

Hydrological drivers of bedload transport in an Alpine watershed

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Key-points

- A streamflow time-series is analyzed to quantify the contribution of rainfall, snow-melt, and their co-occurrence onto bedload transport.
- The co-occurrence of rainfall in a watershed where the snow-melt signal is strong is the dominant driver of bedload transport (77%).
- Rainfall occurring once the snow-melt signal is gentler also represents a substantial contribution to annual bedload (9%).

Abstract

Understanding and predicting bedload transport is an important element of watershed management. Yet, predictions of bedload remain uncertain up to several order(s) of magnitude. In this contribution, we use a five-year continuous time-series of streamflow and bedload transport monitoring in a 13.4 km² snow-dominated Alpine watershed in the Western Swiss Alps to investigate the hydrological drivers of bedload transport. Following a calibration of the bedload sensors, and a quantification of the hydraulic forcing of streamflow upon bedload, a hydrological analysis is performed to identify daily flow hydrographs influenced by different hydrological drivers: rainfall, snow-melt, and mixed rain and snow-melt events. We then quantify their respective contribution to bedload transport. Results emphasize the importance of mixed rainfall and snow-melt events, for both annual bedload volumes (77% in average) and peaks in bedload transport rate. Results further show that a substantial amount of bedload transport may occur during late summer and autumn storms, once the snow-melt contribution and baseflow have significantly decreased (9% of the annual volume in average). Although rainfall-driven changes in flow hydrograph are responsible for a large majority of the annual bedload volumes (86%

in average), the identified melt-only events also represents a non-negligible contribution (14 % in average). Through a better understanding of the bedload magnitude-frequency under different hydrological conditions, the results of this study may help to improve current predictions of bedload transport, and we further discuss how bedload could evolve under a changing climate through its effects on Alpine watershed hydrology.

Plain language summary

Understanding and predicting bedload transport is an important element of watershed management. Yet, it remains a challenge to predict bedload transport accurately. In this paper, we profit from a rare five-year continuous time-series of streamflow and bedload transport in a 13.4 km² snow-dominated Alpine watershed in the Western Swiss Alps to investigate the hydrological drivers of bedload transport. An analysis of the streamflow time-series together with meteorological data allows us to classify daily flow hydrographs over the five years of observation between rainfall-driven, melt-driven, and a mixed of both, and to quantify their contribution with regards to bedload transport. Results of the study show that mixed rainfall and snow-melt events with high baseflow are the dominant driver of bedload transport (77% of annual bedload in average), followed to a lower extent by rainfall occurring in the late summer and autumn (9% of annual bedload in average), when the melt contribution and baseflow are lower. Through a better understanding of hydrological drivers, the results of this study may help improving current predictions of bedload, transport and question how bedload transport could evolve under a changing climate through its effects on Alpine watershed hydrology.

Key-words

Bedload transport; Alpine watershed; Hydrological drivers; Rainfall; Snow-melt; Climate change.. **Introduction**

Bedload transport in Alpine watersheds is a serious natural hazard, which can be costly in economic terms and potential loss of life (e.g. Badoux et al., 2016, 2014a). It often requires river engineering and represents a challenge for land-use planning (e.g. Heritage et al., 2019; Sims and Rutherford, 2017) and hydropower production (e.g. OFEV, 2021; Pralong et al., 2015; Speerli et al., 2020). It also has a direct impact on the ecology of river systems (Badoux et al., 2014b; FOEN, 2021; Gabbud et al., 2019; Hauer et al., 2018; Lane et al., 2020; Wang et al., 2014). Not only are these aspects currently of great concern, but so are their future with regards to the evolution of bedload dynamics under a rapidly changing climate.

Despite decades of development of bedload transport models, best estimates of bedload transport rates still suffer from at least one order of magnitude of error (Ancey, 2020a, 2020b; Recking, 2013; Schneider et al., 2015; Yager et al., 2015). The challenge of bedload transport prediction derives partly from the fact that it is a complex process to express physically (Ancey, 2020a; Ashworth and Ferguson, 1986; Buffington and Montgomery, 1997; Gomez, 1991; Gomez and

Church, 1989; Parker et al., 1982), bedload being the balance between changing sediment transport capacity (as a function of changing streamflow), but also changing sediment availability (both at the streambed and as supply from the drainage network). In addition, it is also extremely challenging to measure in natural settings, and so to obtain the data needed to determine the level of complexity in bedload transport models. Direct sampling devices (e.g. Bunte et al., 2004; Helley and Smith, 1971) may be hazardous to deploy and only provide at-a-point data in time and space. They also commonly requires the signal (or at least its variance) to be known in order to determine a reliable sampling frequency (Bunte and Abt, 2005; Gomez, 1991; Gomez et al., 1989; Parker et al., 1982; Singh et al., 2009). Measurements of the rate of filling of traps or reservoirs dug across streams provided cross-sectional integrated estimates of sediment loads, including during high flows (Gray et al., 2010; Hinderer et al., 2013; Lane et al., 2017; Lenzi et al., 1999). Yet, their resolution depends on the rate at which trap-filling is measured, leading to time-series of low temporal resolution (e.g. a load per event in the best case, but more common are annual loads; Hinderer et al., 2013).

Indirect passive sensors have allowed new perspectives for bedload transport monitoring (Rickenmann, 2017). The noise produced by bedload particles in motion can be captured by underwater microphones (e.g. Barton et al., 2010; Geay et al., 2017; Rigby et al., 2016), by out-of-bank seismometers (e.g. Burtin et al., 2008; Dietze et al., 2019; Roth et al., 2016) or by measuring the vibration of a structure (e.g. plate, pipe) impacted by bedload particles in motion (e.g. Downing, 2010; Mizuyama et al., 2010; Perolo et al., 2019; Rickenmann et al., 2014). Such approaches may allow continuous time-series of bedload transport at high temporal resolution (i.e. down to 1 second), covering both high and low flow conditions (Rickenmann, 2017); and in absolute fluxes if the sensors can be calibrated (e.g. Nicollier et al., 2021; Rickenmann et al., 2012).

Continuous, high-resolution records allow quantification of relationships between bedload transport and discharge (Rickenmann, 2018) as well as evaluation and development of bedload transport models (e.g. Rickenmann, 2020). Such studies have confirmed in field settings the inherent autogenic variability of bedload transport observed in laboratory flumes (Gomez et al., 1989; Hoey and Sutherland, 1991) over short time-periods (i.e. less than a couple of hours; Rickenmann, 2018). Over longer time-periods, stronger correlations between streamflow and bedload transport rate emerge (Rickenmann, 2020, 2018). They suggest at such time-scales some forcing of bedload transport by exogenic controls such as watershed hydrology, and associated hydraulic transport capacity. In the meantime, the relationship remains dependent on sediment supply conditions, both from the streambed and from the surrounding drainage network (Buffington and Montgomery, 1997; Mao, 2018, 2012; Mao et al., 2014; Masteller et al., 2019; Rickenmann, 2020).

Within Alpine watersheds, a range of hydrological processes can lead to streamflow variations, and so trigger bedload transport if the energy is sufficient, and

sediment is available. These hydrological processes notably include ice and snow-melt, rainfall, and the mixed occurrence of rainfall and snow-melt events, which include “rain-on-snow” (ROS) events (Corripio and López-Moreno, 2017; Li et al., 2019; Musselman et al., 2018). Despite the increasing number of bedload transport time-series measured within Alpine watersheds, there are very few studies (Mao, 2012; Rainato et al., 2017) that have related temporal variations in bedload transport to possible hydrological drivers, and their respective contribution in annual bedload budgets. This matters not only for improving our ability to predict bedload transport under current climatic conditions, but also for investigating how bedload transport may evolve with climate change impacts on the hydrology of Alpine watersheds.

The goal of this paper is to relate bedload volumes exported from an Alpine watershed to hydrological drivers (e.g. snow-melt, rainfall, mixed rainfall and snow-melt events). The analysis is based on a five-year (2016-2020) bedload time-series recorded with passive acoustic sensing using a Swiss Plate Geophone system. The system is installed in the stream that drains the Vallon de Nant, a snow-melt-dominated Alpine watershed in the Western Swiss Alps. After calibration, the time-series of bedload transport were associated with streamflow and classified into the different hydrological categories (i.e. snow-melt, rainfall, co-occurrence of rain and snow-melt) likely dominant at different periods of time throughout the year. This allows us to tease out the contribution of different hydrological drivers to bedload transport and, using knowledge of likely future changes in watershed hydrology under a warming climate, assess possible evolution in bedload transport.

2. Material and methods

2.1 The Vallon de Nant watershed

The Vallon de Nant (VdN) is a 13.4 km² watershed located in the western Swiss Alps (Figure 1), with elevations ranging from c. 1200 to 3050 m. Although ~ 3 % of the watershed surface is occupied by the debris-covered Glacier des Martinets, it provides only small amounts of ice melt and the hydrological regime of the Avançon de Nant (AdN), the Alpine stream that drains the VdN, remains snow-dominated (Ceperley et al., 2020; Mächler et al., 2021; Michelon et al., 2021; Thornton et al., 2021). The AdN flows from the glacier snout (2313 m) over a length of ~ 6.5 km down to a hydrological and bedload monitoring station (1200 m) installed at the watershed outlet. The average gradient of the AdN is c. 17 %, but fluctuates (8-29 %) over its course, including braided reaches with lower slopes and steeper step-pool and semi-alluvial reaches (Figure 1). It is fed by ~10 intermittent, steep (40-60%), torrential tributaries that mainly flow during the snow-melt season or briefly during storm events, and which form large coalescent fans at the hillslope base (Figure1; Lane et al., 2016).

During the period 2014-2015, a hydrological and bedload monitoring station was built at the outlet of the watershed (1200 m), through a collaboration between the University of Lausanne (FGSE), the Swiss Federal Institute for Snow, Forest

and Landscape Research (WSL) and the ETH Zürich (Physics of Environmental Systems). Details of the monitoring station are given in the sections below.

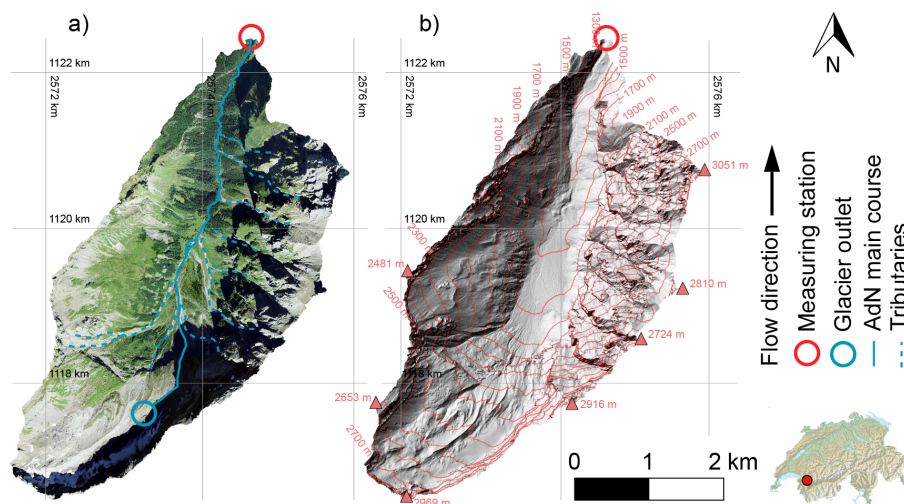


Figure 1. The 13.4-km² VdN watershed with the Glacier des Martinets outlet (blue circle), and the monitoring station at the outlet (red circle). In a) aerial image from 2013. In b) hillshade of the Swiss Alti3d digital elevation model (Acknowledgments © Swisstopo). Coordinates are in the CH1903 Swiss system.

2.2 Streamflow monitoring

Streamflow data were derived from a flow height sensor (a Vegapuls WL 61 radar) which emits short radar pulses that are reflected to the sensor by the water surface. The sensor was mounted on a metallic arm extended over the stream (Figure 2b). The transit time of the radar pulses from emission to reception allows measuring the distance to the water surface. Knowing the height of the sensor above the streambed (1.83 m), absolute water depths can be derived. The pulses are emitted circularly at an angle of 10° (Vegapuls, 2012), averaging the measured distance to the water surface over an area of ~ 0.1 m² at the water surface. The sensor records at a sampling rate of ~ 0.5 s, and data were averaged over 1 minute. Globally, the water height measurement has been reliable throughout the period of interest (2016-2020), with the exception of discrete periods of time where the measurement failed and the data are missing. Missing streamflow data are notably found in the winter period, during which the AdN channel was sometimes covered by ice and snow, biasing the water height sensing. Thus, an equivalent of 80 full days are missing over the 1827 days of the period of observation, and 72 % of the missing data occur in the winter period (December to March), where bedload activity is typically very low (i.e. 98.8 % of the total bedload occurs outside the missing discharge data window).

A calibration is required to transform the measured water depths [m] into a

streamflow per unit time [$l \cdot s^{-1}$]. Salt gauging was performed at the VdN monitoring station to build a rating curve between measured water depths and streamflow (Ceperley et al., 2018). During the years 2016 and 2017, 56 salt gauging samples were collected for water depths varying between 0.05 and 0.3 m. The relationship between water depth and streamflow was best expressed by a power law rating curve (Ceperley et al., 2018):

$$Q = 19998 * d^{1.6244} [1]$$

where Q is the streamflow per unit time [$l \cdot s^{-1}$] and d is the water depth [m], with a $R^2 = 0.91$. This equation is in close agreement with a theoretical discharge equation for a rectangular weir cross-section assuming critical flow conditions.

2.3 Bedload monitoring

A Swiss Plate Geophone (SPG) system developed by the Swiss Federal Research Institute WSL was used in this research (Nicollier et al., 2021; Rickenmann et al., 2014; Wyss et al., 2016a). The SPG system is typically made of a line of steel plates embedded across a river channel. Bedload particles in motion induce a vibration of the steel plates, which is recorded by a geophone sensor mounted below each plate (Rickenmann, 2017). The response of the SPG system under various conditions (e.g. impact magnitude, transport intensities, flow velocities, grain-size mixture) has been investigated in both laboratory and field experiments (Antoniazza et al., 2020; Nicollier et al., 2021; Wyss et al., 2016a, 2016b, 2016c), and successful calibrations of the SPG system using independent concurrent sampling of bedload have been achieved for multiple monitoring stations (Habersack et al., 2017; Kreisler et al., 2017; Nicollier et al., 2021, 2020, 2019; Rickenmann et al., 2012; Rickenmann and Fritschi, 2017).

At the VdN monitoring station, 10 plates of the SPG system were mounted side-by-side across the channel width (Figure 2b, 2c). The plates are made of stainless steel and have a standardized size of 492 mm in width, 358 mm in length (in flow direction), and 15 mm in thickness, with a total mass of 21 kg (Antoniazza et al., 2020; Rickenmann, 2017; Rickenmann et al., 2012; Wyss et al., 2016a). The plates are mounted in a steel frame, which is embodied in a concrete check dam across the channel (Figure 2b, 2c). The plates are mounted flush with the riverbed upstream to avoid biasing approach flow conditions. Below each plate, a 20 DX geophone sensor from Geospace technologies (Houston, Texas, USA) is mounted in a PC801 LPC Landcase set in an aluminum box (Rickenmann et al., 2017, 2012), and the plates are isolated from each other with elastomer elements.

During bedload transport events, particles rolling, sliding and saltating over the SPG system produce impact shocks that generate a change in the electrical voltage sensed by the geophone. The geophone signal was found to be proportional to the total mass of bedload in transport (Rickenmann et al., 2014, 2012; Rickenmann and Fritschi, 2017). The SPG is connected to an industrial PC that records the geophone signal at a frequency of 10 kHz. Geophone data are then summarized in the number of impulses per minute, which corresponds to

the number of times the geophone raw electrical signal exceeds a pre-defined threshold. In previous studies of bedload transport using the SPG system (Antoniazza et al., 2020; Rickenmann et al., 2014, 2012; Rickenmann and Fritschi, 2017; Wyss et al., 2016a, 2016c, 2016b), this threshold was set to 0.1 V in order to include within summary data the smallest detectable grain size fractions (~10-20 mm), while being at the same time greater by at least one order of magnitude in comparison with the noise level for flow conditions without bedload transport. Over the period 2016-2020, an equivalent of 30 full days are considered as biased SPG monitoring. Of these, ~ 10 relates to days that have to be excluded due to work on the measurement station, although these were almost always days with no bedload transport activity. The remaining missing data correspond to ~20 days of power failure at the monitoring station.

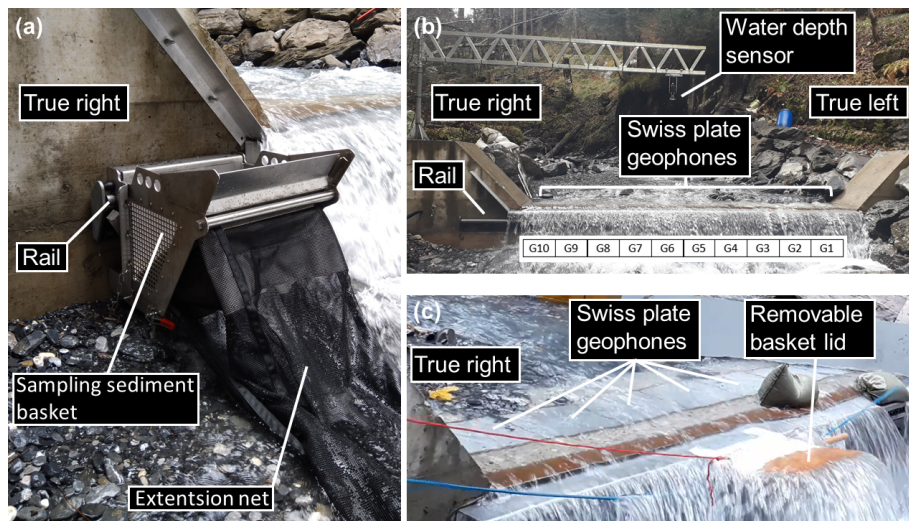
2.4 Geophone calibration

The Swiss geophone plate (SPG) system requires a robust calibration to transform the recorded signal into an actual mass of bedload in transport. This is typically achieved by collecting bedload samples during natural transport events that can be directly related to the signal measured by the sensors (Nicollier et al., 2021, 2020, 2019; Rickenmann et al., 2014, 2012; Rickenmann and Fritschi, 2017).

At the VdN, we used a mobile sediment basket to collect the calibration samples (Figure 2a). The sediment basket was mounted with rollers on a rail fixed on the downstream side of the concrete weir where the SPG are imbedded. Using a system of ropes and pulleys, the sediment basket was moved along the rail and located directly downstream of a given plate. Doing so, every particle that impacts this plate can be collected with the sediment basket. For this purpose, the sediment basket (530 mm) was slightly wider than a SPG (492 mm). The sediment basket had an initial capacity of 100 kg, but we expanded it during the calibration sampling by removing the downstream-facing panel and replacing it by a net that increased the sampling capacity to ~ 500 kg (Figure 2a). A removable lid was also built for the basket to prevent the collection of particles while positioning the basket at the plate targeted for calibration (Figure 2c).

Every bedload sample was collected using the following protocol: (a) the sediment basket (with the net extension) was emptied of sediment, covered with the lid and placed at the true right end of the rail (Figure 2a); (b) one person standing on the true left bank pulled the basket until it was positioned directly downstream of the targeted SPG. Marks on the ropes on both basket sides allowed precise basket positioning (± 0.01 m). Once positioned, ropes were secured on both banks to keep the basket stable during bedload sampling; (c) on the true right bank, a second person removed the basket lid whilst a third person simultaneously started the geophone raw recording (10 kHz) from the station laptop; (d) particles that impacted the targeted plate fell into the basket and progressively filled up the extension net. Bedload sampling lasted between 40 seconds and 10 minutes according to the intensity of bedload transport; (e) once the sampling time had elapsed and/or the sampling net was sufficiently

filled, the second and third operators rapidly pulled the basket back using the ropes. Pulling back the basket typically lasted 2 to 3 seconds, which minimized the risk of collecting additional unwanted particles while bringing the basket back to the bank position; (f) all the bedload particles collected in the basket and extension net were emptied to labelled storage boxes (i.e. sample number, name of the associated calibration file, number of the calibrated plate, sampling duration).



Figure

2. (a) The sediment sampling basket (with the extension net) placed on the rail; (b) General view of the VdN monitoring station. The sensor monitoring the water depth is set above the stream at the end of a metallic arm. Geophone plates are labelled G1 to G10 from the true left to true right bank. The rail that supports the mobile sediment basket is visible to the left of the waterfall; (c) View of the SPG along the concrete weir, and of the sediment sampling basket in experiment conditions. The blue ropes are used to pull the basket across the section. The red rope is used to remove the lid at the start of a sampling.

Calibration samples were collected during four days of fieldwork distributed within the 2019 and 2020 snow-melt seasons (details for each calibration sample are available in Supporting Information S1). The specific fieldwork days were picked in order to have a range of water (and so bedload transport) conditions with sampled discharges ranging from 0.88 to $2.69 \text{ m}^3 \cdot \text{s}^{-1}$. In total, 55 bedload samples were collected using the mobile sediment basket. Samples were alternatively collected over plates G5, G6, G7 and G8. This choice was motivated by a range of reasons. First, an impact experiment conducted over every SPG showed that all the plates at the VdN monitoring station responded similarly to impacts of comparable magnitude (Antoniazza et al., 2020); hence, a unique calibration coefficient could be used for all the different plates at this site. Second, plates G5, G6, G7 and G8 recorded together $\sim 69 \%$ of the total bedload

transport during the investigated period (2016-2020).

In previous studies to calibrate the SPG system in the field, the sampled bedload mass M_{tot} (Rickenmann et al., 2014, 2012; Rickenmann and McArdell, 2008, 2007; Wyss et al., 2016c) or the unit bedload transport rate q_b (Habersack et al., 2017; Kreisler et al., 2017; Rickenmann, 2018; Rickenmann et al., 2020; Rickenmann and Fritschi, 2017) were related to the number of impulses N_{imp} or to the impulse rate $IMPT$, respectively, and typically for particles with a diameter larger than 19 mm. After collection, bedload samples were thus brought from the field to the laboratory of the Swiss Federal Research Institute WSL, and were sieved to include only particles greater than 19 mm. Each sample was then weighted using an industrial scale (precision of 10^{-3} kg). The mass of each sample is reported in a Supplementary Information S1. Geophone raw electrical signal recorded during each sampling was summarized in a number of impulses N_{imp} [imp] by counting the number of times the raw electrical voltage signal exceeds a predefined threshold of 0.1 V (Antoniazza et al., 2020; Nicollier et al., 2021, 2020, 2019; Rickenmann et al., 2014, 2012; Wyss et al., 2016b, 2016a). The number of impulses counted for each calibration sample is reported in Supplementary Information S1.

Earlier research on the calibration of the SPG system (Nicollier et al., 2021; Rickenmann et al., 2014, 2012; Wyss et al., 2016a, 2016b) found that the mass of the material that impacted a given plate could be linearly related to the number of impulses recorded by the associated geophone sensor, i.e. :

$$M_{tot} = c_1 * N_{imp} [1]$$

where M_{tot} [kg] is the mass of material that impacted a given SPG, c_1 [$\text{kg} \cdot \text{imp}^{-1}$] is a field-site dependent constant and N_{imp} [imp] is the recorded number of impulses.

Knowing the sampling duration (Supplementary Information S1) and the width over which bedload occurs (i.e. roughly 0.5 m of plate width), the relationship can also be expressed in terms of rates, such as:

$$q_b = c_2 * IMPT [2]$$

where q_b is a unit transport rate [$\text{kg} \cdot \text{min}^{-1} \cdot \text{m}^{-1}$], c_2 [kg] is a field-site dependent constant, and $IMPT$ an impulse rate [$\text{imp} \cdot \text{min}^{-1} \cdot \text{m}^{-1}$].

In this paper, a linear regression line was fitted through the origin and the 55 calibration samples for both absolute and rate values. The slope of the relationship gives the $c_{1,2}$ value and a R^2 was calculated. The 95% confidence intervals were also calculated as:

$$CI = \pm t \sqrt{\frac{\sum e^2}{n-2} \left[\frac{1}{n} + \frac{(x_0 - \bar{x})^2}{\sum x^2 - n\bar{x}^2} \right]} [3]$$

where t is the t-value of Student, e are the residual values, n is the number of calibration samples, x_0 are the values of the independent variable N_{imp} in the time-serie, x are the values of the independent variable N_{imp} in the calibration

set, and \bar{x} is the mean of x . When bedload masses are summed over a given time period (e.g. months, years), the associated uncertainty is calculated following a summation rule:

$$\sigma_{\text{mass}} = \pm t \left[\sum_{i=1}^T \text{CI}_i^2 \right]^{0.5} \quad [4]$$

where σ_{mass} [kg] is the uncertainty in mass summed over a time period T . In this paper, bedload masses were estimated with a 95 % confidence interval, with $t = 1.96$.

In Figure 3a and 3b, the relationship between the number of impulses N_{imp} and the bedload mass M_{tot} is best expressed by a linear relationship passing through the origin, with significant R^2 values (0.85, 0.88) for both representations of the calibration data. The collection of calibration samples over a wide range of impulses (i.e. 99.4 % of 1-minute data points with bedload over the five-year time-series fall within the calibration domain) further allows narrow confidence intervals over most of the domain of interest, which translates into transport rate uncertainties that are low as compared to the transport rates themselves.

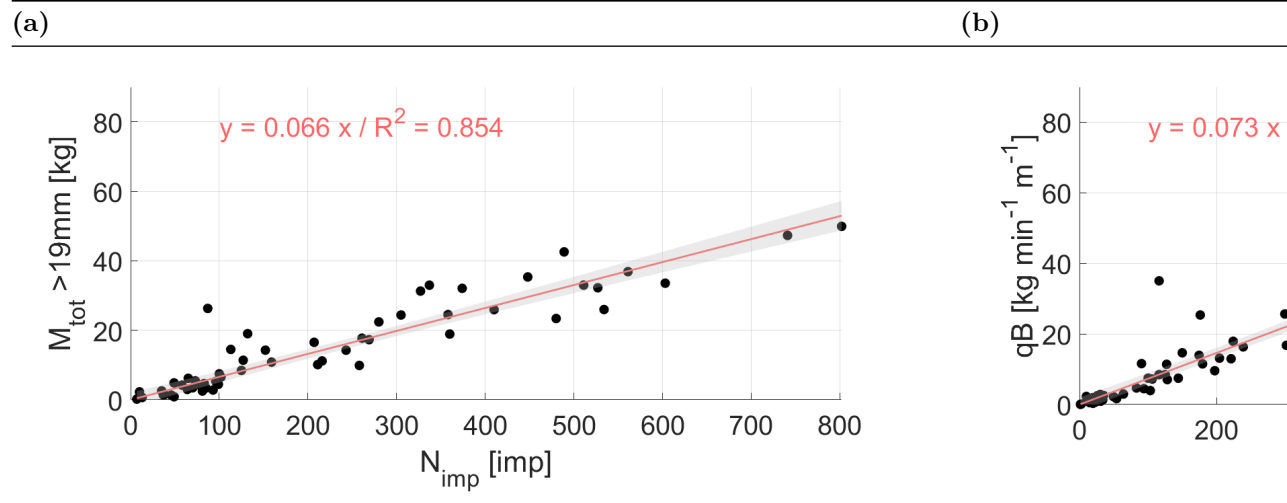


Figure 3. Calibration relationship derived from 55 bedload samples at the VdN in (a) absolute (with coefficient c_1) and (b) rate terms (with coefficient c_2). The shaded area gives the 95% confidence intervals calculated from [3], which are used to propagate the uncertainty into transformed bedload mass and unit bedload transport rates. Fit through 0 was performed using the ‘polyfitzero’ Matlab function (Mikovski, 2021).

Earlier studies interested in the calibration of the SPG system found that calibration coefficients c_1 and c_2 may vary according to a range of factors, which include flow velocity (Nicollier et al., 2021; Wyss et al., 2016a, 2016b), bed roughness (Wyss et al., 2016a, 2016b) and particle grain size (Nicollier et al.,

2021; Wyss et al., 2016c). Furthermore, an impact experiment conducted by Antoniazza et al. (2020) at several bedload monitoring sites equipped with the SPG system (including the VdN) showed that ~10-20% of the signal recorded on a given impacted plate propagates onto the neighbouring non-impacted plates despite the isolating elastomer elements. These elements likely influence the relationship between the SPG impulse count and the actual mass of bedload in transport shown in the scatter in Figure 3. Nevertheless, these sources of variability are implicitly included in the calibration coefficient proposed here, the bedload samples being collected for a range of natural streamflow and bedload transport rates that covers various flow conditions, grain size distribution and rates of signal propagation. The scatter is moreover relatively low. Therefore, the calibration of the SPG system presented here is considered to be reliable.

2.5 Data analysis

The quantification of bedload transport over the five years of observation (2016-2020), and the identification of the hydrological events driving them it, were performed through two main complementary analyses.

2.5.1 Bedload and the hydraulic forcing

First, absolute time-series of bedload transport over the period of interest, together with streamflow time-series were presented and bedload transport was integrated across different time-scales (e.g. years, months) to quantify its variability. Annual erosion rates were also derived from the total volume of bedload exported for comparison with other watersheds where such data are available.

An estimate of the hydraulic forcing of bedload transport at the VdN was performed, by comparing daily measured bedload transport with the daily predicted one, using a set of shear stress-based sediment transport equations proposed in the work of Schneider et al. (2015) and of Rickenmann (2020). The set of equations represents a modified form of the Wilcock and Crowe (2003) equation, which predicts daily bedload transport mass [kg] (of particles greater than 4 mm) using the total shear stress (i.e. transport capacity-based), and integrating bedload transport over the entire channel width, such as:

$$W^* = 0.002 \left(\frac{\tau_{D50}^*}{\tau_{rD50}^*} \right)^{16.1} \quad \text{for } \frac{\tau_{D50}^*}{\tau_{rD50}^*} < 1.143 \text{ and } D > 4 \text{ mm [5.1]}$$

$$W^* = 14 \left(1 - \frac{0.85}{\left(\frac{\tau_{D50}^*}{\tau_{rD50}^*} \right)^{0.7}} \right)^{4.5} \quad \text{for } \frac{\tau_{D50}^*}{\tau_{rD50}^*} \geq 1.143 \text{ and } D > 4 \text{ mm [5.2]}$$

where the dimensionless bed shear stress τ_{D50}^* , the dimensionless reference bed shear stress τ_{rD50}^* and the dimensionless transport rate W^* are defined as:

$$\tau_{D50}^* = \frac{r_b S}{R D_{50}} \quad [6]$$

$$\tau_{rD50}^* = 0.56 S^{0.5} \quad [7]$$

$$W^* = \frac{R g q_b}{u_*^3} \quad [8]$$

and where r_h [m] is the hydraulic radius, S [-] is the channel gradient, $R = \rho_s / \rho - 1$ [-] is the relative sediment density (with the sediment density $\rho_s = 2650$ kg/m³ and the water density $\rho = 1000$ kg/m³), D_{50} [m] is the median of the surface grain-size distribution, $g = 9.81$ [N/s²] is the gravitational acceleration, $u^* = (\tau/\rho)^{0.5}$ [m/s] is the shear velocity, $\tau = g\rho r_h S$ [N/m²] is the bed shear stress and q_b [kg · min⁻¹ · m⁻¹] is the volumetric bedload transport rate per unit width.

In this study, a mean slope S of 0.058 was measured in the 20 m upstream of the monitoring station from a 2-m resolution Swiss Alti3D digital elevation model, the median of the grain-size distribution $D_{50} = 0.048$ m was estimated through a surface Wolman count, and the hydraulic radius $r_h = (b + mh)h / (b + 2h * \sqrt{1 + m^2})$ was estimated for every 1-min measured water depth h [m] within the trapezoidal concrete cross-section of the monitoring station, with $b = 5.3$ m is the trapezoid shorter base, and $m = h / \tan(45) = h$ is the increase in channel width [m] with depth [m], since the slope of the concrete weir is 1:1.

2.5.2 Classification of the hydrological drivers of bedload

Second, the contribution of different hydrological drivers to total bedload transport were identified in the streamflow time-series. We were notably interested to investigate the proportion of bedload transported during rainfall-induced streamflow variations, during melt-induced streamflow variations, and during the co-occurrence of rainfall-induced and melt-induced streamflow variations, because these are the hydrological drivers expected to be able to trigger bedload transport, either separately or in combination.

The first step identified daily flow hydrographs influenced by rainfall. To do so, precipitation and temperature data were obtained from the RhiresD and TabsD datasets of MeteoSwiss. The RhiresD and TabsD datasets represent respectively daily precipitation (rainfall and snowfall equivalent, [mm]) and daily mean temperature [°C] interpolated at a spatial resolution of 1 km² from the dense precipitation-gauge and temperature sensor networks of MeteoSwiss (MeteoSwiss, 2019, 2017). Eighteen 1-km² cells of the RhiresD and TabsD grids covering partially or entirely the VdN were retained, and their coordinates are reported in a Supplementary Information S2. From the RhiresD precipitation dataset, a gross partitioning between rainfall and snowfall was performed, by summing for each grid cell the precipitation that occurred when the temperature of a given grid cell was above or below 1°C, respectively.

In an early stage of the work, an automatic classification of “rain-forced” and “not rain-forced” daily flow hydrographs was attempted, following Mutzner et al. (2015). It used a set of criteria combining the removal of snowy days (precipitation occurring during days where mean temperatures are below 1°C), the height of rainfall (of days where mean temperatures are above 1°C), the amplitude of daily flow hydrographs and the timing throughout the day of high flows and low flows (i.e. to differentiate between rainfall-driven and melt-driven changes in daily flow hydrographs). However, no sensible set of criteria covering the range

of flow hydrograph responses was identified using this approach, notably due to (1) the variable depth of rainfall generating a flow hydrograph response; (2) the variable daily mean temperature generating snowfall or rainfall (i.e. visible in the direct response to precipitation in the flow hydrograph); (3) the variable recession time of rainfall-driven events; and (4) a large variability in the amplitude and timing of daily low and high flows.

Therefore, a visual classification of the 1827 daily flow hydrographs into the two classes “rain-forced” and “not rain-forced” was undertaken. It used as support daily precipitation data, daily mean temperature data and daily flow hydrograph (i.e. amplitude, timing of high flows and low flows) to help driving the classification, but without setting fixed arbitrary thresholds in temperature, precipitation and/or daily flow hydrograph, which were found to be unsuitable at the previous stage. Each daily flow hydrograph was first considered in terms of its amplitude and the timing of high flows and low flows. Then, daily precipitation and mean temperature data were used to determine whether anyone daily flow hydrograph was possibly influenced by rainfall. The daily flow hydrograph of the antecedent day was also systematically used to identify possible recession curves in the daily flow hydrograph of the subsequent day. This approach allowed inclusion within the “rain-forced” category of days where rainfall visually induced a response in the flow hydrograph, including potential recession curves in the subsequent day(s). Within the class “not rain-forced” daily flow hydrographs, it further allowed, the inclusion of days with precipitation, but where the latter did not induce a response in the flow hydrograph. This may include snowfall, light rainfall or rainfall stored in a pre-existing snowpack or in the soil. Examples of typical daily flow hydrographs classified in each category (i.e. “rain-forced” or “not rain-forced”) are provided in the Supplementary Information S3. Annual flow hydrographs, variations in daily precipitations and daily mean temperatures for each year of observation (2016-2020) are available in a Supplementary Information S4 (Figure S4.1a, S4.2a, S4.3a, S4.4a, S4.5a).

Once daily flow hydrographs influenced by rainfall were identified within the streamflow time-series of each year (2016-2020), we partitioned periods of the year with differing melt intensity. The method used to classify daily flow hydrographs according to melt intensity follows Mutzner et al. (2015), and is based on the amplitude of daily melt discharge cycles. To identify days with clear melt signal, only the previously classified “not rain-forced” days are considered (Figure S4.1b, S4.2b, S4.3b, S4.4b, S4.5b). For each “not rain-forced” day, a daily flow hydrograph variation was calculated by subtracting a 24-hour moving average from the measured streamflow, to obtain a so-called detrended flow hydrograph Q_{det} [$\text{m}^3 \cdot \text{s}^{-1}$] (Mutzner et al., 2015). The amplitude of the daily flow hydrograph cycle Q_{amp} [$\text{m}^3 \cdot \text{s}^{-1}$] was estimated as half the difference between the maximum and the minimum value in the detrended daily flow hydrograph (Gribovszki et al., 2010; Mutzner et al., 2015). A visual inspection of the variation in both Q_{det} (Figure S4.1c S4.2c, S4.3c, S4.4c, S4.5c) and Q_{amp} (Figure S4.1d, S4.2d, S4.3d, S4.4d, S4.5d) throughout each year permitted the identification of coherent periods of time when daily flow hydrographs of “not

rain-forced” days would recurrently vary within a comparable range (Figure 4). We labelled them the pre-melt period, the early-melt period, the high-melt period, the late-melt period, and the post-melt period.

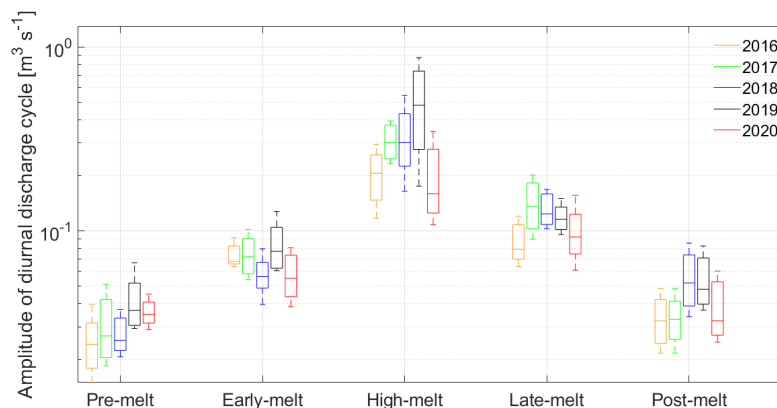


Figure 4. Distribution of daily Q_{amp} values (10th, 25th, 50th, 75th and 90th percentiles) within each period (i.e. pre-melt, early-melt, high-melt, late-melt, post-melt) for “not rain-forced” daily flow hydrographs of all investigated years (2016-2020).

At the VdN, the pre-melt period spans from January 1st to the onset of the melt season in early spring (i.e. April), and typically presents Q_{amp} median values between 0.02 and 0.04 [$m^3 \cdot s^{-1}$] (Figure 4; Table 1). The early-melt period represents the onset of the snow-melt season, during which the amplitude of diurnal hydrograph cycle Q_{amp} remains however relatively low, with median values ranging between 0.06 and 0.08 [$m^3 \cdot s^{-1}$] (Figure 4; Table 1). The high-melt period is the period with high rates of snow-melt, during which the amplitude of the diurnal hydrograph is the highest, with median values typically greater than 0.16 [$m^3 \cdot s^{-1}$] (Figure 4; Table 1). The late-melt period represents the period where a distinctive decrease in the amplitude of the diurnal hydrograph cycle is observed as the watershed snow content decreases, but where the remaining snow-melt still generates intermediate values of Q_{amp} , with median ranging from 0.08 to 0.14 [$m^3 \cdot s^{-1}$] (Figure 4; Table 1). The post-melt period is the period where remaining melt from the previous winter no longer produces large variations in Q_{amp} , and where the amplitude of ‘not rain-forced days’ diurnal discharge mainly relies on evapotranspiration cycle, and/or the melt of the potential first winter snowfall. The post-melt period spans from the late summer until the end of the year, with median values typically ranging between 0.03 and 0.05 [$m^3 \cdot s^{-1}$].

The determined date of the start and end of each period for each year, and the distribution of Q_{amp} values within them are reported in Table 1. Results of the classification (Table 1; Figure 4) show on the one hand the relatively low

overlap between Q_{amp} values of different periods within the same year. On the other hand, it exhibits a remarkable consistency of Q_{amp} values within a same period across years. It is important to note that given the specific meteorological conditions (e.g. temperatures, snow volumes) of anyone year, the different periods may start and end at very different dates (Table 1). If the pre-melt and post-melt periods do present a distribution of daily discharge amplitude that varies within a comparable range, they are quite different in terms of watershed hydrology and bedload dynamics. Indeed, the pre-melt corresponds to a rather cold period with a great amount of snow in the watershed, while the post-melt includes autumn storms, a more prominent evapotranspiration cycle, and the potential occurrence of the first winter snowfall in a watershed mostly free of snow cover. This is why we keep them separated.

Table 1. Dates of start and end of the five identified periods (pre-melt, early-melt, high-melt, late-melt, high-melt) for each investigated year, determined based on the range of variability in Q_{amp} values (25th, 50th and 75th percentile value reported here), and a visual inspection of the variation of both Q_{det} (Figure S4.1c S4.2c, S4.3c, S4.4c, S4.5c) and Q_{amp} through time (Figure S4.1d, S4.2d, S4.3d, S4.4d, S4.d).

		Pre-melt	Early-melt	High-melt	Late-melt	Post-melt	
2016	Dates	50 th [25 th , 75 th]	50 th [25 th , 75 th]	50 th [25 th , 75 th]	50 th [25 th , 75 th]	50 th [25 th , 75 th]	
		Jan. 1 st – Apr.10 th	Apr. 11 th – May 5 th	May 6 th – Aug. 11 th	Aug. 12 th – Aug. 28 th	Aug. 29 th – Dec. 31 th	
		Q_{amp} [m ³ s ⁻¹]	0.02 [0.02, 0.03]	0.07 [0.07, 0.08]	0.21 [0.16, 0.25]	0.08 [0.07, 0.1]	0.03 [0.03, 0.04]
2017	Dates	Jan. 1 st – Apr. 2 nd	Apr. 3 rd – May 13 ^h	May 14 th – Jun. 21 th	Jun. 20 th – Sep. 4 th	Sep. 5 th – Dec. 31 th	
		Q_{amp} [m ³ s ⁻¹]	0.03 [0.02, 0.04]	0.07 [0.06, 0.09]	0.3 [0.25, 0.37]	0.14 [0.1, 0.18]	0.03 [0.03, 0.04]
		2018	Dates	Jan. 1 st – Apr. 7 th	Apr. 8 th – Apr. 16 th	Apr. 17 th – Jun. 24 th	Jun. 25 th – Sep. 4 th
Q_{amp} [m ³ s ⁻¹]	0.03 [0.02, 0.03]			0.06 [0.05, 0.06]	0.3 [0.24, 0.4]	0.12 [0.1, 0.16]	0.05 [0.04, 0.07]

		Pre-melt	Early-melt	High-melt	Late-melt	Post-melt
2019	Dates	Jan. 1st –	Apr. 5th –	May. 16th –	Jul. 9th –	Aug. 30th –
		Apr. 4th	May. 15th	Jul. 8th	Aug. 29th	Dec. 31th
	Q_{amp} [m ³ s ⁻¹]	0.04 [0.03, 0.05]	0.08 [0.06, 0.1]	0.48 [0.31, 0.69]	0.12 [0.1, 0.13]	0.05 [0.04, 0.07]
2020	Dates	Jan. 1st –	Apr. 5th –	Apr. 10th –	Jul. 21th –	Sep. 6th –
		Apr. 4rd	Apr. 9th	Jul. 20th	Sep. 5th	Dec. 31th
	Q_{amp} [m ³ s ⁻¹]	0.04 [0.03, 0.04]	0.06 [0.05, 0.07]	0.16 [0.13, 0.25]	0.09 [0.08, 0.11]	0.03 [0.03, 0.05]

From this hydrological analysis, we were able to partition each year into the five periods of differing melt intensity (i.e. pre-melt, early-melt, high-melt, late-melt and post-melt), and further to know within them whether rainfall was additionally influencing or not the daily flow hydrograph (“rain-forced” and “not rain-forced” days). Bedload could then be integrated along those different categories, separately or in combination, to investigate the proportion of bedload transport driven by the different hydrological categories (i.e. rainfall-induced, melt-induced or a combination of both). The classification further allowed determination of the magnitude-frequency of daily bedload transport at the VdN for the different the hydrological categories. The magnitude of bedload transport is calculated for both the daily total bedload mass transported [kg], and for the daily maximum bedload peak rate reached [kg · min⁻¹]. The frequency is calculated from the number of days within a given category that equals or exceeds a given bedload magnitude.

3. Results

3.1 Absolute bedload time-series, transported masses and hydraulic forcing

Five years of measurement of streamflow and bedload transport rates are presented in Figure 5a. Streamflow follows the general trends expected for a snow-melt dominated Alpine watershed at this altitude (Figure 4, Table 1), with low baseflow during the winter season (pre-melt), increasing slowly during April at the onset of the melt season (early-melt), and more steadily during late May-early June. They then peak in the period June-July at the maximum of the snow-melt season (high-melt), and decrease progressively as watershed snow content decays through the summer season (late-melt), and autumn (post-melt). This

general seasonal trend is disrupted by sudden storms, especially during the summer and the autumn, that can generate short-duration high-magnitude floods. As expected, bedload transport also occurs during periods of high-magnitude streamflow, either during the snow-melt season or during storms throughout the year, with the exception of the winter period, when lower bedload transport tend to be observed. A rough estimate of a constant critical streamflow Q_c , above which bedload is triggered, can be estimated to $\sim 1 \text{ m}^3 \text{ s}^{-1}$, although this value is likely to change in time. Related factors changing over time include: (i) bed configuration, which influences of grain size distribution, bed roughness, grain organization and armoring effects; and (ii) sediment availability both at the bed and supply from the drainage network. As a consequence of fluctuating critical shear stress, 18 % of the total transport that took place at the VdN over the five years of observation occur below $Q_c = 1 \text{ m}^3 \cdot \text{s}^{-1}$.

Annual bedload mass varies significantly from one year to the other across the five years of observation (Figure 5b). 2019 had a much higher annual bedload mass, with $3.75 \cdot 10^6 \text{ kg}$ ($\pm 3.29 \cdot 10^3 \text{ kg}$), followed by the year 2018 with $1.62 \cdot 10^6 \text{ kg}$ ($\pm 1.95 \cdot 10^3 \text{ kg}$). The years 2016, 2017 and 2020 recorded a lower total bedload mass with $0.30 \cdot 10^6 \text{ kg}$ ($\pm 1.51 \cdot 10^3 \text{ kg}$), $0.52 \cdot 10^6 \text{ kg}$ ($\pm 1.57 \cdot 10^3 \text{ kg}$) and $0.65 \cdot 10^6 \text{ kg}$ ($\pm 1.65 \cdot 10^3 \text{ kg}$), respectively. Over the five years investigated, the average annual mass of bedload exported from the VdN is $1.37 \cdot 10^6 \text{ kg}$ ($\pm 1.99 \cdot 10^3 \text{ kg}$). It is common (e.g. Hinderer et al., 2013) to divide sediment export volumes by the average sediment density m^3^{-1} (i.e. $2650 \text{ kg} \cdot \text{m}^{-3}$; Hinderer et al., 2013) and associated watershed area (i.e. 13.4 km^2), to give annual erosion rates due to bedload transport. Although such calculations assume that sediment was eroded in the year that it was exported, we perform them here for comparative purposes with other watersheds where such data are available. From 2016 to 2020, annual erosion rates at the VdN are $0.009 \text{ mm} \cdot \text{y}^{-1}$ ($\pm 4.3 \cdot 10^{-5} \text{ mm}$), $0.015 \text{ mm} \cdot \text{y}^{-1}$ ($\pm 4.4 \cdot 10^{-5} \text{ mm}$), $0.046 \text{ mm} \cdot \text{y}^{-1}$ ($\pm 5.5 \cdot 10^{-5} \text{ mm}$), $0.106 \text{ mm} \cdot \text{y}^{-1}$ ($\pm 9.3 \cdot 10^{-5} \text{ mm}$) and $0.018 \text{ mm} \cdot \text{y}^{-1}$ ($\pm 4.6 \cdot 10^{-5} \text{ mm}$), respectively. Over the five years of measurement, the average annual erosion rate due to bedload transport is $0.039 \text{ mm} \cdot \text{y}^{-1}$ ($\pm 5.6 \cdot 10^{-5} \text{ mm}$). Annual and monthly transported bedload masses throughout the five years of measurement, and their estimation uncertainty, are reported in Supporting Information S5.

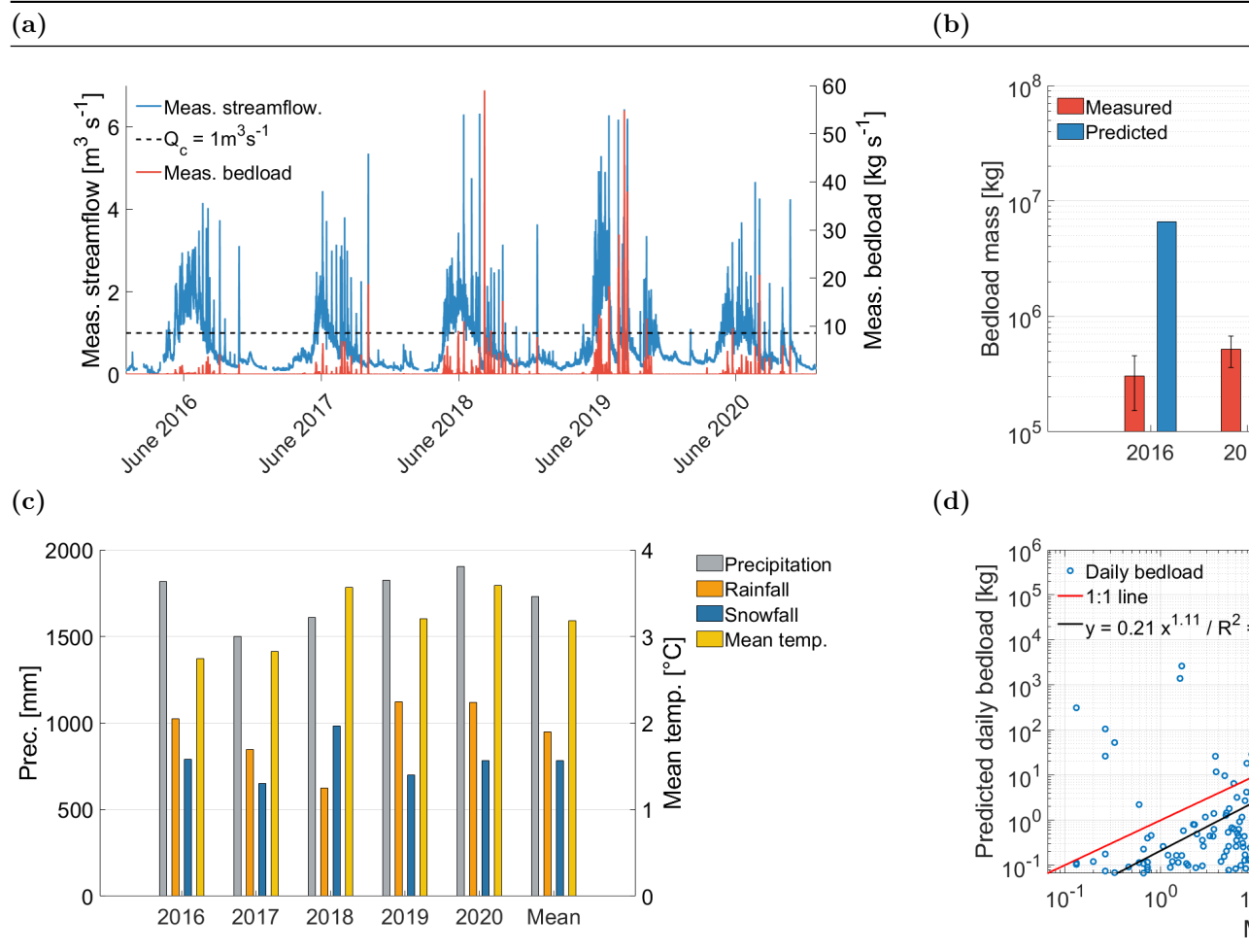


Figure 5. (a) Measured time-series of streamflow (in blue) and bedload transport rates (in red) over the five years of observation (2016-2020), with an estimate of a constant critical streamflow Q_c (dashed black line); (b) measured annual bedload masses (in red) predicted annual bedload masses (in blue) for each of the five years of observation. Note the logarithmic y-scale; (c) annual mean temperature (in yellow), precipitation (in gray), rainfall (in orange), snowfall (in dark blue), for each of the five years of observation; (d) relationship between daily predicted and daily measured bedload transport over the five years of observation. The red line is the 1:1 relationship, and the black line is the best fit power law regression.

The differences observed in the annual bedload yield at the VdN do not scale directly with either the total amount of precipitation (rainfall and/or snowfall) a given year received, or with mean annual temperatures (Figure 5b, 5c). The

annual sum of RhiresD daily precipitation (over the 18 1-km² cells selected for the VdN; Table S2.1) shows indeed that the year 2020 received the greatest amount of precipitation (~1905 mm), followed by the years 2019 (~1825 mm), 2016 (~1810 mm), 2018 (~1610 mm) and 2017 (~1500 mm). A gross estimate of rainfall (i.e. sum of daily precipitation of RhiresD where daily mean temperature TabsD is equal or above 1°C) suggests that the year 2019 received the greatest amount of rainfall (~1125 mm), followed by the year 2020 (~1120 mm), 2016 (~1020 mm), 2017 (~850 mm) and 2018 (~625 mm). A gross estimate of snowfall (i.e. sum of daily precipitation of RhiresD where daily mean temperature TabsD is equal or below 1°C) suggests that the year 2018 received the greatest amount of snow (~985 mm), followed by the year 2016 (~790 mm), 2020 (~785 mm), 2019 (~700 mm) and 2017 (~650 mm). Regarding the annual mean temperature, the three warmest years are indeed the three most active in terms of bedload transport (2019, 2018, 2020), but with proportions that do not really scale with temperature. Note that precipitation in the RhiresD dataset is expected to be underestimated due to snow undercatch (Freudiger et al., 2016).

Regarding the shear stress-based estimate of bedload, calculated from equations [5.2, 5.3, 6, 7, 8] (Figure 5b, in blue), the hydraulic forcing based on time-integrated transport capacity tends to overestimate the actual measured bedload (Figure 5b, in red), with $6.64 \cdot 10^6$ kg in 2016 (factor 22 of difference as compared with the measured load), $2.29 \cdot 10^6$ kg in 2017 (factor 5 of difference), $3.90 \cdot 10^6$ kg in 2018 (factor 3 of difference), $17.4 \cdot 10^6$ kg in 2019 (factor 6 of difference) and $0.832 \cdot 10^6$ kg in 2020 (factor 1 of difference). While these differences are substantial, our estimations remain somehow lower than many bedload predictions, which typically exceed bedload measurements by one or more order(s) of magnitude (Ancey, 2020a, 2020b; Recking, 2013; Schneider et al., 2015; Yager et al., 2015). Comparing the relative difference between years, the annual predicted bedload mass seems to scale approximatively for the years 2017-2020, but not for the year 2016, with regards to relative yearly differences in the measured bedload mass (Figure 5b).

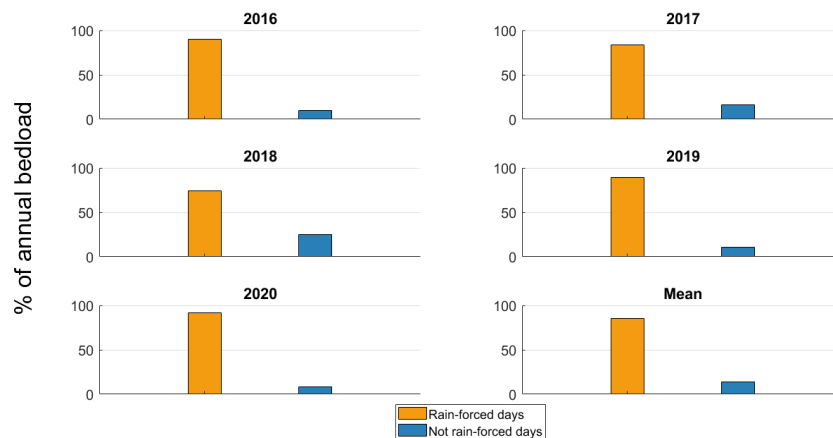
The relationship between the daily bedload mass measured with the SPG system, and the daily bedload mass predicted from the time-integrated shear stress (i.e. transport capacity) equations is presented in Figure 5d. The relationship shows a relatively good agreement with the 1:1 line, with the exponent of the power law regression being close to 1, and a $R^2 = 0.47$, which illustrates the importance of the hydraulic forcing for bedload transport. On the other hand, the scatter around the trend line has up to three orders of magnitude of difference between the daily measured and predicted bedload mass for both over- and under-estimation, which also emphasizes the limits of hydraulic-based estimates of bedload. This may be due to either erroneous estimates of the hydraulic forcing, or the temporally variable availability in sediment both at the bed and from the drainage network. The density of data points below the 1:1 line in Figure 5d (particularly for smaller loads) may suggest that the shear stress-based equations tend in average to underestimate the actual bedload mass transported. Yet, the data points above the 1:1 line (i.e. overestimation of predicted bedload

as compared to the measured one; logarithmic y-scale) have in average more weight when summing up daily values to yearly loads, and largely compensate the underestimates of bedload at lower magnitude transport on a daily time scale (Figure 5b).

3.2 Bedload transport, rainfall and the melt season

Bedload was summed for each year for “rain-forced” and “not rain-forced” days based on the classification of daily flow hydrographs (Figure 6a). Results show that a significantly greater proportion of annual bedload transport takes place during “rain-forced” daily flow hydrographs, as compared with “not rain-forced” daily flow hydrographs. On average over the five years of observation, ~86% of the annual bedload budget (75% to 91%) occurs during “rain-forced” daily flow hydrographs, while “not rain-forced” flow hydrographs (which notably include melt-only signal) represent on average ~14 % of the annual bedload budget (9% to 25%). Note that “rain-forced” days may occur throughout the year, therefore they may be associated with a melt signal of varying intensity.

(a)



(b)

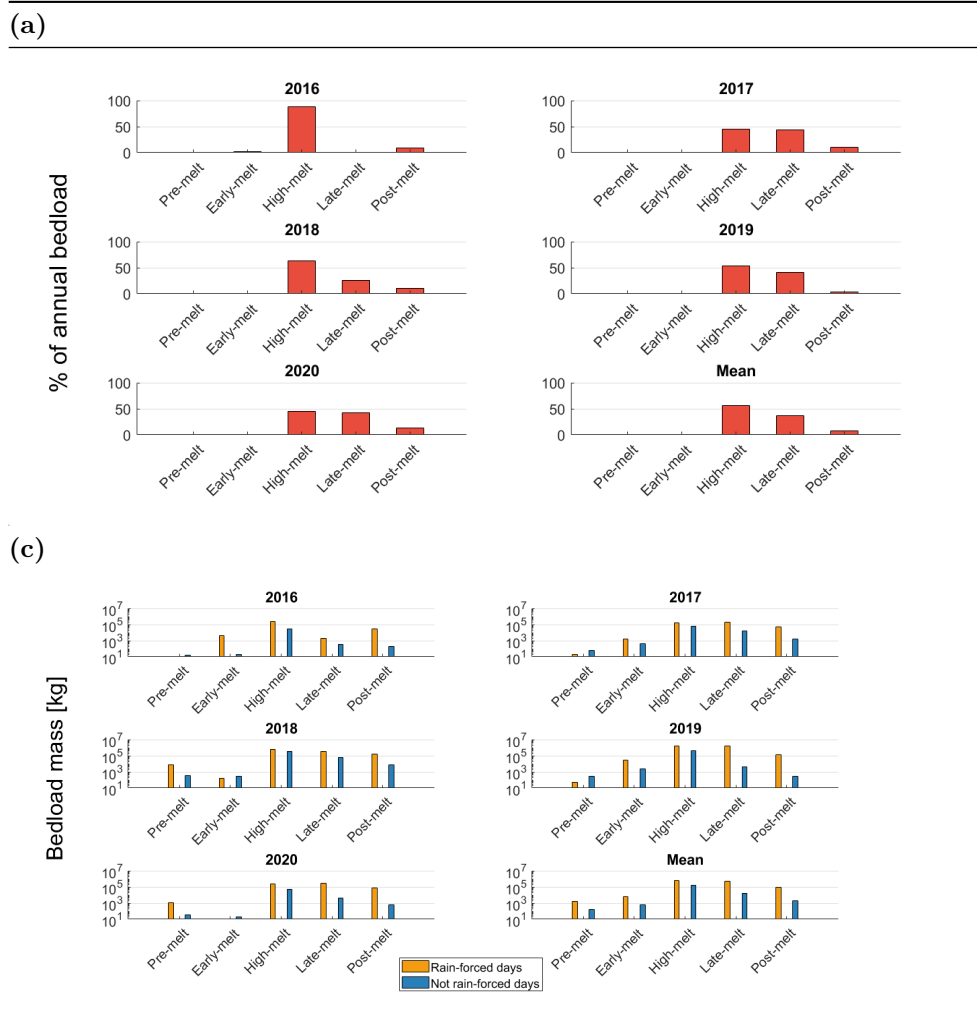


Figure 6. In (a), the proportion of annual bedload transport between “rain-forced” and “not rain-forced” days is presented for each of the five years of observation (2016-2020) and in average over the five years. In (b), the proportion of annual bedload transported for each of the five periods identified in flow hydrographs is presented (i.e. pre-melt, early-melt, high-melt, late-melt, post-melt) for each of the five years of observation and in average over the five years. In (c), total transported bedload mass per year and in average for each of the five periods, and between categories “rain-forced” and “not rain-forced” is presented. Note the logarithmic y-axes in Figure 6c.

Bedload transport was further summed by year for each of the five periods that have been identified based on the amplitude of daily flow hydrograph of “not rain-forced” days (Figure 6b). Results show that while the pre-melt and early-

melt periods record no, or a negligible proportion ($\sim 1\%$) of annual bedload, the high-melt season represents on average $\sim 59\%$ (45% to 89 %) of the annual transported bedload. The late-melt period is the second period carrying the highest proportion of material, with on average $\sim 31\%$ of the annual load (1-44 %), including year 2016 where a comparatively lower proportion of annual bedload was transported (1 %). The post-melt period was also responsible for a non-negligible part of the annual transported bedload, $\sim 9\%$ on average (4% to 13 %). Note that each period contains both “rain-forced” and “not rain-forced” days.

Bedload was also investigated by combining the two categories, that is “rain-forced” and “not rain-forced” daily flow hydrographs, and the five periods with differing melt intensity (Figure 6c). Results show that the greatest masses of bedload are consistently transported during “rain-forced” days of the high-melt season throughout the five years of observation, with an average of $5.9 \cdot 10^5$ kg (1.66-16.3; $\sim 47\%$ of the annual bedload). Then, the second highest volumes are transported during “rain-forced” days of the late-melt period, with $4.8 \cdot 10^5$ kg on average (0.02-15.6; $\sim 30\%$ of the annual bedload). In third place come “not rain-forced” days of the high-melt period, with $1.76 \cdot 10^5$ kg on average (0.29-3.9; $\sim 12\%$ of the annual bedload). Fourth place is occupied by “rain-forced” days of the post-melt season, with on average $0.94 \cdot 10^5$ kg (0.27-1.67; $\sim 9\%$ of the annual bedload). In fifth place, the “not rain-forced” days of the late-melt season have an average of $0.17 \cdot 10^5$ kg (0.003-0.59; $\sim 2\%$ of the annual bedload). These are followed by the other categories, which carry a negligible proportion of the annual bedload transport ($< 1\%$).

3.3 Bedload transport magnitude-frequency

A progressive decline in the magnitude of daily bedload transport is observable with increasing frequency, for both the total mass of bedload transported per day (Figure 7a), and for the daily maximum transport rate reached (Figure 7b).

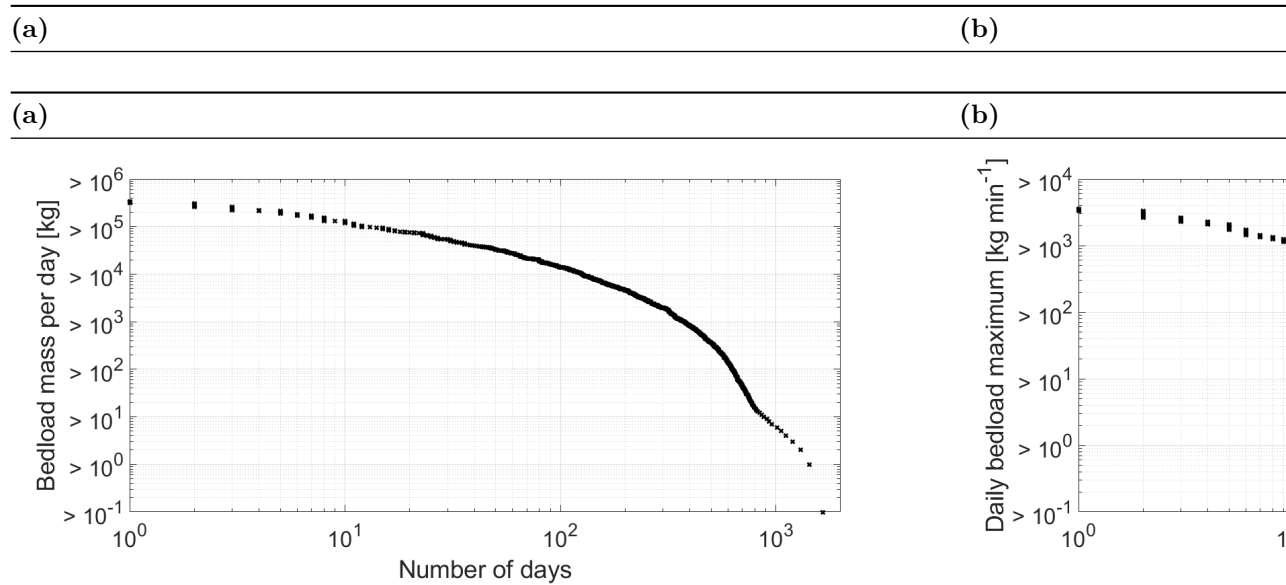


Figure 7. Magnitude-frequency relationship of daily bedload transport at the VdN throughout the five years of observation (2016-2020) for both (a) the daily bedload total mass transported and (b) the daily maximum transport rate reached.

The largest daily bedload total mass is $3.34 \cdot 10^5$ kg, while the highest daily maximum transport rate is $3.5 \cdot 10^3$ kg \cdot min⁻¹. There are 10 days throughout the five years of observation when daily bedload exceeds 10^5 kg, while there are 10 days where daily maximum rate is $> 10^3$ kg \cdot min⁻¹. At intermediate magnitude-frequency, there are about 100 days when daily bedload total mass exceeds 10^4 kg, and 100 days when maximum rates at greater than 10^2 kg \cdot min⁻¹. As magnitude further decreases (i.e. daily mass $< 10^4$ kg; daily peak rate $< 10^2$ kg \cdot min⁻¹) and frequency increases (> 100 days), there is a steep decline in the magnitude-frequency relationship for both variables (Figure 7).

Regarding the magnitude-frequency of “rain-forced” and “not rain-forced” days, “rain-forced” days appear to have daily bedload total mass (Figure 8a) and daily maximum transport rate (Figure 8b) up to an order of magnitude greater than “not rain-forced” days for intermediate to low frequencies (< 100 days). For instance, while the highest magnitude daily bedload mass of “rain-forced days” is $3.34 \cdot 10^5$ kg, the highest magnitude of “not rain-forced” days is $0.76 \cdot 10^5$ kg. Regarding daily maximum rates, the highest “rain-forced” peak rate is $3.5 \cdot 10^3$ kg \cdot min⁻¹, while the highest “not rain-forced” peak rate is $0.58 \cdot 10^3$ kg \cdot min⁻¹.

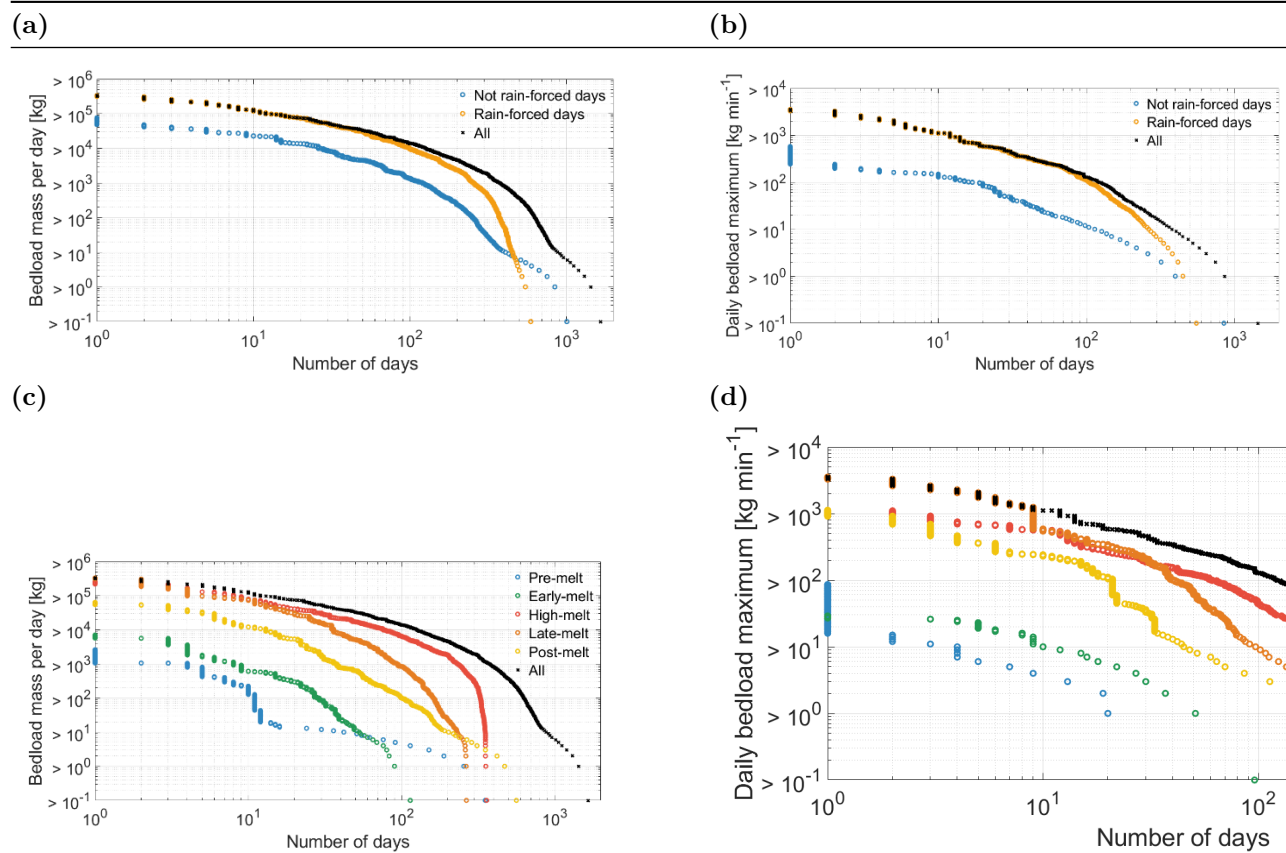
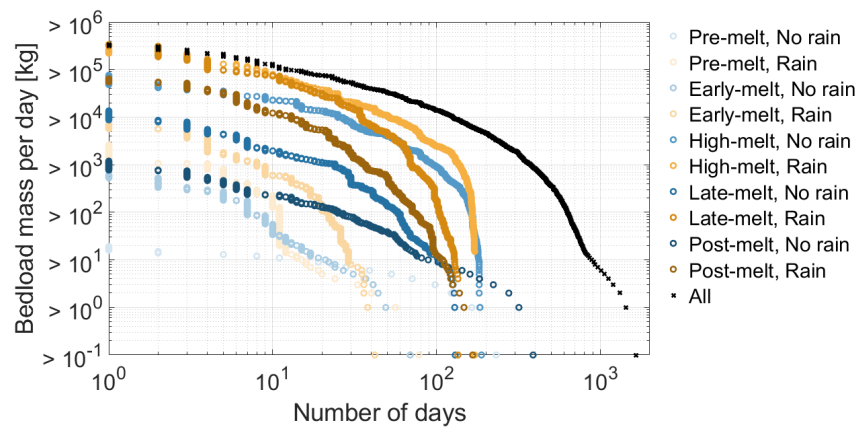


Figure 8. Magnitude-frequency relationship of daily bedload transport at the VdN between “rain-forced” and “not rain-forced” days for both (a) the daily bedload total mass transported and (b) the daily maximum transport rate reached, and between the five identified periods with differing melt intensity for both (c) the daily bedload total mass transported and (d) the daily bedload maximum reached.

By separating daily bedload transport between the five identified periods with differing melt intensity for both the daily bedload total mass (Figure 8c) and the daily maximum transport rate (Figure 8d), the magnitude-frequency of daily bedload in the different periods of the melt season can be investigated. For daily bedload total mass (Figure 8c), the 10 highest magnitude daily bedload days ($> 10^5$ kg) all occur during the high-melt and late-melt periods, followed by the post-melt period (10^4 - 10^5 kg), the early-melt (10^3 - 10^4 kg) and the pre-melt ($5 \cdot 10^2$ - $3 \cdot 10^3$ kg) period. At intermediate frequencies (> 10 days), the high-melt period has the slowest decline in magnitude as the frequency increases. Magnitude decreases more rapidly in the other periods. Considering the daily

maximum transport rate (Figure 8d), the late-melt period has the highest bedload peak rates ($> 3 \cdot 10^3 \text{ kg} \cdot \text{min}^{-1}$), followed by the high-melt and post-melt period ($\approx 3 \cdot 10^3 \text{ kg} \cdot \text{min}^{-1}$), and then the early-melt and pre-melt periods ($< 10^2 \text{ kg} \cdot \text{min}^{-1}$). Similar to the daily bedload total mass, the decline in the magnitude of daily maximum rate with increasing frequency is slower for the high-melt period than for other periods, such that the late-melt period magnitude decreases to the same level as the high-melt period for frequencies of 10-40 days and magnitudes of $0.5\text{-}1 \cdot 10^3 \text{ kg} \cdot \text{min}^{-1}$. At higher frequencies (> 40 days) the high-melt period has the greatest magnitude daily maximum rate for the same frequency. The gap between the group “high-melt, late-melt, post-melt” and the group “early-melt, pre-melt” is even more marked for the daily maximum transport rate magnitude-frequency patterns (Figure 8d) than the ones of the daily bedload total mass (Figure 8c).

(a)



(b)

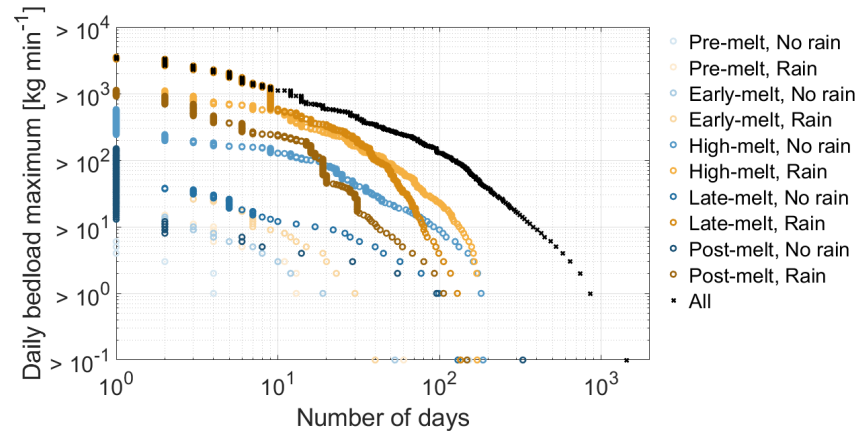


Figure 9. Magnitude-frequency relationship of daily bedload transport at the VdN between the five identified periods with differing melt intensity and between “rain-forced” days and “not rain-forced” days for both (a) the daily bedload total mass transported and (b) the daily bedload maximum transport rate reached.

In Figure 9, the magnitude-frequency relationships for daily bedload transport between “rain-forced” and “not rain-forced” days, and between the five periods with differing melt intensity, for both the daily bedload total mass transported (Figure 9a) and the daily maximum transport rate reached (Figure 9b), are presented. For daily total mass (Figure 9a), for low frequencies (< 10 days), high magnitudes ($> 10^5$ kg) are found during “rain-forced” days of the high-melt and late-melt periods. Then come “rain-forced” days of the post-melt period and “not rain-forced” days of the high-melt period (10^4 - 10^5 kg), followed by “rain-forced” days of the early-melt and “not rain-forced” days of the late-melt period (10^3 - 10^4 kg). “Rain-forced” days of the pre-melt period, and “not rain-forced” days of the post-melt, early-melt and pre-melt periods all record relatively low magnitude bedload magnitudes ($< 10^3$ kg), even at these low frequencies of occurrence. At intermediate frequencies (10-100 days), the highest magnitudes are recorded for, in decreasing order: “Rain-forced” – high-melt; “Rain-forced” – late-melt; “Not rain-forced” – high-melt; “Rain-forced” – post-melt; “Not rain-forced” – late-melt; followed by the other categories, which carry less substantial masses of bedload.

Regarding daily maximum bedload transport rates (Figure 9b), for low frequencies (< 10 days), the highest bedload intensity ($> 3 \cdot 10^3$ kg \cdot min $^{-1}$) are reached for “rain-forced” days of the late-melt period, followed by “rain-forced” days of the high-melt period, “rain-forced” days of the post-melt period, “not rain-forced” days of the high-melt period and “not rain-forced” days of the late-melt period. At intermediate frequencies (10-100 days), the highest bedload intensities are found in “rain-forced” days of the High-melt and Late-melt periods, followed by “rain-forced” days of the post-melt period, and “not rain-forced” days of the high-melt period, followed by the other categories. The magnitude-frequency of daily bedload transport for each year separately integrated over the different hydrological categories developed in this paper is available in a Supplementary Information S6.

4. Discussion

4.1 Annual bedload masses and their variability

Average annual erosion rates estimated from bedload transport export at the VdN can be compared with other Alpine watersheds where bedload data have been reported. We only selected headwater watersheds that are between 5 and 100 km 2 in size, and with a glaciated area $< 40\%$. These two variables, together with associated annual transport capacity, channel gradient and the geological setting, were shown to considerably affect annual bedload export (Hinderer et al., 2013; Lauffer and Sommer, 1982; Rickenmann, 2020, 2012, 1997; Spreafico and Lehmann, 1994; Turowski et al., 2010). Details of the watersheds presented

in Figure 10 are available in a Supplementary Information S7 (Table S7.1).

With an average of $0.039 \text{ mm} \cdot \text{y}^{-1}$, the VdN appears as a relatively active watershed in terms of bedload export (Figure 10a) as compared with most other Swiss (FOEN, 2010; Spreafico and Lehmann, 1994), Austrian (Sextenbach, Taschachbach, Fischbach; Lauffer and Sommer, 1982; Rickenmann, 2018; Vorndran, 1985) and German Alpine streams (e.g. Lahnwisengraben; Schmidt and Morche, 2006). It exports less material than some other catchments, such as the Val Roseg (CH), the Dürrache (AU), the Lainbach (DE), the Ferrand (FR), the Senio d'Elvio (IT), the Nigardsbreen (NO) and the Engabreen (NO) (Becht et al., 1989, 1989; Gurnell, 1987; Lauffer and Sommer, 1982; Mano et al., 2009; Schmidt and Morche, 2006; Tockner et al., 2002; Tropeano, 1991), amongst which some have a much greater glaciated area. The VdN (3 % glaciated) has comparable erosion rates with some watersheds that are more glaciated, such as the Fischbach (16%), the Ruetz (20%), the Minstigerbach (20%) and the Lonza (37 %) (FOEN, 2010; Rickenmann, 2018; Spreafico and Lehmann, 1994). These comparisons are complicated by the basin Sediment Delivery Ratio (SDR) which commonly decreases with increasing watershed area, reflecting that larger basins store more material than smaller ones (e.g. Hinderer et al., 2013), and that specific bedload transport capacities (per unit watershed area) decrease due to decreasing channel steepness (Rickenmann and Koschni, 2010). Figure 10b shows that some large catchments export little bedload and may be subject to significant storage, but this does not seem to apply to the VdN, which has generally higher erosion rates than the smaller reported watersheds. Note also that erosion rates presented here do not include the suspended load, which is likely to represent at least 50 % of the total load exported at the VdN (e.g. Turowski et al., 2010).

When looking at the inter-annual variability in exported bedload over the five years investigated, the VdN has a factor of 10 difference between the least (2016) and the most (2019) active year (Figure 5b). This is more than reported for the Fischbach and the Ruetz basins, where ~10 years of survey show a factor 4.5 and 5 between the least and the most active year, respectively (Rickenmann, 2018; Rickenmann et al., 2020). The factor is less than reported for the Rio Cordon, where annual loads between 0 and $1.5 \cdot 10^6 \text{ kg}$ have been observed over three-decades of survey (Rainato et al., 2017). Inter-annual differences may reflect mean annual temperatures, the annual quantity of precipitation (both snowfall and rainfall), or the time-integrated shear stress, although our results suggest no simple systematic relationships between bedload export and such variables. Of greater importance may be the intensity and timing of the hydrological events taking place (e.g. watershed snow content, timing and magnitude of the melt, timing and magnitude of rainfall, baseflow intensity; Figure 5, 6, 8, 9), and also with regards to change in sediment availability.

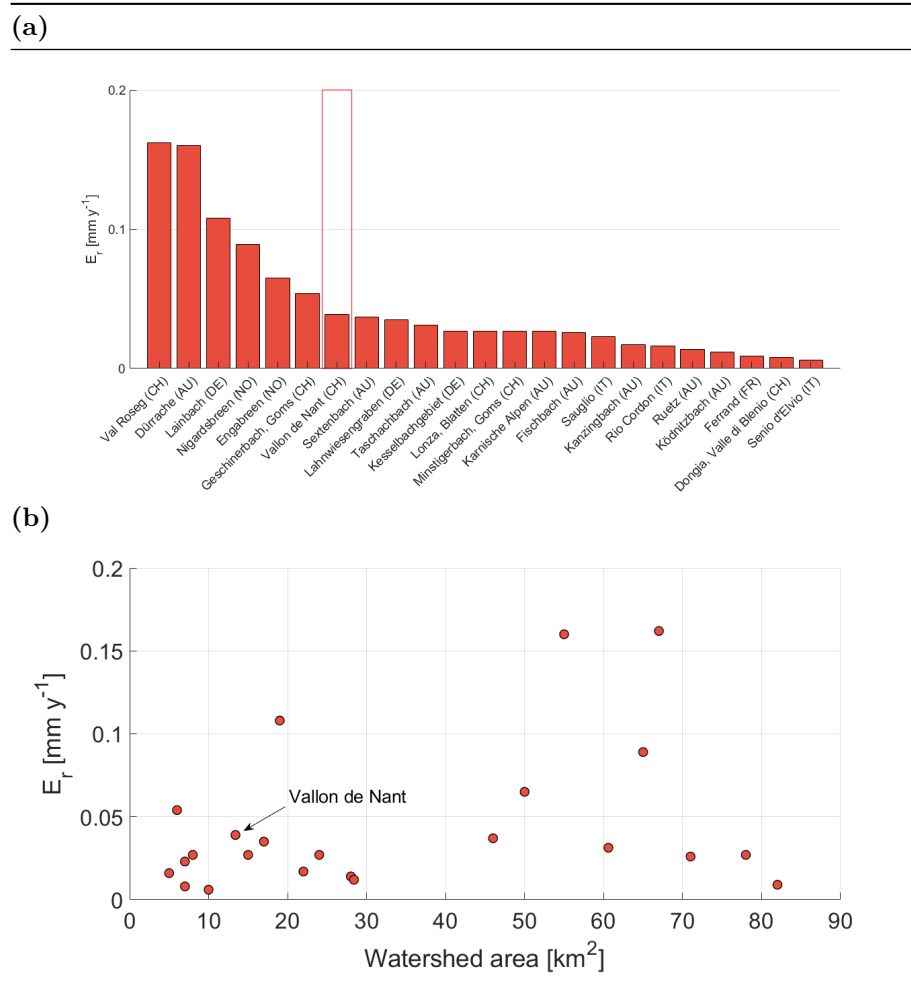


Figure 10. (a) Erosion rates calculated from exported bedload at multiple headwater Alpine watersheds with comparable area and glacier cover as the VdN; (b) Erosion rates against watershed area.

4.2 Hydraulic forcing and bedload transport

The prediction of bedload transport using shear stress-based (i.e. transport capacity) equations have emphasized the likely dominant hydraulic forcing on bedload transport (Figure 5a, 5b, 5d). The relationship between the measured and predicted daily bedload mass (Figure 5d), is notably in general agreement with the 1:1 line, and with previous research, which used the same modified form of the Wilcock and Crowe (2003) equations to compare measured and predicted bedload mass (e.g. Rickenmann, 2020; Rickenmann et al., 2020; Schneider et al., 2015).

Although it is clear that the hydraulic forcing is of importance, the considerable scatter found between the measured and predicted annual bedload (Figure 5b), and in the relationship between daily measured bedload mass and predicted daily bedload mass (Figure 5d), illustrates the importance of other drivers of bedload transport rate. A poor representation of hydraulics near the bed in the driving equations of bedload, in particular around the threshold of motion, represents one set of uncertainties around shear stress-based estimates of bedload transport (e.g. Buffington and Montgomery, 1997; Gomez, 1991). In addition, temporal changes in sediment availability, both as a function of bed material mobility, and as a function of sediment supply from the drainage network (i.e. “travelling bedload”; Piton and Recking, 2017), is another dimension of bedload transport that is poorly covered by capacity-based transport equations (e.g. Rickenmann, 2020). Because the VdN system is likely to oscillate between capacity-limited and supply-limited conditions, the same hydraulic forcing is not expected to systematically induce the same amount of bedload, and this discrepancy is notably visible in the general over-estimation of bedload masses at the VdN when applying the transport capacity-based equations (equations 5a, 5b, 6, 7, 8; Figure 5b).

Many studies have attempted to assess changes in streambed state and associated sediment mobility. Flood regime history in terms of magnitude-frequency was notably found to be an important factor regarding bed armoring cycles and associated sediment mobility (Mao, 2018; Masteller et al., 2019; Rickenmann, 2020). Also, the infiltration of fine material into the bed matrix was also hypothesized as an important control on bed sediment mobility (e.g. An et al., 2019; Venditti et al., 2010). Some research has also attempted to identify potential seasonal trends in sediment availability within Alpine watersheds. Mao et al. (2014) have for instance related the direction of hysteresis loops between streamflow and bedload transport rates to seasonal change in sediment supply from the drainage network. Yet, the balance between bed state and supply from the drainage network in terms of sediment production could not be partitioned. Therefore, the extent to which sediment availability changes through time, and how it affects the relationship between streamflow and bedload transport, remains poorly constrained (Elgueta-Astaburuaga and Hassan, 2019; Reid et al., 2019; Rickenmann, 2020). Sediment availability being a complex variable to quantify, a possible approach for future research could comprise a probabilistic estimate of bedload according to the hydrological conditions met in anyone Alpine watershed. For instance, the results of this study have shown the higher probability of having large bedload transport events during rainy days occurring when the melt signal is strong and baseflow is high, which could reflect both hydraulic forcing and sediment availability conditions. Future research should focus on obtaining distributed estimates of bedload flux to properly quantify change in sediment availability, and its effect on the streamflow-bedload relationship. This could be performed either through the deployment of a network of passive bedload sensors (e.g. Cook et al., 2018; Misset et al., 2021), or through repeated topographical surveys at high spatial and temporal resolutions (Anto-

niazza et al., 2019; Bakker et al., 2019; Dai et al., 2021; James et al., 2020).

4.3 Magnitude-frequency of daily bedload transport during rainfall and the melt season

The approach adopted in this paper allows, for the first time, the comparison of a relatively long-term continuous time-series of bedload export with the hydrological patterns of an Alpine watershed. The visual inspection of 1827 daily flow hydrographs, supported with temperature and precipitation datasets, permitted distinction of daily flow hydrographs influenced by rainfall from the ones that were not. The amplitude of daily flow hydrographs of “not rain-forced” days (Mutzner et al., 2015) was further used to identify five periods with differing melt intensity – the pre-melt, early-melt, high-melt, late-melt and post-melt – that were recurrently met throughout the five years of observation on the one hand, and which varied within a same range of discharge amplitude on the other hand (Figure 4; Table 1).

The results of this study show that the largest quantities of bedload export were associated with a mixed occurrence of rainfall at times when baseflow is high and when the snow-melt signal is still strong (Figure 6, Figure 8, Figure 9). This concerns both the total amount of bedload transported, and the maximum bedload transport intensity reached. At this period of the year, the lower and/or exposed parts of the watershed have already lost snow cover, reducing the storage capacity of the snowpack and exposing more sediment. At higher elevations and/or in sheltered areas of the watershed, large volumes of snow may still be available. Melt has commonly started and subsurface water storage is typically high in the lower parts of the watershed, which is visible in the high baseflow in these periods (Fig5a). When rain occurs in such conditions, the remaining snow cover may provide additional rapid melt but only little additional water storage capacity for incoming water inputs, and significant surface runoff is produced. As the subsurface may already be saturated due to melt and percolation through the snowpack and infiltration into the soil, little incoming water can be absorbed (Corripio and López-Moreno, 2017; Li et al., 2019; Musselman et al., 2018), and a rapid increase in the streamflow hydrograph is expected, favorable to sediment mobilization and bedload transport. In addition, the extension of the stream network (Michelon et al., 2021) may access new sedimentary sources. In comparison, incoming rain occurring earlier in the year (e.g. pre-melt and early-melt period; Figure 6, Figure 8, Figure 9), when the snowpack is colder, more extensive and deeper, can be at least partly stored within the snowpack or in the underlying soil, thus producing a comparatively smaller streamflow response. Retraction of the stream network at this period (Michelon et al., 2021) also reduces the access to sedimentary sources. Under such conditions, little bedload is transported.

Rainfall occurring later in the year, once the watershed snow water equivalent has decreased and the melt signal is not as strong anymore (e.g. post-melt period), can also produce significant amounts of bedload, but to a lesser extent than rainfall occurring during the high-melt and late-melt periods (for both to-

tal bedload per day and daily maximum transport rate), notably because the baseflow is lower (Figure 5a). Intense summer and autumn storms are expected to produce rapid streamflow response and increase bedload transport capacity (e.g. Rainato et al., 2017; Rickenmann, 2020). Those events can produce high transport capacity discharge and bedload transport events (both in terms of total bedload and daily maximum transport rate). However, their magnitude decreases much more rapidly with increasing frequency than for bedload transported during the high-melt and late-melt season (for both “rain-forced” and “not rain-forced” days; Figure 6, Figure 8, Figure 9), again due to lower baseflow at this period of the year. This means that whilst rainfall events of the post-melt season matter for low-frequency high-magnitude events, their role in terms of annual total bedload transported seems less important. Whilst “rain-forced” days dominate the bedload signal at all magnitude-frequency combinations, snow-melt events alone is still capable of transporting a substantial amount of bedload during the high-melt and late-melt periods (Figure 6, Figure 8, Figure 9), when the baseflow is higher.

The dataset to which the observation made in this paper can be best compared is the study of Rainato et al. (2017). The authors investigated the magnitude-frequency of bedload transport events over three decades at the Rio Cordon Alpine watershed (Italian Alps), which was shown to deliver comparable annual bedload yields to the VdN (Figure 10). Over the 31 bedload transport events recorded during the period 1986-2014, a slight majority of them (17) also occurred during the period when snow is still likely present within the watershed (e.g. May-August). Yet, a substantial proportion of bedload transport events also took place when the likelihood of having substantial remaining snow decreases (e.g. September-November). Therefore, the imbalance between bedload transport occurring during the melt season (including rainy days of the melt season), and bedload transport occurring during rainfall once the watershed snow content has significantly decreased, seems to be greater at the VdN as compared with the Rio Cordon. This may be due to particularly intense rainfall during the late summer and autumn at the Rio Cordon (Rainato et al., 2017). However, with no complete hydrological study (e.g. melt signal, rainfall versus melt-driven bedload transport) of the events producing bedload at the Rio Cordon, a direct comparison with the categories developed in this paper remains difficult.

4.4. Bedload transport perspectives under climate change

The dataset presented in this paper shows the importance of the seasonal timing of hydrological drivers for triggering bedload transport, where the seasonal timing is a proxy for the extension of the stream network (Michelon et al., 2021), for the baseflow and for the strength of the melt signal. It suggests the importance of the co-occurrence of rainfall when the melt signal and the baseflow of an Alpine catchment are high. This concerns both low-frequency high-magnitude and intermediate-frequency intermediate-magnitude transport events, and whether for daily bedload total mass or daily maximum bedload

transport rate. It also shows the relative importance of the melt events for intermediate-frequency intermediate-magnitude events (especially for daily bedload total mass). Our results finally underlines the potential of intense rainfall, notably during the summer (high baseflow) and the autumn (intermediate baseflow), for producing significant bedload transport, especially for low frequency high-magnitude events (for both daily bedload total mass and daily maximum transport rate). These results are of importance in the perspective of understanding how bedload transport in Alpine watersheds may evolve with climate change, because the latter is likely to affect both the timing of occurrence and the magnitude of the bedload-driving hydrological events.

A summary of the meteorological, hydrological and bedload transport patterns highlighted over the five years of observation at the VdN, and projections on how these variables could evolve with climate change, is provided in Figure 11. Current mean temperature, rainfall and snowfall have been estimated with the RhiresD and TabsD datasets over the period 2016-2020. Discharge and bedload data come from the VdN monitoring station. Rough projections for the end of the 21th century (2085) were performed using the datasets presented in (CH2018, 2018; FOEN, 2021) and summarized in the paragraphs below.

CH2018 (2018) and FOEN (2021) reviewed modelled climatic evolution of the Alpine region during the 21th century, and highlighted some trends under the RCPs climate scenarios (IPCC, 2014) for the Western Alps. For the RCP4.5 scenario (i.e. moderate warming), temperatures are expected to rise across the Alpine range at all seasons with in average +2.3°C in winter (DJF), +1.9°C in spring (MAM), +2.9°C rise in summer (JJA) and +2.4°C in autumn (SON) until 2085 (CH2018, 2018). Mean precipitation is projected to remain more stable, with changes up to 5-10 % regarding mean annual precipitation until 2085 (CH2018, 2018). Their seasonal distribution is however expected to considerably evolve, with more precipitation in winter (+10 %), even precipitation in spring, less precipitation in summer (-10 %) and less precipitation in autumn (-5 %) for the Northwestern ridge of the Alps (CH2018, 2018; FOEN, 2021). The intensity of extreme precipitation events in all seasons and for most regions is expected to follow the increase that is already observed. Increase in intensity is estimated to be about +20% in magnitude by the end of the century, for both hourly events and multi-day events (CH2018, 2018). Regarding snowfall, they are projected to decrease at all seasons, with -5 to -10% in winter, -20 to -40% in spring and -20 to -40% in autumn (CH2018, 2018).

The impacts of these general climatic trends on high Alpine water resources have long been known (Horton et al., 2006). These impacts are largely related to the evolution of the seasonal snow line (i.e. the average elevation at which snow falls), which is expected to rise by between 300 m and 600 m by the end of the 21th century (CH2018, 2018). Indeed, the wintertime increase in precipitation is projected to not be able to compensate the large loss in snow volume caused by the increase in temperature, except at very high elevations (FOEN, 2021). Less precipitation will thus be stored as snow, the formation of a seasonal snow

cover will occur later in the year, with a shift in maximum snow heights from March to February (CH2018, 2018). Snow-melt is projected to occur earlier in the year, leading to significant shifts of the seasonal streamflow regimes of high elevation watersheds (CH2018, 2018; FOEN, 2021). Groundwater recharge is also expected to evolve with climate change, with an increase of groundwater recharge in winter and spring, and a decrease in summer and autumn, which is of importance to determine change in baseflow (FOEN, 2021).

As a consequence of these changes, the hydrological regime of currently snow-dominated Alpine watersheds such as the VdN is expected to shift to a more rain-influenced streamflow regime by the end of the 21st century, with less snow accumulation, with gentler and earlier snow-melt, and with a monthly streamflow maximum occurring earlier in the year (FOEN, 2021). This will namely result in a marked increase of winter streamflow (+ 80-100%), a moderate increase in spring streamflow (+ 20-40%), a marked decrease in summer streamflow (-40 to -60%), and a moderate decrease in autumn streamflow (FOEN, 2021). Yet, mean annual streamflows are expected to remain generally stable, or to decrease slightly (FOEN, 2021). Regarding high streamflow events, no detailed climate-model based projections are available for Alpine water resources at catchment-scale at the moment because the CH2018 climate scenarios have not been yet downscaled for hydrological purposes to local Alpine conditions.

How could bedload transport evolve together with changes in the hydrological drivers within snow-melt-dominated Alpine watersheds? The increase in the magnitude and frequency of extreme precipitation events, and in the associated magnitude and frequency of floods, has led some researchers to argue for a probable increase in the amount of bedload that will be transported under climate change conditions (CH2018, 2018; FOEN, 2021; Speerli et al., 2020). However, these predictions do not take into account possible change in the hydrological drivers responsible for bedload transport, and this statement can be challenged, to some extent, by the results presented in this paper.

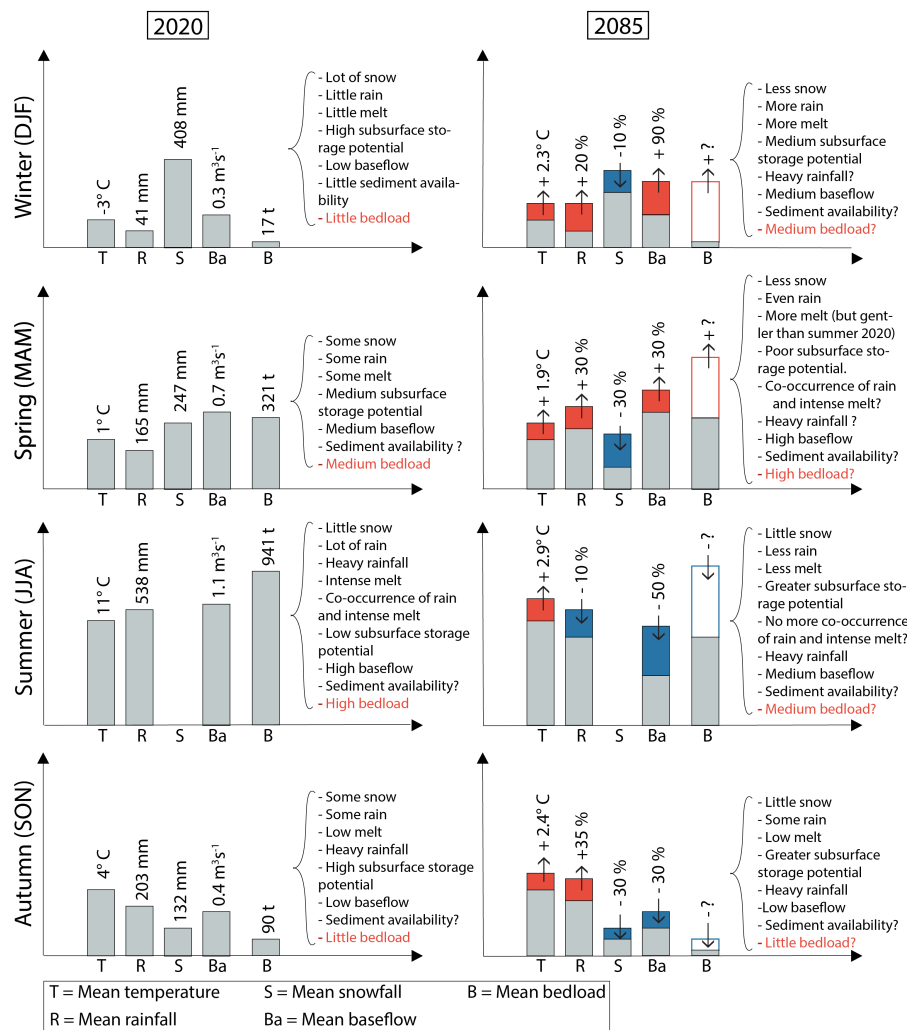


Figure 11. Summary of the meteorological, hydrological and bedload transport patterns observed at the VdN (left panels) over the period 2016-2020. Projections on possible evolutions, and main uncertainties to solve regarding seasonal change in bedload transport with climate change (right panels).

From a hydrological regime shift perspective, the periods of high-melt and late-melt will occur earlier in the year, at lower baseflow (i.e. resulting from a reduced winter snowpack). This shift to earlier periods in the year might reduce the daily melt amplitude because the melt period is shifted to colder periods of the year (Musselman et al., 2017). Accordingly, the contribution of the melt-only events to bedload transport, especially important during the high-melt and late-melt periods, is likely to decrease together with annual snow volumes, due to the combined effect of lowered baseflow and lowered daily flow amplitudes. The

results here show that while it may not affect significantly transport maxima, it may be of importance regarding annual bedload totals (Figure 6, Figure 8, Figure 9).

Translating these changes into meteorological spring and summer periods, we can expect the amount of bedload transport throughout the spring to rise, while the amount of bedload transported throughout the summer can be expected to decrease. A central question that needs to be addressed is whether the importance of the mixed occurrence between heavy rainfall over a watershed where the melt signal is strong and baseflow is high – as occurs currently especially during summer – will be maintained with climate change, or whether a disconnection between the high-melt and late-melt periods and the projected occurrence of heavy rainfall may take place under climate change conditions. If the latter situation occurs, a decrease in the bedload contribution of rain events during the high-melt and late-melt periods is possible in the future.

Another central question regards how the predicted increase in winter rainfall and winter streamflow will impact bedload transport. This general increase of liquid water availability in winter will most likely increase winter bedload transport, but the question of the magnitude of the increase is key. During winter rainfall events within watersheds that continue to show a significant seasonal snow cover, the incoming water may be stored to some extent, filtering out the streamflow and bedload response, as it is visible for current rainfall taking place during the pre-melt and early-melt periods. Thus, the response of any one watershed to winter warming and the occurrence of winter rainfall is likely to depend on its hypsometry (CH2018, 2018).

The last central question regards the increase in heavy rainfall throughout the year. Given that high-magnitude bedload transport events were shown to occur following heavy rainfall events, their timing of occurrence, notably with regards to the co-occurrence with high melt intensity or with high baseflow, may matter to determine the magnitude of the answer of streamflow and bedload transport. It is therefore of great importance to quantify the extent to which the increase in magnitude and frequency of rainfall will affect both maximum values of bedload transport rates and annual bedload export, and whether these events will have the capacity of compensating and/or overcoming reductions of bedload transport that may take place during other periods of the year.

Estimates of the evolution of bedload transport under climate change conditions need also to include expected changes in sediment availability within Alpine watersheds, because the latter matters to determine actual sediment export, whatever transport capacity the streams reach (Lane et al., 2017; Lane and Nienow, 2019; Figure 10). Sediment availability is also expected to change together with climate change, but the sign of the trend remains uncertain. On the one hand, permafrost degradation is thought to increase sediment supply from rockwalls and rockslopes (Messenzehl et al., 2018; Raveland and Deline, 2011), and glacier retreat increases the volume of unstabilized easily-remobilizable material (e.g. Antoniazza and Lane, 2021; Ballantyne, 2002; Carrivick and Heckmann, 2017;

Lane et al., 2017; Mancini and Lane, 2020). Also, the increase in magnitude and frequency of rainfall may increase the frequency of debris flows (e.g. Stoffel et al., 2014) and landslides (Huggel et al., 2012). On the other hand, the effects of climate change may also reduce sediment production, and associated processes (e.g. debris flow) by negative feedbacks such as due to the reduction in the frequency of frost-thaw cycles (e.g. Hirschberg et al., 2021). Similarly, the sustained paraglacial adjustment of Alpine watersheds following the Little Ice Age is thought to lead to the progressive stabilization of glacially-conditioned material (e.g. Antoniazza and Lane, 2021; Ballantyne, 2002; Porter et al., 2019) and to a disruption of sediment connectivity within Alpine watersheds (Lane et al., 2017; Mancini and Lane, 2020; Micheletti et al., 2015; Micheletti and Lane, 2016), which may cause a progressive decrease in sediment transfer. In this context, a critical uncertainty remains to know whether sediment connectivity could also be sustainably enhanced by the increase in the magnitude and frequency of heavy rainfall and high flows (Cossart and Fort, 2008; Porter et al., 2019); or decreased due to feedbacks associated with landscape adjustment to climate change.

An improvement of the modelling and prediction of future bedload export in Alpine watersheds under climate change conditions, based on both field and modelling datasets, is needed for a range of application including flooding risk (Badoux et al., 2016, 2014a; FOEN, 2021; Speerli et al., 2020), hydropower production (FOEN, 2021; Hauer et al., 2018; Pralong et al., 2015) and river ecology (Badoux et al., 2014b; FOEN, 2021; Hauer et al., 2018; Speerli et al., 2020). While multiple studies have suggested an increase in bedload transport within Alpine watershed together with climate change (FOEN, 2021; Pralong et al., 2015; Speerli et al., 2020), the results of this study have shown that this may not be the case depending on how hydrological drivers of bedload will be affected by climate change, notably regarding decreasing snow volumes, the co-occurrence and intensity of future melt periods and heavy summer rainfall, the increase in winter flows and the increase in magnitude and frequency of rainfall.

5. Conclusion

This paper presents a five-year time-series (2016-2020) of bedload transport monitored with the Swiss Plate Geophone (SPG) system at the VdN Alpine watershed, in the Western Swiss Alps. Based on concurrent and independent samples of bedload transport collected during natural bedload transport events with a mobile sediment basket, a calibration relationship was established to infer bedload mass from the number of impulses of the SPG system. A hydrological analysis of the streamflow time-series was also performed in order to distinguish daily flow hydrographs influenced by rainfall from the ones that were not. The amplitude of daily flow hydrographs of days not influenced by rainfall was used to partition the year into periods with different melting intensity. This approach permitted the integration of bedload transport over the different hydrological categories driving it. The analysis over the five years of observation shows the importance of the co-occurrence of rainfall in a watershed with a snow-melt

signal and baseflow that are high enough to frequently produce high-magnitude and intermediate-magnitude bedload transport. High-magnitude low-frequency bedload transport is also shown to occur when the melt signal is much weaker, but the magnitude-frequency of daily bedload masses declines much quicker than when the melt signal is still strong due to lower baseflow. Although rainfall seems to represent the dominant driver of bedload transport (both during and after the melt period), bedload transport can also be caused by the melt-only events, but contribute to a greater extent to bedload totals, as compared to maximum transport rates. The analysis also shows the importance of sediment availability influencing the relationship between streamflow and bedload transport, which requires more attention within future research.

The investigation of hydrological drivers of bedload transport is of importance for a range of current applications, including flooding risk, land planning, hydropower production or river ecology. It also matters regarding how these hydrological drivers will evolve in combination under climate change conditions. Although there are some concerns that bedload transport in Alpine watershed may increase together with the magnitude and frequency of rainfall and floods, the results of this study show that the timing and co-occurrence of hydrological drivers (i.e. rainfall, melt, baseflow) matters to determine the magnitude and frequency of bedload transport. As such, it is not clear yet how those elements and their temporal interplay will evolve under climate change conditions. The paper further discusses the importance of including the evolution of sediment availability under climate change conditions in future research on bedload transport, because the latter is still too poorly constrained.

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Conflict of interest statement

The authors declare no conflict of interest.

Data availability statement

All data presented in this paper will be made available online on the EnviDat repository <https://www.envidat.ch/#/metadata/sediment-transport-observations-in-swiss-mountain-streams> upon publication of the manuscript.

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