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# Advanced thermal stability investigations of the Mn-Al-Ga system

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## ABSTRACT

A ternary Mn–Al-Ga alloy with the nominal composition  $Mn_{55}Al_{38,57}Ga_{6,43}$  was produced by arc melting. After homogenisation, the alloy consisted of the  $\varepsilon$  and  $\gamma_2$  phases. Appropriate heat treatments were used to transform each of these into a phase with the  $L1_0$  structure. These two  $L1_0$  phases had different compositions, lattice parameters and magnetic properties. In order to test the stability of the  $L1_0$  phases against decomposition, heat treatments were carried out at 700 °C for durations of up to 14 days. The results showed that the decomposition started with formation of the  $\beta$ -Mn phase and subsequent appearance of the  $\gamma_2$  phase. The resulting diffusion gradients resulted in composition changes in the  $L1_0$  phases and after 7 days, only a single, intermediate composition remained. After 14 days, the decomposition was almost complete. The decomposition of the  $L1_0$ phases in the ternary Mn–Al-Ga alloy was significantly slower than in binary Mn–Al alloys.

#### 1. Introduction

The ferromagnetic phases with the L1<sub>0</sub> structure at near-equiatomic compositions in the Mn-Al and Mn-Ga binary systems show promising hard magnetic properties [1-4] and are therefore interesting candidates for rare earth free permanent magnets. In both systems, saturation magnetisations of more than 0.75 T were observed and the magnetocrystalline anisotropy constants show values promising for the achievement of coercivities larger than 0.5 T [1,5]. Unfortunately both systems possess disadvantages. Whereas the L10 phase in Mn-Ga is thermodynamically stable, it is metastable in the Mn-Al system [6,7]. At elevated temperatures in Mn–Al alloys, the metastable phase with the L10 structure decomposes into the  $\gamma_2$  and  $\beta$ -Mn equilibrium phases, thus severely limiting the possibility to process the material at elevated temperatures [8]. The common method to tackle this disadvantage is alloying the Mn–Al alloys with carbon [9], but this results in a strong reduction in the Curie temperature [10], which is a significant disadvantage for applications. In the Mn–Ga system, the critical nature of global Ga supplies [11, 12] and the high raw materials cost of Ga make the industrial production of bulk materials with approximately 50 at% Ga unthinkable.

One possibility to overcome the problems of the binary systems is the formation of ternary Mn–Al-Ga alloys. Previous work has shown that samples consisting only of L1<sub>0</sub> phases can be produced for all alloys of the form Mn<sub>55</sub>Al<sub>45-x</sub>Ga<sub>x</sub> ( $0 \le x \le 45$ ) [5]. In alloys with  $5 < x \le 9$  at.% Ga, the formation of two different L1<sub>0</sub> phases was observed. At 1100 °C, the alloys consisted of a mixture of the high temperature  $\varepsilon$  and  $\gamma$  phases [5].

On cooling at intermediate rate from this temperature the  $\gamma$  phase transformed to  $\gamma_2$  and the  $\varepsilon$  phase transformed to L1<sub>0</sub> (further referred to as  $L1_0(\epsilon)$ ), as it does in binary Mn–Al alloys [5]. After annealing the alloy at 500  $^\circ C$  for 2 h, it was observed that the  $\gamma_2$  phase had also transformed into an L1<sub>0</sub> phase (further referred to as L1<sub>0</sub>( $\gamma_2$ )), as it does in binary Mn–Ga alloys [5]. It was shown that the two L10 phases are different in their composition, resulting in different lattice parameters and magnetic properties [5]. The average saturation magnetisation showed even superior values compared to the binary end members and was  $\mu_0 M_{sat} =$ 0.848 T for the Mn<sub>55</sub>Al<sub>39,375</sub>Ga<sub>5.625</sub> alloy [5]. First investigations of the thermal stability in the ternary alloys indicated an improved stability compared to binary Mn–Al: after annealing the ternary alloy at 700 °C for 2 h no decomposition of the L1<sub>0</sub> phases was visible in the XRD patterns, whereas for the binary Mn–Al system a strong decomposition in the β-Mn and  $\gamma_2$  equilibrium phases was observed [5]. BSE images of the annealed ternary alloy nevertheless showed hints of small β-Mn precipitates formed at the grain boundaries, indicating the beginning of the decomposition of at least one of the L10 phases [5]. The aim of the current work is to better clarify the long-term stability of the L10 phases at temperatures of 700 °C, which are typical for bulk deformation methods and therefore longer annealing durations of 4 h, 6 h, 24 h, 7 days and 14 days have been carried out and the resulting phase compositions of the alloys have been analysed.

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Fig. 1. Partial X-ray diffraction patterns of the  $Mn_{55}Al_{38.57}Ga_{6.43}$  alloy at 700 °C for different annealing durations.

#### 2. Experimental

The ternary Mn–Al-Ga alloys were produced by arc melting of elemental materials with purity 99.8% for Mn, 99.99% for Al and 99.999% for Ga in the appropriate quantities. The samples were annealed in quartz tubes filled with Ar. For the production of the L1<sub>0</sub> phases the annealing was carried out at 1100 °C for 48 h followed by an annealing at 500 °C for 24 h. To investigate the thermal stability of the L1<sub>0</sub> phases samples with the composition  $Mn_{55}Al_{38.57}Ga_{6.43}$  (with  $\pm 1$  at.% to the nominal composition) were used and additional heat treatments at 700 °C for 4 h, 6 h, 24 h, 7 days and 14 days carried out. For all heat treatments the furnace was heated to the needed temperature before the samples were inserted. After the annealing the quartz tubes were quenched into water to obtain a fast cooling rate.

The analysis of the crystal structure was done with x-ray diffraction (XRD) using a Bruker diffractometer together with the Rietveld refinement method and the FullProf program [13,14]. Thereby  $\theta$  -  $2\theta$  in the range from 20° to 120° were carried out using Co-K<sub>\alpha</sub> radiation ( $\lambda$ (K<sub>\alpha1</sub>) = 1.78919 Å;  $\lambda$ (K<sub>\alpha2</sub>) = 1.79321 Å; ratio 1:1).

The microstructure of the alloys was observed with a Zeiss Leo Gemini 1530 scanning electron microscope. Additionally the composition of the phases was analysed using an energy dispersive X-ray spectroscopy (EDX) extension from Bruker. The compositions were averaged from at least 5 point measurements per phase. The accuracy of the



Fig. 3. Magnetisation curves up to 14 T after different annealing times at 700  $^\circ C$  for the  $Mn_{55}Al_{38.57}Ga_{6.43}$  alloy.

quantitative EDX measurements can be described as a combination of the experimental inaccuracy together with the statistics of the measurement results and is approximately  $\pm 1$  atomic percent. The preparation of the samples for microscopy was carried out using standard metallographic methods.

The saturation magnetisation of the samples were measured at an applied field of 14 T in the VSM mode of a Quantum Design PPMS. For the thermomagnetic measurements the same device was used with an applied field of 0.1 T. The samples were non-textured and the demagnetisation factors were calculated according to the sample shape and used to calculate the internal magnetic field  $H_{int}$ .

## 3. Results and discussion

The XRD patterns in the range 45°–60° 20 are shown in Fig. 1 (The complete XRD patterns can be seen in the supplemental material) clearly indicate a phase transformation during the heat treatment. After 4 h first evidence of  $\beta$ -Mn formation becomes visible. The fraction of  $\beta$ -Mn is increasing with increasing annealing time and additional  $\gamma_2$  peaks appear after 7 days of annealing, indicating a slow L1<sub>0</sub> decomposition over time. Nevertheless after 7 days strong peaks of the L1<sub>0</sub> structure are still present. After 14 days at 700 °C the peaks of the  $\beta$ -Mn and  $\gamma_2$  phases are dominant but clear L1<sub>0</sub> reflexes are still visible.

Looking at the microstructure after the individual heat treatments (see Fig. 2) the growth of the  $\beta$ -Mn precipitates (bright regions in the BSE



Fig. 2. BSE images of the  $Mn_{55}Al_{38.57}Ga_{6.43}$  alloy after the 700 °C annealing for different durations.

in Fig. 2) at the grain boundaries of the  $L1_0$  phases can be seen. These precipitates slowly increase in size and volume fraction with increasing annealing durations. After the 7 days three different phases exist. Two of the phases appear bright in the BSE images which can be identified as  $\beta$ -Mn and  $\gamma_2$  with the help of EDX analysis. The dark regions in the BSE images correspond to the  $L1_0$  phase. The composition of the  $\beta$ -Mn phase was found to be Mn<sub>59,1</sub>Al<sub>37,6</sub>Ga<sub>3,3</sub> (see Table 1). The high amount of manganese is consistent to the  $\beta$ -Mn region in the binary phase diagrams leading to the identification as the  $\beta\text{-}Mn$  phase. For the second bright phase a composition of  $Mn_{49.1}Al_{42.8}Ga_{8.1}$  was determined. With the reduced amount of Mn in this region an identification as  $\gamma_2$  is suggested. The remaining L10 phase shows a composition of Mn<sub>53.1</sub>Al<sub>40.2</sub>Ga<sub>6.7</sub> and thus the composition of the phase is located between the initial compositions of the  $L1_0(\varepsilon)$  and  $L1_0(\gamma_2)$  phases. As the Mn content is strongly enriched in the β-Mn phase, diffusion of Mn would be necessary for the formation of the  $\beta$ -Mn phase and therefore for the decomposition of the L1<sub>0</sub> phase. Additionally, the Ga content of the  $\beta$ -Mn phase is noticeably lower than that of the other phases. This may indicate a lower solubility of Ga in β-Mn and implies that, in addition to Mn enrichment through diffusion. Ga must also diffuse away from a region in order to form  $\beta$ -Mn. The decomposition into  $\beta$ -Mn and later on into  $\gamma_2$  is therefore accompanied with a strong diffusion leading into a change of the initial  $L1_0$ compositions. This assumption is strengthened by the results of the 14 days annealing at 700 °C. After this duration, a large fraction of the sample was transformed into  $\beta$ -Mn and  $\gamma_2$ . Only some L1<sub>0</sub> grains can be found in the BSE images. A clear distinction between the two L10 phases is no longer possible. The mean composition of the L10 phase was found to be Mn<sub>52,3</sub>Al<sub>40,0</sub>Ga<sub>7,7</sub>, which lies between that of the L1<sub>0</sub>( $\epsilon$ ) and L1<sub>0</sub>( $\gamma_2$ ) initial L1<sub>0</sub> phases.

The individual compositions of the different phases after each annealing is collected in Table 1. There one can see that composition of the  $\beta$ -Mn and  $\gamma_2$  phase are relative constant after each annealing step whereas the composition of the L1<sub>0</sub> phases changes slightly. Especially after 7 and 14 days the diffusion driven change of the L1<sub>0</sub> phase is visible.

Magnetic measurements of the alloys after the heat treatments can be used to give an idea of the remaining volume fraction of the L1<sub>0</sub> phases (see Fig. 3). Up to 24 h more than 77% of the magnetic L1<sub>0</sub> phase was retained. With increasing annealing to 7 days at 700 °C the fact that still about half of the sample consists of L1<sub>0</sub> is remarkable. This stands in good accordance with microstructural investigation. Compared to the binary Mn–Al system this is a huge improvement. Even for alloys with carbon addition it was reported that only one-third of the L1<sub>0</sub> phase was not decomposed after 7 days of annealing at 700 °C [15]. In the case of the ternary Mn–Al-Ga alloy after the same time still more than 50% of the sample remains in the L1<sub>0</sub> phase. After 14 days according to the magnetisation 6% of the L1<sub>0</sub> remained.

Additionally to the hysteresis curves thermomagnetic measurements were carried out to investigate the change of the Curie temperature with the different annealing durations. For the two different  $L1_0$  phases these measurements clearly showed two different Curie temperatures as they are strongly depending on the compositions. This behaviour can also be seen up to 24 h of annealing at 700 °C as shown in Fig. 4. For longer



**Fig. 4.** Curie temperature changes after different annealing durations of the  $Mn_{55}Al_{38.57}Ga_{6.43}$  alloy. Up to 24 h of annealing for the two different  $L1_0$  phases with different compositions 2 Ci temperatures could be found. For 7 and 14 days only 1 Ci temperature remained.

annealing times the typical two step behaviour of the thermomagnetic measurement is not visible anymore. Resulting in only one remaining Curie temperature of  $T_C = 318$  °C for the L1<sub>0</sub> phase with intermediate composition. It is interesting to note that the  $T_C$  of the single L1<sub>0</sub> phase is closer to that of the L1<sub>0</sub>( $\gamma_2$ ) phase although the composition of the single L1<sub>0</sub> phase is closer to that of L1<sub>0</sub>( $\epsilon$ ).

### 4. Conclusion

Extending the heat treatments of the ternary Mn-Al-Ga alloys up to two weeks at 700 °C allowed a better understanding of the thermal stability of the L1<sub>0</sub> phase. It could be shown that the two different L1<sub>0</sub> phases  $L1_0(\gamma_2)$  and  $L1_0(\varepsilon)$  possess an increased thermal stability compared to binary Mn-Al. The beginning of the decomposition process could be observed in the XRD after 4 h and in magnetic measurements after 2 h of annealing at 700 °C. The decomposition of the L10 phase seems to be diffusion driven and starts with the formation of  $\beta$ -Mn. The first hints of the second equilibrium phase ( $\gamma_2$ ) were observed after 6 h of annealing. More than 77 vol% of the L10 phases remained after 24 h of annealing at 700 °C. This is a large improvement compared to binary Mn-Al. The composition of the L1<sub>0</sub> phases changes with increased annealing time and results in one final intermediate composition. After 7 days over 50% of the sample remained in this intermediate L10 phase. An additional 7 days of annealing, resulting in an overall duration of 14 days, led to further decomposition with 6 vol% L10 phase remaining at the end. Thermomagnetic measurements confirmed the change of the composition from two distinct L1<sub>0</sub> phases to one single composition with increasing annealing duration: the Curie temperature of the final L1<sub>0</sub> phase was found to be  $T_C = 318$  °C. Overall, the higher thermal stability of the ternary alloys compared to binary Mn-Al is promising; however,

Table 1

Compositions of the different phases inside the  $Mn_{55}Al_{38,57}Ga_{6.43}$  alloy obtained from at least 20 point measurements for the  $L1_0$  phases and more than 5 points for  $\beta$ -Mn and  $\gamma_2$  resulting in an accuracy of  $\pm 1$  at.% after different annealing times at 700 °C measured with EDX method.

Duration	L1 <sub>0</sub> (ε) (at.%)			$L1_0(\gamma_2)$ (at.%)			L1 <sub>0</sub> (at.%)			β-Mn (at.%)			γ <sub>2</sub> (at.%)		
	Mn	Al	Ga	Mn	Al	Ga	Mn	Al	Ga	Mn	Al	Ga	Mn	Al	Ga
0 h	54.9	39.0	6.1	51.6	41.3	7.0									
2 h	54.6	39.1	6.3	51.4	41.2	7.3									
4 h	54.1	39.4	6.5	50.9	41.8	7.3									
6 h	54.3	39.4	6.3	51.3	41.6	7.1				58.7	37.4	3.9	48.5	43.7	7.8
24 h	53.7	39.6	6.7	51.8	40.9	7.3				58.5	37.6	3.9	48.7	43.2	8.1
7 d							53.1	40.2	6.7	59.1	37.6	3.3	49.1	42.8	8.1
14 d							52.3	40.0	7.7	58.6	37.8	3.6	48.8	42.7	8.5

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from the results presented here, it is not possible to assess whether one of the two original L1<sub>0</sub> phases could be thermodynamically stable at 700  $^{\circ}$ C. Producing samples consisting of only one of these phases is therefore highly important in order to be able to characterise the thermal stability in the absence of the diffusion gradients which led to the decomposition in the current work.

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## Appendix A. Supplementary data

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