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Capacitance–conductance characteristics of Au/Ti/Al₂O₃/n-GaAs structures with very thin Al₂O₃ interfacial layer

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Capacitance–conductance characteristics of Au/Ti/Al₂O₃/*n*-GaAs structures with very thin Al₂O₃ interfacial layer

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Abstract

High- k Al₂O₃ with metallic oxide thickness of about 3 nm on *n*-type GaAs substrate has been deposited by the atomic layer deposition (ALD) technique. Thus, it has been formed the Au-Ti/Al₂O₃/*n*-GaAs MIS structures. It has been seen that the MIS structure exhibits excellent capacitance–voltage (C – V) and current–voltage (I – V) properties at 300 K. The saturation current of the forward bias and reverse bias I – V characteristics was the same value. An ideality factor value of 1.10 has been obtained from the forward bias I – V characteristics. The C – V characteristics of the structure have shown almost no hysteresis from +3 V to –10 V with frequency as a parameter. The reverse bias C – V curves have exhibited a behavior without frequency dispersion and almost hysteresis at each frequency from 10 kHz to 1000 kHz.

1. Introduction

Metal/oxide (insulator)/semiconductor field effect transistor (MOSFET) systems are important conventional devices in integrated circuit technology. MOS transistors are also increasingly used in analog applications such as switched capacitor circuits, analog-to-digital converters and filters [1–9]. As mentioned by Wu and colleagues [10], the integrated circuit fabrication based on MOSFET relies on thermally grown amorphous SiO₂ as a gate dielectric, and a stable Si:SiO₂ interface offers many important materials and electrical properties such as the excellent electrical insulation and interfacial bonding properties. However, in order to avoid severe short channel effects, the gate dielectric thickness must also be reduced to the point that leakage current becomes unacceptable. Therefore, the SiO₂ must be replaced with other gate dielectrics [10–24], that is, the reduction of gate dimensions requires decreasing oxide thickness to prevent the short channel effect and therefore the undesirable gate leakage current is substantial and increases exponentially with decreasing thickness. This calls for other dielectrics with much higher dielectric constants, that is, the high- κ metallic gate oxides which allow maintenance of the gate oxide capacitance needed for reducing short channel effects [10–24]. Wu and colleagues have reported [10] that the atomic layer deposition (ALD) method is the most widely used technique in spite of the fact that other methods have also led to attractive results, and that the ALD has improved the interface quality and reduced the defects density in high- κ films. Furthermore, Deposition of the SiO₂ onto GaAs substrate creates a high density of interface states. These facts practically prevent implementation of MOS capacitor with GaAs substrate [1].

We have prepared the MIS (metal/insulator/semiconductor) Au/Ti/Al₂O₃/*n*-GaAs/In. The Al₂O₃ metal oxide layer on the GaAs substrate was formed by ALD method, and the film thickness of the Al₂O₃ layer was about 3 nm. As stated by Pan *et al* [12], the complementary metal oxide semiconductor (MOS) devices require gate oxide of about 1 nm to reduce the gate leakage current and maintain the gate capacitance. This is the reason

why we take such a thickness. Thickness of conventional SiO₂ less than 20 Å is inevitable to excessive leakage current due to the occurrence of direct tunneling. Therefore, silicon dioxide has to be substituted by a high dielectric constant material, which provides a physically thicker film for the same electrically equivalent oxide thickness [12]. Au(50 nm)/Ti(10 nm) Schottky contacts have been fabricated on Al₂O₃/*n*-GaAs structure using magnetron dc sputter technique. Au thin films are more often used as a top layer to protect other metallic layers. Al₂O₃ is an attractive candidate for the high- κ material; it has a dielectric constant of 8.6 and a wide bandgap of about 6.6 eV (for the amorphous oxide typical of ALD-grown layers). Titanium is commonly used as a standard gate metal in the fabrication of GaAs field effect transistors (FET) and MESFET since it has good adhesion and is stable against inter-diffusion and compound formation and has good electrical properties at room temperature and elevated temperatures [23, 24].

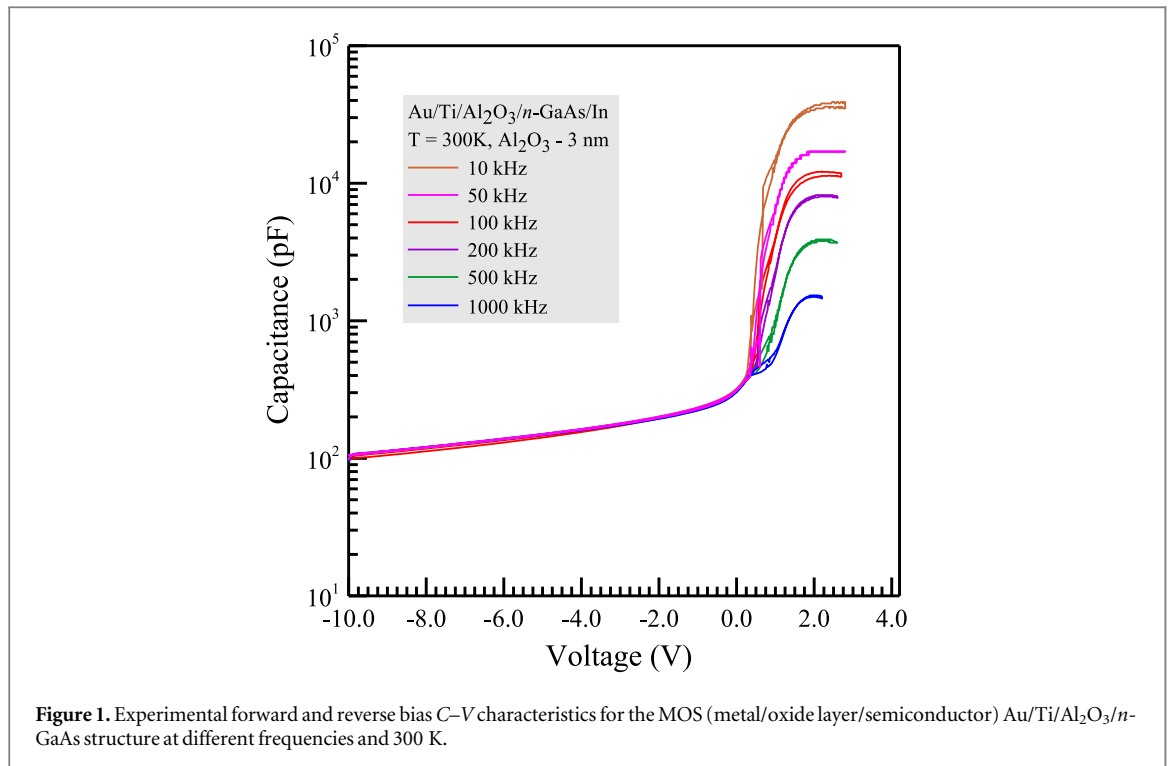
Moreover, the method used to form the oxide layer in the MOS systems affects device performance and stability and plays an important role in integrated circuits. Furthermore, It has been examined that high- κ metallic gate oxides such as Al₂O₃, Nd₂O₃, Gd₂O₃ and HfO₂ become the potential materials and high dielectric permittivity to replace silicon dioxide SiO₂ [9–12], and ALD technique can be preferred to the other techniques for the deposition of metallic gate oxide Al₂O₃, Nd₂O₃ and Gd₂O₃ due to its unparalleled uniformity and precise thickness control technique. Pan *et al* [12] have reported that TiN/Nd₂O₃/*p*-Si/Al MOS capacitors with film thickness of about 6.5 nm grown by reactive rf sputtering exhibit excellent electrical properties such as high electric breakdown field and being without frequency dispersion and almost hysteresis in capacitance–voltage (*C*–*V*) curves after annealing at 700 °C treatment. Raeissi *et al* [13] have investigated electron capture for insulator/silicon interface states for high- κ dielectrics of Gd₂O₃ grown on silicon wafers by molecular beam epitaxy (MBE) and ALD, and for HfO₂ prepared by reactive sputtering by measuring the frequency dependence of MOS capacitance. Kundu *et al* [14] have fabricated GaAs-based MOS devices with TiO₂ layer having three different thicknesses of 33, 54 and 71 nm of TiO₂ by the sol–gel technique and they have shown that the *C*–*V* characteristics have strongly depended on applied voltage and the interfacial layer thickness and frequency in the frequency range 10 kHz–1 MHz [14].

Long *et al* [16, 17] reported the *C*–*V* measurements of Pd/Al₂O₃/GaN MOS capacitors with the Al₂O₃ layer of approximately 8 nm by ALD, over a temperature range of 77–500 K. They [16, 17] have estimated the interface state density of the wide band gap GaN semiconductor by the limitations of the conductance method in this temperature range, and have described the role of the pyroelectric effect in the interpretation of higher temperature capacitance–voltage data, because GaN-based devices are intended for high temperature applications. Saghrouni *et al* [20, 21] have described the effect of post-deposition annealing on the physical and electrical characteristics of Co/Au/Dy₂O₃/*p*-GaAs device with Dy₂O₃ thickness of 10 nm by electron beam deposition (EBD) under ultra-vacuum. They [20] have found that the annealed device exhibited excellent electrical properties such as small density of interface state and low leakage current, and have studied the ac impedance properties of the structures in a wide frequency range at different bias voltage, and have attributed this phenomenon to a rather crystallized Dy₂O₃ structure and to the reduction of the defects at the oxide/GaAs interface.

It has been stated in the above studies that metal oxides are readily formed by atomic layer deposition. The ALD process for HfO₂ using tetraethylmethylamido hafnium as the metal precursor has resulted in an interfacial layer between the oxide and the semiconductor, in contrast to Al₂O₃ deposition by ALD on surfaces such as GaAs and InGaAs. The initial stages of the Al₂O₃ deposition process by ALD have often been reported to result in the decomposition of native oxides formed on the semiconductor surface, with trimethylaluminium (TMA) as the metal source [17]. Furthermore, Dy₂O₃, like most rare earth oxides, is not usually stoichiometric and often contains significant concentrations of oxygen vacancies which can contribute to leakage current. Thus, it is important to evidence the effects of the native oxide and the different defects such as oxygen vacancies and grain boundaries on the electrical and dielectrical properties of MIS or MOS structures [20, 21]. The opto-electrical characteristics of MIS structures are controlled mainly by its interface properties [1–7, 25–30]. As is well-known, the *C*–*V* plot or admittance value differs significantly from that expected for an ideal MIS diode, and thus the performance of the metal oxide/GaAs-based electronic and optical devices is reduced [1–7, 25–30]. Therefore, studies on interface properties are essential in the understanding of the electrical properties of the MIS structures, and are especially of technological importance for developing GaAs-based devices [25–30].

2. Experimental details

Au/Ti/Al₂O₃/*n*-GaAs MIS structures were fabricated using *n*-type single crystals GaAs wafer with (100) surface orientation, having thickness of 300 μm , $6.8 \times 10^{15} \text{ cm}^{-3}$ carrier concentration (N_D) and 1.2 $\Omega \text{ cm}$ resistivity (given by the manufacturer). Before the SBDs fabrication process, the experimental procedure was carried out first as a cleaning procedure, that is: sonicated for two minutes in acetone and two minutes in propanol,



respectively; then, rinsed in DI water of resistivity of 18 M Ω cm for an extended time and dried under N₂ flow. After surface cleaning of n -GaAs, high purity (99.999%), In with a thickness of about 2000 Å was coated for ohmic contact at a base pressure about 10⁻⁶ Torr. Low ohmic contact to n -GaAs was obtained by annealing at 385 °C for three minutes under dry nitrogen flow. The ALD of Al₂O₃ thin films was carried out in Cambridge Nanotech Savannah 100 reactor. The Al₂O₃ deposition was performed at 200 °C using trimethylaluminum (TMA) (Al precursor), and water (oxygen precursor), for a total of 30 cycles. Standard photolithography technique was used for pattern fabrication on GaAs. An Al₂O₃ interface layer is formed by ALD method and Au (90 nm)/Ti(10 nm) Schottky contacts are made using magnetron dc sputter technique. Finally the photoresist was removed by washing with DI water and then with N₂. The $I(V)$ and $C(V,f) - G(V,f)$ characteristics of the device were measured using a Keithley 487 picoammeter/voltage source and an HP 4192 A LF impedance analyzer, respectively, at room temperature in dark.

3. Results and discussion

Figure 1 shows the experimental forward and reverse bias $C-V$ characteristics for the MIS Au/Ti/Al₂O₃/ n -GaAs structure at different frequencies and 300 K. As mentioned above, the thickness of the interfacial layer Al₂O₃ was about 3 nm. For an MIS diode with n -type semiconductor, the curve has an accumulation region of electrons and therefore a high differential capacitance of semiconductor in series with the capacitance of the insulator at positive voltage at the right side. As a result, the total capacitance at the accumulation region is close to the capacitance of the insulator [25–30]. As the positive voltage is reduced sufficiently, a depletion capacitance forms near the semiconductor surface, and the total capacitance decreases because the depletion region acts as a dielectric in series with the interfacial insulator layer [25–30]. As can be seen from figure 1, the hysteresis behavior with a very narrow window was observed for the MIS $C-V$ curves at all frequencies. It can be said that the sample has a negligibly thin interfacial-layer thickness. Another possible reason for this behavior is mobile charges in the oxide layer. This relatively smaller hysteresis phenomenon can be ascribed to the trapped charges at defect sites to be passivized due to the Al₂O₃ layer, and to the reduction of interface traps at Al₂O₃ layer and GaAs interface [3, 25–30].

The characteristics parameters of the ideal Schottky diodes can be calculated using the thermionic emission (TE) current expression. The $I-V$ equation by the forward bias TE theory is given as follows [28–31]

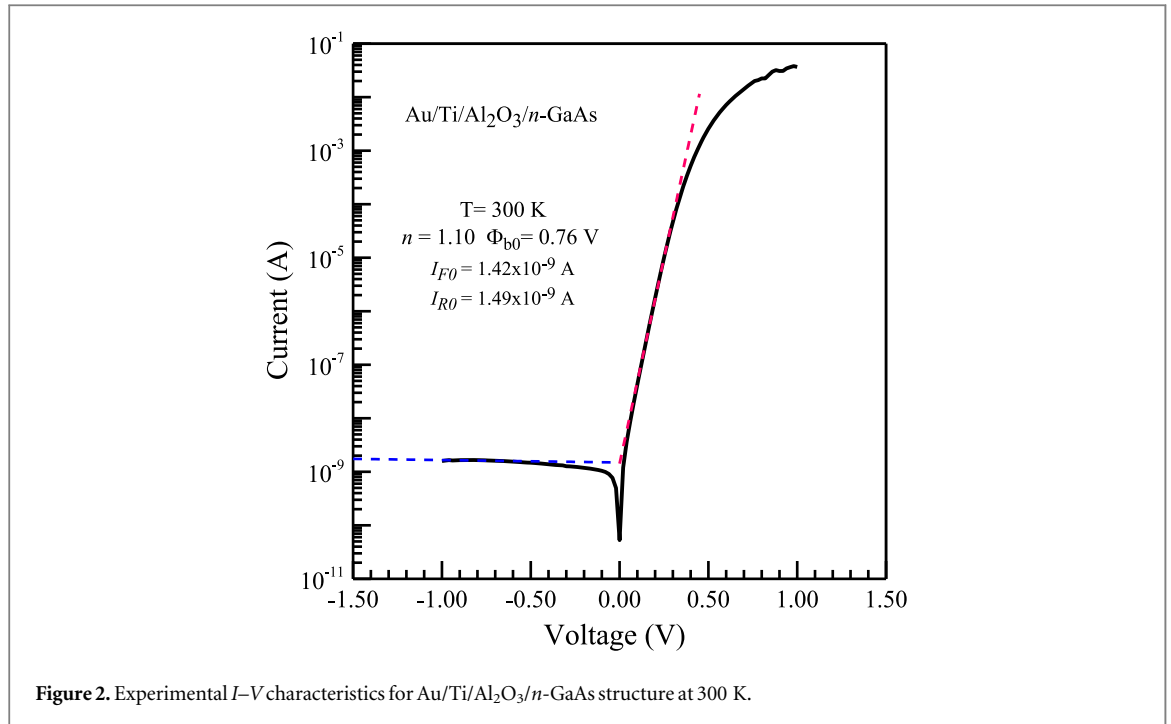


Figure 2. Experimental I - V characteristics for Au/Ti/Al₂O₃/ n -GaAs structure at 300 K.

$$I = I_0 \left[\exp \left(\frac{q(V - IR_s)}{nkT} \right) - 1 \right], \quad (1)$$

Where I_0 is the saturation current

$$I_0 = AA^*T^2 \exp \left(-\frac{q\Phi_{b0}}{kT} \right), \quad (2)$$

is the saturation current density, Φ_{b0} and n are the effective barrier height (BH) at zero bias and ideality factor calculated from the intercept and slope of the linear portion of the semi-log forward bias $\ln I$ - V characteristics, respectively, A^* is the effective Richardson constant of $8.16 \text{ A (cm}^2 \text{ K}^2)^{-1}$ for n -type GaAs, A is the diode area. R_s is the series resistance of the neutral region of the semiconductor substrate between the depletion region and ohmic contact. IR_s and $(V-IR_s)$ are the voltage drop across the series resistance and the depletion region, respectively. The series resistance value of the Au/Ti/Al₂O₃/ n -GaAs MIS diode was calculated as 11.30Ω from the data of downward curvature region of the forward bias I - V characteristics using Cheung's functions [31]. For values of $q(V-IR)$ greater than $3 kT$, the ideality factor is given by

$$n = \frac{q}{kT} \frac{dV}{d(\ln I)}. \quad (3)$$

The value of n indicates the deviation from ideal forward bias characteristics for Schottky diodes. The high values of n can be attributed to effects of the bias voltage drop across the interfacial layer and, therefore, of the bias voltage dependence of the barrier height [32–46].

Figure 2 shows the semi-log reverse and forward I - V curves of the Au/Ti/Al₂O₃/ n -GaAs MIS diode at 300 K. The experimental values of the BH and ideality factor from the intercept and slope of the linear portion of the forward-bias $\ln I$ versus V plot have been calculated as 1.10 and 0.76 eV for 300 K, respectively. The intercepts or the saturation currents at $V = 0$ volts for the reverse bias and forward bias branch correspond to $1.49 \times 10^{-9} \text{ A}$ and $1.42 \times 10^{-9} \text{ A}$. These values say that the device shows an excellent rectification or diode behavior. The saturation current values give a value of about 0.76 eV using equation (2). The ideality factor value of 1.10 says that the current flow across the device is dominated by the thermionic emission over the BH because the Al₂O₃ interfacial layer is very thin. As mentioned by Zussman [33], the sputter process relative to the evaporation process can improve the properties of diode due to a process of cleaning of the surface of the substrate taking place during the sputter deposition as a result of the chemical reactivity of the plasma tail and high energy of the sputtered atoms.

Goksu *et al* [34] used the GaAs semiconductor substrate with the same carrier concentration ($7.43 \times 10^{15} \text{ cm}^{-3}$) and fabricated for Ti/ n -GaAs diodes without the interfacial layer prepared by magnetron dc sputtering and obtained a BH value of 0.90 eV with an ideality factor 1.02 for this diode at 300 K. Myburg *et al*

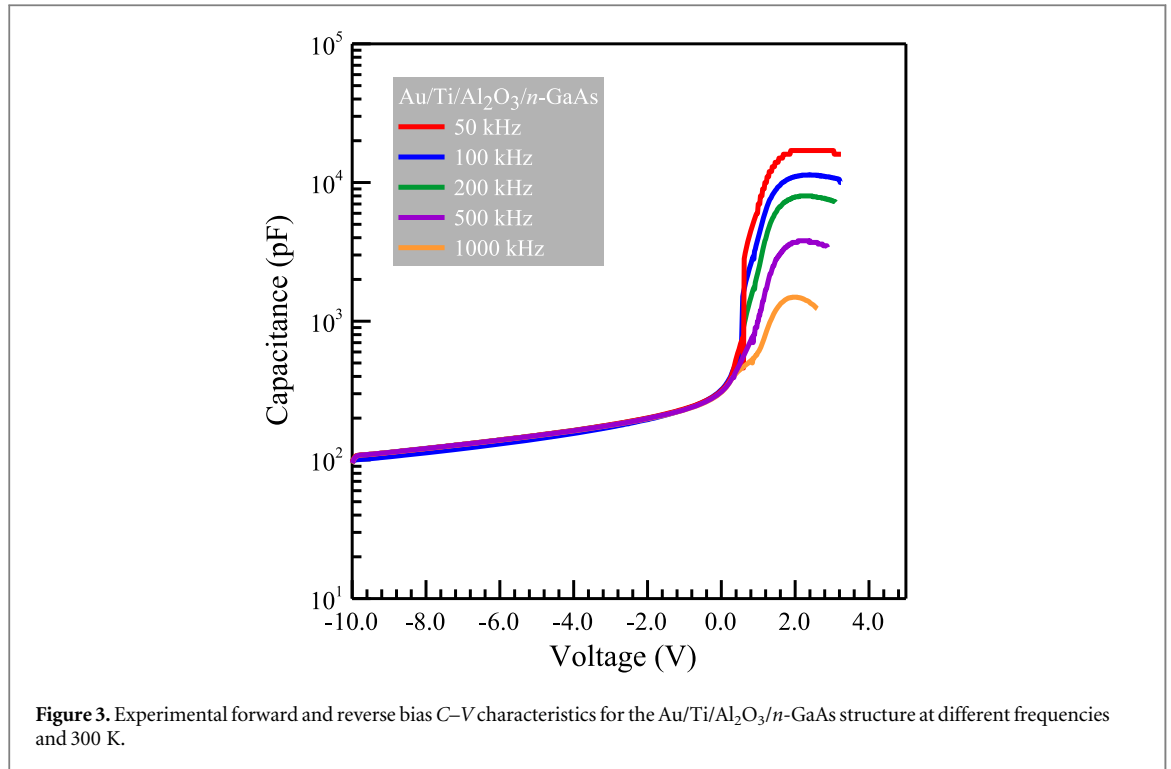


Figure 3. Experimental forward and reverse bias C - V characteristics for the Au/Ti/Al₂O₃/ n -GaAs structure at different frequencies and 300 K.

[35] have fabricated Ti/ n -GaAs Schottky diodes using n -GaAs epilayer layer with a free carrier concentration (Si doped) of $1 \times 10^{16} \text{ cm}^{-3}$ grown on n^+ -GaAs semiconductor substrate by organometallic vapor phase epitaxy, and they [35] have reported a BH value of about 0.83 eV with an ideality factor of 1.03 for this diode at 300 K. Dio *et al* [36] have measured forward and reverse bias I - V characteristics of Au/Ti/ n -GaAs diodes prepared by ion beam sputtering at different sputtering voltages and currents and they [36] have reported BH values from 0.79 to 0.83 eV and ideality factor from 1.03 to 1.10 for these diodes at 300 K. Ayyildiz and Turut [37] have given a BH value of about 0.64 eV with an ideality factor of 1.08 from forward bias I - V characteristics (300 K) of Ti/ n -GaAs diodes prepared by evaporation of Ti. Cola *et al* [38] have reported BH values from 0.828 to 0.854 eV and ideality factor values from 1.01 to 1.08 (300 K) from forward bias I - V characteristics of Au/Ti/ n -GaAs diodes prepared by ion beam sputtering at different sputtering voltages and currents. As can be seen, the value of 0.76 eV we have found for the Au/Ti/Al₂O₃/ n -GaAs MIS diode prepared by magnetron dc sputtering differs from the results in the literature given above. The reason for difference can be due to the presence of the Al₂O₃ layer at the Au/Ti and n -GaAs interface. Therefore, it can be said that the Al₂O₃ layer can be used to realize the barrier height modification in the Schottky diodes.

Let us now consider the MIS structure with the interfacial layer for the I - V characteristics. Kundu *et al* [14] have found ideality factor values of 1.10, 1.13 and 1.15 for n -GaN based MOS structures with TiO₂ thicknesses of 33, 54 and 71 nm prepared by the sol-gel technique, respectively, for which their MOS structures [14] have given the non-saturated reverse bias I - V curves. Reddy *et al* [22] have reported that the BH values of the Au/BaTiO₃/ n -GaN structure with values of 0.87 eV (I - V) and 1.02 eV (C - V) increases compared with those of the Au/ n -GaN MS structure with 0.73 eV (I - V) and 0.96 eV (C - V). They [22] have formed BaTiO₃ thin films of about 60 nm thick on the surface of the cleaned n -GaN substrates by spin coating.

Figure 3 shows the experimental forward (0.0 V to 3.2 V) and reverse bias (0.0 V to -10 V) C - V characteristics for the Au/Ti/Al₂O₃/ n -GaAs MIS structure at different frequencies and 300 K. As can be seen from figure 3, the capacitance curve saturates in the high forward bias voltage. These saturation regions are known as the accumulation region giving the capacitance of the interfacial layer (Al₂O₃) C_{ox} and thus its thickness. The value of C_{ox} determined from the accumulation region in figure 3 decreases with increasing frequency. This value is 17 000 pF at 50 kHz and 1350 pF at 1000 kHz. The values of C_{ox} for each frequency are given in table 1. Furthermore, the capacitance of the interfacial layer per area unit in a MIS diode is given by

$$C_{\text{ox}} = \frac{\epsilon_{\text{in}} \epsilon_0 A}{d}, \quad (4)$$

where ϵ_{in} and d are the permittivity of interfacial layer and its thickness, respectively, ϵ_0 is the permittivity of free space and A is the area of diode. A value of 4.11 nm for the thickness of the interfacial layer Al₂O₃ was obtained using C_{ox} value at 50 kHz in equation (4). This value is in close agreement with the Al₂O₃ layer thickness of

Table 1. Experimental values from the reverse and forward bias characteristics for the Au/Ti/Al₂O₃/n-GaAs MIS structure at different frequencies and 300 K.

<i>f</i> (kHz)	<i>C</i> _{ox} (pF)	ϵ_{in}	<i>R</i> _s (Ω)	0.0 Volts		−10 Volts	
				<i>G</i> (F s ^{−1})	<i>Z</i> (Ω)	<i>G</i> (F s ^{−1})	<i>Z</i> (Ω)
50	17 000	7.97	4.99	1.0×10^{-6}	10 101.00	1.0×10^{-7}	32 362.46
100	11 000	4.70	5.00	2.2×10^{-6}	4972.65	2.0×10^{-7}	16 638.94
200	7200	3.38	4.99	5.1×10^{-6}	2554.28	3.0×10^{-7}	8143.32
500	3800	1.78	4.99	1.5×10^{-5}	1031.57	1.3×10^{-7}	3306.88
1000	1350	0.64	4.99	3.2×10^{-5}	518.94	3.6×10^{-7}	1667.78

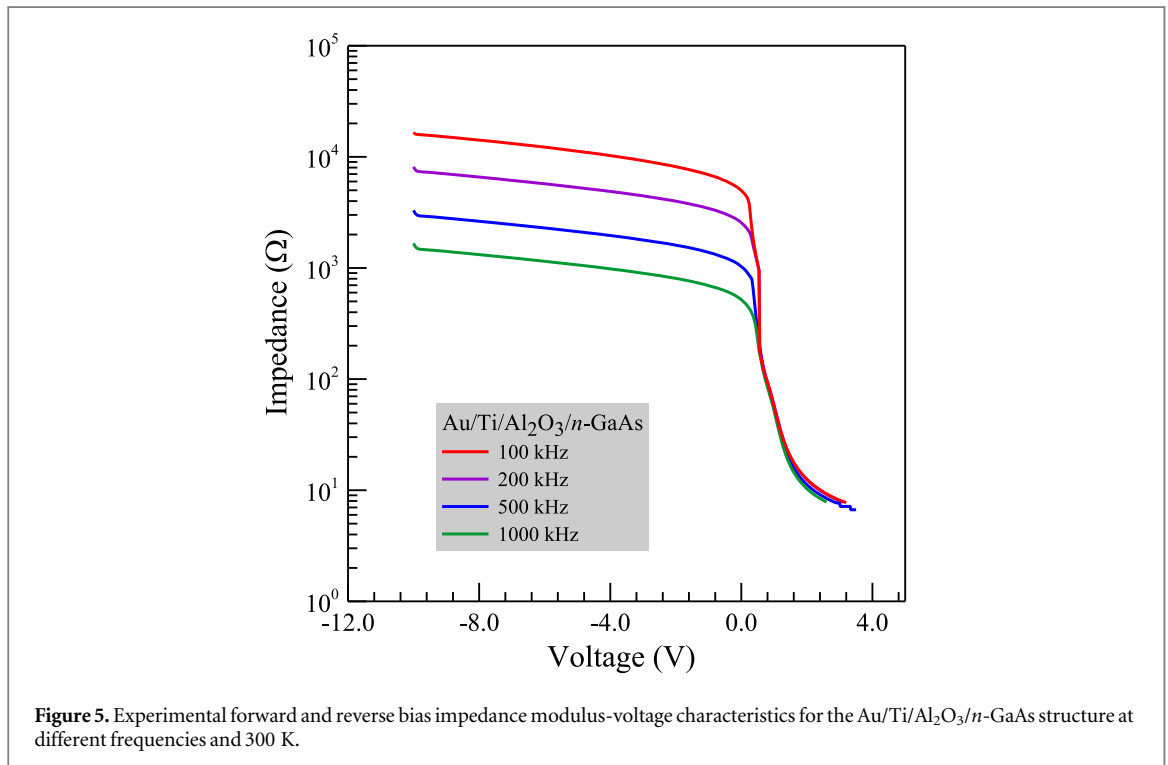
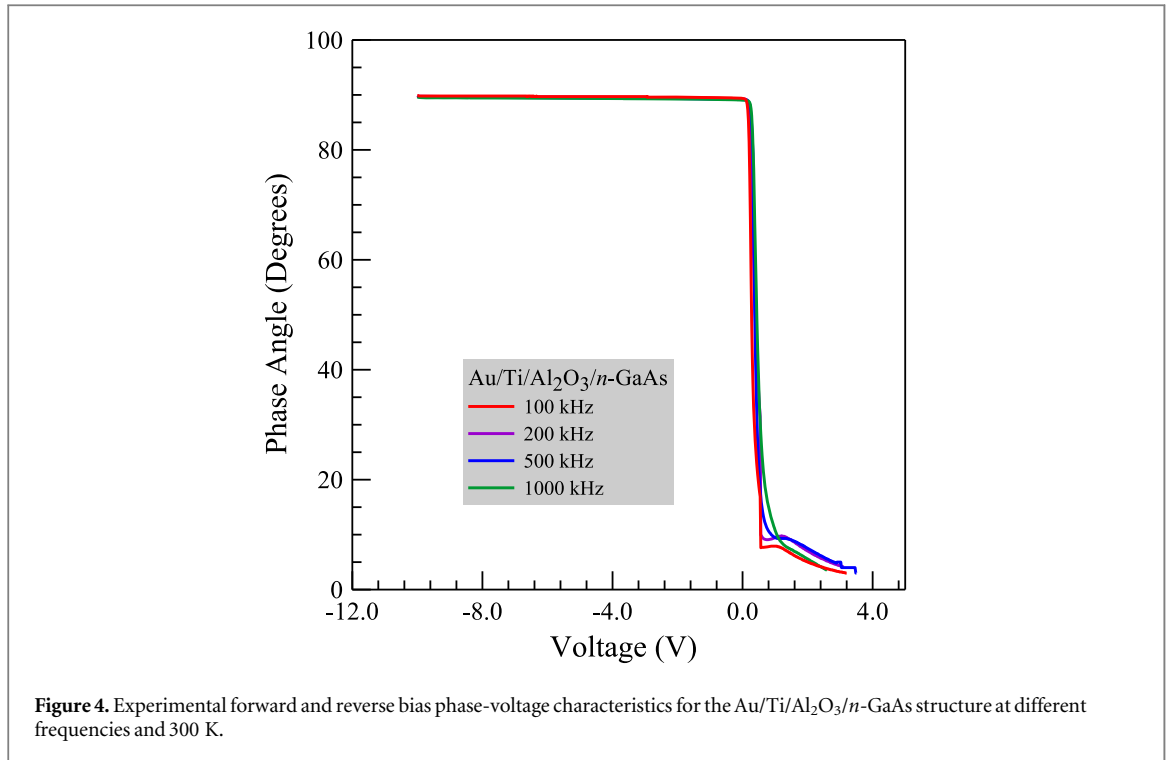
3.0 nm formed on the GaAs wafer by ALD method. As mentioned above, the decrease in the capacitance value with increasing frequency at a given bias voltage in the plots can be attributed to the decrease of the dielectric constant value of the interfacial layer Al₂O₃ with increasing frequency. However, this is attributed to the fact that the interface state charges cannot follow the ac signal at sufficiently high frequencies, or increase in the capacitance with decreasing frequency is ascribed to the contribution of the interface charges in the interface states [25–30, 40–62]. The decrease in capacitance value can be also due to the series resistance of the Al₂O₃ layer plus the neutral region of the semiconductor substrate. The series resistance of the neutral region of the semiconductor substrate between the depletion region and the back contact is the real part of the impedance. A thicker interfacial layer may cause larger series resistance. The series resistance value at each frequency can be large enough to affect the device capacitance. It can cause a serious error in the extraction of the interfacial properties, that is, the series resistance completely masks interface trap loss, and especially the equivalent parallel conductance is much more sensitive to the series resistance than capacitance. Thus, it can be said that the correction for the series resistance is particularly important in conductance measurements. Furthermore, the values of dielectric loss tangent and ac conductivity strongly depend on applied voltage and the thickness of the interfacial oxide layer [1–3, 14–23].

Moreover, the low value of dielectric constant could be due to the formation of the native oxides related to Ga and As during devices fabrication processes. In addition, the diffusion of Ga and As atoms into the high- κ can exacerbate the interface quality between the high- κ dielectric and GaAs [9, 12, 20–22]. The dielectric constant expression of the interfacial layer is given by

$$\epsilon_{in} = \frac{C_{ox}d}{\epsilon_0 A} = \frac{C_{ox}}{C_0}, \quad (5)$$

where *C*₀ is capacitance of an empty capacitor, *d* is the thickness of interfacial layer Al₂O₃. The dielectric constant value of the Al₂O₃ layer was obtained using the *C*_{ox} value from the accumulation region at each frequency in equation (5). The dielectric constant decreases with increase in frequency, as can be seen in table 1.

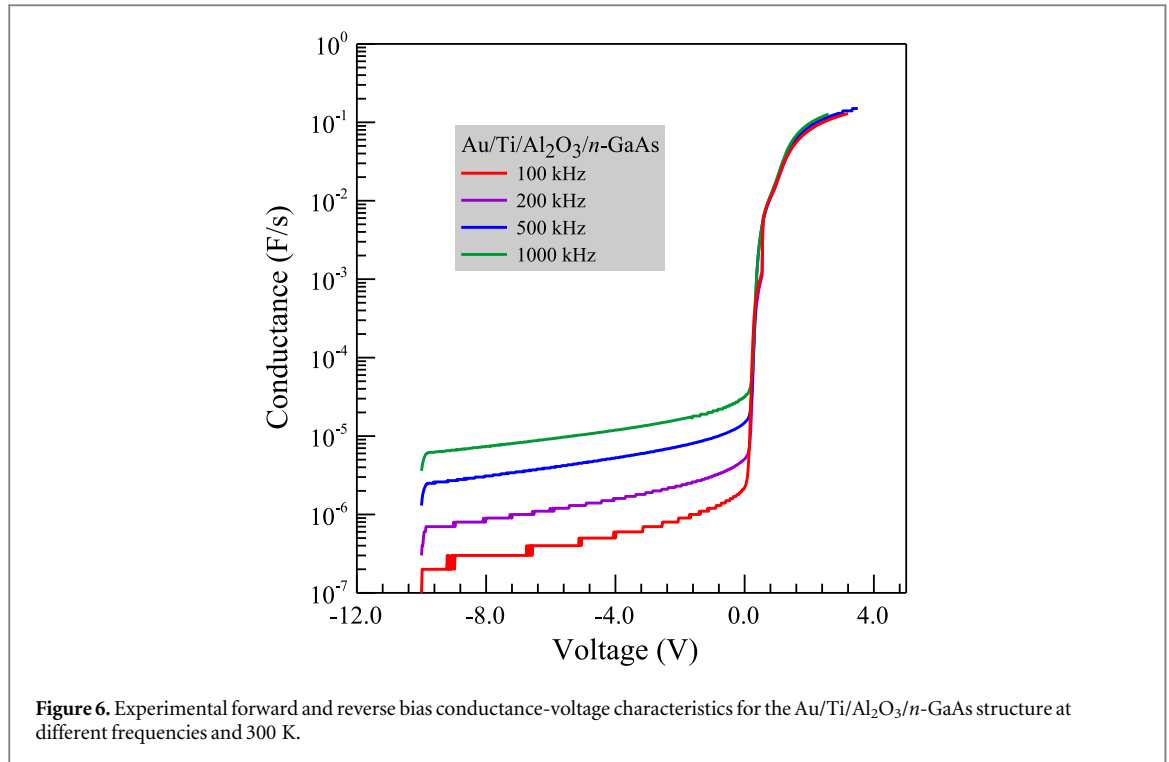
Again, as can be seen from figure 3, the capacitance of the device is independent of the measurement frequency under the reverse bias (0.0 V to −10 V), that is, there is almost no frequency dispersion in the reverse bias. Figure 4 shows the phase angle versus bias voltage curves for the device at different frequencies at the room temperature. The phase angle is always 90° from −10 V to 0.0 V in the reverse bias branch, and it suddenly decreases at 0.0 V and then approaches 0° from 0.0 V to 4.0 V in the forward branch. The case clearly indicates that the diode behaves more capacitively at the reverse bias region rather than the forward bias region [51]. Figure 5 shows the impedance modulus (*Z*) versus bias voltage curves for the device at different frequencies at room temperature. It has been observed that the impedance modulus depends on frequency and bias at the reverse bias while it is frequency-independent and strongly bias-dependent for the forward bias, that is, the impedance modulus decreases with increasing frequency at a given reverse bias, and decreases with increasing bias independently of frequency by coinciding (overlap) with each other from about 0.6 V to 4.0 V at the forward bias. Figure 6 shows the conductance (*G*) versus bias voltage curves for the device at different frequencies at room temperature. The conductance is frequency-dependent and bias-dependent for the reverse bias while it is frequency-independent and strongly bias-dependent at the forward bias, that is, the conductance increases with decreasing frequency at a given reverse bias, and increases with increasing bias as independent of frequency by coinciding with each other from about 0.0 V to 4.0 V for the forward bias. The impedance modulus and conductance values at 0.0 V and −10 V are given in table 1 for different frequencies. It can be clearly seen from values at 0.0 V and −10 V in table 1 how the impedance modulus and conductance values change depending on frequency and bias voltage. This behavior indicates that the device has the same series resistance value at a given forward bias voltage for all frequencies, as can be seen in table 1, thus the conductance data confirm the impedance modulus data in the forward and reverse bias regime. The series resistance expression of the MIS devices is given by [3]



$$R_s = \frac{G_m}{G_m^2 + \omega^2 C_m^2}, \quad (6)$$

where G_m and C_m are the experimental conductance and capacitance values from the strong accumulation region for each frequency. The series resistance of the device is obtained using G_m and C_m values given in table 1 in equation (6). As can be seen in table 1, the series resistance value of the device for each frequency approximately equals 5Ω .

In C - V measurements, the charges at the interface states cannot follow the ac signal at very high frequencies [40–62], and the equivalent circuit of device will be just the interfacial layer and depletion (the space charge region) capacitance in series. At very high frequency, the total capacitance, C , per area unit of MIS diode is a



series combination of the depletion capacitance of the semiconductor C_D and the capacitance of the interfacial layer C_{ox} , and thus the total capacitance C is represented by [27–30, 45–50]

$$\frac{1}{C} = \frac{1}{C_D} + \frac{1}{C_{ox}}, \quad (7)$$

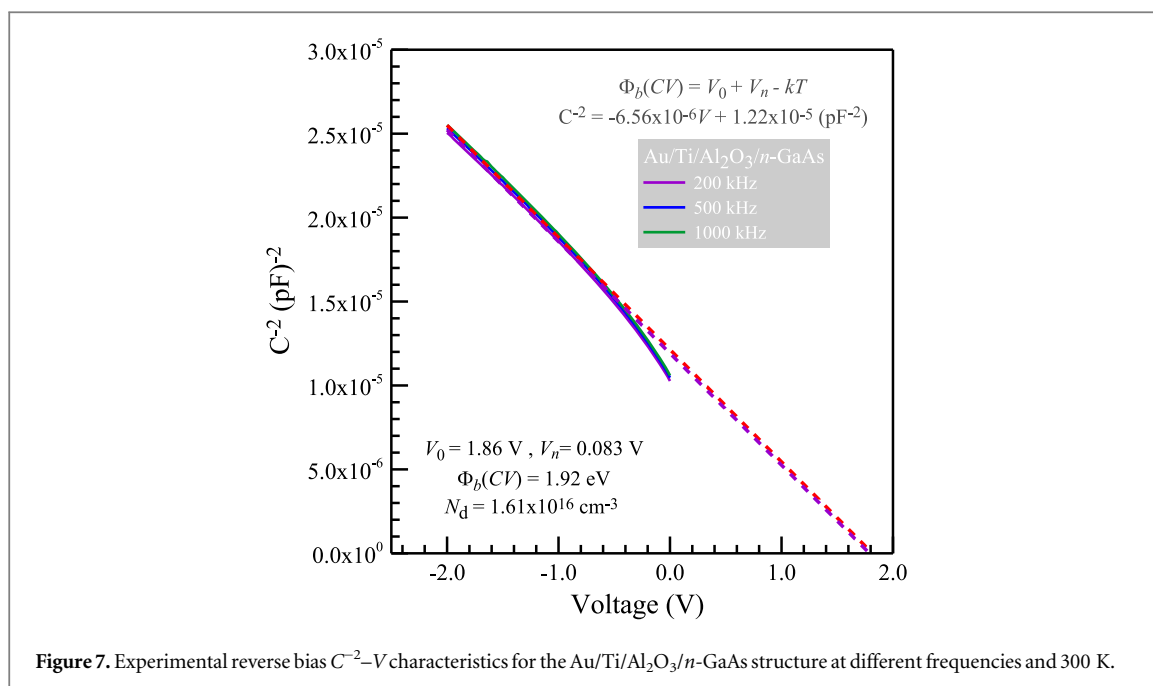
C_{ox} is the capacitance of the interfacial layer and corresponds to the maximum capacitance of the MIS diode, and C_D depends on the bias voltage. It has been stated above that the $C-V$ curve has an accumulation region at positive voltage at the right side which gives the capacitance of the insulator [27–30], as can be seen from figures 1 or 3. A depletion capacitance forms near the semiconductor surface from the positive voltage to negative, or as the positive voltage is reduced sufficiently, and the total capacitance decreases because the depletion region acts in series with the interfacial insulator layer [27–30]. Thus, in this case, it can be said that the negative voltage region in figures 1 and 3 corresponds to the deep depletion condition [3, 27–30]; the depletion capacitance C_D can approximately be given by [27–30, 46–50]

$$\frac{1}{C_D^2} = \frac{2(\Phi_{b0}^{CV} - V - V_n)}{q\epsilon_s N_d A^2}, \quad (8)$$

where V_n is the potential difference between the Fermi level and the conduction band minimum in the neutral region of n -type semiconductor, $(\Phi_{b0}^{CV} - V_n) = V_{D0}$ is the diffusion potential at the zero bias, N_d is the doping concentration of the n -type semiconductor, ϵ_s is the permittivity of the semiconductor, q is the electronic charge and A is the diode area. Figure 7 shows the experimental reverse bias $C^{-2}-V$ characteristics for the Au/Ti/Al₂O₃/n-GaAs structure at various frequencies and 300 K. As can be seen from equation (7), the C^{-2} versus V plot is a straight line whose intercept with V axis gives the value of $V_0 = V_{D0}$, and the slope gives the value of N_d . N_d can be given as follows:

$$N_d = \frac{2}{q\epsilon_s A^2} \frac{dV}{d(C^{-2})}. \quad (9)$$

The values of $V_0 = 1.86$ V, $V_n = 0.083$ V, $\Phi_{b0}^{CV} = 1.92$ V and $N_d = 1.61 \times 10^{16}$ cm⁻³ were obtained from the experimental reverse bias $C^{-2}-V$ plot. As can be seen from the obtained barrier height values, there is an appreciable difference between the barrier height values obtained $I-V$ and $C-V$ characteristics. That is, the barrier height value from $I-V$ characteristics is much lower than that from the $C-V$ characteristics. Likewise, the experimental carrier concentration value of $N_d = 1.61 \times 10^{16}$ cm⁻³ from $C-V$ characteristics is significantly higher than the value of 7.43×10^{15} cm⁻³ given for the n -GaAs used this study. The barrier height and carrier concentration change in the MS contacts with the interfacial layer depends on the position of the Fermi level and interface-state density. The change in positive or negative interface charge will affect the depletion layer of the



semiconductor, and therefore the Fermi-level position. In the absence of the interface states, the negative charge on the metal surface must be equal to the positive space charge due to the neutrality condition. The increase in the barrier height and carrier concentration is evidence for the presence of the negative interface charge, and thus for the positive space charge increase due to the neutrality condition [30, 55, 56].

4. Conclusion

It has been seen that the MIS structure with a high- κ the Al₂O₃ gate dielectric that we have grown by the ALD on the n-GaAs substrate exhibits excellent electrical properties, that is, the structure has shown almost no hysteresis over the whole bias region and no frequency dispersion in the reverse bias C - V curves for all frequencies. This film appears to be a very promising high- κ gate dielectric with very thin film of about 3 nm for future ultra-large scale integration devices.

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