

The design of a new manual wheelchair for sport

*Original*

The design of a new manual wheelchair for sport / Quaglia, G.; Bonisoli, E.; Cavallone, P.. - In: MACHINES. - ISSN 2075-1702. - 7:2(2019), p. 31. [10.3390/machines7020031]

*Availability:*

This version is available at: 11583/2894632 since: 2021-04-16T12:29:09Z

*Publisher:*

MDPI

*Published*

DOI:10.3390/machines7020031

*Terms of use:*

openAccess

This article is made available under terms and conditions as specified in the corresponding bibliographic description in the repository

*Publisher copyright*

(Article begins on next page)

Article

# The Design of a New Manual Wheelchair for Sport

Giuseppe Quaglia \*, Elvio Bonisoli and Paride Cavallone 

Department of Mechanical and Aerospace Engineering, Politecnico di Torino, 10129 Torino, Italy; elvio.bonisoli@polito.it (E.B.); paride.cavallone@polito.it (P.C.)

\* Correspondence: giuseppe.quaglia@polito.it

Received: 28 February 2019; Accepted: 6 May 2019; Published: 9 May 2019



**Abstract:** In this paper, an innovative system of propulsion inspired by a rowing gesture for manual wheelchairs is shown. The innovative system of propulsion, named Handwheelchair.q, can be applied to wheelchairs employed in everyday life and to sports wheelchairs for speed races, such as Handbike and Wheelchair racing. The general features of the innovative system of propulsion and the functional designs of the different solutions are described in detail. In addition, the design of the mechanism for the transmission of motion, employed in a second prototype, Handwheelchair.q02, is presented and analysed. Finally, the dynamic model of the Handwheelchair.q has been developed in order to obtain important results for the executive design of Handwheelchair.q.

**Keywords:** Handwheelchair.q; Disabled sport; Manual wheelchair

## 1. Introduction

Many studies [1–3] assert that wheelchair users suffer from upper limb injuries more frequently than the rest of the population. Since the handrim is the world’s most used manual propulsion system [4], the main causes of upper limb pain depend on the motion of the handrim system that is a pushing movement. Outdoor and indoor motor activities are extremely important for the well-being of everyone. For disabled people, motor activities [5] are also an important tool in rehabilitation from a physical and psychological point of view. Even though motor activities for disabled people are extremely important, they are not easy to practice. First of all, specific sports require specific wheelchairs [6–12]; secondly, the areas where the disabled can practice sport have to be properly equipped; finally, the disabled are not independent for the transportation of the wheelchair for a specific sport.

The above reasons motivated us to develop a wheelchair with an innovative system of propulsion, which not only allows for the practice of outdoor activities autonomously, but also eliminates the need of a specific wheelchair for sport.

As shown in [13], during a propulsion cycle with the handrim system, the glenohumeral contact force has high peaks. This is one of the factors that can increase the risk of injuries to the shoulders. In addition, in the Conclusions section of [14] “The latter makes tangential force propulsion not only less efficient, but also more straining for the shoulder”. Different articles compare the handrim system with alternative systems of propulsion, such as a lever system [15] and a handcycle [13].

Another approach considers the use of a rowing gesture in order to obtain the propulsion. Furthermore, the rowing stroke [16] is divided into four phases and different articles have studied the efficiency of the rowing gesture [17]. The rowing stroke is a complex movement; the muscles of the legs, trunk, back, shoulders and arms are involved. The rowing stroke can be performed by disabled athletes with different levels of spinal injuries [18]. Disabled people can perform this movement depending on the height of the spinal injuries.

In the last two years, the first prototype, named Handwheelchair.q01 [19], was released. The first prototype tested the functioning of the innovative system of propulsion and highlighted some critical issues.

In addition to the Handwheelchair.q01, the authors of this paper have wide experience with means of mobility for disabled people [20,21].

## 2. Rowing Gesture: General Features

The innovative system of propulsion is inspired by the rowing gesture. One of the more important characteristics of the rowing gesture is that the drive phase is obtained using a pulling movement of the arm, instead of a pushing one, typical of handrim and lever systems. The pulling movement could be a good alternative compared to the pushing movement. In this work, a cable solution was introduced in order to realise the rowing motion as a system of propulsion. The cable solution allows users to optimise their motion based on their own individual physical characteristics.

The rowing gesture is composed of two phases. During the traction phase, the user provides power, while in the recovery phase the user goes back to the initial position.

During the traction phase shown in Figure 1, the user pulls two cables by two handles wrapped around two pulleys. Each pulley transmits the torque and rotation to the wheel by a unidirectional mechanism, named a ratchet system. A power spring, which connects the pulley to the chassis of the wheelchair, is loaded. In this phase, the angular speed of the pulley and the wheel are equal.

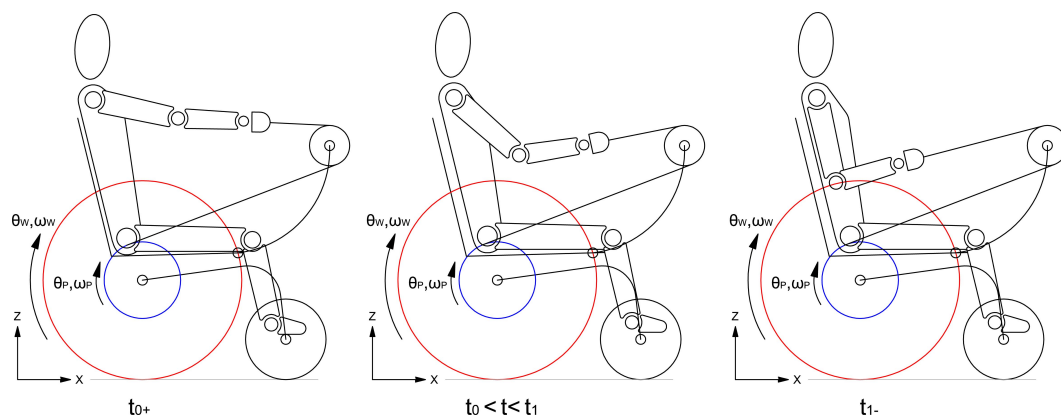


Figure 1. Rowing gesture during the traction phase.

During the recovery phase shown in Figure 2, the user stops pulling and the power spring, previously loaded, rotates the pulleys in the opposite direction ( $\omega_w > 0$ ,  $\omega_p < 0$ ). The cables are wrapped around each pulley and the user can start another traction phase.

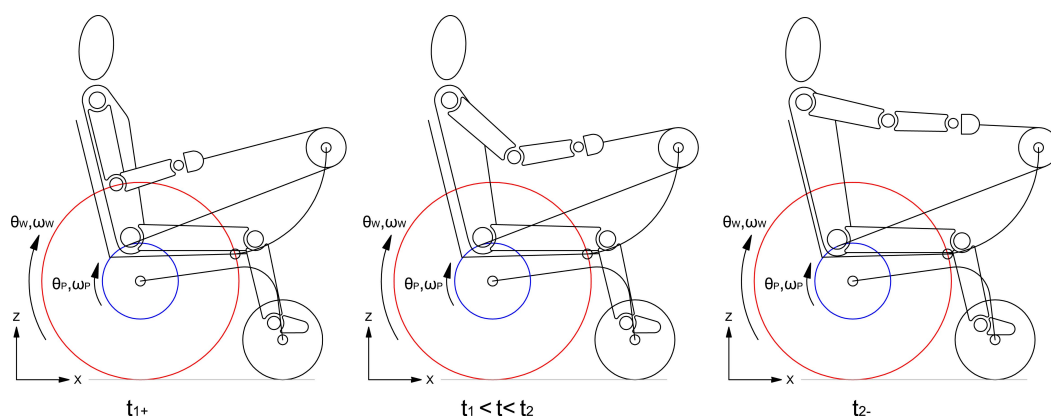


Figure 2. Rowing gesture during the recovery phase.

In Figure 3, the angular position, the angular speed of the pulley and the wheel are shown with the three assumptions:

- The angular speeds are constant;
- The time of the traction phase  $T_P$  is higher than the time of the recovery phase  $T_R$ ;
- Pure rolling motion.

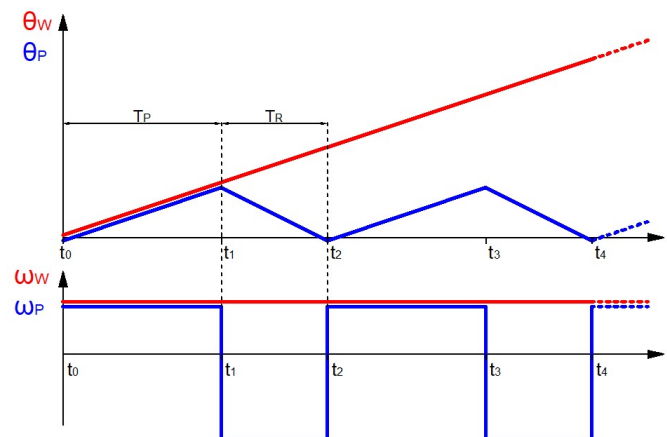


Figure 3. Angular speed and angular position of the pulley and the wheel.

In Section 4, the mechanism of transmission of motion will be accurately described.

### 3. Application of the Innovative System in Sport

The innovative system of propulsion can be employed by different means of manual mobility for sport: Handbike and Wheelchair racing.

The innovative system can be installed on the Handwheelchair.q racing wheelchair, as shown in Figure 4, with a few modifications of standard racing wheelchairs. The push-rims have been removed, while a pair of traction pulleys and a pair of return pulleys have been placed. The Handwheelchair.q racing wheelchair with the innovative system of propulsion keeps the same characteristics of a racing wheelchair: two rear traction wheels and a front steering wheel.

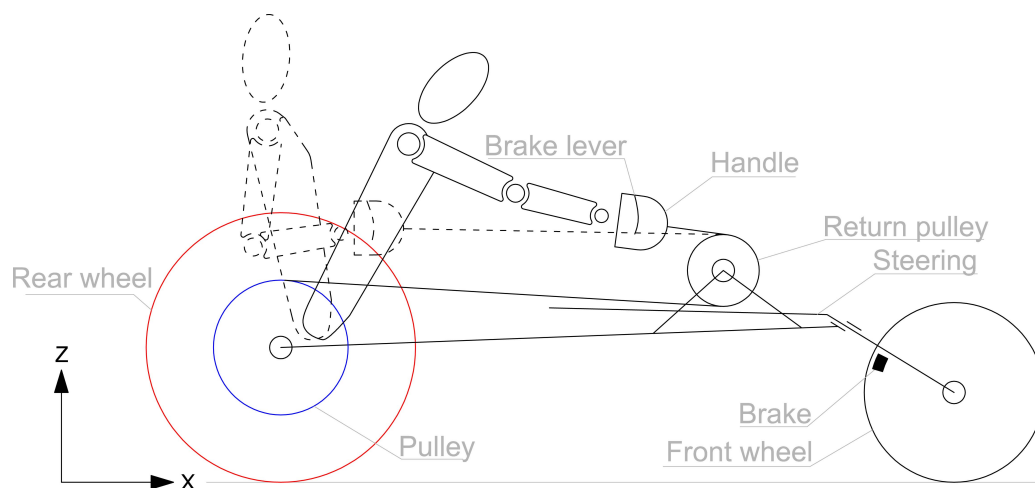
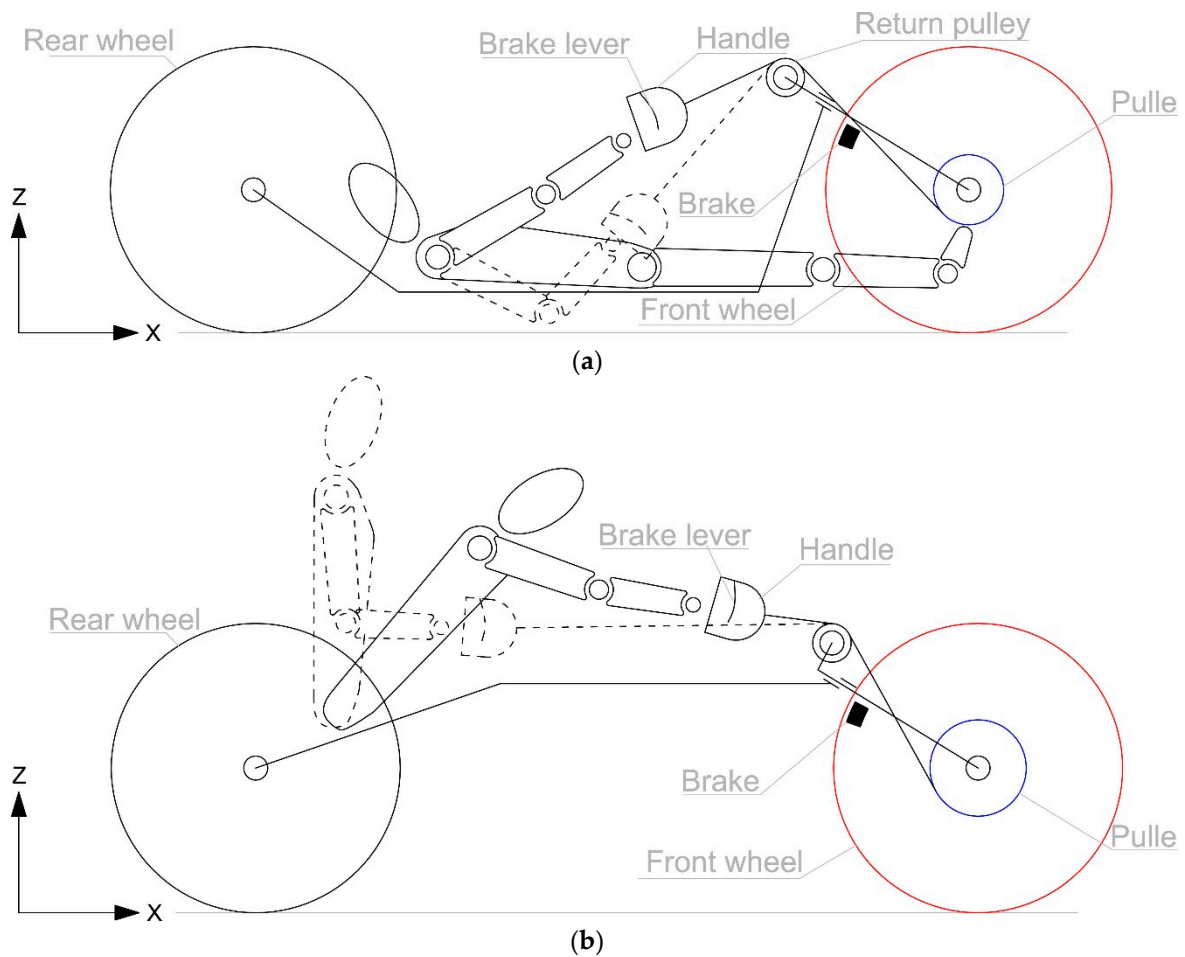


Figure 4. Innovative system applied to the racing wheelchair.

The innovative system can be employed on the Handbike. Figure 5a shows the functional design of Handbike.q for categories H1, H2, H3 and H4, namely disabled with spinal cord injuries and Figure 5b for categories H5, namely disabled with amputated limbs. A pair of pulleys has been seated,

one on each side, in order to balance the fork transversely. A return pulley has been located in order to optimise the athlete's motion. The Handbike.q with the innovative system of propulsion retains the same characteristics of the Handbike: a traction steering front wheel.



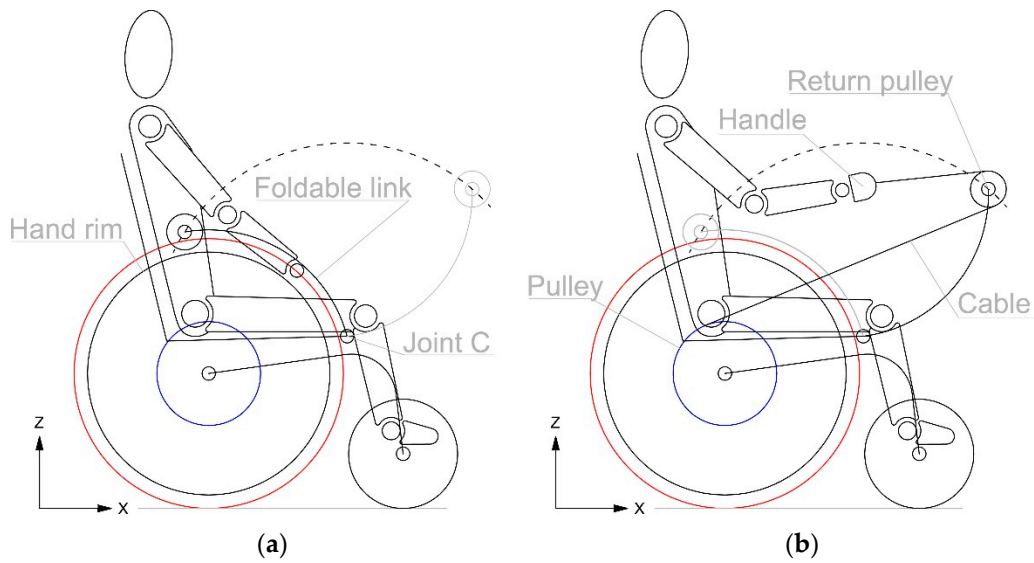
**Figure 5.** (a) Innovative system applied to the recumbent Handbike; (b) Innovative system applied to the Handbike.

#### 4. Handwheelchair.q02

The Handwheelchair.q02 is a wheelchair for everyday life. The main goals of Handwheelchair.q02 are:

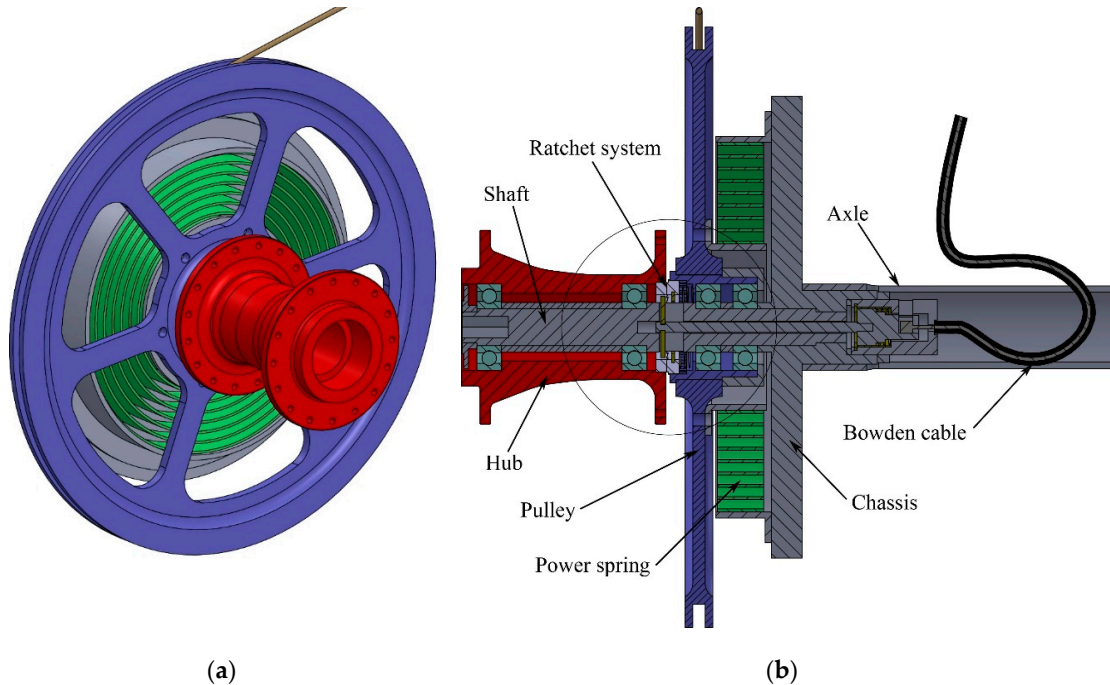
- To facilitate and extend outdoor movement;
- To be firm and maneuverable for indoor spaces; and
- To practice motor activity independently and in such areas as a park and a cycle path.

The Handwheelchair.q02 has two configurations. The first configuration, shown in Figure 6a, is employed for indoor spaces. In this configuration, the wheelchair is used as a common wheelchair, where the propulsion is obtained by the handrim. The foldable links, left and right, that support a pair of return pulleys, are folded in order to minimise the visual impact and to allow for sitting on the wheelchair. The second configuration, shown in Figure 6b, is employed outdoors to facilitate movement, to extend accessible places and to practice motor activities. The user rotates the foldable link, left and right, around the joint C in order to obtain the innovative configuration.



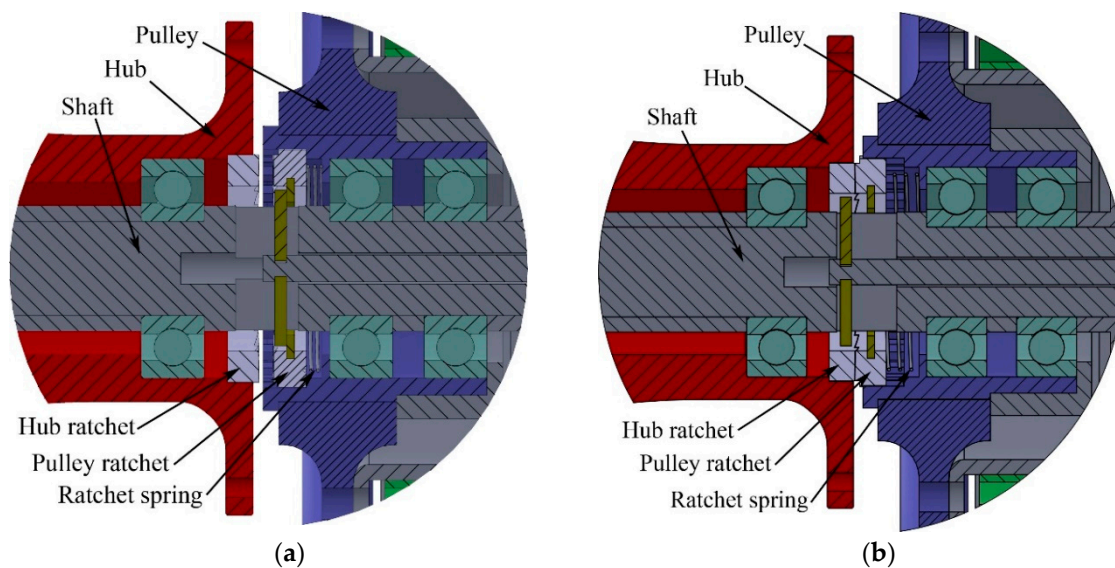
**Figure 6.** (a) Handwheelchair.q02 indoor configuration; (b) Handwheelchair.q02 outdoor configuration.

Figure 7 show the components that enable the use of the wheelchair in the innovative configuration. The red component is the hub of the wheel and the blue one is the pulley around which the cable is wrapped. The green one is the power spring that connects the pulley with the chassis of the wheelchair, in grey. In the first configuration, the mechanism of transmission of motion allows the user to use the wheelchair as a common wheelchair. In fact, the hub of the wheel rotates around the shaft as in the classic wheelchair, as sketched in Figure 8a.



**Figure 7.** (a) Components of the innovative system of propulsion; (b) Section of the mechanism.

When the user takes the handles from their site, a mechanism keeps in contact the two front ratchets, as visible in Figure 8b.



**Figure 8.** Particulars of the mechanism in the (a) Classic configuration; (b) Innovative configuration.

One ratchet is integrated with the pulley and the other one is mounted into the hub of the wheel. In this configuration, the propulsion is obtained by the rowing stroke previously described. During the traction phase, the user pulls the cables with a force  $F_u$  the cables are wrapped around a pair pulleys of radius  $r_p$ . The user transmits a torque to the wheel through the ratchet system. During the traction phase, the user loads a power spring that connects the pulley with the chassis of the wheelchair. In Figure 9, the free-body diagrams during the traction phase of the pulley and of the hub are reported and in Tables 1 and 2 the description of the torques and the reference systems are described.

**Table 1.** Description of the torques in the free-body diagrams.

Torque	Description
$F_u * r_p$	User force multiplied the radius of the pulley
$C_{e0}$	Preload of the power spring
$K_e * \theta_p$	Stiffness of the power spring multiplied by the angular position of the pulley
$I_p * \dot{\omega}_p$	Moment of inertia of the pulley
$C_1$	Torque transmitted by the ratchets
$I_W * \dot{\omega}_W$	Equivalent inertia on the wheel given by the user, the wheel and the wheelchair multiplied by the angular acceleration of the wheel
$C_{f1}$	Friction torque given by rolling resistance and the aerodynamic resistance
$C_{f2}$	Friction torque given by the friction ratchets during the recovery phase

**Table 2.** Reference systems.

Reference System	Description
$\theta_p, \omega_p, \dot{\omega}_p$	Angular position, angular speed and angular acceleration of the pulley
$\theta_W, \omega_W, \dot{\omega}_W$	Angular position, angular speed and angular acceleration of the wheel

During the traction phase, the angular speed of the pulley is the same as the angular speed of the wheel and the equation can be written as follows:

$$\omega_p = \omega_W > 0. \quad (1)$$

The torque equilibrium of the pulley results:

$$F_u * r_p = I_p * \dot{\omega}_p + C_{e0} + K_e * \theta_p + C_1. \tag{2}$$

While the torque equilibrium of the hub is:

$$C_1 = C_{f1} + I_W * \dot{\omega}_W. \tag{3}$$

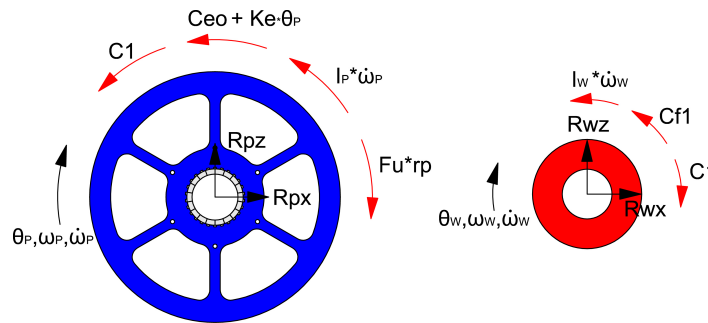


Figure 9. Free-body diagram during the traction phase.

During the recovery phase the user stops pulling, and we assume that  $F_u \sim 0$ , Figure 10. The power spring, previously loaded, has to generate a torque  $C_{e0} + K_e * \theta_p$  to rotate the pulley in the opposite direction in order to rewind the cable around the pulley in a specific time  $T_R$ . The recovery time  $T_R$  is the parameter of the project that defines the torque of the power spring.

During the recovery phase, the angular velocities are:

$$\omega_p < 0; \omega_w > 0. \tag{4}$$

The torque equilibrium of the pulley is:

$$I_p * \dot{\omega}_p + C_{e0} + K_e * \theta_p = C_{f2}. \tag{5}$$

The torque equilibrium of the hub results:

$$C_{f1} + C_{f2} + I_W * \dot{\omega}_W = 0. \tag{6}$$

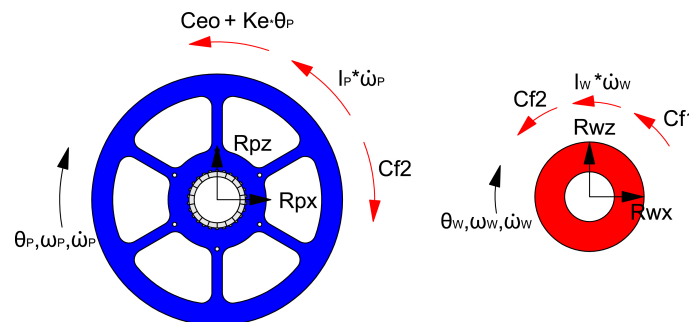


Figure 10. Free-body diagram during the recovery phase.

### 5. Dynamic Model of Handwheelchair.q

In this section, according to the previous paragraph, a simplified dynamic model, Figures 11 and 12, and the description of the free-body diagram, Tables 3 and 4, of Handwheelchair.q are presented, with the following hypothesis and assumptions:

- All dynamic characteristics are concentrated on the wheel 1:  $N_2 = 0, T_2 = 0$ ;



- Even if the rolling-resistance coefficient depends on the speed [22], the rolling-resistance coefficient  $u_1$  can be assumed to be constant for low speed;
- The inertia of the wheels and the pulleys is equal to zero:  $I_{W1} = 0$ ;  $I_{W2} = 0$ ;  $I_P = 0$ ;  $I_{RP} = 0$ ;
- The torque of the power spring  $C_e$  is constant;
- $F_a$  is the aerodynamic force, modelled by [22],  $F_a = k_a \dot{x}^2$  applied on the Center of Pressure; and
- The Center of Pressure coincides with the Center of Mass CM.

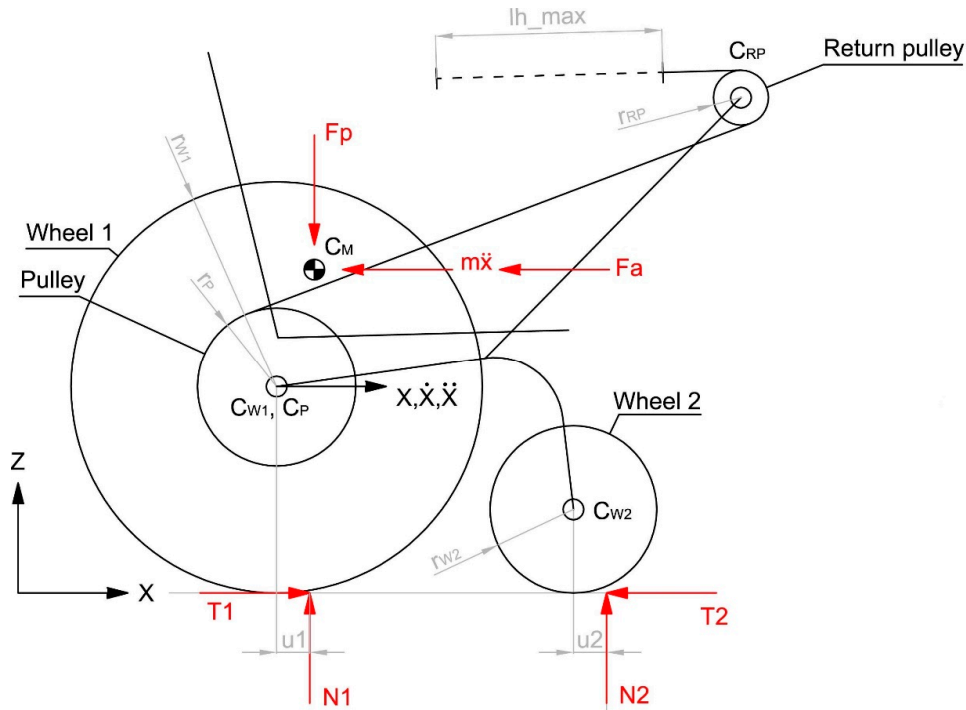


Figure 11. Handwheelchair.q: Free-body diagram.

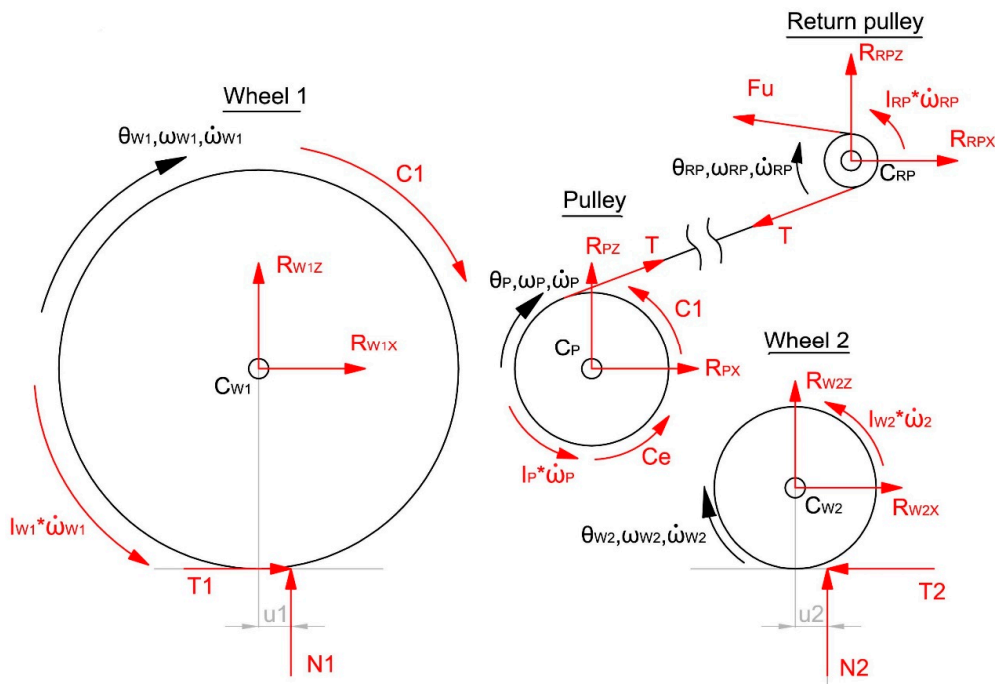


Figure 12. Free-body diagram of wheel 1, wheel 2, the pulley and the return pulley.

**Table 3.** Description of the torques and force of the dynamic model.

Torque/Force	Description
Fp	Weight force of the user and wheelchair
$m\ddot{x}$	Inertial force of the user and wheelchair
Fa	Aerodynamic force
N1	Ground reaction force of the wheel 1 along the z axes
T1	Ground reaction force of the wheel 1 along the x axes
N2	Ground reaction force of the wheel 2 along the z axes
T2	Ground reaction force of the wheel 2 along the z axes
T	Friction torque given by the friction ratchets during the recovery phase
$R_{W1X}$	Joint reaction force of the wheel 1 along x axes
$R_{W1z}$	Joint reaction force of the wheel 1 along z axes
$R_{W2X}$	Joint reaction force of the wheel 2 along x axes
$R_{W2z}$	Joint reaction force of the wheel 2 along z axes
$R_{PX}$	Joint reaction force of the pulley along x axes
$R_{PZ}$	Joint reaction force of the pulley along z axes
$R_{RPX}$	Joint reaction force of the return pulley along x axes
$R_{RPZ}$	Joint reaction force of the return pulley along z axes
$I_{W1} * \dot{\omega}_{W1}$	Moment of inertia of the wheel 1
$I_{W2} * \dot{\omega}_{W2}$	Moment of inertia of the wheel 2
$I_P * \dot{\omega}_P$	Moment of inertia of the pulley
$I_{RP} * \dot{\omega}_{RP}$	Moment of inertia of the return pulley

**Table 4.** Reference system's dynamic model.

Reference System	Description
$x, \dot{x}, \ddot{x}$	Position, speed, and acceleration of the wheelchair
$\theta_P, \omega_P, \dot{\omega}_P$	Angular position, angular speed, and angular acceleration of the pulley
$\theta_{RP}, \omega_{RP}, \dot{\omega}_{RP}$	Angular position, angular speed, and angular acceleration of the return pulley
$\theta_{W1}, \omega_{W1}, \dot{\omega}_{W1}$	Angular position, angular speed, and angular acceleration of the wheel 1
$\theta_{W2}, \omega_{W2}, \dot{\omega}_{W2}$	Angular position, angular speed, and angular acceleration of the wheel 2

The user's force is modelled as follows:

- The time of the traction phase is  $T_p$  and, according to Figure 13, is evaluated as:

$$x(t') - x(t_0) = lh_{max} * \tau \quad (7)$$

$$t' - t_0 = T_p \quad (8)$$

where,  $lh$  is the stroke length of the gesture and  $\tau = 3$  is the transmission ratio defined by:

$$x = lh * \frac{r_{w1}}{r_p} = lh * \tau. \quad (9)$$

The Figure 14, shows the traction phase during the indoor test of the first prototype Handwheelchair.q01.

- According to [12,13], during the tests the propulsion power was between 15 and 55 W. The average propulsion power for a cycle can be assumed to be between 20 and 25 W;
- The user’s force  $F_u$  has been modelled with a polynomial 2-3-4 in order to define an approximate model of the “Handle force  $F_h$ ” [23], as shown in Figure 15;
- The scale of force  $F_u$  is determined in order to obtain the average power of 20–25 W;
- The recovery time  $T_r$  is constant;
- The user’s force during the recovery phase is zero.

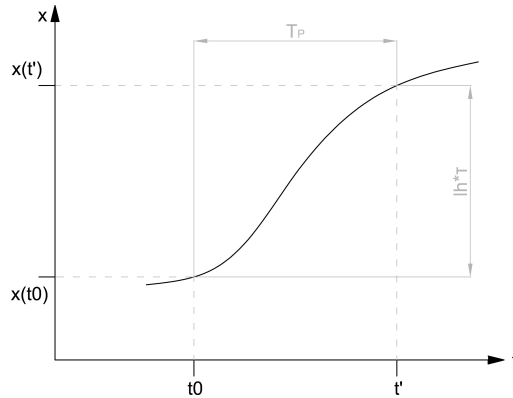


Figure 13. Time of the traction phase.

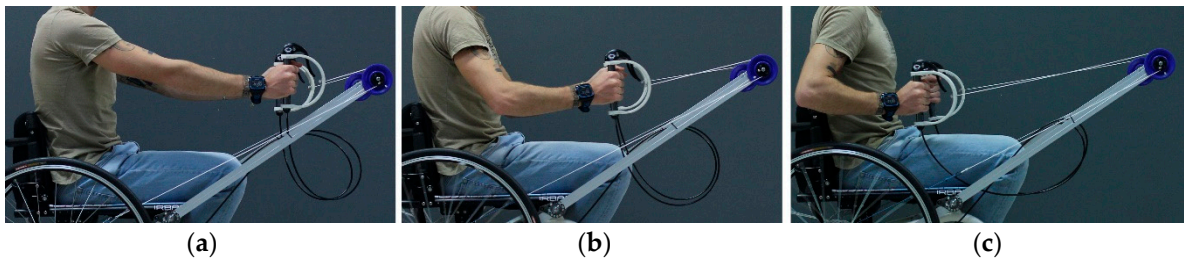


Figure 14. Innovative gesture during the indoor test of the first prototype Handwheelchair.q01. (a)  $t_0$ ,  $lh = 0$ ; (b)  $t_0 < t < t_1$ ,  $0 < lh < lh_{max}$ ; (c)  $t_1$ ,  $lh = lh_{max}$ .

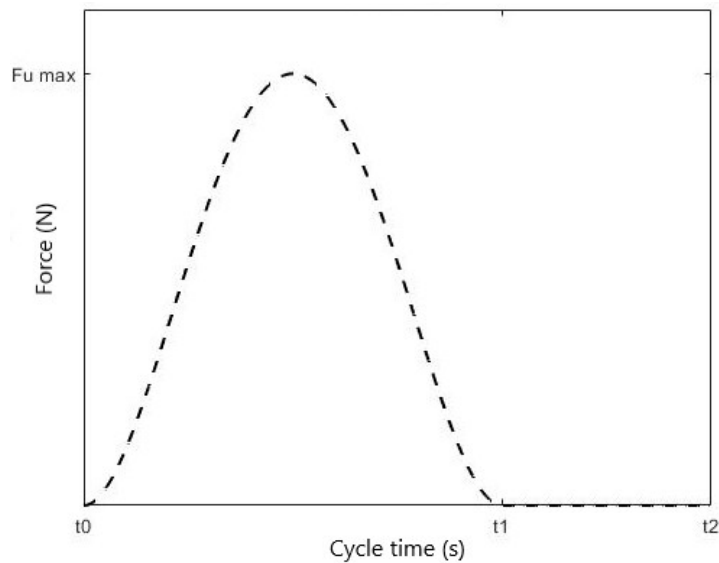


Figure 15. User’s force model.

According to the free-body diagram previously reported, and with the abovementioned hypothesis and assumptions:

The equilibrium of the wheelchair along the axis  $x$  results

$$T1 = m\ddot{x} + Fa = m\ddot{x} + k_a x^2. \quad (10)$$

The equilibrium of the wheelchair along the axis  $z$  is

$$N1 = Fp = mg. \quad (11)$$

The rotation equilibrium of wheel 1 around the joint  $C_{W1}$  results

$$T1 * r_{W1} + N1 * u_1 = C1. \quad (12)$$

The rotation equilibrium of the pulley around the joint  $C_P$  is

$$T * r_p = C1 + Ce. \quad (13)$$

The rotation equilibrium of the return pulley around the joint  $C_{RP}$  is

$$T * r_{RP} = Fu * r_{RP}. \quad (14)$$

By replacing Equations (10), (11), (13) and (14) in Equation (12), it results:

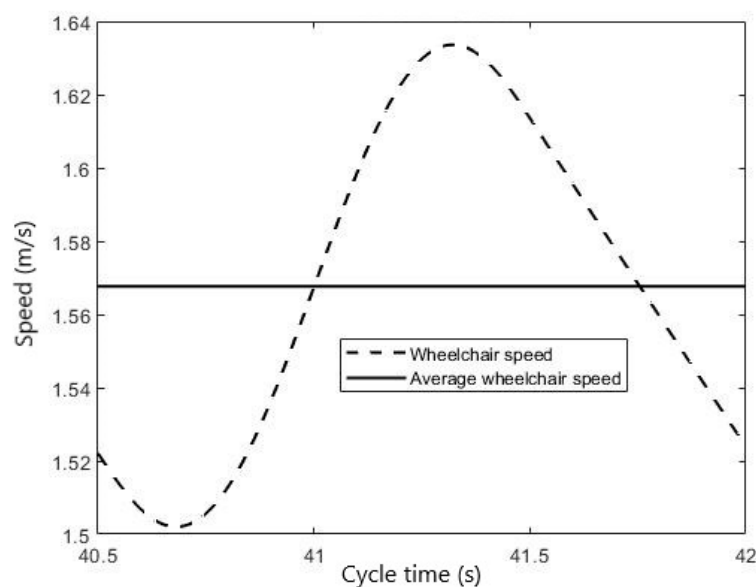
$$Fu * r_{RP} = mg * u_1 + (m\ddot{x} + k_a x^2) * r_{W1} + Ce. \quad (15)$$

By rewriting Equation (15), the acceleration can be evaluated as:

$$\ddot{x} = \frac{Fu}{\tau m} - \frac{k_a}{mr_{W1}} \dot{x}^2 - \frac{mg * u_1}{mr_{W1}} - \frac{Ce}{mr_{W1}}. \quad (16)$$

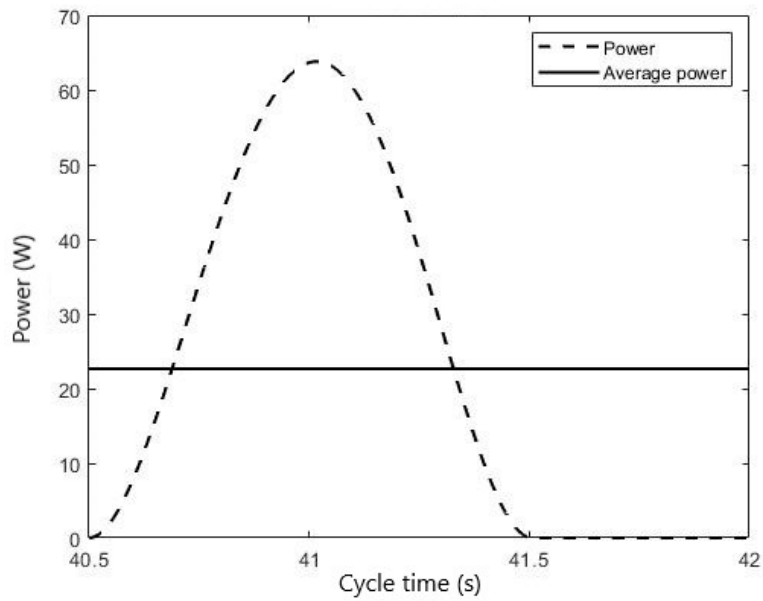
Equation (16) and the model of the user's power have been implemented in Matlab/Simulink.

During the steady-state phase, the average wheelchair speed is constant. Figure 16 show respectively the wheelchair speed and the user's power during a complete cycle: traction phase and recovery phase.



(a)

Figure 16. Cont.



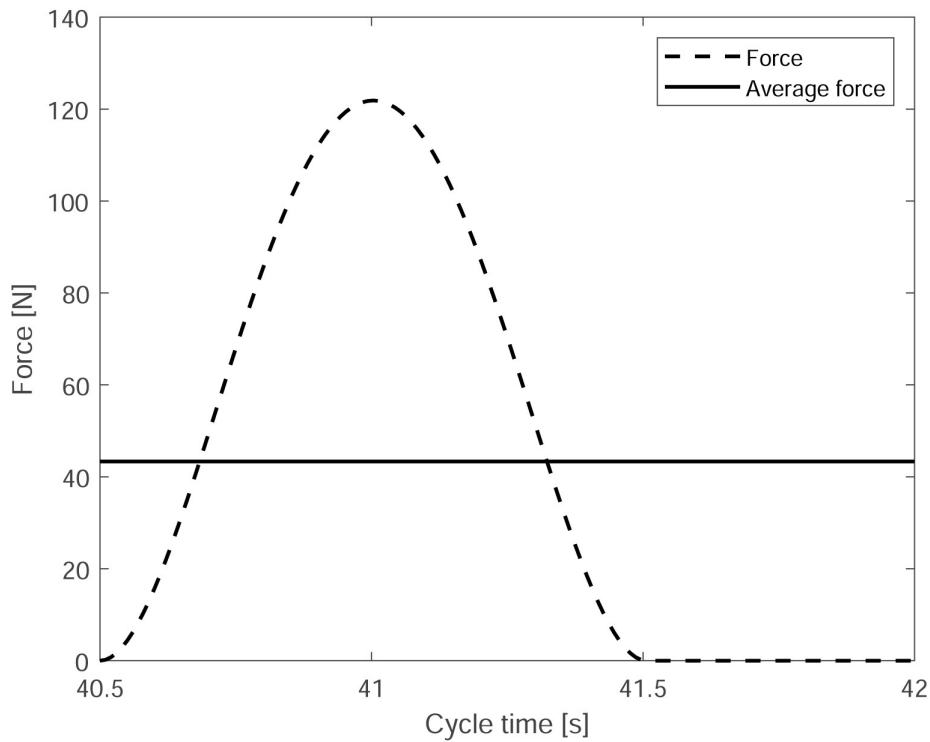
(b)

**Figure 16.** Wheelchair speed (a) and user’s power (b) in a complete cycle during the steady-state phase.

The average power of 23 W and the average speed of 1.57 m/s = 5.65 km/h obtained with the simulation is in accordance with the tests carried out in [12,13,15].

By employing the user’s force model, we obtain a  $F_{u\_max} = 120$  N as shown in Figure 17, while the average force  $F_{u\_avg} = 43$  N. The force  $F_u$  is the sum of the right and left arm contribution:  $F_{u_r} + F_{u_l}$ . Then, the average force for each arm is approximately

$$\overline{F_{u_r}} = \overline{F_{u_l}} = 22 \text{ N.} \tag{17}$$



**Figure 17.** User’s force during the steady-state phase.

## 6. Conclusions

The development of an innovative system of propulsion for manual wheelchairs is described in different possible sketches in order to be implemented in sports wheelchairs and for wheelchairs employed in everyday life. In addition, the design of the mechanism for the transmission of motion is presented. The innovative system of propulsion could be a robust idea to solve injuries on the upper limb caused by the other manual system of propulsion. The project of the prototype, named Handwheelchair.q02, is still being developed.

A simplified dynamic model has provided preliminary results in terms of force and power during a rowing stroke cycle applied to a manual wheelchair. In the future, the test data of the prototype Handwheelchair.q02 will confirm or deny these predictions.

**Author Contributions:** Conceptualization, G.Q. and E.B.; methodology, G.Q., E.B., P.C.; software, E.B. and P.C.; validation, G.Q.; investigation, P.C.; data curation, P.C.; writing—original draft preparation, P.C.; writing—review and editing, G.Q., E.B. and P.C.; visualization, P.C.; supervision, G.Q.; project administration, G.Q.

**Funding:** This research received no external funding.

**Conflicts of Interest:** The authors declare no conflict of interest.

## References

- Lewis, A.R.; Philips, E.J.; Robertson, W.S.P.; Grimshaw, P.N.; Portus, M. Injury prevention of elite wheelchair racing athletes using simulation approaches. *Proceedings* **2018**, *2*, 255. [[CrossRef](#)]
- Curtis, K.A.; Roach, K.E.; Applegate, E.B.; Amar, T.; Benbow, C.S.; Genecco, T.D.; Gualano, J. Reliability and validity of the wheelchair user's shoulder pain Index (WUSPI). *Paraplegia* **1995**, *33*, 595–601. [[CrossRef](#)]
- Cooper, R.A.; Boninger, M.L.; Robertson, R.N. Repetitive strain injury among manual wheelchair users. *Team Rehab. Rep.* **1998**, *9*, 35–38.
- Van Der Woude, L.H.V.; Dallmeijer, A.J.; Jansenn, T.W.J. Alternative modes of manual wheelchair ambulation: An overview. *Am. J. Phys. Med. Rehabil.* **2001**, *80*, 765–777. [[CrossRef](#)]
- Cooper, R.A.; De Luigi, A.J. Adaptive sports technology and biomechanics: Wheelchairs. *Paralympic Sports Med. Sci.* **2014**, *6*, 31–39. [[CrossRef](#)]
- Rice, I. Recent salient literature pertaining to the use of technology in wheelchair sports. *Curr. Phys. Med. Rehabil. Rep.* **2016**, *4*, 329–335. [[CrossRef](#)]
- Van Delen, C.J.R.T.; Gooch, S.; Ingram, B.J.; Borren, G.L.; Jenkins, A.; Dunn, J. Classification efficiency in wheelchair rugby: Strength analysis. *Int. Fed. Autom. Control* **2014**, *47*, 9901–9906. [[CrossRef](#)]
- Gil-Agudo, A.; Del Ama-Espinosa, A.; Crespo-Ruiz, B. Wheelchair basketball quantification. *Phys. Med. Rehabil. Clin. N. Am.* **2010**, *21*, 141–156. [[CrossRef](#)]
- Fung, Y.; Chan, D.K.; Caudwell, K.M.; Chow, B. Is the wheelchair fencing classification fair enough? A kinematic analysis among world-class wheelchair fencers. *Eur. J. Adapt. Phys. Act.* **2013**, *6*, 17–29. [[CrossRef](#)]
- Guan, T.; Lei, L.; Li, J. The human engineering analysis of the racing wheelchair. *Adv. Mater. Res.* **2014**, *538–541*, 2802–2806. [[CrossRef](#)]
- Litzenberger, S.; Mally, F.; Sabo, A. Biomechanics of elite recumbent handcycling: A case of study. *Sport Eng.* **2016**, *19*, 201–211. [[CrossRef](#)]
- Arnet, U.; Van Drongelen, S.; Van der Woude, L.H.V.; Veeger, D.H.E.J. Shoulder load during handcycling at different incline and speed conditions. *Clin. Biomech.* **2012**, *27*, 1–6. [[CrossRef](#)]
- Arnet, U.; Van Drongelen, S.; Scheel-Sailer, A.; Van der Woude, L.H.V.; Veeger, D.H.E.J. Shoulder load during synchronous handcycling and handrim wheelchair propulsion in persons with paraplegia. *J. Rehabil. Med.* **2012**, *44*, 222–228. [[CrossRef](#)]
- Bregman, D.J.J.; Van Drongelen, S.; Veeger, H.E.J. Is effective force application in handrim wheelchair propulsion also efficient? *Clin. Biomech.* **2009**, *24*, 13–19. [[CrossRef](#)]
- Sasaki, M.; Stefanov, D.; Ota, Y.; Miura, H.; Nakayama, A. Shoulder joint contact force during lever-propelled wheelchair propulsion. *Robomech J.* **2015**, *2*, 13. [[CrossRef](#)]

16. Greene, A.J.; Sinclair, P.J.; Dickson, M.H.; Colloud, F.; Smith, R.M. The effect of the ergometer design on a rowing stroke mechanics. *Scand. J. Med. Sci. Sports* **2013**, *23*, 468–477. [[CrossRef](#)]
17. Pelz, P.F.; Verge, A. Validated biomechanical model for efficiency and speed of rowing. *J. Biomech.* **2014**, *47*, 3415–3422. [[CrossRef](#)]
18. Smoljanovic, T.; Bojanic, I.; Pollock, C.L.; Radonic, R. Rib stress fracture in a male adaptive rower from the arms and shoulders sport class: Case report. *Croat. Med. J.* **2011**, *52*, 644–647. [[CrossRef](#)]
19. Quaglia, G.; Bonisoli, E.; Cavallone, P. A proposal of alternative propulsion system for manual wheelchair. *Int. J. Mech. Control* **2018**, *19*, 33–38.
20. Quaglia, G.; Nisi, M. Design of a self-leveling cam mechanism for a stair climbing wheelchair. *Mech. Mach. Theory* **2017**, *112*, 84–104. [[CrossRef](#)]
21. Quaglia, G.; Franco, W.; Nisi, M. Design of a reconfiguration mechanism for an electric stair-climbing wheelchair. In Proceedings of the ASME IMECE 2014 International Mechanical Engineering Congress and Exposition, Montreal, QC, Canada, 14–20 November 2014; p. V04AT04A022.
22. Baldissera, P. Proposal of a coast\_down model including speed-dependent coefficients for the retarding forces. *Proc. Inst. Mech. Eng. Part P* **2017**, *231*, 154–163.
23. Turpin, N.A.; Guèvel, A.; Durand, A.; Hug, F. Effect of power output on muscle coordination during rowing. *J. Appl. Physiol.* **2011**, *111*, 3017–3029. [[CrossRef](#)]



© 2019 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).