

Optimal xylem efficiency

1 Optimal balancing of xylem efficiency and safety explains 2 plant vulnerability to drought

3 4 **Authors:**

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14 Summary

- 15 • In vast areas of the world, the growth of forests and vegetation is water-limited and plant
16 survival depends on the ability to avoid catastrophic hydraulic failure. Therefore, it is remarkable
17 that plants take high hydraulic risks by operating at water potentials (ψ) that induce partial
18 failure of the water conduits (xylem). Here we present an eco-evolutionary optimality principle
19 for xylem conduit design that explains this phenomenon.
- 20 • Based on the hypothesis that conductive efficiency and safety are optimally co-adapted to the
21 environment, we derive a simple relationship between the intrinsic tolerance to negative water
22 potential (ψ_{50}) and the environmentally dependent minimum xylem ψ .
- 23 • This relationship is constrained by a physiological tradeoff between xylem conductivity and
24 safety, which is relatively strong at the level of individual conduits although it may be weak at
25 the whole sapwood level. The model explains observed variation in ψ_{50} both across a large
26 number of species, and along the xylem path in two species. The larger hydraulic safety margin
27 in gymnosperms compared to angiosperms is explained as an adaptation to the gymnosperms'
28 lower capacity to recover from conductivity loss.
- 29 • The constant xylem safety factor provides a powerful principle for simplifying and improving
30 plant and vegetation models.

31

32 **Keywords:** xylem, hydraulic system, vessels, tracheids, optimality, adaptation, water transport,
33 conductance

34

35 Introduction

36 The hydraulic properties of plants constrain their ability to grow and survive in different environments.
37 Therefore, a solid understanding of these constraints is essential for accurate prediction of vegetation
38 responses to droughts and other environmental changes. In stems, the primary function of the xylem is
39 to transport water through the stem, driven by the difference in water potential between the base and
40 the top. The conductivity of the xylem increases steeply with the conduit diameter as long as it is not
41 hampered by cavitation, or embolism, which happens when water potential is too low (too highly
42 negative). The sensitivity to cavitation is often measured in terms of the water potential at which
43 conductivity is reduced by 50%, ψ_{50} . Across a large number of species, ψ_{50} is, on average, close to the
44 minimum midday water potential (ψ_{min}) experienced by each species, implying a remarkably small

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45 hydraulic safety margin ($\psi_{50} - \psi_{min}$) (Choat *et al.*, 2012). The safety margin is lower for angiosperms than
46 gymnosperms and is smallest in wet sites with high ψ_{min} . However, the reason for this apparently risky
47 strategy and its variation with climate are not yet fully understood, despite the importance for our
48 understanding of plant responses to expected climate changes and droughts (Venturas *et al.*, 2017).
49 Here we aim to explain the variation in ψ_{50} through an eco-evolutionary-optimality perspective.

50
51 Eco-evolutionary optimality (EEO) approaches have been used to model a wide range of plant traits and
52 processes (Franklin *et al.*, 2020), including plant stomatal hydraulic regulation (Hölttä *et al.*, 2011; Wolf
53 *et al.*, 2016; Anderegg *et al.*, 2018; Wang *et al.*, 2020), vascular network structure (McCulloh *et al.*, 2003;
54 Savage *et al.*, 2010; Koçillari *et al.*, 2021), and leaf hydraulic and photosynthetic traits (Deans *et al.*,
55 2020). Xylem efficiency and safety in relation to growth environment has only rarely been addressed
56 from an EEO perspective, perhaps due to a lack of consensus on the xylem costs and benefits. For
57 example (Manzoni *et al.*, 2013) used an EEO approach based on the principle that transpiration is
58 maximized, which contrasts to the assumption in most other models that transpiration is a cost (Wang
59 *et al.*, 2017). Furthermore, although a tradeoff balancing xylem conductivity (benefit) and vulnerability
60 (cost) is expected to constrain optimal xylem function, recent studies suggest that this tradeoff is weak
61 (Gleason *et al.*, 2016; Sanchez-Martinez *et al.*, 2020; Liu *et al.*, 2021). Nevertheless, such a tradeoff is
62 invoked in the EEO-based widened pipe model explaining the stem tip to base widening of conduits
63 (Koçillari *et al.*, 2021).

64
65 Here we first show that the xylem efficiency-safety tradeoff is important at the level of conduits, even
66 though it is weaker at the level of whole sapwood tissue. Then, we combine this tradeoff with an EEO
67 hypothesis which states that plants maximize the combination of xylem conductive capacity per unit
68 conduit biomass and tolerance to low ψ . Since conductivity loss is not always reversible (Anderegg *et al.*,
69 2013; Pellizzari *et al.*, 2016) we further extend the vulnerability concept to account for accumulation of
70 irreversible conductivity loss. Our first-principles EEO-based model successfully explains the globally
71 observed relationship between ψ_{50} and the environmentally dependent ψ_{min} , and how it differs between
72 angiosperms and gymnosperms.

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74 Model description and results

75 The conduit conductivity – safety tradeoff

76 The xylem can be seen as a network of interconnected conduits (vessels or tracheids). Xylem
77 conductivity and safety (tolerance to negative water potential, ψ_{50}) depends on both the conduits
78 themselves and their interconnections, the pits and end-walls, and how the conduits are spatially
79 clustered (Lens *et al.*, 2011). The hydraulically weighted conduit diameter (D) is an important
80 determinant of conductivity due to the strong effect on fluid dynamics (Hacke *et al.*, 2017), which is also
81 reflected in the ubiquitous tapering of conduits with stem height which serves to minimize the increase
82 in resistance with path length (West *et al.*, 1999). Following the Hagen–Poiseuille equation, the
83 hydraulic conductivity (maximal conductive capacity, K) of conduits increases with the 4th power of the
84 conduit diameter (D):

$$85 \\ 86 K = c_1 D^4 \quad (1)$$

87
88 The symbol c_1 in eq. 1, and $c_2 \dots c_6$ in the further equations, denote constants that do not matter for our
89 final results.

90
91 Xylem safety can be described by a vulnerability function (P), which describes how sapwood conductivity
92 declines with negative xylem water potential ψ . Among commonly used xylem vulnerability functions,
93 the Weibull function (eq. 2) has the advantages that it always approaches 1 as $\psi \rightarrow 0$ and that its
94 parameter a does not vary significantly with ψ_{50} (Duursma & Choat, 2017).

$$95 \\ 96 P = \left(\frac{1}{2}\right)^{\left(\frac{\psi}{\psi_{50}}\right)^a} \quad (2)$$

97
98 In eq.2, ψ_{50} is ψ that causes 50% loss of conductivity, which is a genetically determined functional trait
99 (Lamy *et al.*, 2014; Lobo *et al.*, 2018; Pritzkow *et al.*, 2020), evolutionarily adapted to the environmental
100 conditions experienced by a species. The parameter a controls the shape of P , and was estimated based
101 on relationship between ψ_{50} and ψ_{88} for each species using the data in (Choat *et al.*, 2012) (Appendix).
102 For angiosperms mean $a=2.48 \pm 0.15$ ($n=153$) and for gymnosperms mean $a=5.34 \pm 0.40$ ($n=29$), where \pm
103 denotes SE.

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105 The relative importance of different underlying traits in determining ψ_{50} varies among studies and
106 species, e.g. pit features and vessel length being most important in *Acer* species (Lens *et al.*, 2011) while
107 D and vessel grouping are important in other species (Scholz *et al.*, 2013; Levionnois *et al.*, 2021). Across
108 species, there is an inverse relationship between safety and D (eq. 3, where $d < 0$), which is strong in
109 some studies e.g. (Sperry *et al.*, 2006; Hacke *et al.*, 2015) and weaker, but significant, across multiple
110 studies combined (Hacke *et al.*, 2017). Thus, although xylem conductivity and safety are determined by
111 different traits in different species, across species D emerges as a reasonable proxy for conduit-level
112 conductivity and safety. From an eco-evolutionary standpoint, a coordination between D and other
113 xylem traits should be expected in order to avoid inefficiencies and bottlenecks in the conductive system
114 as a whole. Furthermore, D is not only linked to xylem conductivity and safety, but also influences
115 conduit wall thickness and the construction cost of conduits, which all together suggests that D should
116 be subject to a strong selection pressure (Koçillari *et al.*, 2021).

117

$$118 \quad \psi_{50} = -c_2 D^d \quad (3)$$

119

120 We estimated d in eq. 3 based on the data in (Sperry *et al.*, 2006) using linear regression of $\ln(\psi_{50})$
121 versus $\ln(D)$. For angiosperms $d = -1.20 \pm 0.14$, $r^2 = 0.72$ ($n=29$) and for gymnosperms $d = -1.32 \pm 0.63$, $r^2 =$
122 0.39 ($n=18$). Although other datasets may yield slightly different values of d , e.g. mean $d = -0.77$ in
123 angiosperms for (Hacke *et al.*, 2017), this would only have minor quantitative effects on the results as
124 long as $d < 0$.

125

126 Because both K and ψ_{50} depend on D , eqs. 1 and 3 can be combined into eq. 4, which represents a
127 conduit-level tradeoff between conductive capacity (K) and safety (ψ_{50}).

128

$$129 \quad K = -c_3 \psi_{50}^{4/d} \quad (4)$$

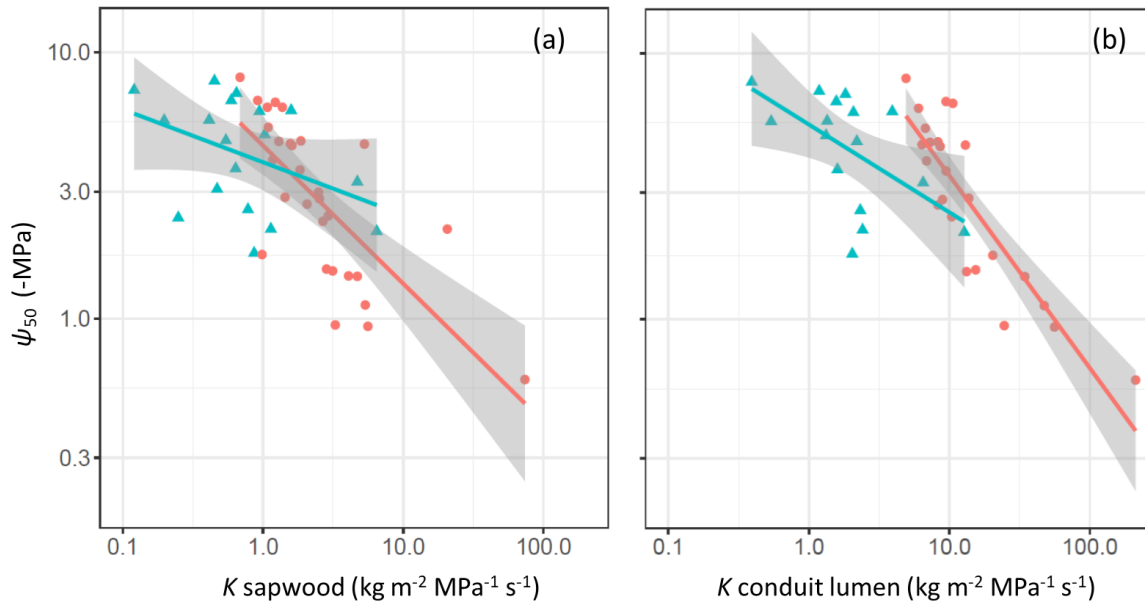
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131 This tradeoff (eq. 4) is defined at the level of conductive tissue (or equivalently, probabilistically at the
132 individual-conduit level) rather than for whole-sapwood tissue. We emphasize that whole-sapwood
133 conductance also depends on the number of conduits per unit sapwood area which weakens this
134 tradeoff at the whole-plant level (Fig. 1).

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138 **Fig. 1 Tradeoff between xylem tolerance to negative water potential (ψ_{50}) and maximal conductive capacity (K).**

139 Panels show measurements for whole sapwood (a) and for conduits only (b). Points show observations of
140 angiosperms (red circles) and gymnosperms (blue triangles) and lines show SMA regressions with SE bands, where
141 $r^2=0.54, 0.16$ for sapwood (a) and $r^2=0.76, 0.32$ for conduits (b), for angiosperms ($n=29$) and gymnosperms ($n=18$),
142 respectively. Data from (Sperry *et al.*, 2006).

143

144 Measured vulnerability curves represent the instantaneous loss of conductivity (cavitation) but do not
145 say anything about its reversibility and long-term costs. Conductivity losses are not always reversible
146 (Anderegg *et al.*, 2013; Pellizzari *et al.*, 2016), which means that consecutive loss events multiply. In this
147 case the total remaining conductivity (P_t) can be described as:

148

$$149 P_t = P \cdot P \cdot \dots = P^i \quad (5)$$

150

151 In eq 5, i determines the degree of loss accumulation (irreversibility). If $i=1$, there is no accumulation of
152 effects; if $i=2$, the fitness-costs of the accumulated loss of conductivity is equal in magnitude to the
153 short-term effects; if $i > 2$, the accumulated (long-term) effects are larger than the instantaneous
154 effects.

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156 Optimal adaptation of conduit efficiency and safety

157 The higher the conductance of water through the xylem, the larger the stomatal conductance and
158 carbon uptake can be. Thus, everything else being equal, higher xylem conductance increases fitness.
159 Further, to make the most of acquired resources, all plant organs should be constructed with maximal
160 efficiency, i.e., their function (or fitness contribution) per resources invested should be maximized. The
161 benefit of the xylem is water transport and the costs accrue from the structural investment in fibers and
162 lignified tissues required to build xylem walls (Sperry, 2003). Thus, optimal xylem conduits should have a
163 high conductivity (K) per unit mass (M), i.e. conductive efficiency (K/M).

164
165 Conduit mass depends on diameter, wall thickness (T), and wall tissue density (ρ). Biophysical
166 considerations, supported by empirical observations (Hacke *et al.*, 2001; Sperry *et al.*, 2006), indicate
167 that for conduit walls to withstand negative pressure without imploding, the ratio of conduit wall
168 thickness to conduit diameter (T/D) scale with ψ_{50} according to eq.6 (Hacke *et al.*, 2001).

169
170
$$\psi_{50} = -c_4 (T/D)^2 \tag{6}$$

171
172 The mass per unit length of a conduit (M , eq. 7) can be approximated (by neglecting the difference
173 between outer and inner conduit diameter) by $\pi \cdot D \cdot T \cdot \rho$ and be expressed in terms of ψ_{50} using eqs. 6
174 and 3. The approximation introduces only a minor error in optimal ψ_{50} at highly negative values of ψ_{min}
175 (1.5% at ψ_{min} -10 MPa).

176
177
$$M = \pi D T \rho = -c_5 \psi_{50}^{1/2+2/d} \tag{7}$$

178
179 In addition to having a high conductivity per mass, optimal conduits should tolerate low ψ with minimal
180 risk of conductivity loss (cavitation), i.e. P (eq. 2) should be as large as possible at the minimum
181 operating water potential (ψ_{min} , the lowest ψ measured for a given site and species). Since ψ_{min} reflects
182 the integrated effect of water flux constraints due to environmental factors and plant stomatal
183 behaviour, it exerts a strong selective force on the xylem (Bhaskar & Ackerly, 2006). Combining the two
184 criteria for optimal xylem function - high conductive efficiency and high tolerance to low ψ – in the most
185 parsimonious way, we obtain the optimality criterion, or fitness proxy, $F = \frac{K}{M} \cdot P_t(\psi = \psi_{min})$. Based on
186 eqs. 2, 4, 5 and 7, F can be expressed as a function of ψ_{50} (eq.8).

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$$188 \quad F = \frac{K}{M} P_t = -c_6 \psi_{50}^{\frac{2}{d}-\frac{1}{2}} \left(\frac{1}{2}\right)^i \left(\frac{\psi_{min}}{\psi_{50}}\right)^a \quad (8)$$

189

190

191 The optimal ψ_{50} results from the tradeoff between increased conductive capacity per unit conduit
192 biomass and increased vulnerability with increasing ψ_{50} (Supplementary Fig. S1). F is maximized when dF
193 $/d\psi_{50} = 0$, which results in an optimal ψ_{50}^* that is proportional to ψ_{min} (eq. 9, derivation in Appendix).

$$194 \quad \psi_{50}^* = \psi_{min} \left(\frac{2 a \ln(2) i d}{d-4}\right)^{\frac{1}{a}} \quad (9)$$

195

196 In agreement with observations, eq. 9 implies a linear relationship between ψ_{min} and ψ_{50} with zero
197 intercept, i.e. a constant ratio, or safety factor ψ_{50}/ψ_{min} (Fig. 2). For angiosperms, the observed mean
198 safety factor (0.92) is almost identical to the predicted (0.91) for the model without accumulation of
199 conductivity losses ($i = 1$). For gymnosperms, the observed safety factor is 1.7, which can be explained by
200 the model with conductivity loss accumulation ($i \neq 1$). For this model, i was estimated based on the
201 observations, resulting in $i = 0.99 \pm 0.057$ (not significant different from 1) for angiosperms and $i = 9.28 \pm$
202 1.94 for gymnosperms, indicating that gymnosperms are much more sensitive to conductivity loss
203 accumulation than angiosperms. The difference in i was the main explanation for the higher safety
204 factor in gymnosperms than in angiosperms, whereas the slightly steeper conductivity-safety tradeoff
205 (lower d) and the steeper slope of vulnerability function (due to larger a) explained 22% of the effect. In
206 addition to the interspecies variation, the model also explains the increase in negative ψ_{50} with ψ_{min}
207 along the hydraulic path from roots to branches in two gymnosperm species (Fig. 2c).

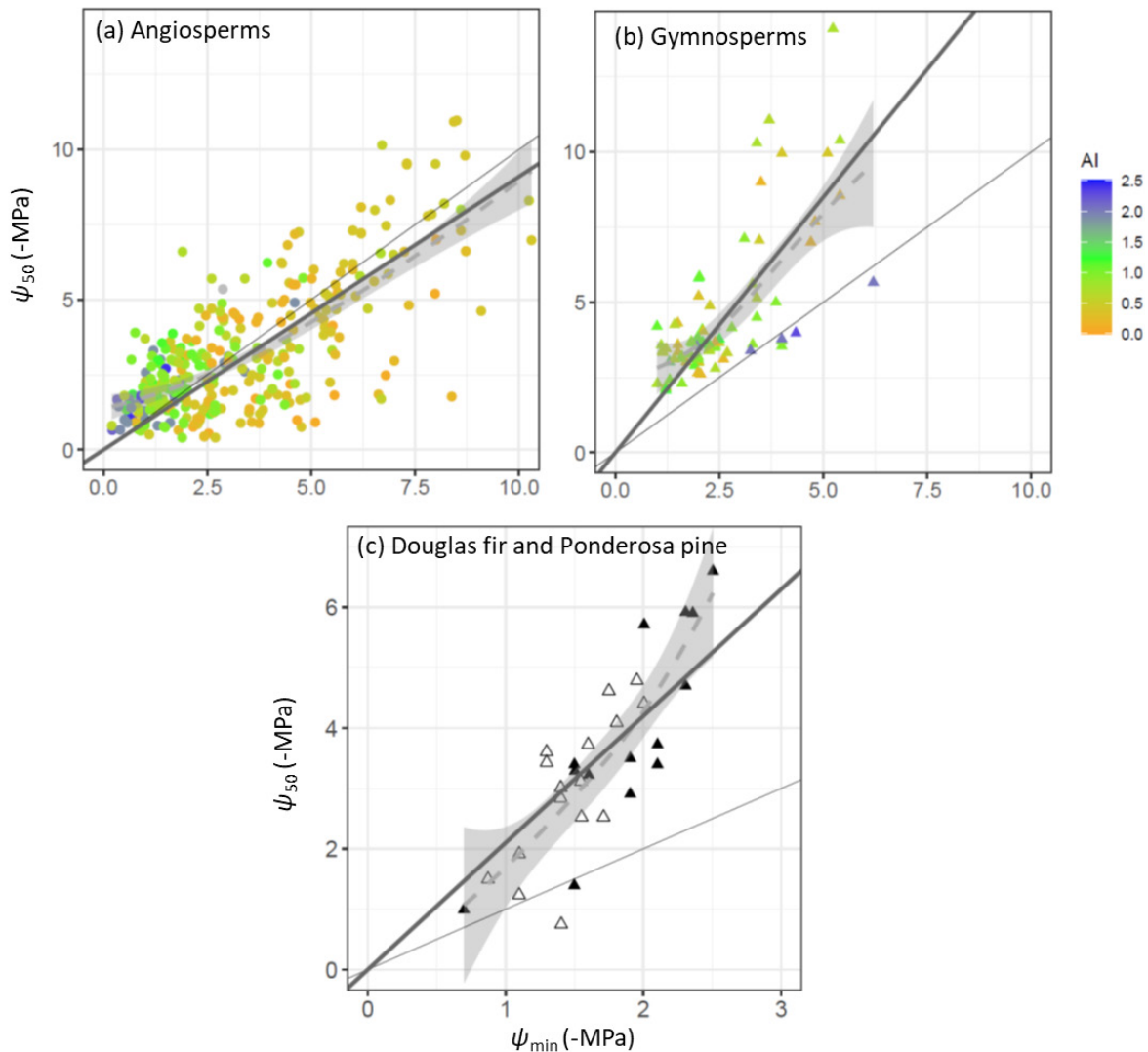
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213 **Fig. 2. Observed and modelled xylem tolerance to negative water potential (ψ_{50}) versus minimum plant water**
214 **potential (ψ_{min}).** (a and b) Measurements in terminal branches for different species and sites (Liu *et al.*, 2019),
215 where colors indicate site aridity index (AI) from arid (orange) to wet (blue). Symbol shape indicates angiosperms
216 (a, circles) and gymnosperms (b, triangles). (c) Measurements (means of 5-6 individuals) along the hydraulic path
217 from roots, trunks and branches in Douglas fir (closed triangles) and Ponderosa pine (open triangles) (Domec *et al.*,
218 2009). The dashed lines with shading show smoothed mean and SE intervals of the observed relationships. The
219 straight thick lines are the model predictions (eq. 9). The thin black line is the 1:1 line. Modeled versus observed r^2
220 was 0.64 for Douglas fir and Ponderosa pine ($n=30$), 0.51 for angiosperms ($n=338$), and 0.48 for gymnosperms ($n =$
221 83).

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223 Importantly, the proposed optimality principle defines the intrinsic properties of conduit tissue but does
224 not determine whole sapwood or whole stem conductance. In a whole plant perspective, the principle
225 of optimal conductive efficiency operates at the lowest organizational level, i.e. the level of conduit
226 tissue. Higher-level organizational principles of xylem function are not alternative but complementary to
227 our tissue level principle. While other principles control the variation in xylem structure with plant
228 height or variation in behavioral strategies, optimal conduit efficiency and safety is always maintained at
229 the conduit level. For example, while our principle determines ψ_{50} and D at the top of stem, the widened
230 pipe model predicts the relative increase of D and decrease of ψ_{50} towards the base (Koçillari *et al.*,
231 2021).

232

233 Discussion

234 It was previously not explained why so many plants operate with such a small safety margin ($\psi_{50} - \psi_{min}$).
235 Our model explains why this is the case – it is the optimal combination of conductive capacity per
236 biomass (K/M) and tolerance to the lowest ψ experienced by a plant in its environment. The variation in
237 conductive capacity (K) relative to low ψ tolerance is constrained by an intrinsic physiological tradeoff
238 linked to conduit diameter (D). Importantly, this tradeoff is most relevant at the level of conductive
239 tissue only rather than for the whole sapwood (Fig. 1). Weak tradeoffs observed at the whole-sapwood
240 level (Gleason *et al.*, 2016) may be caused by the large variability among species in the number of
241 conduits per sapwood area (Zanne *et al.*, 2010) and the associated variation in conductivity. Although
242 vulnerability is often more strongly linked to pit- and other traits than to D within groups of similar
243 species, across a wide range of species D provides a proxy for vulnerability that allows us to link it to
244 xylem conductivity and construction costs. The relevance of optimal adaptation of D based on a
245 conductive efficiency – safety tradeoff is further supported by its success in predicting the relative tip to
246 base widening of D across species (Koçillari *et al.*, 2021).

247

248 The model further provides a theoretical explanation and quantification of the previously observed
249 general increase in the hydraulic safety margin with increasingly negative ψ_{min} (Meinzer *et al.*, 2009;
250 Choat *et al.*, 2012), which results in a constant safety factor (ψ_{50} / ψ_{min}) across species of the same type
251 (Fig. 2). Although relevant observations of variation in ψ_{min} and ψ_{50} within individuals are yet limited, the
252 available data suggest that the same optimality principle determines ψ_{50} both across different species
253 and sites and along the xylem flow path within individuals (Fig. 2).

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255 Our simple theoretical model is limited by the few traits explicitly accounted for, not including variation
256 in capacitance, vessel grouping, and pit structure. However, because consistent data on such additional
257 traits are not widely available across species, adding more traits in the model is unlikely to improve its
258 performance, already explaining 50% of the variation in ψ_{50} across species. Whereas the model captures
259 well the overall trends in ψ_{50} , ψ_{50} for less negative ψ_{min} (wet sites) is more negative than predicted by
260 the model (Fig. 2a, b). This bias could be related to an under-estimation of negative ψ_{min} at wetter sites
261 owing to lower sampling of rare dry days at such sites compared to more frequently occurring dry days
262 at drier sites. Plants at wetter sites may be adapted to infrequent drought events which may be missed
263 in the sampling of ψ_{min} (Martinez Vilalta *et al.*, 2021).

264

265 The model accurately predicts the observed mean safety factor $\psi_{50}/\psi_{min} = 0.92$ in angiosperms, without
266 including irreversible or accumulating loss of conductivity. This may be related to the ability of
267 angiosperms to actively reverse embolism due to the presence of sieve tubes and companion cells in
268 their parenchyma (Johnson *et al.*, 2012; Kiorapostolou *et al.*, 2019). The much higher mean safety factor
269 in gymnosperm $\psi_{50}/\psi_{min} = 1.7$ indicates an adaptation to accumulating effects of conductivity loss and a
270 low reversal capacity (high i). A negative relationship between safety factor and embolism reversal
271 capacity is supported by previous observations (Ogasa *et al.*, 2013). The importance of irreversible
272 effects of conductivity loss for gymnosperms is further supported by the observations of a low lethal
273 negative ψ close to ψ_{50} (Liang *et al.*, 2021).

274

275 The invariant ψ_{50}/ψ_{min} ratio predicted by our theory suggests that the presence of larger conduit
276 diameters in taller plants (Olson *et al.*, 2018) does not necessarily mean that they operate at a higher
277 risk compared to shorter plants. Rather, our hypothesis suggests that taller plants with higher ψ_{50} should
278 also have higher ψ_{min} than shorter plants, which is in agreement with observations across a large
279 number of species and environments (Liu *et al.*, 2019). In a growing tree with increasing conduit
280 diameter, optimal ψ_{50}/ψ_{min} ratio could be maintained by increasing whole xylem conductivity through
281 additional conduits, more conservative stomatal regulation, or by means of increased water uptake with
282 deeper roots, i.e. drought avoidance (Brum *et al.*, 2017; Oliveira *et al.*, 2021). Nevertheless, if these
283 compensatory mechanisms are hampered by severe drought, taller trees would still suffer more than
284 shorter trees (Rowland *et al.*, 2015).

285

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286 In conclusion, our results show that apparent risky hydraulic behavior of plants can be explained by an
287 eco-evolutionarily optimal design of xylem conduits, constrained by a strong xylem efficiency – safety
288 tradeoff at the scale of individual conduits. ψ_{50} is universally proportional to ψ_{min} , corresponding to a
289 constant mean safety factor $\psi_{50} / \psi_{min} \approx 0.9$ and 1.7 for angiosperms and gymnosperms, respectively.
290 The large safety factor in gymnosperms is likely an adaptation to their small capacity to recover from
291 loss of conductivity compared to angiosperms. The constant safety factor holds across environments
292 and species, and potentially also within individual trees, and thus provides a powerful principle for
293 simplifying and improving plant and vegetation models.

294
295

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433 [Author contributions](#)

434 O.F. conceived the original idea, analyzed the data, and wrote the draft manuscript. J.J. and P.F.
435 contributed complementary mathematical analyses. F.H. and J.J. provided complementary data. All
436 authors contributed to conceptual development and the final manuscript.

437

438

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439 Appendix

440 Mathematical derivations

441 Derivation of optimal ψ_{50}

442 The combined conductive efficiency and safety (F) is given by eq.8, as illustrated in Fig. A1.

$$443 \quad F = \frac{K}{M} P = -c_5 \psi_{50}^{\frac{2}{d}-\frac{1}{2}} \left(\frac{1}{2}\right)^i \left(\frac{\psi}{\psi_{50}}\right)^a$$

444

445 Maximization of F with respect to ψ_{50} implies that

$$446 \quad \frac{\partial F}{\partial \psi_{50}} = 0 \text{ and that } \frac{\partial \ln(F)}{\partial \psi_{50}} = 0.$$

447

$$448 \quad \ln(F) = \ln(c_5) + \left(\frac{2}{d} - \frac{1}{2}\right) \ln(\psi_{50}) + i \left(\frac{\psi}{\psi_{50}}\right)^a \ln\left(\frac{1}{2}\right)$$

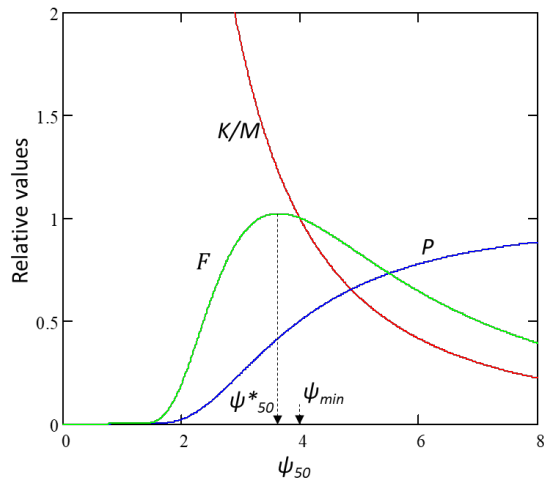
449 $\frac{\partial \ln(F)}{\partial \psi_{50}} = \left(\frac{2}{d} - \frac{1}{2}\right) + i \left(\frac{\psi}{\psi_{50}}\right)^a a \ln(2) = 0$, which is solved for ψ_{50} to yield optimal ψ_{50} (ψ_{50}^*) as a function

450 of $\psi = \psi_{min}$:

$$451 \quad \psi_{50}^* = \psi_{min} \left(\frac{2 a \ln(2) i d}{d-4}\right)^{\frac{1}{a}} \text{ (eq. 9)}$$

452

453



454

455 **Fig A1.** Optimal ψ_{50}^* resulting from maximization of $F = \frac{K}{M} \cdot P$ (eq. 8), where $\frac{K}{M}$ (red line) and F (green

456 line) are shown normalized with respect to their values at $\psi_{50} = \psi_{min}$.

457

458

459 Calculation of the parameter a in the vulnerability function

460 ψ_{88} corresponds to 88% loss of conductivity, which is inserted into the vulnerability function P (eq. 2),

461 which is solved for a .

$$462 \quad P(\psi = \psi_{88}) = 1 - 0.88 = 0.12 = \left(\frac{1}{2}\right)^{\left(\frac{\psi_{88}}{\psi_{50}}\right)^a}$$

463

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$$a = \frac{\ln\left(\frac{-\ln(0.12)}{\ln(2)}\right)}{\ln\left(\frac{\ln(\psi_{88})}{\ln(\psi_{50})}\right)}$$

464

465