

University of Groningen

## Structural and photophysical characterisation of coordination and optical isomers of mononuclear ruthenium(II) polypyridyl 1,2,4-triazole complexes

Browne, Wesley R.; Heseck, Dusan; Gallagher, John F.; O'Connor, Christine M.; Killeen, J. Scott; Aoki, Fumiko; Ishida, Hitoshi; Inoue, Yoshihisa; Villani, Claudio; Vos, Johannes G.

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February 24th, 2003
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Please consider this CIF file for deposition in the Cambridge Structural Database for submitted crystal structures. Two CIF files form this submission. We request a CSD code and number for the compound for future reference in future publications and theses.

The authors are Browne, Hesek, Gallagher,  
O'Connor, Killeen, Villani and Vos.

The crystals diffracted reasonably well and absorption effects were corrected for using psi-scan reflections at 5 degree intervals.

Note:

There is considerable disorder in the hexafluorophosphate anions in both structures and there are partial occupancy solvent molecules as well.

I was collected on an Enraf Nonius CAD4 diffractometer in Guelph, Canada. II was collected on a Siemens P4 diffractometer in DCU, Dublin, Ireland.

Yours sincerely,

John Gallagher

;

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;
Structural and photophysical characterisation of coordination and optical
isomers of mononuclear ruthenium(II) polypyridyl 1,2,4-triazole complexes
;
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'Johannes G. Vos'
'Wesley R Browne'
'D Hesek'
'J. F. Gallagher'
'Christine M O'Connor'
'J. Scott Killeen'
```

'Fumiko Aoki'  
'Hitoshi Ishida'  
'Yoshihisa Inoue'  
'Claudio Villani'

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Refinement of F2 against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
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Ru1 Ru 0.11468(9) 0.15168(8) 0.14601(9) 0.0356(3) Uani 1 d . . .  
N11A N 0.2914(9) 0.1112(8) 0.1305(8) 0.039(2) Uani 1 d . . .  
C2A C 0.3660(12) 0.1859(11) 0.1171(12) 0.053(3) Uani 1 d . . .  
H2A H 0.3377 0.2623 0.1077 0.064 Uiso 1 calc R . . .  
C3A C 0.4802(13) 0.1522(13) 0.1170(13) 0.059(4) Uani 1 d . . .  
H3A H 0.5285 0.2052 0.1070 0.071 Uiso 1 calc R . . .  
C4A C 0.5238(13) 0.0399(13) 0.1315(13) 0.063(4) Uani 1 d . . .  
H4A H 0.6012 0.0161 0.1321 0.075 Uiso 1 calc R . . .  
C5A C 0.4498(12) -0.0374(12) 0.1455(13) 0.056(4) Uani 1 d . . .  
H5A H 0.4776 -0.1138 0.1552 0.067 Uiso 1 calc R . . .  
C6A C 0.3358(11) -0.0005(10) 0.1447(10) 0.042(3) Uani 1 d . . .  
C7A C 0.2511(11) -0.0735(10) 0.1544(10) 0.041(3) Uani 1 d . . .  
C8A C 0.2796(12) -0.1893(10) 0.1596(11) 0.048(3) Uani 1 d . . .  
H8A H 0.3571 -0.2247 0.1545 0.057 Uiso 1 calc R . . .  
C9A C 0.1936(13) -0.2521(11) 0.1724(13) 0.056(4) Uani 1 d . . .  
H9A H 0.2120 -0.3300 0.1778 0.067 Uiso 1 calc R . . .  
C10A C 0.0814(13) -0.1993(11) 0.1773(12) 0.054(3) Uani 1 d . . .  
H10A H 0.0224 -0.2402 0.1850 0.065 Uiso 1 calc R . . .  
C11A C 0.0569(12) -0.0826(10) 0.1704(10) 0.043(3) Uani 1 d . . .  
H11A H -0.0198 -0.0467 0.1739 0.052 Uiso 1 calc R . . .  
N12A N 0.1395(8) -0.0193(7) 0.1588(8) 0.034(2) Uani 1 d . . .  
N11B N 0.0392(9) 0.1505(8) 0.3174(9) 0.042(2) Uani 1 d . . .  
C2B C 0.1006(13) 0.1276(11) 0.3843(11) 0.051(3) Uani 1 d . . .  
H2B H 0.1848 0.1054 0.3529 0.061 Uiso 1 calc R . . .  
C3B C 0.0445(16) 0.1356(14) 0.4957(13) 0.067(4) Uani 1 d . . .  
H3B H 0.0902 0.1220 0.5389 0.080 Uiso 1 calc R . . .  
C4B C -0.0800(16) 0.1640(15) 0.5437(12) 0.071(5) Uani 1 d . . .  
H4B H -0.1197 0.1686 0.6202 0.085 Uiso 1 calc R . . .  
C5B C -0.1462(14) 0.1855(14) 0.4781(12) 0.064(4) Uani 1 d . . .  
H5B H -0.2308 0.2046 0.5093 0.077 Uiso 1 calc R . . .  
C6B C -0.0834(12) 0.1780(10) 0.3646(11) 0.045(3) Uani 1 d . . .  
C7B C -0.1431(11) 0.2012(10) 0.2842(11) 0.043(3) Uani 1 d . . .  
C8B C -0.2671(13) 0.2394(13) 0.3137(13) 0.060(4) Uani 1 d . . .  
H8B H -0.3175 0.2523 0.3871 0.072 Uiso 1 calc R . . .  
C9B C -0.3156(13) 0.2584(14) 0.2339(15) 0.068(4) Uani 1 d . . .  
H9B H -0.3982 0.2857 0.2526 0.082 Uiso 1 calc R . . .  
C10B C -0.2401(14) 0.2365(13) 0.1269(14) 0.062(4) Uani 1 d . . .  
H10B H -0.2712 0.2461 0.0724 0.074 Uiso 1 calc R . . .  
C11B C -0.1163(11) 0.1996(11) 0.1009(11) 0.048(3) Uani 1 d . . .  
H11B H -0.0648 0.1859 0.0279 0.057 Uiso 1 calc R . . .  
N12B N -0.0682(9) 0.1828(7) 0.1800(8) 0.037(2) Uani 1 d . . .  
N1 N 0.1086(9) 0.3238(8) 0.1180(9) 0.039(2) Uani 1 d . . .

C2 C 0.0696(12) 0.3974(10) 0.1945(12) 0.048(3) Uani 1 d . . . .  
H2 H 0.0442 0.3706 0.2698 0.057 Uiso 1 calc R . . .  
C3 C 0.0666(14) 0.5105(11) 0.1634(13) 0.058(4) Uani 1 d . . . .  
H3 H 0.0361 0.5578 0.2194 0.070 Uiso 1 calc R . . .  
N4 N 0.1042(12) 0.5556(9) 0.0598(12) 0.061(3) Uani 1 d . . . .  
C5 C 0.1453(13) 0.4845(11) -0.0186(13) 0.055(3) Uani 1 d . . . .  
H5 H 0.1738 0.5132 -0.0935 0.067 Uiso 1 calc R . . .  
C6 C 0.1466(11) 0.3683(10) 0.0094(11) 0.044(3) Uani 1 d . . . .  
C7 C 0.1801(11) 0.2865(10) -0.0684(10) 0.042(3) Uani 1 d . . . .  
C8 C 0.2279(11) 0.1955(11) -0.2008(11) 0.045(3) Uani 1 d . . . .  
N2 N 0.1715(9) 0.1799(8) -0.0243(8) 0.039(2) Uani 1 d . . . .  
N3 N 0.2148(10) 0.3026(9) -0.1791(9) 0.050(3) Uani 1 d . . . .  
N5 N 0.2021(9) 0.1193(8) -0.1103(8) 0.042(2) Uani 1 d . . . .  
C31 C 0.2685(12) 0.1658(12) -0.3157(11) 0.051(3) Uani 1 d . . . .  
C32 C 0.2797(18) 0.2485(16) -0.4038(14) 0.080(5) Uani 1 d . . . .  
H32 H 0.2575 0.3235 -0.3907 0.096 Uiso 1 calc R . . .  
C33 C 0.3244(19) 0.2205(18) -0.5130(15) 0.087(6) Uani 1 d . . . .  
H33 H 0.3336 0.2768 -0.5723 0.104 Uiso 1 calc R . . .  
C34 C 0.3541(16) 0.1119(19) -0.5321(14) 0.081(5) Uani 1 d . . . .  
H34 H 0.3825 0.0930 -0.6044 0.097 Uiso 1 calc R . . .  
C35 C 0.3424(15) 0.0304(15) -0.4459(14) 0.073(5) Uani 1 d . . . .  
H35 H 0.3649 -0.0443 -0.4598 0.087 Uiso 1 calc R . . .  
C36 C 0.2983(13) 0.0557(13) -0.3389(12) 0.060(4) Uani 1 d . . . .  
H36 H 0.2882 -0.0019 -0.2807 0.072 Uiso 1 calc R . . .  
P1 P 0.5000 0.5000 -1.0000 0.077(2) Uani 1 d SD . . .  
F11A F 0.3754(18) 0.4780(19) -0.905(2) 0.147(11) Uani 0.81(5) d PDU A -1  
F12A F 0.505(3) 0.5997(17) -0.9438(19) 0.140(11) Uani 0.81(5) d PDU A -1  
F13A F 0.570(2) 0.4132(16) -0.938(2) 0.143(12) Uani 0.81(5) d PDU A -1  
F11B F 0.404(10) 0.604(8) -0.951(13) 0.29(9) Uani 0.19(5) d PDU A -2  
F12B F 0.592(8) 0.543(7) -0.969(10) 0.16(5) Uani 0.19(5) d PDU A -2  
F13B F 0.455(13) 0.430(6) -0.884(6) 0.15(5) Uani 0.19(5) d PDU A -2  
P2 P 0.001(5) 0.502(4) 0.500(4) 0.093(3) Uani 1 d SD B -2  
F21A F 0.122(7) 0.458(10) 0.413(5) 0.16(3) Uani 0.42(13) d PDU C -1  
F22A F 0.066(9) 0.554(8) 0.549(6) 0.12(2) Uani 0.42(13) d PDU C -1  
F23A F 0.010(9) 0.398(6) 0.579(6) 0.14(3) Uani 0.42(13) d PDU C -1  
F21B F 0.099(5) 0.411(4) 0.422(4) 0.129(17) Uani 0.58(13) d PDU B -2  
F22B F 0.100(6) 0.514(7) 0.545(6) 0.16(2) Uani 0.58(13) d PDU B -2  
F23B F -0.047(9) 0.405(4) 0.600(4) 0.14(2) Uani 0.58(13) d PDU B -2  
C1S C 0.635(10) 0.418(7) 0.571(10) 0.22(5) Uani 0.35 d PDU D -1  
H1S1 H 0.6908 0.4379 0.4959 0.323 Uiso 0.35 calc PR D -1  
H1S2 H 0.6799 0.3732 0.6126 0.323 Uiso 0.35 calc PR D -1  
H1S3 H 0.5914 0.4855 0.6056 0.323 Uiso 0.35 calc PR D -1  
C2S C 0.553(11) 0.358(8) 0.568(11) 0.26(5) Uani 0.35 d PDU D -1  
H2S1 H 0.5699 0.3534 0.4909 0.307 Uiso 0.35 calc PR D -1  
H2S2 H 0.4711 0.4002 0.6008 0.307 Uiso 0.35 calc PR D -1  
O3S O 0.553(4) 0.247(6) 0.625(5) 0.15(2) Uani 0.35 d PDU D -1  
H3S H 0.5227 0.2104 0.6010 0.218 Uiso 0.35 calc PR D -1  
O4S O 0.514(11) 0.323(10) 0.705(10) 0.25(5) Uani 0.35 d PDU E -2  
H4S1 H 0.5424 0.3060 0.7532 0.375 Uiso 0.35 calc PR E -2  
C5S C 0.511(11) 0.438(9) 0.670(14) 0.23(6) Uani 0.35 d PDU E -2  
H5S1 H 0.4928 0.4550 0.6032 0.279 Uiso 0.35 calc PR E -2  
H5S2 H 0.4458 0.4800 0.7274 0.279 Uiso 0.35 calc PR E -2  
C6S C 0.620(11) 0.471(9) 0.646(10) 0.22(5) Uani 0.35 d PDU E -2  
H6S1 H 0.6691 0.4113 0.6737 0.330 Uiso 0.35 calc PR E -2  
H6S2 H 0.6047 0.5365 0.6818 0.330 Uiso 0.35 calc PR E -2  
H6S3 H 0.6613 0.4868 0.5670 0.330 Uiso 0.35 calc PR E -2  
O1W O 0.366(9) 0.469(7) 0.673(7) 0.15(3) Uani 0.25 d PDU F -1  
H1W H 0.46(9) 0.51(8) 0.64(7) 0.218 Uiso 0.25 d PD G -1  
H2W H 0.55(11) 0.45(6) 0.48(7) 0.218 Uiso 0.25 d PD H -1  
O2W O 0.253(8) 0.513(4) 0.682(5) 0.11(2) Uani 0.25 d PDU I -2  
H3W H 0.15(3) 0.53(7) 0.71(7) 0.162 Uiso 0.25 d PD J -2

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loop\_

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Ru1 0.0364(5) 0.0329(5) 0.0389(6) -0.0019(4) -0.0167(4) -0.0064(4)

N11A 0.045(6) 0.037(5) 0.036(6) -0.005(4) -0.012(5) -0.013(4)

C2A 0.043(7) 0.048(7) 0.071(10) -0.006(7) -0.025(7) -0.011(6)

C3A 0.050(8) 0.064(9) 0.067(10) 0.001(8) -0.025(8) -0.023(7)

C4A 0.041(7) 0.072(10) 0.076(11) -0.008(8) -0.026(8) -0.003(7)

C5A 0.047(7) 0.052(8) 0.066(10) -0.008(7) -0.025(7) 0.002(6)

C6A 0.040(7) 0.047(7) 0.037(7) -0.009(6) -0.013(6) -0.006(5)

C7A 0.052(7) 0.035(6) 0.036(7) -0.001(5) -0.019(6) -0.007(5)

C8A 0.048(7) 0.044(7) 0.046(8) -0.002(6) -0.016(6) -0.005(6)

C9A 0.070(9) 0.031(6) 0.069(10) -0.008(6) -0.031(8) -0.005(6)

C10A 0.067(9) 0.047(8) 0.060(9) -0.008(7) -0.033(8) -0.016(7)

C11A 0.048(7) 0.040(7) 0.045(8) -0.007(6) -0.019(6) -0.010(5)

N12A 0.037(5) 0.029(5) 0.035(6) -0.002(4) -0.016(4) -0.004(4)

N11B 0.050(6) 0.032(5) 0.049(7) -0.006(5) -0.021(5) -0.008(4)

C2B 0.060(8) 0.056(8) 0.045(8) 0.003(6) -0.031(7) -0.012(7)

C3B 0.079(11) 0.082(11) 0.055(10) -0.007(8) -0.040(9) -0.017(9)

C4B 0.080(11) 0.100(13) 0.030(8) -0.012(8) -0.013(8) -0.025(10)

C5B 0.051(8) 0.090(12) 0.042(9) -0.014(8) -0.007(7) -0.013(8)

C6B 0.053(8) 0.039(7) 0.049(8) -0.011(6) -0.021(7) -0.007(6)

C7B 0.034(6) 0.046(7) 0.048(8) -0.007(6) -0.014(6) -0.004(5)

C8B 0.045(8) 0.073(10) 0.056(9) -0.013(8) -0.013(7) -0.003(7)

C9B 0.039(8) 0.075(10) 0.089(13) -0.008(9) -0.030(9) 0.002(7)

C10B 0.056(9) 0.075(10) 0.065(11) 0.001(8) -0.036(8) -0.013(8)

C11B 0.042(7) 0.061(8) 0.042(8) 0.006(6) -0.020(6) -0.018(6)

N12B 0.046(6) 0.030(5) 0.034(6) -0.005(4) -0.016(5) -0.005(4)

N1 0.040(5) 0.032(5) 0.042(6) -0.003(5) -0.017(5) -0.001(4)

C2 0.061(8) 0.035(6) 0.048(8) -0.006(6) -0.023(7) -0.007(6)

C3 0.079(10) 0.039(7) 0.060(10) -0.010(7) -0.027(8) -0.014(7)

N4 0.071(8) 0.039(6) 0.073(9) -0.004(6) -0.032(7) -0.003(6)

C5 0.063(9) 0.046(8) 0.057(9) -0.002(7) -0.023(8) -0.013(7)

C6 0.047(7) 0.037(6) 0.049(8) -0.003(6) -0.021(6) -0.004(5)

C7 0.042(7) 0.041(7) 0.034(7) -0.002(5) -0.008(6) -0.005(5)

C8 0.043(7) 0.049(7) 0.041(8) -0.003(6) -0.018(6) -0.002(6)

N2 0.038(5) 0.038(5) 0.037(6) -0.004(4) -0.012(5) -0.007(4)

N3 0.058(7) 0.045(6) 0.045(7) 0.000(5) -0.019(6) -0.008(5)

N5 0.039(5) 0.046(6) 0.037(6) -0.004(5) -0.014(5) -0.004(5)

C31 0.048(8) 0.063(9) 0.039(8) 0.004(7) -0.017(6) -0.010(6)

C32 0.104(14) 0.081(12) 0.054(11) -0.004(9) -0.036(10) -0.004(10)

C33 0.112(16) 0.097(15) 0.048(11) 0.004(10) -0.033(11) -0.018(12)

C34 0.070(11) 0.131(18) 0.039(10) -0.018(11) -0.016(8) -0.017(11)

C35 0.069(10) 0.081(12) 0.065(12) -0.030(10) -0.016(9) -0.010(9)

C36 0.064(9) 0.070(10) 0.041(8) -0.012(7) -0.018(7) -0.005(8)

P1 0.056(3) 0.045(3) 0.118(6) -0.008(4) -0.031(4) 0.006(3)

F11A 0.088(13) 0.104(18) 0.17(2) -0.024(15) 0.022(13) -0.009(11)

F12A 0.17(3) 0.088(14) 0.164(19) -0.038(12) -0.059(18) -0.020(16)

F13A 0.13(2) 0.101(14) 0.20(3) 0.015(14) -0.10(2) 0.019(12)

F11B 0.27(14) 0.13(8) 0.41(17) -0.17(10) -0.07(12) 0.07(9)

F12B 0.08(6) 0.10(6) 0.30(13) -0.09(7) -0.05(7) -0.01(4)

F13B 0.22(12) 0.05(4) 0.11(6) -0.02(4) 0.00(6) -0.01(5)

P2 0.152(8) 0.071(5) 0.066(5) -0.013(4) -0.052(5) -0.014(5)

F21A 0.16(4) 0.14(6) 0.12(3) -0.05(3) 0.01(3) 0.01(4)

F22A 0.14(4) 0.15(5) 0.10(3) -0.04(3) -0.06(3) -0.03(4)  
F23A 0.17(5) 0.11(4) 0.11(4) 0.02(3) -0.06(4) 0.01(3)  
F21B 0.20(4) 0.09(2) 0.11(2) -0.049(18) -0.09(3) 0.03(2)  
F22B 0.21(5) 0.14(4) 0.17(4) -0.05(3) -0.12(4) 0.01(3)  
F23B 0.27(6) 0.10(3) 0.07(2) 0.008(16) -0.05(3) -0.08(3)  
C1S 0.28(11) 0.15(7) 0.28(12) -0.07(7) -0.17(9) 0.00(6)  
C2S 0.23(8) 0.26(8) 0.28(9) -0.04(7) -0.11(7) -0.04(6)  
O3S 0.04(2) 0.23(6) 0.13(4) 0.02(4) -0.02(3) -0.03(3)  
O4S 0.23(8) 0.30(9) 0.23(9) 0.08(8) -0.14(8) -0.07(8)  
C5S 0.24(9) 0.27(9) 0.21(9) -0.08(7) -0.09(7) -0.01(7)  
C6S 0.21(9) 0.20(9) 0.18(9) -0.04(8) -0.01(8) -0.01(7)  
O1W 0.18(6) 0.11(5) 0.12(5) 0.00(4) -0.01(5) -0.07(5)  
O2W 0.18(6) 0.05(3) 0.07(3) 0.01(2) -0.02(4) -0.05(3)

\_geom\_special\_details

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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loop\_

\_geom\_bond\_atom\_site\_label\_1

\_geom\_bond\_atom\_site\_label\_2

\_geom\_bond\_distance

\_geom\_bond\_site\_symmetry\_2

\_geom\_bond\_publ\_flag

Ru1 N11A 2.036(10) . ?

Ru1 N12A 2.042(9) . ?

Ru1 N12B 2.046(10) . ?

Ru1 N2 2.051(10) . ?

Ru1 N11B 2.064(11) . ?

Ru1 N1 2.069(9) . ?

N11A C6A 1.369(15) . ?

N11A C2A 1.372(15) . ?

C2A C3A 1.366(18) . ?

C2A H2A 0.9300 . ?

C3A C4A 1.37(2) . ?

C3A H3A 0.9300 . ?

C4A C5A 1.389(19) . ?

C4A H4A 0.9300 . ?

C5A C6A 1.371(17) . ?

C5A H5A 0.9300 . ?

C6A C7A 1.468(16) . ?

C7A N12A 1.361(15) . ?

C7A C8A 1.385(16) . ?

C8A C9A 1.375(18) . ?

C8A H8A 0.9300 . ?

C9A C10A 1.362(19) . ?

C9A H9A 0.9300 . ?

C10A C11A 1.392(17) . ?

C10A H10A 0.9300 . ?

C11A N12A 1.350(14) . ?

C11A H11A 0.9300 . ?

N11B C2B 1.344(15) . ?

N11B C6B 1.348(16) . ?

C2B C3B 1.36(2) . ?

C2B H2B 0.9300 . ?



C3B C4B 1.37(2) . ?  
C3B H3B 0.9300 . ?  
C4B C5B 1.38(2) . ?  
C4B H4B 0.9300 . ?  
C5B C6B 1.385(19) . ?  
C5B H5B 0.9300 . ?  
C6B C7B 1.487(17) . ?  
C7B N12B 1.328(16) . ?  
C7B C8B 1.388(17) . ?  
C8B C9B 1.38(2) . ?  
C8B H8B 0.9300 . ?  
C9B C10B 1.37(2) . ?  
C9B H9B 0.9300 . ?  
C10B C11B 1.389(19) . ?  
C10B H10B 0.9300 . ?  
C11B N12B 1.372(15) . ?  
C11B H11B 0.9300 . ?  
N1 C2 1.353(16) . ?  
N1 C6 1.358(16) . ?  
C2 C3 1.371(17) . ?  
C2 H2 0.9300 . ?  
C3 N4 1.305(18) . ?  
C3 H3 0.9300 . ?  
N4 C5 1.347(18) . ?  
C5 C6 1.406(17) . ?  
C5 H5 0.9300 . ?  
C6 C7 1.451(17) . ?  
C7 N3 1.336(16) . ?  
C7 N2 1.338(15) . ?  
C8 N5 1.344(15) . ?  
C8 N3 1.362(16) . ?  
C8 C31 1.485(18) . ?  
N2 N5 1.358(14) . ?  
C31 C32 1.38(2) . ?  
C31 C36 1.38(2) . ?  
C32 C33 1.40(2) . ?  
C32 H32 0.9300 . ?  
C33 C34 1.35(3) . ?  
C33 H33 0.9300 . ?  
C34 C35 1.35(2) . ?  
C34 H34 0.9300 . ?  
C35 C36 1.36(2) . ?  
C35 H35 0.9300 . ?  
C36 H36 0.9300 . ?

loop\_  
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N11A Ru1 N12A 78.6(4) . . ?  
N11A Ru1 N12B 173.3(4) . . ?  
N12A Ru1 N12B 98.4(4) . . ?  
N11A Ru1 N2 90.5(4) . . ?  
N12A Ru1 N2 97.2(4) . . ?  
N12B Ru1 N2 95.8(4) . . ?  
N11A Ru1 N11B 95.7(4) . . ?  
N12A Ru1 N11B 91.6(4) . . ?

N12B Ru1 N11B 78.4(4) . . ?  
N2 Ru1 N11B 170.1(4) . . ?  
N11A Ru1 N1 96.8(4) . . ?  
N12A Ru1 N1 173.5(4) . . ?  
N12B Ru1 N1 86.7(4) . . ?  
N2 Ru1 N1 78.2(4) . . ?  
N11B Ru1 N1 93.4(4) . . ?  
C6A N11A C2A 117.1(10) . . ?  
C6A N11A Ru1 116.9(7) . . ?  
C2A N11A Ru1 125.7(8) . . ?  
C3A C2A N11A 122.4(13) . . ?  
C3A C2A H2A 118.8 . . ?  
N11A C2A H2A 118.8 . . ?  
C2A C3A C4A 120.0(12) . . ?  
C2A C3A H3A 120.0 . . ?  
C4A C3A H3A 120.0 . . ?  
C3A C4A C5A 118.7(12) . . ?  
C3A C4A H4A 120.6 . . ?  
C5A C4A H4A 120.6 . . ?  
C6A C5A C4A 119.7(13) . . ?  
C6A C5A H5A 120.2 . . ?  
C4A C5A H5A 120.1 . . ?  
N11A C6A C5A 122.1(11) . . ?  
N11A C6A C7A 112.9(10) . . ?  
C5A C6A C7A 125.0(12) . . ?  
N12A C7A C8A 121.2(11) . . ?  
N12A C7A C6A 115.2(10) . . ?  
C8A C7A C6A 123.6(11) . . ?  
C9A C8A C7A 120.1(12) . . ?  
C9A C8A H8A 119.9 . . ?  
C7A C8A H8A 119.9 . . ?  
C10A C9A C8A 119.4(12) . . ?  
C10A C9A H9A 120.3 . . ?  
C8A C9A H9A 120.3 . . ?  
C9A C10A C11A 118.6(12) . . ?  
C9A C10A H10A 120.7 . . ?  
C11A C10A H10A 120.7 . . ?  
N12A C11A C10A 123.0(12) . . ?  
N12A C11A H11A 118.5 . . ?  
C10A C11A H11A 118.5 . . ?  
C11A N12A C7A 117.6(10) . . ?  
C11A N12A Ru1 126.4(8) . . ?  
C7A N12A Ru1 115.9(7) . . ?  
C2B N11B C6B 118.1(11) . . ?  
C2B N11B Ru1 126.3(9) . . ?  
C6B N11B Ru1 115.5(8) . . ?  
N11B C2B C3B 122.6(14) . . ?  
N11B C2B H2B 118.7 . . ?  
C3B C2B H2B 118.7 . . ?  
C2B C3B C4B 119.3(13) . . ?  
C2B C3B H3B 120.3 . . ?  
C4B C3B H3B 120.3 . . ?  
C3B C4B C5B 119.6(14) . . ?  
C3B C4B H4B 120.2 . . ?  
C5B C4B H4B 120.2 . . ?  
C4B C5B C6B 118.3(14) . . ?  
C4B C5B H5B 120.9 . . ?  
C6B C5B H5B 120.8 . . ?  
N11B C6B C5B 122.0(12) . . ?  
N11B C6B C7B 114.2(11) . . ?  
C5B C6B C7B 123.8(12) . . ?

N12B C7B C8B 121.7(12) . . ?  
N12B C7B C6B 114.7(10) . . ?  
C8B C7B C6B 123.5(12) . . ?  
C9B C8B C7B 119.9(14) . . ?  
C9B C8B H8B 120.0 . . ?  
C7B C8B H8B 120.0 . . ?  
C10B C9B C8B 119.0(13) . . ?  
C10B C9B H9B 120.5 . . ?  
C8B C9B H9B 120.5 . . ?  
C9B C10B C11B 119.0(13) . . ?  
C9B C10B H10B 120.5 . . ?  
C11B C10B H10B 120.5 . . ?  
N12B C11B C10B 121.8(13) . . ?  
N12B C11B H11B 119.1 . . ?  
C10B C11B H11B 119.1 . . ?  
C7B N12B C11B 118.5(10) . . ?  
C7B N12B Ru1 116.4(7) . . ?  
C11B N12B Ru1 124.5(9) . . ?  
C2 N1 C6 116.2(10) . . ?  
C2 N1 Ru1 128.0(9) . . ?  
C6 N1 Ru1 115.8(8) . . ?  
N1 C2 C3 121.5(13) . . ?  
N1 C2 H2 119.3 . . ?  
C3 C2 H2 119.3 . . ?  
N4 C3 C2 123.7(13) . . ?  
N4 C3 H3 118.1 . . ?  
C2 C3 H3 118.1 . . ?  
C3 N4 C5 116.3(12) . . ?  
N4 C5 C6 122.0(13) . . ?  
N4 C5 H5 119.0 . . ?  
C6 C5 H5 119.0 . . ?  
N1 C6 C5 120.3(12) . . ?  
N1 C6 C7 113.8(10) . . ?  
C5 C6 C7 125.9(12) . . ?  
N3 C7 N2 114.3(11) . . ?  
N3 C7 C6 129.1(11) . . ?  
N2 C7 C6 116.5(11) . . ?  
N5 C8 N3 114.8(12) . . ?  
N5 C8 C31 122.9(12) . . ?  
N3 C8 C31 122.3(12) . . ?  
C7 N2 N5 106.7(10) . . ?  
C7 N2 Ru1 115.7(8) . . ?  
N5 N2 Ru1 137.6(8) . . ?  
C7 N3 C8 100.2(10) . . ?  
C8 N5 N2 104.1(10) . . ?  
C32 C31 C36 117.6(14) . . ?  
C32 C31 C8 120.5(14) . . ?  
C36 C31 C8 121.9(12) . . ?  
C31 C32 C33 120.5(18) . . ?  
C31 C32 H32 119.8 . . ?  
C33 C32 H32 119.8 . . ?  
C34 C33 C32 119.9(17) . . ?  
C34 C33 H33 120.1 . . ?  
C32 C33 H33 120.0 . . ?  
C33 C34 C35 119.8(17) . . ?  
C33 C34 H34 120.1 . . ?  
C35 C34 H34 120.1 . . ?  
C34 C35 C36 121.2(17) . . ?  
C34 C35 H35 119.4 . . ?  
C36 C35 H35 119.4 . . ?  
C35 C36 C31 120.9(15) . . ?

C35 C36 H36 119.6 . . ?  
C31 C36 H36 119.6 . . ?

loop\_

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N12A Ru1 N11A C6A -5.3(8) . . . . ?  
N12B Ru1 N11A C6A 58(4) . . . . ?  
N2 Ru1 N11A C6A -102.6(9) . . . . ?  
N11B Ru1 N11A C6A 85.2(9) . . . . ?  
N1 Ru1 N11A C6A 179.3(8) . . . . ?  
N12A Ru1 N11A C2A -179.0(11) . . . . ?  
N12B Ru1 N11A C2A -116(3) . . . . ?  
N2 Ru1 N11A C2A 83.7(11) . . . . ?  
N11B Ru1 N11A C2A -88.5(11) . . . . ?  
N1 Ru1 N11A C2A 5.5(11) . . . . ?  
C6A N11A C2A C3A 0(2) . . . . ?  
Ru1 N11A C2A C3A 174.1(11) . . . . ?  
N11A C2A C3A C4A -1(2) . . . . ?  
C2A C3A C4A C5A 0(2) . . . . ?  
C3A C4A C5A C6A 0(2) . . . . ?  
C2A N11A C6A C5A -0.2(19) . . . . ?  
Ru1 N11A C6A C5A -174.5(10) . . . . ?  
C2A N11A C6A C7A -178.0(11) . . . . ?  
Ru1 N11A C6A C7A 7.7(13) . . . . ?  
C4A C5A C6A N11A 0(2) . . . . ?  
C4A C5A C6A C7A 177.6(13) . . . . ?  
N11A C6A C7A N12A -6.2(16) . . . . ?  
C5A C6A C7A N12A 176.0(12) . . . . ?  
N11A C6A C7A C8A 174.2(11) . . . . ?  
C5A C6A C7A C8A -3(2) . . . . ?  
N12A C7A C8A C9A -1.7(19) . . . . ?  
C6A C7A C8A C9A 177.8(13) . . . . ?  
C7A C8A C9A C10A 2(2) . . . . ?  
C8A C9A C10A C11A -1(2) . . . . ?  
C9A C10A C11A N12A 0(2) . . . . ?  
C10A C11A N12A C7A -0.3(18) . . . . ?  
C10A C11A N12A Ru1 179.2(10) . . . . ?  
C8A C7A N12A C11A 1.1(17) . . . . ?  
C6A C7A N12A C11A -178.5(10) . . . . ?  
C8A C7A N12A Ru1 -178.5(9) . . . . ?  
C6A C7A N12A Ru1 1.9(13) . . . . ?  
N11A Ru1 N12A C11A -177.9(10) . . . . ?  
N12B Ru1 N12A C11A 8.1(10) . . . . ?  
N2 Ru1 N12A C11A -88.8(10) . . . . ?  
N11B Ru1 N12A C11A 86.6(10) . . . . ?  
N1 Ru1 N12A C11A -133(3) . . . . ?  
N11A Ru1 N12A C7A 1.6(8) . . . . ?  
N12B Ru1 N12A C7A -172.3(8) . . . . ?  
N2 Ru1 N12A C7A 90.7(9) . . . . ?  
N11B Ru1 N12A C7A -93.8(9) . . . . ?  
N1 Ru1 N12A C7A 46(4) . . . . ?  
N11A Ru1 N11B C2B -0.4(10) . . . . ?

N12A Ru1 N11B C2B 78.3(10) . . . . ?  
N12B Ru1 N11B C2B 176.5(10) . . . . ?  
N2 Ru1 N11B C2B -129(2) . . . . ?  
N1 Ru1 N11B C2B -97.6(10) . . . . ?  
N11A Ru1 N11B C6B 178.0(8) . . . . ?  
N12A Ru1 N11B C6B -103.3(8) . . . . ?  
N12B Ru1 N11B C6B -5.1(8) . . . . ?  
N2 Ru1 N11B C6B 49(2) . . . . ?  
N1 Ru1 N11B C6B 80.8(8) . . . . ?  
C6B N11B C2B C3B -2.7(19) . . . . ?  
Ru1 N11B C2B C3B 175.7(11) . . . . ?  
N11B C2B C3B C4B 3(2) . . . . ?  
C2B C3B C4B C5B -1(3) . . . . ?  
C3B C4B C5B C6B 0(2) . . . . ?  
C2B N11B C6B C5B 1.4(18) . . . . ?  
Ru1 N11B C6B C5B -177.1(11) . . . . ?  
C2B N11B C6B C7B -179.6(10) . . . . ?  
Ru1 N11B C6B C7B 1.8(13) . . . . ?  
C4B C5B C6B N11B 0(2) . . . . ?  
C4B C5B C6B C7B -178.8(13) . . . . ?  
N11B C6B C7B N12B 5.0(15) . . . . ?  
C5B C6B C7B N12B -176.1(12) . . . . ?  
N11B C6B C7B C8B -174.7(12) . . . . ?  
C5B C6B C7B C8B 4(2) . . . . ?  
N12B C7B C8B C9B 1(2) . . . . ?  
C6B C7B C8B C9B -179.7(13) . . . . ?  
C7B C8B C9B C10B 1(2) . . . . ?  
C8B C9B C10B C11B -2(2) . . . . ?  
C9B C10B C11B N12B 1(2) . . . . ?  
C8B C7B N12B C11B -1.7(18) . . . . ?  
C6B C7B N12B C11B 178.5(10) . . . . ?  
C8B C7B N12B Ru1 170.2(10) . . . . ?  
C6B C7B N12B Ru1 -9.5(13) . . . . ?  
C10B C11B N12B C7B 0.9(18) . . . . ?  
C10B C11B N12B Ru1 -170.4(10) . . . . ?  
N11A Ru1 N12B C7B 36(4) . . . . ?  
N12A Ru1 N12B C7B 98.0(9) . . . . ?  
N2 Ru1 N12B C7B -163.8(8) . . . . ?  
N11B Ru1 N12B C7B 8.1(8) . . . . ?  
N1 Ru1 N12B C7B -86.0(9) . . . . ?  
N11A Ru1 N12B C11B -153(3) . . . . ?  
N12A Ru1 N12B C11B -90.5(10) . . . . ?  
N2 Ru1 N12B C11B 7.7(10) . . . . ?  
N11B Ru1 N12B C11B 179.5(10) . . . . ?  
N1 Ru1 N12B C11B 85.4(10) . . . . ?  
N11A Ru1 N1 C2 -94.5(10) . . . . ?  
N12A Ru1 N1 C2 -138(3) . . . . ?  
N12B Ru1 N1 C2 79.8(10) . . . . ?  
N2 Ru1 N1 C2 176.4(11) . . . . ?  
N11B Ru1 N1 C2 1.7(10) . . . . ?  
N11A Ru1 N1 C6 86.8(8) . . . . ?  
N12A Ru1 N1 C6 43(4) . . . . ?  
N12B Ru1 N1 C6 -99.0(8) . . . . ?  
N2 Ru1 N1 C6 -2.4(8) . . . . ?  
N11B Ru1 N1 C6 -177.1(8) . . . . ?  
C6 N1 C2 C3 1.2(18) . . . . ?  
Ru1 N1 C2 C3 -177.5(10) . . . . ?  
N1 C2 C3 N4 -2(2) . . . . ?  
C2 C3 N4 C5 1(2) . . . . ?  
C3 N4 C5 C6 1(2) . . . . ?  
C2 N1 C6 C5 0.7(17) . . . . ?

Ru1 N1 C6 C5 179.6(9) . . . . ?  
C2 N1 C6 C7 -176.4(10) . . . . ?  
Ru1 N1 C6 C7 2.6(13) . . . . ?  
N4 C5 C6 N1 -2(2) . . . . ?  
N4 C5 C6 C7 174.9(12) . . . . ?  
N1 C6 C7 N3 176.2(12) . . . . ?  
C5 C6 C7 N3 -1(2) . . . . ?  
N1 C6 C7 N2 -1.1(16) . . . . ?  
C5 C6 C7 N2 -177.9(12) . . . . ?  
N3 C7 N2 N5 -0.1(14) . . . . ?  
C6 C7 N2 N5 177.6(10) . . . . ?  
N3 C7 N2 Ru1 -178.6(8) . . . . ?  
C6 C7 N2 Ru1 -0.9(14) . . . . ?  
N11A Ru1 N2 C7 -95.1(8) . . . . ?  
N12A Ru1 N2 C7 -173.6(8) . . . . ?  
N12B Ru1 N2 C7 87.2(8) . . . . ?  
N11B Ru1 N2 C7 34(3) . . . . ?  
N1 Ru1 N2 C7 1.7(8) . . . . ?  
N11A Ru1 N2 N5 87.1(11) . . . . ?  
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N11B Ru1 N2 N5 -144.1(19) . . . . ?  
N1 Ru1 N2 N5 -176.1(11) . . . . ?  
N2 C7 N3 C8 -0.3(14) . . . . ?  
C6 C7 N3 C8 -177.7(12) . . . . ?  
N5 C8 N3 C7 0.6(14) . . . . ?  
C31 C8 N3 C7 -179.0(11) . . . . ?  
N3 C8 N5 N2 -0.7(13) . . . . ?  
C31 C8 N5 N2 178.9(11) . . . . ?  
C7 N2 N5 C8 0.5(12) . . . . ?  
Ru1 N2 N5 C8 178.5(9) . . . . ?  
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N3 C8 C31 C32 -8(2) . . . . ?  
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C8 C31 C32 C33 176.5(15) . . . . ?  
C31 C32 C33 C34 1(3) . . . . ?  
C32 C33 C34 C35 -1(3) . . . . ?  
C33 C34 C35 C36 2(3) . . . . ?  
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C8 C31 C36 C35 -176.0(13) . . . . ?

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N N 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
Ru Ru -1.2594 0.8363 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
O O 0.0106 0.0060 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
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  'x+1/2, y, z+1/2'
  'x+1/2, -y, -z+1/2'
  'x+1/2, -y+1/2, z+1'
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Refinement of F^2^ against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F^2^, conventional R-factors R are based
on F, with F set to zero for negative F^2^. The threshold expression of
F^2^ > 2sigma(F^2^) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F^2^ are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
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'calc w=1/[\s^2^(Fo^2^)+(0.0281P)^2^] where P=(Fo^2^+2Fc^2^)/3'
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loop\_

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N1 N 0.4318(3) 0.8389(3) 0.8932(2) 0.0497(11) Uani 1 d . . .
N2 N 0.3923(3) 0.8106(3) 0.9479(2) 0.0607(13) Uani 1 d . . .
N3 N 0.4173(3) 0.9334(3) 0.9667(2) 0.0607(13) Uani 1 d . . .
H3 H 0.4190 0.9776 0.9858 0.073 Uiso 0.50 calc PR . .
N4 N 0.4999(3) 0.9120(2) 0.7961(2) 0.0477(10) Uani 1 d . . .
N11 N 0.4991(3) 0.7727(2) 0.7028(2) 0.0546(12) Uani 1 d . . .
N21 N 0.3694(3) 0.8255(2) 0.7503(3) 0.0544(12) Uani 1 d . . .
N31 N 0.5652(3) 0.7630(2) 0.8509(2) 0.0507(11) Uani 1 d . . .
N41 N 0.4390(3) 0.6873(2) 0.8268(2) 0.0543(13) Uani 1 d . . .
C1 C 0.3859(4) 0.8694(4) 0.9907(3) 0.0669(17) Uani 1 d . . .
H1 H 0.3620 0.8661 1.0331 0.080 Uiso 1 calc R . .
C2 C 0.4458(3) 0.9126(3) 0.9055(3) 0.0509(15) Uani 1 d . . .
C3 C 0.4835(4) 0.9552(3) 0.8523(3) 0.0532(18) Uani 1 d . . .
C4 C 0.5047(4) 1.0316(3) 0.8528(4) 0.0736(19) Uani 1 d . . .
H4 H 0.4933 1.0602 0.8915 0.088 Uiso 1 calc R . .
N5 N 0.5394(4) 1.0656(3) 0.8026(4) 0.0811(16) Uani 1 d . . .
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C12 C 0.5649(4) 0.7453(3) 0.6815(3) 0.0651(18) Uani 1 d . . .
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C13 C 0.5807(5) 0.7310(4) 0.6133(4) 0.083(2) Uani 1 d . . .
H13 H 0.6281 0.7119 0.6001 0.100 Uiso 1 calc R . .
C14 C 0.5268(6) 0.7451(5) 0.5667(3) 0.093(2) Uani 1 d . . .
H14 H 0.5362 0.7349 0.5209 0.111 Uiso 1 calc R . .
C15 C 0.4560(7) 0.7753(4) 0.5865(3) 0.091(3) Uani 1 d . . .
H15 H 0.4183 0.7856 0.5543 0.109 Uiso 1 calc R . .
C16 C 0.4433(4) 0.7895(3) 0.6552(3) 0.064(2) Uani 1 d . . .
C22 C 0.3067(4) 0.8532(4) 0.7796(4) 0.078(2) Uani 1 d . . .
H22 H 0.3048 0.8564 0.8270 0.093 Uiso 1 calc R . .
C23 C 0.2443(5) 0.8773(5) 0.7420(5) 0.099(3) Uani 1 d . . .
H23 H 0.2001 0.8949 0.7632 0.119 Uiso 1 calc R . .

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C24 C 0.2502(7) 0.8743(5) 0.6714(6) 0.099(3) Uani 1 d . . .  
H24 H 0.2105 0.8928 0.6445 0.119 Uiso 1 calc R . .  
C25 C 0.3128(5) 0.8448(5) 0.6413(4) 0.085(2) Uani 1 d . . .  
H25 H 0.3158 0.8408 0.5939 0.102 Uiso 1 calc R . .  
C26 C 0.3720(5) 0.8209(3) 0.6817(3) 0.0647(18) Uani 1 d . . .  
C32 C 0.6296(4) 0.8025(4) 0.8609(3) 0.0664(16) Uani 1 d . . .  
H32 H 0.6337 0.8501 0.8401 0.080 Uiso 1 calc R . .  
C33 C 0.6900(4) 0.7776(4) 0.8995(4) 0.082(2) Uani 1 d . . .  
H33 H 0.7338 0.8074 0.9040 0.098 Uiso 1 calc R . .  
C34 C 0.6849(5) 0.7097(5) 0.9308(4) 0.090(2) Uani 1 d . . .  
H34 H 0.7249 0.6922 0.9580 0.108 Uiso 1 calc R . .  
C35 C 0.6201(5) 0.6658(4) 0.9223(4) 0.083(2) Uani 1 d . . .  
H35 H 0.6163 0.6181 0.9430 0.100 Uiso 1 calc R . .  
C36 C 0.5607(4) 0.6934(3) 0.8828(3) 0.0562(14) Uani 1 d . . .  
C42 C 0.3742(4) 0.6523(3) 0.8092(3) 0.0726(18) Uani 1 d . . .  
H42 H 0.3423 0.6748 0.7770 0.087 Uiso 1 calc R . .  
C43 C 0.3535(5) 0.5824(4) 0.8382(5) 0.099(3) Uani 1 d . . .  
H43 H 0.3079 0.5588 0.8259 0.118 Uiso 1 calc R . .  
C44 C 0.4006(6) 0.5496(5) 0.8845(5) 0.106(3) Uani 1 d . . .  
H44 H 0.3871 0.5035 0.9046 0.128 Uiso 1 calc R . .  
C45 C 0.4694(7) 0.5846(3) 0.9022(3) 0.0889(19) Uani 1 d . . .  
H45 H 0.5021 0.5625 0.9341 0.107 Uiso 1 calc R . .  
C46 C 0.4879(4) 0.6536(3) 0.8707(3) 0.0577(19) Uani 1 d . . .  
O1W O 0.6122(7) 1.0000 0.5000 0.145(7) Uani 0.748(18) d SPD . .  
H1W1 H 0.6219 0.9698 0.5327 0.174 Uiso 0.374(9) d PD . .  
H1W2 H 0.6572 1.0093 0.4845 0.174 Uiso 0.374(9) d PD . .  
P1A P 0.6782(15) 0.9942(17) 0.9988(16) 0.098(15) Uani 0.17 d PD A -1  
F11A F 0.6878(18) 0.9785(18) 0.9243(15) 0.145(18) Uani 0.34 d PDU A -1  
F12A F 0.5981(13) 0.9651(11) 0.9970(13) 0.120(7) Uani 0.34 d PDU A -1  
F13A F 0.7063(16) 0.9156(9) 1.0134(10) 0.102(6) Uani 0.34 d PDU A -1  
P1B P 0.6767(7) 1.0027(15) 0.9985(12) 0.080(5) Uani 0.33 d PD B -2  
F11B F 0.6754(9) 0.9805(9) 0.9206(5) 0.127(6) Uani 0.66 d PD B -2  
F12B F 0.6283(10) 0.9296(7) 1.0168(7) 0.165(7) Uani 0.66 d PD B -2  
F13B F 0.7522(6) 0.9546(7) 1.0099(5) 0.148(4) Uani 0.66 d PD B -2  
P2A P 0.7313(8) 0.9207(7) 0.6361(6) 0.101(4) Uani 0.522(16) d PD C -3  
F21A F 0.6473(8) 0.9001(10) 0.6179(9) 0.141(7) Uani 0.522(16) d PD C -3  
F22A F 0.7537(13) 0.8363(8) 0.6258(13) 0.222(14) Uani 0.522(16) d PD C -3  
F23A F 0.7136(8) 0.9077(14) 0.7127(6) 0.159(9) Uani 0.522(16) d PD C -3  
F24A F 0.7072(9) 1.0050(6) 0.6438(9) 0.158(7) Uani 0.522(16) d PD C -3  
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F26A F 0.8145(7) 0.9416(14) 0.6519(10) 0.195(9) Uani 0.522(16) d PD C -3  
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F21B F 0.6600(10) 0.9334(14) 0.6392(11) 0.210(14) Uani 0.478(16) d PDU C -4  
F22B F 0.7328(11) 0.8507(12) 0.5874(7) 0.158(10) Uani 0.478(16) d PDU C -4  
F23B F 0.7172(10) 0.8430(9) 0.6993(8) 0.147(7) Uani 0.478(16) d PDU C -4  
F24B F 0.7534(14) 0.9609(10) 0.7079(10) 0.216(15) Uani 0.478(16) d PD C -4  
F25B F 0.7707(12) 0.9672(10) 0.5960(11) 0.162(9) Uani 0.478(16) d PD C -4  
F26B F 0.8273(7) 0.8785(10) 0.6553(7) 0.123(6) Uani 0.478(16) d PD C -4

loop\_

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N2 0.060(3) 0.069(3) 0.053(3) -0.007(3) 0.008(3) -0.007(3)  
N3 0.064(3) 0.066(3) 0.052(3) -0.020(2) -0.002(3) -0.004(3)

N4 0.043(2) 0.054(2) 0.046(2) -0.001(2) -0.005(2) -0.0032(19)  
 N11 0.066(3) 0.046(2) 0.051(3) -0.009(2) 0.008(3) -0.002(2)  
 N21 0.050(3) 0.047(2) 0.066(3) 0.000(2) -0.007(3) -0.004(2)  
 N31 0.046(3) 0.056(3) 0.050(3) -0.002(2) 0.001(2) 0.005(2)  
 N41 0.057(3) 0.049(3) 0.057(3) -0.010(2) 0.006(2) -0.004(2)  
 C1 0.064(4) 0.085(5) 0.052(4) -0.012(3) 0.009(3) -0.002(4)  
 C2 0.048(4) 0.057(3) 0.047(3) -0.010(2) -0.009(2) 0.008(3)  
 C3 0.053(5) 0.051(3) 0.056(3) -0.009(2) -0.007(3) 0.002(3)  
 C4 0.083(5) 0.053(3) 0.086(5) -0.015(3) 0.001(4) -0.008(3)  
 N5 0.097(4) 0.051(3) 0.095(4) 0.006(3) -0.004(4) -0.018(3)  
 C6 0.070(5) 0.068(4) 0.075(4) 0.010(4) 0.006(4) -0.013(4)  
 C7 0.066(4) 0.054(3) 0.063(4) 0.001(3) 0.004(4) -0.007(3)  
 C12 0.075(5) 0.058(3) 0.062(4) -0.008(3) 0.014(3) -0.003(4)  
 C13 0.091(6) 0.082(5) 0.076(5) -0.007(4) 0.026(5) -0.009(4)  
 C14 0.105(7) 0.123(6) 0.049(4) -0.011(5) 0.020(4) -0.019(6)  
 C15 0.104(8) 0.117(6) 0.052(4) -0.005(3) -0.016(5) -0.022(6)  
 C16 0.084(6) 0.056(3) 0.053(3) -0.006(3) -0.010(3) -0.017(3)  
 C22 0.055(5) 0.069(4) 0.109(6) -0.014(4) -0.014(4) 0.008(4)  
 C23 0.063(5) 0.090(6) 0.145(9) -0.007(6) -0.027(6) 0.020(5)  
 C24 0.082(7) 0.086(6) 0.130(8) 0.030(6) -0.058(7) 0.000(6)  
 C25 0.073(6) 0.092(6) 0.091(5) 0.010(5) -0.025(5) -0.008(5)  
 C26 0.073(5) 0.056(4) 0.065(4) -0.003(3) -0.016(4) -0.007(3)  
 C32 0.051(4) 0.076(4) 0.072(4) -0.007(4) -0.005(3) -0.010(4)  
 C33 0.046(4) 0.105(6) 0.095(5) 0.002(4) -0.012(4) 0.002(4)  
 C34 0.062(5) 0.122(6) 0.086(5) 0.021(5) -0.017(4) 0.018(5)  
 C35 0.081(6) 0.085(5) 0.084(5) 0.021(4) -0.005(4) 0.021(5)  
 C36 0.061(4) 0.055(3) 0.052(3) 0.001(3) 0.011(3) 0.003(3)  
 C42 0.064(4) 0.061(4) 0.092(5) -0.010(4) -0.010(4) -0.017(3)  
 C43 0.087(6) 0.075(5) 0.134(7) -0.003(5) 0.000(6) -0.023(5)  
 C44 0.118(8) 0.071(5) 0.130(8) 0.021(5) 0.008(6) -0.025(5)  
 C45 0.098(5) 0.077(4) 0.092(4) 0.019(3) 0.003(8) -0.016(7)  
 C46 0.066(6) 0.051(3) 0.055(3) -0.001(3) 0.008(3) 0.005(3)  
 O1W 0.164(13) 0.108(9) 0.163(12) -0.066(8) 0.000 0.000  
 P1A 0.06(3) 0.055(19) 0.18(3) 0.019(16) 0.07(3) -0.01(2)  
 F11A 0.17(3) 0.10(2) 0.17(3) -0.03(2) 0.04(2) 0.05(2)  
 F12A 0.096(12) 0.116(18) 0.148(15) 0.029(17) -0.014(12) -0.046(11)  
 F13A 0.15(2) 0.070(9) 0.087(11) 0.003(7) -0.041(15) 0.009(11)  
 P1B 0.096(12) 0.098(10) 0.045(4) 0.011(4) -0.015(17) -0.03(2)  
 F11B 0.188(13) 0.142(12) 0.052(6) 0.009(6) -0.020(7) -0.050(9)  
 F12B 0.240(19) 0.115(10) 0.142(11) 0.018(7) 0.066(12) -0.058(12)  
 F13B 0.118(9) 0.196(13) 0.131(8) -0.001(10) -0.009(8) 0.055(7)  
 P2A 0.090(7) 0.106(6) 0.108(7) -0.022(5) 0.036(5) -0.005(5)  
 F21A 0.110(11) 0.187(13) 0.127(11) -0.023(10) 0.008(9) -0.059(10)  
 F22A 0.26(3) 0.095(11) 0.31(3) 0.039(17) 0.09(3) 0.040(15)  
 F23A 0.117(12) 0.27(3) 0.091(10) 0.022(14) 0.031(8) 0.021(17)  
 F24A 0.169(15) 0.125(10) 0.180(15) -0.039(10) 0.026(12) 0.024(10)  
 F25A 0.132(12) 0.195(18) 0.111(10) 0.010(10) 0.049(9) 0.029(11)  
 F26A 0.072(10) 0.27(3) 0.24(2) -0.01(2) 0.012(10) -0.033(14)  
 P2B 0.089(8) 0.136(10) 0.104(7) 0.006(6) 0.031(5) 0.002(6)  
 F21B 0.109(18) 0.36(4) 0.16(2) 0.00(2) 0.048(14) 0.07(2)  
 F22B 0.158(16) 0.21(2) 0.103(10) -0.060(13) 0.027(9) -0.063(16)  
 F23B 0.168(16) 0.151(13) 0.123(12) 0.014(10) 0.044(10) -0.063(12)  
 F24B 0.34(4) 0.122(13) 0.19(2) -0.085(14) 0.03(2) 0.006(17)  
 F25B 0.20(2) 0.139(14) 0.151(18) 0.038(14) 0.054(19) -0.001(14)  
 F26B 0.108(11) 0.158(13) 0.105(9) -0.011(9) 0.014(7) 0.001(11)

\_geom\_special\_details

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles

and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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Ru1 N4 2.071(4) . ?
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N4 C3 1.365(6) . ?
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N11 C16 1.380(7) . ?
N21 C22 1.329(8) . ?
N21 C26 1.344(8) . ?
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N31 C36 1.371(7) . ?
N41 C42 1.334(7) . ?
N41 C46 1.348(7) . ?
C1 H1 0.9300 . ?
C2 C3 1.441(7) . ?
C3 C4 1.388(7) . ?
C4 N5 1.299(8) . ?
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C6 C7 1.368(8) . ?
C6 H6 0.9300 . ?
C7 H7 0.9300 . ?
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C12 H12 0.9300 . ?
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C13 H13 0.9300 . ?
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C14 H14 0.9300 . ?
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C23 H23 0.9300 . ?
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C24 H24 0.9300 . ?
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C25 H25 0.9300 . ?
C32 C33 1.370(9) . ?
C32 H32 0.9300 . ?
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C33 H33 0.9300 . ?  
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C34 H34 0.9300 . ?  
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C35 H35 0.9300 . ?  
C36 C46 1.472(8) . ?  
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C42 H42 0.9300 . ?  
C43 C44 1.353(11) . ?  
C43 H43 0.9300 . ?  
C44 C45 1.394(14) . ?  
C44 H44 0.9300 . ?  
C45 C46 1.395(8) . ?  
C45 H45 0.9300 . ?  
O1W H1W1 0.846(3) . ?  
O1W H1W2 0.859(12) . ?  
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P1A F12A 1.49(3) . ?  
P1A F11A 1.49(3) . ?  
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P1B F12B 1.58(2) . ?  
P1B F13B 1.584(18) . ?  
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P2A F22A 1.541(14) . ?  
P2A F24A 1.543(14) . ?  
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P2A F21A 1.554(14) . ?  
P2A F25A 1.575(14) . ?  
P2B F24B 1.521(15) . ?  
P2B F26B 1.541(15) . ?  
P2B F22B 1.546(15) . ?  
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C13 C14 H14 119.8 . . ?  
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C15 C16 C26 123.4(7) . . ?  
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F13A P1A F12A 89.8(15) . . ?  
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F11B P1B F12B 90.6(13) . . ?  
F11B P1B F13B 91.0(12) . . ?  
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Ru1 N1 N2 C1 -178.1(4) . . . . ?  
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N21 Ru1 N31 C32 146(3) . . . . ?  
N11 Ru1 N31 C32 85.0(5) . . . . ?  
N41 Ru1 N31 C32 178.1(5) . . . . ?  
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Ru1 N1 C2 N3 178.3(3) . . . . ?  
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Ru1 N1 C2 C3 1.1(6) . . . . ?  
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C1 N3 C2 C3 176.8(6) . . . . ?  
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C7 N4 C3 C2 -179.8(5) . . . . ?  
Ru1 N4 C3 C2 -0.7(6) . . . . ?  
N1 C2 C3 N4 -0.3(7) . . . . ?  
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N5 C6 C7 N4 -1.6(11) . . . . ?  
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C12 N11 C16 C26 -179.0(5) . . . . ?  
Ru1 N11 C16 C26 -1.0(6) . . . . ?  
C14 C15 C16 N11 -1.2(10) . . . . ?  
C14 C15 C16 C26 179.9(7) . . . . ?

C26 N21 C22 C23 0.0(10) . . . . ?  
 Ru1 N21 C22 C23 173.8(5) . . . . ?  
 N21 C22 C23 C24 -2.3(12) . . . . ?  
 C22 C23 C24 C25 3.7(14) . . . . ?  
 C23 C24 C25 C26 -2.8(14) . . . . ?  
 C22 N21 C26 C25 1.0(9) . . . . ?  
 Ru1 N21 C26 C25 -173.3(5) . . . . ?  
 C22 N21 C26 C16 -179.8(6) . . . . ?  
 Ru1 N21 C26 C16 6.0(7) . . . . ?  
 C24 C25 C26 N21 0.4(12) . . . . ?  
 C24 C25 C26 C16 -178.7(7) . . . . ?  
 N11 C16 C26 N21 -3.2(8) . . . . ?  
 C15 C16 C26 N21 175.7(6) . . . . ?  
 N11 C16 C26 C25 176.0(6) . . . . ?  
 C15 C16 C26 C25 -5.1(11) . . . . ?  
 C36 N31 C32 C33 0.6(9) . . . . ?  
 Ru1 N31 C32 C33 173.8(5) . . . . ?  
 N31 C32 C33 C34 -1.0(11) . . . . ?  
 C32 C33 C34 C35 1.3(11) . . . . ?  
 C33 C34 C35 C36 -1.3(11) . . . . ?  
 C32 N31 C36 C35 -0.6(8) . . . . ?  
 Ru1 N31 C36 C35 -174.6(5) . . . . ?  
 C32 N31 C36 C46 179.0(5) . . . . ?  
 Ru1 N31 C36 C46 5.0(6) . . . . ?  
 C34 C35 C36 N31 1.0(10) . . . . ?  
 C34 C35 C36 C46 -178.6(6) . . . . ?  
 C46 N41 C42 C43 3.5(9) . . . . ?  
 Ru1 N41 C42 C43 -168.4(5) . . . . ?  
 N41 C42 C43 C44 -0.7(12) . . . . ?  
 C42 C43 C44 C45 -0.9(14) . . . . ?  
 C43 C44 C45 C46 -0.2(13) . . . . ?  
 C42 N41 C46 C45 -4.6(9) . . . . ?  
 Ru1 N41 C46 C45 168.2(5) . . . . ?  
 C42 N41 C46 C36 175.1(5) . . . . ?  
 Ru1 N41 C46 C36 -12.1(6) . . . . ?  
 C44 C45 C46 N41 3.0(10) . . . . ?  
 C44 C45 C46 C36 -176.7(7) . . . . ?  
 N31 C36 C46 N41 4.9(7) . . . . ?  
 C35 C36 C46 N41 -175.6(6) . . . . ?  
 N31 C36 C46 C45 -175.4(6) . . . . ?  
 C35 C36 C46 C45 4.1(10) . . . . ?

\_diffn\_measured\_fraction\_theta\_max 1.00  
 \_diffn\_reflns\_theta\_full 27.14  
 \_diffn\_measured\_fraction\_theta\_full 1.00  
 \_refine\_diff\_density\_max 0.30  
 \_refine\_diff\_density\_min -0.37  
 \_refine\_diff\_density\_rms 0.06