Computation of the Resonant Frequency of Electrically Thin and Thick Rectangular Microstrip Antennas with the Use of Fuzzy Inference Systems

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ABSTRACT: A new method for calculating the resonant frequency of electrically thin and thick rectangular microstrip antennas, based on the fuzzy inference systems, is presented. The optimum design parameters of the fuzzy inference systems are determined by using the classical, modified, and improved tabu search algorithms. The calculated resonant frequency results are in very good agreement with the experimental results reported elsewhere. © 2000 John Wiley & Sons, Inc. Int J RF and Microwave CAE 10: 108–119, 2000.

Keywords: microstrip antenna; resonant frequency; fuzzy inference systems; tabu search algorithms

I. INTRODUCTION

Accurate determination of the resonant frequency of rectangular microstrip antennas is important in the design of microstrip antennas because they have narrow bandwidths and can only operate effectively in the vicinity of the resonant frequency. Several methods [1–45] are available to determine the resonant frequency of rectangular patch antennas. These methods have different levels of complexity, require vastly different computational efforts, and can generally be divided into two groups: simple analytical methods and rigorous numerical methods. Simple analytical methods can give a good intuitive explanation of antenna radiation properties. Exact mathematical formulations in rigorous methods involve extensive numerical procedures, resulting in round-off errors, and may also need final experimental adjustments to the theoretical results. They are also time consuming and not easily included in a computer-aided design (CAD) package.

Most of the previous theoretical and experimental work has been carried out with only electrically thin rectangular microstrip antennas, normally on the order of $h/\lambda_d \leq 0.02$, where *h* is the thickness of dielectric substrate and λ_d is the wavelength in the substrate. Recent interest has developed in radiators etched on electrically thick substrates. The need for theoretical and experimental studies of microstrip antennas with electrically thick substrates is motivated by several major factors. Among these is the fact that microstrip antennas are currently being considered for use in millimeter-wave systems. The substrates proposed for such applications often have

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high relative dielectric constants and, hence, appear electrically thick. The need for greater bandwidth is another reason for studying thick substrate microstrip antennas. Consequently, this problem, particularly the resonant frequency aspect, has received considerable attention. The theoretical resonant frequency values obtained by using the previous methods are also not in very good agreement with the experimental results of both electrically thin and thick rectangular microstrip antennas. For these reasons, in this work a new method based on fuzzy inference systems (FISs) for calculating the resonant frequency of both electrically thin and thick rectangular microstrip antenna elements has been presented. The improved, modified, and classical tabu search algorithms have been applied to find the design parameters of the FISs.

FISs [46-49] are nonlinear systems capable of inferring complex nonlinear relationships between input and output variables. The nonlinearity property is particularly important when the underlying physical mechanism to be modeled is inherently nonlinear. The system can "learn" the nonlinear mapping by being presented a sequence of input signal and desired response pairs, which are used in conjunction with an optimization algorithm to determine the values of the system parameters. The system produced by the learning algorithm should be able to generalize to certain regions of the multidimensional space where no training data were given. Even if the process to be modeled is nonstationary, the system can be updated to reflect the changing statistics of the process. Unlike conventional stochastic models used to model such processes, FISs do not make any assumptions regarding the structure of the process, nor do they invoke any kind of probabilistic distribution model, i.e., they belong to the general family of model-free, data driven, nonparametric methods. Because of the fascinating features of FISs, many applications can be found in the literature. They include those in automatic control, data classification, decision analysis, expert systems, and computer vision. FISs in this article are used to model the relationship between the parameters of the microstrip antenna and the measured resonant frequency results.

A number of learning algorithms [47–49] used in FISs are available in the literature. These learning algorithms can be used to construct FISs with different properties and characteristics. Some of these algorithms are data intensive, some are aimed at computational simplicity, some are recursive (thus giving the FISs an adaptive nature), some are offline, and some are application specific. In the design of FISs, it is very important to determine the types and parameters of membership functions, and the consequent parameters, necessary to adequately represent a given system. Given an initial set of membership functions, one wants to select the best possible subset of membership functions for an effective representation. The tabu search algorithms used in this paper enable us to obtain the best possible parameters of FIS.

The classical tabu search meta-strategy [50–53] has been shown to be an effective and efficient scheme for combinatorial optimization that combines a hill-climbing search strategy based on a set of elementary moves and heuristics to avoid stops at suboptimal points and the occurrence of cycles. It has been successfully applied to obtain optimal or suboptimal solutions to problems such as scheduling, timetabling, traveling salesperson, and layout optimization. In our previous work [54], we successfully introduced the modified tabu search algorithm (MTSA) to compute the resonant frequencies of triangular microstrip antennas. In [54], first, a model for the effective side length expression of triangular microstrip antenna was chosen, then the unknown coefficient values of the expression were optimized by the MTSA. The number of neighbors of each variable was fixed to the two values, and the tabu restrictions based on recency and frequency memories were used. The disadvantages of the MTSA are that it has a very limited number of candidate solutions at each iteration and is typically slow to converge. Because of these disadvantages, in this study the MTSA is improved.

The resonant frequency of rectangular microstrip antennas is a function of the dimensions of the patch, the permittivity of the substrate, and its thickness. Principally, the resonant frequency is calculated by using a resonant-length transmission line or cavity model, together with equations for the effective dielectric constant and edge extension from the literature. The FIS proposed here requires neither a formula nor the calculation of the effective dielectric constant and the edge extension. The proposed system only requires the dimensions of the patch, the permittivity of the substrate, and its thickness.

The main aims of this paper are:

• to show the applicability of the FIS to the calculation of resonant frequency for elec-

trically thin and thick rectangular microstrip antennas;

- to improve the tabu search algorithms proposed in the literature;
- to determine optimally the design parameters of the FIS by using the classical tabu search algorithm (CTSA) proposed by Glover [50, 51], the MTSA proposed by Karaboga et al. [54], and the tabu search algorithm improved in this work; and
- to compare the performance of the improved tabu search algorithm (ITSA) with the CTSA and the MTSA.

The theoretical resonant frequency results calculated by using the FIS proposed in this paper are in very good agreement with the experimental results [23, 33, 43, 44]. The model is simple and very useful to antenna engineers for predicting accurately the resonant frequencies of both electrically thin and thick rectangular microstrip antennas. The authors [55–60] also proposed simple methods and formulas for calculating accurately the resonant frequencies of circular and triangular microstrip antennas. These methods and formulas are also very useful for engineering applications and CAD.

II. RESONANT FREQUENCY OF RECTANGULAR MICROSTRIP ANTENNA

Consider a rectangular patch of width W and length L, both comparable to $\lambda_d/2$, over a ground plane with a substrate of thickness h and a relative dielectric constant ε_r , as shown in Figure 1. The resonant frequency f_{mn} of the antenna can



Figure 1. Geometry of rectangular microstrip antenna.

be evaluated from

$$f_{mn} = \frac{c}{2(\varepsilon_e)^{1/2}} \left[(m/L_e)^2 + (n/W_e)^2 \right]^{1/2}$$
(1)

where ε_e is the effective relative dielectric constant for the patch, *c* is the velocity of electromagnetic waves in free space, *m* and *n* take integer values, and L_e and W_e are the effective dimensions. To calculate the resonant frequency of a rectangular patch antenna driven at its fundamental TM₁₀ mode, eq. (1) is written as

$$f_{10} = \frac{c}{2(\varepsilon_e)^{1/2} L_e}$$
(2)

The effective length L_e can be defined as follows:

$$L_e = L + 2\Delta L \tag{3}$$

The effects of the nonuniform medium and the fringing fields at each end of the patch are accounted for by the effective relative dielectric constant, ε_e , and the edge extension, ΔL , being the effective length to which the fields fringe at each end of the patch. The following effective dielectric constant expression proposed by Schneider [61] and edge extension expression proposed by Hammerstad [20] can be used in Eqs. (2)–(3)

$$\varepsilon_{e}(W) = \frac{\varepsilon_{r} + 1}{2} + \frac{\varepsilon_{r} - 1}{2\sqrt{1 + 10h/W}}$$
(4)
$$\Delta L = 0.412h \frac{[\varepsilon_{e}(W) + 0.300](W/h + 0.264)}{[\varepsilon_{e}(W) - 0.258](W/h + 0.813)}$$
(5)

The resonant frequency can be also calculated by using the following formula [2]

$$f_{r1} = f_{r0} \frac{\varepsilon_r}{\sqrt{\varepsilon_e(W)\varepsilon_e(L)}} \frac{1}{(1+\Delta)}$$
(6)

$$\Delta = \frac{h}{L} \left[0.882 + \frac{0.164(\varepsilon_r - 1)}{\varepsilon_r^2} + \frac{(\varepsilon_r + 1)}{\varepsilon_r \pi} \right]$$
$$\times \left(0.758 + \ln\left(\frac{L}{h} + 1.88\right) \right),$$

and

$$f_{r0} = \frac{c}{2L\sqrt{\varepsilon_r}} \tag{7}$$

It is clear from eqs. (1)–(7) and all of the formulas proposed in the literature [1–45] that the resonant frequency of a rectangular microstrip antenna is determined by W, L, h, and ε_r .

In this work, the resonant frequency of the rectangular microstrip antennas is calculated by using a new model based on FIS. Only four parameters, W, L, h, and ε_r , are used in calculating the resonant frequency. The new model requires neither a formula given by eqs. (1), (2), and (6) nor the calculations of the edge extension given by eq. (5) and the effective permittivity constant given by eq. (4).

In the following sections, the FISs and the CTSA are described briefly, and the tabu search algorithm improved in this work and the application of FIS to the calculation of the resonant frequency of both electrically thin and thick rectangular microstrip antennas are then explained.

III. FIS

The FIS [47–49] is a popular computing framework based on the concepts of fuzzy set theory, fuzzy if-then rules, and fuzzy reasoning. Basically, a FIS is composed of four functional blocks as shown in Figure 2:

- a) Fuzzification maps the crisp inputs into fuzzy sets, which are subsequently used as inputs to the inference engine. A fuzzy set U is characterized by a membership function (MF) μ: U → {0,1}. The membership functions are labeled by a linguistic term such as "small," "medium," or "large." In the following, the several classes of parameterized functions commonly used to define membership functions are given
 - i) Gaussian MFs

Gaussian(x; a, b, c)
=
$$\exp\left(-\left(\frac{x-a}{c}\right)^{2b}\right)$$
 (8)



Figure 2. Basic fuzzy inference system.

ii) Generalized bell MFs

Bell(x; a, b, c) =
$$\frac{1}{1 + \left|\frac{x-a}{c}\right|^{2b}}$$
 (9)

iii) Trapezoidal MFs

· 1/

$$=\begin{cases} 0, \ x \ge c + \frac{b}{2} + \frac{1}{a} \text{ or } x \le c - \frac{b}{2} - \frac{1}{a} \\ 1, \ x < c + \frac{b}{2} \text{ or } x > c - \frac{b}{2} \\ a\left(c + \frac{b}{2} + \frac{1}{a} - x\right), \ x > c \\ a\left(x - c + \frac{b}{2} + \frac{1}{a}\right), \ x \le c \end{cases}$$
(10)

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The parameterized membership functions given in eqs. (8)–(10) play an important role in the FISs. In order to obtain a desired MF which minimizes the cost function, the parameter set $\{a, b, c\}$ in eqs. (8)–(10) is optimized by using the ITSA, MTSA, and CTSA.

b) **Fuzzy rule base** is a set of fuzzy rules in the form of if-then clauses. For a multi-input single output case, the *t*th rule can be expressed by

$$R^{t}$$
: if x_{1} is A_{1}^{t} and x_{2} is A_{2}^{t} and ...
and x_{n} is A_{n}^{t} then y is B^{t} (11)

where $\mathbf{x} = (x_1, x_2, ..., x_n)$ is the input vector, y is the output variable, and A_i^t and B^t are the labels of membership functions associated to the input variable x_i in the rule t and to the output variable y in the rule t, respectively.

c) Fuzzy inference engine is a decision-making logic which performs the inference operations on the rules and a given condition to derive a reasonable output or conclusion. Three types of FISs [48], the Mamdani fuzzy model, the Sugeno fuzzy model, and the Tsukamoto fuzzy model, have been widely used in various applications. The differences between these three FISs lie in the consequents of their fuzzy rules, and thus their aggregation and defuzzification procedures differ accordingly. In this work, the Sugeno fuzzy model was used. In this model, the *t*th rule can be written as

$$R^t$$
: if x_1 is A_1^t and x_2 is A_2^t and ...
and x_n is A_n^t then y_t is $\xi_{0t} + \xi_{1t} x_1$

$$+ \xi_{2t} x_2 + \ldots + \xi_{nt} x_n$$
 (12)

where ξ_{it} is the consequent parameters of the Sugeno model.

d) **Defuzzification** transforms the fuzzy results of the inference into a crisp output. The most commonly used defuzzification strategy is the centroid of area, which is defined as

output =
$$\frac{\int_{Y} y \mu_B(y) \, dy}{\int_{Y} \mu_B(y)}$$
(13)

where $\mu_B(y)$ is the aggregated output MF. Other defuzzification strategies arise for specific applications, which includes bisector of area, mean of maximum, largest of maximum, and smallest of maximum, and so on. These defuzzification strategies are shown in Figure 3. These strategies are computation intensive, and there is no rigorous way to analyze them except through experimental-based works.

In this work, the optimum design parameters of FIS explained above are determined by using the ITSA, MTSA, and CTSA.

IV. CTSA

The tabu search [50-53] is a meta-heuristic algorithm which uses memory to guide an iterative



Figure 3. Various defuzzification strategies.

- 1) j = 0; initialize s_{now} ; $s_{best} = s_{now}$; tabu $(j) = \emptyset$.
- Construct a list of candidate moves from the neighborhood of s_{now}. Evaluate each candidate move.
- 3) If a move is in tabu(*j*), but leads to a highly desired solution, perform the move, update s_{now} , and go to step 4. Otherwise, select the non-tabu move with the highest evaluation. Perform the move, and update s_{now} .
- 4) If s_{now} is better than s_{best} , update s_{best} .
- 5) If stopping criteria are satisfied, terminate with s_{best} . Otherwise, j = j + 1; update tabu(j); go to step 2.

Figure 4. Main structure of classical tabu search algorithm.

search. At each iteration of the search, a neighborhood is examined to construct new solutions. These solutions are compared against the memory structure (i.e., tabu list) to prevent cycling. The best new solution which is not tabu list is selected and the system moves to that new solution. This process continues until a predetermined termination criterion is reached, e.g., every move is tabu or a maximum number of iterations has been reached. The main structure of the basic tabu search is given in Figure 4. In the figure, s_{now} , s_{best} , j, and tabu(j) represent, respectively, the solution at the current iteration, the best solution found so far, the current iteration counter, and the set of tabu moves at iteration j.

V. ITSA

The CTSA uses a solution vector consisting of a string of bits. Thus, in solving a numerical problem, the transformation from binary to real numbers should be used. This process has two major disadvantages. The first disadvantage is that the process yields a large number of neighbors (e.g., too many evaluations) when the word chosen is very long. The second disadvantage is the difficulty with neighborhood processing. This difficulty is that while a neighbor of the solution vector (e.g., a string of bits) is obtained, the changing of the most significant bit does not produce a number near the present variable. So, this is not reasonable regarding the neighborhood. In order to overcome these difficulties, the MTSA and ITSA have been proposed in our previous work [54] and in this work, respectively.

A real-valued solution vector is used by the ITSA and MTSA; thus, a new neighbor production mechanism is constructed. In this mechanism, the neighbors are chosen adaptively, adding an adaptive coefficient at each iteration. Due to the diversification principle, the coefficient is large at early iterations; therefore, the neighbors are chosen too far from the present solution. This neighbor production mechanism enables us to find the most promising region of the search space. After some iterations, the coefficient is getting smaller; thus, the intensive searching at the most promising region can be done.

The difference between the ITSA and the MTSA is the number of neighbors produced at each iteration. While the MTSA uses the fixed number of neighbors for each variable in the solution vector, the ITSA obtains the number of neighbors, adaptively. At each iteration, the average of the results obtained from the neighbors of each variable is used in the ITSA for calculating the number of neighbors at the next iteration. The neighbors of a present solution of the ITSA are created by the following procedure.

At the first iteration, each variable on the solution has two neighbors. After all neighbors are evaluated, the average of evaluation values is calculated for each variable. If $\mathbf{s}_j = (s_{j,1}, s_{j,2}, ..., s_{j,n})$ is the solution vector at the *j*th iteration, the number of neighbors, NumOf_N($s_{j+1,k}$), at the next iteration is determined by the following formula developed in this work,

NumOf_N(
$$s_{j+1,k}$$
) = NumOf_N($s_{j,k}$)

$$\times \left(2\frac{A(k) - \min(A)}{\max(A) - \min(A)}\right)$$
(14)

where A(k) is the average value of evaluations of the kth variable's neighbors and max(A) and min(A) are the maximum and the minimum averages of all variables at the *j*th iteration, respectively. The value of eq. (14) is rounded towards the nearest integer value. It is clear from Eq. (14) that the variables having good averages get more neighbors at the next iteration, otherwise the number of neighbors becomes smaller.

At the *j*th iteration, the *i*th neighbor N of the kth variable is produced by the following expression proposed in this work,

$$N(s_{j,k}) = N(s_{j-1,k}) + \frac{i}{2}(-1)^{i}\Delta(j) \quad (15)$$

with

$$\Delta(j) = \frac{\lambda}{j} \left[\frac{\text{LatestImprovementIteration}}{j + \text{LatestImprovementIteration}} \right]^{\alpha}$$
(16)

where λ determines the initial magnitude of $\Delta(j)$, and α controls the change of $\Delta(j)$. The index, j, in $\Delta(j)$ represents the iteration number. The suitable values for the parameters λ and α in eq. (16) are determined by experience on the tabu search. LatestImprovementIteration in Eq. (16) is the iteration number at which the latest improvement was obtained.

Later, in order to prevent from any excess of the boundary values of the kth variable, every neighbor is inserted into a search space by using

$$N(s_{j,k}) = s_{k_{\min}} + \operatorname{Remain}(N(s_{j,k}), s_{k_{\max}} - s_{k_{\min}})$$
(17a)

with

$$\operatorname{Remain}(x, y) = x \mod y \tag{17b}$$

where $s_{k_{\min}}$ and $s_{k_{\max}}$ are the minimum and maximum boundary values of the *k* th variable, respectively. The "remain function" in eq. (17b) keeps the elements of solution within the desired ranges.

At initialization, the goal is to make a coarse examination of the solution space, known as "diversification," but as the candidate locations are identified the search is more focused to produce local optimal solutions in a process of "intensification." At the early iterations, $\Delta(j)$ is too high, and owing to the remain function, it seems that the search direction looks like a random search as in the diversification principle. While the number of iterations increases, $\Delta(j)$ decreases exponentially and the neighbors produced become very near to the solution.

In order to describe clearly the ITSA proposed in this work, the main structure of this algorithm is given in Figure 5.

A solution vector \mathbf{s} consists of real and integer values and is given by

$$\mathbf{s} = [k_{11}a_{11}b_{11}c_{11}k_{12}a_{12}b_{12}c_{12}\dots k_{1m}a_{1m}b_{1m}c_{1m}$$

$$\xi_{10}\xi_{11}\xi_{12}\dots\xi_{1m}\dots$$

$$k_{n1}a_{n1}b_{n1}c_{n1}k_{n2}a_{n2}b_{n2}c_{n2}\dots k_{nm}a_{nm}b_{nm}c_{nm}$$

$$\xi_{n0}\xi_{n1}\xi_{n2}\dots\xi_{nm}]$$
(18)

{initialization} N := Number of variables (e.g. length of solution vector) Best := Infinitive; $tabu_List[1..100] := NULL;$ NumNeigh[1..N] := 5; {all averages set to 1} $A[1..N] \coloneqq 1;$ $S_0 = \operatorname{random}(N);$ for $i \coloneqq 2$ to Last_Iteration begin For $k \coloneqq 1$ to N begin {calculating number of neighbors for each variable using eqs. (14–17)} For i = 1 to NumNeigh[k] begin {producing neighbors} $C_{k,i} = S_k + 0.5^* i^* (-1)^{i*} \Delta(j)$ {projection to search space} $C_{k,i} = S_{k\min} + \operatorname{Remain}(C_{k,i}, (S_{k\max} S_{k \min}))$ If $C_{k,i}$ not in tabu–list then $E_{k,i} = \text{evaluate}(C_{k,i})$ End; End; $A(k) = \operatorname{Average}(E_k)$ End; $E_{\min} \coloneqq \min(E)$ {update the best solution} If $E_{\min} < \text{Best then Best} := E_{\min}$; {update tabu list} Add(tabu_List, parameters of C_{\min})

End;

Figure 5. Main structure of improved tabu search algorithm.

where k_{ij} , a_{ij} , b_{ij} , and c_{ij} are the type, the position, the slope, and the flatness parameters of input membership functions, respectively. The subscripts *n* and *m* in eq. (18) are the number of rules and the number of inputs, respectively. The rule constructed by the input membership function and consequent parameters can be written as

$$R_{i} = [M_{i1}M_{i2}\dots M_{im}\,\xi_{i0}\,\xi_{i1}\,\xi_{i2}\dots\xi_{im}] \quad (19)$$

where M_{ij} is the *j*th input membership function for the *i*th rule, and is a function of k_{ij} , a_{ij} , b_{ij} , and c_{ij} .

While the MTSA uses the tabu restrictions based on the recency and frequency memories, the ITSA uses the tabu restriction strategy based on the type of list form. Each list element in the ITSA consists of the input membership function parameters M_{ij} . Therefore, four parameters, k_{ij} , a_{ij} , b_{ij} , and c_{ij} , are stored in a list element. The structure of the list used is LIFO (last in first out). If a membership function exists in the tabu list, this function is rejected and the membership function which is not in the tabu list is reproduced. If all of the membership functions produced are listed in the tabu list, the aspiration criterion is used. The aspiration criterion used in this work is that the last element in the tabu list is extracted from the list.

VI. APPLICATION OF FIS TO THE CALCULATION OF THE RESONANT FREQUENCY

The proposed technique involves training a FIS to calculate the resonant frequency (RF) when the values of W, L, h, and ε_r are given. Figure 6 shows the FIS model used in computation of the RF. Training the FIS by the ITSA, MTSA, and CTSA to compute the RF involves presenting them sequentially with different (W, L, h, ε_r) sets and corresponding measured values $f_{\rm ME}$. Differences between the target output $f_{\rm ME}$ and the actual output RF of the FIS are used to determine optimally the types and parameters of the membership functions and the consequent parameters. This optimum determination is made by using the ITSA, MTSA, and CTSA. The optimization is carried out after the presentation of each set (W, L, h, ε_r) until the calculation accuracy of the FIS is deemed satisfactory according to the root-mean-square error between the target output $f_{\rm ME}$ and the actual output RF for all the training sets that fall below a given threshold or the maximum allowable number of iteration is reached.

The training and test data sets used in this paper have been obtained from previous experimental works [23, 33, 43, 44] and are given in Table I. Nine data sets (marked with superscript b) are used for testing, and the remaining 37 data



Figure 6. Fuzzy model for resonant frequency computation.

f_{ANN}	[45]	2309 2890	4224	5841	6832	//04	82/0	0414	7820	2226	2190	2181	7736	8414	3966	7725	4600	5058	4828	6542	5581	6189	7023	5801	5266	7967	6554	5157	7990	7107	6067	204/	7600	4632	4602	3510	3954	3882	3978	3982	3460	3187	2963 3141	1410
f_{KA2}	[44]	786 1219	2983	6712	9375	14005	C2171	10107	1500	266	266	266	412	488	510	1610	113	1621	1460	2550	1769	2860	4792	3259	3383	8674	5486	5437	8067	7242	6103	C/8C	0705	4600	4603	3574	3955	3895	3982	3903	3493	3197	2982 3160	OULC
$f_{\rm KA1}$	[44]	628 963	2294	5032	6955 10261	10201	16706	10/00	10061	281	281	281	295	349	358	1775	14548	1294	1169	2719	1907	3019	4942	3399	3281	8153	5236	5457	8089	7241	6113	1880	6700	4600	4556	3554	3920	3863	3940	3852	3450	3160	2954 3125	0710
$f_{\rm GU}$	[41]	2323 2831	4191	5919	6798 7520	87.01	8254	1416	75 85	2197	2180	2168	7717	8389	3887	7376	4430	4797	4573	6114	5194	5735	6433	5326	4842	6822	5951	4338	6367	5452	4735	4015	41.29	3479	2921	2461	2572	2555	2509	2356	2137	1983	1924	71/17
$f_{\rm CH}$	[35]	2377 2908	4331	6089	6909 7.000	1889	8402	60/0	601 C	2222	2206	2210	7720	8396	3917	7551	4614	4924	4688	6357	5374	5988	6769	5586	5081	7570	6264	4830	7160	6179	5341	2010	0666 4830	3949	3446	2845	3015	2987	2966	2823	2549	2357	2229	0007
$f_{\rm GA}$	[34]	2389 2915	4296	5965	6761 7920	078/	3020	2025	50LL	2245	2221	2204	7763	8446	3950	7639	4729	4958	4724	6382	5414	5987	6682	5552	5030	7339	6135	4678	6889	5904	5125	4880	7710	3770	3168	2670	2790	2771	2721	2554	2317	2151	2086 2139	C17
$f_{\rm SE}$	[30]	2458 3042	4681	6918	8109	11051	17500	00071	866/	2248	2228	2216	7737	8417	3951	7763	4979	5101	4846	6729	5625	6413	7504	6078	5572	8885	7076	5693	8447	7342	6317	6042 6452	5804	4689	4209	3430	3668	3629	3626	3473	3129	2889	2612	007
$f_{\rm JA}$	[2]	2296 2795	4108	5700	6467	/482	8132	40004	452U 7463	2175	2158	2148	7635	8298	3838	7322	4455	4741	4520	6067	5158	5682	6320	5259	4762	6917	5794	4407	6464	5525	4803	40/04	4 / 04	3526	2938	2485	2590	2573	2522	2364	2146	1992	1936 1982	70/1
$f_{\rm BA}$	Ξ	2452 3013	4529	6448	7405	8/11	6/56	17001	9154 8154	2259	2241	2230	7791	8478	3983	7733	4641	5070	4824	6566	5535	6201	7052	5801	5287	7981	6550	5092	7519	6484	5606	2002	2002	4141	3615	2983	3162	3133	3112	2964	2675	2474	2370	2470
$f_{\rm CA}$	[23]	2373 2893	4239	5928	6806 7057	006/	8980	00011	1604601	2232	2204	2184	7750	8431	3949	7605	4407	4989	4749	6421	5424	6053	6867	5653	5155	7813	6390	4993	7546	6601	5660	5423	070C	4227	3824	3115	3335	3299	3294	3147	2838	2623	2502	0007
$f_{\rm HA}$	[20]	2381 2911	4327	6085	6958 0127	8157	CU68	1006	1010	2209	2208	2208	7697	8369	3898	7442	4254	4865	4635	6220	5270	5845	6566	5435	4943	7334	0209	4667	6845	5870	5092	4800	1010	3746	3201	2668	2808	2785	2753	2608	2358	2183	2102	0017
$f_{\rm HO}$	[19]	2586 3222	5039	7559	8933	10001	14030	140.00	0022 0022	2292	2292	2292	7804	8496	4027	7940	4697	5283	5014	6958	5795	6653	7828	6325	5820	9319	7412	5945	8698	7485	6478	0819	07 CO	4768	4084	3408	3585	3558	3510	3313	3001	2779	2684 2763	7102
odels	f_{CTSA}	2310.0 2890.0	4240.2	5840.0	6799.8" 7700.1	1.990/	8271.3	0.0004	78607	2228.0	2200.0 ^b	2181.0	7740.0	8449.6^{b}	3970.2	7730.7	4600.0	5061.9	4802.9 ^b	6560.5	5600.3	6197.0^{b}	7050.5	5801.9	5268.5	7991.8	6570.0	5095.1 ⁰	7997.0	7137.9	6068.8	2858.2	5.60C0	4660.8	4600.2	3579.5 ^b	3974.5	3904.7	3982.0	3898.6	3471.0	3200.3	2980.2 3140.0	0.7710
sent FIS Mo	$f_{\rm MTSA}$	2310.0 2890.0	4240.1	5839.7	6800.7 °	/098.4	82/2.1	1.6616	7860.0	2228.0	2200.0 ^b	2181.0	7740.1	8449.6 ^b	3970.1	7730.4	4600.0	5060.4	4804.4 ^b	6560.0	5600.2	6199.2 ^b	7050.6	5801.1	5269.0	7990.6	6569.0	5098.30	7.8667	7136.1	6066.6	77.6780	0.1100	4660.4	4600.0	3579.4 ^b	3975.5	3903.8	3981.7	3899.0	3470.8	3200.3	2980.4 3140.0	0.7410
Pre	f_{ITSA}	2310.0 2890.0	4240.1	5839.5	6800.7 °	/0/00/	82/17	7.6016	4/50.0	2228.0	2200.0 ^b	2181.0	7740.1	8449.7 ^b	3970.1	7730.3	4600.0	5060.0	4804.9^{b}	6559.8	5600.1	6200.0^{b}	7050.1	5800.5	5269.6	7990.2	6569.6	5100.0°	7999.5	7134.9	6069.5	0.1280	7 0805	4660.1	4599.9	3579.5 ^b	3978.0	3901.7	3981.2	3899.0	3471.2	3200.7	2980.6 3148-1	7140.1
$f_{ m ME}$ [23, 33, 43, 44]	Measured	2310^{a} 2.890^{a}	4240^{a}	5840 ^a	6800" 7700 ^a	/ /00 ⁻	82/0 ⁻	9140 4770 ⁸	4/30 7870 ⁸	2228°	2200°	2181°	7740	8450	3970	7730	4600	5060	4805	6560	5600	6200	7050	5800	5270	7990	6570	5100	8000	7134	6070	0785	0000 5 000	4660	4600	3580	3980	3900	3980	3900	3470	3200	2980 3150	0.010
	$(h/\lambda_d) \times 10^2$	3.7317 4.6687	6.8496	9.4344	10.9852	12.4592	13.3600	2000.41	6 1076 A	1.7896	1.7671	1.7518	0.6535	0.7134	1.5577	3.2505	6.2193	4.0421	3.8384	5.6917	4.8587	6.6004	9.0814	7.7800	8.3326	12.6333	10.3881	12.9219	14.0525	15.1895	14.5395	14./402 16 1650	17 5363	15.5278	20.9105	18.1413	20.1683	19.7629	21.1852	22.8353	22.1646	21.8197	20.3196 21.4787	10/4-17
	ε_{I}	2.33 2.33	2.33	2.33	2.33	2.33	2.33	CC.7	2.55 2.22	2.50	2.50	2.50	2.22	2.22	2.22	2.55	10.2	2.33	2.33	2.55	2.55	2.55	2.55	2.55	2.50	2.50	2.50	2.55	2.55	2.55	2.55	CC.7	25 C	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2.55	2:55	CC.4
	<i>h</i> (cm)	0.3175 0.3175	0.3175	0.3175	0.3175	C/15.0	C/15.0	2020 0	0.1574	0.1524	0.1524	0.1524	0.0170	0.0170	0.0790	0.0790	0.1270	0.1570	0.1570	0.1630	0.1630	0.2000	0.2420	0.2520	0.3000	0.3000	0.3000	0.4760	0.3300	0.4000	0.4500	0.4760	0.4700	0.6260	0.8540	0.9520	0.9520	0.9520	1.0000	1.1000	1.2000	1.2810	1.2810	0107.1
	L (cm)	3.800 3.050	1.950	1.300	1.100	006.0	0.800	0./00	1 100	4.140	4.140	4.140	1.290	1.185	2.500	1.183	1.000	1.860	1.960	1.350	1.621	1.412	1.200	1.485	1.630	1.018	1.280	1.580	1.080	1.255	1.450	1.440	1.440 1.620	1.970	2.300	2.756	2.620	2.640	2.676	2.835	3.130	3.380	3.500 3.400	004.0
	W (cm)	5.700 4.550	2.950	1.950	1.700	1.400	1.200	000.1	1 700	4.100	6.858	10.80	0.850	0.790	2.000	1.063	0.910	1.720	1.810	1.270	1.500	1.337	1.120	1.403	1.530	0.905	1.170	1.375	0.776	0.790	0.987	0.014	0.790	1.200	0.783	1.256	0.974	1.020	0.883	0.777	0.920	1.030	1.265	1,000

^aThese frequencies measured by Chang et al. [33]. ^bShows the test results. Resonant frequencies are in MHz. ^cThese frequencies measured by Carver [23], the remainder measured by Kara [43, 44]. sets are used for training the FISs. In microstrip antenna designs, the most important parameter is the electrical thickness h/λ_d of the antenna. The electrical thickness values are given in the fifth column of Table I. It is clear from Table I that the range of electrical thickness h/λ_d is very wide for microstrip antennas. As can be also seen from Table I that nine different electrical thicknesses, which are not close to each other, are chosen to test the performance of FISs. These testing sets are also the same as those used for the artificial neural networks [45].

The parameters of the learning algorithms are: for the ITSA, MTSA, and CTSA, the number of iterations is fixed to 2000 in the training process, the number of membership functions for the input variables (W, L, h, and ε_r) are 3, 3, 3, and 2, respectively, the number of rules is then 54 [3 imes $3 \times 3 \times 2 = 54$], three types of membership functions, gaussian, generalized bell, and trapezoidal, are used, and the values of *n* and *m* in eq. (18) are 54 and 4, respectively; for the ITSA and MTSA, 1134 [54(4 + 4 + 4 + 4 + 5) = 1134] parameters are optimized, and the values taken for λ and α in eq. (16) are 100,000 and 2, respectively; for the ITSA, the size of the tabu list is fixed to 100; for the CTSA and MTSA, the tabu restrictions based on the recency and frequency memories are used, and the recency and frequency factors are 1.5 and 2, respectively; for the CTSA, k_{ii} is expressed by 2 bits, each of a_{ii} , b_{ii} , c_{ij} , and ξ_{ij} are represented by 4 bits, and the solution vector consists of 4104 [54(14 + 14 +14 + 14 + 20 = 4104 bits.

The computer program based on the FIS proposed here is written in C. The program begins by asking for the four parameters, W, L, h, and ε_r . The resonant frequency is then calculated directly by the FIS (The program source code for the FIS proposed in this paper can be obtained from the authors either by mail or electronic mail.)

VII. RESULTS AND CONCLUSIONS

In order to determine the most appropriate suggestion given in the literature, we compared our computed values of resonant frequencies for electrically thin and thick rectangular microstrip patch antennas with the theoretical and experimental results reported by other scientists, which are all given in Table I. The entries for $f_{\rm ME}$, $f_{\rm ITSA}$, $f_{\text{MTSA}}, f_{\text{CTSA}}, f_{\text{HO}}, f_{\text{HA}}, f_{\text{CA}}, f_{\text{BA}}, f_{\text{JA}}, f_{\text{SE}}, f_{\text{GA}},$ $f_{\rm CH}, f_{\rm GU}, f_{\rm KA1}, f_{\rm KA2}$, and $f_{\rm ANN}$ represent, respectively, the values measured [23, 33, 43, 44], calculated by the FIS with the use of the ITSA, MTSA, CTSA, by Howell [19], by Hammerstad [20], by Carver [23], by Bahl and Bhartia [1], by James et al. [2], by Sengupta [30], by Garg and Long [34], by Chew and Liu [35], by Güney [41], by using the curve-fitting formula proposed by Kara [44], by using the modified cavity model [44], and by using the artificial neural networks [45]. The results of Carver [23] are obtained by using a program called MSAnt which was written by Pozar [6]. The total absolute errors (absolute error = |theoretical result-experimental result) for every suggestion in Table I are also listed in Table II.

It can be clearly seen from Tables I and II that the previous methods give comparable results some cases are in very good agreement with measurements, and others are far off. The results of the FIS proposed in this work are superior to those predicted by other scientists and are also better than those calculated by using the artificial neural networks proposed in our previous work [45]. The very good agreement between the measured values and our computed resonant frequency values supports the validity of the present FIS.

From the results, we can find that the best results are obtained from the FIS trained by the ITSA. The ITSA is a very powerful method that allows us to design highly accurate and parsimonious FISs. It also needs to be emphasized once more that better and more robust results may be obtained from the proposed method if more input data set values are supplied for training.

Since the model presented in this work has high accuracy and requires no complicated mathematical functions, it can be very useful for the development of fast CAD algorithms. This CAD model, capable of accurately predicting the resonant frequency of electrically thin and thick rectangular microstrip antennas, is also very useful to antenna engineers. Using this model with a personal computer, one can calculate accurately the resonant frequency of rectangular patch antennas without possessing any background knowledge of microstrip antennas. The real-time calculation is less than 200 μ s after training. Thus, the FIS is very fast after training. Finally, we expect that the FIS models will find wide applications in CAD of antennas and microwave integrated circuits.

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	Pre	sent FIS Moc	dels	f _{HO}	$f_{\rm HA}$	$f_{\rm CA}$	$f_{\rm BA}$	$f_{ m JA}$	$f_{\rm SE}$	$f_{\rm GA}$	$f_{\rm CH}$	$f_{\rm GU}$	$f_{\rm KA1}$	f _{KA2}	f_{ANN}
Methods	f_{ITSA}	$f_{\rm MTSA}$	f_{CTSA}	[19]	[20]	[23]	[1]	[2]	[30]	[34]	[35]	[41]	[44]	[44]	[45]
Total absolute deviations from the measured data (MHz)	23.5	50.5	81.6	36059	26908	1104916	19179	32930	23746	23761	19899	31436	108707	126945	751

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