



SPIRAL II Project (electron option) - Preliminary Design Study

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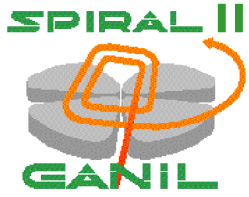
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 <p>Laboratoire CEA/DSM - CNRS/IN2P3</p>	SPIRAL II PROJECT (electron option)	page 1/36
	Preliminary Design Study	GANIL/SPI2/007-A

TITLE

Preliminary Design Study (PDS) of the project SPIRAL II (electron option)

SUMMARY

This document presents :

- 1 - the objectives of the project
- 2 - the general principles of the radioactive ion production
- 3 - a technical description of the facility
- 4 - the radioactivity issues and the consequences on the safety
- 5 - a proposal of implantation on the GANIL site
- 6 - an estimation of the planning construction
- 7 - an estimation of the cost of the project

DOCUMENT PURPOSE

This document has been written, in its initial version, for :

The SPIRAL II International Committee
The GANIL Scientific Council
The GANIL Directory Committee

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1. Objectives

This document presents a Preliminary Design Study (PDS) of the electron option of the SPIRAL II project. This PDS is based on the SPIRAL II PDS carried out in 2000 and 2001 by a working group supervised by D.Guillemaud-Mueller whose initial task was to compare technically the two following options : [1]

- fission of uranium by photons created by Bremsstrahlung from electrons accelerated up to 45 MeV by a superconducting linear accelerator (electron option)

- fission of uranium by fast neutrons (40 MeV) created by fragmentation of deuterons accelerated by a cyclotron up to 80 MeV (deuteron option)

During this study, a third option has been introduced and compared with the previous options :

- fission of uranium by fast neutrons (20 MeV) created by fragmentation of deuterons accelerated by a superconducting linear accelerator up to 40 MeV, this linear accelerator being the first step of the LINAG project (LINAG I option)

The directors of GANIL, estimating that the data contained in the APS report were not sufficient to trigger a decision, required a complementary study for the electron option and for the LINAG I option.

The complementary study, carried out during the first five months of 2002, has tried to better describe the points which were technically a challenge, in particular the target design and the safety issues and to precise the plannings and the costs.

2. Ion Production

2.1. Photofission Principle

Fission can be induced by photons exciting the Giant Dipolar Resonance (GDR) of the nucleus. This well-known process is called photofission.

The GDR cross section for ^{238}U is shown on Figure 1 below.

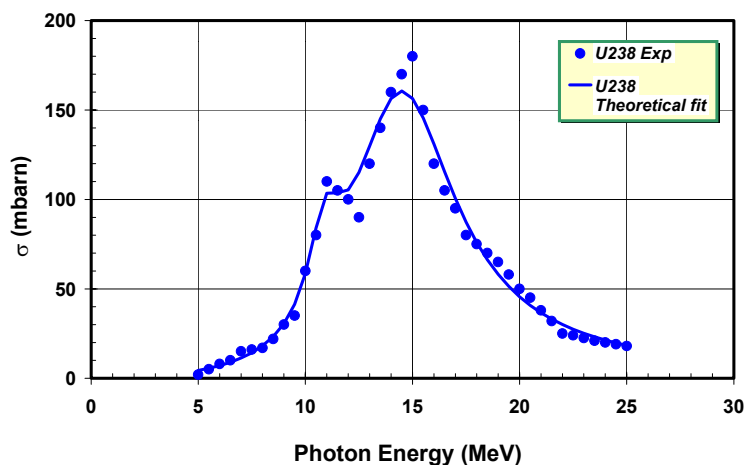


Figure 1 Giant Dipolar Resonance (GDR) cross section

A maximum fission probability of 160 mb is obtained for photons having energy around 15 MeV. At that energy, the photoelectric and the Compton and Rayleigh scattering cross sections are starting to fall off rapidly so the main contributions to gamma absorption are e^+e^- pair production and the photonuclear reactions (γ, f) , (γ, n) and $(\gamma, 2n)$. Although the absolute fission cross section is rather small (compared to normal fission with neutrons), its contribution is not negligible as even a pair production reaction may in a thick target eventually lead to a fission through the resulting photon produced. In the same manner the neutrons produced by (γ, n) and $(\gamma, 2n)$ reactions as well as the (γ, f) itself can also induce fission, this time by the regular (n, f) high cross section (0.5 barn for fast neutrons). Therefore, in a thick target, photofission may be a rather interesting way of creating radioactive fission fragments.

2.2. Electron Beam Energy

Unfortunately, no efficient monochromatic sources of 15 MeV photons are available. The most common way for producing high gamma fluxes is the Bremsstrahlung radiated by passage of electrons through matter. This process has a cross section rising linearly with energy. It will dominate the ionization process above a critical

energy (around 20 MeV). But the resulting Bremsstrahlung spectrum is widely spread in energy from zero up to the full initial electron energy (Figure 2 below). Although each single electron may ultimately produce as high as 20 photons, only a small fraction of it (0.5 to 0.7 gamma per e⁻) are "useful" photons lying in the GDR range (15 ± 5 MeV).

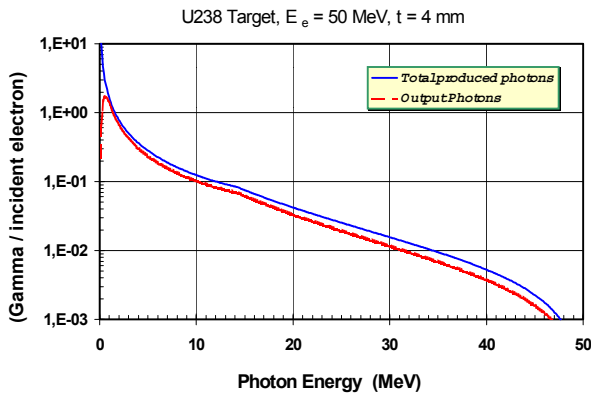


Figure 2 Bremsstrahlung Yield vs photon energy

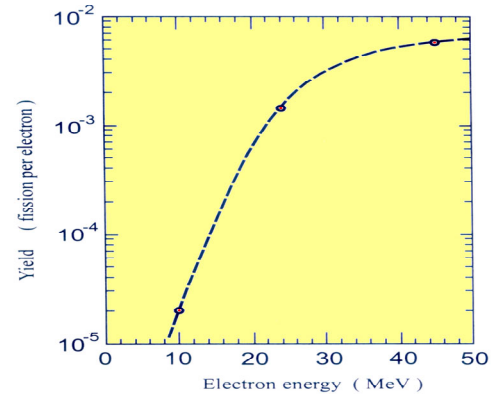


Figure 3 Fission yield vs electron energy

A simple calculation including the main electron interactions (Bremsstrahlung and ionization) and the main nuclear reactions of interest (pair production and fission cross section) in a thick depleted uranium target can give the expected number of fission per incident electron. In Figure 3 above, the number of fissions produced by the (γ, f) reaction is plotted as a function of the electron energy. This result is a complete Monte Carlo calculation performed with a MCNP code offering also photonuclear capability (full electron, photon and neutron transport). The obtained result is in accordance with the simple analytic calculations.

Electron energy around 45 MeV seems a good compromise.

2.3. Electron Beam Intensity

Gamma can be produced by using a tungsten converter (4 mm thick) in front of the ²³⁸U target or by using directly the ²³⁸U target. It appears that when using a converter, less than 30% of the beam power is lost inside the converter (in contrast to the deuteron driver option). In the direct method one will produce about 25% more fission per electron (and probably more when taking in account neutron induced fission).

In order to compare photofission with and without converter, measurements of Kr and Xe isotopic distributions produced by photofission and diffused out of a thick UCx target has been performed using the PARRNe1 device in the same conditions that with deuterons beams and with the same target (see Figure 4). The measurements have been done with a 4 mm W converter in different positions (8 mm from the target, 4 mm from the target) and one measurement without W converter. Comparison with the 80 MeV deuteron induced fission measurements are also presented.

The following

Table 1 sums up the results with converter (at 4 mm in front of the target) and without converter to reach the goal of 10¹³ fissions/s.

for 10 ¹³ fissions/s	beam intensity	beam power	power inside the converter	power inside the target core
with converter	5 mA	225 kW	80 kW	6 kW
without converter	0.5 mA	22.5 kW	x	11 kW

Table 1 Comparison of the power levels between using or not using converter

As the use of a converter increases drastically the beam intensity without decreasing significantly the power inside the target, the best option is to use the target without converter.

Consequently, the required beam intensity will be roughly 500 μA (= 3.10¹⁵ e⁻/s) directly on the target.

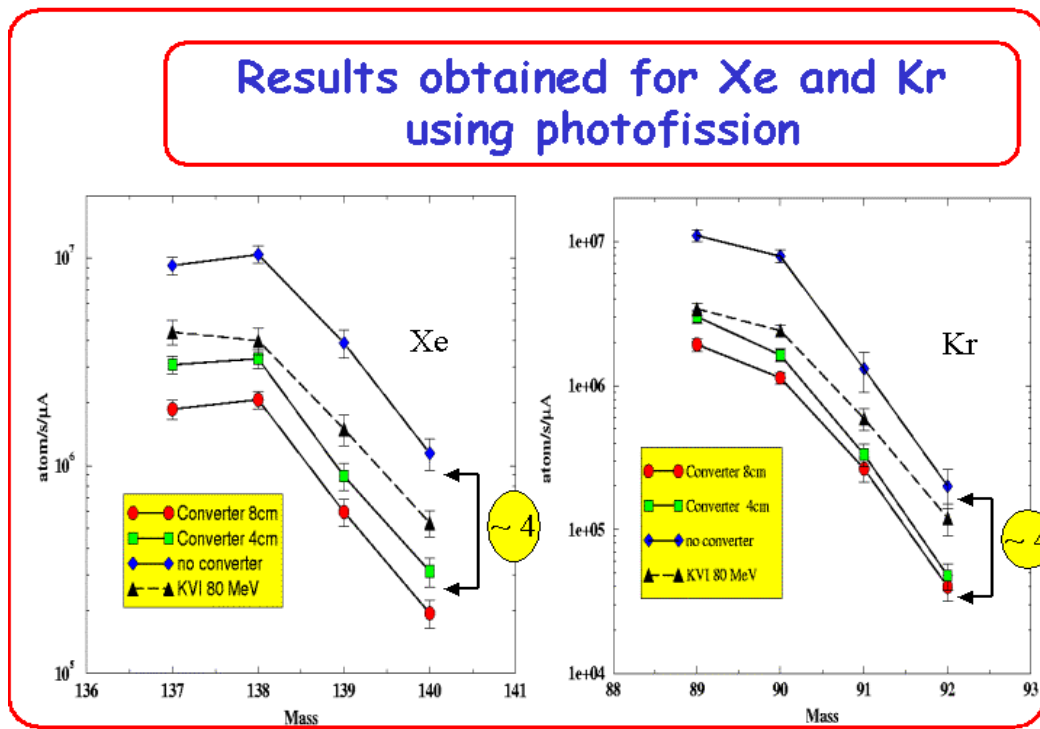


Figure 4 Experiments carried out with the LEP preinjector (collaboration IPNO - DAPNIA - GANIL)

2.4. Radioactive Ion Production Rate

The Figure 5 below shows the radioactive ion spectrum produced by the photofission. This computation has been carried out with the code ORIHET which is an adaptation of the code ORIGEN from Oak Ridge. This spectrum does not take into account the nuclei produced by neutron induced fissions, neutrons provided by the photofission itself or by the (γ, n) and $(\gamma, 2n)$ reactions. These nuclei produced by neutrons represents roughly 5 % of the photofission induced nuclei and does not change the spectrum shape.

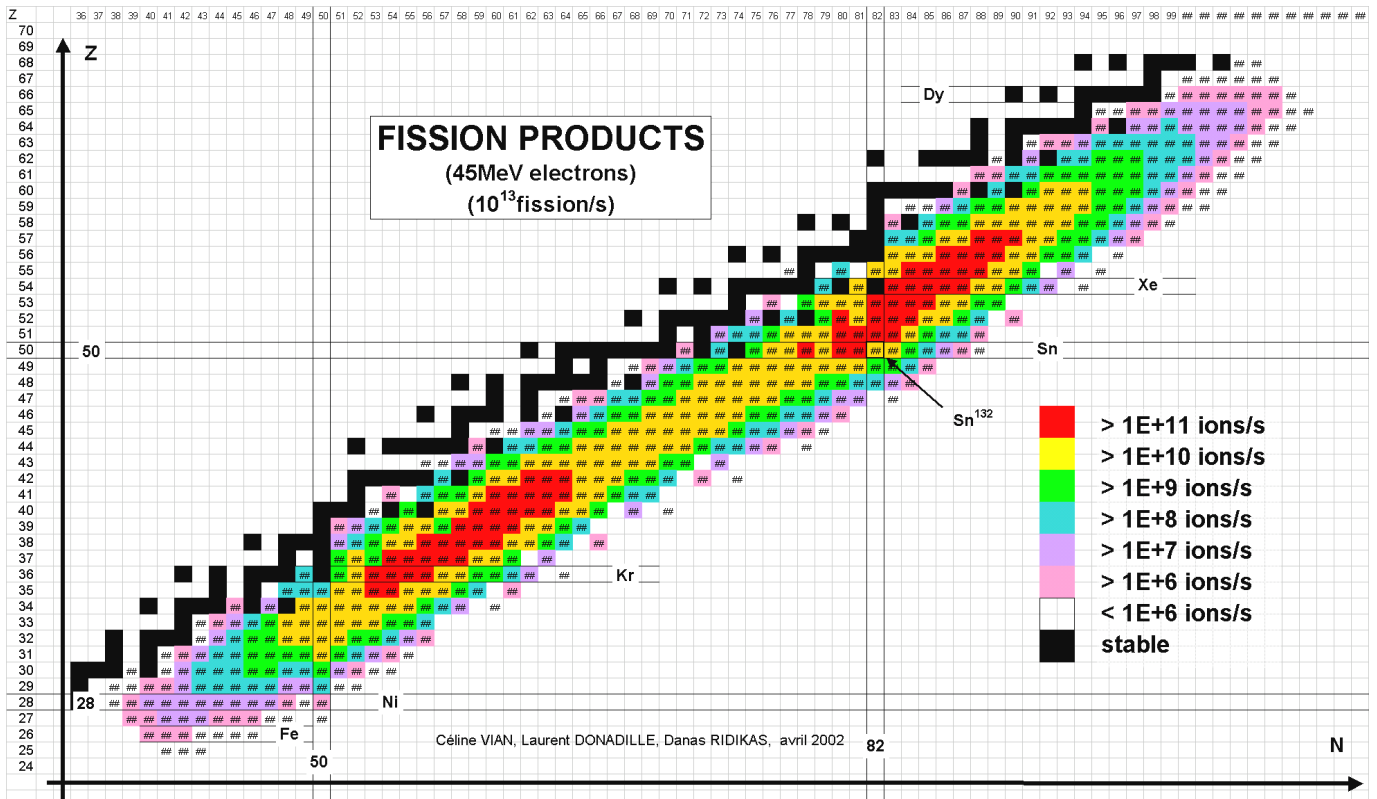


Figure 5 Fission Products Spectrum

Taking into account the transmission efficiency of the various components (target, source, charge breeder, CIME) and the life time of the ions, the flux of radioactive ions provided to experiments could be the following (order of magnitude for some samples) :

Xe ¹³⁹ or Xe ¹⁴⁰ :	10 ⁹ to 10 ¹⁰ ions/s
Xe ¹⁴⁴ :	10 ⁷ to 10 ⁸ ions/s
Kr ⁸⁹ to Kr ⁹² :	10 ⁹ to 10 ¹⁰ ions/s
Nb ¹⁰⁰ to Nb ¹⁰⁵ :	10 ⁹ to 10 ¹⁰ ions/s
Sn ¹³² :	10 ⁸ to 10 ⁹ ions/s

The lightest ions produced are around Fe (2.10⁶ ions/s of Fe⁶⁸ produced in the target)

The heaviest ions produced are around Dy (2.10⁶ ions/s of Dy¹⁷¹ produced in the target)

These production rates will be better estimated when all the components are designed and tested. In particular, the effusion-diffusion inside the target can change drastically the effective production at the output of the target for the condensable elements.

3. Technical Description of the Facility

3.1. Electron Accelerator

3.1.1. General Layout

The accelerator layout is shown on Figure 6 below and is quite similar to the MACSE project [2]. The injector comprises a 100 keV gun and a short cryomodule containing a single superconducting cavity. At the injector exit, the electron beam is already well relativistic. Then the beam runs in a long cryomodule through four SCRF cavities bringing the electrons to the final energy of approximately 45 MeV. A bending magnet followed by a transport beam line will get the beam at the right place and shape onto the target.

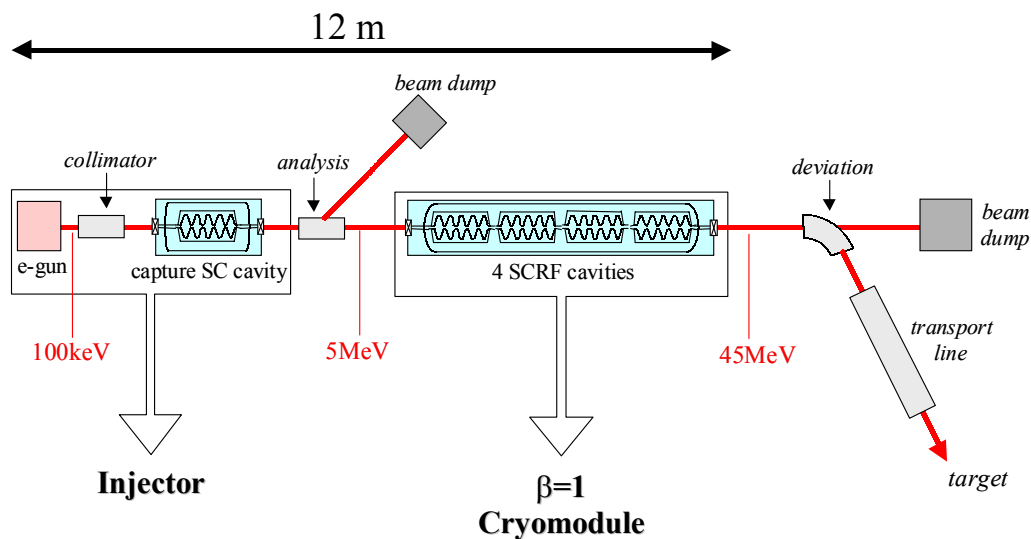


Figure 6 Layout of the electron driver

3.1.2. Gun

The gun uses a standard thermoionic cathode sited on a 100 kV platform. The power supply can deliver up to 3 mA in current. In order to bunch the beam at the proper frequency of 1.5 GHz, a specific line consisting of two rectangular RF cavities (chopper) are used to cut a 60° phase out of the DC beam delivered from the cathode. Another cylindrical cavity (buncher) is used to bunch the beam down to a 10° phase at the entrance of the capture cavity.

An attractive alternative method would be to set up a gridded cathode similar to the one used in Inductive Output Tubes (IOT). In that way, the beam could be bunched right from the starting emission point that suppresses the need of the rather cumbersome bunching line. This new technique could be tested at CEA/Saclay and if successful, will be implemented on the SPIRAL II machine.

A collimator can be placed after the gun in order to control the beam emittance. This could be of importance for safety and radiation issues (see § 4.2.1) as undesired beam tails can be quite easily suppressed at that stage without creating too much radiation.

3.1.3. Capture Cavity

The capture cavity is a superconducting cavity with a reduced beta value due to the not fully relativistic beam coming out from the gun. Geometry has to be optimized to properly capture the beam without degrading too much the longitudinal emittance. Figure 7 below shows some simulations where different cavity shapes have been studied.

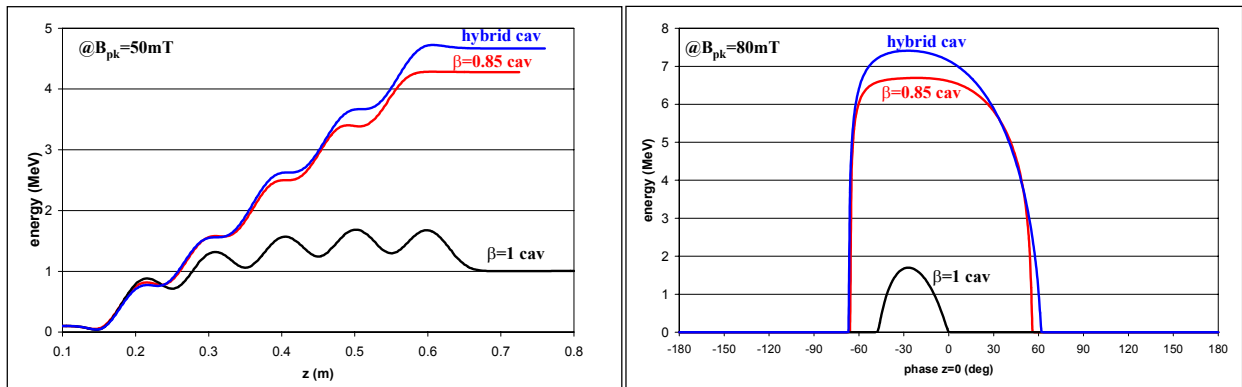


Figure 7 Output energy as a function of position and phase for three different cavity shapes. A $\beta = 1$ cavity is clearly not adequate to use as a capture cavity.

The output dispersion of the beam shown on Figure 8 below is simulated for two different cavity shapes assuming an input beam with 200 eV and 30° extension in phase. It can be noticed that the output beam will feature less than 40 keV and 5° in the longitudinal phase space.

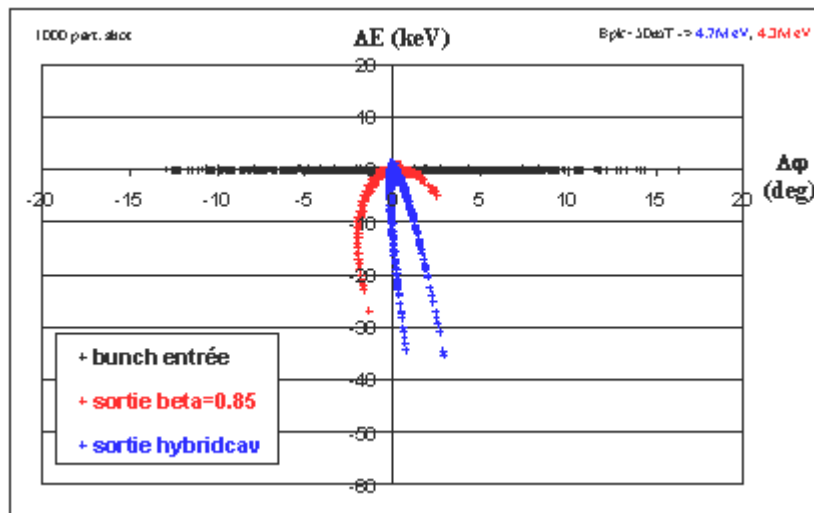


Figure 8 Longitudinal dispersion at the output of the capture cavity for two different shapes

3.1.4. SCRF Cavities

The four SCRF cavities are standard $\beta=1$ elliptical cavities working at the resonance frequency of 1.5 GHz. The characteristics of these cavities are summarized in Table 2. The important thing to point out is the high accelerating field operation (19 MV/m) and the very low bandwidth (40 Hz) due to the low beam current.

The cavity will use an integrated helium tank vessel and a specific tuner will have to be developed. A great care should be taken as regard to the low bandwidth. Therefore, any improvement made on tuners developed in the frame of the CEA/Saclay-IPN/Orsay collaboration for SCRF cavities could be implemented in SPIRAL II. For example, the use of piezoelectric tuners if demonstrated would be of great benefit.

SPIRAL II SCRF CAVITY					
Frequency	1 500	MHz	Beam Power	4,756	kW
β	1,000		Dissipated Power	9,058	W
λ	0,200	m	Incident Power	4,767	kW
$(\beta*\lambda/2)$	0,100	m	Incident Q	3,80E+07	
$(r/Q)/\text{cell}$	50	Ω	Zero Current Voltage	1,90E+07	V
			Slope X	1,90E+10	Ω
Number of cells	5		V	9,52E+06	V
Bpeak	80	(mT)			
Bpk / Eacc	4,2				
Eacc	19,05	(MV/m)	All External Q's	1,00E+11	
Q0	2,00E+10		Loaded QL	3,79E+07	
Length	0,500	m	Bandwidth (2. Δ f)	40	Hz
(R/Q)	250	Ω			
			α inc	0,997724	
Stored Energy	19,222	J	α cavity	0,001897	
			α ext	0,000379	
Maximum Voltage	9,52E+06	V	Reflected Power	1,72E-04	W
Beam Current	5,00E-04	A	Cavity Losses	9,058	W
Phase	2,000	degrees	Transmitted Power	1,812	W
Actual Voltage	9,51E+06	V			
Energy Gain	9,512	MeV			
Detuning Angle	-1,992	degrees			
Cavity Frequency	1 500,000	MHz			
Frequency Shift	-0,69	Hz			

Table 2 Typical SCRF cavity characteristics.

3.1.5. Cryomodules

Two separate cryomodules are needed. The first will house the single capture cavity and the second one the four SCRF $\beta=1$ cavities. These cryomodules are similar to the one used on the MACSE test bed but will be modified to take into account the fact that the helium vessel is suppressed, each cavity having an individual helium tank. Schematic drawings of the largest cryomodule are shown in Figure 9 and Figure 10.

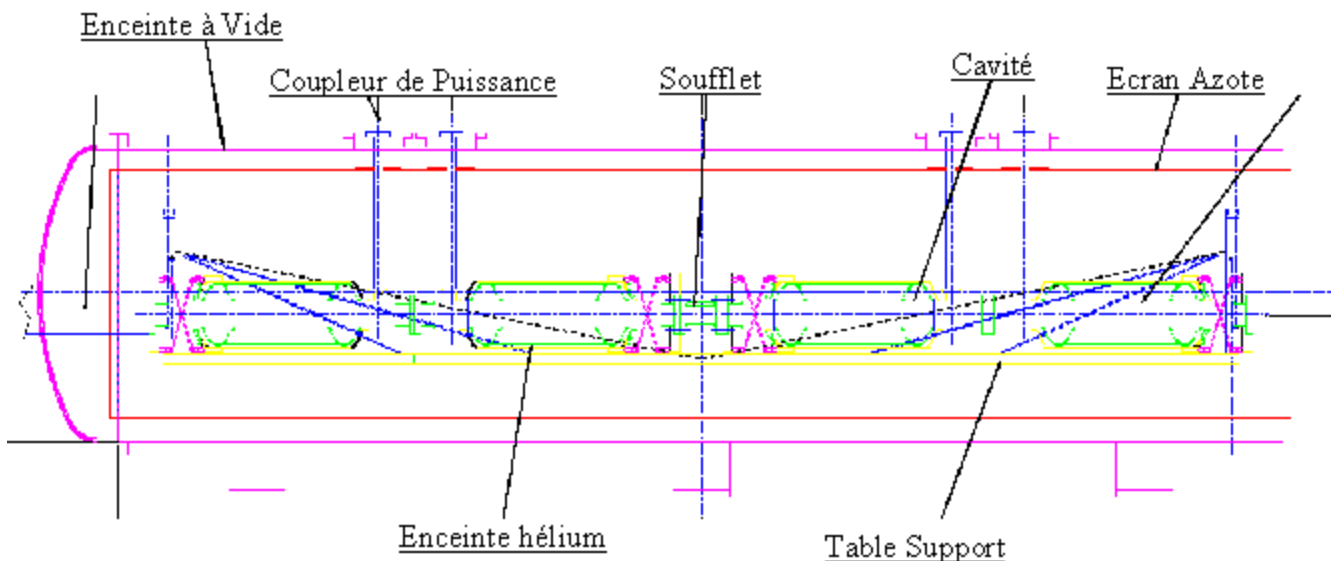


Figure 9 Longitudinal view of the cryomodule.

The assembly of cavities and couplers has to be done inside a class 100 clean room in order to avoid dust contamination. The assembly can be done outside the clean room provided the cavity/coupler ensemble is leak tight and sealed. The insertion in the cryomodule of the full 4-cavity assembly has to be done from the side.

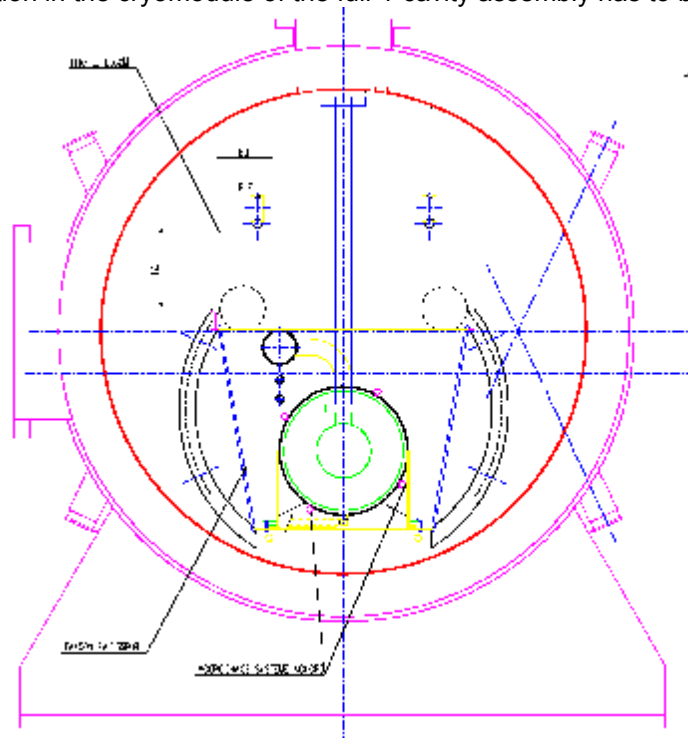


Figure 10 Front view of the cryomodule. The cavity is laid on a cooled table in a cradle shape structure on the bottom side of the helium vessel.

3.1.6. Power Coupler

The power coupler is an important (and weak) element bringing the RF power from room temperature down to the cold cavity. It should be stressed that even though the power level is rather low (5 kW), this item should be developed and fully tested during the TDS phase. If not, the overall schedule would shift as the power coupler is on the critical path. Moreover, in view of a future upgrade, it would be very interesting to check whether the power coupler could be designed to withstand a CW power of 100 kW. Some basic parameters for the two options (5 kW & 100 kW) are described in Table 3. Basically the external diameter should be higher for the high power operation to avoid the multipacting bands. The mechanical impact on the cryomodule mounting has also to be thoroughly analyzed. The TDS work should determine if a high power coupler could be safely implemented at that stage or not.

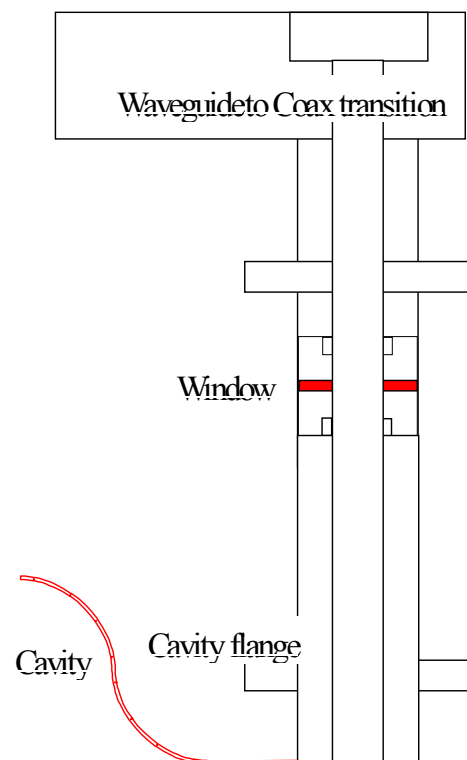


Figure 11 Schematic design of the coaxial coupler for SPIRAL II.

Parameters	5 kW	100 kW	
External Diameter (mm)	41.3 (note)	41.3 (note)	80
Impedance (ohms)	50	50	50
Internal Diameter (mm)	17.9	17.9	35
First Multipactor Barrier (kW)		125	1765
Total Dissipated power at 300K (W/m)	25.7	514	265
Inner Conductor Dissipated Power at 300K (W/m)	18	358	185
Outer Conductor Dissipated Power (W/m)	7.8	156	80
Inner Conductor Maximum Field (kV/cm)	0.95	4.23	2.18
Outer Conductor Maximum Field (kV/cm)	0.41	1.84	0.95
Dielectric Losses in the Window (W)	1.4	28	28
Inner Conductor Losses cavity side (W)	5.4	107	55
Thermal Gradient at the Window (K)	3.5	68.7	42

note : standard 1"5/8

Table 3 Coaxial power coupler parameters for both the 5 kW and 100 kW options

3.1.7. RF Source

The RF power is a 5 kW CW klystron TH2466 from Thalès (formerly Thomson) company. A complete RF power source includes :

- The klystron tube (5 kW CW)
- A power supply (11 kV, 1.2 A)
- A waveguide WR650 circulator (5 kW any phase)
- A water power load WR650 (5 kW CW)
- Miscellaneous waveguide components, couplers, elbows, transitions, etc...

The RF tube could be installed right close to the cryomodule minimizing the length of waveguides and reducing the RF losses.

3.1.8. Low Level RF

SCRF cavities have to be regulated in frequency, field amplitude and phase. A precise regulation is required to maintain the cavity at the right frequency and the accelerating field at the right value and phase. The frequency is controlled using the cavity tuning system to better than 1 Hz. It is generally a rather low speed (typically one second) when using the stepping motor. A high gain feedback loop for cavity phase and amplitude is necessary to compensate for mechanical vibration and microphonics. It should be possible to obtain with a properly designed phase lock loop a field control better than 1% and a phase control better than 0.1 degree. Each cavity has to be driven by a single RF power source. This is very important to guarantee the phase and amplitude control.

3.1.9. Beam Transport

The beam transport is rather simple taking in account the fact that a 45 MeV electron beam is highly relativistic ($\gamma \sim 90$). In particular, no specific focusing is required inside the cryomodules. An intermediate analysis line could be useful in between the two cryomodules (at an energy of 5 MeV) in order to fully characterize the beam at the exit of the capture cavity.

3.1.10. Diagnostics and Control

The diagnostics required for the driver are of two types. The first type is mainly for operation to check whether the parameters are properly set as expected and do not change with time. That includes beam current monitors, beam position monitors, beam profile measurements (during commissioning) and all current measurement of the magnetic elements. For the cavities, the RF signals will be measured (input, reflected and transmitted fields) together with frequency (phase), amplitude and error signals. Cavity vibrations could also be measured using a piezoelectric device on the tuner mechanism. X-ray signal in case of field emission could be monitored using simple diodes. Of course, all cryogenic diagnostics like helium pressure, temperature and mass flow will also be measured on line, in addition to vacuum measurements, especially on sensitive locations like the gun or the cryogenic insulation vacuum.

The second type of diagnostics will be used for interlocks in case of severe failure leading to beam interruption. First, for safety reasons, beam losses should be maintained below a given value. Therefore, they should be continuously measured online using for example a calibrated differential current monitor at the beam exit. Then, all possible failure scenarios for each element (gun, cavity, cryogenics, RF power source, RF coupler, vacuum leaks, etc...) should be investigated and interlocks set to mitigate each case. A common failure

scenario is for example a vacuum leak in the cryostat insulation. Mitigation in this case would include a specific device added (as a rupture disk) at a calibrated pressure (2 bars) and a corresponding beam interlock.

3.1.11. Cryogenic Plant

The required cryogenic power is of the order of 150 W at the working temperature of 1.9 K including the static losses, the power coupler losses and a standard margin. The Héliol 2000 liquefier from Air Liquide can fulfill these requirements. Using nitrogen pre-cooling, its performance can reach 130 l/h in the liquefying mode and over 400 W (@ 4.5 K) in the refrigeration mode. This liquefier has many interesting characteristics as the static gas bearing expansion turbines and the industrial oil lubricated screw compressor. It offers the remote monitoring from a distant location (control room) through a fully automated controller.

Although the liquefier is the major component of the cryogenic plant, the overall plant should include the liquefier (150 W @ 1.9 K), a large dewar, a helium compressor, a storage tank for helium gas, a pumping station, transfer lines for helium and nitrogen, a liquid nitrogen reservoir and all ancillary components : controller, gas purification, heater, etc...

3.2. Electron Beam Line

The electron beam is sent horizontally upon the target. Because of the beam energy stability which is estimated to 2 %, a doubly achromatic deviation is thought useful so that the instabilities on target are avoided. Two 90° bending dipoles and 7 quadrupoles are needed (see on Figure 13 below).

The magnetic rigidity being small (0.15 T.m..), the size of the magnetic elements are small too. For instance, the size of dipôles could be 500x500x300 mm³ and their weight about 300 kg.

According to the target size and shape, the beam spot can be moved using a pair of deviating magnets. This easily allows covering any area shape on the target. For example, an annular beam can be formed using only 0.05 T deviating magnets in the (xy) planes and located 2.5 m away from the target.

The tuning of the linac will be carried out by sending the full intensity beam on a beam dump (see § 3.3)

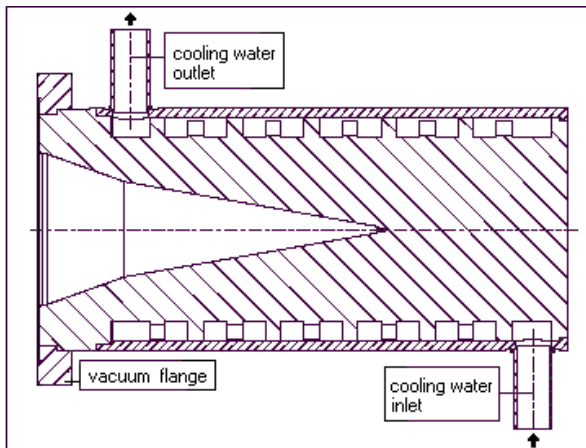


Figure 12 Beam Dump Principle

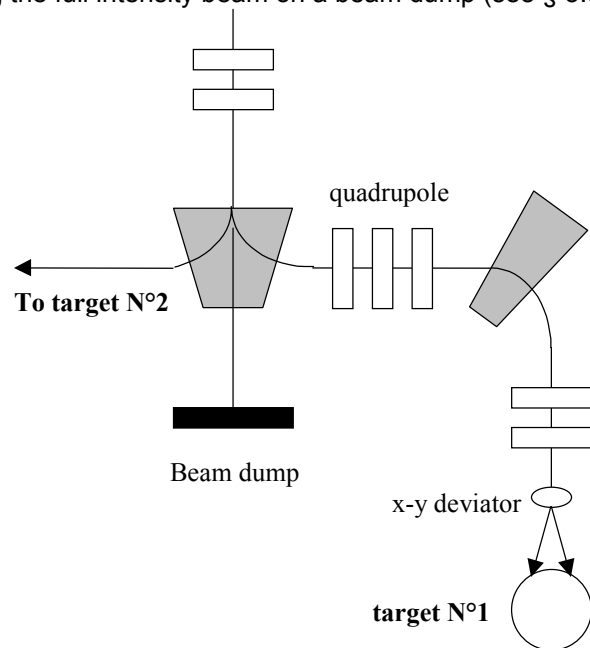


Figure 13 Electron Beam Line Principle

3.3. Beam Dump

The full intensity beam can hit the beam dump, which means that the 22.5 kW power of the beam must be evacuated. The core must be cone-shaped and the beam defocused to spread the beam power (see principle on Figure 12 above)

Moreover, the materials must be chosen to reduce as more as possible the activation and the outside radiation (see § 4.3.1)

The beam dump designed of the ELBE project could be used as an example. [3]

3.4. Production Target

3.4.1. Introduction

The target material is based on the use of depleted uranium. In order to release efficiently by diffusion in the solid matrix the fission products, the target has to be heated to the highest possible working temperature (around 2000°C). Therefore, a ceramic compound of uranium able to withstand that temperature without degradation has to be selected like for example uranium carbide. But the carbide has many thermodynamic phases depending on temperature and composition. Moreover, the metallurgical form is also of importance as for example the open porosity or the small grain size which are proved to be better for the diffusion process. As a consequence, a full and proper characterization of the material target (fabrication process, density, porosity, phase composition and proportion, thermal properties like thermal conductivity at 2000°C, emissivity, etc...) is thoroughly needed as it may strongly impact the target design. It is important to notice that the optimal target for photofission should clearly be somewhat different from the usual ISOL type target used until now with neutron beams all around the world.

One important issue for the target is its thermal capability. Due to the fact that a significant fraction of the beam power will be deposited inside the target, a proper management of the heat transfer inside the target is needed. Therefore, an annular target geometry has been selected for the two main following reasons :

- it allows a much better heat transfer to the outer wall and a better flatness of the radial temperature distribution inside the target,
- it offers the great possibility of taking out very rapidly the short lived radioactive fission products by an effective effusion through the wide open central area.

Therefore the target geometry will look like a long hollow cylindrical shape containing a stacking of several uranium carbide washers. Consequently, the incoming beam has to be shaped accordingly to the target cross section. But the annular shape required is quite easy to deliver with a relativistic electron beam, as any shape, even quite cubersome, could be painted on the target using a set of different magnetic coils and quads. As a matter of fact, in § 3.2, a very simple arrangement using a set of deviating magnets 90° out of phase, is proposed to establish the desired beam profile on the annular target.

The technology to produce these thin uranium carbide disks has to be demonstrated in the Preliminary Design phase. The present technology commonly used either at IPN Orsay (Parrne) or at CERN (ISOLDE) enables to fabricate (by cold pressing of a mixture of uranium oxide and graphite powders) disks of 14 mm in diameter and about 1 mm thickness. Larger diameters could eventually be achieved with the same technology but it is unlikely that much thinner material could be fabricated using the same process. Therefore, a different technology is proposed to obtain the required uranium carbide disks geometry. Based on already commercially available 0.125 mm shaped graphite washers, the fabrication process will use a thin uranium layer deposition followed by an adequate heat treatment. This new technology is presently under investigation at CEA Saclay.

As a result, an example of a target design that could be used for a photofission target is shown on Figure 14

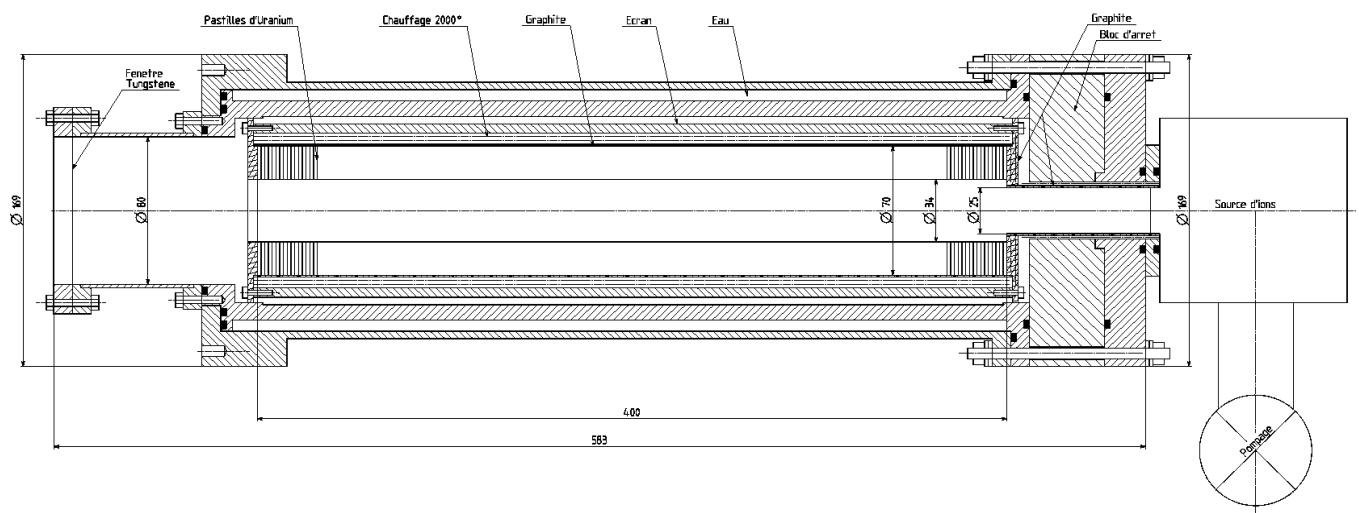


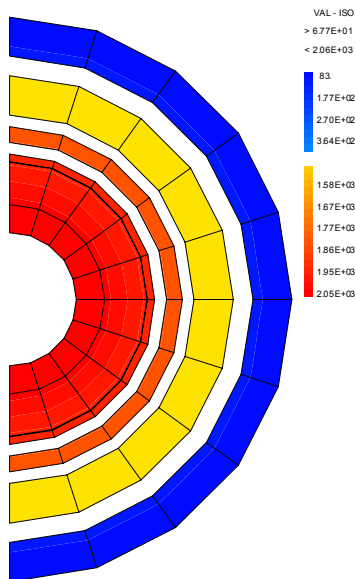
Figure 14 Target Design and Geometry

3.4.2. Heat management

A complete calculation of the temperature profile inside the target has to be done in order to assess its thermal capability. Therefore, even though the total deposited heat is only about 50% of the beam power, the target has been designed to withstand the full power beam heating (22.5 kW). The final temperature will be achieved by adding some external heat power through a heater installed quite close (or even bounded) to the target container.

First in the radial direction, the deposited heat by the beam is transported through the matrix to the outer container wall (mostly by conduction, but also due to the high working temperature, the radiation transfer has also been taken into account). A contact resistance between each disk and the container has been assumed. From the container to the outer cooling, channel, the heat transfer is done mainly by radiation. Therefore, a screen has to be added in between the cooling outer shell (containing the water flow) and the target container (where the temperature has to be maintained at 2000°C). It is important to notice that our heat problem is neither a regular target type (where the heat has to be evacuated very efficiently), nor an oven type (where the insulation has to be very effective to maintain a high temperature at low flux). Here, both the deposited heat and the temperature are fixed. So, the heat problem has quite well constrained boundary conditions. A first order simple calculation give the radial temperature profile in the center of the target. This profile is confirmed using complete 3-D calculation (based on CASTEM code) and shows that a temperature of 2000°C can be readily achieved in the target even using a full power beam deposition (20 kW). In those calculations, an average thermal conductivity of 20 W/m.K has been assumed for the uranium carbide.

There are two possible ways of achieving the most uniform temperature longitudinal profile. Uniformity is desired for two reasons : avoiding the hot spots that may induce local overheating and even damage and avoiding the cold spots where the fission products can have longer sticking time. The first way is to design the target to spread out the interaction all along the beam path. This can be done either by shaping the disk profile and/or the beam or by changing the disk composition. The second way is to compensate the underheating of the second half part of the target by adding a separate heater. Of course, both ways could be simultaneously implemented to finally achieve a quite uniform smoothening of the deposited heat all along the z axis. Of course, a special care has to be taken for the end parts as they will also be affected by radiation especially on the back side.



Champ de température final

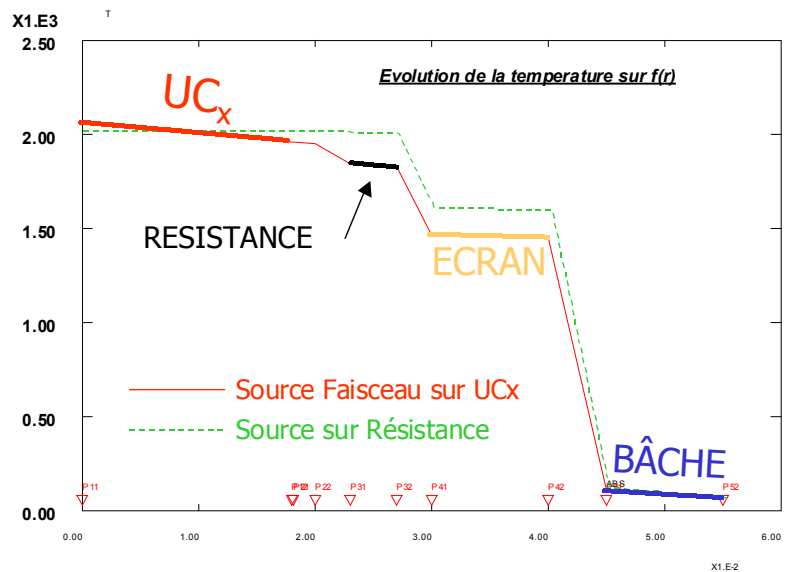


Figure 15 Temperature profile along the radial direction

3.4.3. Effusion

Once the diffusion process has brought the atom up to the surface and expelled it in the vacuum, the heavy atom has to travel to the output opening by bouncing on the different surfaces. The fly path is done with an average velocity corresponding to the Maxwellian distribution at the operating temperature. Depending on the atom, each collision with a surface will result in a sticking residence time corresponding to the bonding energy during the adsorption phase (for example, the sticking time of a rare gas element is extremely small – a few μs, whereas the sticking time of some refractory elements can be very large – seconds or more due to chemisorption). This is called the "effusion" process. The average path length and the number of wall collisions can be calculated for a given geometry by Monte-Carlo techniques.

It turns out that there is an optimum value for the ratio of disk thickness (=a) to the spacing (=d) between two disks. If the disks are too close to each other (d/a small), the atoms will bounce indefinitely between the disks,

hardly getting in the open central area. Whereas, if the disks are too far from each other (d/a large), the overall length of the target and hence the fly path will be too long. As can be seen from Figure 16, the optimum value for (d/a) is around 0.75.

A quite important feature is resulting from the effusion calculation. As stated earlier, this target geometry is very favorable for the effusion of short lived elements. Due to the large central hole, a non negligible fraction of the short lived fission products can be collected in the ion source. In fact, some atoms (a few percent) can even cross the whole target without any collision. A histogram distribution of the number of collisions is shown in Figure 17. The total effusion time can be calculated by adding the flight pass time to the total sticking time. As an example for tin, the flight path time is of the order of 10 ms, while the total average sticking time is 90 ms for a single sticking time of 0.2 ms. It is important to note that, depending on the surface composition and condition, the single sticking time may vary with several orders of magnitudes (from 10^{-8} s to 10^{-1} s for Sn). The collision probability, as can be expected, follows an exponential decrease, the highest value being at zero collision. We believe this is a very important added value for this project.

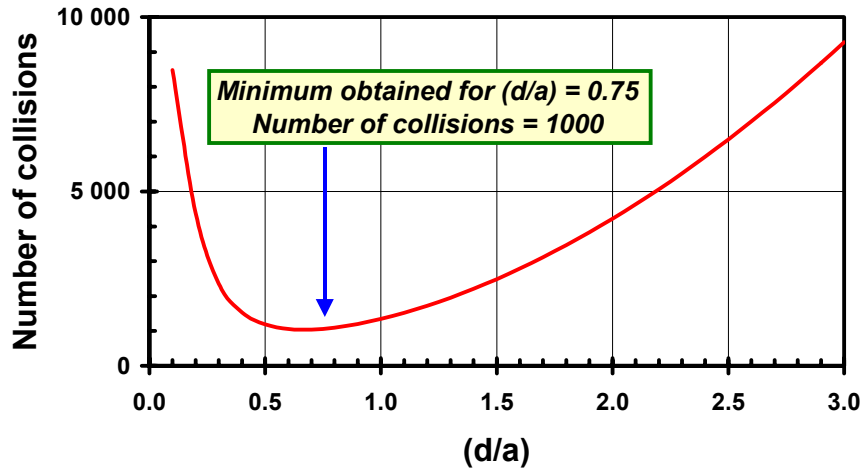


Figure 16 The number of collision variation with the ratio of disk spacing to thickness (d/a).

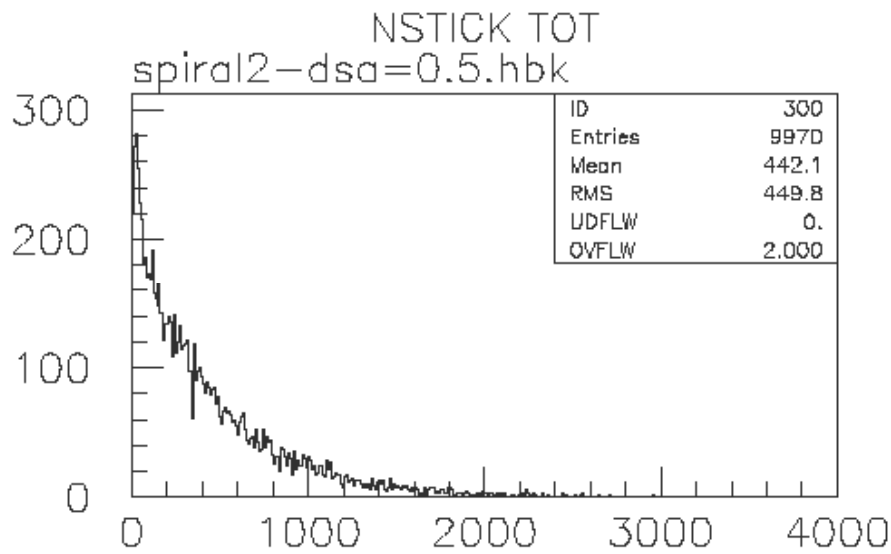


Figure 17 Histogram of number of collisions for a 10000 particle Monte-Carlo

3.5. Target-Ion-Source System (TISS)

The ionization source will be installed in a module described below, as close as possible to the target. The chemical features of the radioactive element to produce will define the type of the ionization source regarding its efficiency. The main methods considered are surface ionisation for alkali elements, an electron cyclotron resonance ion source for noble gases or for volatile mono-atomic or molecular elements, and a laser ion source for refractory elements. Correspondingly existing sources for radioactive ion production are respectively described in the references [4, 5, 6]. These sources (an exemple is given on Figure 18 with the SCRMAG ion source used at ISOLDE) can be implemented inside the plug that implies an angle of 90° between the primary beam and the axis of the separator.

However the field of production is always under developments and new sources are under studies keeping in mind that the design of the target and ion source system should, particularly, take into account the parameters having an effect on the global efficiency; i.e. the diffusion of the radioactive atoms out of the target, their effusion up to the source and the ionisation efficiency. Different experiments and developments were carried out at GANIL concerning the target-source system of SPIRAL. The experience acquired in these works and the know-how for the conceptions of such production systems are of paramount importance in achieving good design and performances.

Original works are underway in numerous laboratories like TRIUMF, GANIL or ISOLDE to maximise the efficiency of the target source system specially dedicated to gases. A new inexpensive fully permanent magnet 2,45 GHz ECRIS, called MINIMONO (see Figure 19), has been developed at GANIL and will be tested at ISOLDE. A new version of this ion source with coils (with better radiation hardness) is presently under development. Special radiation resistant coils will be tested soon in a different ECRIS at TRIUMF. The combination of the technological developments at GANIL and the know-how of TRIUMF and ISOLDE will allow increasing significantly the production efficiency of radioactive ions with high reliability.

It will be possible to install any one of the proposed sources in the production module, the ECRIS being the biggest one. In all cases, the lifetime to be considered for the production system is 3 months. The replacement of the whole production system will be performed in a hot cell, specially designed for such an operation.

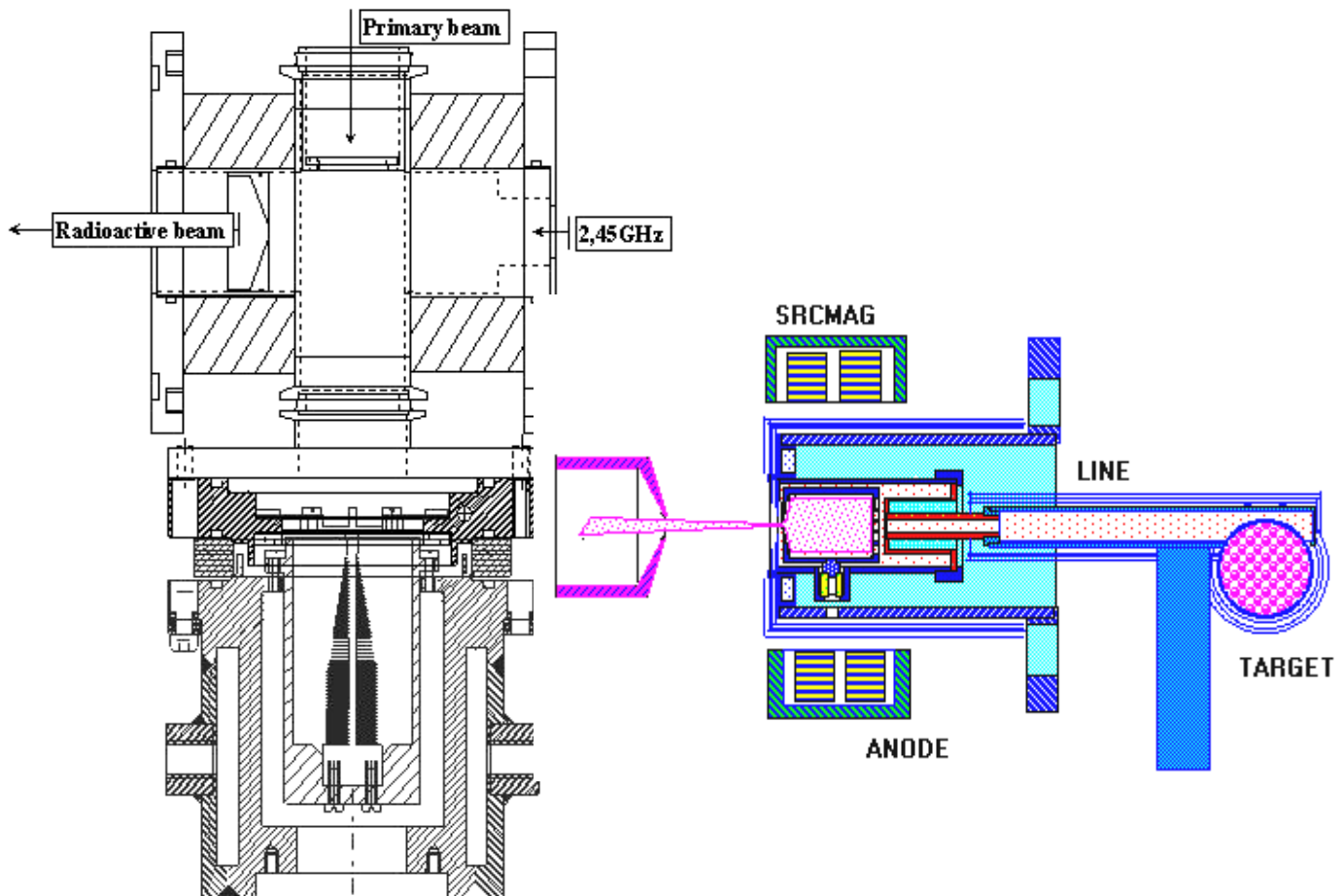


Figure 19 MINIMONO ion source connected to the present SPIRAL target

Figure 18 SCRMAG ion source used at ISOLDE

3.6. Low energy Ion Beam Lines

3.6.1. Extraction beam line and Separator

The ion source associated to the target system will produce $1+$ ions. The beam emittance depends on the kind of the ion sources which will be used. It may be from $10 \mu\text{m.mrad}$ with the surface ionisation sources for alkaline atoms to $100 \mu\text{m.mrad}$ with the ECR sources for the noble gas. New smaller ECR sources under development (MONO1000 or MINIMONO) could provide lower emittance ($30 \mu\text{m.mrad}$) The extraction optics will be calculated, if possible, for the maximal emittance expected.

The extraction optics, located in a high activation level environment, has to be simple. The number of diagnostics elements and, consequently, of optics elements, should be minimized.

A large number of elements are produced in the target-source system. According to the experiment requirement, several masses may be selected by a mass pre-separator.

The mass separator may be a magnetic dipole or a Wien filter. The advantage of the last one is that the mass used at low energy may be chosen almost independently of the mass post-accelerated. Yet, a dipole is easier, particularly to put in a high activation environment. Its curve radius could be 500 mm.

One mass will be driven to a charge breeder, for post-acceleration, while one (or two) other(s), in the range of +/-15 % (or +/-20 %) from the central mass, will be sent to low-energy experimental area(s). The lateral beam(s) may be deflected with an electrostatic deflector, which is movable parallel to the focal plane of the pre-separator to select the ion mass, and to drive it back to the right trajectory. This scheme is inspired by GPS at ISOLDE whom Figure 20 below shows the electrostatic part. [7]

Note that this mass separator is not a precision spectrometer. The resolution will be about 1/100. The separation will be finalized in CIME, or with a high precision spectrometer for the low energy experiments.

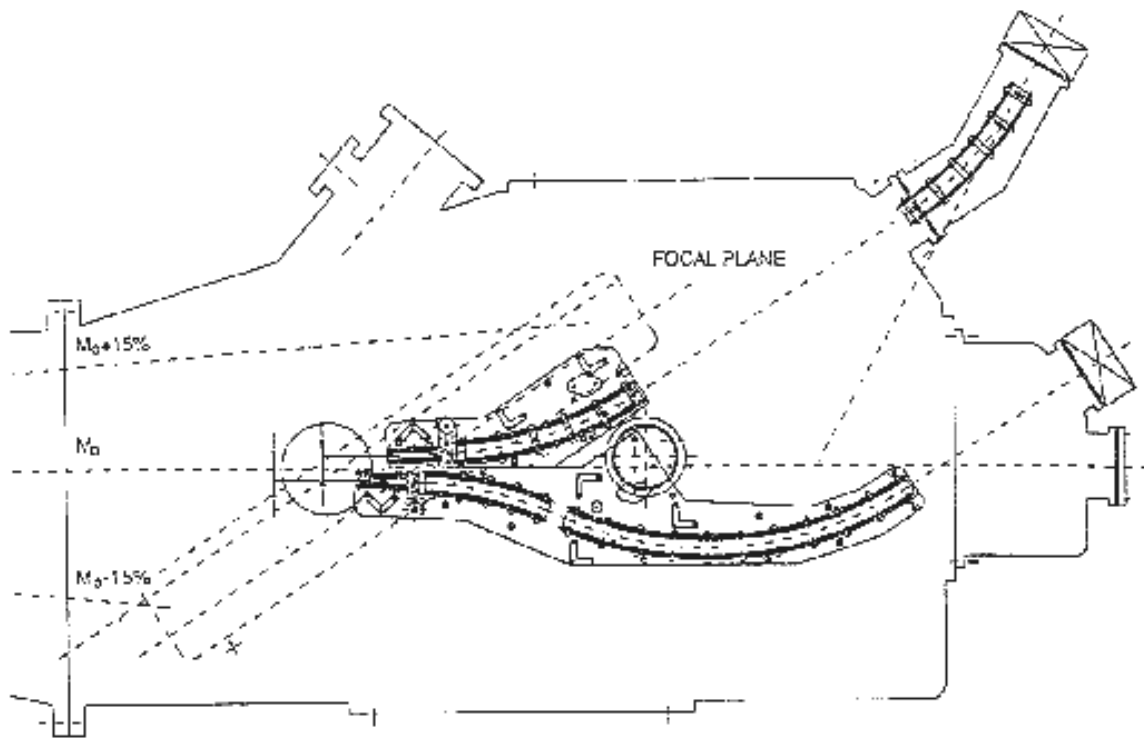


Figure 20 ISOLDE Separator Principle : movable electrostatic deflectors behind the dipole

The optics elements before the dipole have to be electrostatic, to drive all masses up to the pre-separator. A quadrupole triplet is one solution.

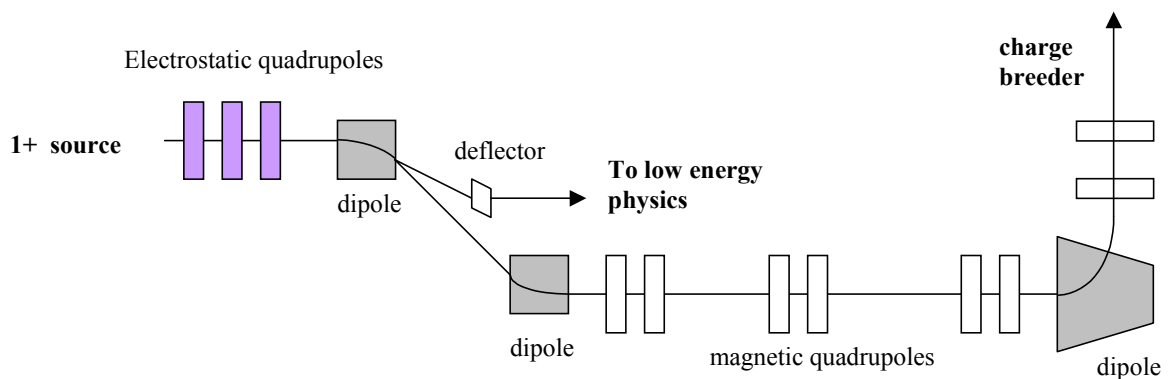


Figure 21 Schematic Ion Beam Line between the 1+source and the Charge Breeder

3.6.2. From pre-separator to low energy experiment area

A simple beam line will conduct the low energy beam to experimental areas. The equipment used at LIRAT (in construction) might be used both by SPIRAL I and SPIRAL II

In addition, it may be useful to build a spectrometer dedicated to low-energy physics. A 1/2000 mass resolution may be reached with a dispersion of 4 meters and a beam width at object point of +/- 0.5 mm, with an emittance of 10 to 30 π .mm.mrad.

3.6.3. From pre-separator to charge breeder

The 1+ beam has to be matched before entering the n+ source, to ensure a good efficiency. A second dipole (the first one is the separator) may be used to obtain a doubly achromatic beam, so that the tuning does not depend on the presence of impurities. The beam line is described on Figure 21.

3.6.4. N+ beam line from charge breeder to CIME

The N+ beam line is described on Figure 22 below. It is thought, apart some details, as a symmetry of the SPIRAL I injection beam line (from source to matching point). The identification bench will be 45 degrees rotated to serve both for SPIRAL and SPIRALII. The 45 degrees dipole D52 has to be changed into a double-entrance dipole.

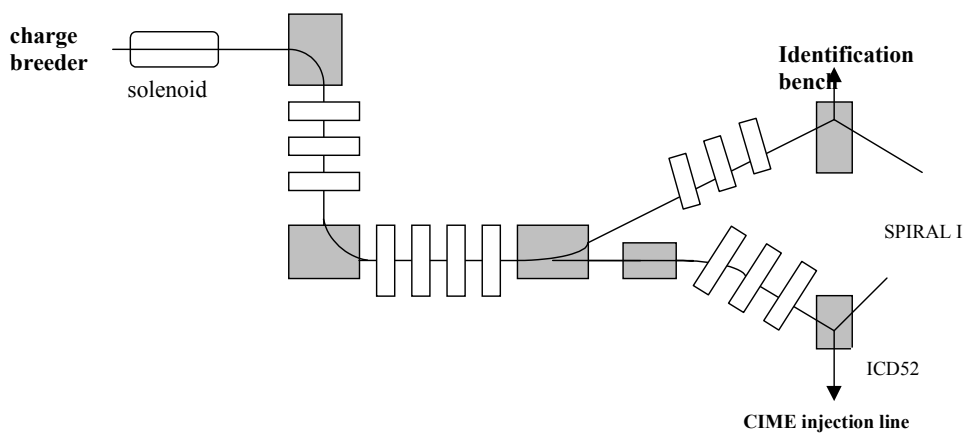


Figure 22 Schematic Ion Beam Line between the Charge Breeder and CIME

3.7. Charge Breeder

The goal of the 1+/n+ transformation consists in increasing the charge state of the singly charged incoming ion to a charge state compatible with the acceleration by the CIME cyclotron or by the C0. For the heaviest elements like ¹⁴⁴Xe, that means a 36+ charge state to reach Q/A= 0.25 that corresponds to an energy of around 15 MeV/A after acceleration.

It's obvious that the efficiency of the 1+ to the n+ ion production and the charge breeding time are fundamental parameters in this method for radioactive ions.

An ECR booster has been developed by the SSI group at ISN Grenoble (France) based on the use of a Phoenix ion source at 14 GHz. The present results with this source are summarized in

Table 4 below :

	Charge Breeding Efficiency on the most abundant charge state	Overall Efficiency
Noble gas	10%	50 to 70%
Condensable elements	6%	45%

Table 4 Order of magnitude of charge breeding characteristics with stable elements.

The most abundant charge state can be shifted to higher values by using higher UHF frequency.

In that way, an upgrade of the source is going on by increasing the radial magnetic field until 1.6 T and the plasma volume. The UHF frequency will be 18 GHz.

Other solutions like the use of superconducting ion sources (SERSE or GYROSERSE) for example could be studied in the future.

3.8. Identification Stations

Two identification stations are proposed : one between the 1+ source and the charge breeder and the other one at the output of CIME, after the charge breeder.

They allow to :

- control the production of the target via the 1+ source and the separator
- control the good behaviour of the charge breeder
- control the identity of the ions injected into CIME.

The present identification station used for SPIRAL can be used also for SPIRAL II

3.9. Acceleration

GANIL presents several possibilities of post-acceleration :

a - CIME can deliver a beam energy from 7 to 10 MeV/n with charge provided by a charge breeder designed with the top-end ECR source technology. (Figure 23 below).

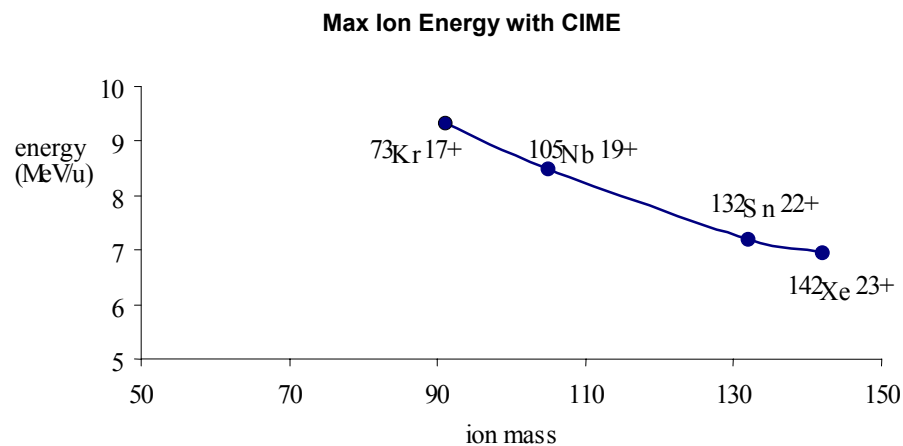


Figure 23 Maximum Energy at the output of CIME

b - CSS2 coupled to CIME can accelerate the same ions between 11 and 21 MeV/n, with a stripping between them. The maximum energy could reach 39 MeV.A, but with a degrade of the possibilities of C0-CSS1-CSS2 (modification of injection radius of CSS1 and extraction radius of CSS2). This solution is not recommended.

c - the ions going out the 1+ source can be accelerated by **C02, CSS1 and CSS2** and the energy at output of SSC2 would range from 35 to 50 MeV.A.

This beam line could be constructed underground, partly inside the power supplies building. A long straight line (80 meters) could be constructed as in the PIAFE project. Then the line would have to turn left, up to a charge breeder. Afterwards, a beam line would drive the beam up and inject it into the C02. The two beam lines before and after the charge breeder are similar to IC line of SPIRAL and the total length is about 40 m.

These last option has been precisely studied in the frame of the LINAG-1 project [8]

d - a specific booster can be designed to accelerate the ions after CIME or instead CIME. These options are out of the frame of this project but the implantation of the facility will try to keep free the room needed for such a booster.

4. Radioactivity Issues

4.1. Generalities

4.1.1. Main Rules

The main rules to respect concerning the radioactivity issues are :

- the ALARA (As Low As Reasonably Achievable) approach which advises (imposes?) to reduce as low as possible (technically and economically) the radiation dose received by people.

- the thresholds of radiation or contamination :

	not regulated zones	"zones surveillées"	"zones contrôlées"
radiation dose	< 2.5 $\mu\text{Sv/h}$	< 7.5 $\mu\text{Sv/h}$	> 7,5 $\mu\text{Sv/h}$
α emitters contamination	<8 mBq/m^3	< 25 mBq/m^3	> 25 mBq/m^3
$\beta\gamma$ emitters contamination	< 3.5 Bq/m^3	< 10 Bq/m^3	> 10 Bq/m^3

The not regulated zones are all the zones outside the building

The "zone surveillées" are the technical galleries where category B people can work permanently

The "zones contrôlées" are the caves being able to receive the beam or having a high level of radiation and whose access is regulated

- the release of nuclear waste to atmosphere (gas) or to used water network (liquid) must respect the authorizations of release

4.1.2. Types of radioactivity

The types of radioactivity which must be dealt with are:

- the radiation induced by the beam impact onto the matter :

***gamma photons induced by electrons** (Bremsstrahlung) : their energy spectrum and their intensity depends on the angle emission and on the type of materials. This type of radioactivity occurs along the electron beam line where the beam can be lost or fully stopped (the beam dump and the target). The maximum flux is obtained when the full beam is stopped. It can reach $3 \cdot 10^{16}$ MeV/s if the electron beam is stopped in heavy metal (copper or iron).

***neutrons induced by photofission** ((γ, f) reactions) : These neutrons are created in the target where uranium photofission occurs. The production yield is around 3.4 n/fission. The total flux is therefore about $3 \cdot 10^{13}$ n/s. The flux is roughly isotropic and the energy spectrum can reach 20 MeV for an average energy of 4 MeV. The energetic flux is therefore around 10^{14} MeV/s.

***neutrons induced directly by gamma photons** ((γ, n) and $(\gamma, 2n)$ reactions). These neutrons are created everywhere gamma photons go through matter, in particular in the beam dump and in the concrete around the beam dump. They exist also in the target and induce complementary fissions. Such a flux inside the target is roughly equivalent to the fission induced neutron flux.

***neutrons induced by energetic ions** : When their energy is higher than the Coulomb barrier, the ions can create nuclear reactions which induce a flux of neutrons. That can occur only inside CIME and along the high energy beam lines. The consequent radiation is already taken into account in SPIRAL facility.

These radiations stop as soon as the beam stops.

X-Rays radiation from linac cavities due to electron emission. This radiation stops when the cavities are turned off.

- the activation of the matter , consequences of the nuclear reactions :

***fission of uranium by gamma photons** inside the target creates two fragments per fission. Most of them are radioactive (it is the goal of the project) and their desintegration emits both β radiation which induce gamma photons by Bremsstrahlung and gamma photons by desexcitation. The global activity is shown in Figure 24 below. It reaches 1500 Ci after 15 days of irradiation. Taking an average decay energy of 2 MeV, the global gamma radiation energy is 10^{14} MeV/s. Although, by the principle of the target, a part of these radionuclides go out of the target but, for radioprotection issue, all the radionuclides are considered staying inside the target.

***fission of uranium by neutrons** (neutrons from (γ,n) or $(\gamma,2n)$ reactions and from photofission). The global production of fission products by this way reaches 80 Ci after 15 days of irradiation (5 % of the photofission products) which must be added to the photofission products.

***transuranic elements produced by neutron capture.** From codes CINDER and DARWIN, the activity of alpha emitters is around 2 mCi after 15 days of irradiation and is roughly constant after several years of cooling. 99 % of this activity is due to Uranium (238 +235) used in the target. The main artificial element is Pu239 which is responsible of 99.9 % of the artificial activity. Among the artificial elements, a very small activity is provided by Radon. It seems (to be checked precisely) this activity is lower than 1 Bq just after the irradiation and reaches almost 50 Bq after several years of transuranic element decay. If these results are confirmed, the problem of the radon release has not to be taken into account.

***nuclear reactions induced by neutrons** : the neutrons created by photofission or directly by the gamma photons induced nuclear reactions in the matter. In particular, all the matters (copper, tungsten, concrete, cooling water) put down around the radiation sources (beam dump, target and others) will be made radioactive. The air inside the caves can also be activated. This matter activation will have to be taken into account and the materials will have to be chosen to minimize it.

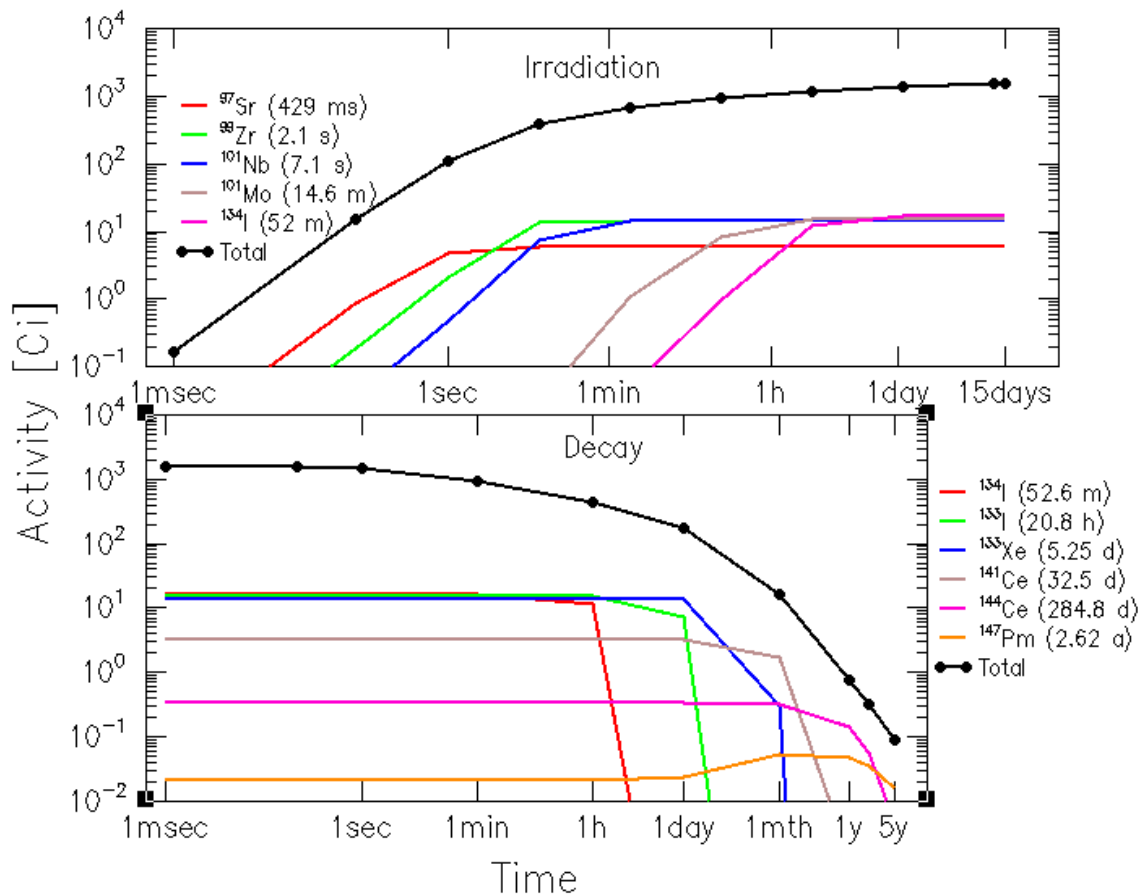


Figure 24 Activity of the photofission induced products

The radiations induced by matter activation are permanent and decrease according to the life time of the radionuclides initially created and of the radionuclides coming from their desintegration. In particular, the activity of the target decreases according to the law shows on Figure 24 above.

- the contamination by radioactive materials (dust, gas, aerosol) which are carried and deposited. This contamination is mainly coming from the fission products which go out the target.

The Figure 25 below describes the main routes followed by the fission products (parents only) according to their physical state. One of the problem to take into account is the fact the radioactive nuclei can break up into another nuclei whose the physical state is different. For instance, a solid can be desintegrated into a gas (Sb gives Te which gives Iodine which gives Xenon).

The intensities mentioned on Figure 25 are the highest ones which can be got. In particular, the intensity at the output of the separator (10^{11} ions/s) is for a gaseous element (Kr or Xe) selected by the separator, element whose transmission efficiency is assumed 100 % between the target and the source output.

4.1.3. Types of protection :

- Protection of workers against radiation

The goal of the protection is to keep the radiation dose received by the workers as low as possible and, in any case, lower than the threshold acceptable for the classification of the place.

As it is difficult to reduce the source level (it is sometimes possible by reducing the beam intensity for instance), the only means are to put down shielding between the source and the workers.

Normal concrete (d=2.4) or heavy concrete (d=3.2) will be the basic shielding.

Sometimes, an association of different materials can be interesting (metal plus concrete).

Figure 26 below gives two examples of transmission : Bremmstrahlung gammas (20 MeV in average) and fission neutrons (4 MeV : high part of the spectrum).

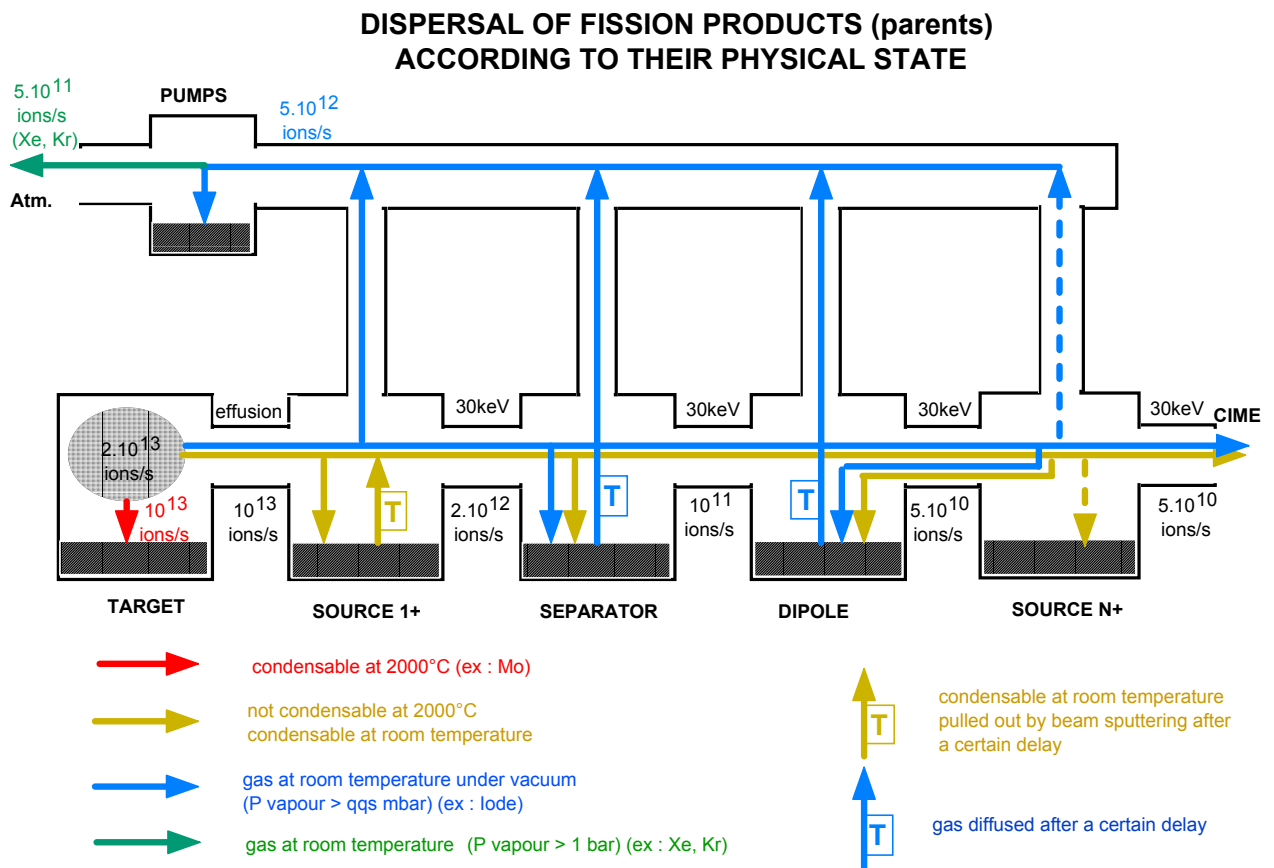


Figure 25 Dispersal of the fission products

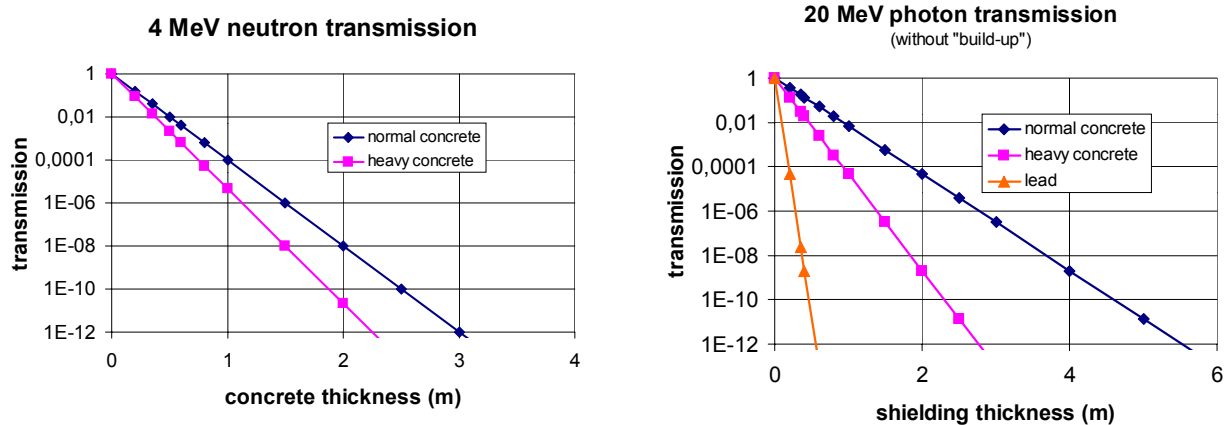


Figure 26 Transmission of gammas and neutrons in shielding

- Protection of workers against contamination

The goal is to avoid that workers swallow or breathe radioactive matter. The best solution is to reduce as much as possible contamination inside the rooms, therefore to keep the fission products and their descendants in containers (vacuum chambers, gas bottles) without leakage outside, except by the way of the authorized means of release. One of the problems is these ions can change their states (a solid can give a gas like iodine ions which decay into xenon ions)

Protection of environment

The release of nuclear waste will have to respect the authorizations in any cases. In order to keep a safety margin sufficient to include the consequences of accidents, the release in normal conditions of working will have to stay at least two orders below the authorization level.

The next paragraphs deal with the radioactivity issues for each major part of the facility : linear accelerator, electron beam line and its beam dump, target ion source system (TISS), source extraction beam line, separator, low energy radioactive beam line and its main components (identification bench, charge breeder, dipoles), CIME

4.2. Linear Accelerator (Linac)

4.2.1. Radiation from beam

In a superconducting electron linac, a beam loss never occurs inside the RF cavities. However, it seems impossible to demonstrate this fact because the codes used to simulate the electron dynamics consider that the components are without defects. Also, the maximal beam loss taken into account for the radioprotection is the one which can be detected. The accuracy of the instrumentation allows to measure a beam loss of 1 % with reliability. This electron beam loss induces an energy flux of 10^{15} MeV/s. The Bremsstrahlung yield in copper or iron (about 0.4) induces a gamma flux of 3.10^{14} MeV/s with a mean energy of 20 MeV. The radiation, at 1 m, is $2.4.10^9$ MeV/cm²/s if we assume the radiation is isotropic. The dose equivalent at 1 m is therefore $2.4.10^7$ μSv/h (the conversion coefficient is 0.01 μSv/h/MeV/cm²/s for 20 MeV gamma). To reach 7.5 μSv/h behind the shielding (at 3 m), its thickness, around the linac, must be **about 2.5 m if it makes of normal concrete or 1.5 m of heavy concrete.**

4.2.2. Activation and contamination

As the beam losses will be very small in practice and as the activation induced by 45 MeV electrons is very low (only secondary neutrons can activate a little), the activation and, therefore, the contamination of the linac should be negligible.

4.2.3. X-Rays radiation from cavities

The X-Rays appear when internal electron emissions occur inside the RF cavities. These electrons, accelerated by the RF field, induce photons exactly as the electron beam itself. The cavity RF field chosen to reach 45 MeV should not induce X-Rays. However, X-Rays detectors check permanently the X-Rays level and the RF field will be adjusted to keep compatible with the shielding.

4.3. Beam Dump

4.3.1. Materials

The full intensity beam can hit the beam dump. The electrons can transfer their energy by ionisation, excitation and Bremsstrahlung. To reduce the gamma radiation created by Bremsstrahlung, the material which stops the beam must be light. The best material is the carbon because there is no production of long life time radioactive ions and a very low neutron production.

To stop the gammas which can go out the carbon block, a shielding in heavy material can be added around the dump. Iron is good candidate because its activation by neutrons is low (only short life-time nuclei are created)

The beam dump used at ELBE facility [3] is a good example (Figure 27)

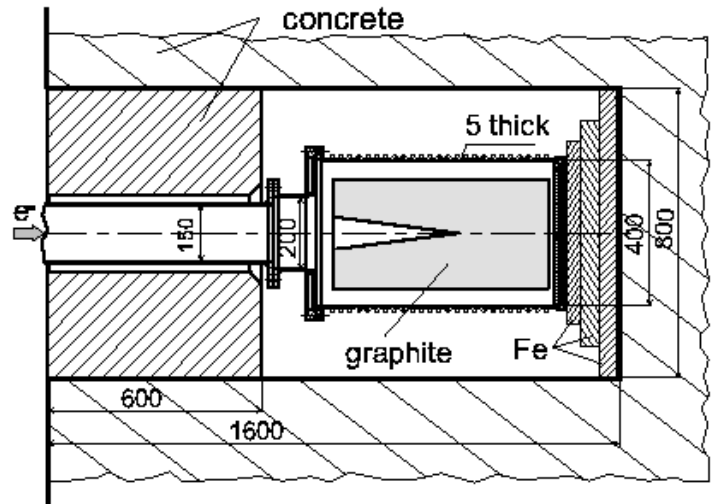


Figure 27 Beam Bump designed for the project ELBE

4.3.2. Radiation from beam

The Bremsstrahlung yield in carbon is 0.1. The gamma flux is therefore 10^{16} MeV/s. A similar calculation as for the linac shows the dose equivalent reaches 10^9 μ Sv/h at 1 m (if isotropic). The iron shielding reduces the radiation by a factor 10^3 roughly. **2 m of concrete** (1 m of heavy concrete) could be sufficient to reduce the dose equivalent down to 7.5 μ Sv/h. Similar calculation will be to carry out around the beam dump, taking into account the energy of the gammas are lower.

4.3.3. Activation

The activation of the materials of the beam dump (carbon, iron, copper) and of the shielding (concrete) by the neutrons is to be calculated.

4.3.4. Contamination

The contamination will be confine inside the beam dump chamber.

4.3.5. Incident Cases

The major incident could be the loss of cooling without stopping the beam.

The container where the beam dump is installed will design to catch the melted matters.

4.4. Electron Beam Lines

4.4.1. Radiation from beam

The beam loss should be negligible. In case of failure of guidance elements, the beam loss will be detected either directly (measurement of the beam transmission) or by the means of the induced radiation and the beam stops.

4.4.2. Activation and contamination

The activation and, therefore, the contamination of the beam line components (vacuum chamber) should be negligible.

4.4.3. Incident Cases

The major incident could be the boring of the vacuum chamber by the beam. The pressure elevation in the chamber triggers security actions.

4.5. Target Ion Source System

4.5.1. Radiation during irradiation

As shown on Figure 28 below, the radiation going out the target (included the source) consists of :

- **electrons** (10^{15} MeV/s) from the electron beam
- **gammas** (10^{16} MeV/s) from :
 Bremsstrahlung of electron beam
 decay of fission products
 Bremsstrahlung of β^- radiation

This radiation induces a flux of 10^{11} MeV/cm²/s at 1 m (if isotropic) and a dose equivalent of 10^9 μ Sv/h.

- **neutrons** (10^{14} MeV/s) from : (γ,n) and ($\gamma,2n$) reactions
 fission reactions

This radiation induces a flux of $5 \cdot 10^8$ n/cm²/s at 1 m (mean neutron energy of 2 MeV) and a dose equivalent of $3 \cdot 10^7$ μ Sv/h.

With the target design as presented in § 3.4, the spectra of these radiation are shown Figure 29, Figure 30 and Figure 31.

The shielding is designed by taking into account the most energetic radiation, therefore the gamma radiation. 3.5 m of normal concrete or 2 m of heavy concrete is sufficient around the target to allow the permanent presence of workers behind the shielding during the irradiation. A further shielding made of heavy metal (lead, tungsten or, better for activation issues, iron) around the target can reduce drastically the concrete thickness needed.

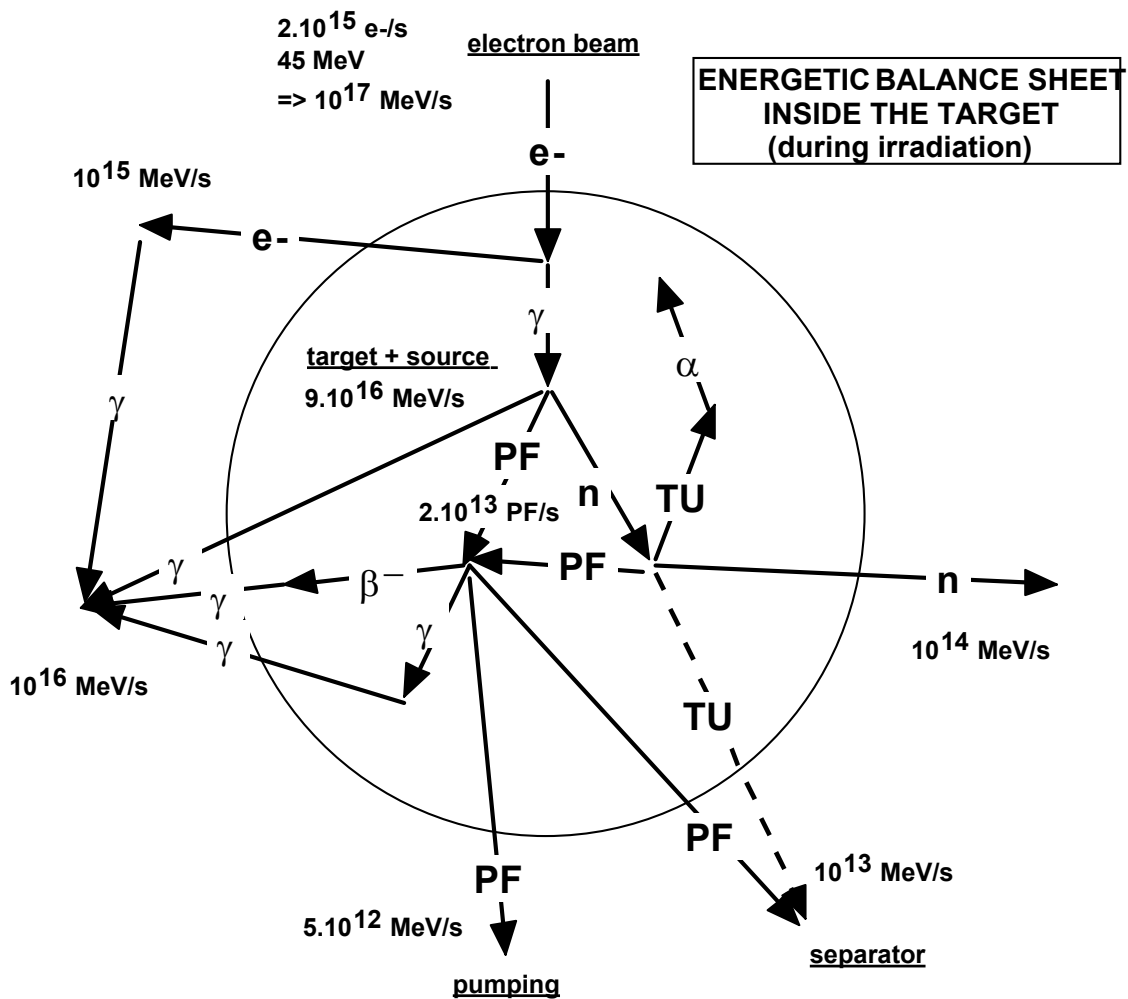


Figure 28 Energetic Balance Sheet in the Target

Neutron Spectra out of Target

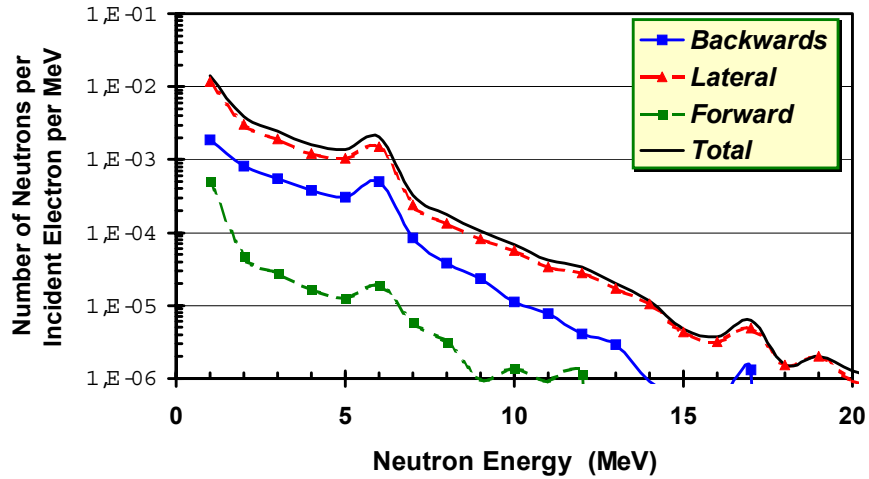


Figure 29 Neutron Spectra out of the target

Electron Spectra out of Target

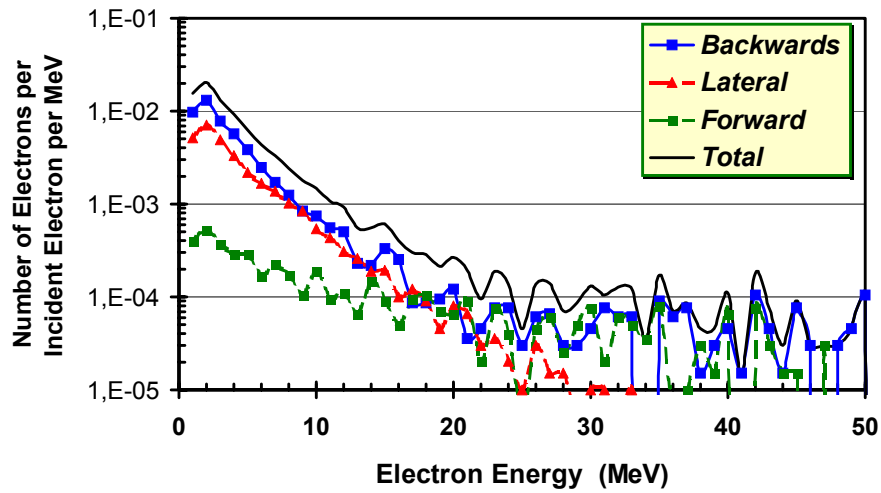


Figure 30 Electron Spectra out of the target

Photon Spectra out of Target

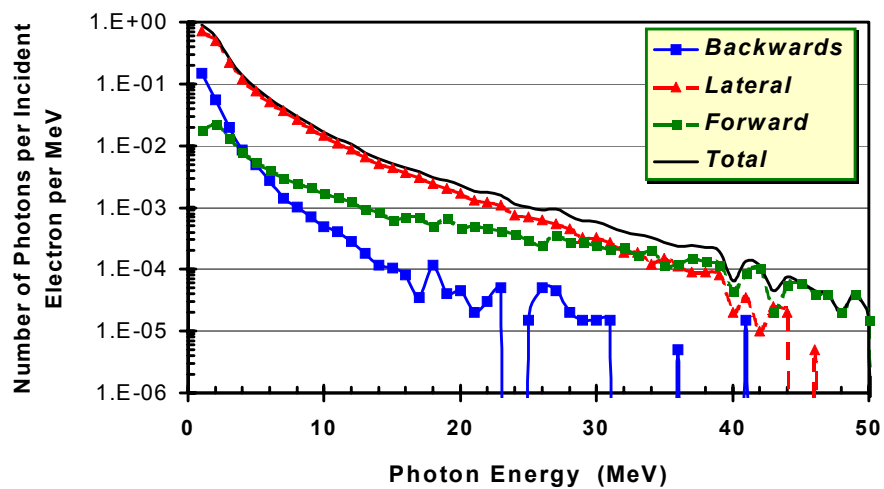


Figure 31 Photon Spectra out of the target

4.5.2. Activation of the target

After the irradiation stops, the only cause of radiation is the decay of the fission products. To simplify, we assume that all the fission products stay inside the target.

The graphs Figure 24 show the activity versus time during irradiation and the decay of the activity after the end of irradiation. After 15 days of irradiation, the activity is roughly 1500 Ci, that corresponds to 10^{14} MeV/s of beta radiation if we assume that the mean decay energy is 2 MeV. The gamma radiation is 10^{13} MeV/s if we assume that mean Bremsstrahlung coefficient is 0.1. At 1 m, the radiation flux is therefore 10^8 MeV/cm²/s (if isotropic) and the dose equivalent $2 \cdot 10^6$ μ Sv/h. The shielding adapted to the irradiation period (10^9 μ Sv/h) is sufficient to protect workers against this level of radiation.

If the target is stored after waiting for one day of cooling, the activation is only 150 Ci with a dose equivalent of $2 \cdot 10^5$ μ Sv/h and the shielding needed is roughly 1 m of concrete or less according to the internal shielding of the target (see § 4.5.1 above)

4.5.3. Principle of the plug

The dose rate due to gamma radiation just after the stop of the primary beam is estimated to attain 2 Sv/h at 1 m from the target after 15 days of irradiation (see § 4.5.2 above). One day after, the radiation rate is still 200 mSv/h. This high level of radiation does not permit manual intervention on the target itself. Thus the different operation must be studied with this constraint in mind.

The target and the ion source will be placed in a rectangular module (called plug) that is surrounded by 2 m of concrete for shielding of workers and equipment. The same principle has been applied on the ISAC facility at TRIUMF (Vancouver, Canada), for the production of radioactive beams with a 500 MeV, 100 μ A primary beam. At this time, two solutions are under studies : the first one consists in sending the primary beam vertically while the second one prefers to send it horizontally. These two solutions will be studied in details during the next months and a final approach will be taken considering the advantages and the disadvantages of each one.

Two turbo molecular pumps and the insulators are thereby located on the top of the plug where they are protected from radiations. This increases the life time of the different components and permits the manual disconnection of the electrical powers.

The 2 m thickness of concrete reduces the dose rate on the top of the plug down to 7.5 μ Sv/h when the beam is stopped that allows people to come and work on the equipments located at this place.

The target ion source system is immersed in the vacuum created by the two turbo molecular pumps located on the plug. The plug can be closed at the entrance and at the exit by two plates moved with air piston. The plug itself is contained in a large vacuum tank with concrete packed tightly around to minimize air activation. This tank contains three modules. Module 1 contains the target ion source system and the radioactive nuclear beam extraction electrodes. Module 2 contains electrode, profile monitors, slits and beam profile to monitor, transport and adjust beam characteristics of the RNB from the ion source to the mass separator. Module 3 contains the magnetic dipole, the energy slits and the electrostatic deflectors (see § 4.6 below) The vacuum connections between the modules do not need seals as the plug is immersed in vacuum.

After irradiation, the different connections of the plug (electrical connections, primary pumping, water connections,...) can be manually removed. The plug is then remotely removed from the production cave and is evacuated to a storage cell. Depending on the state of the target ion source system, the plug can be re-used or moved to a hot cell where the elements at the bottom of the module can be replaced with master/slave manipulators.

A dedicated handling system will be studied for the manipulation of the plugs taking into account the different risks induced by this action. In particular, the risk of fall involving a risk of dispersion of contamination will be carefully studied.

However, the handling system will permit to remove the plug and to put it again into the tank to be re-used or to bring it up to the shielded cell to be dismantled.

4.5.4. Activation of the materials around the target

As already said, the **air activation** is reduced to its minimum as the plug and the TISS are immersed in vacuum. Nevertheless, the small volume of air surrounding the target tanks will be considered as the same level as the hot cell inner volume and the building is zoned to ensure that the air movement is directed to these volumes. The air of each room surrounding the hot cell and target tanks is sampled and monitored.

The problem of the **water activation** has been studied in ISAC facility and the same system will be installed. It consists in a closed loop passing through a heat exchanger. The water of the primary circuit is drained to a buffer volume where it can be monitored prior to release to the outside drains.

All the materials around the target (concrete in particular) will be irradiated and activated by neutrons. However, this activation will be more a problem of nuclear waste than a problem of radioprotection. The calculation of this activation will have to be carried out in the frame of the nuclear waste management.

4.5.5. Gas Contamination

All pumps exhaust into a series of tanks where the activity can be sampled and evaluated. This activity is mainly due to the rare gas nuclei (⁸⁵Kr with a half time of 11 years or ¹³³Xe for example).

Figure 33 shows the decrease of the activity of noble gases produced in the target after 15 days of irradiation. The storage time depends on the release authorizations given by the safety authorities (see § 6). However a storage time of three month is assumed to be sufficient all the more so as the activity is roughly constant afterwards because of the life-time of the Kr⁸⁵.

The main flow of gas comes from the gas injected into the ion source. The present ion sources need a flow that do not exceed 10⁻³ mbar.l.s⁻¹. For all the calculations a factor 10 has been applied on this flow and the number of 10-2 mbar l s-1 has been retained.

The flow of gas represents a volume of 80 liters after 3 months of production.

The storage system is presented on Figure 32. The tanks 1 and 2 have a volume of 200 liters. Before the first run, the tanks 1 and 2 are pumped to a pressure of 100 mbar.

After this prepumping, the valves VST1 and VST2, VET1 and VET2 are closed. The volume of the tube between the primary pumps and VET1 and 2 is considered as a buffer. When the gauge G0 detects a pressure greater than 800 mbar, the valve VET1 is triggered and the buffer volume is pumped by the tank. The VET1 is then closed when the pressure measured by the gauge G0 is equal to the pressure measured in the tank with the GT1 gauge.

After three month of irradiation, the valves of the tank1 are closed and the storage can continue with the tank2 allowing the decrease of the activity in the tank1.

After three months of irradiation the tank 1 is pumped after analysis of the residual radioactivity and the gas is exhausted through the high efficiency filters of the nuclear ventilation.

The risk of leak in a chamber induces a rapid raise of the pressure read on the G0 gauge that can be detected by measuring the slope of the increase of pressure in fonction of time. If this slope is too high the primary beam and the vacuum are stopped

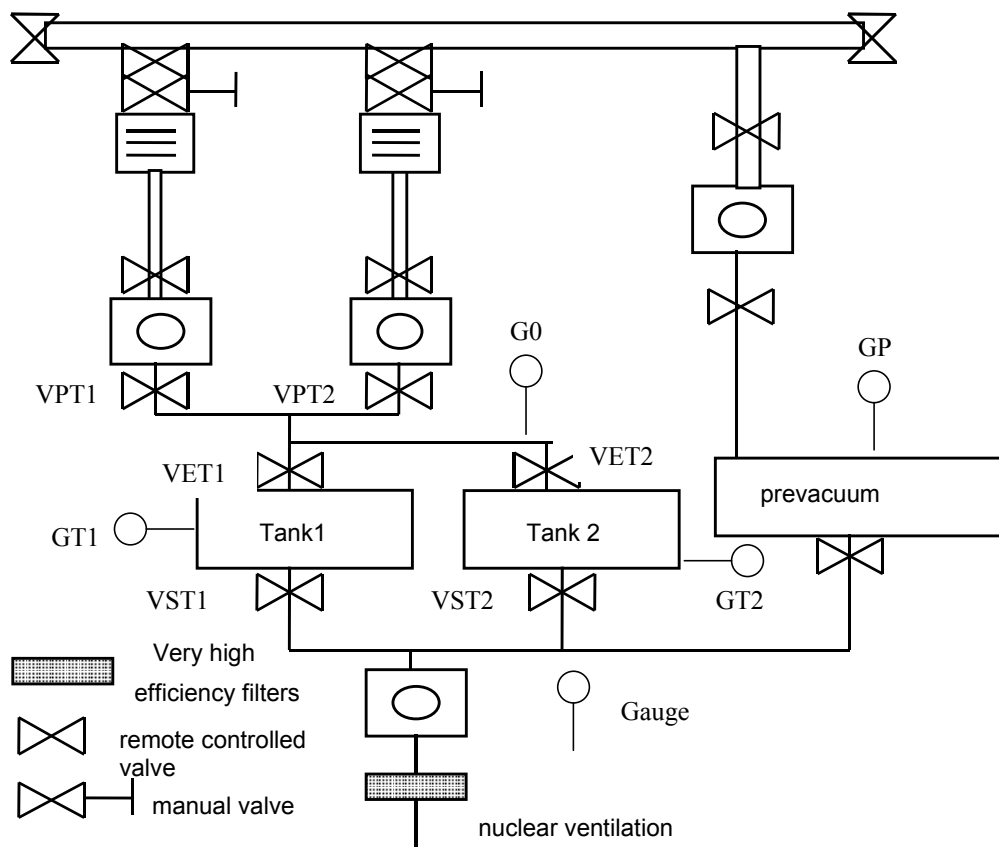


Figure 32 Gas Storage System Principle

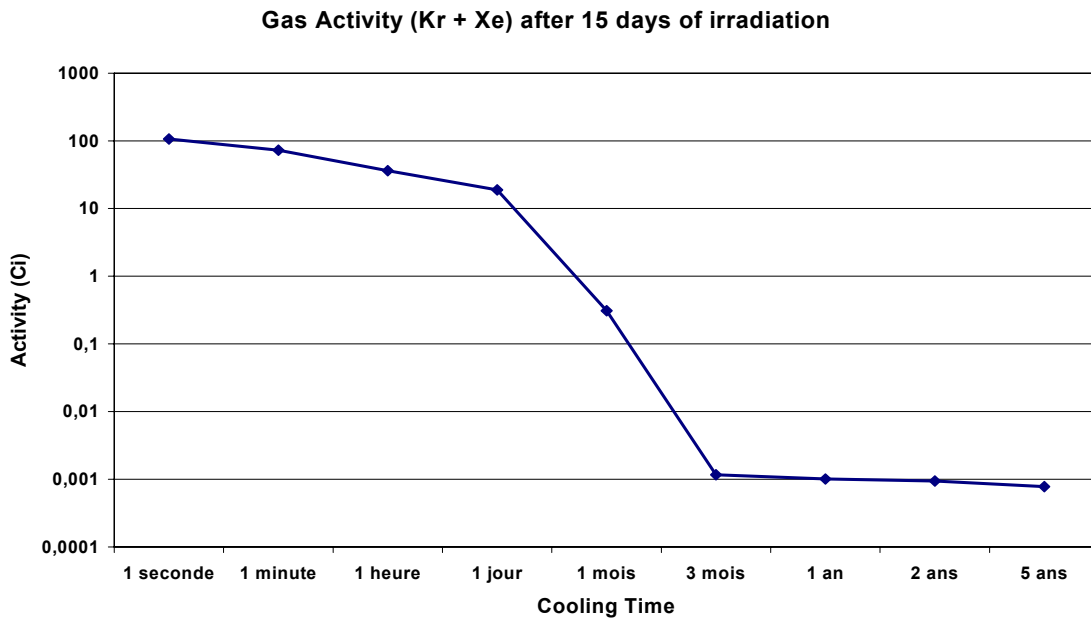


Figure 33 Gas Activity after 15 days of irradiation

4.5.6. Incident Cases

Internal Causes

Numerous malfunctionnings can induce consequences on the safety.

It is not realistic to determine an exhaustive list of this possible incidents. Among them, we can think about :

- the target melting due, for example, to a bad control of the heating power
- a deviation of the electron beam from the good trajectory in spite of a permanent control of its position
- a vacuum leakage which breaks the confinement or fills up the gas bottle very quickly
- a cooling water leakage which contaminates the ground floor
- a bad TISS plug handling

All these incidents will have to be studied and solutions to avoid serious consequences on the safety will have to be set.

External Causes

As for the incidents due to component malfunctionning, the external causes of damage as fire, flood or loss of electrical power will have to be taken into account in the facility design to limit their consequences on the safety.

4.6. Separator

A large part of the fission products which go out the target are ionized and go to the separator with an energy of 30 kV. Except the ions which are selected to be accelerated or used in LIRAT (less than 1 %), these ions are implanted in the slits which are used to select the ions. If we assume that 10 % of the total fission products created in the target are implanted in the slits (data to be checked), the activity of these slits can reach 150 Ci after 15 days of production and 200 Ci after 6 months.

A simple calculation gives a gamma radiation rate of 100 mSv/h at 1 m if we consider that the β - radiation is stopped by the slits and transform into gamma photons by Bremsstrahlung (mean energy : 2 MeV and Bremsstrahlung coefficient of 0.05 in iron)).

The decay of the activity (Figure 24 at § 4.1.2) induces the following radiation rate versus the time (Table 5):

	after 15 days of production	after 6 months of production
just after production stop	100 mSv/h	150 mSv/h
after one day	10 mSv/h	15 mSv/h
after one month	1 mSv/h	2 mSv/h
after one year	50 μ Sv/h	500 μ Sv/h

Table 5 dose equivalent induced by the target activity

15 cm of lead or 80 cm of concrete is enough to protect workers against this gamma radiation, even just after the production stops.

The gaseous radioactive atoms implanted in the slits will be pumping by the vacuum system and managed as the radioactive gas pumping from the TISS (see § 4.5.5)

Two options could be envisaged for the separator maintenance.

- a robot to disconnect the active part of the separator before intervention. The major problem, with this solution, is the risk of radionuclei spread and, consequently, the risk of a general contamination.
- a plug which contains the separator under a container, plug which is compatible with the TISS plug and which can be changed by a new one in case of failure. The former one, failed, will be fixed after a time of cooling in one of the storage cells. Three separator plugs are needed : one in use, one in cooling and one ready to be installed.

The plug option seems the most efficient because it minimizes the risk of contamination. and, maybe, less expensive than a sophisticated robot.

4.7. Low Energy Ion Beam Lines and Charge Breeder

After the pre-separator, if its resolution was high enough, only one type of ions would be transferred up to CIME.

In practice, several other types of ions can go out the pre-separator with characteristics lightly different. These ions will be lost all along the beam lines, inside and after the charge breeder and up to the CIME injection line.

That means that 10^{10} or more ions/s could be lost at certain points of the lines. In particular, half of the beam comes back from the charge breeder and will be lost in the first dipole before the charge breeder.

If we assume than $3 \cdot 10^{10}$ ions can be lost per second, the total activity could reach 1 Ci (at saturation) and the radiation 1 mSv/h at 1 m if all the beam is lost at the same place (this level of radiation depends on the nuclei taken into account and the materials where the decay β^- are stopped). That means that the access to caves where the beam lines are installed will be forbidden during running and after a certain time of cooling. This time of cooling depend of the types of nuclei. To reduce this time, the points where the activity is the highest could be shielded.

The maintenance of the components, in particular of the charge breeder, must be dealt with.

Moreover, all the gaseous ions, produced directly or produced by decay, will be pumped. The pumping gas must be stored and managed as for the separator and the TISS (see § 4.5.5).

4.8. CIME and High Energy Ion Beam Lines

The radioactive beam can be lost anywhere from CIME to the target of the experiments.

Permanently, the beam can be lost inside CIME during the tuning, along the CIME extraction channels, on the beam stoppers, after the stripping foils to sort the nuclei (in case of pollution by other ions) and, above all, inside the experiment targets.

These ions will be deeply implanted, inducing activity thanks to their decay. If we take the most intense of these beams, the intensity can reach 10^{10} ions/s (Xe^{139} for instance), therefore induce an activity of 0.3 Ci (in case of saturation). The radiation provided by this activity could be reach 1 mSv/h at 1 m (it depends on the nuclei taken into account and the materials where the decay β^- are stopped).

Some of them are gaseous or become gaseous by decay and will be partly pumping. All along the beam lines and the experiment chambers, the pumping gas must be stored and managed as the pumping gas from the low energy lines (see § 4.7)

4.9. Nuclear Waste Management

4.9.1. Gas

The radiological impact of the INB 113 (SPIRAL II included) on its nearby environment must be acceptable and kept as low as reasonably achievable (ALARA concept) while the EURATOM recommendations (n° 96/29) are respected

The management of the gaseous radioactive effluents created inside the SPIRAL II facility must follow a strict and precise regulations. In particular :

- analysis of the stored gas activity before releasing them to the environment ;
- release of all the gaseous effluents, included those coming from the permanently ventilated rooms, by a dedicated system like a chimney ;
- permanent control of the activity of the gas released by the chimney

- respect of the thresholds of released activity (instantaneous and cumulated on a year) for each type of radionuclides (noble gas, tritium, halogen and aerosol)

Moreover, tests carried out on vegetable samples picked up outside INB, in particular in the wind direction, allow to check that the facility induces no impact on the environment.

All these technical and statutory regulations will be mentioned inside the release authorization decree needed to operate the facility.

4.9.2. Liquid

The constraints for the release of liquid radioactive effluents are similar to those for the gaseous effluents.

As there is no river or sea near GANIL where the liquid effluents could be diluted, the only way to release these effluents is to consider them as nuclear waste (see § 4.9.3 below) and to evacuate them towards facilities adapted to this task (ANDRA, CEA or COGEMA). Indeed, it is not very probable to get the authorization to throw the radioactive effluents in the public sewer. However, it may be envisageable to release in the sewer the liquid effluents whose radioactivity, checked by a measurement, is null.

4.9.3. Not gaseous Nuclear Wastes

Before the beginning of the exploitation, the present « Etude déchets de l'INB 113 » - which describes the process of treatment of the nuclear wastes – will be modified in order to integrate the new part of the INB represented by SPIRAL 2. The updating of this document makes part of the statutory procedures to get the authorization of operation of SPIRAL II facility.

4.10. Summary

	Radiation from beam	Activation after 15 days of irradiation		Contamination after 15 days of irradiation	
		Without cooling	One year of cooling	Without cooling	One year of cooling
Linac	0-45 MeV gamma : 25 Sv/h at 1 m	negligible	x	x	x
Beam dump	0-45 MeV gamma : 1000 Sv/h at 1 m	Low if adequate materials	negligible	confined	confined
Electron beam lines	Short bursts of 0-45 MeV gamma	x	x	x	x
Target	0-45 MeV gammas : 1000 Sv/h at 1 m 0-20 MeV neutrons : 30 Sv/h at 1 m	1500 Ci of PF 2 Sv/h at 1 m	1 Ci 2 mSv/h at 1 m	x	x
Pumping gas	x	150 Ci 200 mSv/h at 1 m	1 mCi 2 µSv/h at 1 m	x	x
Separator	x	x	x	150 Ci 100 mSv/h at 1 m	0.1 Ci 50 µSv/h at 1 m

Table 6 Summary of the dose equivalent

5. Facility Layout

5.1. Constraints

5.1.1. Radioactivity Constraints

The layout of the facility must take into account all the constraints imposed by the safety issues.

In particular, room must be kept to put down concrete shielding. One of the solutions is to install the beam components (linac, beam lines, TISS and their management) underground. Most of the services (cryogenic plant, linac RF, gas storage, power supplies, ..) could be set up in the ground floor.

Another assumption is to have a complete spare TISS facility in case of accident (as a high contamination for instance) which prevents from using the TISS. To be efficient, this spare facility must be independent from the first one. In a first step, this spare facility may be not equipped.

5.1.2. Connection with the present facilities

The implantation of SPIRAL II must guarantee the running of the other facilities, as well for its construction as for its use. In particular, the truck access to the GANIL hall must be kept.

5.1.3. Evolutions

The facility must be designed to welcome evolutions as the acceleration by the CO-CSS facility or by a specific booster.

The existence of a second TISS facility as spare can also be useful to develop and test new concept of production.

5.2. Schematic Description

The facility layout is schematically presented [Figure 34](#).

This implantation respects the constraints defined previously. However, it is just one of the numerous possible implantations which is presented to demonstrate that solutions exist.

The different parts of the facility are the :

1. Linear accelerator in a tunnel. A 2 m thick roof covers the tunnel.
2. Gallery where the electronic devices of the beam lines are installed.
3. Electron beam dumper.
4. Electron beam lines which allows to irradiate the target parallel to the source axis or perpendicularly.
5. Target and mono-charge state source in its plug.
6. Extraction ion line in a plug.
7. Mass separator consisting in a low magnetic field dipole set into a plug.
8. Ion beam line towards the low energy experiment area (LIRAT)
9. High efficiency mass spectrometer (optional).
10. Ion beam line towards CIME
11. Charge breeder.
12. Identification station.
13. Gallery for the transport of plugs
14. Cells to store plugs
15. Shielded cell to dismount the TISS from the plug.
16. Spare facility.
17. Junction with the CIME injection line . The identification bench is adapted to be used jointly by SPIRAL I and SPIRAL II.
18. Existing SPIRAL cave 1
19. SPIRAL cave 2 not yet equipped. Probably, this cave will be equipped with a two stage ionisation system.
20. Low energy experiment area (LIRAT)
21. Free room to install a booster to post-accelerate the beam coming from CIME or directly from the target via a charge breeder.
22. Beam line to possibly transport ions from SPIRAL target to GANIL injector or from CIME to CSS2 in order to re-accelerate them.
23. Limit of an external building for services.

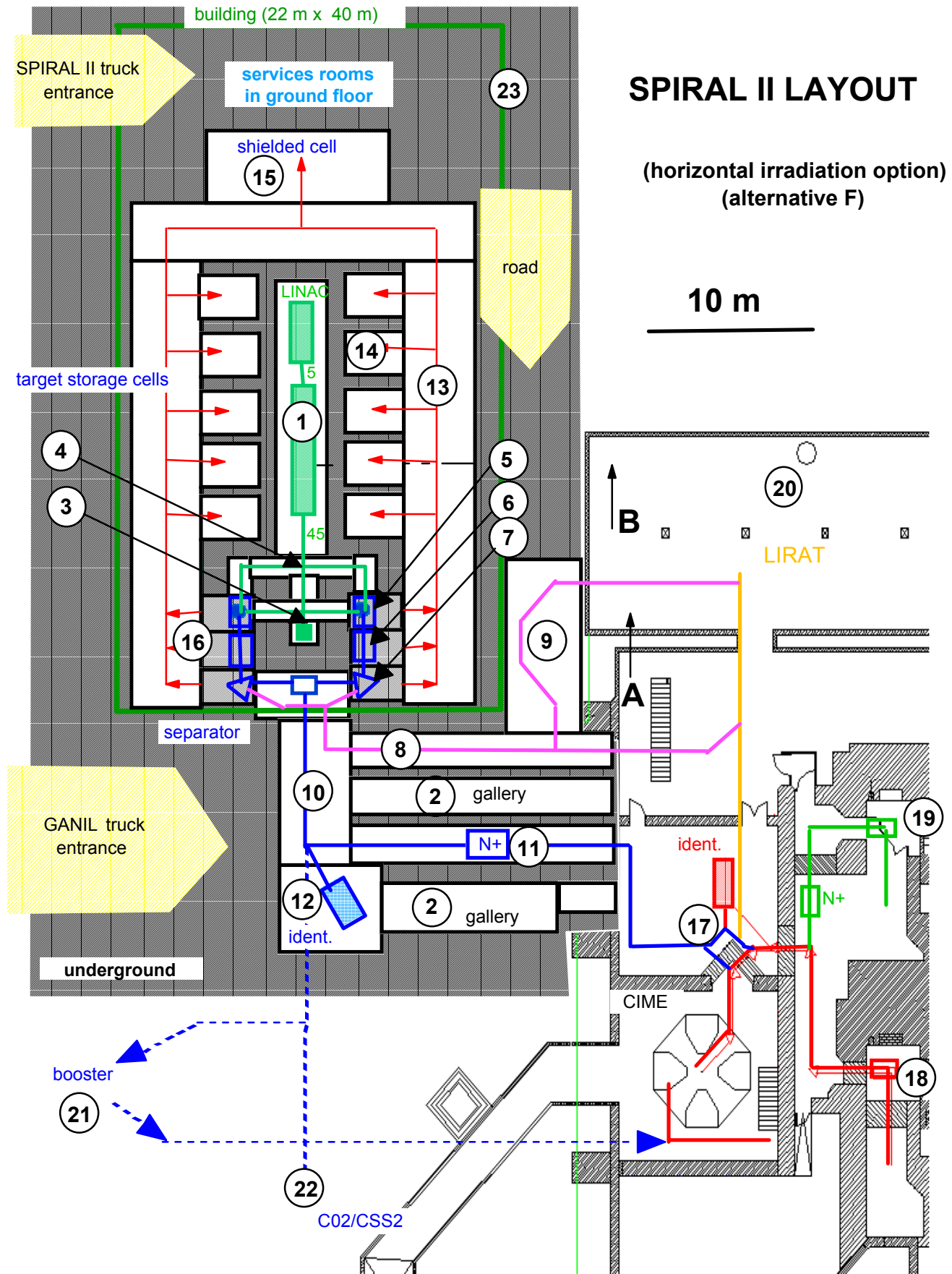


Figure 34 Schematic Layout of SPIRAL II Facility

6. Planning

6.1. Safety Regulation Actions

According to the French regulations, the construction of SPIRAL 2 on the GANIL site is a modification of the "Installation Nucléaire de Base" (INB 113). Therefore, statutory authorizations are required to build and operate this new facility. These authorizations are issued by the national competent authorities : the "Direction Générale de la Sûreté Nucléaire" (DSIN), on the basis of the analysis of the Safety reports which are written by GANIL.

Also, there are 3 main reports, and 2 mains steps, in this administrative procedure :

- first step, at the present stage of the project : a "Dossier d'Option de Sûreté" (DOS), whose aim is to describe the complete Safety options (such as confinement of radioactive matters) and the associated disposals;
- second step, once the studies are completed and the technical choices validated :
 1. a "Rapport Préliminaire de Sûreté" (RPS), which describes technically the facility and proposes an analysis of the identified risks ;
 2. in parallel, an application for an authorization of effluent release (radioactive and non radioactive), which evaluates the activity of radioactive effluents released and estimates the consequent impact on the environment.

The approval of these documents by the Safety Authority is followed by the issue of 2 legislative texts that allows to operate the modified nuclear facility GANIL : a decree of authorization of effluent release, and a local authorization (from "Préfecture du Calvados") to modify the nuclear facility.

The total delay to write all the documents, their study and approval by the Safety Authority up to the issue of the legislative texts, is nearly 4 years. However, to write the "Rapport Préliminaire de Sûreté" (RPS), the design must be sufficiently detailed to propose realistic solutions, that means this RPS can not completed before the end of the detailed design processus.

6.2. Technical Planning

Until the end of 2003, time will be dedicated to the detailed design of the project. During this time, research and development will be carried out on :

- the linac (RF couplers in particular),
- the charge breeder with the adaptation of the SIRA experimental area for this purpose,
- the target design with tests on SAPHIR accelerator (Saclay)
- the completion of the calculation on the radioactivity and, more generally, on the safety issues ,
- the layout of the facility with the help of an architect

At the end of this period, a precise budget and a detailed planning will be proposed.

The construction of the various parts of the facility takes around two years and one year and half more for the installation, the technical tests and the commisioning.

This technical planning is strongly linked to the statutory actions (see § 6 above)

6.3. Global Planning

Two options are proposed according to the date of the authorization to start the construction of the building : just after the approval of the DOS (option A : Table 7) or only after the agreement for the RPS (option B : Table 8). In our state of information, we can not know which option is the most realistic.

Planning (option A)	2002	2003	2004	2005	2006	2007	2008
start of the project	▲						
Detailed Design Study	—————						
"Dossier d'Option de Sûreté"	—————	★ approval				
"Dossier Préliminaire de Sûreté"		—————	—————	★ agreement			
release authorization dossier		—————	—————				
INB modification dossier		—————	—————				
"Enquêtes publiques"			—————				
"CIINB"				★			
Release authorization decree				★			
INB modification decree				★			
construction plans, call for tenders		—————	—————				
MACSE injector update and test		—————	—————	—————			
linac components construction			—————	—————	—————		
prototype TISS construction			—————	—————	—————		
2 TISS Construction				—————	—————	—————	
building construction			▼	—————	—————		
installation				—————	—————		
linac commissioning					—————	—————	
commissioning						—————	
physics experiments starting							★

Table 7 Planning (option A)

Planning (option B)	2002	2003	2004	2005	2006	2007	2008
start of the project	▲						
Detailed Design Study	—————						
"Dossier d'Option de Sûreté"	—————		agreement			
"Dossier Préliminaire de Sûreté"		—————	—————	★			
release authorization dossier		—————	—————				
INB modification dossier		—————	—————				
"Enquêtes publiques"			—————				
"CIINB"				★			
Release authorization decree				★			
INB modification decree				★			
construction plans, call for tenders		—————	—————				
MACSE injector update and test		—————	—————	—————			
linac components construction			—————	—————	—————		
prototype TISS construction			—————	—————	—————		
2 TISS Construction				—————	—————	—————	
building construction			—————	—————		
installation					—————	—————	
linac commissioning						—————	
commissioning							—————
physics experiments starting							★

Table 8 Planning (option B)

7. Costs

Two options have been taken to estimate the cost of the project :

- **The optimum option** which plans the future evolutions and the installation of all the means to operate the facility in the best conditions. This option corresponds to the implantation proposed in Figure 34 (see § 5.2) with only one TISS equipped and without the high resolution separator for LIRAT.
- **The minimum option** plans to build and install only one TISS without possibility to easily install a second one later and with simplified beam lines (no spectrometer after the N+ source for instance). This option can be compared to the LINAG I project.

Any intermediary solutions are envisageable like, for instance, to keep the possibility to build a second TISS easily.

5 % of hazards have been added. The salary cost of the laboratory people have not been taken into account.

Table 9 below presents the cost of these two options. The re-use of MACSE can save 2.5 M€.

SPIRAL II BUDGET		
(M€)	45 MeV electron (optimum)	45 MeV electron (minimum)
R & D for design	1,55	1,55
Building / Infrastructure	6,00	5,00
Linac Driver	6,10	6,10
Targets / Sources 1+	6,10	5,70
Source N+	0,45	0,45
Beam lines	5,65	4,15
Radioprotection	1,75	1,75
Control system	0,30	0,30
Miscellaneous & hazards	1,75	1,75
TOTAL (M€)	29,65	26,75
MACSE re-use	-2,50	-2,50
GRAND TOTAL (M€)	27,15	24,25

Table 9 Cost of the project

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