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# Changes in viscoelastic vibrational properties between

# compression and normal wood: roles of microfibril angle and of lignin

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## Abstract

This study aims at better understanding the respective influences of specific gravity  $(\gamma)$ , microfibril angle (MFA), and cell-wall matrix polymers on viscoelastic vibrational properties of wood in axial direction. The wide variations of properties between normal wood (NW) and compression wood (CW) are in focus. Three young bent trees (Picea abies, Pinus sylvestris and Pinus pinaster) that recovered verticality were sampled. Several observed differences between NW and CW were highly significant in terms of anatomical, physical (y, shrinkage, CIELab colorimetry), mechanical (compressive strength), and vibrational properties. Specific dynamic modulus of elasticity  $(E'/\gamma)$  decreases with increasing MFA, and Young's modulus (E') can be satisfactorily explained by  $\gamma$ and MFA. Apparently, the type of the cell wall polymer matrix is not influential in this regard. The damping coefficient  $(\tan \delta)$  does not depend solely on MFA of NW and CW. The tan $\delta - E'/\gamma$ relationship evidences that, at equivalent  $E'/\gamma$ , the  $\tan \delta$  of CW is approx. 34% lower than that of NW. This observation is ascribed to the more condensed nature of CW lignins, and this is discussed in the context of previous findings in other hygrothermal and time/frequency domains. It is proposed that the lignin structure and the amount and type of extractives, which are both different in various

species, are partly responsible for taxonomy-related damping characteristics.

**Keywords:** Compression wood; Damping coefficient; FT-IR; Lignin; Internal friction; Microfibril angle (MFA); Picea abies; Pinus pinaster; Pinus sylvestris; Specific dynamic modulus of elasticity; Viscoelastic vibrational properties.

### Introduction

Wood is a cellular and composite material. Its macroscopic properties depend on porosity and on the orientation of reinforcing elements. The viscoelastic behaviour of wood is due to its composite polymeric nature consisting of crystalline cellulosic microfibrils (MFs) embedded in a more or less amorphous matrix (Salmén and Burgert 2009; Stevanic and Salmén 2009). Specific gravity ( $\gamma$ ), which is inversely proportional to porosity, determines the axial Young's modulus (E) to a large extent, i.e. it explains approx. 65% of variability in E over several hundred species with  $\gamma$  ranging from 0.1 to 1.4 (Brémaud et al. 2009; unpublished database at CIRAD). The residual variability mainly expresses variations at the cell wall level. Axial vibrational properties of wood (specific modulus of elasticity –  $E/\gamma$  and damping coefficient – tan $\delta$ ) are theoretically independent of specific gravity and shall be proportional to cell wall properties. Microfibril angle (MFA) is the main parameter influencing  $E/\gamma$  in the wide range of observed MFA values. Various models have been developed to describe this dependency (Norimoto et al. 1986; Koponen et al. 1989; Astley et al. 1998; Yamamoto and Kojima 2002; Bergander and Salmén 2002; Xu and Liu 2004). Although models differ in their formulation, the relationship between  $E/\gamma$  and the MFA  $\varphi$  has a more or less sigmoid shape, which can be approximated by:

 $E/\gamma = 1/(a \times \cos^4 \phi + b \times \cos^2 \phi \sin^2 \phi + c \times \sin^4 \phi)$ (1)

Viscoelastic damping of vibration (tan $\delta$ ) in the audio-frequency domain ( $\approx 0.1-10$  kHz) is also known to be strongly dependent on MFA (Norimoto et al. 1986; Obataya et al. 2000). However, much fewer micromechanical models were developed due to lack of experimental data on viscoelasticity of wood constituents in this frequency range. The fact that both E'/ $\gamma$  and tan $\delta$  depend on MFA, is translated in a relationship between these two properties with a shape close to a power law. The empirical curve obtained by Ono and Norimoto (1983) can be used as a standard reference, to which new experimental results can be compared:

$$\tan \delta_s = 10^{-A} \times (E \, \gamma)^{-B} \tag{2}$$

Where coefficients A and B are 1.23 and 0.68 from more than 1200 specimens belonging to 25 softwood species (Ono and Norimoto 1983). It has also been proved that chemical composition of extractives, which are acting as "natural chemical modifiers", leads to some shifts of the tan $\delta$  – E'/ycurve, either upwards or downwards (Obataya et al. 2000; Brémaud et al. 2010ab, 2011a, 2012). The influence of extractives explain the differences in tan $\delta$  that are observed between sapwood and heartwood in the same tree (Yano 1994; Brémaud 2006; Brémaud et al. 2011a, 2012), which have essentially the same chemical composition of the cell wall matrix in terms of hemicelluloses and lignin.

In conifers, compression wood (CW) is known to be strongly different from normal wood (NW) in terms of specific gravity, MFA, polymeric composition, while the and extractives are quite similar (Timell 1982; Yeh et al. 2006; Diaz-vaz et al. 2009). Juvenile wood (JW) of conifers is also quite different from mature NW in terms of specific gravity and MFA. However the difference in chemical composition between JW and mature wood is not as much as that between CW and NW (Yeh et al. 2005, 2006; Nanayakkara 2007). The chemical composition of opposite wood (OW) has high similarity to NW in the same log (Timell 1973, 1982; Yeh et al. 2006; Nanavakkara 2007). In summary, CW contains less cellulose (ca. 10%) and less crystalline moiety. Accordingly, the moiety of the amorphous matrix is 10% higher, mainly due

to increased lignin content (Timell 1982). Changes in hemicelluloses of CW are mostly of qualitative nature; for example, the galactoglucomannans are partly substituted by galactans. Increased lignification of the secondary cell wall (S2) is the first symptom of CW formation (Donaldson et al. 2004). In CW lignin, the content in p-hydroxyphenyl (H) units is significantly higher (up to 30%), which are present only in traces in NW lignins (Timell 1982; Yeh et al. 2005, 2006; Nanayakkara et al. 2009). The peculiarities of CW were also demonstrated by gene expression studies during wood formation (Yamashita et al. 2009). In general, CW attracted a lot of attention also in the last decade concerning lignin deposition in the S2 layer (Yoshizawa et al. 1999), air permeability (Tarmian and Perré 2009), lignin structure (Önnerund 2003), shear strength (Gindl and Teischinger 2003), morphological and chemical variations (Yeh et al. 2006). galactans characterisation of bv immunofluorescece (Altaner et al. 2007), relation of MFA and lignin content (Jungnikl et al. 2008), and ultrastructure (Hänninen et al. 2012), just to mention a few. Thus CW is well known and the pair CW/NW is well suited for the investigation of the combined influence of specific gravity, MFA, and chemistry of the cell wall polymers on mechanical properties of wood.

Considerable research has been conducted on physical or elastic mechanical properties of CW, but its dynamic viscoelastic behaviour was seldom addressed. Matsumoto (1961) and Norimoto et al. (1984) studied the dynamic properties of air-dry CW in the acoustic range around 0.1-10 kHz. However, the CW sampling in the quoted papers was limited and the data were not related to microstructural or physico-chemical parameters.

The present study is dedicated to the vibrational properties of CW and attempts to find correlations to other parameters. The focus is on the respective influences of microstructure and of matrix composition on viscoelastic vibrational properties of wood. The hypothesis was that clear results would be obtained as in CW several parameters are clearly different from those of NW.

# Material and methods

#### Plant material and sampling of test specimens.

Three young trees - Norway spruce (Picea abies [L.] Karst.), maritime pine (Pinus pinaster Aiton.) and Scots pine (Pinus sylvestris L.) - (21, 9 and 13 annual rings at DBH) were sampled with DBH (diameter at breast height) ranging from 20 to 25 cm. The trees were grown in the region of Bordeaux, France. They had been strongly inclined because of a strong storm that occurred 10 years ago, and then recovered verticality on their upper part. In situ measurements of maturation strains proved that the lower part of their trunk was in high compressive stress state (Alméras et al. 2005). The expectation, that this section should contain CW, was fulfilled: after cutting a small log (50 cm long) just below the growth strain measurement level, the occurrence of CW was verified by visual observation (Figure 1a). Anatomical observations on safranin stained thin slides (Figure 1b) confirmed the pure CW character of zones appearing as dark-red macroscopically, while other pale zones are for NW. From these small logs, longitudinal rods (20×20×360 mm<sup>3</sup>; R×T×L) were cut and air-dried (down to equilibrium at 20°C and 65% RH) to perform standard physical and mechanical measurements. Some of these rods were selected as representative of CW (16) and NW (14), respectively (Figure 1a). 30 shorter rods  $(20\times20\times150 \text{ mm}^3; \text{R}\times\text{T}\times\text{L})$  were taken from the long ones and cut into 2 smaller strips per rod (12×2×150 mm ; R×T×L). These radial strips systematically included both earlywood and latewood (Figure 2).

#### Microfibril angle, colour and FT-IR spectroscopy

**Mean MFA** was measured for each rod by the iodine crystals procedure (Senft and Bendtsen 1985). 15  $\mu$ m thick radial sections were cut and stored in 50% ethanol solution. Sections were dehydrated in absolute ethanol for 5 min twice, and then immersed in a 2% solution of iodine-potassium iodide for 5 s. Finally, the sections were placed on a slide before adding one or two drops of 60% nitric acid on it. Observations were performed on 3 pictures of 112 × 84  $\mu$ m<sup>2</sup> per specimen at a 500× magnification. Each picture contained approx. 10 tracheids and the measurement was done on approx. 80 MFs per specimen (Figure 1c). Standard deviation of MFA measurements within a specimen was of 4.2±0.6°, irrespective of species or wood type.

**Colorimetric parameters** were measured on the RL surfaces of the 2 mm thick strips (Datacolor Microflash 200d with a sensor aperture diameter of 8.7 mm) using CIE standard observer 10° (colour matching function for 10° angle of vision) and illuminant A (corresponding to incandescent light). Measurements were conducted within a few days after cutting of the specimens, with 3 repetitions per specimen. Data were collected in the CIE*Lab* system, where  $L^*$  is lightness (0 = black, 100 = white),  $a^*$  is the green (-) to red (+) axis and  $b^*$  is the blue (-) to yellow (+) axis.

**FT-IR spectra** were acquired in ATR (attenuated total reflectance) mode on the smooth radial surfaces of wood strips under air-dry conditions. A torque clamp insured uniform pressure on all specimens. Spectra were recorded with a Nicolet 6700 spectrometer, between 4000 and 600 cm<sup>-1</sup>, at a resolution of 4 cm<sup>-1</sup>. Each measure is

the average of 64 specimen scans, with "blanks" consisting of 64 background scans each time. Spectra were simply baseline-corrected in the 3750-2750 cm<sup>-1</sup> and 1800-780 cm<sup>-1</sup> (fingerprint) regions, and averaged (first between specimens of a given wood type and species, then for CW and NW over the 3 species), with the software "Omnic 8.1" (Thermo Fischer Scientific). Differences were studied on the basis of bands potentially relevant for comparison of CW and NW (Faix 1991; Gindl 2002; Schwanninger et al. 2004; Altaner et al. 2009).

#### Standard physical and mechanical measurements.

Routine methods of CIRAD for standard measurements of mechanical and physical properties were applied (Ruelle et al. 2007). Mechanical properties and air-dry specific gravity ( $\gamma$ , calculated from mass and volume of specimens) were determined in equilibrium state at 20 ± 1°C and 65 ± 2% RH (moisture content, MC, was in the range of 11 to 12%).

**Longitudinal dynamic modulus of elasticity** (*E'*) was measured on air-dry wood by natural vibrations (Bordonné 1989) on the long rods  $(360 \times 20 \times 20 \text{ mm}^3)$ . In this method, *E'* is determined through Timoshenko theory, i.e. the shear and rotary inertia is taken into account (Brancheriau et al. 2002). Tests also provide an evaluation of the anisotropy between axial *E'* and inplane shear modulus (*E'/G'*<sub>LT</sub>).

Crushing strength in compression parallel to the grain was measured (ISO standard 3132:1975) on specimens ( $20 \times 20 \times 60 \text{ mm}^3$ ;  $R \times T \times L$ ) taken from rods used for *E*' measurement (Figure 2). Instrument: MTS 20/M universal testing machine equipped with a 10 kN load cell. Load was applied parallel to the grain at a rate of 0.6 mm min<sup>-1</sup>.

Shrinkages in L, R, and T direction were calculated based on the ratio of the dimensional variation in each direction between saturated and anhydrous states. Fibre saturation point (*FSP*) was assessed by the intersection point of volumetric shrinkage. Initial dimensions of specimens, also taken from rods used for *E*' measurements, were  $20 \times 20 \times 50$  mm<sup>3</sup> (R, T, L) for L shrinkage and *FSP*, and  $20 \times 20 \times 10$  mm<sup>3</sup> (R, T, L) for R and T shrinkage.

#### Measurement of vibrational properties on strips.

All tests were performed after at least 3 weeks of stabilization under controlled conditions at  $20 \pm 1^{\circ}C$  and  $65 \pm 2\%$  RH. There were no significant differences in MC between CW and NW. Measurements were made by non-contact forced-released flexural vibrations of freefree bars, on the thin strips  $(12 \times 2 \times 150 \text{ mm}^3; \text{R} \times \text{T} \times \text{L})$ . Specimens were made to vibrate through an electromagnet facing a thin iron plate (0.02 g) glued on one end of the strip, and their displacement at a belly of vibration was measured by a laser triangulation sensor. Vibration emission and detection were computer-driven by means of a specific development in Labview® Software (Brémaud 2006; Brémaud et al. 2012). Specific dynamic modulus of elasticity  $(E'/\gamma)$  was deduced from the first resonant frequency according to the Euler-Bernouilli equation. Damping coefficient  $tan\delta$  was measured both by the 'quality factor' (bandwidth at half power in the frequency domain) and by the logarithmic decrement of amplitude after stopping the excitation (in the time domain). Frequencies were in the range of 200-400 Hz. Three repetitions were made for each specimen, and the mean error was  $\leq 5\%$ .



Figure 1 Macroscopic and microscopic description of investigated wood material.

a) Localisation of sampled rods inside the studied trees (*Picea abies, Pinus sylvestris* and *Pinus pinaster*). Circles: compression wood (CW); triangles: normal wood (NW). CW sector is always positioned on the left part of the pictures. Scale bars: 5 cm. b) Microscopic observations of anatomy in transverse plane of CW and NW. Staining with safranin. × 500. Scale bars: 25  $\mu$ m. c) Example of measurement of MFA on *P. abies* tracheids of normal wood (left, MFA=22.6°) and compression wood (right, mean MFA=32.4°). × 500. scale bars: 25  $\mu$ m.



"Rods" for natural vibration tests

Figure 2 Cutting plan of specimens for the different physical and mechanical tests.

#### Results and discussion

#### Differences between CW and NW in general

The mean values of structural, physical and mechanical properties measured on rods are presented in Table 1. The results are in agreement with those of the literature (e.g. Timell 1986). CW has a higher MFA, specific gravity, L shrinkage and compression strength, but lower FSP, R and T shrinkage and axial Young's and specific modulus. Axial-to-shear anisotropy  $(E'/G'_{LT})$  is also lower in CW with the same amplitude of differences as observed for  $E'/\gamma$ . However, due to the high slenderness of the strips (length/height ratio of 75),  $E'/\gamma$  measured on rods (by Timoshenko theory) or on strips (by Bernouilli theory) were identical both for NW and CW (Figure 3a) independently of their different values of  $E'/G'_{LT}$ . The fact that determinations of  $\gamma$ , E' and E'/ $\gamma$  were equivalent in tests both on rods and on strips allows further comparison of properties determined on the two sizes of specimens.

The mean measured values on strips are presented in Table 2. The lower  $E'/\gamma$  of CW is associated with higher tan $\delta$ . CW is darker and mostly more coloured with a higher contribution of redness a\* (Figure 3b), which, when low amounts of extractives are present, is usually ascribed to more lignified, thicker cell-walls, as cellulose and hemicelluloses do not absorb visible light (Hon and Shiraishi 2001). The higher amplitudes of FT-IR bands at  $\approx 1600$  cm<sup>-1</sup> and at  $\approx 1510$ cm<sup>-1</sup>, related to aromatic ring skeletal vibrations (Faix 1991; Schwanninger et al. 2004; Altaner et al. 2009), confirmed higher lignin content of CW compared to NW in the samples under study (Figure 4).



Figure 3 Comparison of specific modulus of elasticity and colour between compression wood (CW, filled symbols) and normal wood (NW, open symbols).

a) Plot of  $E'\gamma$  on rods (determined through Timoshenko theory) vs. that on small strips (determined through Bernouilli theory) cut from the same rods. b) Plot of yellowness (b\*) vs. redness (a\*) measured on strips.

Table 1 Comparison between compression wood (CW) and normal wood (NW) in terms of average values of structural, physical and mechanical properties measured on air-dry rods

r,												
		d pith	MFA	γ	$E'_{\rm L}$	$E'_{\rm L}/\gamma$	$E'/G'_{LT}$	Comp.	FSP	R shr.	T shr.	L shr.
Rods		(cm)	(°)		(GPa)	(GPa)		(MPa)	(%)	(%)	(%)	(%)
CW ( <i>n</i> =16)	mean	10.1	36.8	0.66	4.7	6.9	4.3	37.1	26.9	2.3	4.2	2.7
	s.d.	3.5	5.5	0.08	1.8	2.1	1.1	9.2	1.5	0.4	1.6	1.3
NW ( <i>n</i> =14)	mean	6.9	22.4	0.47	8.1	16.8	10.4	27.4	30.0	4.1	8.2	0.2
	s.d.	2.6	5.2	0.06	2.5	3.3	3.0	7.6	1.6	0.4	1.5	0.1
CW/NW	mean	1.47	1.64	1.40	0.57	0.41	0.41	1.4	0.9	0.5	0.5	13.8

(*d* pith): distance to the pith; (MFA) mean microfibril angle; ( $\gamma$ ) specific gravity; (R, T, L shr.) radial, tangential and longitudinal shrinkages from green to oven-dry; (FSP) fibre saturation point; (E' and  $E'/\gamma$ ) dynamic Young's and specific modulus by Timoshenko theory; ( $E'/G'_{LT}$ ) axial modulus/in-plane shear anisotropic ratio; (Comp.) crushing strength in compression parallel to the grain.

Table 2 Comparison between compression wood (CW) and normal wood (NW) in terms of average values of physical, vibrational and colorimetric properties measured on air-dry strips

r-jr-											
		γ	Ė <sub>L</sub>	$\dot{E_L}/\gamma$	$\tan \delta_{\rm L}$	L*	a*	b*	C*	h*	
Strips			(GPa)	(GPa)	$(10^{-3})$					(°)	
CW(n-22)	mean	0.66	4.8	7.1	14.2	80.4	12.9	29.0	31.8	66.0	
C W (n=32)	s.d.	0.06	1.8	2.1	2.4	1.0	0.8	1.5	1.7	0.5	
NW $(n-28)$	mean	0.48	8.3	17.1	10.5	87.5	8.2	22.2	23.7	69.7	
1000 (n-20)	s.d.	0.07	2.5	3.4	1.6	1.2	0.7	1.3	1.4	1.1	
CW/NW	mean	1.39	0.58	0.41	1.36	0.92	1.57	1.31	1.34	0.95	

( $\gamma$ ) specific gravity; (E' and E'/ $\gamma$ ) dynamic Young's and specific modulus by Bernouilli theory; (L\*) lightness; (a\*) redness; (b\*) yellowness; (C\* =  $\sqrt{a^{*2} + b^{*2}}$ ) saturation/chromaticity; (h\* = arctan(b\*/a\*)) hue angle.



**Figure 4** Baseline corrected and normalized FT-IR spectra in the fingerprint region from 1800 to 750 cm<sup>-1</sup>. (a) Mean spectra of normal wood (thick lines) and compression wood (thin lines) averaged over the three wood species indicated in Figure 1. (b) Mean spectra of NW (c,d,e) and CW (f,g,h) for spruce (c,f), maritime pine (d,g) and Scots pine (e,h) averaged over the studied specimens.

Although there is a rather important variability in most properties within each wood type, CW or NW, the differences between CW and NW were all highly significant (shown by one-way ANOVA). The biggest amplitude of relative differences in physical-mechanical properties between CW and NW occurred for L shrinkage (as it was close to zero in NW). The next biggest amplitudes of differences are for MFA, specific modulus and elastic anisotropy, followed by redness and R and T shrinkages. The difference in damping coefficient is more moderate, nearly twice smaller than differences in  $E'/\gamma$ .

#### Relationships between $\gamma$ , E', E'/ $\gamma$ , and MFA

The relationship between E' and  $\gamma$  is shown in Figure 5a. There are strong differences between CW and NW and there is no simple way to predict E' from  $\gamma$ . On the contrary, the relationship between  $E'/\gamma$  and MFA (Figure 5b) is classical and its shape is very similar to that of previous results (e.g. Norimoto et al. 1986; Koponen 1989; Astley et al. 1998; Yamamoto and Kojima 2002; Bergander and Salmén 2002; Xu and Liu 2004). Empirical constants for the curve shape described by Eq. 1 were fitted to experimental data by optimization with the help of the solver in MS Excel; the best fitting gives the formula:

$$E' \gamma = \frac{1}{(0.03426 \times \cos^4 \phi + 0.2053 \times \cos^2 \phi \sin^2 \phi + 0.6797 \times \sin^4 \phi)}$$
(2)

If any, a residual difference between CW and NW that might be linked to variations in the cell

wall matrix is hardly noticeable (Figure 5b). Indeed, it was proposed based on micromechanical models that variations in the content of lignin and hemicelluloses play only a weak role in L elasticity, although some differences in cellulose structure might have a bigger effect (Bergander and Salmén 2002; Xu et al. 2011).



**Figure 5** Relationships between modulus of elasticity, specific gravity and microfibril angle.

a) E' vs.  $\gamma$  as measured on rods. b)  $E'/\gamma$  vs. MFA as measured on rods. c) Calculated E' data (taking into account  $\gamma$ , and MFA through Eq. 3) vs. experimental data of E'.

The statistical curve fitting in Eq. 3 is suited for estimating elastic modulus E' from  $\gamma$  and MFA values (Figure 5c), which explained 77% of the variability in E'. Both the calculated-experimental values relationship and the residual dispersion were equivalent for CW and NW. However, residual variability might also express the secondary influence of other factors, such as

differences in the proportion of crystalline cellulose MFs, which might differ depending on sample origin (Yamamoto and Kojima 2002), or anatomical parameters such as rounded cell

shapes or helical cavities (Timell 1983; Burgert et al. 2004). It may also simply reflect the variability in MFA within specimens (e.g. Sedighi-Gilani et al. 2005).



**Figure 6** Relationships between damping coefficient and microfibril angle or specific modulus of elasticity. a) Damping coefficient  $(\tan \delta)$  vs. MFA. b)  $\tan \delta$  vs.  $E'/\gamma$  measured on strips. c) Experimental values of  $\tan \delta$  vs. those of statistical model (Eq. 2) based only on  $E'/\gamma$ . d)  $\tan \delta$  calculated by statistical model (Eq. 5) based on  $E'/\gamma$  and chemistry-related indicator DS $\delta$ , vs. experimental  $\tan \delta$ .

#### Relationships between $\tan \delta$ , MFA and $E'/\gamma$

Damping coefficient  $tan\delta$  is related to MFA (Figure 6a) in a way quite similar to observations of Norimoto et al. (1986) on hinoki wood (Chamaecyparis obtusa). However, there is an important scattering in the tan $\delta$  - MFA relationship in the present results. Although the range of MFA considered here was larger ( $10^{\circ}$  to  $45^{\circ}$ ) than in previous data on hinoki wood ( $5^{\circ}$  to  $25^{\circ}$ ), the observed maximum of  $tan\delta$  is not much higher (0.018) versus 0.015). By combining Eq. 2 (standard trend between  $\tan \delta$  and  $E'/\gamma$ ) and Eq. 3 (dependence of  $E'/\gamma$  on MFA), a predicted relationship between  $tan\delta$  and MFA can be drawn (Figure 6a). In this way, the shape of the relationship is closer to the theoretical dependence of  $tan\delta$  on changing orientations (Norimoto et al. 1986; Obataya et al. 2000; Brémaud et al. 2011b). Looking at this predictive curve, the damping behaviours of CW and NW are different.

The direct observation (Figure 6b) of the relationship between  $\tan \delta$  and  $E'/\gamma$  (which is closely related to MFA and thus gives similar information) is a good alternative, as scale effects between test specimens and MFA observations are circumvented. NW from the 3 species followed a single, similar trend which, if extended towards higher values of  $E'/\gamma$ , would join the data for 'resonance' spruce from the literature (Haines 2000; Yano et al. 1992; Bucur 2006; Brémaud 2012). CW of the three species also followed a common trend, but shifted downwards lower  $tan\delta$  when compared with the trend for NW. When compared to the 'standard' curve from Ono and Norimoto (1983), the curve for NW is above and that for CW is below the reference. Measured  $\tan \delta$  values are proportional to those calculated by this empirical model based on  $E'/\gamma$  (Figure 6c) with CW being 15% lower and NW 19% higher. Values of tan $\delta$  higher than the 'standard' are often observed in NW of Pinaceae (Brémaud et al. 2009). There are

some small differences between the 3 species, but these are not highly significant. So that, at equivalent  $E'/\gamma$ , CW had damping values 34% lower than NW. This strong difference shall be due to differences in chemical composition. According to simulations based on cell wall models (Akitsu et al. 1993; Obataya et al. 2000), vertical shifts in the tan $\delta - E'/\gamma$ representation are essentially related to changes in matrix viscosity. The deviation from standard damping (DS $\delta$ , Eq. 4), that is, the percentage difference from the standard curve, can serve as an empirical indicator for such putative chemical accounting differences, as it was previously introduced for the effect of extractives (Brémaud et al. 2010b, 2012).

$$DS\delta = \frac{\tan \delta_i - \tan \delta_s}{\tan \delta_s} \tag{4}$$

Where  $\tan \delta_i$  is the measured damping coefficient of a given sample, and  $\tan \delta_s \left(=10^{-1.23} \times (E'/\gamma)^{-0.68}\right)$  is the standard trend from Eq. 2.

Damping coefficient can then be estimated from specific modulus  $E'/\gamma$  and DS $\delta$  according to Eq. 5:

$$\tan \delta_n = \tan \delta_s \times (1 + DS\delta) \tag{5}$$

Where  $\tan \delta_p$  is the predicted damping coefficient, which, in the present case, accounts for 92% of the measured variability in damping (Figure 6d).

# Role of variations in matrix chemistry on viscoelastic properties

The changes between NW and CW may be quite gradual ( $\gamma$  or MFA) or more abrupt (amount and structure of lignin). Therefore, some properties may be distributed along a continuum, and others not, depending on their predominant affecting factors. Gindl (2002) found that, despite a higher MFA, the more abundant and condensed lignin leads to increased compression strength parallel to the grain in CW, which was also found in the present study, although  $\gamma$  still had a dominant effect.

Concerning vibrational properties, the important residual differences in tan $\delta$  between CW and NW, after taking MFA into account, can be clearly interpreted as an influence of the changes in polymers of the cell wall matrix. On the contrary, it was not possible to detect a

convincing influence of matrix composition on  $E'/\gamma$ , which mostly depends on MFA. These results are similar to those from other studies focused on extractives from several species (Yano 1994; Matsunaga et al. 1998; Obataya et al. 1999; Minato et al. 2010; Brémaud et al. 2010ab, 2011b). Between CW and NW, differences in extractives are generally negligible compared to differences in matrix polymers.

Lignin is known to be responsible for the main thermal-softening transition in watersaturated wood, which has notably been studied by DMA (dynamic mechanical analysis) (Salmén 1984; Furuta et al. 1997, 2000, 2008, 2010). Dynamic IR spectroscopy (in dry conditions) also indicates that lignin exhibits a much more viscoelastic behaviour than carbohydrates do (Akerholm and Salmén 2003). Thus, an increased lignin/cellulose ratio in CW should result in an increased viscosity, instead of the reduction which is observed in the present paper after separating the effect of MFA variations.

Samples of the 3 trees/species studied in the present work exhibit the generally known characteristic differences in lignin between CW and NW, according to FT-IR spectra (Figure 4). Bigger amplitude of bands at 1600 and at 510 cm-1, related to aromatic skeletal vibrations (Faix 1991; Schwanninger et al. 2004), is for higher lignin content in CW. The smaller ratio between the bands at 1510 and 1600 cm-1 in CW spectra indicates a lower proportion in guaiacyl (G) units (Faix 1991; Gindl 2002; Schwanninger et al. 2004), while a small band at 834 cm-1, present in CW but absent in NW spectra, is related to phydroxyphenyl (H) units (Faix 1991; Gindl 2002). Both spectral features indicate that the CW lignin consist of G and H units (i.e. is a HG lignin) while NW lignins in conifers is a G lignin. CW lignins are also known to be more condensed (Timell 1982; Yeh et al. 2005, 2006; Nanayakkara et al. 2009), which is probably reflected by the higher band at 1227cm-1 (Schwanninger et al. 2004).

In the quasi-static domain, a lower S/G (syringyl/guaiacyl) ratio was related to lower relative creep at similar MFA levels, in an unusual wood growth in branches of a specific hardwood (HW) (Wang et al. 2010). Thermo-activated dynamic mechanical studies on water-saturated wood have shown that an increase in cross-linking density of lignin,

brought about by thermal and/or chemical treatments, results in a shift of the main softening transition of wood towards higher temperatures (Olsson and Salmén 1992; Placet et al. 2008; Assor et al. 2009). Similarly, in untreated wood, softening temperatures are lower in HW of the temperate zone, having GS lignins, than in softwoods (SW) of the temperate zone with G lignins (Olsson and Salmén 1992, Furuta et al. 2008). Tropical HW may contain very different S/G ratios and lignin contents (Sarkanen and Ludwig 1971; Wu 1993); their softening temperatures are often in between those found for temperate zone HW and SW (Furuta et al. 2008). Olsson and Salmén (1997) found a nearly linear decrease of softening temperature of wet wood as a function of methoxy group contents, which can be considered as 'bulking' groups preventing cross-linking via chemical linkages in position 5 of the aromatic ring. CWs of 2 Pinus species had both the highest softening temperatures and activation energies, and the lowest methoxy group contents (Olsson and Salmén 1997). However, in another study (Placet et al. 2008), softening temperature of CW was lower than that of NW. Probably, the softening temperature of bulk wood results from interactions between polymer structure, supramolecular architecture of wood components in the cell wall, and topochemistry of the tissue. Molecular modelling coupled with experiments on synthetic polymers of lignin precursors have also shown that higher methoxy contents led to more flexible polymers (Rusell et al. 2000). In summary, the results of the present work - more condensed CW ligning with elevated H contents have lower wood tand at a similar MFA/stiffness level - are consistent with data of the literature. In short: condensed lignins with less methoxy groups lead to decreased wood viscosity.

The influence of lignin on viscoelasticity in the audio-frequencies range of air dried wood had hitherto only been hypothesized, but had never been assessed experimentally. Interestingly, damping deviations due to lignin found in the present paper were of lower absolute amplitude (approx. 34%) than those observed in other studies in the case of some particular extractives (up to ≥45%). Differences between species in the amount and chemical structure of lignin and of extractives could explain damping characteristics that are

observed between temperate or tropical zones, and between botanical groups (Brémaud et al. 2009, 2012; Brémaud 2012).

## Conclusion

The deviating properties of compression wood (CW) and normal wood (NW) within a single tree offer a good opportunity for studying the influence of specific gravity ( $\gamma$ ), microfibril angle (MFA), and cell-wall matrix composition and chemistry on wood viscoelastic properties. The present work was focusing on viscoelastic vibrational tests of three wood species, and interrelations with MFA, physical-mechanical and IR-spectroscopic characteristics were observed. Results showed that:

- Differences in all properties between CW highly and NW are significant. Amplitudes of absolute differences rank in the order: axial shrinkage > MFA  $\geq$ specific modulus of elasticity  $(E'/\gamma)$  and axial-to-shear anisotropy  $\geq$  colour intensity and redness  $\geq$  transverse shrinkage > Young's modulus  $(E') \ge \gamma \ge$ compressive strength >damping coefficient  $(\tan \delta)$ .
- Specific modulus of elasticity (E'/γ) decreases with increasing MFA, following a common trend between CW and NW. Young's modulus (E') can be predicted from γ and MFA, and the residual variability does not appear to be linked to wood type nor to changes in polymer matrix in the cell walls.
- Damping coefficient  $(\tan \delta)$  tends to increase with MFA, but MFA as a parameter is not sufficient to describe changes in  $tan\delta$  between NW and CW. After taking into account the effect of (through the  $tan\delta$ \_ MFA E'/vrelationship), it appears that CW has a lower (by ca. 34%) 'normalized' damping than NW. This can be ascribed to lignin chemistry (as readily visible in FT-IR spectra): more condensed lignins with fewer methoxy groups lead to decreased viscosity.

Present results are consistent with previous findings on different materials and in other physical domains, particularly in thermalsoftening studies. Obviously, the effects of matrix polymers chemistry on macroscopic viscoelasticity are in relation to the

supramolecular structure at the micro- and nano-level of the cell wall. It would be interesting to verify if differences in lignin structure could also be involved in taxonomyrelated damping characteristics.

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