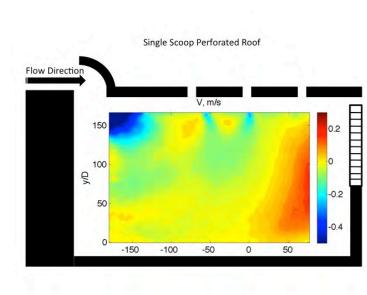


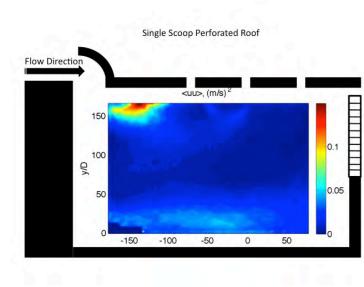


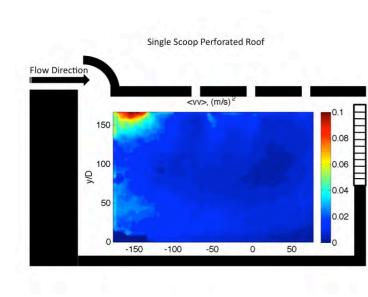


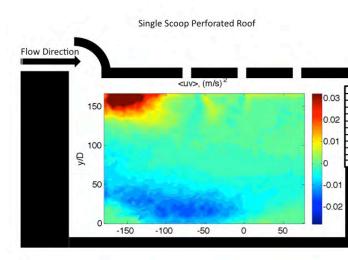




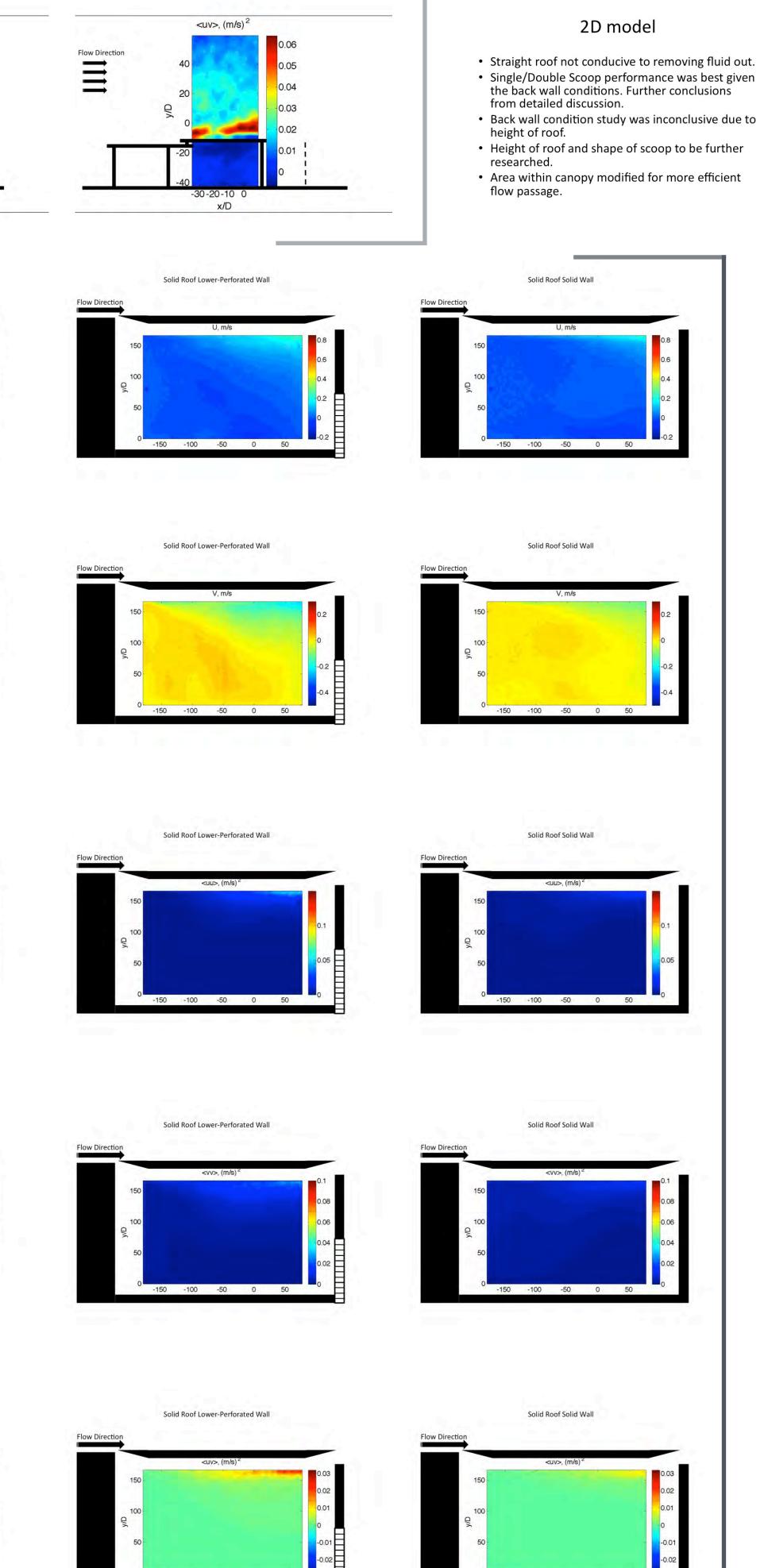








Data Matrix First Results from the Wind Tunnel



-150 -100 -50 0 50

-150 -100 -50 0 50