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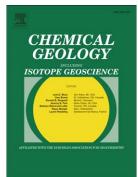
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# A model for the activity of silica along the carbonatitekimberlite-mellilitite-basanite melt compositional joint

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#### Abstract

Carbon dioxide and water, being present in the Earth's mantle at concentration levels of tens to hundreds of ppm, greatly lower the peridotite solidus temperature and drastically modify the composition of produced melts. The presence of CO<sub>2</sub> produces silica-poor, carbonate-rich liquids at the onset of melting, and these liquids shift toward silica rich compositions as the degree of melting increases. Numerous geochemical observations and experimental studies have revealed the complexity of the transition between carbonate-rich and silicate-rich melts. It is characterized by a strongly non-linear evolution and, under specific conditions, by immiscibility. To better constrain this transition, we have used the thermodynamic activity of silica as a probe of the mixing properties between molten carbonate and molten silicate. The activity of silica  $(a_{SiO_2(l)})$  was calculated for a large number of experimental liquids from two equilibria: olivine-orthopyroxene-melt and immiscible silicate-rich melt-carbonate-rich melt (491 data points ranging from 1 to 14 GPa and 1090 to 1800°C). We modeled  $a_{SiO_2(1)}$  during incipient melting of the peridotite in presence of CO<sub>2</sub> with a generalized Margules function. Our model well reproduces the silica activity-composition relationships of the experimental database, and can be used to predict the silica content of the melts coexisting with olivine and orthopyroxene. We show that water content and Ca/Mg ratio in the melts have an important influence on the  $a_{SiO_2(1)}$ . In contrast to a recent empirical model (Dasgupta et al., 2013), the analysis of the experimental database reveals that the transition from carbonate to silicate melt with decreasing depth should occur abruptly in oceanic mantle. Our model predict that carbonatitic melts with ~5 wt.% SiO<sub>2</sub> can be stabilized from ~150 km depth, at the onset of incipient melting by "redox melting", up to  $\sim$ 75 km, above which the liquid evolves abruptly to a carbonated silicate composition (> ~25 wt.% SiO<sub>2</sub>). In the cratonic mantle lithosphere, our model predicts that carbonatitic melts are prevailing up to shallow depth, and conflicts the recent model (Russell et al., 2012) of CO<sub>2</sub>-saturation triggered by orthopyroxene assimilation during kimberlite ascent.

Keywords: incipient partial melting; carbonate-silicate melt transition; thermodynamic model; silica activity; ridge adiabat; immiscibility

### 1. Introduction

Partial melting in the Earth's mantle is a key process in the global geodynamics since it produces the igneous rocks constituting the continental and oceanic crusts and it most likely gives rise to the geophysical signal of mantle mechanical weakening (Green and Liebermann, 1976; Presnall and Gudfinnsson, 2005; Holtzman and Kohlstedt, 2007; Gaillard et al., 2008; Hirschmann, 2010; Stagno et al., 2013; Sifré et al., 2014). Experimental petrology provides a key step in addressing the impact of mantle melting on global geodynamics, but the development of models capable of interpolating and extrapolating these data is mandatory. Such models must allow defining 1) the pressure-temperature location of the peridotite solidus and 2) the composition of the partial melts formed at a given pressure, temperature and bulk composition. Ghiorso and co-workers (Ghiorso et al., 1983; Ghiorso and Sack, 1995) have pioneered the numerical modelling of liquid-solid phase equilibria applied to magmatic systems, and this methodology has subsequently been extended to mantle melting (Hirschmann et al., 1998; Asimow et al., 2004).

The presence of volatiles species, water  $(H_2O)$  and carbon dioxide  $(CO_2)$ , is long known from experimental petrology to greatly affect both solidus and composition of partial melts produced in the mantle (Wyllie and Huang, 1976; Olafsson and Eggler, 1983; Taylor and Green, 1988; Wallace and Green, 1988; Thibault et al., 1992; Dasgupta and Hirschmann, 2006; Jakobsson and Holloway, 2008; Hirschmann, 2010; Rohrbach and Schmidt, 2011; Dasgupta, 2013; Tumiati et al., 2013; Ghosh et al., 2014; Hammouda & Keshav, 2015). In particular, volatiles, being present in the Earth's mantle at low concentration levels, give rise to incipient melting, which is the formation of small melt fractions being stable in a large pressure-temperature domain (Fig.1). Modelling incipient melting in the presence of CO<sub>2</sub> is particularly challenging because it produces carbonate-rich liquid compositions at low temperature, which evolve toward basaltic compositions with increasing temperature or decreasing pressure. The transition between carbonate-dominated and silicate-dominated melts coexisting with a peridotite/eclogite assemblage is rather well constrained by experimental petrology. However, the different experimental surveys on various chemical systems (quaternary to multicomponent) reveal a complex behaviour. The transition from carbonate melt to silicate melt is generally strongly non-ideal, and can show, under specific conditions, a miscibility gap between the two types of liquids.

In simple carbonated (CMAS-CO<sub>2</sub>) peridotite systems, carbonate-silicate liquids immiscibility has been reported (Novella et al., 2014). In quasi-natural systems, the transition between ionic carbonate melts (Jones et al., 2013) and polymerized silicate melts (i.e.  $Q^n$  species, Mysen, 1999) seems to be continuous (miscible) although the change in melt chemistry is abrupt, and this transition becomes increasingly sharp with decreasing pressure. For example, at 3 GPa, the silica content of the liquid coexisting with a peridotite evolves from less than 10 wt.% (carbonatitic melt) to more than 25 wt.% (carbonate-rich silicate melt) from 1325 to 1350°C (Dasgupta et al., 2007). With increasing pressure, the carbonate to silicate melt transition is smoother possibly because of a higher CO<sub>2</sub> solubility in the silicate melt (Brey and Green, 1976; Morizet et al., 2002; Guillot and Sator, 2011). The carbonate-silicate melt transition is also strongly dependent on the chemistry of the system. At a given pressure and temperature, the melt in equilibrium with a peridotite can be silica-poor ( $< 10 \text{ wt.\% SiO}_2$ ) in an alkali-free system and becomes richer in silica ( $> 15 \text{ wt.\% SiO}_2$ ) if alkalis are present (Moore, 2012).

Immiscibility between carbonate-rich and silicate-rich melts was reported in carbonated eclogitic compositions (Hammouda, 2003; Dasgupta et al., 2006; Tsuno and Dasgupta, 2011; Kiseeva et al., 2012). At 3 GPa, Dasgupta et al. (2006) interpreted the coexistence of both melts by the lower melting temperature of silicate in the eclogitic system compared to the peridotitic system; low temperature tends to favour immiscibility (Brooker and Kjarsgaard, 2011). The lower silicate solidi for the eclogitic bulk composition are related to the lower Mg-numbers and higher alkali contents (Kogiso et al., 2004), which may also impact the miscibility gap. For example, Kiseeva et al. (2012) observed immiscibility at 3.5 and 5.5 GPa, that they attributed to the addition of H<sub>2</sub>O and K<sub>2</sub>O. Chemical composition of the melts (alkalis, H<sub>2</sub>O, MgO), temperature, and pressure have therefore complex and interrelated effects on the carbonate-silicate transition.

Several models address the H<sub>2</sub>O-induced incipient mantle melting (Asimow and Langmuir, 2003; Katz et al., 2003; Hirschmann et al., 2009). The incorporation of CO<sub>2</sub> in the systems was modelled in more recent studies (Dasgupta and Hirschmann, 2010; Hirschmann, 2010; Dasgupta et al., 2013). These empirical models are based on limited databases and are hardly applicable out of their range of calibration. In this study, we use the thermodynamic activity of SiO<sub>2</sub> as a probe of the mixing properties between molten carbonate (carbonatite) and molten silicate (basalt). The activity of silica in the melts  $(a_{SiO_2(1)})$  is a powerful probe to characterize melts and their evolution with temperature, pressure and compositional variations as pioneered by Carmichael et al. (1970) in the case of silicate melts. This approach was also developed for carbonate melts (Barker, 2001; Luth, 2009). These studies explained the methodology of calculation of  $a_{SiO_2(1)}$  but did not compare the evolution of the  $a_{SiO_2(1)}$  relative to its actual fraction of silica determined by phase equilibria studies (i.e.,  $a_i = X_i \cdot \gamma_i$ , with a, the activity, X, the molar fraction and  $\gamma$ , the activity coefficient).

We compiled a large database of equilibria involving carbonate melts with an important chemical diversity ranging from quaternary to quasi-natural systems, and with pressure and temperature ranging from 1 to 14 GPa and 1090 to 1800°C (Fig. 1; Table 1). We considered two type of equilibrium: (i) coexistence of melt with olivine and orthopyroxene, and (ii) immiscible carbonate-rich and silicate-rich melts. We develop a thermodynamic model, based on the Margules formalism (Ghiorso et al., 1983; Ghiorso and Sack, 1995; Ghiorso et al., 2002; Green et al., 2012a). Using oxide components, this formalism is used to calculate the  $a_{SiO_2(1)}$  during incipient melting of the peridotite in presence of CO<sub>2</sub> in the system SiO<sub>2</sub>-TiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-FeO-MnO-CaO-MgO-Na<sub>2</sub>O-K<sub>2</sub>O-P<sub>2</sub>O<sub>5</sub>-H<sub>2</sub>O-CO<sub>2</sub>. Our model satisfactorily reproduces the activity-composition relationships of SiO<sub>2</sub> in the 1-10 GPa pressure range and the 1100-1700°C temperature range, and can therefore be used to predict the silica content of CO<sub>2</sub>-bearing melts in the upper mantle.

### 2. Modelling

### 2.1. Experimental database

The selected experimental database regroups 491 experimental melts from CMS-CO<sub>2</sub> to quasi-natural systems, at pressures and temperature ranging from 1 to 14 GPa and 1090 to 1800°C (Table 1). The database includes hydrous experiments, as well as some volatile-free experiments (see Supplementary Information Part 1 for details on the determination of CO<sub>2</sub> and H<sub>2</sub>O contents when both are present). We also performed additional experiments at 3 GPa in order to better constrain the role of alkalis and Ca/Mg on the miscibility gap (see Supplementary Information Part 2 for details on the experimental protocol and melt compositions). Note that experimental data in quasi natural systems bearing K<sub>2</sub>O, Na<sub>2</sub>O, CO<sub>2</sub> and H<sub>2</sub>O together are rare (36 data points for the crystal-liquid equilibrium, 0 data point for the liquid-liquid equilibrium). Moreover, some experimental studies in presence of water were not included in the model due to the lack of chemical analyses, experimental conditions, difficulties to estimate the CO<sub>2</sub> and H<sub>2</sub>O contents in the melt phase.

#### 2.2. Calculation of silica activities from thermodynamic database

#### 2.2.1. Crystal-liquid equilibrium

We consider melts in equilibrium with olivine and orthopyroxene and assume that the  $a_{SiO_2(l)}$  in the melt is constrained by the equilibrium (e.g. Carmichael et al., 1970; Luth, 2009)

$$Mg_2SiO_4 + SiO_2(l) = Mg_2Si_2O_6, (1)$$

where  $SiO_2(l)$  is the silica component in the melt,  $Mg_2SiO_4$  is the forsterite component in olivine and  $Mg_2Si_2O_6$  is the enstatite component in orthopyroxene.

At given P and T, equilibrium implies

$$\Delta G^* + R T \ln(K) = 0, \quad (2)$$

where R is the universal gas constant (8.314 J.mol<sup>-1</sup>.K<sup>-1</sup>),  $\Delta G^*$  is the standard state Gibbs free energy of the reaction

$$\Delta G^* = G^*_{Mg_2Si_2O_6} - G^*_{Mg_2SiO_4} - G^*_{SiO_2(l)}, \quad (3)$$

K is the equilibrium constant

$$K = a_{Mg_2Si_2O_6} / (a_{SiO_2(l)} a_{Mg_2SiO_4}), \quad (4)$$

 $a_{Mg_2SiO_4}$  and  $a_{Mg_2Si_2O_6}$  are the activity of forsterite in olivine, and the activity of enstatite in orthopyroxene, respectively. The calculation of  $\Delta G^*$  was based on the thermodynamic database of Holland and Powell (2011) (see Supplementary Information Part 3). For enstatite, the distinction between 2 polymorphs, orthoenstatite and clinoenstatite, is considered, as a function of the pressure and temperature conditions (Ulmer and Stalder, 2001). Eq. (4)

implies that, at a given pressure and temperature, the only way to vary the  $a_{SiO_2(l)}$  is to vary the ratio of forsterite to enstatite activities. However, in all experiments, as well as in the mantle (production of small melt fractions by incipient melting should not modify the composition of olivine and orthopyroxene in terms of Mg#), this ratio can be considered constant compared to the variability of  $\Delta G^*/(R T)$ . Therefore  $a_{SiO_2(l)}$  mainly varies as a function of pressure or temperature as an increase in temperature and a decrease of pressure will increase  $a_{SiO_2(l)}$  (see Fig. S2).

In quasi-natural systems, a non-ideal solid solution is often considered for olivine and orthopyroxene (Ghiorso et al., 1983; Stagno and Frost, 2010; Green et al., 2012b); however in the present work we chose to use ideal solid solutions definition. This approximation is relatively safe due to the predominant magnesian character in the data and will only introduce minor deviations on  $a_{SiO_2(l)}$  (see Supplementary Information Part 5). Consequently, their activities are given by

$$a_{Mg_2SiO_4} = \left( X_{Mg}^{M1,Fo} X_{Mg}^{M2,Fo} \right) \quad (5)$$

and

$$a_{Mg_2Si_2O_6} = \left( X_{Mg}^{M1,Ens} X_{Mg}^{M2,Ens} \right), \quad (6)$$

where  $X_{Mg}^{M1,Fo}$  and  $X_{Mg}^{M2,Fo}$  are the mole fraction of Mg in the M1 site and the M2 site of forsterite, respectively, and  $X_{Mg}^{M1,Ens}$  and  $X_{Mg}^{M2,Ens}$  are the mole fraction of Mg in the M1 site and the M2 site of enstatite, respectively. Following Ghiorso and Carmichael (1980), Hirschmann (1991) and Ghiorso et al. (1983), the site mole fractions are estimated by:

$$X_{Mg}^{M1,Fo} = n_{Mg}^{M1,Fo} / (n_{Ni} + n_{Fe}^{M1,Fo} + n_{Mg}^{M1,Fo}), \quad (7)$$
  

$$X_{Mg}^{M2,Fo} = n_{Mg}^{M2,Fo} / (n_{Ca} + n_{Mn} + n_{Fe}^{M2,Fo} + n_{Mg}^{M2,Fo}), \quad (8)$$
  

$$X_{Mg}^{M1,Ens} = n_{Mg}^{M1,Ens} / (n_{Ti} + 0.5 n_{Al} + n_{Cr} + n_{Fe}^{M1,Ens} + n_{Mg}^{M1,Ens}), \quad (9)$$

and

$$X_{Mg}^{M2,Ens} = n_{Mg}^{M2,Ens} / \left( n_{Ca} + n_{Na} + n_{Mn} + n_{Fe}^{M2,Ens} + n_{Mg}^{M2,Ens} \right), \quad (10)$$

where

$$n_{Mg}^{M1,Fo} = \left(n_{Mg} / \left(2\left(n_{Mg} + n_{Fe}\right)\right)\right) \left(n_{Ca} + n_{Mn} + n_{Fe} + n_{Mg} - n_{Ni} - n_{Ti} - 0.5 n_{Al}\right), \quad (11)$$

$$n_{Mg}^{M1,Ens} = \left(n_{Mg} / \left(2\left(n_{Mg} + n_{Fe}\right)\right)\right) \left(n_{Ca} + n_{Mn} + n_{Na} + n_{Fe} + n_{Mg} - n_{Cr} - n_{Ti} - 0.5 n_{Al}\right), \quad (12)$$

$$n_{M1,Fo}^{M1,Fo} = n_{M1,Fo}^{M1,Fo} \left(1 / \left(n_{Mg} + n_{Hg}\right)\right) = 1\right) \quad (13)$$

$$n_{Fe}^{M1,H0} = n_{Mg}^{M1,H0} \left( \frac{1}{(n_{Mg}/(n_{Mg} + n_{Fe})) - 1}, (13) \right)$$
$$n_{Fe}^{M1,Ens} = n_{Mg}^{M1,Ens} \left( \frac{1}{(n_{Mg}/(n_{Mg} + n_{Fe})) - 1}, (14) \right)$$

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Transition Carbonate-silicate mantle melt model Massuyeau et al. 2015

$$n_{Mg}^{M2,Fo} = n_{Mg} - n_{Mg}^{M1,Fo}, \quad (15)$$
  

$$n_{Mg}^{M2,Ens} = n_{Mg} - n_{Mg}^{M1,Ens}, \quad (16)$$
  

$$n_{Fe}^{M2,Fo} = n_{Fe} - n_{Fe}^{M1,Fo} \quad (17)$$

and

$$n_{Fe}^{M2,Ens} = n_{Fe} - n_{Fe}^{M1,Ens}.$$
 (18)

The silica activity in the melt is given by:

$$ln(a_{SiO_2(l)}) = (\Delta G^* / (R T)) + ln((X_{Mg}^{M1,Ens} X_{Mg}^{M2,Ens}) / (X_{Mg}^{M1,Fo} X_{Mg}^{M2,Fo}))$$
(19)

Therefore the silica activity coefficient  $\gamma_{SiO_2(l)}$  writes

$$R T \ln(\gamma_{SiO_2(l)})_{exp} = \Delta G^* + R T \ln((X_{Mg}^{M1,Ens} X_{Mg}^{M2,Ens}) / (X_{Mg}^{M1,Fo} X_{Mg}^{M2,Fo})) - R T \ln(X_{SiO_2(l)})$$
(20)

 $SiO_2$  activity-composition relationships for the experimental crystal-liquid equilibria are reported in Figs. 2A-E, 2G.

#### 2.2.2. Liquid-liquid equilibrium

When two immiscible silicate-rich melt (SL) and carbonate-rich melt (CL) coexist at equilibrium, their  $a_{SiO_2(l)}$  is identical, with

$$a_{SiO_2(l)}^{SL} = a_{SiO_2(l)}^{CL}$$
 (2)

Then, we can write

$$X_{SiO_{2}(l)}^{SL} \gamma_{SiO_{2}(l)}^{SL} = X_{SiO_{2}(l)}^{CL} \gamma_{SiO_{2}(l)}^{CL}$$
(22)

or

$$R T \ln(\gamma_{SiO_{2}(l)}^{CL} / \gamma_{SiO_{2}(l)}^{SL})_{exp} = R T \ln(X_{SiO_{2}(l)}^{SL} / X_{SiO_{2}(l)}^{CL})$$
(23)

R T  $\ln(\gamma_{SiO_2(l)}^{CL}/\gamma_{SiO_2(l)}^{SL})_{exp}$ -composition relationships for the experimental liquid-liquid equilibria are reported in Fig. 2H.

### 2.3. Model for the activity coefficient $\gamma_{SiO_2(l)}$

We describe the chemical space between carbonate and silicate end-members using oxide components (SiO<sub>2</sub>, TiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, Cr<sub>2</sub>O<sub>3</sub>, FeO, MnO, CaO, MgO, Na<sub>2</sub>O, K<sub>2</sub>O, P<sub>2</sub>O<sub>5</sub>, H<sub>2</sub>O, CO<sub>2</sub>) (Richet and Bottinga, 1985). Following DeCapitani and Kirschen (1998), we relate  $\gamma_{SiO_2(l)}$  to the excess Gibbs free energy of the liquid  $G_{(l)}^{XS}$  as follows:

$$R T \ln(\gamma_{SiO_{2}(l)})_{calc} = G_{(l)}^{XS} + \left(\partial G_{(l)}^{XS} / \partial X_{SiO_{2}(l)}\right)_{p,T,X_{k},k \neq SiO_{2}(l)} - \sum_{j=1}^{nc} X_{j} \left(\partial G_{(l)}^{XS} / \partial X_{j}\right)_{p,T,X_{k},k \neq j}, \quad (24)$$

where *nc* is the number of components.  $G_{(1)}^{XS}$  was taken as a generalized Margules function in which the SiO<sub>2</sub>-CO<sub>2</sub> interaction is modelled by a third-degree polynomial (asymmetric part) using two Margules parameters,  $W_{SiO_2-CO_2}^a$  and  $W_{SiO_2-CO_2}^b$ , in order to account for the strong non-ideality between these two components. The interaction between the other selected binaries is modelled by a second-degree polynomial (symmetric part) with single Margules parameters  $W_{i-j}$ . The Margules parameters are assumed to be independent on pressure and temperature. The construction of a more complete thermodynamic formulation, e.g. including the activity coefficient of all components, would certainly be worthwhile but is beyond the scope of the present study.

Preliminary calculations were performed in order to select the terms of  $G^{XS}$  relevant for calculating  $\gamma_{SiO_2(1)}$ . We rejected the binaries having (1) absolute values of the correlation coefficient with  $RT \ln(\gamma_{SiO_2(1)})$  lower than 0.2 (see Supplementary Table S4), and (2)  $W_{i-j}s$  with uncertainties higher than 50% (see Table 2). The selected  $G_{(1)}^{XS}$  function is

$$G_{(l)}^{XS} = W_{SiO_2-CO_2}^a X_{SiO_2}^2 X_{CO_2} + W_{SiO_2-CO_2}^b X_{SiO_2} X_{CO_2}^2 + W_{Al_2O_3-SiO_2} X_{Al_2O_3} X_{SiO_2} + W_{CaO-SiO_2} X_{CaO} X_{SiO_2} + W_{Na_2O-SiO_2} X_{Na_2O} X_{SiO_2} + W_{K_2O-SiO_2} X_{K_2O} X_{SiO_2} + W_{Al_2O_3-CO_2} X_{Al_2O_3} X_{CO_2} + W_{FeO-CO_2} X_{FeO} X_{CO_2} + W_{MgO-CO_2} X_{MgO} X_{CO_2} + W_{Na_2O-CO_2} X_{Na_2O} X_{CO_2} + W_{K_2O-CO_2} X_{K_2O} X_{CO_2} + W_{H_2O-CO_2} X_{H_2O} X_{CO_2} + W_{Al_2O_3-FeO} X_{Al_2O_3} X_{FeO} + W_{Al_2O_3-MgO} X_{Al_2O_3} X_{MgO} + W_{FeO-CaO} X_{FeO} X_{CaO} + W_{CaO-Na_2O} X_{CaO} X_{Na_2O},$$
(25)

which yields, when substituted in Eq. (24),

$$RT \ln(\gamma_{SiO_{2}(1)})_{calc} = W^{a}_{SiO_{2}-CO_{2}} \left( 2 X_{SiO_{2}} X_{CO_{2}} - 2 X^{2}_{SiO_{2}} X_{CO_{2}} \right) + W^{b}_{SiO_{2}-CO_{2}} \left( X^{2}_{CO_{2}} - 2 X_{SiO_{2}}^{2} X_{CO_{2}} \right) + W^{b}_{SiO_{2}-CO_{2}} \left( X^{2}_{CO_{2}} - 2 X_{SiO_{2}}^{2} X_{CO_{2}} \right) + W^{b}_{SiO_{2}-CO_{2}} \left( X^{2}_{CO_{2}} - 2 X_{SiO_{2}}^{2} X_{CO_{2}} \right) + W^{b}_{Na_{2}O_{3}-SiO_{2}} X_{Al_{2}O_{3}} 1 - XSiO_{2} + W_{CaO} - SiO_{2} X_{CaO} \left( 1 - X_{SiO_{2}} \right) + W_{Na_{2}O-SiO_{2}} X_{Na_{2}O} \left( 1 - X_{SiO_{2}} \right) + W_{K_{2}O-SiO_{2}} X_{K_{2}O} \left( 1 - X_{SiO_{2}} \right) - W_{Al_{2}O_{3}-CO_{2}} X_{Al_{2}O_{3}} X_{CO_{2}} - W_{FeO-CO_{2}} X_{FeO} X_{CO_{2}} - W_{MgO-CO_{2}} X_{MgO} X_{CO_{2}} - W_{Na_{2}O-CO_{2}} X_{Na_{2}O} X_{CO_{2}} - W_{K_{2}O-CO_{2}} X_{K_{2}O} X_{CO_{2}} - W_{H_{2}O-CO_{2}} X_{H_{2}O} X_{CO_{2}} - W_{Al_{2}O_{3}-FeO} X_{Al_{2}O_{3}} X_{FeO} - W_{Al_{2}O_{3}-MgO} X_{Al_{2}O_{3}} X_{MgO} - W_{FeO-CaO} X_{FeO} X_{CaO} - W_{CaO-Na_{2}O} X_{CaO} X_{Na_{2}O}.$$
(26)  
2.4. Uncertainties, bias and strength of the model:

The general formula for the uncertainty propagation on  $a_{SiO_2(l)}$  is

$$\delta_{a_{SiO_2(l)}}^2 = \left(\frac{\partial a_{SiO_2(l)}}{\partial (\Delta G^* / (R T))}\right)^2 \delta_{[\Delta G^* / (R T)]}^2 + \left(\frac{\partial a_{SiO_2(l)}}{\partial a_{Mg_2Si_2O_6}}\right)^2 \delta_{a_{Mg_2Si_2O_6}}^2 + \left(\frac{\partial a_{SiO_2(l)}}{\partial a_{Mg_2SiO_4}}\right)^2 \delta_{a_{Mg_2SiO_4}}^2.$$
(27)

The uncertainty on  $\Delta G^*/(R T)$  is predominant relative to the uncertainties on  $a_{Mg_2Si_2O_6}$  and  $a_{Mg_2SiO_4}$ . Consequently, the errors on the latter activity terms are neglected in the error propagation (~10-15 % of the actual error on  $a_{SiO_2(1)}$  calculated with only  $\Delta G^*/(R T)$ ).

The uncertainty on  $\Delta G^*/(R T)$  is calculated by propagating experimental (P, T) and thermodynamic (reference states H<sub>i</sub>) uncertainties (see Supplementary Information Part. 3). Unless specified by the author, we consider an error of 12°C (Dasgupta et al., 2005) and 0.1 GPa for piston-cylinder experiments (Dasgupta et al., 2013), and an error of 30°C (Keshav et al., 2011) and 0.3 GPa for multi-anvil experiments (Dasgupta et al., 2013). This typically results in uncertainties on  $a_{SiO_2(I)}$  of about 10-15 % (Figs. 2-3). In most cases, the uncertainty on the silica content is given by the experimental studies (see Fig. S5A). When the error on the silica content is unknown, we approximate the uncertainties using an exponential function which provides a representative error within the investigated SiO<sub>2</sub> content (Fig. S5A; see Supplementary Information Part 4b). Details on the calculation of uncertainties are reported in the Supplementary Information Parts 4.

Some biases tarnish the model, principally due to the definition of the  $G_{(1)}^{XS}$ . Firstly, the Margules parameters are only calibrated via the RT  $\ln(\gamma_{SiO_2(1)})$  (Eq. 24), which implies a partial description of the melt mixing properties. Secondly, the choice of ideal interaction between some components for the  $G_{(1)}^{XS}$  implies corresponding directions in the compositional space are not well constrained.

Nevertheless, the strength of the model is the incorporation of data points for the immiscibility between silicate and carbonate liquids. Indeed, this equilibrium only constrains the mixing properties of the melts, independently of the standard states (Berman and Brown, 1984).

### 2.5. Optimization

The Margules parameters were optimized for the activity coefficients calculated according to Eq. (26) to best match the experimental activity coefficients given by Eqs. (20) and (23), i.e. by minimizing

$$\sum_{i=1}^{nd1} \left( \left( \left( R \ T \ ln(\gamma_{SiO_{2}(l)}) \right)_{calc \ i} - \left( R \ T \ ln(\gamma_{SiO_{2}(l)}) \right)_{exp \ i} \right) / \delta_{\left( R \ T \ ln(\gamma_{SiO_{2}(l)}) \right)_{exp \ i}} \right)^{2} + \\ \sum_{i=1}^{nd2} \left( \left( \left( R \ T \ ln(\gamma_{SiO_{2}(l)}^{CL} / \gamma_{SiO_{2}(l)}^{SL}) \right)_{calc \ i} - \left( R \ T \ ln(\gamma_{SiO_{2}(l)}^{CL} / \gamma_{SiO_{2}(l)}^{SL}) \right)_{exp \ i} \right) / \delta_{\left( R \ T \ ln(\gamma_{SiO_{2}(l)}^{CL} / \gamma_{SiO_{2}(l)}^{SL}) \right)_{exp \ i}} \right)^{2} ,$$

$$(28)$$

where the sum is done over all the crystal-liquid equilibria (nd1 = 400) and the liquid-liquid equilibria (nd2 = 91).

In addition to the Margules parameters, we also refined the standard volume of reaction because the volume of  $SiO_2(l)$  has only been calibrated at low pressures (<6 GPa) in the database of Holland and Powell (2011) (see Supplementary Information Part 3; Fig. S4).

The optimized Margules parameters for the  $G_{(1)}^{XS}$  function (Eq. 25) are reported with associated uncertainties in Table 2. The calculated  $X_{SiO_2(1)}$  for crystal-liquid equilibria and  $\gamma_{SiO_2}^{CL}/\gamma_{SiO_2}^{SL}$  for liquid-liquid equilibria compares fairly well with the experimental data (Fig. 3). Deviations mostly compare to experimental uncertainties, and are 15% on average (Fig. S5B). Our model is reliable for 1-10 GPa and 1100-1700°C, since most of experiments lie in this range (Fig. 1), and therefore covers most of the upper mantle conditions without extrapolation.

### 3. Discussion

3.1. Observed versus predicted effect of pressure, temperature and bulk composition on  $a_{SiO_2}$  in magmatic liquids

As expected,  $a_{SiO_2(1)}$  globally increases with the silica concentration of the experimental melts (e.g. Fig. 2A). At highest SiO<sub>2</sub> content (>~ 30 wt.%), mixing is close to ideal although small negative deviations are observed. However, a strong positive deviation from ideal mixing is observed in the carbonate part (<~ 20 wt.% SiO<sub>2</sub>), together with a broadening of the activity ranges. This is even more striking from the evolution of the  $\gamma_{SiO_2(1)}$  as a function of silica content (Fig S6), which is about 1 for 30-50 wt.% SiO<sub>2</sub> and strongly increases up to more than 10 for <30 wt.% SiO<sub>2</sub>.

Activity decreases significantly as a function of pressure. This effect is especially pronounced in the most carbonate part, where  $a_{SiO_2(1)}$  drops from ~ 0.3 to 0.1 from 1 to 10 GPa (Fig. 2A). On the other hand, no clear trend is observed with temperature but it is likely because it varies less than pressure among experiments (Fig. 2B). As shown in Fig. 2C, experiments performed with significant amount of water (> 0.2 wt.% bulk) have significantly lower SiO<sub>2</sub> activities than nominally dry experiments, especially in the carbonate part. Water therefore makes carbonate melts closer to ideal mixture.

There is no discernible difference between CMAS and quasi-natural systems except for the carbonate part (< ~20 wt. SiO<sub>2</sub>), where CMAS systems display higher deviations from ideal mixing (Fig. 2D). This mainly stems from higher Ca/Mg ratios which are found to strongly enhance positive deviations from ideal mixing (Fig. 2E). Actually, most of the range of the experimental data can be reproduced by our model by changing the Ca/Mg ratio together with the water content (Fig. 4A). Interestingly, there is a strong dependence of the Ca/Mg ratio on pressure in carbonate melts with <20 wt.% SiO<sub>2</sub>; the higher the pressure, the lower the Ca/Mg ratio (Fig. 2F; Dalton and Wood, 1993). There is therefore a correspondence between pressure and the chemistry of the melts.

The weak variation of activities at intermediate  $SiO_2$  content (15-35 wt.%), leading to the overall sigmoidal shape of the database (e.g. quasi-natural data on Fig. 2D) and which is

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reproduced by our model (e.g. Fig. 4A), implies that the transition from silicate to carbonate melt from high to low  $a_{SiO_2(l)}$  occurs within a narrow range of activity. Importantly, as activity decreases with increasing pressure, this implies that melts change rather abruptly from silicate to carbonate compositions with depth when not accompanied by important change in temperature.

Moreover, the dependence of  $a_{SiO_2(1)}$  on  $X_{SiO_2(1)}$  may even reverse and be negative at intermediate  $X_{SiO_2(l)}$ , depending on melt composition. This is for instance visible for the CMAS data in figure 2D which globally have higher Ca/Mg ratios, and this is also reproduced by our model for high Ca/Mg ratios (Fig. 4A). This pattern is indicative of immiscibility between carbonate and silicate melts though, the whole surface of the Gibbs free energy of mixing is required to predict immiscibility. Ca-rich melts therefore strongly deviate from ideality and our model predict that immiscibility may occur at the highest enrichments, which is in consistency with the immiscibility of carbonated eclogitic systems (Dasgupta et al, 2006).

Alkalis also favor immiscibility. This is less apparent from crystal-liquid equilibrium data (Fig. 2G) because almost of these melts contain relatively small amount of alkalis (<  $\sim$ 5-6 wt.%). However, the immiscible liquid-liquid equilibrium data, where high alkalis content were used (mostly >  $\sim$ 5%), clearly show that the miscibility gap increases with the (Na+K)/Mg ratio (Fig. 2H). The favoring of immiscibility by alkalis is in line with the conclusion of Brooker and Kjarsgaard (2011), but it requires rather elevated alkalis content (Fig. 4B).

### 3.2. Evolution of the melt along a ridge adiabat

We applied our model to predict the evolution of the  $SiO_2$  content of incipient melts in the oceanic upper mantle (Fig. 5A). Calculations were performed from 60 to 300 km depth (2 to 10 GPa) along a ridge adiabat with a potential temperature  $Tp = 1350^{\circ}C$  (temperature at pressure of 1 bar in a adiabatic system), and assuming melt in equilibrium with olivine and orthopyroxene of pyrolitic composition. This calculation therefore remains in the range of calibration of our model. For this application, we propagated the uncertainties on the Margules parameters as reported in Table 2, and the uncertainties on the reference states H<sub>i</sub>, which overall, produce the green envelop surrounding the dry curve (Fig. 5A). The silicate and carbonate melt end-members were taken similar to those of Dasgupta et al. (2013), but we consider additionally that the Ca/Mg ratio in the carbonate end-member varies as a function of pressure as mentioned above and reported in Fig. 2F (see Supplementary Information Part 6 for calculation details). Similarly to Dasgupta et al. (2013), both end-members are dry.

In these conditions, the  $a_{SiO_2(1)} - X_{SiO_2(1)}$  relationship predicted by our model presents a slope inversion as discussed above, so the evolution of melt composition is bounded by two limit cases between which immiscibility may occur. In the first case, the melt is carbonatitic between 300 and 110 km depth, with a nearly constant silica content of 3-5 wt.%. At about 110 km, the melt abruptly shifts from about 5 to 25-30 wt.% SiO<sub>2</sub> and progressively evolves

to basanite type (~45 wt.%  $SiO_2$ ) at shallow depths. In the second case, the evolution is similar, but the sharp transition occurs at a shallower depth of ~75 km. The uncertainty on the transition and immiscibility between carbonate and silicate melt is therefore limited to a 40 km range, between ~110 and 75 km depth.

This abrupt transition is evidently different from the gradual transition yielded by ideal mixing, but also from that predicted by the model of Dasgupta et al. (2013) (Fig. 5A). While the silica contents of the melt calculated from our model are similar to those of Dasgupta et al. (2013) down to ~110 km depth, the model of Dasgupta et al. (2013) predicts a gradual decrease of the melt SiO<sub>2</sub> content at greater depth, being ~25 and ~10 wt.% at 150 and 250 km depth, respectively. However, the model of Dasgupta et al. (2013) is extrapolated for pressures above 5 GPa (~150 km). This extrapolation likely does not consider the decrease in Ca/Mg of carbonate melts with increasing pressure (Fig. 2F). The conversion of their model in term of  $a_{SiO_2(1)} - X_{SiO_2(1)}$  relationship is fairly well reproduced by our model in their experimental range of calibration when using their compositions (Fig. 4C for  $X_{SiO_2(1)} > 0.2$ ). However their extrapolation at lower SiO<sub>2</sub> content significantly deviates from our calculation (even though performed with a constant Ca/Mg ratio), and lies at the margin of the experimental database (Fig. 4C). Actually, even when using the composition of Dasgupta et al. (2007, 2013) and setting it constant with depth, our model still predicts an abrupt change to carbonate melts with <~ 5 wt. % SiO<sub>2</sub> at ~150 km depth.

We calculated the evolution of incipient melt along a ridge adiabat in presence of water (Fig. 5A; same pressure-temperature conditions as dry curve), with varying H<sub>2</sub>O/CO<sub>2</sub> ratio in the carbonate component: 0.1 (1.92 wt.% H<sub>2</sub>O in the incipient carbonate melt at solidus, melt fraction F = 0), 0.2 (3.77 wt.% H<sub>2</sub>O) and 0.5 (8.93 wt.% H<sub>2</sub>O). For instance, if a partition coefficient of 0.006 is considered (average partition coefficient in the pressure range from 2 to 10 GPa; Hirschmann et al., 2009), the corresponding water bulk content is 115 ppm, 226 ppm and 536 ppm, respectively. As mentioned earlier, the melt becomes more ideal in presence of water (e.g. Fig. 4A), therefore the transition from silicate melt to carbonate melt is less abrupt with increasing bulk water content and the potential immiscibility area is narrower than in the dry case. The immiscibility ranges from 20 km between 110 and 90 km depth for H<sub>2</sub>O/CO<sub>2</sub> = 0.2, and disappears for H<sub>2</sub>O/CO<sub>2</sub> = 0.5. Considering different adiabatic P-T profiles also changes the depth of the transition, with carbonatitic melts being likely stable at >~60 km depth for Tp = 1250°C and >~130 km depth km for Tp = 1450°C (Fig. 5B). Thus higher temperatures tend to shift the melt composition toward higher silica contents.

The melting of CO<sub>2</sub>-bearing peridotite is not only defined by the pressure and temperature conditions, but it also depends on the speciation of carbon in depth. The oxidation state of the mantle combined with the equilibrium EMOD (MgSiO<sub>3</sub> + MgCO<sub>3</sub> = Mg<sub>2</sub>SiO<sub>4</sub> + C + CO<sub>2</sub>), defines the onset of incipient melting by "redox melting" between 120 and 150 km depth (Stagno et al., 2013). Therefore, incipient melting should not occur at depth exceeding 150 km, though Rohrbach and Schmidt (2011) defined a greater depth for the redox melting (250 km). In both cases, we calculate that the first liquids produced by redox melting are

carbonatitic ( $<\sim 10 \text{ wt.\% SiO}_2$ ) conversely to Dasgupta et al. (2013) who claimed that melt at such depth must be much silica richer ( $>25 \text{ wt.\% SiO}_2$ ).

### 3.3. Evolution of the melt along a cratonic geotherm

Russell et al. (2012) proposed that the assimilation of orthopyroxene in the cratonic mantle lithosphere is an efficient mechanism to exsolve a volatile-rich fluid phase by enriching in silica any rising carbonatitic melts: orthopyroxene assimilation at lithospheric depth is then suggested to provide sufficient buoyancy for rapid ascent of kimberlites. Russell et al. (2012) suggests that this assimilation drives the melt towards more silicic composition during the ascent (Fig. 5C), with an evolution for the SiO<sub>2</sub> content from 5 to 20 wt.% between 120 and 60 km depth.

We calculated the evolution of melt composition along a cratonic geotherm (modified from Lee et al., 2011; see Fig. S7) in Fig. 5C, keeping all other parameters the other calculation settings identical to Fig. 5A. Our calculation yields a decrease of the silica content in the cratonic lithosphere, from ~2-6 (dry or hydrous respectively) to ~0 wt.% between 200 and 60 km depth, implying that carbonatite melt rising through the cratonic lithosphere cannot assimilate orthopyroxene since the opposite is expected from a thermodynamic point of view: orthopyroxene must crystallize. Even though our model is here applied outside the temperature range of calibration, it predicts that melts remain carbonatitic at any depth below cratons. Our conclusions conflict with the hypothesis of Russell et al. (2012) for cratons. However, we recognize that, more silicic melts could be produced with a hotter geotherm and this could match Russell's model. The temperature range required to stabilize orthopyroxene-undersaturated melts nevertheless needs an investigation using our model in the pressure-temperature space, which is beyond the scope of our study.

### 4. Conclusion

We developed a model calculating the silica activity of the CO<sub>2</sub>-H<sub>2</sub>O-bearing melts typically produced by partial melting of the H<sub>2</sub>O-bearing carbonated mantle. It is calibrated and reproduces a large experimental database (491 melts), covering an important chemical diversity and large pressure-temperature ranges (1-10 GPa, 1100-1700°C). Our model is therefore applicable to most of upper mantle conditions without extrapolation. The water content and the Ca/Mg ratio (correlated to pressure) are found to be among the most influent parameters on the  $a_{SiO_2(l)} - X_{SiO_2(l)}$  relationships in carbonate melts.

Our model can be used to characterize the change of the melt composition along ridge adiabatic pressure-temperature paths. In contrast to the gradual transition predicted by ideal mixing and the model of Dasgupta et al. (2013), we show that carbonatitic melts with a maximum SiO<sub>2</sub> content of ~10 wt.% can be stabilized at the onset of incipient melting by "redox melting" at depth of 150 km. Furthermore, the liquid is predicted to change abruptly from a carbonatitic to a carbonated silicate melt (SiO<sub>2</sub> content ~ 25 wt.%) above ~110-75 km depth respectively, with potential immiscibility between a carbonate-rich and a silicate-rich melt in this range. The extrapolation of our model to cratonic mantle lithosphere conditions

predicts the stabilization of carbonatitic melts, with no increase of the  $SiO_2$  content during the ascent conversely to the model of Russell et al. (2012).

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## Figures

### Table 1:

Study	Temperature (°C)	Pressure (Gpa)	System	Equilibrium	Number of experiments
Takahashi 1986	1325 - 1550	1 - 3	NFTCrMnCMAS	CL	2
Wasylenki et al. 2003	1270 - 1390	1	NKFTCrMnCMAS	CL	17
Schwab and Johnston 2001	1270 - 1390	1	NKFTCrMnCMAS	CL	20
Hirose and Kushiro 1993	1250 - 1500	1 - 3	NKFTCrMnCMAS	CL	26
Gaetani and Grove 1998	1185 - 1370	1.2 - 2	NKFTPCrMnCMAS-H <sub>2</sub> O	CL	19
Hirose and Kawamoto 1995	1100 - 1350	1	NKFTCrMnCMAS-H <sub>2</sub> O	CL	8
Tenner et al. 2009	1380	3	NKFTCrMnCMAS-H <sub>2</sub> O	CL	1
Moore and Wood 1998	1300 - 1600	3	CMS-CO <sub>2</sub>	CL	8
Dalton and Presnall 1998a	1405 - 1505	6	CMAS-CO <sub>2</sub>	CL	5
Dalton and Presnall 1998b	1245 - 1430	3 - 7	CMAS-CO <sub>2</sub>	CL	6
Gudfinnsson and Presnall 2005	1400 - 1800	3.2 - 8	CMAS-CO <sub>2</sub>	CL	22
Keshav et al. 2011	1525 - 1675	10 - 14	CMAS-CO <sub>2</sub>	CL	5
Keshav and Gudfinnsson 2013	1330 - 1390	1.1 - 1.7	CMAS-CO <sub>2</sub>	CL	3
Novella et al. 2014	1225 - 1560	2.1 - 3	CMAS-CO <sub>2</sub>	CL	19
Moore 2012	1200 - 1400	3	NCMAS-CO <sub>2</sub>	CL	13
Litasov and Ohtani 2009	1420 - 1600	10.5	NCMAS-CO <sub>2</sub>	CL	3
Stagno and Frost 2010	1100 - 1600	2.5 - 11	$FCMAS-CO_2(Ir)$	CL	23
Liu et al. 2006	1200-1317	1.1	NCMAS-CO <sub>2</sub> ,H <sub>2</sub> O	CL	37
Ryabchikov et al. 1989	1400 - 1450	5	NKFCMAS-CO <sub>2</sub>	CL	3
Ghosh et al. 2009	1550 - 1560	12.5 - 13.5	NKFTCrCMAS-CO <sub>2</sub>	CL	2
Ghosh et al. 2014	1600 - 1700	10 - 12.5	NKFTCrCMAS-CO <sub>2</sub>	CL	3
Dasgupta et al. 2007	1300 - 1600	3	NKFTCrMnCMAS-CO <sub>2</sub>	CL	19
Dasgupta and Hirschmann 2007a	1200 - 1260	6.6	NKFTCrMnCMAS-CO <sub>2</sub>	CL	29
Dasgupta and Hirschmann	1330 - 1360	6.6	NKFTCrMnCMAS-CO <sub>2</sub>	CL	2
			15		

Dasgupta et al. 2006 Brooker 1998	1225 - 1375 1250 - 1300	3 2.5	NKFTCrMnCMAS-CO2 NKFTPCrMnCMAS-CO2,F	LL LL	5 16
Martin et al. 2013	1160 - 1260	1 - 3.2	NKFTPCMAS-CO <sub>2</sub>	LL	12
Martin et al. 2012	1220	1.7	NKFTPCMAS-CO <sub>2</sub>	LL	7
Massuyeau et al. (this study)	1300 - 1400	3	NKFCMAS-CO2	LL	8
Brooker and Hamilton 1990	1225	1.5	NKCMAS-CO2	LL	7
Lee and Wyllie 1996	1350 - 1450	2.5	NCMAS-CO2	LL	7
Brooker and Kjarsgaard 2011	1275 - 1700	1 - 2.5	NCAS-CO <sub>2</sub>	LL	29
Brey et al. 2009	1300 - 1600	6 - 10	NKFTPCrMnCMAS-CO <sub>2</sub> ,H <sub>2</sub> O (Ni)	CL	6
Girnis et al. 2011	1400 - 1800	6 - 10	NKFTPCrCMAS-CO <sub>2</sub> ,H <sub>2</sub> O (Ni)	CL	11
Thibault et al. 1992	1100	3	NKFTMnCMAS-CO <sub>2</sub> ,H <sub>2</sub> O	CL	1
Foley et al. 2009	1090 - 1290	4 - 6	NKFTCrCMAS-CO <sub>2</sub> ,H <sub>2</sub> O	CL	12
Brey et al. 2011	1200 - 1700	6 - 10	NKFTPCrMnCMAS-CO2 (Ni)	CL	15
Brey et al. 2008	1300 - 1700	6 - 10	NKFTPCrMnCMAS-CO2 (Ni)	CL	22
Tenner et al. 2012	1200-1450	3.5	NKFTCrMnCMAS-CO <sub>2</sub> ,H <sub>2</sub> O	CL	16
Mallik and Dasgupta 2014	1375	3	NKFTCrMnCMAS-CO <sub>2</sub>	CL	8
Mallik and Dasgupta 2013	1375	3	NKFTCrMnCMAS-CO2	CL	6
Rohrbach and Schmidt 2011	1575	10	NKFTCrCMAS-CO2 (Ni)	CL	1
Dasgupta et al. 2013	1300 - 1750	2 - 5	NKFTCrMnCMAS-CO <sub>2</sub>	CL	7

Experimental database used in this study. The experiments labelled in italics referred to the systems considered as 'quasi-natural' in the text.

A: Al<sub>2</sub>O<sub>3</sub>, C: CaO, Cr: Cr<sub>2</sub>O<sub>3</sub>, F: Feo, Ir: IrO<sub>2</sub>, K: K<sub>2</sub>O, M: MgO, Mn: MnO, N: Na<sub>2</sub>O, Ni: NiO, P: P<sub>2</sub>O<sub>5</sub>, S: SiO<sub>2</sub>, T: TiO<sub>2</sub>

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Table 2:
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Parameter	Calc. Value (J.mol	<sup>1</sup> )
W <sup>a</sup> SiO <sub>2</sub> -CO <sub>2</sub>	-222792±13193	
W <sup>b</sup> SiO <sub>2</sub> -CO <sub>2</sub>	20238±7901	
$WAl_2O_3$ -Si $O_2$	-86189±24503	
WCaO-SiO <sub>2</sub>	83743±5065	
WNa <sub>2</sub> O-SiO <sub>2</sub>	-85227±33274	
WK <sub>2</sub> O-SiO <sub>2</sub>	-85967±41414	
$WAl_2O_3\text{-}CO_2$	-791128±91536	
WFeO-CO <sub>2</sub>	-428390±48413	
WMgO-CO <sub>2</sub>	-91257±10254	
WNa <sub>2</sub> O-CO <sub>2</sub>	-266442±48438	
$WK_2O-CO_2$	-277798±84106	
$W_{H_2O-CO_2}$	-38029±15844	
WAl <sub>2</sub> O <sub>3</sub> -FeO	-990442±158670	
WAl <sub>2</sub> O <sub>3</sub> -MgO	174780±62096	
WFeO-CaO	722813±106230	
WCaO-Na <sub>2</sub> O	-168280±41555	~

Optimized Margules parameters for the calculation of the silica activity coefficient ( $\gamma_{SiO_2(l)}$ ) (Eq. 26), and associated uncertainties (1 $\sigma$ ).

### Figure 1:

P-T conditions of the experimental database used in this study, with solidus temperatures for different bulk compositions. The experimental data points correspond to 1) liquid-olivineorthopyroxene equilibrium, and 2) immiscible carbonate-rich and silicate-rich liquids equilibrium. Solidus temperatures are from Wallace and Green (1988; "W.&G.1988"), Dalton and Presnall (1998a; "D.&P.1998"), Hirschmann (2000; "H.2000"), Brey et al. (2009; "B.2009"), Foley et al. (2009; "F.2009"), Brey et al. (2011; "B.2011"), Dasgupta (2013; "D.2013"), Keshav et al. (2011; "K.2011"), Keshav and Gudfinnsson (2013; "K.&G.2013"). The CMS-CO<sub>2</sub> solidus is calculated from the combination of the solidus temperatures of Dalton and Presnall (1998a), from 0 to 7 GPa, and Keshav et al. (2011) at higher pressures. The CMAS-CO<sub>2</sub> solidus is calculated from the combination of the solidus temperatures of Keshav and Gudfinnsson (2013), from 0 to 6.5 GPa, and Keshav et al. (2011) at higher pressures.

### Figure 2:

(A-E, G) Silica activity as a function of silica content in experimental partial melts coexisting with olivine and orthopyroxene. (A) and (B) represent the experimental data in dry systems only, as a function of pressure and temperature respectively. (C) Comparison between nominally dry and hydrated experimental melts (all the experimental data are represented

here). (D) Comparison between simple (CMS and CMAS) and dry quasi-natural systems. (E,G) Experimental data in dry systems sorted as a function of different oxide molar ratios: Ca/Mg(E) and (Na + K)/Mg(G).

(F) Evolution of the Ca/Mg molar ratio as a function of the pressure for the experimental melts coexisting with olivine and orthopyroxene. The black solid line represent the fit of the data with < 20 wt.% SiO<sub>2</sub> (Ca/Mg =  $5 * (e^{(-1.5*P)})^{0.3} + 0.4$ ).

(H) Activity ratios between carbonate-rich (CL) and silicate-rich (SL) liquids measured in immiscibility experiments  $(RT \ln(\gamma_{SiO_2(l)}^{CL}/\gamma_{SiO_2(l)}^{SL})) = RT \ln(X_{SiO_2(l)}^{SL}/X_{SiO_2(l)}^{CL}))$  as a function of silica content, and sorted for different (Na + K)/Mg ratio in the silicate liquid. The grey dashed line separates carbonate liquids from silicate liquids.

### Figure 3:

(A) Comparison of the SiO<sub>2</sub> melt molar fraction calculated with our model to that measured in experimental melts coexisting with olivine and orthopyroxene. (B) Comparison of  $\text{RT}\ln(\gamma_{SiO_2}^{\text{CL}}/\gamma_{SiO_2}^{\text{SL}})$  calculated with our model to that measured in immiscibility experiments (i.e.,  $\text{RT}\ln(X_{SiO_2}^{\text{SL}}/X_{SiO_2}^{\text{CL}})$ ). The uncertainties on  $X_{SiO_2(1)}$  and  $\text{RT}\ln(X_{SiO_2}^{\text{CL}}/X_{SiO_2}^{\text{SL}})$  are reported as given from the experimental studies or, when unspecified, approximated by typical errors (see Supplementary Information Part 4b).

### Figure 4:

Predicted evolution of silica activity as a function of  $X_{SiO_2(1)}$  according to our model for various melt chemical compositions between carbonate end-members and silicate end-members. The molar composition of the carbonate is mentioned in the legend (see Table S5 and Supplementary Information Part 6 for composition and calculation details). (A) Evolution of the silica activity as a function of Ca/Mg ratio and water content in the carbonate melt at 1400°C (except for the light blue curve at 1600°C). The silicate end-member is a basaltic component, except for the pink dashed curve, representing the silica activity as a function of the silica activity as a function of the silica to the silica activity as a function of the silicate end-member is a basaltic component (see Table S5). (B) Evolution of the silica activity as a function of the silicate end-member is a basaltic component (see Table S5). (C) Evolution of the silica activity as predicted by the model of Dasgupta et al. (2013) compared to that of our model using identical carbonate and silicate end-members (see Table S5).

### Figure 5 :

Evolution of melt silica content in (A-B) oceanic and (C) cratonic settings according to our model (see Table S5 and Supplementary Information Part 6 for composition and calculation details). (A) Melt evolution of dry (brown curve) and hydrous ( $H_2O/CO_2 = 0.1$ , 0.2 and 0.5; blue curves) systems along a ridge adiabat with potential temperature Tp = 1350°C, compared to ideal mixing (grey dashed curve) and the model of Dasgupta et al. (2013) (purple curve,

dashed for extrapolation). The shaded regions for dry (light brown) and hydrous (blue) systems represent the regions where melt composition cannot be unequivocally predicted and where immiscibility may occur. Example of uncertainties on predicted silica content is reported as light green shaded area for the dry system (see Supplementary Information Part 4c). (B) Melt evolution of hydrous system ( $H_2O/CO_2 = 0.2$ ) for different potential temperatures (1250°C, 1350°C and 1450°C). (C) Melt evolution of dry (brown curve) and hydrous (blue curves) systems along a cratonic geotherm (Fig. S7), compared to the model of Russell et al. (2012) (purple curve).

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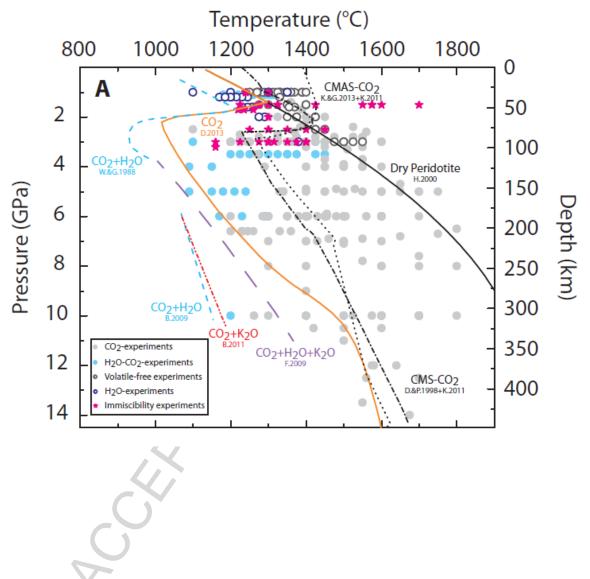
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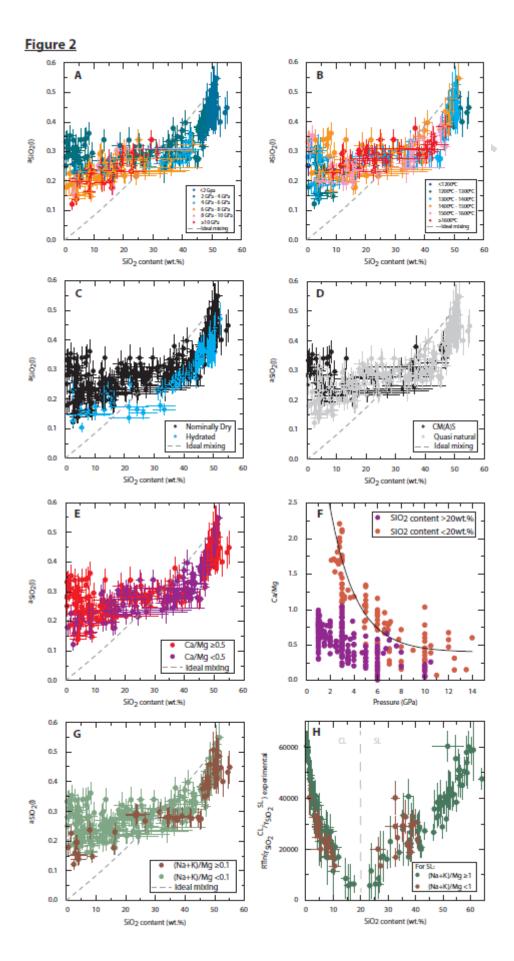
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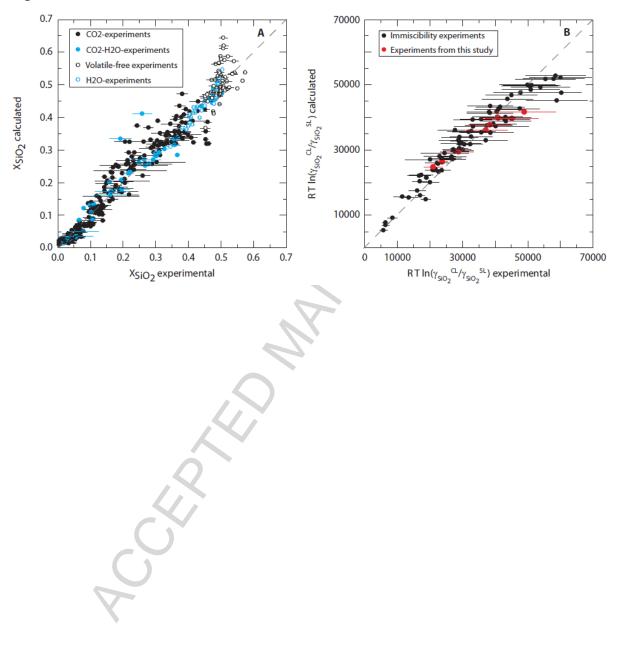


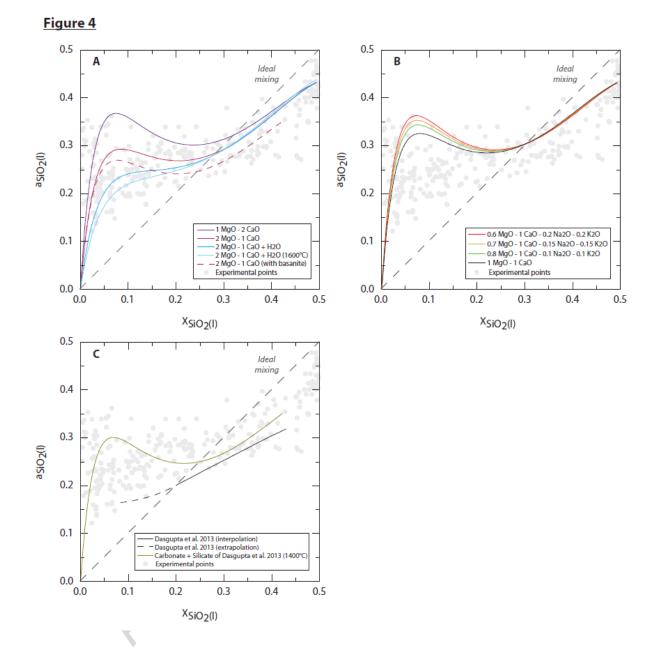


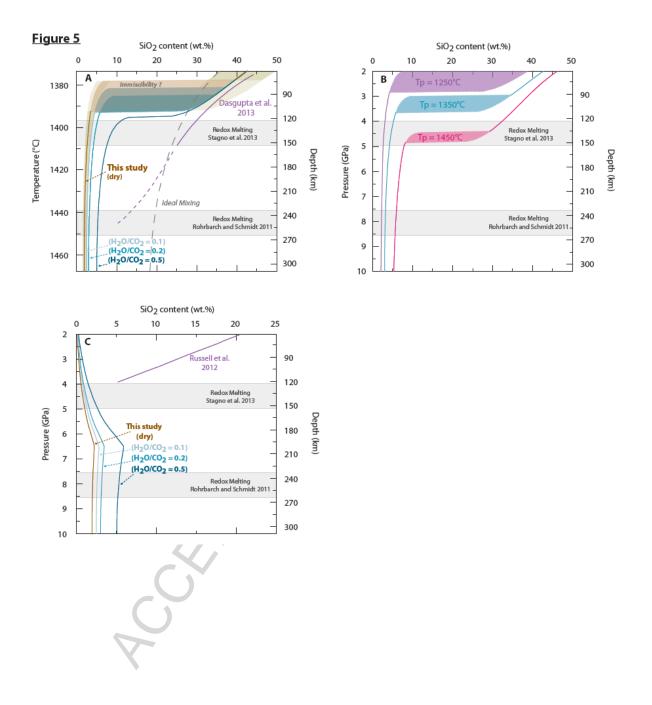


### Transition Carbonate-silicate mantle melt model Massuyeau et al. 2015

Figure 3







### Highlights

- We use the thermodynamic modelling of the silica activity in melts in CO<sub>2</sub>-bearing peridotite.
- We define thermodynamic mixing properties between molten carbonate (carbonatite) and molten silicate (basalt).
- A generalized Margules function is adjusted, principally describing the non-ideal interaction for SiO<sub>2</sub>-CO<sub>2</sub>.
- We can characterize the change of the melt composition along ridge adiabatic pressuretemperature paths.
- Carbonatitic liquids stabilized at the onset of incipient melting by "redox melting" (~150 km).

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