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# WIAS-TeSCA - Two-dimensional semi-conductor analysis package 

Herbert Gajewski, Matthias Liero, Reiner Nürnberg, Holger Stephan
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Weierstrass Institute
Mohrenstr. 39
10117 Berlin
Germany
email: Herbert.Gajewski@wias-berlin.de
Matthias.Liero@wias-berlin.de
Reiner.Nürnberg@wias-berlin.de
Holger.Stephan@wias-berlin.de

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[^0]Edited by
Weierstraß-Institut für Angewandte Analysis und Stochastik (WIAS)
Leibniz-Institut im Forschungsverbund Berlin e. V.
Mohrenstraße 39
10117 Berlin
Germany

Fax: $\quad+4930$ 20372-303
E-Mail: preprint@wias-berlin.de
World Wide Web: http://www.wias-berlin.de/


#### Abstract

WIAS-TeSCA (Two- and three-dimensional semiconductor analysis package) is a simulation tool for the numerical simulation of charge transfer processes in semiconductor structures, especially in semiconductor lasers. It is based on the drift-diffusion model and considers a multitude of additional physical effects, like optical radiation, temperature influences and the kinetics of deep impurities. Its efficiency is based on the analytic study of the strongly nonlinear system of partial differential equations - the van Roosbroeck system - which describes the electron and hole currents. Very efficient numerical procedures for both the stationary and transient simulation have been implemented. WIAS-TeSCA has been successfully used in the research and industrial development of new electronic and optoelectronic semiconductor devices such as transistors, diodes, sensors, detectors and lasers and has already proved its worth many times in the planning and optimization of these devices. It covers a broad spectrum of applications, from heterobipolar transistor (mobile telephone systems, computer networks) through high-voltage transistors (power electronics) and semiconductor laser diodes (fiber optic communication systems, medical technology) to radiation detectors (space research, high energy physics). WIAS-TeSCA is an efficient simulation tool for analyzing and designing modern semiconductor devices with a broad range of performance that has proved successful in solving many practical problems. Particularly, it offers the possibility to calculate self-consistently the interplay of electronic, optical and thermic effects.


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## About this manual

WIAS-TeSCA (Two-dimensional semiconductor analysis package) is a simulation tool for the numerical simulation of charge transfer processes in semiconductor structures, especially in semiconductor lasers. It is based on the drift-diffusion model and considers a multitude of additional physical effects, like optical radiation, temperature influences and the kinetics of deep impurities. Its efficiency is based on the analytic study of the strongly nonlinear system of partial differential equations - the van Roosbroeck system - which describes the electron and hole currents. Very efficient numerical procedures for both the stationary and transient simulation have been implemented.
WIAS-TeSCA has been successfully used in research and industrial development of new electronic and optoelectronic semiconductor devices such as transistors, diodes, sensors, detectors and lasers and has already proved its worth many times in the planning and optimization of these devices. It covers a broad spectrum of applications, from hetero-bipolar transistor (mobile telephone systems, computer networks) through high-voltage transistors (power electronics) and semiconductor laser diodes (fiber optic communication systems, medical technology) to radiation detectors (space research, high energy physics).
WIAS-TeSCA is an efficient simulation tool for analyzing and designing modern semiconductor devices with a broad range of performance that has proved successful in solving many practical problems. Particularly, it offers the possibility to calculate self-consistently the interplay of electronic, optical and thermic effects.

This user manual describes how to use WIAS-TeSCA. It is divided into the following parts:

- Chapter 1 presents the physical models that are implemented in WIAS-TeSCA.

■ Chapter 2 describes the script language used in WIAS-TeSCA and how to do simulations.

- In Chapter 3 information on the numerical schemes and implementations is given.


## 1 Physics in TeSCA

The aim of this chapter is to sketch the mathematical and physical model which is used by the simulation tool WIAS-TeSCA. Instructions and references for the related WIAS-TeSCA commands, which are descibed in detail in Chapter 2, are given.

### 1.1 Fundamental system of equations

### 1.1.1 Drift-diffusion model

WIAS-TeSCA is a simulation tool which is designed for numerically solving the fundamental system of equations of charge carrier transport in semiconductors in the two-dimensional case (cross sections or rotational symmetry, see Fig. 1.1 and description of DEVICE command). The widely accepted phenomenological system of equations for modeling semiconductor devices was deduced by van Roosbroeck [vR50] in 1950. It is based on Boltzmann statistics and is governed by the Poisson equation and continuity equations for electrons and holes, respectively, that read

$$
\begin{align*}
-\nabla \cdot\left(\varepsilon_{0} \varepsilon_{\mathrm{r}} \nabla \varphi\right) & =q\left(C_{\mathrm{net}}+p-n\right)  \tag{1.1a}\\
q \frac{\partial}{\partial t} n-\nabla \cdot \mathbf{J}_{n} & =q(G-R)  \tag{1.1b}\\
q \frac{\partial}{\partial t} p+\nabla \cdot \mathbf{J}_{p} & =q(G-R) \tag{1.1c}
\end{align*}
$$



Figure 1.1: Left: Sketch of ridge waveguide laser, Right: Sketch of a cylindric solar cell

The three calculated physical quantities are the electron density $n$, the hole density $p$, and the electrostatic potential $\varphi$. The latter gives the electric field $\mathbf{E}=-\nabla \varphi$. The electron and hole densities and the electrostatic potential are functions of time $t$ and of two spatial coordinates $x$ and $y$. Further variables are
$\varepsilon_{0} \quad$ vacuum permittivity $\approx 8.854 \cdot 10^{-12} \mathrm{C} /(\mathrm{Vm})$,
$\varepsilon_{\mathrm{r}} \quad$ relative permittivity of the material,
$q \quad$ elementary charge $\approx 1.6021 \cdot 10^{-19} \mathrm{As}$,
$C_{\text {net }} \quad$ net doping density of donators and acceptors $=N_{\mathrm{D}}-N_{\mathrm{A}}$,
$\mathbf{J}_{n}, \mathbf{J}_{p} \quad$ vectorial current density of electrons and holes, respectively,
$G-R$ generation-recombination rate.
The vectorial electron and hole current densities $\mathbf{J}_{n}$ and $\mathbf{J}_{p}$, respectively, are calculated from $\varphi, n$, and $p$ as follows

$$
\begin{equation*}
\mathbf{J}_{n}=-q n \mu_{n} \nabla \varphi_{n}, \quad \mathbf{J}_{p}=-q p \mu_{p} \nabla \varphi_{p}, \tag{1.2}
\end{equation*}
$$

where $\mu_{n}, \mu_{p}$ denoted the mobility of electrons and holes, respectively, and $\varphi_{n}$ and $\varphi_{p}$ are the quasi-Fermi potentials of electrons and holes. The quasi-Fermi potentials $\varphi_{n}$ and $\varphi_{p}$ are related to the electron and hole densities $n$ and $p$ by

$$
\begin{equation*}
n=N_{\mathrm{c}} \mathcal{F}\left[\frac{q\left(\varphi-\varphi_{n}\right)-E_{\mathrm{c}}}{k_{\mathrm{B}} T}\right], \quad \text { and } \quad p=N_{\mathrm{v}} \mathcal{F}\left[\frac{q\left(\varphi_{p}-\varphi\right)+E_{\mathrm{v}}}{k_{\mathrm{B}} T}\right], \tag{1.3}
\end{equation*}
$$

where
$T$ lattice temperature,
$k_{\mathrm{B}} \quad$ Boltzmann constant $\approx 1.380662 \cdot 10^{-23} \mathrm{VA} / \mathrm{K}$,
$N_{\mathrm{c}}, N_{\mathrm{v}}$ effective density of states of electrons and holes, respectively,
$E_{\mathrm{c}}, E_{\mathrm{v}}$ conduction and valence band edge, respectively,
$\mathcal{F} \quad$ Boltzmann or Fermi statistic.
WIAS-TeSCA is suited to solve the van Roosbroeck system (1.1)-(1.3) numerically in practically any two-dimensional area (including three-dimensional domains with rotational symmetry). Heterostructures are modeled by dividing the computational domain into several subareas (material regions). For each subarea individual material parameters ( $\varepsilon_{\mathrm{r}}, E_{\mathrm{c}}, E_{\mathrm{g}}, N_{\mathrm{c}}, N_{\mathrm{v}}$, etc.) can be defined.
For transient calculations, in WIAS-TeSCA the continuity equations for the electrons and holes (1.1b) and (1.1c) as well as the total current balance instead of the Poisson equation are used, namely

$$
\begin{equation*}
\nabla \cdot \mathbf{J}=0, \quad \mathbf{J}=\mathbf{J}_{n}+\mathbf{J}_{p}-\varepsilon_{0} \varepsilon_{\mathrm{r}} \nabla \frac{\partial \varphi}{\partial t} . \tag{1.4}
\end{equation*}
$$

Here, the total current $\mathbf{J}$ is the sum of electron hole and displacement current. ${ }^{1}$

[^1]WIAS-TeSCA is designed for the numerical treatment of both the stationary and the transient case. To limit the numerical complexity, defect calculations are used to decide dynamically whether the full system can be reduced temporary by suppressing one equation.

### 1.1.2 Equations of state

In WIAS-TeSCA, either Boltzmann statistics or Fermi-Dirac statistics can be used. In general, the following relationship between the charge carrier densities $n, p$, the electrostatic potential $\varphi$, and the quasi-Fermi potentials $\varphi_{n}, \varphi_{p}$ is assumed

$$
\begin{array}{ll}
n=N_{\mathrm{c}} \mathcal{F}\left(\eta_{n}\right), & \eta_{n}=\frac{q\left(\varphi-\varphi_{n}\right)-E_{\mathrm{c}}}{k_{\mathrm{B}} T} \\
p=N_{\mathrm{v}} \mathcal{F}\left(\eta_{p}\right), & \eta_{p}=\frac{q\left(\varphi_{p}-\varphi\right)+E_{\mathrm{v}}}{k_{\mathrm{B}} T} \tag{1.5b}
\end{array}
$$

The function $\mathcal{F}$ is given via

$$
\mathcal{F}(\eta)=\left\{\begin{array}{lll}
F_{1 / 2}(\eta) & \Leftrightarrow & \text { Fermi-Dirac statistics }  \tag{1.6}\\
\exp (\eta) & \Leftrightarrow & \text { Boltzmann statistics. }
\end{array}\right.
$$

The Fermi integral $F_{1 / 2}(s)$, which holds for Fermi-Dirac statistics for free particles, is defined in the following way:

$$
\begin{equation*}
F_{1 / 2}(\eta)=\frac{2}{\sqrt{\pi}} \int_{0}^{\infty} \frac{\sqrt{y}}{1+\exp (y-\eta)} \mathrm{d} y \tag{1.7}
\end{equation*}
$$

If Boltzmann statistics holds, the relations in (1.5) can be written in terms of the intrinsic charge carrier density $n_{\mathrm{i}}$ and intrinsic Fermi level $E_{\mathrm{i}}$

$$
\begin{align*}
n & =n_{\mathrm{i}} \exp \left[\frac{q\left(\varphi-\varphi_{n}\right)-E_{\mathrm{i}}}{k_{\mathrm{B}} T}\right]  \tag{1.8a}\\
p & =n_{\mathrm{i}} \exp \left[\frac{q\left(\varphi_{p}-\varphi\right)+E_{\mathrm{i}}}{k_{\mathrm{B}} T}\right],  \tag{1.8b}\\
n_{\mathrm{i}} & =\sqrt{N_{\mathrm{c}} N_{\mathrm{v}}} \exp \left[\frac{E_{\mathrm{v}}-E_{\mathrm{c}}}{2 k_{\mathrm{B}} T}\right]  \tag{1.8c}\\
E_{\mathrm{i}} & =\frac{E_{\mathrm{c}}+E_{\mathrm{v}}}{2}+\frac{k_{\mathrm{B}} T}{2} \ln \left[\frac{N_{\mathrm{v}}}{N_{\mathrm{c}}}\right] . \tag{1.8d}
\end{align*}
$$

and by substituting $\frac{\partial}{\partial t} p$ and $\frac{\partial}{\partial t} n$ using the continuity equations in (1.1c) and (1.1b)

$$
\begin{aligned}
q\left(\frac{\partial p}{\partial t}-\frac{\partial n}{\partial t}\right) & =\left(q(G-R)-\nabla \cdot \mathbf{J}_{p}\right)-\left(q(G-R)+\nabla \cdot \mathbf{J}_{n}\right) \\
& =\nabla \cdot\left(\mathbf{J}_{n}+\mathbf{J}_{p}\right)
\end{aligned}
$$

By canceling the derivatives with respect to time $\frac{\partial}{\partial t} n$ and $\frac{\partial}{\partial t} p$ the transient case becomes stationary.

In the case of Fermi-Dirac statistics, the actual calculation of the densities is realized by replacing the exponential function of the Boltzmann case with the Fermi integral (1.7) to the index $1 / 2$. However, these relations are traced back to the Boltzmann relations in the intern implementation by iteratively calculated correction variables, which read

$$
\begin{equation*}
\gamma_{n}=\frac{F_{1 / 2}\left(\eta_{n}\right)}{\exp \left(\eta_{n}\right)}, \quad \text { and } \quad \gamma_{p}=\frac{F_{1 / 2}\left(\eta_{p}\right)}{\exp \left(\eta_{p}\right)} \tag{1.9a}
\end{equation*}
$$

With this, we can write the Fermi case as a corrected Boltzmann statistic via

$$
\begin{align*}
n & =n_{\mathrm{i}}^{\prime} \exp \left[\frac{q\left(\varphi-\varphi_{n}\right)-E_{\mathrm{i}}^{\prime}}{k_{\mathrm{B}} T}\right],  \tag{1.9b}\\
p & =n_{\mathrm{i}}^{\prime} \exp \left[\frac{q\left(\varphi_{p}-\varphi\right)+E_{\mathrm{i}}^{\prime}}{k_{\mathrm{B}} T}\right],  \tag{1.9c}\\
n_{\mathrm{i}}^{\prime} & =n_{\mathrm{i}} \sqrt{\gamma_{n} \gamma_{p}},  \tag{1.9d}\\
E_{\mathrm{i}}^{\prime} & =E_{\mathrm{i}}+\frac{k_{\mathrm{B}} T}{2} \ln \left[\frac{\gamma_{p}}{\gamma_{n}}\right] . \tag{1.9e}
\end{align*}
$$

For optoelectronic applications (see Section 1.5), Fermi-Dirac statistics are automatically employed. In WIAS-TeSCA the command FERMI is used to describe the state equations (see Section 2.8).

### 1.1.3 Mobility models

Various models for the electron and hole mobilities $\mu_{n}$ and $\mu_{p}$ in (1.2) are implemented in WIAS-TeSCA. They describe the dependence of the mobilities on temperature, doping, and electric field. The models and the related parameters are set via the MOBILITY command, which is discussed in Section 2.11.

### 1.1.4 Generation and recombination

The generation-recombination term $G-R$ in the continuity equations for electrons and holes in (1.1b) and (1.1c) is additively split into various effects, viz.

$$
G-R=G_{\mathrm{Ava}}-R_{\mathrm{rad}}-R_{\mathrm{Aug}}-R_{\mathrm{SRH}}-R_{\mathrm{surf}} \delta_{\Gamma_{\text {Gate }}} \pm \ldots,
$$

where $\delta_{\Gamma_{\text {Gate }}}$ denotes the Dirac distribution concentrated on a Gate contact, where surface recombination takes place.
In WIAS-TeSCA the following recombination models are implemented

$$
\begin{array}{ll}
\text { Radiative recombination } & R_{\mathrm{rad}}=a_{\mathrm{b}}\left(n p-n_{\mathrm{i}}^{2}\right), \\
\text { Auger recombination } & R_{\mathrm{Aug}}=\left(a_{n} n+a_{p} p\right)\left(n p-n_{\mathrm{i}}^{2}\right), \\
\text { Shockley-Read-Hall recombination } & R_{\mathrm{SRH}}=\frac{n p-n_{\mathrm{i}}^{2}}{\tau_{n}\left(n+r_{n}\right)+\tau_{p}\left(p+r_{p}\right)}, \\
\text { Surface recombination at gate contacts } & R_{\mathrm{Surf}}=\frac{n p-n_{\mathrm{i}}^{2}}{\frac{n+r_{n}}{v_{n}}+\frac{p+r_{p}}{v_{p}}} .
\end{array}
$$

The Avalanche generation is given via

$$
G_{\mathrm{Ava}}=a_{1}\left|\mathbf{J}_{n}\right| \exp \left[-\frac{a_{2}}{\beta_{n}}\right]+b_{1}\left|\mathbf{J}_{p}\right| \exp \left[-\frac{b_{2}\left(\beta_{p}\right)}{\beta_{p}}\right]
$$

where $\beta_{n}=\left|\mathbf{E} \cdot \mathbf{J}_{n}\right| /\left|\mathbf{J}_{n}\right|$ and $\beta_{p}=\left|\mathbf{E} \cdot \mathbf{J}_{p}\right| /\left|\mathbf{J}_{p}\right|$, respectively, see [Sel84, p. 110].
The command RECOMBINATION (described in Section 2.18) allows the input of data for the generation-recombination model. In addition to the recombination terms above, trap dynamics can be included as well. They are described in detail in Section 1.3. Moreover, the SPECIAL allows to include a generation rate $G_{\text {ext }}$ that describes the generation of electron-hole pairs e.g. due to Lambert-Beer absorption or by the trace of an incident particle in a sensor device.

### 1.1.5 Doping

In WIAS-TeSCA, several different analytically specified doping profiles are implemented, which enter the Poisson equation in (1.1a). They can be superposed with each other and with one-dimensional profiles. Other analytically given or in files defined two-dimensional doping profiles can be included as well. The doping profile can be selected by entering the command DOPING.

### 1.1.6 Including external magnetic fields

The effects of an external magnetic field perpendicular to the $x y$-plane can be taken into account in the simulation. We define

$$
\begin{equation*}
b_{n}=\mu_{n}|\mathbf{B}|, \quad \text { and } \quad b_{p}=\mu_{p}|\mathbf{B}|, \tag{1.10}
\end{equation*}
$$

where
$\mu_{n}, \mu_{p}$ electron and hole Hall mobility, respectively,
B vectorial magnetic field.

In this case, the current densities in the continuity equations (1.1b) and (1.1c) are replaced by

$$
\begin{align*}
& \mathbf{J}_{n}(\mathbf{B})=\frac{\mathbf{J}_{n}(0)+\mu_{n} \mathbf{B} \times \mathbf{J}_{n}(0)}{1+b_{n}^{2}},  \tag{1.11a}\\
& \mathbf{J}_{p}(\mathbf{B})=\frac{\mathbf{J}_{p}(0)+\mu_{p} \mathbf{B} \times \mathbf{J}_{p}(0)}{1+b_{p}^{2}} \tag{1.11b}
\end{align*}
$$

Here $\mathbf{J}_{n}(0)$ and $\mathbf{J}_{p}(0)$ are the vectorial current densities without magnetic field given in (1.2). Note that $\mu_{n} \mathbf{B}= \pm b_{n} \mathbf{e}_{z}$ and $\mu_{p} \mathbf{B}= \pm b_{p} \mathbf{e}_{z}$, where $\mathbf{e}_{z}$ is perpendicular to the $x y$-plane.

The influence of the magnetic field is set by providing values for $b_{n}$ (parameter BMUEN) and $b_{p}$ (parameter BMUEP) in the DEVICE command.

### 1.1.7 Boundary conditions

The system of differential equations in (1.1) is complemented by boundary conditions, that model the interaction of the device with its vicinity. In WIAS-TeSCA the following types of boundary conditions are implemented.

## Ohmic contacts

At ohmic contacts the program merely needs the applied potential $\varphi_{\mathrm{a}}$ as input (in the STEP command). The following Dirichlet boundary values at the contact are assumed:

$$
\begin{equation*}
\varphi=\varphi_{\mathrm{a}}+U_{0}, \quad \text { and } \quad n=n_{0}, \quad p=p_{0} . \tag{1.12}
\end{equation*}
$$

Here $U_{0}=U_{T} \ln \left(n_{0} / N_{i}^{\mathrm{eff}}\right)$, and the boundary values $n_{0}$ and $p_{0}$ are determined as positive solutions of the equilibrium and charge neutrality condition, namely

$$
\begin{equation*}
n_{0} p_{0}=\left(N_{i}^{\mathrm{eff}}\right)^{2}, \quad C_{0}+p_{0}-n_{0}=0 \tag{1.13}
\end{equation*}
$$

with $C_{0}$ denoting the doping at the contact.

## Bulk contact

WIAS-TeSCA offers the possibility to characterize an ohmic contact as bulk contact (by assigning the respective contact number to the integer parameter IBULK in the DEVICE command). At the bulk contact, $n$ and $p$ are treated like in the case of ohmic contacts. However, the ohmic boundary condition for the electrostatic potential $\varphi$ is modified as follows:

$$
\begin{equation*}
\varphi=\varphi_{\mathrm{a}}+U_{0}+R_{\mathrm{AB}} J_{\mathrm{b}} . \tag{1.14}
\end{equation*}
$$

Here, $U_{0}$ is as above and $R_{\mathrm{AB}}$ is the bulk resistance (in $\Omega$ ) that must be entered in the STEP command (parameter name RAB). Furthermore, $J_{\mathrm{b}}$ is the calculated current through the contact (for example caused by avalanche generation cf. Schütz-Selberherr-Pötzl [SSP82]).

## Schottky contacts

For Schottky contacts, WIAS-TeSCA needs the applied potential $\varphi_{\mathrm{a}}$ as well as the Dirichlet value for the electron density $n_{0}$ (in the STEP command). Then, the following boundary conditions are assumed at the contact

$$
\begin{equation*}
\varphi=\varphi_{\mathrm{a}}+U_{T} \ln \left(n_{0} / N_{\mathrm{i}}^{\mathrm{eff}}\right), \quad n=n_{0}, \quad p_{0}=\left(N_{\mathrm{i}}^{\mathrm{eff}}\right)^{2} / n_{0} \tag{1.15}
\end{equation*}
$$

Note: In the literature, it is usually set

$$
\begin{equation*}
n_{0}=N_{i}^{\mathrm{eff}} \exp \left[\frac{E_{\mathrm{g}}-2 \Phi_{\mathrm{S}}}{2 U_{T}}\right] . \tag{1.16}
\end{equation*}
$$

Here, $E_{\mathrm{g}}=E_{\mathrm{c}}-E_{\mathrm{v}}$ is the band gap of the semiconductor material at the contact and $\Phi_{\mathrm{S}}$ is the Schottky barrier.

## Gate contacts

For gate contacts, the following boundary conditions hold:

$$
\begin{align*}
& \varepsilon_{s} \nabla \varphi \cdot \mathbf{n}+\frac{\varepsilon_{\mathrm{ox}}}{d_{\mathrm{ox}}}\left(\varphi-\varphi_{\mathrm{a}}-\varphi_{\mathrm{k}}\right)=Q_{\mathrm{SS}},  \tag{1.17}\\
& \mathbf{J}_{n} \cdot \mathbf{n}=\mathbf{J}_{p} \cdot \mathbf{n}=0 \tag{1.18}
\end{align*}
$$

The used variables are:
n unit vector perpendicular to contact pointing outwards,
$\varepsilon_{\mathrm{ox}} \quad$ dielectric coefficient of oxide,
$d_{\mathrm{ox}} \quad$ thickness of the oxide,
$\varphi_{\mathrm{a}} \quad$ applied voltage at gate,
$\varphi_{\mathrm{k}} \quad$ contact voltage at gate,
$Q_{\mathrm{SS}} \quad$ density of states at boundary surfaces.
The quantities $\varepsilon_{\mathrm{ox}}, d_{\mathrm{ox}}$ and $\varphi_{\mathrm{k}}$ are entered in the DEVICE command, $\varphi_{\mathrm{a}}$ is entered in the STEP command.

## Inductivity, capacity, and resistance

For transient calculations, it is possible to attach an external circuit at each contact. This circuit contains an inductance, a resistance and a parallelly connected capacitance. For this purpose, the parameter ICLR must be set to 1 or 2 in the DEVICE command and for each of the parameters $A_{\mathrm{C}}$ (capacitance), $A_{\mathrm{L}}$ (inductance) and $A_{\mathrm{R}}$ (resistance) and each of the contacts a value has to be assigned. Then, at contacts with $\max \left(A_{\mathrm{C}}, A_{\mathrm{L}}, A_{\mathrm{R}}\right)>0$ the dynamic boundary condition

$$
\begin{equation*}
A_{\mathrm{L}} \frac{\mathrm{~d}^{2}}{\mathrm{~d} t^{2}} J+A_{\mathrm{R}} \frac{\mathrm{~d}}{\mathrm{~d} t} J+\frac{1}{A_{\mathrm{C}}} J=\frac{\mathrm{d}}{\mathrm{~d} t} U \tag{1.19}
\end{equation*}
$$

is realized as (natural) boundary condition for the total current equation.
For $\operatorname{ICLR}=1$ we have

| $U=U_{i}-U_{a} \quad$ | $U_{i}$ inner and $U_{a}$ outer electrostatic potential at the con- |
| :--- | :--- |
| tact, |  |
| total current through the contact, |  |

otherwise, for ICLR $=2$ we have

$$
\begin{array}{ll}
U=U_{i}(x)-U_{a}(x) & \begin{array}{l}
U_{i}(x) \text { inner and } U_{a}(x) \text { outer electrostatic potential in the } \\
\text { boundary point } x, \\
\text { current component pointing outwards in the boundary } \\
\\
\text { point } x .
\end{array}
\end{array}
$$

If an ohmic contact is marked (by assigning the corresponding contact number to the parameter ISTROM or ICAP in the DEVICE command), the equation

$$
\begin{equation*}
J-J_{\mathrm{S}}=A_{\mathrm{C}} \frac{\mathrm{~d} U}{\mathrm{~d} t} \tag{1.20}
\end{equation*}
$$

will be realized as a (natural) boundary condition for the total current equation (instead of AC in the DEVICE command, the parameter CAP in the STEP command can be used). ${ }^{2}$ The quantities are:

$$
\begin{array}{ll}
U=U_{i}(x)-U_{a}(x) & \begin{array}{l}
U_{i}(x) \text { inner and } U_{a}(x) \text { outer electrostatic potential in the } \\
\text { boundary point } x, \\
\text { current component pointing outwards in the boundary } \\
\text { point } x .
\end{array}
\end{array}
$$

The parameters for the current $J_{\mathrm{S}}$ (STROM) and if necessary for the capacity $A_{\mathrm{S}}$ (CAP) have to be entered in the STEP command for each working point, respectively.
The electron and hole densities $n$ and $p$ are fixed by the Dirichlet conditions in the Ohmic case in (1.12).
Note: This type of boundary condition can be used to calculate the potential at the current contact (as asymptotic value in the time domain), that corresponds to a given current $J_{\mathrm{S}}$ (current controlled simulations).

## Isolating and symmetry conditions

Boundaries of the device that are not contacts are treated with ideal Neumann boundary conditions, namely,

$$
\begin{equation*}
\nabla \varphi \cdot \mathbf{n}=\mathbf{J}_{n} \cdot \mathbf{n}=\mathbf{J}_{p} \cdot \mathbf{n}=0 \tag{1.21}
\end{equation*}
$$

[^2]
### 1.1.8 Initial conditions

WIAS-TeSCA is able to execute alternately stationary and transient calculations. As initial value of a transient calculation always the solution of the last calculated stationary problem is chosen (if not an interrupted calculation is continued with saved values). If there is no preceding stationary calculation, the program automatically starts from the thermodynamic equilibrium.
For modulation experiments, in the transient case it is e.g. possible to apply a timely varying external voltage $U(t)$.

### 1.1.9 Oxide and passivation layers

As limiting cases, isolating and conducting areas are allowed. Oxide areas are characterized by an intrinsic charge carrier density of zero. Conduction areas can be modeled as oxide areas with a very large dielectric constant. In oxide areas only the linear Poisson equation is solved:

$$
\begin{equation*}
-\nabla \cdot\left(\varepsilon_{0} \varepsilon_{\mathrm{ox}} \nabla \varphi\right)=q C_{\mathrm{ox}}, \quad C_{\mathrm{ox}}=\gamma_{\mathrm{ox}}\left(N_{\mathrm{D}}-N_{\mathrm{A}}\right) \tag{1.22}
\end{equation*}
$$

The factor $\gamma_{o x}$ can be entered in the DEVICE command (parameter name FADOOX). If $\gamma_{o x}$ is zero, the Laplace equation will be solved in the oxide area. At the boundary surface between the semiconductor and the oxide area the relation

$$
\begin{equation*}
\varepsilon_{0}\left(\varepsilon_{\mathrm{r}} \nabla \varphi-\varepsilon_{\mathrm{ox}} \nabla \varphi\right) \cdot \mathbf{n}=q Q_{\mathrm{SS}}, \quad \mathbf{J}_{n} \cdot \mathbf{n}=\mathbf{J}_{p} \cdot \mathbf{n}=0 \tag{1.23}
\end{equation*}
$$

is realized as natural transition condition. Here the quantities are :
n unit vector perpendicular to boundary surface and pointing into oxide,
$\varepsilon_{\mathrm{ox}} \quad$ relative dielectric constant of oxide,
$Q_{\mathrm{SS}} \quad$ density of states at boundary surface.
With the simulation of floating gate transistors in mind a model for the injection of hot charge carriers into the oxide area is implemented.

### 1.2 Thermodynamic model

In WIAS-TeSCA the heat equation

$$
\begin{equation*}
\frac{\partial}{\partial t}\left(\left[C \rho+\frac{3}{2}(n+p) k_{\mathrm{B}}\right] T\right)-\nabla \cdot[\kappa(T) \nabla T]=Q \tag{1.24}
\end{equation*}
$$

is implemented. It can be solved simultaneously with the continuity equation and the optical equation. In (1.24) $C$ is the heat capacity, $\rho$ is the material density, and $\kappa$ is the thermal conductivity.

The source term $Q$ accounts for the following components (energy dissipation):

$$
\begin{equation*}
Q=Q_{\mathrm{joule}}+Q_{\mathrm{rec}}+Q_{\mathrm{rad}}, \tag{1.25}
\end{equation*}
$$

where

$$
\begin{equation*}
Q_{\text {joule }}=\frac{\mathbf{J}_{n}^{2}}{e \mu_{n} n}+\frac{\mathbf{J}_{p}^{2}}{e \mu_{p} p} \tag{1.26}
\end{equation*}
$$

accounts for joule heat, and

$$
\begin{equation*}
Q_{\mathrm{rec}}=q R_{\mathrm{nr}}\left(F_{n}-F_{p}+T\left(P_{n}+P_{p}\right)\right) \tag{1.27}
\end{equation*}
$$

for recombination heat ${ }^{3}$ ( $R_{\mathrm{nr}}$ is the non-radiative SRH and Auger recombination, $P_{n}$ and $P_{p}$ are thermoelectric powers).
The last heat source $Q_{\mathrm{rad}}$ in (1.24) is due to the absorption of spontaneous and stimulated emission of radiation:

$$
\begin{equation*}
Q_{\mathrm{rad}}=Q_{\mathrm{rad}}^{\mathrm{spont}}+Q_{\mathrm{rad}}^{\mathrm{stim}} . \tag{1.28}
\end{equation*}
$$

Below the lasing threshold the first term dominates, above it the second contribution becomes decisive. The spatial distribution of spontaneously emitted radiation is difficult to determine, moreover the absorption itself is a non-local process. Usually, it is assumed that the heating contribution through absorption of spontaneously emitted radiance is small. Thus, in WIAS-TeSCA it is neglected for modeling. Therefore, the total power equation ( $U I=$ coupled out power + dissipated power) is not fulfilled anymore. However, above the lasing threshold this should cause only a small error as the second term clearly dominates. ${ }^{4}$

The heat source which draws its energy from absorption of coherent radiation is governed by the equation

$$
\begin{equation*}
Q_{r a d}^{\text {stim }}=\frac{\omega \varepsilon_{0}}{2} \Im m\left[\varepsilon_{\text {intra }}(n, p)\right]|\mathbf{E}(\mathbf{r})|^{2} \tag{1.29}
\end{equation*}
$$

Here the imaginary part of the intra band part of the relative dielectric function $\varepsilon_{\text {intra }}$ accounts for all absorption processes, that change the number of charge carriers within the valence band and the conduction band, respectively. This is possible through free charge carrier absorption and inter valence band absorption. The distribution of the electric field $\mathbf{E}$ corresponds with the laser mode, plus other possibly considered modes.
Therefore, in (1.24) the heat source is estimated to be the following:

$$
\begin{equation*}
Q_{\mathrm{rad}}^{\mathrm{stim}}=\left(\alpha_{\mathrm{fc}}+\alpha_{\mathrm{bg}}\right) \cdot\left(P_{1}\left|\Phi_{1}\right|^{2}+P_{2}\left|\Phi_{2}\right|^{2}\right) \tag{1.30}
\end{equation*}
$$

where $\alpha_{\mathrm{fc}}$ is the free charge carrier absorption

$$
\begin{equation*}
\alpha_{\mathrm{fc}}=f_{\mathrm{cn}} n+f_{\mathrm{cp}} p \tag{1.31}
\end{equation*}
$$

and $\alpha_{\mathrm{bg}}$ describes the background absorption.

[^3]
### 1.3 Trap model and incomplete ionization

The Shockley-Read-Hall recombination was extended to incorporate deep traps in volume and on interfaces. These trap levels can take different states (neutral, negatively charged, positively charged) that are governed by additional equations. Therefore the basic equations in (1.1) were extended as follows. The partly ionized traps enter the Poisson equation (1.1a)

$$
\begin{equation*}
-\nabla \cdot\left(\varepsilon_{0} \varepsilon_{\mathrm{r}} \nabla \varphi\right)=q\left(C_{\mathrm{net}}+p-n\right)+\sum_{k=1}^{K} q_{k} N_{k} f_{k} \tag{1.32a}
\end{equation*}
$$

Here, $q_{k}= \pm q, N_{k}>0$, and $0 \leq f_{k} \leq 1$ denote the charge number (donor type $q_{k}=+q$ or acceptor type $q_{k}=-q$ ), the trap density, and defect occupancy, respectively. In particular, $f_{k}=1$ means that the trap is completely ionized.

The continuity equations for electrons and holes are augmented by the trap recombination rates

$$
\begin{align*}
\frac{\partial}{\partial t} n-\frac{1}{q} \nabla \cdot \mathbf{J}_{n} & =G-R-\sum_{k=1}^{K} R_{n, k}^{\mathrm{trap}}  \tag{1.32b}\\
\frac{\partial}{\partial t} p+\frac{1}{q} \nabla \cdot \mathbf{J}_{p} & =G-R-\sum_{k=1}^{K} R_{p, k}^{\mathrm{trap}} \tag{1.32c}
\end{align*}
$$

We drop the index $k$ from now on, then, the trap recombination rates are given via

$$
\begin{align*}
& R_{n}^{\text {trap }}= \begin{cases}N\left(s_{n} n(1-f)-e_{n} f\right) & \text { acceptor-type traps } \\
N\left(s_{n} n f-e_{n}(1-f)\right) & \text { donor-type traps }\end{cases}  \tag{1.33a}\\
& R_{p}^{\text {trap }}= \begin{cases}N\left(s_{p} p f-e_{p}(1-f)\right) & \text { acceptor-type traps } \\
N\left(s_{p} p(1-f)-e_{p} f\right) & \text { donor-type traps }\end{cases} \tag{1.33b}
\end{align*}
$$

where $s_{n}$ and $s_{p}$ are the capture coefficients and $e_{n}$ and $e_{p}$ the emission coefficients. The latter are given via

$$
\begin{align*}
& \frac{e_{n}}{s_{n}}=n_{\mathrm{i}} \exp \left[\frac{E_{\mathrm{r}}}{k_{\mathrm{B}} T}\right]=N_{\mathrm{c}} \exp \left[\frac{E_{\text {trap }}-E_{\mathrm{c}}}{k_{\mathrm{B}} T}\right],  \tag{1.33c}\\
& \frac{e_{p}}{s_{p}}=n_{\mathrm{i}} \exp \left[-\frac{E_{\mathrm{r}}}{k_{\mathrm{B}} T}\right]=N_{\mathrm{v}} \exp \left[\frac{E_{\mathrm{v}}-E_{\text {trap }}}{k_{\mathrm{B}} T}\right] \tag{1.33d}
\end{align*}
$$

with trap energy level $E_{\text {trap }}=E_{\mathrm{i}}+E_{\mathrm{r}}\left(E_{\mathrm{i}}\right.$ is the intrinsic Fermi level, cf. (1.8), and $E_{\mathrm{r}}$ the trap level relative to $E_{\mathrm{i}}$ ).

## 1 Physics in TeSCA

In addition to (1.32), evolution equations for the trap occupancy functions $f$ have to be solved, namely,

$$
N \frac{\mathrm{~d}}{\mathrm{~d} t} f= \begin{cases}R_{n}^{\text {trap }}-R_{p}^{\text {trap }} & \text { acceptor-type traps },  \tag{1.34}\\ R_{p}^{\text {trap }}-R_{n}^{\text {trap }} & \text { donor-type traps }\end{cases}
$$

In particular, in the stationary case the left-hand side in (1.34) is equal to zero. Thus, an algebraic equation for $f_{\text {stat }}$ is obtained and we find

$$
f_{\text {stat }}= \begin{cases}\frac{e_{p}+s_{n} n}{s_{n} n+e_{n}+s_{p} p+e_{p}} & \text { for acceptor-type traps } \\ \frac{e_{n}+s_{p} p}{s_{n} n+e_{n}+s_{p} p+e_{p}} & \text { for donor-type traps }\end{cases}
$$

Using this expression in (1.33) leads to

$$
R_{n}^{\text {trap }}=R_{p}^{\text {trap }}=\frac{n p-n_{\mathrm{i}}^{2}}{\tau_{n}\left(n+r_{n}\right)+\tau_{p}\left(p+r_{p}\right)},
$$

where $\tau_{n / p}=\frac{1}{s_{p / n} N}$ and $r_{n, p}=\frac{e_{n / p}}{s_{n / p}}$. In particular, this corresponds to the classical Shockley-Read-Hall recombination (cf. Subsection 1.1.4). Note, however, that the trapped charges contribute to the space charge via the Poisson equation (1.32a).
The parameters for the trap model are set in the RECOMBINATION command.

### 1.4 Small signal analysis

After the calculation of stationary solutions of (1.1), small signal analysis can be carried out. Here, the consequences of disturbances of the form

$$
\begin{equation*}
a \exp (\mathrm{i} \omega t) \quad \text { with } a \text { small, } \tag{1.35}
\end{equation*}
$$

of the contact potential $\varphi_{\mathrm{a}}$, see (1.14), are analyzed and used for the calculation of conductance and capacitance matrices $A$ and $B$ resp. according to the following formulas (cf. [Lau85]):

$$
\begin{equation*}
A_{k j}=\operatorname{Re}\left[\frac{\mathrm{d} J_{j}}{\mathrm{~d} U_{\mathrm{a}, k}}\right], \quad \text { and } \quad B_{k j}=\operatorname{Im}\left[\frac{\mathrm{d} J_{j}}{\mathrm{~d} U_{\mathrm{a}, k}}\right], \tag{1.36}
\end{equation*}
$$

where

$$
\begin{array}{ll}
\mathrm{Re}, \operatorname{Im} & \text { real and imaginary part, } \\
\mathrm{i} & \text { imaginary unit, } \\
\omega & \text { excitation frequency, } \\
t & \text { time variable, } \\
\mathrm{d} J_{j} & \text { the change of current through contact } j, \\
\mathrm{~d} U_{\mathrm{a} k} & \text { the change of potential at contact } k .
\end{array}
$$

The system of equations that arises from small signal analysis couples real and imaginary parts of $\varphi, n$ and $p$. It is solved by block iteration that combines a linearized Gummel method with a SOR method [GG92]. The latter decouples real and imaginary parts and was introduced by Laux [Lau85]. Small signal analysis is activated by entering the excitation frequency $\omega$ in the STEP command.

### 1.5 Optoelectronic model

The mathematical modeling of optoelectronic devices has some essentially new additional possibilities compared to the pure electronic simulation.

- By default, in the case of optoelectronic applications in WIAS-TeSCA the Fermi-Dirac statistics is active, in order to describe heterostuctures with degenerate semiconductor components.
- The van Roosbroeck system is extended by a (scalar) waveguide equations for TE- or TM- modes. in the following section 1.5.1 are treated.
- Different models for the local optical gain $g_{i}$ in the active region are implemented (details in section 2.9.1).
- To the continuity equations (1.1b), (1.1c) a term is added, modeling the stimulated recombination $R^{\text {stim }}$. It has the form

$$
\begin{equation*}
R^{\text {stim }}=g_{\text {net }}(\hbar \omega) * P|\Phi|^{2} /(\hbar \omega) \tag{1.37}
\end{equation*}
$$

$\hbar \omega$ is the photon energy, $P$ the total power and $|\Phi|^{2}$, the transversal intensity distribution. The net gain $g_{n e t}$ is the local gain $G(\hbar \omega)$ minus the local losses $\alpha$, as later described in section 1.5.1.

- In WIAS-TeSCA two variants are implemented, considering the optical power $P$

1. self-consistently (see section 1.5.2) assuming spatial homogeneity in the remaining spatial direction, or
2. parametrically, see section 1.5.3.

### 1.5.1 Helmholtz equation

A quasi-planar layered waveguide structure is supposed. Most epitaxial laser structures belong to this type, including ridge-waveguide lasers. The growth direction is $y$, the layer plane is $x$.

The optical field $\mathbf{E}(\mathbf{r}, t)$ is prescribed in the following way:

$$
\begin{equation*}
\mathbf{E}(\mathbf{r}, t)=\sum_{i} a_{i} \sqrt{P_{i}} \mathbf{e}_{i} \Phi_{i}(x, y) \cdot \Re e\left[e^{i \omega t}\left(e^{i \beta_{i} z}+e^{-i \beta_{i} z}\right)\right] \tag{1.38}
\end{equation*}
$$

where $i$ is a mode index. The values $\beta_{i}$ and $\Phi_{i}(x, y)$ are the eigenvalues and eigenfunctions of the corresponding Helmholtz equation, respectively. The norm of $\Phi_{i}(x, y)$ is normalized to unity. The constant $a_{i}$ is choosen such that $P_{i}$ is the corresponding modal power. The central frequency

$$
\begin{equation*}
\omega=2 \pi c / \lambda \tag{1.39}
\end{equation*}
$$

can be specified by the user via the wavelength $\lambda$.
For TE-modes $\left(\mathbf{e}_{i} \| \mathbf{x}\right)$, the following Helmholtz equation is solved:

$$
\begin{equation*}
\left[\Delta_{x, y}+\frac{\omega^{2}}{c^{2}}\left(\bar{n}^{2}-\bar{n}_{\mathrm{TE}}^{2}\right)\right] \Phi_{\mathrm{TE}}(x, y)=0 \quad \text { where } \quad \bar{n}=\bar{n}(x, y) \tag{1.40}
\end{equation*}
$$

is the local refractive index varying in the transvers $(x, y)$ plane. $\Phi_{\mathrm{TE}}$ and its derivatives are continuous at material boundaries. Available temperature dependent models for the local refractive index $\bar{n}$ are described under the command FERMI in section 2.9.2.
For TM modes $\left(\mathbf{e}_{i} \| \mathbf{y}\right)$ the Helmholtz equation for the "generating" magnetic field component $H_{x}^{\mathrm{TM}}$ is solved.

$$
\begin{equation*}
\left[\bar{n}^{2} \nabla_{x, y} \frac{1}{\bar{n}^{2}} \nabla_{x, y}+\frac{\omega^{2}}{c^{2}}\left(\bar{n}^{2}-\bar{n}_{\mathrm{TM}}^{2}\right)\right] H_{x}^{\mathrm{TM}}(x, y)=0 . \tag{1.41}
\end{equation*}
$$

$H_{x}^{\mathrm{TM}}(x, y)$ and $\bar{n}^{-2}\left(\vec{e}_{n} \nabla_{x, y}\right) H_{x}^{\mathrm{TM}}(x, y)$ are continuous at material boundaries with normal unit vector $\vec{e}_{n}$. The corresponding dominant electric field component ( $\perp$ to the layer level) is calculated according to the rule

$$
\begin{equation*}
\Phi_{\mathrm{TM}}(x, y)=\frac{-\beta_{\mathrm{TM}}}{\omega \varepsilon_{0} \bar{n}^{2}} H_{x}^{\mathrm{TM}}(x, y) \tag{1.42}
\end{equation*}
$$

WIAS-TeSCA currently allows the self-consistent consideration of up to 2 modes. The corresponding behavior can be select by the switch ISpec. An extension to more modes is under preparation.

### 1.5.2 Self-Consistent photon balance

The longitudinally averaged internal optical power $P_{i}$ of transverse mode $i$ is determined from the rate equation

$$
\begin{equation*}
\frac{d}{d t} P_{i}=v_{g i}\left(G_{i}-\alpha_{i}-\gamma_{i}\right) P_{i}+\dot{P}_{i}^{\text {spont }} . \tag{1.43}
\end{equation*}
$$

The modal group velocity $v_{g i}=c / n_{g i}$ can be specified by the user via the modal group index $n_{g i}$. The net gain of the mode traveling along the cavity is calculated as

$$
\begin{equation*}
G_{i}=\int\left(g-\alpha_{b}\right)\left|\Phi_{i}\right|^{2} \mathrm{~d} x \mathrm{~d} y . \tag{1.4}
\end{equation*}
$$

Models for the optical background losses $\alpha_{b}$ are described in Section 2.8 on page 81. $\alpha_{i}$ are possible additional losses (for example by scattering into radiation modes), that do not contribute to heating. In addition, outcoupling losses of a Fabry-Perot (FP) laser with facet reflectivities $R_{i}(0)$ on the left facet $(z=0)$ and $R_{i}(L)$ on the right facet $(z=L)$ are included,

$$
\begin{equation*}
\gamma_{i}=-\frac{1}{L} \log \left(R_{i}(0) R_{i}(L)\right) . \tag{1.45}
\end{equation*}
$$

DFB lasers can be treated as FP lasers with appropriate reflectivities. The rate of spontaneous emission into transverse mode $i$ is modeled as

$$
\begin{equation*}
\dot{P}_{i}^{\text {spont }}=K_{i} \hbar \omega_{i} \frac{v_{g i}}{L} \int\left[1-\exp \left(\frac{\hbar \omega-e U_{F}}{k T}\right)\right]^{-1} v_{g i} g(\hbar \omega)\left|\Phi_{i}\right|^{2} \mathrm{~d} x \mathrm{~d} y . \tag{1.46}
\end{equation*}
$$

$K_{i}$ is a correcture (e.g. Petermann factor), that can be specified by the user (parameter PEFA). $L$ is the laser length.
The following calculated powers are written to the terminal in mW : total internal power $P_{1}+P_{2}$ (named Power), internal power ratio $\eta=\frac{P_{1}-P_{2}}{P_{1}+P_{2}}$ (named eta), output power $\operatorname{Pout}(i, 0)$ of each mode $i$ at facet $z=0$, modal output powers $\operatorname{Pout}(i, \mathrm{~L})$ at facet $z=L$, where
$\operatorname{Pout}(i, 0)=\frac{\rho}{1+\xi} P_{i} \quad$ and $\quad \operatorname{Pout}(i, \mathrm{~L})=\frac{\xi \rho}{1+\xi} P_{i} . \quad\left\{\begin{array}{c}\rho=-\ln \left(\sqrt{R_{i}(0) R_{i}(L)}\right) \\ \xi=\frac{1-R_{i}(L)}{1-R_{i}(0)} \sqrt{\frac{R_{i}(0)}{R_{l}}}\end{array}\right.$

### 1.5.3 Treating Powers as Parameters (TPP)

Another approach enabled in WIAS-TeSCA provides data for a quasi-3D treatment of edge-emitting semiconductor lasers in the stationary case (see e.g. [WBW93]) Suppose the currents flow only transversely, the status of a transverse cross section does not explicitely depend on the longitudinal position $z$, but only implicitely via the powers $P_{i}(z)$. The letter ones can be used as transverse-longitudinal separation parameters. To this purpose, WIAS-TeSCA solves the transverse transport and wave equations for an externally given series of powers and stores quantities like modal gain $G_{i}$ in tabular form. Postprocessing programs for the longitudinal propagation (not incorporated in WIAS-TeSCA) can determine e.g. the local modal gain without rerunning WIAS-TeSCA by interpolation in these tables. More details and the input parameters will be described further below on page 82 .

## 2 Simulations with TeSCA

Simulations with WIAS-TeSCA are either controlled by a script file (DIO file) or/and directly by the user on a command line.
A simulation consists of several commands that define e.g. the material properties, control the graphic output, or start the computation. All WIAS-TeSCA commands are listed in Table 2.1.

| Command | Short description |
| :---: | :---: |
| break | Sets break point i |
| device | Fundamental values for the semiconductor device, such as temperature, scaling and symmetry factors, relative dielectric permittivity, etc., can be entered |
| energy | Sets parameters for energy transport model described in Section 1.2 |
| fermi | Sets parameters for carrier statistics, e.g. conduction and valence band edges for Boltzmann or Fermi case, and optical parameters for the simulation of optoelectronic devices |
| graphic | Specifies and controls graphical output |
| grid | Defines computational domain, i.e. triangulation and boundary conditions |
| load | Reads WIAS-TeSCA save files from previous simulations and loads analytical profiles or interpolates profiles from external meshes |
| mobility | Sets parameters for intrinsic density and carrier mobility models |
| numeric | Used to define the accuracy and termination parameters required for the numerical calculations |
| recombination | Defines the parameters for the generation-recombination processes |
| save | Used to write output files for subsequent evaluation or continuation of the simulation or offline coupling to other simulation tools |
| special | Describes physical effects not covered by the standard model |
| step | Defines external bias, step control parameters, and time intervals for transient simulations. Solution of drift-diffusion system is calculated, printed (to the terminal) and saved |
| substrate | Used to initialize the layer system |
| title | Sets title of simulation and allocates memory for computation |
| use | Switch from DIOS process simulation to WIAS-TeSCA device simulation. |

Table 2.1: Main WIAS-TeSCA commands in alphabetical order
In the subsequent sections all commands are thoroughly discussed. Parameters without comments are special ones, useable by the developers, only.

### 2.1 DIO script files

Comments in DIO files have to be preceded by an exclamation mark

```
! This is a comment
```

It is possible to split the DIO file into many separate files, which are then included into the main DIO file using the command, viz.

```
! main.dio
```

@file1.dio !include file1.dio
@file2.dio !include file2.dio

### 2.2 Device command

With the use of the DEvice-command fundamental values for the semiconductor device can be entered. Moreover, using the DEvice-command, an internal scaling of all physical parameters is done.

### 2.2.1 Cylindrical symmetry

WIAS-TeSCA is able to treat problems that have cylindrical symmetry. If the parameter IZYLIN1 is set, the y-axis will be interpreted as cylindrical axis and the x-coordinate will be utilized as radius. In this case, the parameter ZAUS which usually specifies the extension of the device in the third dimension has no impact.

### 2.2.2 Comments

During the execution of the DEvice-command, the validity of all parameters is tested.

These physical parameters are: The temperature TEMP, the intrinsic density ENI, the dielectric constant for the substrate EPSSI, the extension of the device in $z$ direction ZAUS and the explicit specification of the time scaling TSkal. All given parameters have default values.
For the treatment of heterostructures (devices with different materials), the device can be partitioned in up to 55 zones (sub-regions) using the DOMAIN-command. This is a possibility to consider spatial varying values of intrinsic density, dielectric constant and basic mobilities. Moreover, the Fermi level - constant in every zone - can be given. For this purpose values for ENIFA, EPSSI, AMUNFA, AMUPFA, PHIN and PHIP have to be entered. In this case the calculation will be performed, with the parameters ENIFA(i)*ENI, EPSSI(i), AMUNFA(i)*AMUNO, AMUPFA(i)*AMUPO, $\operatorname{PHIN}(i)$ and PHIP(i) in the zone with index $i$.

If ENIFA(i)=0, the $i$-th zone is understood as oxid. In such zones, the Laplace equation (Poisson equation with vanishing right hand side) is solved. However,
if $\operatorname{FADOOX}=1$, in oxid-zones the doping is considered, whereas the mobile charge carriers are set to zero.
A zonally constant interface charge QSSIOX (i) between the semiconducter and oxid layers can be taken into account.
More general, it is possible to consider surface charges along interfaces.

### 2.2.3 Scaling

Units of Measurement and Scaling:
All physical values, entered as a parameter and can be changed, subject to an internal scaling in the following way:

```
entered value = internal value * scale factor
internal value = entered value / scale factor
```

The scaling factors are calulated internally during the execution of the DEvicecommand and depend on temperature, intrinsic density and dielectric constant. The user has to note the unities of the physical parameters used in WIAS-TeSCA. This is the CGS system. By way of derogation from the CGS system in the mobility model, incoming energies are specified in eV (electron volts).
The following constants are used:

$$
\begin{array}{ll}
\text { vacuum permittivity } & \varepsilon_{0}=8.85419 \cdot 10^{-14} \frac{A s}{V / m} \\
\text { Boltzmann constant } & k_{\mathrm{B}}=1.380662 \cdot 10^{-23} \frac{\mathrm{HAs}^{-}}{K} \\
\text { elementary charge } & q=1.6021 \cdot 10^{-19} \mathrm{As}
\end{array}
$$

A display of the values of the scaling factors is possible by using the commands PRINT.

### 2.2.4 Parameters

| name | unit <br> type <br> option | default | comment |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| AC() | real $[s / \Omega]$ | $0 . d 0$ | capacity on <br> Length $\leq$ mdiri | contact, |  |
| AL() | real $[\Omega \cdot s]$ | $0 . \mathrm{do}$ | inductivity on <br> Length $\leq$ mdiri | contact, |  |
| AR() | real $[\Omega]$ | $0 . \mathrm{do}$ | resistance on <br> Length $\leq$ mdiri | contact, |  |
|  |  |  | continued on next page |  |  |



| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| ENi | real $\left[\mathrm{cm}^{-3}\right]$ | rundef | intrinsic density (constant part) |
| ENIFA() | real | 1.d0 | factor for the space-dependent intrinsic density Length $\leq$ mreg |
| EPSOx () | real | 3.8d0 | relative permittivity constant of the oxide at the gate contacts Length $\leq$ mnatur |
| EPSSi () | real | 11.67 do | relative permittivity constant of the substrate (Si) Length $\leq$ mreg |
| Execute | real | 0.d0 | toggle on/off the execution and, therefore, the tests of the values and the automatic calculation of the scaling. |
| FADOOX |  | 0. | cancellation factor for the oxide doping |
| GAbez | AN | GATE | names of the gate contacts (natural boundary conditions) |
| Ger () | real [V] | 0.d0 | Length $\leq 10$ |
| GNR() | real $\left[\mathrm{cm}^{-2}\right]$ | 0.d0 | Length $\leq 10$ |
| GSN() | real | 0.d0 | Length $\leq 10$ |
| GSP() | real | 0.d0 | Length $\leq 10$ |
| GEN() | real | 1.d0 | Length $\leq 10$ |
| GEP() | real | 1.d0 | Length $\leq 10$ |
| IAZPQ | integer | 0 | number of zone pairs for interface charge |
| IBulk | integer | 0 | number of the contact with resistance |
| ICap | integer | 0 | number of the contact with capacity |
| ICLR | integer | 0 | outer current control |
| continued on next page |  |  |  |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| IDiri | integer | 0 | number of Dirichlet-contacts |
| IGRenz | integer | 0 | traps on boundary |
| INatur | integer | 0 | number of Gate-contacts |
| IPERio | integer | 0 | periodic boundary conditions |
| ISPAN() | integer | 0 | Length $\leq 5$ |
| ISTROM() | integer | 0 | Length $\leq 5$ |
| IZPQ() | integer | 0 | indices of zone pairs for interface charge, Length $\leq 2 *$ IAZPQ |
| IZYlin | integer | 0 | switch for cylindrical symmetry |
| KAC() | integer | 1 | Length $\leq 15$ |
| KADI | integer | 0 | number of Dirichlet boundary parts |
| KANA | integer | 0 | number of Gate boundary parts |
| MDiri | integer | 20 | max. number of Dirichlet boundary parts |
| MNatur | integer | 10 | max. number of Gate boundary parts |
| Odi () | real [cm] | 35.d-7 | Length $\leq$ mnatur |
| PHIN() | real [V] | 0.d0 | quasi-Fermi potential for electron, Length $\leq$ mreg |
| PHIP() | real [V] | 0.d0 | quasi-Fermi potential for holes, Length $\leq$ mreg |
| Qss () | real $\left[\mathrm{cm}^{-2}\right]$ | 0.d0 | surface state density at the gate contacts, Length $\leq m n a t u r$ |
| QSSIox () | real $\left[\mathrm{cm}^{-2}\right]$ | 0.d0 | surface state density at the gate contacts, Length $\leq$ mreg |
| QZP () | real $\left[\mathrm{cm}^{-2}\right]$ | 0.d0 | interface charge, Length $\leq$ IAZPQ |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| RAB | real [ $\Omega$ ] | $0 . \mathrm{d} 0$ | resistance at the contact IBULK |
| SPULE | real [ $\Omega$ ] | $0 . \mathrm{d} 0$ | inductivity on contact IBULK |
| TEmp | real [K] | 300 | temperature |
| TSkal | real [s] | rundef | timescale |
| Ukonga() | real [V] | 0.55d0 | contact voltages at the gate contacts, Length $\leq$ mnatur |
| Xskal | real [cm] | rundef | internal length scale |
| Zaus | real [cm] | $1 \mathrm{~d}-4$ | length of the device in the z direction |
| ZAUSFA () | real | 1.d0 | Length $\leq$ mreg |
| SYMfak | real | 1.d0 | symmetry factor |

### 2.3 Break command

The break command is used to define a break point in the processing of a DIO script file. At this point the execution of the script is stopped and the user can enter commands in the interactive mode e.g. to change the graphical output. The execution of the script can be resumed by typing GO in the interactive mode.

### 2.4 Title command

The command TITle has to precede each WIAS-TeSCA simulation. In the command the problem size can be specified. Memory is allocated and deallocated during the simulation using the specified maximum values.
By default no memory limitations are defined, i.e. the program automatically reallocates memory if this is required by refinement of the mesh of the layer system or during the delaunization of the mesh. It might be useful to restrict the number of nodes in the grid adaptation or to allocate a fixed small amount of memory on machines with small main memory resources or to initially allocate a large amount of memory if the problem is known to be huge.

### 2.4.1 Parameters

| parameter name | unit <br> type <br> options | default <br> value | comment |
| :---: | :---: | :---: | :---: |
| Title | string*80 | blank | title line for the simulation. |
| MAXV | integer | undefined | Maximum node number of vertices in the triangle tree. Refinement is stopped if the new mesh would have more mesh points. MAXV can be specified to limit the memory growth on small machines. |
| MAXVDelaun | y $\mathbf{y}$ teger | undefined | Maximum total number of nodes. Specifying this value might turn o the delaunization of the mesh This is not recommended. It is recommended to specify MAXV only. |
| MPOINTS | integer | 10000 | Initially allocated number of points in the layer system. This number is increased internally if required. |
| MXT | integer | 2000 | Initially allocated number of triangles in the user triangulation. Increased internally if necessary. |
| MAXT | integer | 0 | Maximum number of triangles in the triangle tree. Refinement is stopped if the new tree would exceed MAXT. Internal default 4/3MAXV. |
| MAXUTR | integer | 0 | Initial maximum number of triangles and boundaries in the final UTRI-grid. |
| MAXL | integer | 0 | Internal Switch. The max. number of multigrid levels in the ITRI grid. |

continued on next page

| name unit <br> type <br> option default |  |  |  |
| :--- | :--- | :--- | :--- |
| INFO | integer | 0 | controls the default printed <br> output on the terminal $(0,1$, <br> $2, \ldots)$. |
| PRInt | integer | 0 | controls the default printed <br> output into the protocol file $(0$, <br> $1,2, \ldots)$. |

### 2.5 Energy command

In WIAS-TeSCA the heat equation is implemented. It can be solved simultaneously with the continuity equations and the optical equation. In (1.24) $C$ is the heat capacity and $\kappa$ is the thermal conductivity.
As usual, temperature-depending parameters are normalized with respect to the room temperature $T_{0}=300 \mathrm{~K}$. In some formulas, the reduced temperature $t=T / T_{0}$ is used.

The heat capacity $C=$ HEATFA (default $=1$, zonewise) can be specified by the user.

The thermal conductivity depends on temperature according to the formula

$$
\begin{equation*}
\kappa(T)=\kappa \cdot T^{\gamma} \tag{2.1}
\end{equation*}
$$

The avalanche generation is temperature dependent according to the formulas

$$
\begin{align*}
R_{a v a} & =-\alpha_{n} \frac{j_{n}}{q}-\alpha_{p} \frac{j_{p}}{q}  \tag{2.2}\\
\alpha_{n, p} & =\alpha_{n, p}^{0} \exp \left(-\frac{\beta_{n, p}}{E}\right)  \tag{2.3}\\
\alpha_{n, p}^{0} & =\alpha_{n, p}^{0}\left(1+\alpha_{n, p}^{1}(t-1)(t+1)\right)  \tag{2.4}\\
\beta_{n, p} & =\beta_{n, p}^{0}\left(1+\beta_{n, p}^{1}(t-1)(t+1)\right) \tag{2.5}
\end{align*}
$$

The parameters $\alpha$ and $\beta$ depend on energy for the holes and differ for $E<E_{0}$ and $E>E_{0}$ for a user given $E_{0}$.

| variable | TeSCA-name | Proc | default | Stift |
| :--- | :--- | :--- | :--- | :--- |
| $\alpha_{n}^{0}$ | AVA1 | RECOMB | 1.00 d 6 | 7.00 d 5 |
| $\beta_{n}^{0}$ | AVA2 | RECOMB | 1.66 d 6 | 1.23 d 6 |
| $\alpha_{p}^{0}, E<E_{0}$ | AVA3 | RECOMB | 1.582 d 6 | 1.58 d 6 |
| $\beta_{p}^{0}, E<E_{0}$ | AVA4 | RECOMB | 2.036 d 6 | 2.04 d 6 |
| $\alpha_{p}^{0}, E>E_{0}$ | AVA5 | RECOMB | 6.71 d 5 | 1.58 d 6 |
| $\beta_{p}^{0}, E>E_{0}$ | AVA6 | RECOMB | 1.693 d 6 | 2.04 d 6 |
| $E_{0}$ | AVA7 | RECOMB | $4 . \mathrm{d} 5$ | $4 . \mathrm{d} 5$ |
| $\alpha_{n}^{1}$ | AVAT1 | ENERGY | 0.0 d 0 | 0.43 d 0 |
| $\beta_{n}^{1}$ | AVAT2 | ENERGY | 0.0 d 0 | 0.375 d 0 |
| $\alpha_{p}^{1}, E<E_{0}$ | AVAT3 | ENERGY | 0.0 d 0 | 0.42 d 0 |
| $\beta_{p}^{1}, E<E_{0}$ | AVAT4 | ENERGY | 0.0 d 0 | 0.33 d 0 |
| $\alpha_{p}^{1}, E>E_{0}$ | AVAT5 | ENERGY | 0.0 d 0 | 0.42 d 0 |
| $\beta_{p}^{1}, E>E_{0}$ | AVAT6 | ENERGY | $0.0 d 0$ | 0.33 d 0 |

Stift are the values used in the thesis of Martin Stiftinger. They differ even for $T=T_{0}$ from the WIAS-TeSCA defaults.

The Auger recombination is temperature dependent according to the formulas

$$
\begin{align*}
& R_{\text {aug }}=\left(C_{n}^{\text {aug }} n+C_{p}^{\text {aug }} p\right)\left(n p-n_{i}^{2}\right)  \tag{2.6}\\
& C_{n}^{\text {aug }}=C_{n}^{0}\left(T / E_{n}\right)^{\gamma_{n}}\left(e^{E_{n} / T_{0}-E_{n} / T}\right)  \tag{2.7}\\
& C_{p}^{\text {aug }}=C_{p}^{0}\left(T / E_{p}\right)^{\gamma_{p}}\left(e^{E_{p} / T_{0}-E_{p} / T}\right) \tag{2.8}
\end{align*}
$$

| variable | TeSCA-name | Proc | default |
| :--- | :--- | :--- | :--- |
| $C_{n}^{0}$ | AUGN | RECOMB | $2.8 d-31$ |
| $\gamma_{n}$ | AUGNGAM | ENERGY | 0.0 d 0 |
| $E_{n}$ | EAN | ENERGY | 0.1 d 0 |
| $C_{p}^{0}$ | AUGP | RECOMB | $9.9 \mathrm{~d}-32$ |
| $\gamma_{p}$ | AUGPGAM | ENERGY | 0.0 d 0 |
| $E_{p}$ | EAP | ENERGY | 0.1 d 0 |

The radiant or optical recombination is temperature dependent according to the formulas

$$
\begin{equation*}
R_{o p t}=C^{0} T^{\gamma} \tag{2.9}
\end{equation*}
$$

| variable | TeSCA-name | Proc | default |
| :--- | :--- | :--- | :--- |
| $C^{0}$ | AUGB | RECOMB | 0. d0 |
| $\gamma$ | AUGBGAM | ENERGY | 1.5 d 0 |

The Shockley - Read - Hall - recombination is temperature dependent according to the formulas

$$
\begin{align*}
R_{s r h} & =\frac{n p-n_{i}^{2}}{\tau_{p}\left(n+n_{1}\right)+\tau_{n}\left(p+p_{1}\right)}  \tag{2.10}\\
\frac{1}{\tau_{n}} & =\frac{1}{t^{\gamma_{n}}}\left(\frac{1}{\tau_{n}^{0} \tau_{n}^{1}}+C_{n}^{s r h} D\right)+\frac{1}{t^{\delta_{n}}} C_{n} p^{2}  \tag{2.11}\\
\frac{1}{\tau_{p}} & =\frac{1}{t^{\gamma_{p}}}\left(\frac{1}{\tau_{p}^{0} \tau_{p}^{1}}+C_{p}^{s r h} D\right)+\frac{1}{t^{\delta_{p}}} C_{p} n^{2} \tag{2.12}
\end{align*}
$$

| variable | TeSCA-name | Proc | default | remark |
| :--- | :--- | :--- | :--- | :--- |
| $n_{1}$ | REN | RECOMB | 1.09 d 10 |  |
| $\tau_{n}^{0}$ | TAUN0 | RECOMB | $2 \mathrm{~d}-4$ |  |
| $\tau_{n}^{1}$ | TAUNFA | RECOMB | $1 . \mathrm{d} 0$ | zone-depend. |
| $C_{n}^{s r h}$ | CSRHN | RECOMB | $0 . \mathrm{d} 0$ |  |
| $C_{n}$ | CAUGN | RECOMB | $0 . \mathrm{d} 0$ |  |
| $\gamma_{n}$ | GAMMAN | RECOMB | $0 . \mathrm{d} 0$ |  |
| $\delta_{n}$ | DELTAN | RECOMB | $0 . \mathrm{d} 0$ |  |
| $p_{1}$ | REP | RECOMB | 1.09 d 10 |  |
| $\tau_{p}^{0}$ | TAUP0 | RECOMB | $2 \mathrm{~d}-6$ |  |
| $\tau_{p}^{1}$ | TAUPFA | RECOMB | $1 . \mathrm{d} 0$ | zone-depend. |
| $C_{p}^{\text {srh }}$ | CSRHP | RECOMB | $0 . \mathrm{d} 0$ |  |
| $C_{p}$ | CAUGP | RECOMB | $0 . \mathrm{d} 0$ |  |
| $\gamma_{p}$ | GAMMAP | RECOMB | $0 . \mathrm{d} 0$ |  |
| $\delta_{p}$ | DELTAP | RECOMB | $0 . d 0$ |  |

The refractive index is temperature dependent according to the formulas

$$
\begin{align*}
& n(T)=\left(n\left(T_{0}\right)-n_{d}(n+p) / 2\right)+n_{T}\left(T-T_{0}\right), \quad \text { typ }=0  \tag{2.13}\\
& n(T)=\left(n\left(T_{0}\right)-n_{d}\left(n+p-\left|D_{\text {net }}\right|\right) / 2\right)+n_{T}\left(T-T_{0}\right), \quad \text { typ }=1  \tag{2.14}\\
& n(T)=n\left(T_{0}\right)+n_{T}\left(T-T_{0}\right), \quad \text { typ }=\ldots \tag{2.15}
\end{align*}
$$

| variable | TeSCA-name | Proc | default | remark |
| :--- | :--- | :--- | :--- | :--- |
| $n\left(T_{0}\right)$ | BRE | FERMI | $1 . \mathrm{d} 0$ |  |
| $n_{d}$ | BREFAK | FERMI | $1 \mathrm{~d}-19$ | zone-depend. |
| $n_{T}$ | BREA | ENERGY | $6.8 \mathrm{~d}-4$ |  |
| typ | BRETYP | FERMI | 0 | model type |

The transverse optical losses $\alpha_{t}$ in the bulk laser are composed of the free carriers absorption ( $f_{c n}$ and $f_{c p}$ ) and the inter valence band absorption $\alpha$. We have

$$
\begin{align*}
\alpha_{t} & =\alpha(T)+f_{c n}(T) n+f_{c p}(T) p  \tag{2.16}\\
\alpha(T) & =\alpha_{0} \alpha_{1}\left(e^{E_{0} / T_{0}-E_{0} / T}\right)  \tag{2.17}\\
f_{c n}(T) & =f_{c n 0} T^{\gamma_{n}}  \tag{2.18}\\
f_{c p}(T) & =f_{c p 0} T^{\gamma_{p}} \tag{2.19}
\end{align*}
$$

| variable | TeSCA-name | Proc | default | remark |
| :--- | :--- | :--- | :--- | :--- |
| $\alpha_{0}$ | AALPHA | FERMI | 1 d 4 |  |
| $\alpha_{1}$ | AALPHF | FERMI | 1 d 0 | zone-depend. |
| $E_{0}$ | EA | FERMI | 0.1 d 0 |  |
| $f_{c n 0}$ | FCNALF | FERMI | 0d0 |  |
| $\gamma_{n}$ | GN | MOBILITY | 2.33 d 0 |  |
| $f_{c p 0}$ | FCPALF | FERMI | 0d0 |  |
| $\gamma_{p}$ | GP | MOBILITY | $2.33 d 0$ |  |

### 2.5.1 Parameters

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| IEnergy | integer | -1 |  |
| BOUnd | real | $5 . \mathrm{d0}$ |  |
| CONDuc ( $)$ | real $\left[\mathrm{cm}^{6} / \mathrm{s}\right]$ | $0 . \mathrm{d} 0$ | Length $\leq 20$ |
| EPS1 | real | $1 \mathrm{~d}-4$ |  |
| EPS | real | $1 \mathrm{~d}-5$ |  |
| EPTemp | real | $1 \mathrm{~d}-2$ |  |
| EREL | real $[\mathrm{cm}]$ | $9 \mathrm{~d}-7$ |  |
| ERLO | real $[\mathrm{cm}]$ | $9 \mathrm{~d}-7$ |  |
| HEATFA( $)$ | real | $1 . \mathrm{d0}$ |  |
| HETERO | integer | 0 |  |
| IHO | integer | 3 | capacity, Length $\leq$ mreg |
| ITAU | integer | 2 |  |
| ITEMO | integer | 0 | continued on next page |
|  |  |  |  |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| ITEMP | integer | 0 |  |
| ITIN | integer | 3 |  |
| Joule | integer | 0 |  |
| KATE | integer | 0 |  |
| MODel | integer | 1 |  |
| MTemp | integer | 20 |  |
| RANDDI() | real [cm] | 1d-4 | Length $\leq 20$ |
| SIKO | real | 0.03 d 0 |  |
| SIK1 | real | 0.00156 d 0 |  |
| SIK2 | real | 1.65d-6 |  |
| TKN | real | 2.5 d 0 |  |
| TKP | real | 2.5 d 0 |  |
| SIW | real | 1.636584 d 0 |  |
| TEMPScal | real | $300 . d 0$ |  |
| EGA | real | 2.73d-4 |  |
| EA | real | 0.1 d 0 |  |
| BREA | real | 6.8d-4 | $n_{T}$ in formulas (2.13-2.15) |
| AUGBGam | real | 1.5 d 0 | $\gamma$ in formula (2.9) |
| AUGNGam | real | 0.0d0 | $\gamma_{n}$ in formula (2.7) |
| AUGPGam | real | 0.0 d 0 | $\gamma_{p}$ in formula (2.8) |
| EAN | real | 0.1 do | $E_{n}$ in formula (2.7) |
| EAP | real | 0.1 do | $E_{p}$ in formula (2.8) |
| AVAT1 | real | 0.d0 | See formulas (2.2-2.5) |
| AVAT2 | real | 0.d0 | See formulas (2.2-2.5) |
| AVAT3 | real | 0.d0 | See formulas (2.2-2.5) |
| AVAT4 | real | 0.d0 | See formulas (2.2-2.5) |
| AVAT5 | real | 0.d0 | See formulas (2.2-2.5) |
| AVAT6 | real | 0.d0 | See formulas (2.2-2.5) |
| continued on next page |  |  |  |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| TEBIas () | real | $300 . \mathrm{d0}$ | Length $\leq 100$ |
| TLOwboun | real | $0.25 \mathrm{d0}$ |  |
| TUPbound | real | $5 . \mathrm{d0}$ |  |
| WLEIFA () | real $\left[\mathrm{cm}^{6} / \mathrm{s}\right]$ | $1 . \mathrm{d0}$ | $\kappa$ in formula $(2.1)$ <br> Length $\leq \mathrm{mreg}$ |
| WLEX | real | $-1.33 \mathrm{d0}$ | $\gamma$ in formula $(2.1)$ |
| ZUSatz | real | $5 . \mathrm{d}-2$ |  |

### 2.6 Grid command

The GRID command is used to generate an initial triangulation and to do a first refinement of this grid. The GRID command has to be executed before defining the substrate area. In WIAS-TeSCA there are different triangulation types, that can be used to triangulate simple geometrical areas (rectangles, trapezoids, etc.) Two triangulation types are preferred: $\mathrm{TYPe}=\mathrm{Def}$ ault and $\mathrm{TYPe}=1 \mathrm{D}$.

### 2.6.1 Default Grid

```
GRID(XLeft=..., XRight=..., YBottom=..., YTop=..., TYPe=Default,
    NX=..., DX=..., CONTrol(MAXTRl=...))
```

The rectangle [XLeft, XRight] $\times$ [YBottom, YTop] is tessellated into equilateral triangles each having a horizontal edge. Exceptionaly, at the right and the left side of the rectangle right-angled triangles are used.

The number NX of the triangles along the surface (XLeft, XRight) can be prescribed. Otherwise it is computed from the minimum edge length in the finest grid DX and the number of the refinement levels MAXTRI(from the parameter record CONTrol, see 2.13, p 98). YBottom is eventually reduced in order to choose equilateral triangles. If a new user grid is generated after a few processing steps, by default the extensions of the layer system are used for expanding the grid.

### 2.6.2 1D-Grid

$$
\begin{gathered}
\operatorname{GRID}(\operatorname{TYPe}=1 D, X=(\ldots), \quad Y=(\ldots), N X=(\ldots), D X=(\ldots), N Y=(\ldots), \\
\operatorname{DY}=(\ldots),)
\end{gathered}
$$

A triangulation is generated, which might have only one vertical stripe of rectangles inhomogeneously subdivided in vertical direction. Each of the rectangles is
split into two triangles. On these grids 1D-simulations can be done with a minimum overhead. The mesh refinement usually applied in WIAS-TeSCA is inappropriate for a 1D simulation. One may either turn off any refinement

```
REPLace(CONTrol(MAXTRI=1))
```

or do a special 1D-refinement, using:

```
REPLace(CONTrol(1D=on))
```

The vectors X and Y define reference points in the grid. Equidistant subdivisions between the reference values are applied. Either the number of subdivisions NX, NY or the step sizes DX DY can be prescribed. The sign of NX and NY defines, which of the diagonals is used to split the rectangles into two triangles. This allows to construct a symmetric initial grid. The vertical spacing can also be read from a 1D cross section file:

If contained in the file, also the 1D layer structure is read. It is saved temporarily and can be used in the SUBStrate command. Saving the structure in TESIM-4 provides the required file content. If a 1D grid adaptation is desired, one can use the default grid and the switch REPLace (CONTrol(1D=on)). First the usual grid adaptation is done and after that a 1D-grid is constructed, using only the nodes at the left side of the domain.

### 2.6.3 Boundary condition types

The GRID-command is used also, to define the types of boundary conditions (contacts) on the outer boundary of the triangulation domain. This is used to define boundary conditions for the monolayer diffusion NEWDIFf=0. The main application is the definition of the contacts for the device simulation with WIAS-TeSCA.

The following conditions are used for process simulation in WIAS-TeSCA: typ... $=1$ homogeneous Neumann conditions (default type), > 1 inhomogeneous Neumann conditions (default at substrate surface), $<0$ Dirichlet conditions.

To define the contacts for a device simulation with WIAS-TeSCA a new default type of boundary conditions must be defined TYPEO=999(symmetry conditions, homogeneous Neumann condition).
The types of boundary conditions is prescribed by the WIAS-TeSCA-conventions: typ $\ldots=999$ symmetry conditions (default type) $>0$ Gate contact (increasing from 1) $<0$ Metal contact (decreasing from -1)
In addition, optical or thermal contacts can be defined on the outer contour of the grid. The following rule is applied: type $=\operatorname{sign}(e l) \cdot 100 \cdot$ opt $+\|e l\|$ where el denotes the index of the electrical contact(or 0 ) and opt $\geq 0$ denotes the index of the thermal or optical contact.

For FERMI (ISPec=0) the optical contacts are not used and for ENergy (IEnergy=-1) the thermal contacts are not used. There is no way of specifying different optical and thermal contacts in the same device.

All contacts of the device have to be numbered contiguously, i.e. $-1,-2, \cdots,-10$ for the metal contacts, $-1,-2, \cdots,-5$ for the gate contacts and $1,2, \cdots, 20$ for optical and thermal contacts.

The names of the contacts can not be specified in the Grid command. They can be defined in the Use or Device commands.

If the initial triangulation is of complicate shape, the definition of the boundary conditions should (must) be supported by the (approximate) location of the starting and end points on the boundary of the triangulation. The node in the User-grid, closest to one of the given points, is used as start or end point of the contact.
(XRT, YRT), (XLT, YLT) , (XLB, YLB) (XRB, YRB)

$$
\begin{gathered}
\operatorname{GRID}(\ldots \mathrm{BCtyp}(\mathrm{TYPE} 0=\ldots, \mathrm{NAME} 1=\ldots, \mathrm{TYPE} 1=\ldots, \mathrm{XB} 1=\ldots, \mathrm{YB} 1=\ldots, \\
\mathrm{XE}=\ldots, \mathrm{YE}=\ldots,)
\end{gathered}
$$

Note! The first and second end point of the contacts are defined such that moving from the first to the last, the aouter boundary of the simulation domain is traversed in positive direction ( i.e. COUNTERclockwise!!!!).

Note! Instead of using the GRID command the USE command should be preferred for the definition of boundary conditions (see 2.20, p. 135).

### 2.6.4 Parameters

| parameter <br> name | unit <br> type <br> options | default value | comment |
| :---: | :---: | :---: | :---: |
| Y | real $[\mu \mathrm{m}]$ | 0 . | Vector of coordinates for the definition of the vertical discretization of a "1D" grid. If more than 2 elements of the vector are specified, $\mathrm{TYPe}=1 \mathrm{D}$ is assumed automatically. For TYPe=Default the vertical extension of the grid can be defined by the first two values of this vector. Unlike YBottom the exact values are used but only nearly equilateral triangles are produced. |
| DY | Distance | undefined | Vector of stepsizes between each pair of Y-values for TYPe=1D. |
| NY | integer | 1 | Vector of the numbers of subintervals between each pair of Yvalues for $\mathrm{TYPe}=1 \mathrm{D}$. |
| X | real | 0. | Vector of coordinates for the definition of the lateral extension of a "1D" grid. For TYPe=Default the lateral extension of the grid can be defined by the first two values of this vector. |
| NX | integer | 1 | number of user triangles at the top edge for TYpe=Default vector of the numbers of subintervals between each pair of X -values for TYPe=1D. number of nodes for TYPe=4Triangle,2Triangle. |

continued on next page

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| DX | real | undefined | Vector of stepsizes between <br> each pair of X-values for <br> TYPe=1D Minimum edge length <br> for TYPe=Default DX and <br> ConTrol MAXTRI define the <br> number of user triangles NX at <br> the top side of the user grid. |
| YLeft | real $[\mu \mathrm{m}]$ | -1. | left end of the top line |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| GLUE1 | integer | 0 | Boundary type of the first grid, which is used for manipulations. GRid=Add: select all nodes for the given boundary type GRid=Glue: merge the nodes on the given boundary type with nodes from the second grid. |
| GLUE2 | integer | 0 | boundary type of the second grid, which is used for manipulations. GRid=Glue: merge the nodes on the given boundary type with nodes from the first grid. |
| Filein | string*80 | undefined | name of the input file, if one is required |
| DOMfile | boolean | off | controls the output of the triangulation into a file |
| FILEOut | string*80 | undefined | name of output file |
| SIDEfac | real | 0.5 | Width of a boundary triangle for comTYPe=Default compared to internal triangles. For SIDEfac=0.5, right angled triangles at the left and right sides are assumed. For SIDEFAC=1, all triangles in a row have the same size. |
| MATerial | record | undefined | List of material names for the selection of triangles |
| BC |  |  | data record to define boundary conditions (contacts) $\leq 15$ |
| TYPE1 | integer |  | type of the first contact |
| XB1 | real $[\mu \mathrm{m}]$ |  | lateral position of the start point of the first contact. |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| YB1 | real [ $\mu \mathrm{m}$ ] |  | vertical position of the start point of the first contact. |
| XE1 | real $[\mu \mathrm{m}]$ |  | lateral position of the end point of the first contact. |
| YE1 | real $[\mu \mathrm{m}]$ |  | vertical position of the end point of the first contact. |
| TYPEO | integer | 1 | default type of the boundary conditions. Note! For WIAS-TeSCA , TYPO=999. |
| XRT | real $[\mu \mathrm{m}]$ |  | approximate lateral position of the right top corner of the simulation domain. If not specified, the maximum lateral coordinate of all nodes $x \max$ is used. |
| YRT | real $[\mu \mathrm{m}]$ |  | approximate vertical position of the right top corner of the simulation domain. If not specified, the maximum vertical coordinate of all nodes ymax is used. |
| XLT | real $[\mu \mathrm{m}]$ |  | approximate lateral position of the left top corner of the simulation domain. If not specified, the minimum lateral coordinate of all nodes xmin is used. |
| YLT | real $[\mu \mathrm{m}]$ |  | approximate vertical position of the left top corner of the simulation domain. If not specified, then set to ymax . |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| XLB | real [ $\mu \mathrm{m}$ ] |  | approximate lateral position of the left bottom corner of the simulation domain. If not specified, then set to $x$ min . |
| YLB | real $[\mu \mathrm{m}]$ |  | approximate vertical position of the left bottom corner of the simulation domain. If not specified, the minimum vertical coordinate of all nodes ymin is used. |
| XRB | real $[\mu \mathrm{m}]$ |  | approximate lateral position of the right bottom corner of the simulation domain. If not specified, then set to $x \max$. |
| YRB | $\operatorname{real}[\mu \mathrm{m}]$ |  | approximate vertical position of the right bottom corner of the simulation domain. If not specified, then set to ymin . |
| ) |  |  | end of record BC |
| BCLeft | integer | 1 | type of boundary condition at the left side of the triangulation. In WIAS-TeSCA: 1:Hom.Neumann, -2:1D-Dcontinuation. |
| BCRight | integer | 1 | type of boundary condition at the right side of the triangulation. In WIAS-TeSCA:1 Hom. Neumann, $-2: 1 \quad$ Dcontinuation. |
| BCBottom | integer | 1 | type of boundary condition at the bottom side of the triangulation. In WIAS-TeSCA: 1:Hom.Neumann, -3 no modification during diffusion |

continued on next page

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| BCTop | integer | 2 | type of boundary condition at the top side of the triangulation. If BCTop=-999 the boundary conditions that are defined in the triangulation program (e.g. ITEDGE in the input file) are used. |
| DCHAN | real $[\mu \mathrm{m}]$ | 0.2 | For TYPe=MOS, channel depth. |
| DDEV | real $[\mu \mathrm{m}]$ | 6 | For TYPe=MOS, depth of the device. |
| DDOT | real [ $\mu \mathrm{m}$ ] | 0.6 | For TYPe=MOS, depth of the doping region |
| DFG | real [ $\mu \mathrm{m}$ ] | 0.046 | For TYPe=MOS, thickness of the floating gate (for IYFG $>0$ ). |
| DFG1 | real $[\mu \mathrm{m}]$ | 0.046 | For TYPe=MOS, thickness of the oxide on top of the floating gate (for IYFG1 > 0). |
| DOXI | real [ $\mu \mathrm{m}$ ] | 0.046 | For TYPe=MOS, oxide thickness (for IYOXI>0). |
| DSUB | real $[\mu \mathrm{m}]$ | 2.0 | For TYPe=MOS, depth of the transition region. |
| IXAVA | integer | 3 | For TYPe=MOS, number of columns in the avalanche region. |
| IXDRAI | integer | 3 | For $\mathrm{TYPe}=\mathrm{MOS}$, number of columns in the drain region. |
| IXEFF | integer | 3 | For $\mathrm{TYPe}=\mathrm{MOS}$, number of columns in the channel region. |
| IXSOUR | integer | 3 | For $\mathrm{TYPe}=\mathrm{MOS}$, number of columns in the source region. |
| IYBULK | integer | 3 | For TYPe=MOS, number of rows in the bulk region. |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| IYCAN | integer | 3 | For TYPe=MOS, number of rows in the channel region. |
| IYDOT | integer | 3 | For TYPe=MOS, number of rows between channel and substrate. |
| IYFG | integer | 0 | For TYPe=MOS, number of rows in the floating gate. |
| IYFG1 | integer | 0 | For TYPe=MOS, number of rows in the oxide on top of the floating gate. |
| IYOxi | integer | 0 | For TYPe=MOS, number of rows in the oxide. |
| IYSub | integer | 3 | For $\mathrm{TYPe}=\mathrm{MOS}$, number of rows in the substrate. |
| IZONEN | integer | 1 | For $\mathrm{TYPe}=\mathrm{MOS}$, number of zones in the simulation domain. |
| LAVA | real [ $\mu \mathrm{m}$ ] | 0.4 | For TYPe=MOS, length of the transition region. |
| LDEV | real [ $\mu \mathrm{m}$ ] | 10.0 | For TYPe=MOS, length of the device. |
| LEFF | real [ $\mu \mathrm{m}$ ] | 6.0 | For TYPe=MOS, effective gate length. |
| LGAT | real $[\mu \mathrm{m}]$ | 8.0 | For TYPe=MOS, gate length. |
| LISO | real $[\mu \mathrm{m}]$ | 0.0 | For TYPe=MOS, length of the isolator at source and drain. |
| XUnits() | record | 1. | Vector of 2 scaling factors in lateral and vertical directions. Parameter for the MOS- and the Netz-type. laterally: $x_{\text {dios }}$ $=x-$ tria $\cdot$ XUnits (X1), vertically: $y_{\text {dios }}=y-$ tria . XUnits (X2) |
|  |  |  | continued on next page |


| name unit <br> type <br> option default |  |  |  |
| :--- | :--- | :--- | :--- |
| YO | real $[\mu \mathrm{m}]$ | 0. | Fom TYPe=MOS, vertical position <br> of the substrate surface. |
| TEST | integer | 0 | check the user triangulation <br> with respect to internal edges, <br> boundary conditions and over- <br> lapping triangles. 1:check 0:no <br> check |
| CONTrol () | 2.13, p. 98 |  |  |

### 2.7 Graphic command

The Graphic command should be used for checking the simulation results. REPLace (CONTrol(NGraphic=10)) can be used, to force WIAS-TeSCA to repeat the selected graphical output every 10 time steps and at the end of each processing step. REPLace CONTrol NGraphic turns off this mode.

In the interactive mode the command Graphic (calls a local command loop, where graphical output can be done. If the closing parenthesis is entered, the simulator leaves this local command loop ...
Replace (Control(NGraphic=10)) can be used, to force WIAS-TeSCA to redraw a picture every 10 time steps and at the end of each process step.
Replace (Control (NGraphic=0)) turns off this mode and is the default. A complete list of all parameters of the Graphics command is given at the end of this section.

By default the layer system and the net profile are shown:

```
Graphic (Plot).
```

The pictures are drawn (in X11) into a separate window. The DISPLAY variable is checked. In batch mode no X11-output is done.

The execution of input files continues, if the picture is drawn. The parameter WAit (default 1) defines a waiting time between finishing the output and continuation of the simulation. For WAit=0 each picture has to be confirmed by pressing the return key. The CTRL-C cancels the output of the current picture. The selected switches and modified parameters remain unchanged even if the Graphic command is left, so the next time a short command is sufficient: Graphic (Plot), Graphic (SUrface) or Graphic (Cross).

WIAS-TeSCA is now reading and handling some events in the X11 window. Moving the pointer with pressed left mouse button selects a zoom region. If the button
is released, a zoomed picture is drawn. If the pointer is moved to a certain position and then the left mouse button is clicked, the pointer position is taken as the new center of the zoomed picture for Sample=off. For Sample=on the pointer coordinates, the function values and the index of the closest vertex and triangle are printed.
If the middle mouse button is clicked a zoom-out is done, and if the right mouse button is clicked, the unzoomed picture is redrawn.
Moving the pointer with pressed middle mouse button selects the cutting line for a 1 D cross section in the 2D picture. A 1D cross section along the selected line is drawn for the selected species. The length of the cutting line is printed. If the cutting line is outside the grid, it is moved. The first point of the cutting line or the first intersection of the cutting line and the grid are used as origin of the 1D plot. The distance along the cutline is displayed on the x -axis of the 1 D plot.
The graphical output is repeated, if the window size of the (X11) window has been modified, or if the window had been hidden (partially) and is now visible completely.
The event queue is checked frequently during program execution and before a new command is read from standard input. A new picture can be drawn only at the end of a time step, where it does not disturb the simulation.
During the simulation the CTRL-C key can be used to interrupt the computation. WIAS-TeSCA enters the TControl mode. In this mode graphic and print commands can be used. The simulation is continue, when the closing parenthesis is entered.

The variables, that are displayed can be selected by SPecies. WIAS-TeSCA variable names have to be used. The selection of variables can be done even before they are introduced in the simulation. Of course they can not be drawn before defined. Before any user selection, Net is drawn.

The displayed region of the simulation domain can be selected by:
SCale(Xmid=..., YMid=..., Factor=...)
or

```
SCale(XLeft=..., XRight=..., YBottom=..., YTop=...)
```

SCale (Equal=on) is the default for equal scaling of the X- and Y-axes in the picture. The selected region is used for the 1D-, 2D- and 3D-pictures and for the output in the Print and LControl commands. The region, selected by the user is kept unchanged, otherwise the displayed region is adapted to the current size of layer system and grid.

```
SCale(Factor=1)
```

resets user selected region. For SCale(Rescale=off) a fixed region is kept during the entire simulation (movies!). If ABS is specified, the absolute value of the
selected functions is drawn in the 1D-, 2D- and 3D-pictures, resp. If the two components of a vector are selected, and if ABS is specified, isolines or isoareas of the norm of the vector field are displayed, rather than isoareas or isolines of the components.

If MIN or MAX are specified, the drawn functions are cut at the specified values.
CUT prescribes the minimum absolute value, displayed in the pictures. For each of the variables a logarithmic, hyperbolic or linear transformation can be selected: LOGswitch Net Flog, Atot=Ashsur, POF=Linear. The used color map is affected by the selected transformation.

To define 1D cross sections, the lateral or vertical positions have to be specified: XSection(...), YSection(...). Vertical cross sections are shifted (by default to the current local substrate surface) and scaled.

In XYSectio (. . .) the starting and end points of arbitrary straight cross sections can be prescribed. The cross section is displayed as a function of the distance along the specified line.

All intersection points of the specified 1D cross section line and triangle edges are used. Some of the variations of the 1D profiles might result just from interpolation. The cross sections are computed and drawn, using the Cross command.

I-V-characteristics of a device simulation with WIAS-TeSCA can be displayed, using the IVCurve command. The parameters, displayed at the axes can be defined interactively, or using the parameters XName, YName, BBIas and EBIas. I-Vcharacteristics can be read from a protocol or spool file from a separate WIAS-TeSCA simulation, if a file name and the switch READ=on are specified before the IVCurve command. BBIas and EBIas denote numbers of user specified BIAS points. All BIAS points are numbered increasingly.

Arbitrary x-y plots can be read and displayed with the LIneplot command. A quite general (ASCII) file format is supported: all input lines, not containing exactly 2 numbers, are interpreted as comment lines. A dataset is defined by a comment line and several data lines. The first value of a data line is used as abscissa and the second as ordinate.

The NLinplot command can be used to redisplay the curves with different parameter settings.

If DELete=off has been specified also 1D cross sections and I-V-curves are not deleted after they have been displayed. Using (... DELete=on, NLinplot ...) all curves are deleted.

If SAVE is specified, 1D cross sections, I-V-curves and externally read curves are written to a $\mathrm{FIle}=\ldots$, by default in xgraph format.

2D pictures are drawn with the Plot command. The elements of the picture have to be selected with switches before drawing: Isoline, Layer, Vector, Triangle, GLayer, BORder, Junction.

Material, areas and boundary lines, in which grid and doping are shown, can be selected. MATerial(...) ISOMaterial(...) AREA(...) LINE(...)

For BORder=on the outer contour line of the grid is drawn.
Isoline=No Onebyone, Allinone, SFill, Linked, Fill selects the drawing style of isolines or isoareas.
The levels for the isoline plot are chosen automatically, but the $(\leq)$ levels can be overwritten by the user. LEvel (Species=..., Nlevel=..., L1=..., L2=...).
The chosen levels are kept until the extremal values of the variable in the selected regions and the selected window are changed by more than LEvel REselect percent. In that case, using the new extremal values, the levels are reselected automatically.

Layer=No, Contour, Material, Area, Lines, Sort, SOMat and LIArea select different representations of the layer system. GLayer does the same for the approximation of the layer system in the grid. If Junction=off, the p-n-junctions are not highlighted. PNStyle=solid | bold defines the line style for the p-njunctions.

Vector valued functions are drawn as a vector field, if Vector=on is specified, and if at least one of the components is selected. First, the x -component has to be selected. If VSw=on a vector is drawn in each grid point, otherwise VNX and VNY define a tensor product mesh in the currently displayed regions for which the values are interpolated and the vectors are drawn. For Grid=Itri internally VSw=on is assumed always.

The lengths of the vectors is defined by the norm. By default the lengths are scaled with respect to the maximum of the norms of the displayed vectors, such that the drawn vectors do not overlap. A minimum relative length VMIN independent of the norm is used to display small vectors. The drawn vectors are enlarged if VFactor $>1$.
VNOrm prescribes a global maximum of the norm used in all vector plots. Vectors are not drawn, if their norm is smaller that VSuppress.

The parameter VSHape $=-11,0,11,12,13,14 \ldots$ selects the drawing style of the arrows.

The parameter Numbers=No, On, Diffgrid, Polygrid, OXidgrid selects the output of point, triangle and edge numbers. The various grids known in WIAS-TeSCA are selected by Grid=Itri, Utri, Diff, the default is Utri. For the ITRI grid the various hierarchical (multigrid) levels can be displayed: GRId=Itri, MLevel=... If MLevel=0 the user grid is displayed.

The boundary conditions and contacts for the device simulation with WIAS-TeSCA are drawn, if Contacts= on. For Contacts=Pieces the different connectivity components of the contacts are displayed. By default no contacts are drawn (Contacts=No).
The command Value ( $\mathrm{x}=\mathrm{y}=$ ) prints the (interpolated) doping values at the given point.
The command SUrface is used to draw 3D-surface plots of the selected species, by default the functions are interpolated on a rectangular mesh. NST, MAXX and

MAXY define the maximum number of grid points and the limits in the coordinate directions of that grid.

The rotation and the tilt angle can be incremented Rotate, Tilt or prescribed exactly RAngle, TAngle. Alternatively the coordinates of a view point VIEWX, VIEWY, VIEWZ can be specified. The finest triangle grid can also be drawn as surface plot: 3DSwitch=Triangle.

XName, YName and ZName are the names of the coordinate axes that are displayed.

Additional text, markers, lines or arrows can be drawn. The displayed coordinate system in a 1D or 2D picture is used to position them. For the 3D pictures and for the LABel command the positions are to be defined in the internally used picture coordinates: $(0 \ldots 29.7) \times(0 \ldots 21)$.

A vector of text strings, lateral and vertical positions and colors has to be defined for the text. For markers and lines the style also has to be defined.

```
TEXt(T1='...',...,T10='...'), XText(...), YText(...), CTExt (...),
STarrow(s1=arrow) XArrow(x1=10, y1=12) YArrow(y1=0 2) CArrow(c1=1).
```

The LABel command just draws the specified text, markers and lines.
The parameters in the data record WIndow(...) control the subdivision of the graphical window. The lengths are interpreted in the internal plot rectangle $(0 \ldots 29.7) \times(0 \ldots 21)$. Left= Right= Bottom= Top= define the size and position of the next picture. LSHIFT and VSHIFT define the offset, reserved for scales. By default WORDs=off and the entire window is used for the picture. Text is drawn into the picture. The content MBox, IBox, NBox position XBox, YBox and orientation Box=No, Lateral, UPward, Horizont, Downward of the palette can be specified. (MBox=on material list, NBox=on species name and unit, IBox=on doping levels).

If WORDs=on, the drawing region is subdivided into picture and text part. PLeft, PRight, PBottom and PTop define the picture. 2D pictures are drawn in the right or bottom part. The text is drawn in the left or upper side. PLeft and PTop prescribe the used picture range, DLeft and DTop are used as defaults. TTop and TLeft locate the text window, LPos and VPos locate the simulation domain in the picture region; (Centered, Left, Right resp. Centered, Bottom, Top) For WORDs=off these parameters are ignored.

In WIAS-TeSCA only a single text font can be used. The X11 font can be predefined by an environment variable:
setenv GMSFONT "adobe-courier-bold-r-normal--25-*-*-*-*-*"
or specified in the input file as WIndow(FONT='screen.b.16') ZLine defines the line spacing and ZSize the character height and the offset of an exponent with respect to the internal plot range ( $0 \ldots 21$ ). ZDist defines the lateral spacing of the characters with respect to ( $0 . \ldots 29.7$ ) HIgh, DOtlow, LInelow and BOLd define the lengths and the thicknesses for the various line styles. If the font or the size
of the graphical window has been modified, these parameters should be adapted.
The colors can be defined in the data record CoLors. The switches Substrate and GAS control the filling of the polygon in the substrate and the gas regions when drawing the layer system. Color indices can be given for SCales, TExt, TRiangle, triangle and node numbers TriangleNumber, NodeNumber, contours in the layer system LayerSystem, the outer contour of the simulation domain Border, vectors Vector, and Vector1, p-n-junctions PNcolor, and the top and bottom side of a 3D plot SUTop and SUBottom.

The color indices for each Material (...), the triangles in the material TRIMaterial (...) and the bounary type $\operatorname{SOrt}(. .$.$) can be defined too.$

Area(Area=.., Color..) and Line(Line=.., Color=..) can be used to highlight a certain region or line.

The colors of the contacts are selected by DIrichlet (..) and Gate (..)
The parameter vectors $\operatorname{Index}(\ldots), \operatorname{Red}(\ldots), \operatorname{Green}(\ldots)$ and Blue(... $)$ define the RGB color values for the various color indices. Index 0 is used for the background color (white: Red=255 Green=255 Blue=255). Index 1 defines the inverse (black: Red=0 Green=0 Blue=0). The color indices $1 \ldots 7$ (black, red, green, blue, yellow, magenta, cyan) are used for grid, scales, surfaces plots etc. and if necessary, repeatedly used. The indices $8 \ldots 18$ are preserved for the materials in the layer system and the remaining colors are used as a rainbow to display the doping. To modify a color, the indices and the RGB values have to be specified.
STeps defines the number of color levels in the isoline plot. If $\mathrm{STeps}=2$ in the net doping, only n - and p-regions are distinguished. If STeps is larger than the number of allocated colors all colors from the rainbow are used. The levels in the palette are drawn each in a single color, otherwise the line of change of the color defines the isoline to the specified level.

WIAS-TeSCA pictures can be saved as HPGL plotter files .hpgl, encapsulated postscript files .eps, Sun raster files .ras or GIF-files .gif. This can be selected by TERminal=PS HPGL ras ras.Z ras.gz gif gif.Z. Postscript and HPGL files are written explicitly, for the other formats the following commands are used: xwd -name ...|xwdtopnm | pnmtorast xwd -name . . .|xwdtopnm| ppmtogif.

WIAS-TeSCA can also be used, to save a series of similar pictures as a "movie". (MOVIE=ras ras.Z ras.gz gif gif.Z gif.gz).
The command sequence to display the "movie" is written into a file with the extension .xmovie. After the WIAS-TeSCA simulation the movies can be displayed using: xmovie xxx.xmovie.

A second command sequence to display the "movie" using screenload commands is written into an executable shell script with the extension .movie.

To illustrate the total processing time an analog watch can be drawn:
CLock (Xmid=..., Ymid =..., XDiameter=..., YDiameter=...)
The temperature can be displayed:
TEMperature (Xleft= Ybottom= ).

Alternatively a diagram can be used to show the current process step time (and the temperature profile):
CLock(STGone=Difbar).
In WIAS-TeSCA several pictures can be displayed on the screen. First the picture size has to be defined WIndow(Left= Right= Bottom= Top= ). Next the picture is drawn and then the current graphics parameter set is saved using: NEXTpicture(). The largest non-overlapping rectangle is used as default for the next picture. This procedure may be repeated. The command DRAWpicture() restores the saved parameter sets one after the other and redraws the pictures.

The command ERASepicture() deletes the saved data sets. These functions can be called with a data set number (default 0), and work then with a single data set DRAWpicture(1).

Note! Only the graphics parameters are saved and restored, not the grid, layer system, doping etc. If the simulation continues or after loading a file, a redraw changes all pictures.

### 2.7.1 Parameters shared by all plots

In this section parameters are listed, which are not specified in 1D, 2D or 3D plots. They can be specified as Graphic (Name=value...)


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| CCUTN | real | undefined | Shift the negative data <br> range of the logarithm for <br> LOGswitch=Flog |
| CHAracters | boolean | on | Do text output. |
| CLEar | PlotArea | Clean (part of) X11 window, <br> before drawing. |  |
|  | No | Do not clear at all. Draw all <br> on top of each other. |  |
|  | PlotArea | Fill the plot area for the next <br> picture with background color. |  |
|  | OnceWindow | Clear the entire graphical win- <br> dow. GKS: call clrwk |  |
|  | Border | Clear once the window and <br> switch back to plotArea |  |
|  | NewWindow | Fill scales, text, palette in <br> background color. Draw on the <br> old picture. |  | | Delete the X11 Window and |
| :--- | :--- |
| build a new one. |


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| MIN | real | -1 e32 | Minimum cut off value for the <br> plot. |
| MAX | real | 1. e32 | Maximum cut off value for the <br> plot. |
| CUT | real | undefined | Minimum absolute value for <br> the plot. |
| Grid | Urocedure | utri | Selection of the displayed grid <br> and node numbers: Itri, <br> Utri, Diff, USER. |
| SCale ( | real | Parameters for the definition <br> of the zoom window in the sim- <br> ulation domain. |  |
| Ymid | real | undefined | Input value for the lateral po- <br> sition of the midpoint. |
| Factor | real | rition of the midpoint. |  |


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| YTop | real | undefined | Input value for the top bound- <br> ary of the zoom window. |
| XLEFT | real | Currently used left boundary <br> of the zoom window. |  |
| XRIGHT | real | Currently used right boundary <br> of the zoom window. |  |
| XBOTTOM | real |  | Currently used bottom bound- <br> ary of the zoom window. |
| YTOP | real | Currently used top boundary <br> of the zoom window. |  |
| GXLeft | real | Left boundary of the simula- <br> tion domain. |  |
| GXRight | real | Right boundary of the simula- <br> tion domain. |  |
| GYBottom | real | Bottom boundary of the simu- <br> lation domain. |  |
| GYTop | real | Top boundary of the simula- <br> tion domain. |  |
| FX | real | real | undefined | | Input value for the lateral |
| :--- |
| zoom factor. |


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter | type [unit] | default | Comment |
| name | type options | value |  |


| ) | End of the procedure Scale. |
| :--- | :--- |
| Window $($ record | Position of picture and text |
|  | in the graphical window: |
|  | x:0...29.7 y:0...21. |


| Left | real | 0 | Left boundary. |
| :--- | :--- | :--- | :--- |
| Right | real | 29.7 | Right boundary. |
| Top | real | 21 | Top boundary. |
| Bottom | real | 0. | Bottom boundary. |
| PLeft | real | undefined | Left boundary of the picture <br> for WORDs=on. |
| PRight | real | undefined | Right boundary of the picture <br> for WORDs=on. |
| PBottom | real | Top boundary of the picture <br> for WORDs=on. |  |
| DLeft | real | 9.5 | Default left boundary of the <br> picture, if picture is at the <br> right, for WORDs=on. |
| DTop | real | 17. | Default upper boundary of the <br> picture, if picture is at the bot- <br> tom for WORDs=on. |


| TLeft real | 0.5 | Left text boundary for <br> WORDs=on. |  |  |
| :--- | :--- | :--- | :--- | :--- |
| TTop | real | 20.8 | Upper text boundary for <br> WORDs=on. |  |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] type options | $\begin{aligned} & \text { default } \\ & \text { value } \end{aligned}$ | Comment |
| Maxword | integer | 0 | Number of characters reserved for scales, names and logo at the left side of the picture (internally increased for the next picture). |
| LShift | real | 1.5 | Lateral offset between text and picture. |
| VShift | real | 0 | Vertical offset between text and picture. |
| LPos | Centered <br> Left <br> Right | Centered | Lateral position of the simulation domain in the picture for WORDs=on. |
| VPos | Centered <br> Bottom <br> Top | Centered | Vertical position of the simulation domain in the picture for WORDs=on. |
| SCWindow | record |  | Additional text window for WORDs=on. Used only if much text is displayed. Default: inside the picture. |
| Left | real | undefined | Left boundary. |
| Right | real | 29. | Right boundary. |
| Bottom | real | 22. | Bottom boundary. |
| Top | real | undefined | Top boundary. |
|  |  |  | continued on next page |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| ) |  |  | End of record SCWindow. |
| XLogo | real | undefined | Lateral position of the WIAS-TeSCA logo. |
| YLogo | real | undefined | Vertical position of the WIAS-TeSCA logo. |
| FONT | string*80 |  | Name of an X11 text font. |
| DISPLAY | string*32 |  | Overwrites DISPLAY variable. |
| ZSize | real |  | Character size relative to the (0... 21). |
| ZDist | real |  | Character spacing relative to (0. . . 29.7). |
| ZLine | real |  | Line spacing relative to (0...21). |
| MSize | real |  | Marker width relative to (0. . 29.7). |
| MHeight | real |  | Marker height relative to (0...21). |
| PRIVateCol | ormap boolean | off | switch between shared and private colormap. |
| WIdth | integer | 2 | X11 line width in pixels. |
|  |  |  | continued on next page |


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| WSize | real |  | X11 window width relative to <br> $0 \ldots 1$. |
| WHeight | real | X11 window height relative to <br> $0 \ldots 1$. |  |
| HIgh | real | 0.15 | Length of a gap in dashed or <br> dotted lines. |
| DOtlow | real | 0.1 | Length of a dot in dotted lines. |
| LInelow | real | 0.3 | Length of a dash in dashed <br> lines. |
| BOLd | real | 0.15 | Width of a bold line. |
| BOX |  | UpOrLateral | Orientation of the palette <br> No Lateral Up Horizontal <br> Down UpOrLateral. |
| YBox | Length | undefined | Lateral position of the palette <br> in the displayed coordinate <br> system. |
| YBox | Length | undefined | Vertical position of the palette <br> in the displayed coordinate <br> system. |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] <br> type options | $\begin{aligned} & \text { default } \\ & \text { value } \end{aligned}$ | Comment |
| IBox | boolean | on | Display doping levels in the palette. For isoareas and small STeps the color change represents the isoline level. At most 40 data items with each $\leq 14$ characters are displayed in the palette. |
| MBox | boolean | on | Display materials in the palette. |
| NBox | boolean | on | Display variable names and units in the palette. |
| LOGO | string*32 | WIAS-TeSCA | Text of WIAS-TeSCA logo. Used if COLors(LOgo=...) is defined. |
| ) |  |  | End of record Window. |
| COLors ( | Procedure |  | Color definitions. |
| Reset | Procedure |  | Return to default colors. |
| Substrate | boolean | on | fill polygon for the substrate. |
| GAS | boolean | off | if on, fill the gas layer. |
| BAckground | integer | - | Index of the background color. |
| SCales | integer | undefined | Color index of the scales. |
| TExt | integer | undefined |  |
| continued on next page |  |  |  |


| Graphic( |  |  |
| :---: | :---: | :---: |
| parameter type [unit] name type options | $\begin{aligned} & \text { default } \\ & \text { value } \end{aligned}$ | Comment |
| TRiangle integer | undefined |  |
| TriangleNumber integer | undefined | color index of triangle numbers. |
| NodeNumber integer | undefined | color index of node numbers. |
| LayerSystem integer | 1 | Only for Layer=Contour . |
| Border integer | undefined | Outer contour of the simulation grid. |
| LOgo integer | undefined | By default a ball, containing all WIAS-TeSCA colors is used as a WIAS-TeSCA-logo. If LOgo=. . ., then the text string WIndow (LOGO='=DIOS=') is drawn. For LOgo=0 the text is drawn in background color. |
| Vector integer | undefined |  |
| VPoint integer | undefined | Vector point for VSHape=0. |
| SUTop integer | undefined | "Up" side in 3D-plots. |
| SUBottom integer | undefined | "Down" side in 3D-plots. |
| Material() record | undefined | Color indices for materials in Layer plot. If not specified, the internally reserved colors are used. |
|  |  | continued on next page |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] type options | $\begin{aligned} & \text { default } \\ & \text { value } \end{aligned}$ | Comment |
| TRIMaterial() record |  | undefined | Color indices of triangles for the materials. |
| STeps | integer | 3 | Number of color steps. |
| SOrt | record |  | Color indices of the boundary types. |
| Area() | task |  | Color index for areas, defined as Area=. . .Color= . . . |
| Line() | task |  | Color index for lines, defined as Area=. . . Color=. . . |
| DIrichlet() record |  |  | Color indices of the Dirichlet contacts. |
| Gate() | record |  | Color indices of the Gate contacts. |
| Index () | integer | undefined | Vector of color indices. 0:background, 1 :inverse of 0 . Currently (in X11) the indices 8... 18 are reserved for the layer materials and the indices $\geq 19$ are used for the rainbow. The colors $1 \ldots 7$ are used for everything else. |
| Red () | real | undefined | Red values 0...255 corresponding to Index (). |
| Green() | real | undefined | Green values 0... 255. |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] <br> type options | $\begin{aligned} & \text { default } \\ & \text { value } \end{aligned}$ | Comment |
| Blue() | real | undefined | Blue values 0... 255. |
| XBLUE ( | record |  | Position and RGB values of "blue" in the rainbow. Similar records are defined for XCYAN, XGREEN, XYELLLOW, XRED |
| POSition | real |  | XBLUE:0 XCYAN:0.35 <br> XGREEN:0.5 XYELLOW 0.65 XRED:1 position in the rainbow:0... 1 . |
| Red | real |  | XBLUE:0.01 XCYAN:0.01 XGREEN:0.01 XYELLOW 0.8 XRED:0.8 Red value 0... 1 . |
| Green | real |  | XBLUE:0.01 XCYAN:0.8 <br> XGREEN:0.8 XYELLOW 0.8 <br> XRED:0.01 Green value: $0 . . .1 .$ |
| Blue | real |  | XBLUE:0.8 XCYAN:0.8 <br> XGREEN:0.01 XYELLOW 0.01 <br> XRED:0.01 Blue value: 0... 1 . |
| ) |  |  | end of record XBLUE, XCYAN, XGREEN, XYELLOW, XRED |
| ) |  |  | End of the procedure COLors. |
| WAit | integer | -1 | Waiting time in csec. If 0 each picture has to be confirmed by pressing Return. |
|  |  |  | continued on next page |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] <br> type options | default value | Comment |
| Terminal | Typ | X11 | 0 Regis 4ColorRegis 8ColorRegis 16ColorRegis 16FreeColorRegis TEK4014 TEK4014Emulation TEK42xx X11 PS BGI SUNVIEW GMSHPGL HPGL Off ras ras.Z ras.gz gif gif.Z gif.gz The default type can be predefined by the environment variable GMSDEFAULT. Only one terminal type can be defined at a time. For the types ras* gif* the X11 window is required and a system command is used to generate the files. The file name can be specified. xwd -name ...\|xwdtopnm|pnmtorast xwd -name ...|xwdtopnm|ppmtogif. |


| NCutp | integer | undefined | Number of orders of magni- <br> tudes used in the positive data <br> range for LOGswitch=Flog. |
| :--- | :--- | :--- | :--- |
| NCUTN | integer | undefined | Number of orders of magni- <br> tudes used in the negative data <br> range for LOGswitch=Flog. |
| CCutp | real | undefined | Shift of the positive data <br> range of the logarithm for <br> LOGswitch=Flog. |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| CCUTN | real | undefined | Shift of the negative data range of the logarithm for LOGswitch=Flog. |
| TRAnsformed boolean |  | off | Plot of transformed functions. For concentrations in polysilicon: <br> off: $c^{g}, c^{g b}$ <br> on: $c^{g}+F \cdot c^{g b}, F \cdot c^{g b}$ <br> off: silicon consumption for 02Dif=Zone <br> on:silicon density for 02Dif=Zone |
| SCARrow | boolean | off | Select scale arrows or scale rectangle. |
| SECscale | Tic Default Grid No | Default | Tic: Only one set of scale tics. <br> Default: Second set of scale tics at the opposite side. <br> Grid: Rectangular grid in the entire picture. |
| CHAracters | boolean | on | Do text output. |
| WORDs | boolean | off | on: Picture and text separated. <br> off: Text inside the picture. |
| XName | strin*8 | undefined | Name of the x-axis. Used also to select I-V-curves. |
|  |  |  | continued on next page |


| Graphic( |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| XScale | record | undefined | Vector of scale values, used for <br> the x-axis. |


| YName | record | undefined | Name of the y-axis. Up to 5 <br> names can be specified to se- <br> lect I-V-curves. |
| :--- | :--- | :--- | :--- |
| YScale real | undefined | Vector of scale values, used for <br> the y-axis. |  |


| ZName | string*8 | undefined | Name of the z-axis in 3D-plots. |
| :--- | :--- | :--- | :--- |
| ZScale | real | undefined | Vector of scale values, used <br> for the z-axis. For 2D plots <br> this overrides the level defini- <br> tion for all species. |


| PLOtter integer 0 | Pen velocity, when writing a <br> HPGL file. TERminal=HPGL |
| :--- | :--- | :--- |


| RESET | procedure | Reset the graphics command <br> to its initial state. |  |
| :--- | :--- | :--- | :--- |
| EXponent | boolean | on | Representation of real num- <br> bers on: $10^{20}$, off:1E20 |


| TEXt | string ${ }^{* 80}$ | undefined | Vector of $\leq 15$ text lines. |
| :--- | :--- | :--- | :--- |
| XTEXT | real | undefined | Lateral positions for TEXt. In <br>  |
|  |  | 1D- and 2D-pictures, with re- <br> spect to the displayed coordi- |  |
|  |  | nate system. In 3D-pictures |  |
| with respect to $0 \ldots 29.7$. |  |  |  |

continued on next page

| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| YTEXT | real | undefined | Vertical positions for TEXt. In <br> 1D- and 2D-pictures, with re- <br> spect to the displayed coordi- <br> nate system. In 3D-pictures <br> with respect to 0 ...21. |
|  |  |  |  |
| CTExt | integer | undefined | Vector of color indices for |
|  |  |  | TEXt. |
|  |  |  | Style of text representation. |
| STExt |  |  | Draw text in the given color. |
|  |  |  | Draw text in a rectangle of |
|  |  |  | background color. |


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| XArrow | real | undefined | Vector of lateral positions of <br> markers and lines. |
| YArrow | real | undefined | Vector of vertical positions of <br> markers and lines. |
| YArrow | real | undefined | Vector of vertical positions of <br> markers and lines. |
| CArrow |  | undefined | Vector of color indices of mark- <br> ers and lines. |
| LABEL() | procedure |  | Display only text, markers and <br> lines. The graphics window is <br> not erased and subwindows are <br> not respected. |
| IPLOtu | integer | 0 | Graphical output channel. In- <br> ternally defined. |
| IWT | integer |  | Workstation type for GKS out- <br> put. Internally defined. |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] type options | ```default value``` | Comment |
| MOVIE | No ras <br> ras.Z gif <br> ras.gz <br> gif. $Z$ <br> gif.gz | No | After each picture is drawn, an image file is created: |
|  |  |  | xwd -name |
|  |  |  | ...\|xwdtopnm|pnmtorast <br> ...\|xwdtopnm|ppmtogif The |
|  |  |  | names of the image files are written into a script file with extension .xmovie After the |
|  |  |  | WIAS-TeSCA simulation the |
|  |  |  | movie can be displayed using xmovie xxx.xmovie At the |
|  |  |  | same time a shell script with extension .movie is written |
|  |  |  | that uses screenload to display |
|  |  |  | the movie files. (Works on Sun only). Internally defined. |


| MOVPIC | integer | 0 | Number of the first picture, <br> incremented after a picture is <br> dumped. |
| :--- | :--- | :--- | :--- |
| MOVCMD | string*80 | undefined | User defined command for <br> dumping pictures. Internally <br> only the name of the picture <br> file and the number are ap- <br> pended to the string. |
| FILe | string*80 | undefined | File name, used to save 1D <br> cross sections, to read curves, <br> to save pictures for movies. |
| CLEar | Action | Window | Erase (parts of) the graphical <br> window. |
|  | No | Do not clear at all. |  |
|  |  | continued on next page |  |


| Graphic |  |  |
| :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value |
|  | PlotArea | Comment |
|  | Window | Fill the plot area for the next <br> picture with background color. |
|  | OnceWindow | Clear the entire graphical win- <br> dow. GKS: call clrwk |
|  | Border | Clear once the window and <br> switch back to PlotArea |
|  | NewWindow | Fill scales, text, palette in <br> background color. Draw on the <br> old picture. |
|  | Destroy | Delete the X11 window and <br> build a new one. |
| NEXTpicture procedure | Delete the X11 window . |  |
|  |  | Store the plot parameter set <br> of the just drawn picture, de- <br> fine the maximum new window <br> size. A picture number can be |
|  | specified to overwrite a param- |  |
| eter set. Default: 0i.e. append |  |  |
| a new parameter set. |  |  |

continued on next page

| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| Xmid | Length | undefined | Lateral position of the mid- <br> point and the left boundary of <br> a time bar, resp. |
| Ymid | Length | undefined | Vertical position of the mid- <br> point and the bottom bound- <br> ary of a time bar, resp. |
| XDiameter | Length | undefined | Width of the clock and time <br> bar, resp. |
| YDiameter | Length | undefined | Height of the clock and time <br> bar, resp. |
| BackColor |  | 0 | Background color index. |
| BOrderColor | Solid | Border color index. <br> GoneColor | Color index for already simu- <br> lated time. |
| STBorder |  | Minutes of the borderline: Solid, |  |
| Sold. |  |  |  |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| Time | Time | undefined | Start time of the analog clock. |
| TIMElist | Time | undefined | List of parameters for the time axis for STGone=Bar. TEMPList Parameters, displayed as a piecewise linear function of TIMEList. If undefined during diffusion steps, the temperature ramps are displayed. |
| Scale | Time | undefined | Vector of scale values for the time scale, if STGone=Bar. |
| ) |  |  | End of record CLock. |
| TEMperature record |  |  | Parameters for the temperature display. |
| Xleft | Length | undefined | Left boundary. |
| Ybottom | Length | undefined | Bottom boundary. |
| XRight | Length | undefined | Right boundary. |
| BackColor |  | 0 | Background color index. |
| BOrderColor |  | 1 | Borderline color index. |
| GoneColor |  | 2 | Color of the temperature. |
| STBorder |  | Solid | Style of the borderline: Solid Bold. |
| Minimum | Temperature | undefined | Minimum value. |
| MAximum | Temperature | undefined | Maximum value. |
| Name | string*8 | blank | Name of the temperature axis. |
| TemperatureTemperature |  | undefined | value to be displayed. |
|  |  |  | continued on next page |


| Graphic |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| TEMPList | Temperature | undefined | List of parameters for the tem- <br> perature axis for STGone=Bar. <br> TEMPList is displayed as a <br> piecewise linear function of <br> TIMEList. If undefined dur- <br> ing diffusion steps, the temper- <br> ature ramps are displayed. |
| Scale | Temperature | undefined | Vector of scale values for the <br> temperature scale. |
| ) |  |  | End of record TEMperature |
| XCoordinate |  | YCoord | Variable used as x-coordinate. |
| YCoordinate | 10 | Variable used as y-coordinate. <br> =Itri. |  |
| MLevel | integer | undevel, used for Grid |  |
| XSecond( | record | undefined | Parameters for a second x- <br> scale |
| Xminimum | real | minimum value for the 2nd x- <br> axis in x-y-plots. |  |
| axis in x-y-plots. |  |  |  |


| Graphic ( |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| Name | string*8 | undefined | name of the second y-axis |
| ) |  |  | End of record YSecond |
| VARiable() | record |  | see section 20, p.224 |

### 2.7.2 Parameters for 1D Plots



| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| ) |  |  | End of procedure XSection. |
| YSection | procedure |  | Vertical position of the lateral cross sections. |
| C1 | Length | ---um | 1st position (a WIAS-TeSCA ycoordinate). |
| MIN | real | undefined | Starting point (a WIAS-TeSCA x -coordinate). |
| MAX | real | undefined | End point (a WIAS-TeSCA xcoordinate). |
| ) |  |  | End of procedure YSection. |
| XYsection | procedure |  | Define ( $\leq 3$ ) arbitrary straight cross sections by specifying start and end points. |
| Xb1 | Length | Oum | X-coordinate of the first starting point. |
| Yb1 | Length | Oum | Y-coordinate of the first starting point. |
| Xe1 | Length | Oum | X-coordinate of the first end point. |
| Ye1 | Length | Oum | Y-coordinate of the first end point. |
| ) |  |  | End of procedure XYSection. |
| SHift | real | $1 . \mathrm{e} 10$ | Shift of vertical cross sections. displayed_ value $:=$ (DIOS_ value-SHift). FACtor For SHift>1E9 the local position of the substrate surface is used. |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| FACtor | real | -1000 | Scaling factor for the coor- <br> dinates of a vertical cross <br> section. ( -1000 to invert <br> the direction and to scale <br> from WIAS-TeSCA $\mu \mathrm{mm}$ into <br> TESIM-4's nm). |
| Append | boolean | on | Append or replace when saving <br> curves into a file. |
| BBIas | integer | undefined | First BIAS point, selected for <br> an I-V- curve. |
| EBIas | integer | undefined | Last BIAS point, selected for <br> an I-V- curve. |
| READ | boolean | off | on: Read I-V-curves from a <br> file, resp. read all curves from <br> the file when using LIneplot. <br> off: Select the curves from <br> the file interactively when us- <br> ing LIneplot. |
| FOrmat | Tesim <br> Xgraph <br> All plx <br> plt | All | File format for the input/out- <br> put file of x-y plots. |
| MErge | boolean | off | Linear combination of two se- <br> lected curves. |
| XMInimum | real | real | real |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| X0 | real | 0. | Parameter for the transforma- <br> tion $y:=Y X \cdot x+Y Y \cdot y+Y 0$. |
| YX | real | 1 |  |
| YY | real | -1 | Spacing for an interpolation of <br> the curves to an equidistant <br> grid. |
| YO | real | 0 | Number of grid point for an <br> equidistant grid. |
| DX | real | 0 | Scaling factor of the first curve <br> for MErge. |
| NX | integer | 0 | Scaling factor of the second <br> curve for MErge. |
| Y2merge | real | 1 | Compress the curve list. <br> COmpress |
| boolean | on | Vector of curve indices for per- <br> mutation of curves. |  |
| PERMUTation record | 0 | Vector of line styles for <br> each of the curves: No |  |
| LIStyle | record | 1 | Solid Dotted DAshed <br> DASHDotted DASH2Dot Bold <br> BDotted BDAshed BDASHDott <br> BDASH2Do |
| INStyle | boolean | on | Increment line style (after each <br> curve, resp. if all colors have <br> been used). |
| INColor | boolean | on | Color indices of the curves. |
|  |  | Increment the color index. |  |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| LIMarker | record | 0 | Marker style for each of the curves: No Plus Asterisk X Square Rhomb TTriangl BTriang RTriangl LTriangl Circle FSquare FRhomb FTTriang FBTriang FRTriang FLTriang BUllit |
| INMarker | boolean | off | Increment the marker style. |
| LIText | record | undefined | Comment text for each of the curves. |
| LILogsw | Linear Flog Ashsur | Flog | Transformation of the y-values of all curves. For general plots or if different LOGswitch values are defined for the displayed species. |
| LIEQual | boolean | off | Equal scaling of $x$ - and $y$-axis in plots. |
| Select | record | 0 | List of curve indices. If possible, the curves are selected from the previously displayed curves, otherwise from all defined curves. |
| INTNorm | boolean | off | Scale the curves to fit INTegral. |
| MAXNorm | boolean | off | Scale the curves to fit MIN and MAX. |
| XYchange | boolean | off | Toggle the axes. |
| Invert | boolean | off | Invert the order of the points in the curves. |
| LICLear | boolean | on | Delete unnecessary curve points with the same y-values. |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| IPU | integer | 0 | Additional print channel for x- <br> y plot comments, extrema, val- <br> ues, sheet resistance. |
| PCOmment | boolean | off | Print the curve comments. |
| PExtrema | boolean | off | Print the extremal values of <br> the curves. |
| PVALues | boolean | off | Print all curve values. |
| RS | boolean | off | Print the sheet resistance be- <br> tween the p-n-junctions of the <br> 1D cross sections. |
| PIntegral | boolean | off | Print the integrals. |
| PPlot | boolean | on | Plot the curves. <br> SAVE <br> boolean <br> offSave the curves into a file. <br> Note! For xgraph the max- <br> imum of the absolute values <br> and 1e-32 are written into the <br> file. |
| SAVTrans | boolean | off | Save the transformed curves, <br> i.e. log(...), into the file. |
| DELete | boolean | on | Delete the (selected) curves. |

### 2.7.3 Parameters for 2D Plots

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| Plot | procedure |  | Command to display 2D cross <br> pictures. |
| LEvel ( | task | Selection of isoconcentration <br> levels. |  |
| NCon | integer | undefined | Minimum number of levels for <br> Set |
|  |  | continued on next page |  |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| REselect | Percent | 100\% | Reselect levels if extremal values changed by given percentage. |
| Set | procedure |  | define new levels. |
| Species | string*8 | S1 | Variable, for which the levels should be chosen. |
| Nlevel | integer |  | Currently used number of levels. |
| L1 | real |  | $\leq 20$ concentration values. |
| ) |  |  | End of task LEvel. |
| MATerial() |  | undefined | List of WIAS-TeSCA materials in which the grid should be displayed. |
| ISOMateria |  | undefined | List of WIAS-TeSCA materials, in which the doping is displayed. |
| AREA () | record | undefined | List of Area numbers to be plotted. |
| LINE() | record | undefined | List of LINE numbers to be plotted. |
| ISoline | Isolines | Fill | Draw style for the doping. |
|  | Onebyone |  | One doping level at a time. |
|  | Allinone |  | All doping levels at the same time. |
|  | SFill |  | Fill each triangle. |
|  | Linked |  | Define a linked list of isolines. Cannot be used for GRID=ITRI. |
|  | Fill |  | Fill isoareas. |
| Triangle | boolean | off | Display the grid. |
| Border | boolean | off | Display the outer contour of the grid. |

continued on next page

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| Vector | boolean | off | display vector valued functions as vector field. |
| Layer |  | Material | Draw style for the layer system. |
|  | No |  |  |
|  | Contour |  | Only contour lines. |
|  | Material |  | Fillarea with the material colors. |
|  | Area |  | Fillarea for the areas. |
|  | Lines |  | Draw the contour Lines. When using this together with a marker, LIMarker the points in the layer system are marked |
|  | Sort |  | Draw boundary sorts. |
|  | SOMat |  | Do Material and Contour. |
|  | Zone |  | Fill WIAS-TeSCA zones. |
| Contacts |  | No | Display style for boundary conditions and contacts. |
|  | on |  | Draw contact types. |
|  | BC |  | Draw boundary condition types. |
|  | Pieces |  | Draw connectivity components of the contacts. |
| GLayer |  | No | Similar to Layer but for the regions of the UTRI-grid. |
| Junction | boolean | off | Draw thick isoline at th p-njunctions. |
| PNStyle |  | Bold | Linestyle for the p-n-junctions. See LIStyle. |
| PNcolor | integer | 1 | Color index for the p-njunctions. |

continued on next page

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| PNMarker |  | No | Marker style for the p-njunctions. See LIMarker. |
| Number |  | No | Display triangle and node numbers. |
|  | On |  | numbers in the grid |
|  | Diff |  | Node numbers, used in the matrix (for the total concentrations). |
|  | Poly |  | Node numbers used in the matrix (for the grain boundary concentrations). |
|  | Oxid |  | Node numbers used in the matrix (for the oxidant diffusion). |
|  | All |  | debugging. draw all UTRI triangles. |
| VNX | integer | 40 | Number of lateral discretization points for VSW=off. |
| VNY | integer | 35 | Number of vertical discretization points for VSW=off. |
| VFactor | real | 1.5 | Scaling factor for vector plot. By default the vectors are scaled with respect to their maximum value or VNOrm and the minimum grid spacing, such that they do not overlap, and then multiplied by VFactor. |
| VNOrm | real | undefined | Maximum norm. If specified, this value is used to scale all vector fields. |
| VSuppress | real | undefined | Minimum norm. Vectors with smaller norm are not displayed. |

continued on next page

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| VMIN | real | 0.3 | Minimum relative length. The smallest, displayed vector is drawn at this length compared to the largest vector. If VMIN=1 all vectors are drawn with the same length. |
| VSHape | integer | -11 | Arrow style. For $\pm 11$ and $\pm 12$ the tip is defined relative to the body. For $\pm 11$ and $\pm 13$, the tip is filled. For 0 , the tip is displayed in a different color. For values $<0$, a bold vector body is drawn. For $>0$, a line, for $>10$ a different line style is used. |
| VSW | boolean | off | on: Display vectors in the nodes of the grid. off: Use a VNX $\times$ VNY tensor product grid to display the vector field. |
| VLength | real | 0.4 | Relative length of the vector tip. |
| VWidth | real | 0.23 | Relative width of the vector tip. |
| MVLength | real | 0.5 | Absolute length of the vector tip. |
| MVWidth | real | 0.4 | Absolute width of the vector tip. |
| XFill | integer | 1000 | Number of lateral lines for the fillpolygon function. |
| YFill | integer | 0 | Number of vertical lines for the fillpolygon function. |
| RFill | integer | 0 | Display borderline in the fillpolygon function. |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| IMAGline | boolean | off | highlight the imaginary lines. <br> LSWitch=Contour |
| LI1 | integer | undefined | First boundary type, displayed <br> with Contacts. |
| LI2 | integer | undefined | Last boundary type, displayed <br> with Contacts. |
| CTHickness | real | 0.3 | Thickness of the contacts. |
| Value( | procedure |  | Print the interpolated values in <br> the specified points. |
| X | Length | undefined | Position. |
| Y | Length | undefined | Position. |
| ) |  |  | End of procedure Value. |
| LOngtext | boolean | off | Length of text when displaying <br> grid, contacts, boundaries. |


| name | unit | default | comment |
| :--- | :--- | :--- | :--- |
|  | type |  |  |

### 2.7.4 Parameters for 3D plots

In this section parameters are listed, which control the 3D surface plots. They can be specified as Graphic (Name=value...)

| Graphic ( |  |  |  |
| :--- | :--- | :--- | :--- |
| parameter <br> name | type [unit] <br> type options | default <br> value | Comment |
| 3Switch | Rectangle <br> Triangle <br> SRectangle | Rectangle | Selection of displayed grid. |
|  |  |  |  |


| Graphic( |  |  |  |
| :---: | :---: | :---: | :---: |
| parameter <br> name | type options | default value | Comment |
| MAXX | integer | 126 | Maximum number of <br> discretization  points <br> in $x$ direction for <br> 3Switch=Rectangle, SRectangle.   |
| MAXY | integer | 126 | Maximum number of <br> discretization  points <br> in $y$ direction for <br> 3Switch=Rectangle, SRectangle.  |
| NEW | boolean | on | Repeat the interpolation to the rectangular mesh before each 3D plot. |

### 2.8 Fermi command

WIAS-TeSCA is based on the Boltzmann statistics. For the simulation of optoelectronic heterostructures and degenerated semiconductor materials it is possible to use Fermi-Dirac statistics. The FERmi-command is used to enter the required parameters. Using Fermi-Dirac statistics (IFERMI=1), the exp-function is replaced by the Fermi integral $F_{1 / 2}(s)$.
Moreover, the FERmi-command is used to enter the optical parameters for the simulation of optical devices like semiconductor lasers with the models described in section 1.5 on page 13 .
In command DOMAIN the parameter TYPe $=3$ (analogously for other values of TYPe).
ILASER $>0$ has to be set (number of "laser contacts") and the number IANSEI of the sides and, for each of these sites, the zone number IZ and the local number of a side in a zone has to be specified.

### 2.9 Models and their parameters

The model parameters of following quantities are set within FERMI.

### 2.9.1 Gain $g$

The optical gain (amplification coefficient) is always set nonzero only in the active material, i.e. the material with smallest band gap in the device. Parameter GTYP chooses one of the following gain models.

Default Model for Maximum Gain, GTYP=0

$$
\begin{equation*}
g=\kappa \cdot\left[\exp \left(\frac{e U_{F}-\hbar \omega}{k T}\right)-1\right] \cdot \frac{n p}{N_{i}^{2} e^{e U_{F} / k T}} ; \quad e U_{F}=F_{n}-F_{p} \tag{2.20}
\end{equation*}
$$

$T$ is the current local temperature. $g$ is the density-dependent gain at a fixed userset lasing wavelength $\lambda=$ ALAM $\mathrm{cm} . \kappa=$ AKAPPA $\mathrm{m}^{-1}$ is the absorption coefficient at this wavelength in equilibrium. $g$ is negative at small densities, goes through zero at $e U_{F}=\hbar \omega$ and increases proportional to $n p$ at much higher densities. Only a small interval above the zero is needed in lasers, where the slope can be fitted by $\kappa$.

Maximum Gain Model, GTYP=1 Source: H. Wenzel and G. Erbert, in Physics and Simulation of optoelectronic devices IV, SPIE vol. 2693 (1996).

$$
\begin{align*}
g=\kappa \cdot & {\left[\exp \left(\frac{e U_{F}-\hbar \omega}{k T}\right)-1\right] f\left(\frac{F_{n}-E_{c}}{k T}\right) f\left(\frac{E_{v}-F_{p}}{k T}\right) }  \tag{2.21}\\
& \text { with } f(x)=\frac{1}{1+e^{x}} .
\end{align*}
$$

Like GTYP=0, but with saturating asymptotics above crossing zero.
Spectral Gain Model, GTYP=2 Source: H.-J. Wünsche et al., IEEE Journ. Quant. Electron. 29, no. 6, pp 1751-61 (1993).

$$
\begin{equation*}
g=\kappa \sqrt{\frac{\max (\Delta, 0)}{k T}} \cdot\left[f\left(\frac{E_{c}+\frac{m_{h}}{M} \Delta-F_{n}}{k T}\right)-f\left(\frac{E_{v}-\frac{m_{c}}{M} \Delta-F_{p}}{k T}\right)\right] \tag{2.22}
\end{equation*}
$$

with $\Delta=\hbar \omega-E_{g}$ being the photon energy in excess of the band gap and $M=m_{e}+$ $m_{h} . g$ is the textbook gain formula for parabolic bands and no multiparticle effects. It depends correctly on densities and wavelength within this approximation. $\kappa$ is the band-band absorption coefficient in equilibrium at $\Delta=k T$. Note: the difference between the arguments of the two occupation factors is $\left(\hbar \omega-e U_{F}\right) / k T$. Hence, $g$ crosses also zero at $e U_{F}=\hbar \omega$.

### 2.9.2 Refractive index $\bar{n}$

$\bar{n}$ is temperature dependent according to the formulas

$$
\begin{align*}
\bar{n}(T)=\left(\bar{n}\left(T_{0}\right)-\bar{n}_{d} \cdot(n+p) / 2\right)+\bar{n}_{T} \cdot\left(T-T_{0}\right), & & \text { typ }=0  \tag{2.23}\\
\bar{n}(T)=\left(\bar{n}\left(T_{0}\right)-\bar{n}_{d} \cdot\left(n+p-\left|D_{n e t}\right|\right) / 2\right)+\bar{n}_{T} \cdot\left(T-T_{0}\right), & & \text { typ }=1  \tag{2.24}\\
\bar{n}(T)=\left(\bar{n}\left(T_{0}\right)-\theta_{A} \cdot \sqrt{\bar{n}_{d} \cdot(n+p) / 2}\right)+\bar{n}_{T} \cdot\left(T-T_{0}\right), & & \text { typ }=3  \tag{2.25}\\
& \theta_{A}=1 \text { in active layer and zero elsewhere. } &
\end{align*}
$$

| Variable | Name in TeSCA | Proc | remark |
| :--- | :--- | :--- | :--- |
| $\bar{n}\left(T_{0}\right)$ | BRE | FERMI |  |
| $\bar{n}_{d}$ | BREFAK | FERMI | material factor |
| $\bar{n}_{T}$ | BREA | ENERGY |  |
| $T_{0}$ |  |  | fixed temperature |
| typ | BRETYP | FERMI |  |

### 2.9.3 Internal optical loss $\alpha_{b}$

$\alpha_{b}$ is composed of the free carriers absorption $\left(f_{c n}\right.$ and $\left.f_{c p}\right)$ and the inter valence band absorption $\alpha$. We have

$$
\begin{align*}
\alpha_{b} & =\alpha(T)+f_{c n}(T) n+f_{c p}(T) p  \tag{2.26}\\
\alpha(T) & =\alpha_{0} \alpha_{1}\left(e^{E_{0} / T_{0}-E_{0} / T}\right)  \tag{2.27}\\
f_{c n}(T) & =f_{c n 0} T^{\gamma_{n}}  \tag{2.28}\\
f_{c p}(T) & =f_{c p 0} T^{\gamma_{p}} \tag{2.29}
\end{align*}
$$

| Variable | Name in TeSCA | Proc | Bemerkung |
| :--- | :--- | :--- | :--- |
| $\alpha_{0}$ | AALPHA | FERMI |  |
| $\alpha_{1}$ | AALPHF | FERMI | material factor |
| $E_{0}$ | EA | FERMI |  |
| $f_{c n 0}$ | FCNALF | FERMI |  |
| $f_{c p 0}$ | FCPALF | FERMI |  |
| $\gamma_{n}$ | GN | MOBILITY |  |
| $\gamma_{p}$ | GP | MOBILITY |  |

### 2.9.4 Photon balance

Concerns the model equations (1.43-1.46) on page 14.

| Variable | Name in TeSCA | Proc | Bemerkung |
| :--- | :--- | :--- | :--- |
| $\alpha_{1}$ | AALPH1 | FERMI | scattering losses mode 1 |
| $\alpha_{2}$ | AALPH2 | FERMI $\uparrow$ mode 2 |  |
| $\bar{n}_{g 1}$ | GRUP1 | FERMI | group index mode 1 |
| $\bar{n}_{g 2}$ | GRUP2 | FERMI $\uparrow$ mode 2 |  |
| $K_{1}$ | PEFA1 | FERMI | Petermann factor mode 1 |
| $K_{2}$ | PEFA2 | FERMI $\uparrow$ mode 2 |  |
| $R_{1}(0)$ | R01 | FERMI | reflectivity left facet mode 1 |
| $R_{1}(L)$ | RL1 | FERMI | dto. right facet |
| $R_{2}(0)$ | R02 | FERMI $\uparrow$ mode 2 |  |
| $R_{2}(L)$ | RL2 | FERMI | dto. right facet |
|  | SRELAX | FERMI | numerical parameter |

### 2.9.5 Treat Powers as Parameters (TPP)

The basics of this approach are sketched on page 15. The folowing parameters can be used to steer the content of the calculated tables.

| Variable | Name in TeSCA | Proc | Bemerkung |
| :--- | :--- | :--- | :--- |
|  | NPower | FERMI | number of power values |
| $P_{1}+P_{2}$ | POwers | FERMI | power values (mW) |
|  | IEtam | FERMI | number of $\eta$ values |
|  | NLAM1 $\leq 20$ | FERMI | number of wavelengths mode 1 |
|  | NLAM2 $\leq 20$ | FERMI | ditto mode 2 |
| $\lambda_{1}$ | LAM1 | FERMI | wavelengths mode 1 (cm) |
| $\lambda_{2}-\lambda_{1}$ | LAM2 | FERMI | wavel. mode 2 relative to mode $1(\mathrm{~cm})$ |

The model powers are calculated according to $P_{1,2}=$ POwers $\cdot(1 \pm \eta) / 2$, where $\eta$ runs over IEtaem values equally spaced between -1 and +1 .

### 2.10 Parameters

| name | unit <br> type option | default | comment |
| :---: | :---: | :---: | :---: |
| AALPHA | real $\mathrm{m}^{-1}$ | 1d4 | $\alpha_{0}(2.27)$ p. 81 |
| AALPHF() | real | 1.d0 | $\alpha_{1}$ material factors for AALPHA |
| AKAPPA | real $\mathrm{m}^{-1}$ | 1 d 3 | $\kappa(2.20)$ to (2.22) p. 80 |
| AKAPPF () | real | 1.d0 | $\kappa_{1}$ material factors for AKAPPA |
| ALAM | real [cm] | 1.3d-4 | Lasing Wavelength, Sec. 1.5 |
| ALPHA | real | 0.1 d 0 | strain field |
| BRE() | real | 1.d0 | $\bar{n}\left(T_{0}\right)$ for all materials (2.13) p. 27 |
| BREFAK | real $\mathrm{cm}^{3}$ | 1d-19 | $\bar{n}_{d}(2.13)$ p. 27 |
| BENRADI | real [ cm ] | 1d-4 |  |
| BCENTER | real [ cm ] | Od0 |  |
| BRETyp | integer | 0 | type of refr. index (2.13) ff. p. $27$ |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| CMO1 () | real [1/cm] | 0.d0 | constant for optical boundary condition for mode 1, CMO1=0: natural bc, CMO1 $\gg 1$ : Dirichlet bc, Length $\leq 20$ |
| CMO2() | real | 0.d0 | Length $\leq 20$, see $\uparrow$ |
| COMPOS | real | 0.22 do | Material Composition |
| DEFKON | real [ $\mathrm{cm}^{-3}$ ] | 1 d 18 | Defect concentration |
| EC() | real [V] | 0.562 d 0 | Conduction band edge Length $\leq$ mreg |
| EG() | real [V] | 1.124 dO | Energy band gap Length $\leq$ mreg |
| EIGANF() | real | 3.6 d 0 | initial values for $c \Re e \beta_{i} / \omega$ |
| EIGMAX | real | 3.6d0 | upper bound for $c \Re e\left(\beta_{i}\right) / \omega$ |
| R01 | real | 0.36 d 0 | facet reflectivity at $z=0$, mode 1 |
| RL1 | real | 0.36 d 0 | facet reflectivity at $z=L$, mode 1 |
| R02 | real | 0.36 d 0 | facet reflectivity at $z=0$, mode 2 |
| RL2 | real | 0.36 d 0 | facet reflectivity at $z=L$, mode 2 |
| PEFA1 | real | 1.d0 | Petermann factor $K_{1}$ for mode 1, (1.46) p. 15 |
| PEFA2 | real | 1.d0 | $\uparrow$ mode 2 |
| GRUP1 | real | 3.6d0 | group index $\bar{n}_{g i}$ mode 1, (1.43) p. 14 |
| GRUP2 | real | 3.6d0 | $\uparrow$ mode 2 |
| AALPH1 | real | 0.d0 | scatt. losses $\alpha_{i}$ mode 1, (1.43) p. 14 |
| AALPH2 | real | 0.d0 | $\uparrow$ mode 2 |
| EPSP1 | real | 0.d0 | nonlin. gain saturation |
| continued on next page |  |  |  |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| EPSP2 | real | 0.d0 | $\uparrow$ mode 2 |
| SRELAX | real | 1.d0 | numerical parameter |
| EA | real | 0.1 d 0 | optical loss (2.27) p. 81 |
| FCNalf | real | 0.d0 | optical loss (2.28) p. 81 |
| FCPalf | real | 0.d0 | optical loss (2.29) p. 81 |
| GTYP | integer | 0 | which gain model, cf. Sec. 2.9.1 |
| HAOM | real | 0.d0 | Parameters (photogen.) |
| HHMAS | real | 0.44 d 0 | Parameters (photogen.) |
| IEtam | integer | 0 | Step number (variation of ETA) (TPP-method p. 82) |
| IFERMI | integer | 0 | IFERMI $=0$ (Boltzmann statistics), IFERMI=1 (Fermi-Dirac statistics) |
| INCNV | integer | 0 |  |
| IFOTO | integer | 0 | switch on the photogeneration |
| IPOL1 | integer | 1 | polarization mode 1, IPOL1=1 (TE polarization), IPOL1=2 (TM polarization) |
| IPOL2 | integer | 2 | polarization mode 2 , see $\uparrow$ |
| IFARfld | integer | 0 |  |
| IPtotm | integer | 0 | switch on the self consistent calculation of the optical gain, step number (variation of PTOT) |
| ISPec | integer |  | switch eigenmode calculation, ISPec < 0 activate the simple gain function |
|  |  | 0 | optics is switched off |
|  |  | 1 | one mode (TE or TM) |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
|  |  | 2 | two modes (TE or TM) |
| ITUN | integer | 0 | switch, tunnel generation |
| LAM1 () | real [cm] | 1.5d-4 | $\begin{aligned} & \text { wave-lengths } \quad \text { Length } \leq 20 \\ & \text { (TPP-method p. 82) } \end{aligned}$ |
| LAM2 () | real [cm] | 0.0 d 0 | differences of wave-lengths Length $\leq 20 \quad$ (TPP-method p. 82) |
| EFMN() | real [ $\mathrm{V} / \mathrm{cm}$ ] | 1.18d0 | Length $\leq$ mreg |
| EFMP() | real [ $\mathrm{V} / \mathrm{cm}$ ] | 0.5 d 0 | Length $\leq$ mreg |
| NC() | real [ $\mathrm{cm}^{-3}$ ] | 2.86 d 19 | Density of states (electrons) Length $\leq$ mreg |
| NV () | real $\left[\mathrm{cm}^{-3}\right]$ | 3.10d19 | Density of states (holes) Length $\leq$ mreg |
| NLAM1 | integer | 1 | Number of wave-lengths (TPP-method p. 82) |
| NLAM2 | integer | 0 | Number of observed wavelengths (TPP-method p. 82) |
| NPower | integer | 0 | Number of powers (TPPmethod p. 82) |
| POwers() | real | 0.0 d 0 | powers Length $\leq 100$ (TPPmethod p. 82) |
| PTOTM | real | 20.d0 | Total output (laser) |

### 2.10.1 Parameters for photogeneration

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| RICH | real | $0 . \mathrm{d} 0$ |  |
| R0 | real | $7 . \mathrm{d}-8$ | Localization radius |
| TS | real | 300.d0 | radiation temperature |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| VERL | real | $1 . \mathrm{d0}$ | Loss factor |
| VMA | real | $0 . \mathrm{d0}$ |  |
| XF1 | real $[\mathrm{cm}]$ | $0 . \mathrm{d0}$ | Window coordinate |
| XF2 | real $[\mathrm{cm}]$ | $0 . \mathrm{d0}$ | Window coordinate |
| YF1 | real $[\mathrm{cm}]$ | $0 . \mathrm{d0}$ | Window coordinate |
| YF2 | real $[\mathrm{cm}]$ | $0 . \mathrm{d0}$ | Window coordinate |

### 2.11 Mobility command

### 2.11.1 Models

The MObility-command defines the parameters for the intrinsic density, the carrier mobilities and the diffusion.
The intrinsic density and the carrier mobilities can depend on the temperature $T$ (the temperature is always normalized $T=\frac{\text { Temp in } K}{300 K}$ ), the dopant concentration $D$ and the electrical field $E$. Moreover, the dependence on the material $M$ can be considered by a constant factor. Thus, the quantities have the general form

$$
\begin{align*}
N_{i}^{\text {eff }}=N_{i}(T, M) & =N_{i}(T) N^{\text {mat }}(M)  \tag{2.30}\\
\mu_{n}^{\text {eff }}=\mu_{n}(T, D, E, M) & =\mu_{n}(T, D, E) \mu_{n}^{\text {mat }}(M)  \tag{2.31}\\
\mu_{p}^{\text {eff }}=\mu_{p}(T, D, E, M) & =\mu_{p}(T, D, E) \mu_{p}^{\text {mat }}(M) \tag{2.32}
\end{align*}
$$

The parameters $N_{i}(E N i), N^{\text {mat }}(M)(E N I F A)$ and $T$ (TEmp) can be set in the command DEvice.

Six models (parameter Model) are offered to handel different dependings of the mobilities on the temperature, doping, and the field strength.

### 2.11.2 General description of the models

## Model = 1

Use the basic quantities for the intrinsic density ( $N_{i}^{e f f}$ ) and the mobilities $\left(\mu_{n}^{e f f}, \mu_{p}^{e f f}\right)$.
Model $=2$
Mobilities and intrinsic carrier density depend on temperature and doping. No dependency on field strength.
Model $=3,5,6$
Like Model $=2$ but a saturation of the carrier velocity is taken into account. The formulas ( $2.52,2.36,2.39,2.60,2.62,2.40$ ) are used.

The models Model $=1,2,3,5,6$ are based on Einstein's relation between diffusion coefficient and mobility.

Model = 4
The same as Model $=3$ but a modified mobility for electrons and a generalized Einstein relation is used. This model is suitable for devices with electrons as majority-carriers like GaAS-MESFET devices.
The general dependence of the carrier mobilities $\mu_{n, p}(T, D, E, M)$ on temperature $T$, carrier concentration $D$, electrical field $E$ and material $M$, can be turned off, successively:
mobility( modell=5 amun4=0 amun5=0 amup4=0 amup5=0 egap=0 )
(no temperature dependence)
mobility( modell=5 gn=0 gp=0 evn=0 evp=0 amun4=0 amun5=0 amup4=0 amup5=0
egap=0 )
(completely no temperature dependence)
mobility ( modell=5 ealph=1 vgrn=1e+30 vgrp=1e+30 )
(no dependence on electrical field)
mobility ( modell=5 amun2=1e+30 amun3=0 amup2=1e+30 amup3=0 )
(no dependence on carrier concentration and/or dopants)
The dependence on the material $M$ can be turned off, setting
mobility ( modell=5 amunfa(1 $\left.1 \begin{array}{llllll}1 & 1 & 1 & 1 & 1 & 1\end{array}\right)$ amunfa(1 1
with mreg times the parameter 1 (here mreg=7).

### 2.11.3 Mobility dependence on the temperature

The following formulas and the defaults are taken from [Sel84, S. 86, 4.1-20] formulas (2.35,2.38), [Sel84, S. 87/88, 4.1-24/25] formulas (2.52,2.36,2.39), [Sel84, S. $95,4.1-48]$ formulas $(2.34,2.37)$, and [Sel84, S. 96, 4.1-54] formulas (2.60,2.62).

$$
\begin{gather*}
N_{i}(T)=N_{i} T^{\frac{3}{2}} e^{-\frac{1}{2} E_{g}(1-T)}  \tag{2.33}\\
\mu_{n}(T, D, E)=\frac{\mu_{n}(T, D)}{\left(1+\left(\frac{\mu_{n}(T, D) E_{n}^{\|}}{v_{n}^{\text {at }}}\right)^{\beta_{n}}\right)^{\frac{1}{\beta_{n}}}}  \tag{2.34}\\
\mu_{n}(T, D)=\mu_{n}^{\min }(T)+\frac{\mu_{n}(T)-\mu_{n}^{\min }}{1+\left(\frac{N_{A}+N_{D}}{c_{n}^{\text {ret }}(T)}\right)^{\alpha_{n}}}  \tag{2.35}\\
\mu_{n}(T)=\mu_{n} T^{-\gamma_{n}}, c_{n}^{\text {ref }}(T)=c_{n}^{\text {ref }} T^{-\kappa_{n}}, \mu_{n}^{\min }(T)=\mu_{n}^{\min } T^{-\delta_{n}} \tag{2.36}
\end{gather*}
$$

$$
\begin{gather*}
\mu_{p}(T, D, E)=\frac{\mu_{p}^{\min }(T, D)}{\left(1+\left(\frac{\mu_{p}^{\min }(T, D) E_{p}^{\|}}{v_{p}^{\text {sat }}}\right)^{\beta_{p}}\right)^{\frac{1}{\beta_{p}}}}  \tag{2.37}\\
\mu_{p}(T, D)=\mu_{p}^{\min }(T)+\frac{\mu_{p}(T)-\mu_{p}^{\min }}{1+\left(\frac{N_{A}+N_{D}}{c_{p}^{\text {ref }}(T)}\right)^{\alpha_{p}}}  \tag{2.38}\\
\mu_{p}(T)=\mu_{p} T^{-\gamma_{p}}, c_{p}^{\text {ref }}(T)=c_{p}^{\text {ref }} T^{-\kappa_{p}}, \mu_{p}^{\min }(T)=\mu_{p}^{\min } T^{-\delta_{p}} \tag{2.39}
\end{gather*}
$$

Some values are fixed: $\beta_{n}=2, \beta_{p}=1$.
The saturation can depend on temperature:

$$
\begin{equation*}
v_{n}^{\text {sat }}(T)=v_{n}^{\text {sat }} \cdot T^{-e_{n}}, v_{p}^{\text {sat }}(T)=v_{p}^{\text {sat }} \cdot T^{-e_{p}} \tag{2.40}
\end{equation*}
$$

Model: Model $=2$

$$
\begin{equation*}
N_{i}^{e f f}(T)=\sqrt{N_{c} * N_{v}} * \exp \left(-E_{g} /(2 k T)\right) \tag{2.41}
\end{equation*}
$$

The densities in conduction $N_{c}$ and valence $N_{v}$ bands and the band gap $E_{g}$ are calculated according to the formulas (see [Sel84], S.24-29):

$$
\begin{gather*}
N_{c}=2 *\left(6.28 * k T * m_{n} / \hbar^{2}\right)^{3 / 2}, \quad N_{v}=2 *\left(6.28 * k T * m_{p} / \hbar^{2}\right)^{3 / 2},  \tag{2.42}\\
E_{g}=E_{g 1}-E_{g 2} \cdot T-E_{g 3} \cdot T^{2},  \tag{2.43}\\
m_{n}=m_{0} \cdot\left(c_{n 1}+c_{n 2} \cdot T\right)  \tag{2.44}\\
m_{p}=m_{0} \cdot\left(c_{p 1}+c_{p 2} \cdot T-c_{p 3} \cdot T^{2}\right) \tag{2.45}
\end{gather*}
$$

Here, $m_{n}, m_{p}$ and $m_{0}$ are the effective electron mass, effective hole mass and electron rest mass. $\hbar$ is the Planck constant.
The dependence on temperature is considered according to the formulas (see $\left[\mathrm{SCW}^{+} 81\right]$ and [Sel84], S.82, 4.1-5/6).

$$
\begin{align*}
& \mu_{n}(T)=\left(\frac{T^{e_{n 1}}}{f_{n 1}}+\frac{T^{e_{n 2}}}{f_{n 2}}\right)^{-1}  \tag{2.46}\\
& \mu_{p}(T)=\left(\frac{T^{e_{p 1}}}{f_{p 1}}+\frac{T_{p 2}^{e_{p 2}}}{f_{p 2}}\right)^{-1} \tag{2.47}
\end{align*}
$$

### 2.11.4 Mobility dependence on dopants

$N_{A}, N_{D}$ are the dopant concentrations.

## Model: Model $=2,3$

The formulas are taken from [Sel84], S.37, (2.4-65).

$$
\begin{align*}
N_{i}^{e f f}(T, D) & =N_{i}^{e f f}(T) \cdot \exp \left(\frac{v_{1} \cdot a+\sqrt{a^{2}+C}}{U_{T}}\right)  \tag{2.48}\\
a & =\log \frac{C_{i}}{x_{n 0}}  \tag{2.49}\\
C_{i} & =N_{D}+N_{A} \tag{2.50}
\end{align*}
$$

$N_{i}^{e f f}(T)$ depends on temperature like for Model $=2$.
For the mobility, the following formulas, introduced from Arora et al (see [Sel84], S. 87/88, (4.1-24/25/29)), are used.

$$
\begin{gather*}
\mu_{n}(T, D)=\mu_{n}^{\min }(T)+\frac{\mu_{n}(T)}{1+\frac{C_{i}}{C_{n}^{\text {tet }}(T)}}  \tag{2.51}\\
\mu_{p}(T, D)=\mu_{p}^{\min }(T)+\frac{\mu_{p}(T)}{1+\frac{C_{i}}{C_{p}^{C_{p}^{e t}}(T)}},  \tag{2.52}\\
C_{i}=D \cdot\left(N_{D}+N_{A}\right)+(1-D) \cdot(n+p)  \tag{2.53}\\
C_{i}=0.667 \cdot\left(N_{D}+N_{A}\right)+0.333 \cdot(n+p) \tag{2.54}
\end{gather*}
$$

The last formulae is used in Model $=6$

## Model: Model $=4,5,6$

Formulas introduced from Caughey and Thomas are used (see [Sel84] S.95, (4.1-48) and S.86, (4.1-20))

$$
\begin{align*}
& \mu_{n}(T, D)=\mu_{n}^{\min }+\frac{\mu_{n}-\mu_{n}^{\min }}{1+\left(\frac{C_{i}}{c_{n}^{c_{t e}}}\right)^{\alpha_{n}}}  \tag{2.55}\\
& \mu_{p}(T, D)=\mu_{p}^{\min }+\frac{\mu_{p}-\mu_{p}^{\min }}{1+\left(\frac{C_{i}}{c_{p}^{\text {cef }}}\right)^{\alpha_{p}}} \tag{2.56}
\end{align*}
$$

### 2.11.5 Mobility dependence on the electric field

$E_{n, p}^{\|}$and $E_{n, p}^{\perp}$ are the transversal and parallel projections of the electrical field of the electron (hole) current vector.

Model: Model $=3,5$
The following formulas are used (see [Sel84], S.95, 4.1-48):

$$
\begin{align*}
& \mu_{n}(T, D, E)=\frac{\mu_{n}}{\sqrt{1+\left(\frac{\mu_{n} \cdot E_{n}^{\|}}{v_{n}^{\text {sat }}}\right)^{2}}}  \tag{2.57}\\
& \mu_{n}(T, D, E)=\frac{\mu_{p}}{1+\mu_{p} * E_{p}^{\| \|} / v_{p}^{\text {sat }}} \tag{2.58}
\end{align*}
$$

For EALPH $>0$ (Model = 3,5), the dependence on the electrical field is considered in a different way, due to [Yam83]

$$
\begin{gather*}
\mu_{n}(T, D, E)=\frac{\mu_{n}(T, D) G_{n}}{\left(1+\frac{\left(a_{n}^{c}\right)^{2}}{a_{n}^{c}+y_{n}}+\left(a_{n}^{s}\right)^{2}\right)^{\frac{1}{2}}}  \tag{2.59}\\
a_{n}^{c}=\frac{v_{n}^{c}}{y_{n}^{c}}, a_{n}^{s}=\frac{v_{n}^{c}}{v_{n}^{\text {sat }}}, v_{n}^{c}=\mu_{n}(T, D) G_{n} E_{n}^{\|}, G_{n}=\frac{1}{\left(1+\frac{E_{n}^{\perp}}{y_{n}^{\circ}}\right)^{\frac{1}{2}}}  \tag{2.60}\\
\mu_{p}(T, D, E)=\frac{\mu_{p}(T, D) G_{p}}{\left(1+\frac{\left(a_{p}^{c}\right)^{2}}{a_{p}^{c}+y_{p}}+\left(a_{p}^{s}\right)^{2}\right)^{\frac{1}{2}}}  \tag{2.61}\\
a_{p}^{c}=\frac{v_{p}^{c}}{y_{p}^{c}}, a_{p}^{s}=\frac{v_{p}^{c}}{v_{p}^{s a t}}, v_{p}^{c}=\mu_{p}(T, D) G_{p} E_{p}^{\|}, G_{p}=\frac{1}{\left(1+\frac{E_{p}^{\perp}}{y_{p}^{\circ}}\right)^{\frac{1}{2}}} \tag{2.62}
\end{gather*}
$$

Model: Model $=4$
Electron mobility and diffusion coefficient $D$ are calculated in the following way (see [YTK75]). The hole mobility does not depend on the electrical field. The Einstein condition is used. $E$ is the absolute value of the electic field.

$$
\begin{gather*}
\mu_{n}(T, D, E)=\frac{\mu_{n}(T, D)+v_{n}^{\text {sat }} \frac{E^{3}}{E_{\text {crit }}^{4}}}{\left(1+\frac{E}{E_{\text {crit }}}\right)^{4}}  \tag{2.63}\\
D=U_{T} \cdot \mu_{n}(T, D), \text { if } E<D_{0},  \tag{2.64}\\
D=\mu_{n}(T, D) \cdot\left(U_{T}+2 / 3 * D_{1} * E^{2} \cdot \mu_{n}(T, D)\right), \text { if } E \geq D_{0}, \tag{2.65}
\end{gather*}
$$

## Model: Model $=6$

A reduction of the mobility on the surface of the device is taken into account (see Selberherr, Schütz und Pützl, in Process and Device Simulation for MOS-VLSI Circuits, edi. by Antognetti et.al., The Hagü 1983, Martinus Nijhoff Publishers.)

$$
\begin{align*}
\mu_{n}(T, D, E) & =A_{n} /\left(1+\left(A_{n} * E_{n}^{\| \|} / v_{n}^{\mathrm{sat}}(T)\right)^{2}\right)^{1 / 2}  \tag{2.66}\\
\mu_{p}(T, D, E) & =A_{p} /\left(1+A_{p} * E_{p}^{\|} / v_{p}^{\text {sat }}(T)\right) \tag{2.67}
\end{align*}
$$

with

$$
\begin{align*}
v_{n}^{\text {sat }}(T) & =v_{n}^{\text {sat }} T^{-e_{n}}  \tag{2.68}\\
v_{p}^{\text {sat }}(T) & =v_{p}^{\text {sat }} T^{-e_{p}}  \tag{2.69}\\
A_{n} & =B_{n} \cdot \mu_{n}(T, D)  \tag{2.70}\\
A_{p} & =B_{p} \cdot \mu_{p}(T, D)  \tag{2.71}\\
B_{n} & =\left(Y+Q_{n}\right) /\left(Y+\left(2+E_{n}^{\perp} / E_{n 0}^{\perp}\right) \cdot Q_{n}\right)  \tag{2.72}\\
Q_{n} & =y_{n 0} /\left(1+E_{n}^{\|} / E_{n 0}^{\|}\right),  \tag{2.73}\\
B_{p} & =\left(Y+Q_{p}\right) /\left(Y+\left(2+E_{p}^{\perp} / E_{p 0}^{\perp}\right) \cdot Q_{p}\right)  \tag{2.74}\\
Q_{p} & =y_{p 0} /\left(1+E_{p}^{\|} / E_{p 0}^{\|}\right), \tag{2.75}
\end{align*}
$$

### 2.11.6 Parameters

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| A1 | real | $1.35 \mathrm{~d}-20$ |  |
| A2 | real | 3.59d-18 |  |
| A3 | real | 2.86d-17 |  |
| ALN | real | $0.125 d 0$ |  |
| ALP | real | 0.0317 d 0 |  |
| AMUNO | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 1030.d0 | $\mu_{n}$ in (2.36) |
| AMUN1 | real | 0.72 d 0 | $\alpha_{n}$ in (2.36) $\longrightarrow(2.35)$ |
| AMUN2 | real $\left[\mathrm{cm}^{-3}\right]$ | 8.5d16 | $c_{n}^{\text {ref }}$ in (2.36) $\longrightarrow(2.35)$ |
| AMUN3 | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 65.d0 | $\mu_{n}^{\min }$ in (2.36) $\longrightarrow(2.35)$ |
| AMUN4 | real | 2.546 d 0 | $\kappa_{n}$ in (2.36) |
| AMUN5 | real | 0.57 d 0 | $\delta_{n}$ in (2.36) |
| AMUNFA () | real | 1.d0 | $\begin{aligned} & \mu_{n}^{\text {mat }}(M) \text { in }(2.31), \\ & M=1, \ldots, \text { mreg } \end{aligned}$ |
| AMUPO | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 495.d0 | $\mu_{p}$ in (2.39) |
| AMUP1 | real | 0.76 d 0 | $\alpha_{p}$ in (2.39) $\longrightarrow(2.38)$ |
| AMUP2 | real $\left[\mathrm{cm}^{-3}\right]$ | 6.3d16 | $c_{p}^{\text {ref }}$ in (2.39) $\longrightarrow(2.38)$ |
| AMUP3 | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 47.7 d 0 | $\mu_{p}^{\min }$ in (2.39) $\longrightarrow(2.38)$ |
| AMUP4 | real | 2.546 d 0 | $\kappa_{p}$ in (2.39) |
| AMUP5 | real | 0.57 d 0 | $\delta_{p}$ in (2.39) |
| AMUPFA () | real | 1.d0 | $\begin{aligned} & \mu_{p}^{\text {mat }}(M) \text { in }(2.32), \\ & M=1, \ldots, \text { mreg } \end{aligned}$ |
| BETA | real | 1.d0 |  |
| Bn | real $[\mathrm{cm} / \mathrm{s}]$ | 4.75 d 7 |  |
| Bp | real $[\mathrm{cm} / \mathrm{s}]$ | 9.925d6 |  |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| C | real | 0.5 d 0 | formula (2.48) |
| CN | real | 1.74 d 5 |  |
| CN1 | real | 1.045 d 0 | $c_{n 1}$ in formula (2.44) |
| CN2 | real | 4.5d-4 | $c_{n 2}$ in formula (2.44) |
| CONstant | integer | 1 |  |
| CP | real | 8.842d5 |  |
| CP1 | real | 0.523 d 0 | $c_{p 1}$ in formula (2.45) |
| CP2 | real | $1.4 \mathrm{~d}-3$ | $c_{p 2}$ in formula (2.45) |
| CP3 | real | $1.48 \mathrm{~d}-6$ | $c_{p 3}$ in formula (2.45) |
| DLN | real | 5.82 d 14 |  |
| DLP | real | 2.05 d 14 |  |
| DIFE0 | real | 0. | $D_{0}$ in formula (2.64) |
| DIFTau | real [s] | 1E-13 | $D_{1}$ in formulas (2.64, 2.65) |
| DOTKOM | real | 1.d0 | $D$ in formula (2.53) |
| Ealph | real | 1.d0 | toggel Model $=3,5$ see formu- <br> las (2.57-2.62) |
| EG1 | real [V] | 1.1785d0 | $e_{g 1}$ in formula (2.43) |
| EG2 | real [V] | 9.025d-5 | $e_{g 2}$ in formula (2.43) |
| EG3 | real [V] | 3.05d-7 | $e_{g 3}$ in formula (2.43) |
| EGAP | real [V] | 1.12d0 | $E_{g}$ in (2.52) |
| EKrit | real [V/cm] | 4d3 | $E_{\text {crit }}$ in formula (2.63) |
| EN1 | real | 1.5d0 | $e_{n 1}$ in formula (2.46) |
| EN2 | real | 3.13d0 | $e_{n 2}$ in formula (2.46) |
| EPON | real [V/cm] | 1.E4 | $E_{n 0}^{\\|}$in formula (2.73) |
| EPOP | real [ $\mathrm{V} / \mathrm{cm}$ ] | 8.E3 | $E_{p 0}^{\\|}$in formula (2.75) |
| EP1 | real | 1.5 d 0 | $e_{p 1}$ in formula (2.47) |
| EP2 | real | 3.25d0 | $e_{p 2}$ in formula (2.47) |
| ETON | real [V/cm] | 1.8E5 |  |
| continued on next page |  |  |  |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| ETOP | real [V/cm] | 3.8 E 5 | $E_{p 0}^{\perp}$ in formula (2.74) |
| EVN | real | 0.87 d 0 | $e_{n}$ in formula (2.40) |
| EVP | real | 0.52d0 | $e_{p}$ in formula (2.40) |
| FN1 | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 4195.d0 | $f_{n 1}$ in formula (2.46) |
| FN2 | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 2153.d0 | $f_{n 2}$ in formula (2.46) |
| FP1 | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 2502.d0 | $f_{p 1}$ in formula (2.47) |
| FP2 | $\begin{aligned} & \text { real } \\ & {\left[\mathrm{cm}^{2} /(\mathrm{Vs})\right]} \end{aligned}$ | 591.d0 | $f_{p 2}$ in formula (2.47) |
| GAMMA | real | 0.d0 |  |
| General | integer | 3 |  |
| GN | real | 2.33d0 | $\gamma_{n}$ in (2.36) |
| GP | real | 2.23d0 | $\gamma_{p}$ in (2.39) |
| IFELD | integer | 1 |  |
| MESFET | integer | 4 |  |
| Modell | integer | 5 | number of model |
| Temp | integer | 2 |  |
| T300K | integer | 5 |  |
| V1 | real [V] | 9d-3 | $v_{1}$ in formula (2.48) |
| VGRN | real [cm/s] | 1.d7 | $v_{n}^{\text {sat }}$ in (2.60) $\longrightarrow(2.59)$ |
| VGRP | real $[\mathrm{cm} / \mathrm{s}]$ | 8.37d6 | $v_{p}^{\text {sat }}$ in (2.62) $\longrightarrow(2.61)$ |
| XNO | real $\left[\mathrm{cm}^{-3}\right]$ | 1.d17 | $x_{n 0}$ in formula (2.49) |
| YON | real [cm] | 5.E-7 | $y_{n 0}$ in formula (2.73) |
| YOP | real [cm] | 4.E-7 | $y_{p 0}$ in formula (2.75) |
| YETON | real [ $\mathrm{V} / \mathrm{cm}$ ] | 6.493 d 4 | $y_{n}^{\circ}$ in (2.60) $\longrightarrow(2.59)$ |
| YETOP | real [V/cm] | 1.869 d 4 | $y_{p}^{\circ}$ in (2.62) $\longrightarrow(2.61)$ |
| YGN | real | 8.8d0 | $y_{n}$ in (2.60) $\longrightarrow(2.59)$ |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| YGP | real | 1.6 d 0 | $y_{p}$ in $(2.62) \longrightarrow(2.61)$ |
| YVCN | real $[\mathrm{cm} / \mathrm{s}]$ | 4.9 d 6 | $y_{n}^{\mathrm{c}}$ in $(2.60) \longrightarrow(2.59)$ |
| YVCP | real $[\mathrm{cm} / \mathrm{s}]$ | 2.928 d 6 | $y_{p}^{\mathrm{c}}$ in $(2.62) \longrightarrow(2.61)$ |

### 2.12 Numeric command

The NUmeric-command is used to define the accuracy and termination parameters required for the numerical calculations.

### 2.12.1 Some comments on the numerical methods

A Gummel-Iteration $U_{i+1}$ with a current $J_{i+1}$ is accepted as solution, if the following conditions are fullfilled:

$$
\begin{align*}
\operatorname{dist}\left(U_{i-1}, U_{i}\right)+\operatorname{dist}\left(U_{i}, U_{i+1}\right) & \leq 2 \cdot \text { EPGUAB }  \tag{2.76}\\
\operatorname{dist}\left(J_{i}, J_{i+1}\right) & \leq\left|J_{i+1}\right| \cdot \operatorname{EPCURE} . \tag{2.77}
\end{align*}
$$

A Newton-Iteration $U_{i}$ is accepted as solution of the nonlinear Poisson equation, if the following condition is fullfilled:

$$
\begin{equation*}
\operatorname{dist}\left(U_{i-1}, U_{i}\right) \leq \text { EPPOAB. } \tag{2.78}
\end{equation*}
$$

A CG-Iteration $U_{j k}$ is accepted as $(j+1)$-th approximation of the solution of the nonlinear Poisson equation, if the following condition is fullfilled:

$$
\begin{equation*}
\operatorname{dist}\left(U_{j k-1}, U_{j k}\right) \leq \operatorname{dist}\left(U_{i-1}, U_{i}\right) \cdot \text { EPPORE. } \tag{2.79}
\end{equation*}
$$

Moreover, EPPORE is the relative termination constant for the Jacobi-Iteration of the continuity equations.

For transient calculations EPPOAB and EPPORE are used as termination constant if MOCKEU > 1 .

A Jacobi-Iteration $N_{j k}$ is accepted as $(j+1)$-th Gummel-approximation of the electron density $N_{j+1}$ if

$$
\begin{equation*}
\operatorname{def}_{n}\left(N_{j k}\right) \leq \operatorname{def}_{n}\left(N_{j}\right) \cdot \operatorname{EPCURE} \tag{2.80}
\end{equation*}
$$

Here $\operatorname{def}_{n}(\cdot)$ is the defect of the continuity equation for electrons (similar for the hole equation).

The embedding method for the calculation of a UI-characteristic-line is controlled in the following way: The euclidian norm $|\cdot|$ of a new working point $A_{i+1}$ has to satisfy

$$
\begin{equation*}
\left|A_{i+1}-A_{i}\right| \leq \frac{\left|A_{i+1}-A_{i}\right|}{F\left(x_{i}, x_{i-1}\right)} \cdot \text { FISTEP } \tag{2.81}
\end{equation*}
$$

Here $x_{i}=\left(U_{i}, N_{i}, P_{i}\right)$ is the solution vector and $F$ the free energy functional

$$
\begin{equation*}
F(X, x)=\frac{1}{2} \int\left(\varepsilon|\nabla(U-u)|^{2}+k T((N-n) \log N / n+(P-p) \log P / p)\right) d x \tag{2.82}
\end{equation*}
$$

For transient calculations the new time step $\delta_{n}$ is calculated from the old time step $\delta_{o}$ according to the relation

$$
\begin{equation*}
\delta_{n} \leq \delta_{o} \sqrt{\frac{\text { EPSTEP }}{F\left(X(t), X\left(t-\delta_{o}\right)\right)}} \tag{2.83}
\end{equation*}
$$

Here $X(t)=(U(t), N(t), P(t))$ is the solution vector at time $t$ and $F$ the free energy functional.
A calculation is switched from Gummel- to Newton-iterations, if the following conditions are fullfilled:

$$
\begin{align*}
\text { test }_{j} & \leq \text { SNEWT, }^{2}  \tag{2.84}\\
\text { test }_{j} \cdot \text { GUMNEW } & \leq \text { test }_{j-1},  \tag{2.85}\\
\text { def }_{j} \cdot \text { GUMNEW } & \leq \text { def }_{j-1} . \tag{2.86}
\end{align*}
$$

We have a cancellation threshold OMItnp for the continuity equations:

$$
\begin{align*}
\operatorname{def}_{n} & \leq \operatorname{def}_{n} \cdot \text { OMItnp }  \tag{2.87}\\
\operatorname{def}_{p} & \leq \operatorname{def}_{p} \cdot \text { OMItnp. } \tag{2.88}
\end{align*}
$$

### 2.12.2 Parameters

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| SFActo | real | $1 . \mathrm{d} 0$ |  |
| AZEr | real | $1 . \mathrm{do}$ | current splines at boundary |
| CUitre | real | $10 . \mathrm{do}$ |  |
| CURnul | real | $1 . \mathrm{d}-16$ | zero current threshold |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| Damp0 | real | 1.d-10 | Initial value for the regularisation parameter Damp (improvement of the conditioning of the current matrices) |
| DELzer | real | 2.0d0 | current splines at boundary |
| EPCure | real | 0.001 do | termination constant, see ( $2.77,2.80$ ) |
| EPGUAB | real | 0.01 d 0 | termination constant, see (2.76) |
| EPPOAB | real | 0.01 do | termination constant, see (2.78) |
| EPPORE | real | 0.01 d 0 | termination constant, see (2.79) |
| EPSIL | real |  | $\varepsilon$ in formula (2.82) |
| EPStep | real | 0.5 d 0 | Control value for the instationary (transient) case, see (2.83) |
| FISTEP | real | 1.d10 | Control value for the stationary case, see (2.81) |
| GUMnew | real | 1.5d0 | Threshold value for the transition from Gummel- to Newton method, see $(2.85,2.86)$ |
| IANEW | integer | 0 |  |
| IGUMAX | integer | 100 |  |
| IRAND | integer | 0 |  |
| IRed | integer | 5 | Maximum number of bisection for the Newton method. |
| ITnew | integer | 20 | Maximum number of block iterations for the Newton method and the AC analysis. |
| OMItnp | real | 0.001 d 0 | Threshold value for the cancellation of the $n$ - and $p$ equations, see (2.87,2.88) |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| PARdiso | integer | 0 | switch on Pardiso |
| POFAK | real | $1 . \mathrm{d0}$ | $1 . \mathrm{d0}$ |
| RELax | real | SOR parameter for the AC <br> analysis. |  |
| SNEwt | real | 3.0 dO | Threshold value for the transi- <br> tion to Newton's method, see <br> $(2.84)$ |
| TEPot | real | $2 . \mathrm{dO}$ |  |

### 2.13 Control and Replace command

The record parameter CONTrol is used for general control purposes in particular for the grid adaptation. The parameters can be specified in the REPLace command in the normal command input mode and in the TControl mode
REPLace(CONTrol (name=value))

They can be specified in most of the process steps locally
GRID (CONTrol(MAXtrl=2)).

First all parameters declared in the REPLace command are reset to their default values. Then the required modifcations are done and the modified values are stored as new default values. Note! When using the REPLace command in the TControl mode local changes in the process step are lost In the REPLace-command, the CONTrol record and the variable parameters VARiable(...) can be specified.

The command ADAPtation() can be used to force a readaptation of the grid In the TControl mode a readaptation can be required at the end of the current step by REPLace (CONTrol (LADA=1)). The ADAPtation command can not be used in the TControl mode.

### 2.13.1 Parameters

| parameter name | unit <br> type <br> options | default value | comment |
| :---: | :---: | :---: | :---: |
| VAroutswit | integer |  | Selects the variables for the default print of integrals and extremal values. For each variable ivar there is defined a parameter varout(ivar). For LPRot=2 the extremal values and integrals of variables with varout(iva) $\geq$ varoutswitch are printed each time step. |
| NPrint | integer | undefined | Number of time steps after which the last Print com$\operatorname{mand}(\mathrm{s})$ are repeated. If undefined or $<0$, no output is done, otherwise also at the end of each process step. |
| NGraphic | integer | undefined | Number of simulation steps after which a new picture is drawn. If undefined or $<0$, no output is done, otherwise also at the end of each simulation step. |
| NSAve | integer | undefined | Number of simulation steps after which a save file is written. If undefined, no automatical saves are done for $<0$. Even explicit save commands are ignored. For $\geq 0$ a save file is written at the end of each simulation step. |
| Saveeach | Time | undefined | Defines a time (human time, neither CPU nor simulated processing time) after which a save file is written. |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| SName | string*80 |  | Save file name. Used for the automatically saved files. A counter is added to the file name, and the file name is written to terminal and protocol. |
| SIndex | integer | -2 | Defines the index of the first automatically saved file if $\geq$ 0 . If undefined no index is added. If -1 , the index of a loaded file is incremented by 1 and used for the first automatically saved file. If -2 , the automatical save toggles between indices -1 and -2 . This is the default. |
| MAXV | integer | undefined | Maximum number of nodes during grid adaptation. Specify this value rather than MAXVDelaunay to limit the mesh size. |
| MPOINTS | integer | 0 | MPOINTS integer Maximum number of points in the layer system. Internally increased, if necessary. |
| MAXVDel | integer | undefined | Maximum number of nodes in the final simulation grid. Contains all mesh points in triangles and line segments. If specified, delaunization of the mesh might be incomplete. |
| IOU | integer | 6 | Terminal output channel. In batch mode the only output channel. |


| name | unit <br> type option | default | comment |
| :---: | :---: | :---: | :---: |
| IPU | integer | 4 | Output channel for the protocol. For IPU no protocol file is written. |
| PNV1 | integer | 10000 | First node to be printed in a list. |
| PNV2 | integer | 1 | Last node to be printed in a list. |
| PNT1 | integer | 10000 | First triangle to be printed in a list. |
| PNT2 | integer | 1 | Last triangle to be printed in a list. |
| AR1 | integer | 10000 | First area in a Print command. |
| AR2 | integer | 1 | Last area in a Print command. |
| LI1 | integer | 10000 | First line in a Print command. |
| LI2 | integer | 1 | Last line in a Print command. |
| ITYPhc | integer |  | Type of "honeycomb" for each of the nodes. |
|  | 1 |  | "Honeycomb" defined by lines connecting triangle vertex and midpoint of opposite edge. |
|  | 2 |  | Voronoi cells. |
|  | 3 |  | Voronoi cells in cylindrical coordinates, for rotational symmetric 3D situations. X-axis: radius. $X=0$ origin of cylin der coordinates. Y-axis height. |
| LPRot | integer | 0 | Length of the protocol file (0/1/2) |

continued on next page

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| XX | real | 1 | Coefficient for coordinate transformations (input and output) e.g. load of external doping and grid. $x_{\text {foreign }}=$ $\mathrm{xx} \cdot x_{\text {dios }}+\mathrm{xy} \cdot y_{\text {dios }}+\mathrm{x} 0$ $y_{\text {foreign }}=\mathrm{yx} \cdot x_{\text {dios }}+\mathrm{yy} \cdot y_{\text {dios }}+$ y0 |
| XY | real | 0 |  |
| X0 | Length | undefined |  |
| YX | real | 0 |  |
| YY | real | -1 (!!!) |  |
| YO | Length | undefined |  |
| MASS | integer | 2 | Selection of triangle measure in trmas.f |
|  | 1 |  | Arithmetic average of the gradients of the logarithm of the concentrations along the triangle edges. |
|  | 2 |  | Maximum of the gradients of the logarithm of the concentrations along the triangle edges This is the default. |
|  | 6 |  | Difference of the logarithms (ashsur) of the concentrations along the triangle edges. |
| INFO | integer | 0 | General control of the terminal output. In particular, used to print model parameters and for test prints. |
| MAXVFL | integer | 0 | Maximum number of refinement loops per refinement criterion. Internal default 2.MAXTRI. |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| IPGRID | integer | 0 | Draw the grid during the refinement. 1: Draw the nested ITRI-grid at the end of adaptation. 2: Draw all ITRI-grids during adaptation. 3: Draw each UTRI-grid during adaptation and at any change of the layer system. $>3$ : Draw each ITRI- and each UTRI- grid. |
| IVERADA | Percent | 10\% | Fraction of "bad" triangles that is allowed without readaptation. If more triangles ar found to be "bad" the grid is readapted. |
| AUTOada | integer | 1 |  |
|  | -1 |  | Turns off the automatic readaptation of the grid. |
|  | 1 |  | Turns on the automatic readaptation of the grid. |
|  | 0 |  | Automatic readaptation of the grid is turned off internally since the refinement with respect to MARKM was not finished. |
| MAXTRI | integer | 4 | Maximum triangle level (only triangles of the MAXTRI-1 generation or a lower generation can be marked for refinement). |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| TRI () | record |  | For each of the materials a separate MAXTRI value can be defined. TRL (SI=3,0X=5) All materials that are not specified receive the global value. Note! The refinement criteria are limited by the maximum of the global value and the values for the materials. |
| DX | Length | $\mu$ | The smallest triangle might be defined by a length. From the length MAXTRI is determined. |
| DXL () | record |  | For each of the materials a separate DX can be prescribed. From this TRI is determined. |
| MARKH | integer | 0 | Parameter for the homogeneous refinement. |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level < - MARKH. |
| MARKM | integer | -4 | Parameter for the refinement of doping gradients |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level $<-$ MARKM. |
| MARKGS | integer | 1 | parameter for the refinement of "green stars". 0: off, 1:on <br> Note! 1 may require a lot of refinement loops. |
| REC1 ( | record |  | First rectangle used for the refinement. |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| Markr | integer | -4 | $>0$ Number of refinement loops. < 0 Refine only triangles with a triangle level $\leq$ Markr. |
| XLeft | Length [ $\mu \mathrm{m}$ ] | 0. | Left boundary. |
| XRight | Length [ $\mu \mathrm{m}$ ] | -1 | Right boundary. |
| YBottom | Length [ $\mu \mathrm{m}$ ] | 0. | Bottom boundary. |
| YTop | Length [ $\mu \mathrm{m}$ ] | -1 | Top boundary. |
| Icoswitch | Geometrical <br> Physical | Geometrical | Type of coordinates. |
| MAXtrl |  |  | Maximum triangle level in the rectangle. The grid remains coarse even if a refinement criterion is met. |
| ) |  |  | End of record REC. |
|  |  |  | The rectangles $2,3, \ldots, 10$ can be specified similarly. By default for these rectangles Icoswitch = Physical. |
| MARKG | integer | -5 | Parameter for the refinement at material interfaces |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level $<-$ MARKG. |
|  |  |  | Note! For a very coarse grid several interfaces may intersect a triangle edge. The boundary type might not be defined properly from the materials of the nodes. |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| MARKP | integer | -6 | Parameter used for the refinement in the vicinity of certain points. Vertices and steps in lines of the layer system are defined internally and used in the refinement. |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level $<-$ MARKP. |
| POInts() | record [ $\mu \mathrm{m}$ ] |  | Vector of $x-$ and $y-$ coordinates of $\leq 100$ points to be marked in MARKP. Vertices and points with large curvature are defined in the layer system and added to the user-defined list. |
| MARKGNR | record | 2 | List of boundary types used for the boundary refinement. For the readaptation before a WIAS-TeSCA simulation, the contact numbers have to be specified: -1...-ndiri for metal contacts and 1...nnatur for gate contacts. The level of refinement is controlled by MARKG. |
| MARKJ | integer | -5 | Refinement at p-n-junctions. |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level < -MARKJ. |
| MARKL | integer | 1 | Refinement of triangles in front of doping fronts. |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level MARKL. |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| MARKMAX | integer | -4 | Refinement at local dopant maximum. To prevent a homogeneous refinement, only functions with minimum variation are handled: varmax > CMAMI - varmin |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level $<-$ MARKMAX. |
| MARKI | integer | 0 | Refinement of triangles with change of the curvature of the doping (concave-convex). |
|  | $>0$ |  | Number of refinement loops. |
|  | $<0$ |  | Refine only triangles with a triangle level < - MARKI. |
| 1D | boolean | off | Automatical grid adaptation during a 1D simulation for $1 \mathrm{D}=\mathrm{on}$. The grid is adapted as usual according to the refinement criteria. After refinement the $y$-coordinates at the left side of the refined grid are used to construct a 1D grid. |
| ANGstroem | Length | $1 \mathrm{e}-4$ | Internal test length. |
| IVER() | record |  | For each of the variables var a critical triangle measure IVER(var) (in \%) is defined such that the triangle is refined if the limit is exceeded measure (var, triangle) $>$ IVER(var) |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| ASHdiff | real | 1. | Reference value for the differences of ashsur (conc) from MASS=6. A triangle is refined if $\frac{\operatorname{ashsur}(c 1)-\text { ashsur (c2) }}{\text { ASHdiff }}>$ IVER/100. |
| RESM | real | 1. | "Reserve" factor for the triangle size. Prevents from frequently readaptation. If the area of a triangle $k$ exceeds RESM $\cdot a_{m}$ the triangle $k$ has to be checked for the grid quality. Here $a_{m}$ denotes the area of the largest triangle that would be refined by MARKM right after the grid adaptation. |
| RESJ | real | 1.5 | "Reserve" factor for the triangle size for MARKJ. |
| RESI | real | 1.5 | "Reserve" factor for the triangle size for MARKI. |
| CMAMI | real | 1000. | MARKMAX is applied only to functions with a minimum variation: varmax $>$ CMAMI. varmin. |
| IMAX () | Percent [\%] | 90 | For each of the variables var a maximum value IMAX (var) in $\%$ is defined. If the concentration exceeds the value for one of the nodes in the triangle, i.e., value(var, node(triangle)) $>\operatorname{varmin}+\frac{\operatorname{IMAX}(\mathrm{var})}{100}$ (varmax - varmin ), the triangle is refined. |

continued on next page

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| CMAX | record $\left[\mathrm{cm}^{3}\right]$ | 1 e 23 | For each of the variables var a maximum value CMAX (var) is defined. If the concentration exceeds the value for one of the nodes in the triangle, i.e., value(var, node(triangle)) $>$ CMAX (var) the triangle is refined. |
| LADA | integer | 1 | Turns on the grid readaptation. May be defined in the TControl mode. At the end of the current simulation step the grid is readapted. |
| REAdapt | integer | 1 | Controls complete readaptation ( $=1$ ) or further refinement $(=0)$ of the grid. |
| RETriangul | ate integer | 1 | Selection of the user grid before a readaptation. |
|  | 1 |  | Use the previous coarse grid. |
|  | 2 |  | Use the old geometrical grid. |
|  | 3 |  | Construct a new user grid using the last defined GRID parameters. |
| MOvtrans | No Extrema <br> Integral <br> EPIintegral | EPIintegral | Selection of the rescaling type of the dopants after a vertical grid transformation, i.e. compute integral and extrema before the vertical transformation and rescale the profiles to restore minimum/maximum or the minimum/integral after the transformation. By default restore minimum/integral only during epitaxy. |

continued on next page
\(\left.$$
\begin{array}{llll}\hline \text { name } & \begin{array}{l}\text { unit } \\
\text { type } \\
\text { option }\end{array} & \text { default } & \text { comment } \\
\hline \text { STCenter } & \text { integer } & 5 & \begin{array}{l}\text { Number of simulation steps af- } \\
\text { ter which the grid is centered. }\end{array} \\
\hline \text { BFLip } & \text { integer } & 20 & \begin{array}{l}\text { Number of edge flipping loops } \\
\text { before a grid centering. }\end{array} \\
\hline \text { CEnter } & \text { integer } & 2 & \begin{array}{l}\text { Number of grid centering } \\
\text { loops. }\end{array} \\
\hline \text { EFLip } & \text { integer } & 20 & \begin{array}{l}\text { Number of edge flipping loops } \\
\text { after a grid centering. }\end{array} \\
\hline \text { AFLip } & \text { Angle ["] } & 115 & \begin{array}{l}\text { Maximum angle that is allowed } \\
\text { after the edges are flipped. If } \\
\text { the edge flipping would lead to }\end{array}
$$ <br>
larger (but compensated) an- <br>
gles the edges are not flipped <br>
since otherwise a "hole" in the <br>

grid would be created.\end{array}\right]\)| Factor to multiply the radii of |
| :--- |
| surrounding spheres for detect- |
| ing non-Delaunay situations. |
| Must be 1. |
| stabilities arising from round- |
| ing errors. |


| name unit <br> type <br> option default comment |  |  |  |
| :--- | :--- | :--- | :--- |
| LAtriangle integer | 2 | Number of neighboring trian- <br> gle shells, added for the next <br> centering step, if the local cor- <br> rection failed. |  |
| LACenter | integer | 3 | Number of added centering <br> loops, if neighboring triangle <br> shells have to be added. |
| LCTriangleEdges Wedges <br> Triangle <br> WTriangl No | Triangle | Selection of the local centering <br> method. |  |
| integer | 2000 | Maximum number of edges in- <br> cident into a bulk node of the <br> mesh. If the number is ex- <br> ceeded, an additional subdivi- <br> sion is done. |  |
| CInterface integer | 2000 | Maximum number of edges in- <br> cident into an interface node of <br> the mesh. If the number is ex- <br> ceeded, an additional subdivi- <br> sion is done. |  |

### 2.14 Substrate command

The SUBStrate command is used to initialize the layer system.
The location of the layer system in the X- and Y-direction can be defined (XLeft, XRight, YBottom, YTop). In addition also the initial position of the substrate surface YSubs can be prescribed. If these values are not specified the values are copied from the GRID command.

### 2.14.1 Parameters

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| YSubs | Length $[\mu \mathrm{m}]$ | 0.0 dO | initial position of the substrate <br> surface |
| XLeft | Length $[\mu \mathrm{m}]$ | 0.0 dO | left end of the substrat region |
| XRight | Length $[\mu \mathrm{m}]$ | 0.0 dO | right end of the substrat region |
| YBottom | Length $[\mu \mathrm{m}]$ | 0.0 dO | bottom of the substrat region |
| YTop | Length $[\mu \mathrm{m}]$ | 0.0 dO | Initial top position of the en- <br> tire layer system |

### 2.15 Special command

The SPECIAL command is used for physical effects not covered by the standard model. This includes hot carrier injection models for gate leakage and the generation of charge by the trace of an incident particle. The latter can be used as a simple model describing the Lambert-Beer absorption in solar cells.

### 2.15.1 Parameters

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| Aisf | real | -0.0287d0 |  |
| AE | real | 1.d0 |  |
| ALpha | real | 3d4 |  |
| ALPHA1 | real [cm] | 1d3 |  |
| ALPHA2 | real [cm] | $0 . \mathrm{d} 0$ |  |
| ALPHAL | real [cm] | $0 . \mathrm{d} 0$ |  |
| Bisf | real | 8.4933d0 |  |
| ELAM | real [V] | 0.2 d 0 |  |
| EMN | real | 0.5 d 0 | Eff. electron mass of hot electrons |
| EMP | real | 0.5 d 0 | Eff. holes mass of hot electron |
|  |  |  | continued on next page |



| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| TMean | real [s] | 1.d-9 |  |
| TNO | real $\left[\mathrm{cm}^{-3}\right]$ | 3.125d18 | track density |
| TS | real | 7.21d7 |  |
| WS | real [cm] | 1.d-3 |  |
| WTRack | real [cm] | $0.1 d-4$ | track width |
| X1 | real | 8.26d-6 |  |
| X1S | real | 4.40d-4 |  |
| X2 | real | 11.3d0 |  |
| X2S | real | 3.72d0 |  |
| X3 | real | -0.745d0 |  |
| X3S | real | -0.66d0 |  |
| XF1 | real [cm] | $0 . \mathrm{d} 0$ | track limiting |
| XF2 | real [cm] | $0 . \mathrm{d} 0$ | track limiting |
| XN1S | real $\left[\mathrm{cm}^{-3}\right]$ | 9.48 d 13 |  |
| XN2S | real $\left[\mathrm{cm}^{-3}\right]$ | 3.01d10 |  |
| XNS | real $\left[\mathrm{cm}^{-3}\right]$ | 1.24 d 11 |  |
| XS | real | 1d-3 |  |
| XS1 | real | $1.4 \mathrm{~d}-6$ |  |
| YO | real [cm] | 0.0d-7 | track model |
| Y1 | real [cm] | 3.0d-7 | track model |
| YF1 | real [cm] | $0 . \mathrm{d} 0$ | track limiting |
| YF2 | real [cm] | 0.d0 | track limiting |

### 2.16 Save command

The SAVE command is used, to write output files for subsequent evaluation, continuation of the simulation (.dmp*) and for offline coupling to other simulation tools, respectively.

SAVE (File=xxx, TYPe=dmp, exp, prf, plf, dmp.gz, bound, dp, cmd, geb, mdraw, dmp.Z, dom, USer, ITri, Picasso, MESHDp, lay, lai,

## KPIF) )

By default a binary WIAS-TeSCA save file is written. All the other supported file types can be derived from a .dmp file, after loading it into WIAS-TeSCA.

## Geometry Description

The geometry description in the xxx.rand file contains the polygons that define regions and contacts. A MATerial() list or an Arealist() can be specified to select regions. By default all WIAS-TeSCA regions are selected.
The WIAS-TeSCA material names are "translated" into DATEX material names.

## Contact Definition

Up to 20 contacts for device simulation can be defined in the data record Contacts(Contact1 (name= , $x=$, $y=, x e=, y e=$ )...).

If all parameters for a contact are specified, a list of line segments is defined and added into the .rand file as a contact region. The line in the WIAS-TeSCA layer system, closest to the two specified points is determined. The two WIAS-TeSCA points closest to the specified start and end of the contact are kept but all line segments in between are smoothed in the usual way. After smoothing the line segments between the two points are defined as contact. All line segments of one contact are on the same DIOS line.
If xe, ye remain undefined for a contact, one of the WIAS-TeSCA regions is renamed. The approximate position $\mathrm{x}, \mathrm{y}$ of the midpoint of the bounding box of the region can be specified to select the region.
If no midpoint is specified regions are renamed from right to left. Renaming is applied only to regions, which consist of a material, that has been redefined in Synonyms(...) to appear as Metal in the file.
The contact definition is assumed to support simple standard cases only.
The defined line contacts cannot be displayed in WIAS-TeSCA. The modified region names are kept in WIAS-TeSCA. The WIAS-TeSCA material of a region is not affected by Synonyms (...).

## Command File

A command file $\mathrm{xxx} . \mathrm{cm}$ for mdraw is written, which refers to the WIAS-TeSCA simulation grid and doping file and which contains refinement data.
Global refinement parameters MaxElementSize, MinElementSize, MaxTransDiff and MaxAspectRatio can be specified in the WIAS-TeSCA inputfile.
Polysilicon regions (in contact to oxide but not to silicon) are treated as "gate" contacts. The parameters in the Gate record are used to select and define the refinement at these "gates". The parameters VerticalSmooth and LateralSmooth
are used to select the relevant parts of the material interfaces. No smoothing of the boundaries is applied near the gates.

In addition, there are defined refinement regions in the silicon underneath the "gates". These lateral extension of regions can be modified with the parameter LateralRefine. The MaxAspectRatio and a series of vertical stepsizes MaxElementHeight and NumberDfIntervals can be specified to generate a graded fine grid in the silicon. If VerticalSmooth=undefined is specified, "gate" refinement is turned off.

## Grid And Doping

The WIAS-TeSCA simulation grid is saved in xxx_dios.geo and the doping functions are saved in xxx_dios.dop file. Both files are compressed by default. The variables in the .dop file can be selected with SPecies (...). By default, the net doping and the total doping of the several dopants are saved.

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| FILE | strin*80 |  | Name of the save file, the default file extensions are added internally. If the default extension is specified, the file type is defined from the extension and can be omitted. |
| Type | record | dmp.z | Type of output file, that has to be written. Several files are saved by specifying more than one type. |
| SPecies() | record |  | Names of WIAS-TeSCA variables, that have to be written into the file. |
| MATerial() | record |  | Names of WIAS-TeSCA materials which should be used in the output. |
| FNET | real | 1 | Net doping is divided by FNET if it is written into the file. In DIOS : Net = donator-acceptor |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| FORMat | integer | 0 | For TYPe=user, itri, picasso, dmp, formatted or unformatted files can be written. For TYPe=mdraw, the following values of FORmat can be used: 0: DF-ISE, 1: DATEX binary, 2: <br> DATEX text compressed, 3: DATEX portable 5: DATEX text gzip |
| APPend | boolean | on | Append a snapshot to an existing file or replace the file. Only for TYPe=plf. |
| DXproeth | real [ $\mu \mathrm{m}$ ] | 0.05 | Lateral step size for PROETH doping file. |
| DYproeth | real [ $\mu \mathrm{m}$ ] | 0.05 | Vertical step size for PROETH doping file. |
| Xproeth | integer | undefined | Number of lateral discretization points for PROETH doping file. |
| Yproeth | integer | undefined | Number of vertical discretization points for PROETH doping file. |
| EPSEq | real [ $\mu \mathrm{m}$ ] | $2 . \mathrm{e}-3$ | Minimum distance of two points in .rand |
| EPSLoc | real [ $\mu \mathrm{m}$ ] | $1.5 \mathrm{e}-3$ | Minimum local y-coordinate in .rand |
| DISTmin | real [ $\mu \mathrm{m}$ ] | $3 . e-3$ | Minimum distance for subdivision of edges with small slope. |
| EPSAngle | Angle | 3. degree | Smallest slope in .rand. Edges with smaller slopes are subdivided or moved. |
| MINAngle | Angle | 5. degree | Angle, achieved in the subdivision. |
|  |  |  | continued on next page |



continued on next page

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| ) |  |  | End of record Contact1. |
| ) |  |  | End of record Contacts. |
| DOTrect | boolean | on | Switches between doping on a tensor product grid or isolines in .geb. |
| LMAX | real [ $\mu \mathrm{m}$ ] |  | Maximum triangle edge in .geb. |
| LMIN | real [ $\mu \mathrm{m}$ ] |  | Minimum triangle edge in .geb. |
| Levels() | record |  | Up to 10 levels for isolines of net doping in .geb. |
| BC( |  |  | Data record for the definition of $\leq 15$ contacts in .geb. |
| TYPE1 | integer |  | Boundary condition type of the first contact in .geb. |
| XB1 | real [ $\mu \mathrm{m}$ ] |  | Lateral position of the start of the first contact in .geb. |
| YB1 | real [ $\mu \mathrm{m}$ ] |  | Vertical position of the start of the first contact in .geb. |
| XE1 | real [ $\mu \mathrm{m}$ ] |  | Lateral position of the end of the first contact in .geb. |
| YE1 | real [ $\mu \mathrm{m}$ ] |  | Vertical position of the end of the first contact in . geb. |
| ) |  |  | End of record BC. |

### 2.17 Step command

The STep-command is used to define the bias and the step control parameters.
For transient (time depending) calculations it is possible to enter time intervalls.
Executing the STep-command the solution of the equations are calculated, printed (to the terminal) and saved.

### 2.17.1 Comments

We call a "working point" the user given voltages on the Dirichlet (i.e., ohmic and Schottky contacts) and the gate contacts. Between the working points the embedding method adds additional operating points automaticly and more or less regularly.
Executing the STep-command the solution of the equations - the potential and the electron- and hole densities - are calculated and can be printed (to the terminal) and saved. Moreover, some more quantities (e.g., the contact and recombination currents and others) are calculated and can be printed/plotted.
If an ac-analysis frequency OMega() is given, a resistance and capacity matrix are calculated.
A typical WIAS-TeSCA output on terminal or in the log file looks like this

```
***** BIAS-point: 1 ** Step: 4** Time: 0.00000E+00
contact voltage/ V current/ A ** contact voltage/ V current/ A
contact 0.0000E+00 -3.13474E-05 substrat 0.0000E+00 3.13475E-05
I-Shockley-Read-Hall* I-Auger *I-Avalanche* I-surface*
                        2.069E-25 0.000E+00 0.000E+00 0.000E+00
    I-Reabs * I-Korro * I-Tunnel * I-Photo
    0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
N-charge = 3.7207188030E-10 P-charge = 2.8164628214E-30
dN-charge = 2.3785474651E-17 dP-charge = 5.0122137430E-38
relative distribution of N-charge:
    4.0503E-01 2.9225E-01 3.0272E-01
relative distribution of P-charge:
    6.7439E-01 1.4861E-05 3.2560E-01
    GU-st: 1, IT= 1, UDI=1.691E-08, JDI= 0.000E+00, DEF= 9.059E-06
    GU-st: 1, IT= 1, UDI= 1.481E-07, JDI= 6.353E-07, DEF= 9.059E-06
```

    CPU-Time: 3.00000E-02, Control: 3.79198E-05
    GUMMEL-steps: 1, NEWTON-steps: 0, Test: 1.481E-07, Defect: 9.059E-06
    The meaning of the key-words is contained in the following table.

### 2.17.2 Parameters

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| CApacity() | real | 0.d-12 | capacity at the contact No. IPAC ( $\leq$ mbias, see (2.89)) |
| CHARGEN() | real | rundef | Length $\leq$ mreg |
| CHARGEP() | real | rundef | Length $\leq$ mreg |
| Continue | integer | 0 | continue the calculation on the current point, no recalculation of the thermodynamic equilibrium is required, after processing the Step-command the value is reset to 0 |
| Execute | $l$ | set by SET | toggle the command execution |
| IGUMAX | integer | 100 | max. gummel steps |
| Dibias | $\begin{aligned} & \text { array } \\ & V \end{aligned}$ | 0. .. | bias on Dirichlet-contacts. Length $=$ IDIRI $\cdot$ NBias |
| Gabias | $\begin{aligned} & \text { array } \\ & V \end{aligned}$ | 0. ... | bias on gate-contacts Length $=$ INatur • NBias |
| IPRINT | integer | 1 | The solution is printed at each IPRINT time point (only transient case). |
| IPROT | integer | 10 | output control |
| IPOT | integer | 0 | solve only Poisson eqn. |
| ITSTEP | integer | 1 | actual working step number |
| MAstep() | integer | iundef | max. step number ( $\leq$ mbias). In the transient case DELT = TIMINT/MASTEP is the starting time step |
| MBIAS | integer | mbias | number of working points |
| MISTep() | integer | iundef | minstep <br> Length $\leq$ mbias number |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| MOckeu | integer | 20 | For $\quad$ TIMINT(I) > 0 MOCKEU determines the type of time discretization. MOCKEU = 1 means MockMethod |
| NBias | integer | iundef | working point number |
| OMega() | real | 0.d9 | ac-analysis frequency <br> Length $\leq$ mbias  |
| NOMEGA | integer | 1 | ac-analysis |
| DELTAu | real [V] | 0.00048 d 0 | ac-analysis |
| SETTIM | integer | 0 | time will be initialed after each time interval TImint |
| Save | integer | 0 | toggle result saving |
|  |  | 0 | no save |
|  |  | 1 | save each time step |
|  |  | 2 | save before and after call dynewt only |
| Load | integer | 0 | toggle result loading |
|  |  | $100$ | load the 100. dataset |
|  |  | -100 | load all datasets 1... 100 |
| STrom() | real | 0.d-12 | current at the contact No. IPAC ( $\leq$ mbias, see (2.89)) |
| TImint () | real [s] | -1.d0 | time intervalls |
| VAOXDI () | real [cm] | $0 . \mathrm{d} 0$ | Length $\leq 50$ |
| WORKstor | integer | 2000000 | max. integer workspace |
| RWORKstor | integer | 2000000 | max. real workspace |
| Functions | integer | 55 | max. number of functions |

### 2.17.3 Some more comments on parameters

The capacity $C$ (the corresponding parameter is CApacity) can be entered in the transient calculations on the ICAP-th edge according to the boundary conditions

$$
\begin{equation*}
J-J_{i}=C A_{i} \frac{d V}{d t}, i=1, \ldots, \text { mbias } \tag{2.89}
\end{equation*}
$$

The number of the contact ICAP has to be defined in the STEP command.

### 2.18 Recombination command

The REcombination-command defines the parameters of the generation-recombination model.

### 2.18.1 Models

For the generation-recombination we use the general additive ansatz of different generation-recombination processes.

$$
\begin{equation*}
G-R=G_{\mathrm{ava}}-R_{\mathrm{SRH}}-R_{\mathrm{Aug}}-R_{\mathrm{Surf}}-R_{\mathrm{rad}} \pm \ldots \tag{2.90}
\end{equation*}
$$

where
$G_{\text {ava }}$ Avalanche-generation,
$R_{\text {SRH }}$ Shockley-Read-Hall-recombination,
$R_{\text {Aug }}$ surface-recombination,
$R_{\text {Surf }}$ Auger-recombination,
$R_{\mathrm{rad}}$ radiative recombination.
We describe these generation-recombination processes in detail. The temperature $T$ is always normalized $T=\frac{\text { Temp in } K}{300 K}$, the dopant concentration is $D$

Moreover, the dependence on the material $M$ can be considered by a constant factor.

## Shockley-Read-Hall recombination

The models are taken from Selberherr [Sel84], S.105, Eqns.(4.2-14), and H.C. de Graaf and F. M. Klaassen, Compact Transistor Modelling for Circuit Design, Springer, Wien (1990)

$$
\begin{equation*}
R_{s r h}(n, p)=\frac{n p-N_{i}^{2}}{\tau_{p}\left(n+r_{n}\right)+\tau_{n}\left(p+r_{p}\right)} \tag{2.91}
\end{equation*}
$$

with

$$
\begin{align*}
\frac{1}{\tau_{n}} & =T^{\gamma_{n}}\left(\frac{1}{\tau_{n 0}}+C_{n} D\right)+T^{\delta_{n}} A_{n} p^{2}  \tag{2.92}\\
\frac{1}{\tau_{p}} & =T^{\gamma_{p}}\left(\frac{1}{\tau_{p 0}}+C_{p} D\right)+T^{\delta_{n}} A_{p} n^{2} \tag{2.93}
\end{align*}
$$

## Auger recombination

(see Selberherr[Sel84], S.109,(4.2-35))

$$
\begin{equation*}
R_{\text {aug }}(n, p)=\left(a_{b}+a_{n} n+a_{p} p\right)\left(n p-N_{i}^{2}\right) \tag{2.94}
\end{equation*}
$$

## Surface recombination

(see Selberherr[Sel84], S.110,(4.2-36))

$$
\begin{equation*}
R_{s u r f}(n, p)=\frac{n p-N_{i}^{2}}{\frac{n+r_{n}}{v_{n}}+\frac{p+r_{p}}{v_{p}}} \tag{2.95}
\end{equation*}
$$

## Avalanche generation

(see Selberherr [Sel84], S.110ff)

$$
\begin{equation*}
G_{a v a}=a_{1}\left|\mathbf{J}_{n}\right| \exp \left(-a_{2} / E \mathbf{J}_{n}\right)+a_{x}\left|\mathbf{J}_{p}\right| * \exp \left(-a_{y} / E \mathbf{J}_{p}\right) \tag{2.96}
\end{equation*}
$$

with

$$
\begin{align*}
& E \mathbf{J}_{n}=\left|E * \mathbf{J}_{n}\right| /\left|\mathbf{J}_{n}\right| \\
& E \mathbf{J}_{p}=\left|E * \mathbf{J}_{p}\right| /\left|\mathbf{J}_{p}\right| \\
& a_{x}=a_{3}, \text { for } E J p \leq a_{7}  \tag{2.97}\\
& a_{y}=a_{4}, \text { for } E J p \leq a_{7}  \tag{2.98}\\
& a_{x}=a_{5}, \text { for } E J p \geq a_{7}  \tag{2.99}\\
& a_{y}=a_{6}, \text { for } E J p \geq a_{7}  \tag{2.100}\\
& a_{1} \geq 0 \tag{2.101}
\end{align*}
$$

## Trapped charges

The Shockley-Read-Hall recombination was extended to incorporate deep traps in volume and on interfaces. These trap levels can take different states (neutral, negatively charged, positively charged) that are governed by additional equations, see 1.3.

According to the parameters in Section 1.3 on page 11, the following parameters can be set:
TER $=E_{\mathrm{r}}$, the difference between trap energy level and intrinsic Fermi energy;
TNR $=N$, the total density of the impurity;
$\operatorname{TSN}=s_{n}$ and $\mathrm{TSP}=s_{p}$ are the capture coefficient (this is the product of capture cross section and thermal velocity).

## Incomplete Ionization

Incomplete Ionization is handled in the same way as trapped charges.
According to the parameters in section 1.3 on page 11, the following parameters can be used:
$\mathrm{EDR}=E_{D}-E_{i}$, the difference between trap energy level and intrinsic Fermi energy;
$\operatorname{EAR}=E_{A}-E_{i}$, the ionized part of traps
$\mathrm{SND}=s_{n}$ and $\mathrm{SPA}=s_{p}$ are the capture coefficient (this is the product of capture cross section and thermal velocity).

### 2.18.2 Parameters

## Recombination

| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| AUGB | real | $0 . \mathrm{d} 0$ | $a_{b}$ in $(2.94)$ |
| AUGN | real | $2.8 \mathrm{~d}-31$ | $a_{n}$ in $(2.94)$ |
| AUGP | real | $9.9 \mathrm{~d}-32$ | $a_{p}$ in $(2.94)$ |
| AVA1 | real $[1 / \mathrm{cm}]$ | 1.00 d 6 | $a_{1}$ in $(2.96) ;$ AVA1 $=0$ turns off <br> the avalanche-generation. |
| AVA2 | real $[\mathrm{V} / \mathrm{cm}]$ | 1.66 d 6 | $a_{2}$ in $(2.96)$ |
| AVA3 | real $[1 / \mathrm{cm}]$ | 1.582 d 6 | $a_{3}$ in $(2.97)$ |
| AVA4 | real $[\mathrm{V} / \mathrm{cm}]$ | 2.036 d 6 | $a_{4}$ in $(2.98)$ |
| AVA5 | real $[1 / \mathrm{cm}]$ | 6.71 d 5 | $a_{5}$ in $(2.99)$ |
| AVA6 | real $[\mathrm{V} / \mathrm{cm}]$ | 1.693 d 6 | $a_{6}$ in $(2.100)$ |
| AVA7 | real $[\mathrm{V} / \mathrm{cm}]$ | $4 . \mathrm{d5}$ | $a_{7}$ in $(2.97, \ldots, 2.100)$ |
| CAUGn | real | $0 . \mathrm{d0}$ | $A_{n}$ in $(2.92)$ |
|  |  |  | continued on next page |


| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| CAUGp | real | 0.d0 | $A_{p}$ in (2.93) |
| CSRHn | real | 0.d0 | $C_{n}$ in (2.92) |
| CSRHp | real | 0.d0 | $C_{p}$ in (2.93) |
| DELTAn | real | 0.d0 | $\delta_{n}$ in (2.92) |
| DELTAp | real | 0.d0 | $\delta_{p}$ in (2.93) |
| GAMMAn | real | 0.d0 | $\gamma_{n}$ in (2.92) |
| GAMMAp | real | 0.d0 | $\gamma_{p}$ in (2.93) |
| IBulk | integer | -1 | number of the BULK-contact |
| IVREN() | real | 1.d0 | factor of surface recombination velocity for gate contacts, Length $\leq$ mreg |
| IVREP () | real | 1.d0 | factor of surface recombination velocity for gate contacts, Length $\leq$ mreg |
| RAB | real $[\Omega]$ | Od0 |  |
| RABT | real $[\Omega]$ | 0.d0 | BULK-resistance, time dependent |
| REN | real $\left[\mathrm{cm}^{-3}\right]$ | 1.09 d 10 | $r_{n}$ in (2.91, 2.95) |
| REP | real $\left[\mathrm{cm}^{-3}\right]$ | 1.09 d 10 | $r_{p}$ in (2.91, 2.95) |
| RENI | real | 0.d0 | intrinsic carrier density for SRH recombination |
| TAUNO | real [s] | 2d-4 | $\tau_{n 0}$ in (2.92), life time (electrons) |
| TAUNFA () | real | 1.d0 | $\tau_{n}^{\text {mat }}(M), \quad M=1, \ldots, \mathrm{mreg}$ |
| TAUPO | real [s] | 2d-6 | $\tau_{p 0}$ in (2.93), life time (holes) |
| TAUPFA () | real | 1.d0 | $\tau_{p}^{\text {mat }}(M), \quad M=1, \ldots$, mreg |
| VREN | real [cm/s] | 5.d0 | $v_{n}$ in (2.95), recombination speed |
| VREP | real [cm/s] | 5.d0 | $v_{p}$ in (2.95), recombination speed |

## Trap Model

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| ITRAP | integer | 0 | ITRAP number of traps, ITRAP>1 activate the trap model |
| IZTR() | integer | 0 | ITRAP numbers of zones, in which relevant traps are active, Length $\leq$ mreg |
| TER() | real [V] | 0.d0 | Trap model, $E_{r}$ in formula (1.33c) and (1.33d), Length $\leq$ mreg |
| TNR() | real $\left[\mathrm{cm}^{-3}\right]$ | 0.d0 | Trap model, Length $\leq$ mreg if $\mathrm{TNR}<0: \quad N_{k}^{\text {trap }}=-\mathrm{TNR}$, acceptor-type trap in formula (1.32a); if TNR>0: $N_{k}^{\text {trap }}=$ + TNR, donor-type trap in formula (1.32a); |
| TSN () | real | 1.3d-6 | Trap model, electron capture coefficient $s_{n}$ in formula (1.33), Length $\leq$ mreg |
| TSP () | real | 1.3d-7 | Trap model, hole capture coefficient $s_{p}$ in formula (1.33), Length $\leq$ mreg |

## Incomplete Ionization

| nameunit <br> type <br> option | default | comment |
| :---: | :--- | :--- | :--- |
| INCOMpleteinteger 0 INCOM=1 activates incomplete <br> ionization | continued on next page |  |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| EAR | real [eV] | 0.d0 | Trap model, Length $\leq$ mreg if EAR<0: $N_{a}=-\mathrm{EAR}, N_{d}=$ 0 in formula $1.32 \mathrm{~b}, 1.32 \mathrm{c}$; if $\mathrm{EAR}>0: N_{a}=0, N_{d}=\mathrm{EAR}$, |
| EDR | real [ eV ] | $0 . d 0$ | $E_{r}$, Length $\leq$ mreg |
| END | real | 1.d-0 |  |
| EPA | real | 1.d-0 |  |
| SND | real $\left[\mathrm{cm}^{3} / \mathrm{s}\right]$ | 1.3d-6 | $s_{n}$, Length $\leq$ mreg |
| SPA | real $\left[\mathrm{cm}^{3} / \mathrm{s}\right]$ | 1.3d-7 | $s_{p}$, Length $\leq$ mreg |

### 2.19 Load command

The LOAD-command is used, to read WIAS-TeSCA save files from previous simulations and to load analytical profiles or interpolate profiles from external meshes. Loading a WIAS-TeSCA save file is the default. When loading a WIAS-TeSCA save file, grid, layer structure and doping profiles are read from the file and the simulation can be continued. The save files may be compressed. Incompatibilities of the storage sizes between loaded file and current WIAS-TeSCA run are indicated and corrected internally.
Incompatibilities of old save files with newer program versions, reflect frequently only modifications in the parameter lists. By default the command parameters are not read from the save file. In this case all changes of default parameter values that had been made for the simulation are lost and have to be repeated after loading the file. LOAD (DEFAULT=on) can be used to force reading the command parameter values from the file.
Other incompatibilities in the save files are handled by different internal version numbers in the save file. A warning indicates, if the program has to modify the file content in order to be able to continue the simulation. If save files have to be exchanged between different machines, the file can be saved as compressed ASCIIfile SAVE(File=...,FORMat=1). When loading the file LOAD (FORMat=on. . .) can be specified.
The LOAD command can be used also, to define analytical profiles or to interpolate values on external numerical results. The user grid and the layer structure have to be defined before loading the profiles. For all nodes in the existing grid the values in the loaded profiles are interpolated. By default, the interpolated values are added to the already existing nodal values. If ADD=off is specified, the old
doping values are erased on the entire grid and only the loaded new values are used. The final profile is used to refine the mesh automatically.

The analytical functions are defined in the entire $x$ - $y$-plane and the profiles interpolated from an external file are extended in vertical and lateral directions, to cover the entire plane too. There is no extrapolation formula used, instead a "1D-continuation" is assumed in vertical or lateral direction.
Several species can be loaded at the same time. A list of species names can be supplied in the LOAD command. It is used to select some of the species from a file. If no species can be identified, the specified names are assigned to the profiles in the order as they appear in the file. The species names are used also for the analytical profiles. If no name can be identified, a net doping profile is assumed.

Doping profiles are interpreted as total concentrations. If the read file or the analytical function provide only a net profile, its absolute value is taken for the total doping profile. From the net and total doping profiles the donor and acceptor concentrations are computed and added to the specified acceptor and donator species:

$$
\begin{aligned}
& \text { FNET } \cdot \text { net }=\text { donator }- \text { acceptor } \\
& \\
& \text { total }=\text { donator }+ \text { acceptor }
\end{aligned}
$$

The external prescription of active concentrations, net and total concentrations, electron and hole density and electrostatic potential is impossible, since these variables are defined internally from the total concentrations due to clustering and charge neutrality assumptions (or by solving device equations).

### 2.19.1 Parameters

| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| FILE | strin*80 | undefined | File name. |
| TYPe |  | dmp | Type of doping definition: dmp plt exp prf plx Constant Gauss Erf Prosim DIFfgaus Relief GAUSS3 Tesim WIAS-TeSCA XGraph Mdraw dmp.Z dmp.gz |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| IGNore | boolean | off | Applies to $\mathrm{TYPe}=\mathrm{dmp}, \mathrm{dmp} . \mathrm{Z}$, dmp.gz If a save file is created during the diffusion process (NSAVE Saveeach) the already passed process time is saved into the file. By default IGNore=off, and this time is read and the diffusion time, immediately after the LOAD command is reduced by this time. This enables continuation of the diffusion simulation. For IGNore=on, the loaded time is ignored. |
| SPecies() | record |  | Names of species, to be selected from the file are defined by analytical profiles. |
| XLeft | Length | um | Left window boundary. Must be specified for TYPe=DIFfgaus, GAUSS. |
| XRight | Length | um | Right window boundary. Must be specified for TYPe=DIFfgaus, GAUSS. |
| EPS | Length | 0.1 um | Length of linear decay at the sides of the window if ULeft, URight, UTop or UBottom are undefined. |
| XSYLeft | Length | um | Left symmetry line. |
| XSYRight | Length | um | Right symmetry line. |
| SHIFt | real | $1 . \mathrm{e} 10$ | Vertical shift transformation. If $\mathrm{SHIFt}>1 \mathrm{e} 9$ the profile is shifted to the local substrate surface. |

continued on next page

| name | unit type option | default | comment |
| :---: | :---: | :---: | :---: |
| FACtor | real | -1000. | Vertical scaling factor for 1D profiles. |
| ADD | boolean | on | Summation of already existing and newly loaded profiles. off: erase the existing profiles in the entire grid, before loading the new profile. |
| ULeft | Length | um | Lateral "diffusion" length at the left side. Must be specified for TYPe=DIFfgaus, GAUSS3. |
| URight | Length | um | Lateral "diffusion" length at the right side. Must be specified for TYPe=DIFfgaus, GAUSS3. |
| Dot | Concentration /cm3 |  | Doping concentration (with sign). Must be specified for TYPe=Constant, Gauss, Erf, DIFfgaus, GAUSS3. <br> Additional scaling factor of the doping for $\mathrm{TYPe}=$ Prosim, Relief: <br> $\operatorname{Net}($ WIAS-TeSCA $)=$ FNET <br> Dot • net(file) <br> Total (WIAS-TeSCA) $=$ Dot. total(file) |
| Y | Length | um | Position of the maximum doping. Must be specified for TYPe=Gauss, Erf. Note! $Y Y=-1$ ! |
|  |  |  | continued on next page |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| S | Length | um | Standard deviation of the doping. Must be specified for TYPe=Gauss, Erf, DIFfgaus, GAUSS3. |
| L | Length | um | Diffusion length. Must be specified for TYPe=DIFfgaus . |
| R | Length | um | Projected range. Must be specified for TYPe=DIFfgaus . |
| LAT | Length | um | Lateral diffusion length. Must be specified for TYPe=DIFfgaus. |
| SAT | Concentration /cm3 |  | Saturation value of the profile. Must be specified for TYPe=GAUSS3. |
| YTop | Length | um | Top window boundary. If YTop=undefined no upper limit is assumed. Must be specified for TYPe=GAUSS3. |
| YTop | Length | um | Top window boundary. If YTop=undefined no upper limit is assumed. Must be specified for TYPe=GAUSS3. |
| YBottom | Length | um | Bottom window boundary. If YBottom=undefined no bottom window boundary is assumed. Must be specified for TYPe=GAUSS3 . |
| continued on next page |  |  |  |


| name | unit <br> type <br> option | default | comment |
| :--- | :--- | :--- | :--- |
| UTop | Length | um | "Diffusion length" at the top <br> window boundary. |
| UBottom | Length | um | "Diffusion length" at the bot- <br> tom window boundary. |
| FNET | real | 1 | Scaling factor of the net <br> doping. In DIOS : Net $=$ <br> donator- acceptor |
| ACCeptor | Dopant | B | Acceptor element when load- <br> ing Net and Total profiles. |
| DONator | Dopant | P | Acceptor element when load- <br> ing Net and Total profiles. |
| DEFaults | boolean | off | Prevents WIAS-TeSCA from <br> reading the default parame- <br> ter values for the command <br> interpreter from a save file. <br> Only the WIAS-TeSCA layer <br> system, grid, doping and <br> work arrays are read. Note! <br> Default values, modified in <br> the previous simulation run, <br> have to be changed again after <br> loading the file. |

$\qquad$

### 2.20 Use command

This command should be used always when the transition from process simulation to a device simulation with WIAS-TeSCA is done. The command has to be used if regions that are defined in WIAS-TeSCA should be omitted in the WIAS-TeSCA simulation.
In particular the contacts for the device simulation can be defined in the Use command.

### 2.20.1 Parameters

| parameter <br> name | unit <br> type <br> options | default <br> value | comment |
| :--- | :--- | :--- | :--- |
| Triangle | task | Selection of triangles for the <br> device simulation. |  |
| Material() record | All triangles of a WIAS-TeSCA <br> material can be treated as one <br> zone. They may not be con- <br> nected Material (SI=1, 0X=2) |  |  |
| Area( | task | Deliberate selection of ar- <br> eas. First an area num- <br> ber followed by a zone num- <br> ber have to be specified. <br> This overrides a zone number <br> specied from the material list |  |
|  |  |  | Area (area=52, zone=1, <br> area=53, zone=2). |
| Area |  |  | Number of the area. |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| Contacts( | task |  | Denition of contacts for the device simulation. The contact number is composed of: sign (el) $*(\mathrm{opt} * 100+\mathrm{abs}(\mathrm{el}))$, where el denotes the number of the gate or metal contact and opt the number of the optical or thermal contact. If Energy (IEnergy=-1) no thermal contacts are assumed, and if FERmi ( $\mathrm{ISPec}=0$ ) no optical contacts are assumed. el=-1...-10 for metal contacts el=1...5 for gate contacts opt=1...20 for optical or thermal contacts. |
| Points ( | record |  | Specification of contacts by approximate location of starting and end point. The outer boundary of the selected triangulation is used, to define the closest points for the starting and end point of the specified contacts. The corresponding edges on the outer boundary of the triangulation is selected to define the contact. The outer connectivity component is surrounded counterclockwise, the inner components (e.g., omitted polysilicon inclusions) clockwise. Up to 15 contacts can be specified. |
| TYPE | integer |  | Contact type of the first contact. |


| name | unit <br> type <br> option | default | comment |
| :---: | :---: | :---: | :---: |
| XB1 | Length | um | Approximate lateral position of the starting point of the first contact. |
| YB1 | Length | um | Approximate vertical position of the starting point of the first contact. |
| XE1 | Length | um | Approximate lateral position of the end point of the first contact. |
| YE1 | Length | um | Approximate vertical position of the end point of the first contact. |
| TYPE0 | integer | 999 | Default boundary condition type, symmetry condition. |
|  |  |  | For completeness the parameters XRT YRT XLT YLT XLB YLB XRB YRB BCLeft BCRight BCBottom BCTop can be specified, too. (cf. GRID command) |
| ) |  |  | End of record Points. |
| Dibez() | record |  | Names (string * 8) of the Dirichlet (metal) contacts in the order of their type numbers $-1,-2,-3, \ldots,-10$. |
| Gabez () | record |  | Names (string * 8) of the gate contacts in the order of their type numbers 1, 2, 3, 4, 5 . |
| ) |  |  | End of task Contacts. |

## 3 Numerical methods

### 3.1 Discretization of space

In WIAS-TeSCA, the discretization of space is realized with the finite elements method. As finite elements, triangles are used. By means of the DOMAIN command, different triangulation possibilities can be selected. In particular, it is possible to include user-defined grids. The potential and the charge carrier densities are the unknowns in the discrete versions of the Poisson continuitity and total current equations. These were derived with the aid of similar thoughts as described by Buturla et al. [ECGS81] for the programming system FIELDAY. In particular, the discretization of the continuity equations is based on Scharfetter's and Gummel's assumption of constant current densities along the edges of the triangles. The command POTENTIAL provides for an automatic grid refinement.

### 3.2 Discretization of time

In WIAS-TeSCA, the necessary complexity for the realization of one time step is essentially determined by the setting of the iteration parameter MOCKEU in the STEP command. For MOCKEU=1, a method examined and described by Mock [Moc83] is used that is based upon the successive solution of the continuity and the total current equations at one single time step. The iteration of this procedure depends on the choice of MOCKEU. For sufficiently high values of MOCKEU, this results in the implicit Euler method.
The time-step is controlled by the use of an energy functional, which plays a key role in analytical investigations where it is known as Lyapunov function [Gaj85].

### 3.3 Linearization

For the calculation of characteristics, WIAS-TeSCA works with the natural embedding method which uses the terminal voltage as embedding parameter. Unless a new start with saved values is carried out, the first operation point on a characteristic is reached from the thermodynamic equilibrium. Each time, from two calculated operation points, a starting point for the iterative calculation of the new operation point is gained by extrapolation of the electrostatic and the quasi-Fermi potential. The iteration is always started with the successive Gummel method.

It is switched to the simultaneous Newton method automatically if the rate of convergence falls below the parameter value GUMNEW. In the Gummel method, the necessary solution of the non-linear Poisson equation is generally carried out with the Newton method.

### 3.4 Solution of linear systems of equations

As a result of discretization and linearization, sparse systems of linear equations appear that are solved in WIAS-TeSCA through a combination of sparse-matrixtechniques and iteration methods.

To solve the decoupled Poisson equation, a multi-grid method is used, and if necessary an automatic grid adaption to the given doping profile is employed.

Due to the Gummel method a linear system of equations arrises from the nonlinear Poisson equation. It is solved with a conjugated gradient method with pre-conditioning and if necessary with a sparse-matrix-correction. The sparse-matrix-technique is also used for the solution of the discretized continuity and total current equations. However, the necessary relatively complex factorization is not carried out in each iteration cycle. On the contrary, as long as a sufficient speed of convergence is achieved the old factoring is used for the iteration. The coupled linear systems of equations that arise from the simultaneous Newton method are successively solved with a block iteration method that is based upon the Gummel method with the additional aid of the sparse-matrix-technique [GG92] .

### 3.5 Current calculation

In WIAS-TeSCA, consistent with the realized discretiziaton of the continuity equations, the current $J_{j}$ through the $j$-th contact is calculated according to the following formula which is based on Gauss' theorem.

$$
\begin{equation*}
J_{j}=\left(J, H_{j}\right):=\int \mathbf{J} \cdot \nabla H_{j} . \tag{3.1}
\end{equation*}
$$

Here, the expression on the right hand side denotes an area integral of the scalar product of the vectorial current density $\mathbf{J}$ and the gradient of a test-function $H_{j}$, which is equal to one in the neighborhood of the j -th contact and disappears in the proximity of the remaining contacts. To generate these test-functions $H_{j}$, solutions of the discrete Laplace equation with appropriate boundary conditions are utilized.

## 4 External tools

### 4.1 DEVICE - Grid and doping generator for TeSCA

The DEVICE tool is used to generate two-dimensional grids and doping profiles for the semiconductor simulation tool WIAS-TeSCA. DEVICE takes a '.dev' file as input and outputs a '.dom' and a '.dot' file, each with the same base name as the input file, e.g. example.dev yields example.dom and example.dot. The first file contains the grid description while the second describes the doping profile.

### 4.1.1 Usage of device

DEVICE is called on the command line with the '.dev' file (without suffix!) as only parameter:

```
> device example
```


### 4.1.2 Structure of the input files

The '. DEV' file consists of several sections - one grid section and several doping sections:

```
! This is a comment
! FILE: example.dev
&grid
    nw lllllll
    ! (left to right)
    ncol = 10 5 10 20 l subdivision of each column
    xstretch = +0.4 -0.3 +0.4 -0.4 l lateral stretch factor for each column
    nd = 3 ! number of rows
    d = 0.1 0.2 0.3 ! thickness of each row in [\mum]
    ! (bottom to top)
    nrow = 6 8 16 subdivisions of each row
    ystretch = +0.4 0.0 -0.4 l vertical stretch factor of each row
    mat = 1 1 2 2 material zones bottom row
material zones middle row
! material zones top row
    diag = +1 ! direction of triangle diagonal +/-1
    yorigin = ! number of row that contains origin
    xorigin = 1 number of column that contains origin
    ypos = 'b, ! position of origin in row
    xpos = 'l, ! position of origin in column
! ('l'eft, 'c'enter, 'r'ight)
```

```
/ ! end of grid description
&doping
    net= 1.0E18 1.0E16 -1.0E19 ! row-wise doping for all columns
/ ! end of first doping section
&doping
    net= 1.0E18 0.0 0.0 ! row-wise doping for first column
    ! (added to existing doping)
    / ! end of second doping section
...
```


## The stretch factors

The lateral and vertical stretch factors xstretch and ystretch are used to refine the subdivisions of a column or row in a direction and can take values in the interval $\left(-\frac{1}{2},+\frac{1}{2}\right)$. A positive value means that the length of the subdivisions is increasing from left to right in the lateral direction and increasing from bottom to top in the vertical direction. For negative values it is the other way round.

## The doping profile

The doping is specified in the doping section. The first section describes the doping for ALL columns in a row-wise fashion (bottom to top). The succeeding doping sections describe the doping in the columns: The first section describes the first column, the second section describes the second column, and so on. Doping levels for the same area are added.

### 4.1.3 Including the grid and doping profile in TeSCA simulations

The grid generated with DEVICE is used in WIAS-TeSCA via the GRID command:

```
! example.dio
! load grid
grid(type=dom, file='example.dom')
```

However, the 'DOM' file does not contain information about the position and types of boundary conditions. Hence, these have to be also defined in the grid command using the bc subcommand:

```
! example.dio
! load grid and define boundary conditions
grid(type=dom, file='example.dom'
    bc(type0=999,
        type1=ID1, XA1, YA1, XB1, YB1
        type2=ID2, XA2, YA2, XB2, YB2
        type3=ID3, XA3, YA3, XB3, YB3
        type4=ID4, XA4, YA4, XB4, YB4
        type5...
    )
```

Here, ID $i$ is a placeholder for the type of the boundary condition. The first type always has to be type0 $=999$, which corresponds to symmetry conditions or homogeneous Neumann conditions. The succeeding boundary condition types are of the form type $i= \pm(i \cdot 100+k)$, where $i$ should be an (increasing by one) positive number, which can be used for the definition of temperature and optic boundary conditions. Moreover, $k$ is a unique nonnegative number that describes the electrical contact, that is referenced e.g. in the device command. If $k=0$, then no-flux boundary conditions are assumed. Finally, if type $i$ is positive, e.g. type1=101, gate contacts are defined, otherwise, for type1=-101 metal contacts are assumed.

The coordinates (XAi, YA $i$ ) and (XBi, YBi) denote the starting and end of a boundary segment. The starting and end points for the segments have to be given counter-clockwise.
The triangulation along with the boundary types can be plotted in WIAS-TeSCA with the graphic command, namely

```
graphic(isol=no, contact=on, lay=no, glay=no, tria=on, text='Triangulation', plot)
```

The information on the doping profile from the 'DOT' file is included using the @ operator which embeds the 'DOT' file into the 'DIO' file:

```
! example.dio
! include doping file
@example.dot
```

...

### 4.1.4 Full example

```
! example.dev
&grid
nw = 4
w =}\begin{array}{lllll}{\textrm{w}}&{0.1}&{0.05}&{0.1}&{0.2}
ncol = 10 5 10
xstretch = +0.4 -0.3 +0.4 -0.4
nd = 3
d = 0.1 0.2 0.3
nrow = 6 8 16
ystretch = +0.4 0.0 -0.4
mat =}\begin{array}{llll}{1}&{1}&{2}&{2}\\{3}&{3}&{2}&{2}
    4450
    = +1
    yorigin = 1
    xorigin = 1
    ypos = 'b'
/
&doping
net = 1.0E18 1.0E16 -1.0E19
/
```

4 External tools

```
&doping
net = 1.0E18 0 0
```

/

```
! example.dio
l =============
! set title
title('Grid test',
    iphy = 0,
    maxv = 20000,
    mxt = 40000)
! load grid and define boundary conditions
grid( typ = dom,
    file = example.dom,
        bc( type0 = 999
            type1 = - 101, 0.25, 0.6, 0.0, 0.6
            type2 = 200, 0.0, 0.6, 0.0, 0.0
            type3 = -301, 0.0, 0.0, 0.45, 0.0
            type4=400,0.45,0.0,0.45,0.6
            )
    )
! initialize layer system
subs()
! plot triangulation and boundary conditions
graphic(isol=no, contact=on, scale(equal=no), lay=no, glay=no, tria=on,
    text=',Triangulation' plot)
! pause, continue with GO
break
! plot material regions
gra(isol=no, text='Material zones', contact=on notria lay=no glay=zone plot)
! pause, continue with GO
break
! include doping file
@example.dot
! plot net doping
graphic(junction, lay=no, isol=no, noabs, text='Doping',
    contacts=no, glay=no, spec(net), isol=fill,
        isolin=no, glay=no, isol=fill, plot
)
! pause, continue with GO
break
```


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[^1]:    ${ }^{1}$ The continuity equation in (1.4) can be obtained by differentiating the Poisson equation in (1.1a) with respect to time

    $$
    \nabla \cdot\left(\varepsilon_{0} \varepsilon_{\mathrm{r}} \frac{\partial}{\partial t} \mathbf{E}\right)=q\left(\frac{\partial p}{\partial t}-\frac{\partial n}{\partial t}\right)
    $$

[^2]:    ${ }^{2}$ In particular, with $A_{\mathrm{C}} \rightarrow 0$ the boundary condition $J=J_{\mathrm{S}}=$ const can be realized, see below.

[^3]:    ${ }^{3}$ The expression for recombination heat is only exact in the stationary case.
    ${ }^{4}$ The origin of $Q_{\text {rad }}^{\text {spont }}$ is the term $R_{\text {rad }}$ in the total charge carrier equation.

