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SUPRA-CONSERVATIVE FINITE-VOLUME METHODS FOR THE EULER EQUATIONS OF SUBSONIC COMPRESSIBLE FLOW

ARTHUR E. P. VELDMAN*

Abstract. It has been found advantageous for finite-volume discretizations of flow equations to possess additional (secondary) invariants, next to the (primary) invariants from the constituting conservation laws. The paper presents general (necessary and sufficient) requirements for a method to convectively preserve discrete kinetic energy. The key ingredient is a close discrete consistency between the convective term in the momentum equation and the terms in the other conservation equations (mass, internal energy). As examples, the Euler equations for subsonic (in)compressible flow are discretized with such supra-conservative finite-volume methods on structured as well as unstructured grids.

Key words. CFD, conservation laws, finite-volume method, supra-conservative discretization

AMS subject classifications. 65M08, 65M12, 76G25

1. Introduction.

1.1. Background. The equations describing fluid dynamics can be expressed as conservation laws in terms of primary variables: mass, momentum and (internal) energy. In the absence of dissipative mechanisms, according to Noether's theorem [5,80], they possess a number of invariants induced by the symmetries of the Hamiltonian/Lagrangian structure. Next to the (obvious) primary invariants expressed by the explicit conservation laws, other secondary invariants exist [21, 86, 116]. Preserving (globally and/or locally) one or more of these analytical invariants in a discrete setting has proven quite useful over the years, but is not obvious to realize, e.g. [91]. Gradually, experience is built up about which additional discrete invariants are worthwhile to preserve, and about the way to achieve this. In this paper, we analyze the steps that can lead to simultaneous discrete conservation of several of these (primary and secondary) invariants.

In particular, we consider the Euler equations for subsonic (in)compressible flow. These will be formulated as conservation laws in terms of the primary variables mass density ρ , momentum per unit mass \mathbf{u} , and internal energy per unit mass e :

$$(1.1a) \quad \frac{\partial \rho}{\partial t} + \nabla \cdot \mathbf{m} = 0;$$

$$(1.1b) \quad \frac{\partial \rho \mathbf{u}}{\partial t} + \nabla \cdot (\mathbf{m} \otimes \mathbf{u}) = -\nabla p;$$

$$(1.1c) \quad \frac{\partial \rho e}{\partial t} + \nabla \cdot (\mathbf{m} e) = -p \nabla \cdot \mathbf{u}.$$

Here, $\mathbf{m} \equiv \rho \mathbf{u}$ denotes the mass flux and p the pressure. The set of equations is closed by an equation of state which relates p , ρ and e (for the limit of incompressible flow, see Appendix A).

The introduction of the mass flux \mathbf{m} will help to distinguish between the two appearances of \mathbf{u} in the momentum equation: one as transporting velocity, the other as transported quantity. We will also see that the particular value of \mathbf{m} is relevant only at two places in the analysis: in the derivation of the pressure Poisson equation

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(Sect. 4.2) and in the limit between compressible and incompressible flow (Sect. 5.3). All other considerations in this paper hold for *any* vector field \mathbf{m} . Note that the time derivative in (1.1b) contains the product of the density ρ and the velocity \mathbf{u} (together making the momentum per unit volume), and not the mass flux \mathbf{m} (which nevertheless has the same value). The mathematical reason behind this will become clear in the sequel, when studying the evolution of kinetic energy (see also [132, Sect. 7]).

The equations are solved on a (two- or three-dimensional) domain Ω with appropriate initial and boundary conditions. For convenience, we will assume either homogeneous boundary conditions or periodic ones, such that we do not have to bother with terms along the boundaries. Physically, this means that in this paper external influences on the flow field are excluded.

The equations (1.1) have been written in conservation form, immediately revealing the primary invariants. As main invariants, next to mass and linear momentum, also angular momentum, mean kinetic energy, helicity and circulation (Kelvin) are (globally) preserved [72, 75, 86]. Furthermore, in two dimensions, enstrophy and other integrals of the vorticity are invariant. In [2, 21, 25, 116] methods are presented to construct even more invariants.

The convection term in the momentum equation (1.1b) can be written in various formulations. For incompressible flow, next to the conservative form $\nabla(\mathbf{u} \otimes \mathbf{u})$, one has the convective form $\mathbf{u} \cdot \nabla \mathbf{u}$, the skew-symmetric form $\frac{1}{2} \mathbf{u} \cdot \nabla \mathbf{u} + \frac{1}{2} \nabla \cdot (\mathbf{u} \otimes \mathbf{u})$, the rotational form $(\nabla \times \mathbf{u}) \times \mathbf{u} + \frac{1}{2} \nabla(\mathbf{u} \cdot \mathbf{u})$, the closely related velocity-vorticity(-helicity) formulations [51, 82, 83] and the streamfunction-vorticity formulation [3]. For compressible flow, with even more freedom in formulating the equations, Coppola et al. [27, 28] have analyzed a large family of variants.

Analytically all formulations are equivalent, because of the equation for mass conservation (1.1a), and they possess the same invariants. But after discretization this equivalence is partly lost, and differences appear in the induced discrete invariants. Depending upon the desired discrete invariant, e.g. kinetic energy or helicity, a different analytical formulation can be chosen as a starting point. The present paper intends to study how this loss of discrete equivalence can be reduced. In particular it is shown how discrete energy can be conserved, as this property directly improves numerical stability; for incompressible flow stability is even guaranteed. Recently, Edoh et al. [34] have shown in detail how other means of achieving numerical stability, such as artificial dissipation and solution-filtering, result in (nonphysical) inaccuracies of the numerical solution.

1.2. History - incompressible flow. Around 1960, in long-time numerical weather prediction [3, 13, 67, 94, 95], the (possibly negative) influence of the discretization of the non-linear convective term on numerical stability (in those days coined non-linear instability) was already discussed. In particular, Arakawa [3], working in 2D, advocated the use of the streamfunction-vorticity formulation of the flow equations, which he shows to discretely conserve mean kinetic energy and enstrophy.

Building on the staggered-grid formulation by Harlow and Welch [50], Piacsek and Williams [96] promoted the discretization of the skew-symmetric convective formulation, as it directly leads to discrete global energy conservation and its numerical stability. Several years later, Horiuti [54] and Zang [152] were among the first to systematically explore the rotational form of the equations. Later, Perot et al. [90, 153] stressed how on unstructured grids using the rotational form, next to global conservation of kinetic energy and circulation, also local conservation can be achieved.

89 *Finite-element methods.* In search for more ‘useful’ secondary invariants, in a
 90 finite-element setting Layton et al. [63] compared several formulations of the equa-
 91 tions, but they did not include the conservation form (1.1) which is our starting
 92 point. As a follow-up, Rebholz and colleagues [23, 24, 29] further extended the quest
 93 for finite-element methods with enhanced conservation properties, again motivated
 94 by accurate long-time integration [8]. Also, Lehmkuhl et al. [65] advocate the use of
 95 low-dissipative and conservative finite-element schemes. In general, the geometrical
 96 flexibility of a finite-element discretization can be combined with the conservation
 97 properties of a finite-volume formulation. This led to a number of closely-related
 98 methods [6, 148], like the discontinuous Galerkin method [26], the spectral volume
 99 method [125, 126] and the energy-stable flux reconstruction method [20, 55, 147, 149].

100 *Mimetic methods.* Inspired by the work of Samarskii in the 1970s, the support oper-
 101 ator method was developed in which basic analytical relations between the main oper-
 102 ators of calculus (div, grad and curl) were preserved [111, 118]. Later, this approach
 103 was renamed by Hyman and Shashkov [56] as a mimetic finite-difference method. A
 104 broad overview of these methods is given by Lipnikov et al. [68]. Links with differen-
 105 tial geometry and algebraic topology were made in the language of discrete exterior
 106 calculus, e.g. [11, 19, 31, 35, 52]. Note that in the latter language the mass flux \mathbf{m} is a
 107 2-form, whereas the velocity \mathbf{u} is a 1-form, again making the distinction between \mathbf{m}
 108 and $\rho\mathbf{u}$. Explanations for non-specialists of this, highly mathematical, approach can
 109 be found in [36, 93]. These methods have been applied mainly in diffusion-dominated
 110 flow problems, see the overview paper by Perot [92], but a few convection-dominated
 111 studies can be mentioned [30, 45, 76].

112 *Finite-difference methods.* An extensive overview of finite-difference options for
 113 the incompressible flow equations has been presented by Morinishi [78]. He discusses
 114 the discretization of the convective, divergence and skew-symmetric forms on uniform
 115 grids. A generalization of his approach to non-uniform grids was presented by Vasilyev
 116 [139] and Ham et al. [49]. As a curvilinear case, the energy-preserving formulation
 117 in cylindrical coordinates was studied in [40, 79, 87]; a more general approach for
 118 structured curvilinear staggered grids has been proposed in [138]. Discrete skew-
 119 symmetry of the convective terms also features in the summation-by-parts (SBP)
 120 method introduced by Strand [123] and Olsson [84, 85], and generalized in [74, 81,
 121 127, 128]. Next to these approaches to globally preserve discrete energy, also ideas to
 122 preserve helicity [69, 100, 116] and angular momentum [44] have been proposed.

123 *Finite-volume methods.* Around the same time, similar considerations for finite-
 124 volume discretizations were discussed. Starting from the conservation laws behind
 125 the equations given in Eq. (1.1), conservation of the primary variables is ‘automatic’
 126 in this approach. In the 1990s, inspired by [143], by means of a symmetry-preserving
 127 approach Verstappen and Veldman [144] were among the first to combine discrete
 128 mass, momentum and energy conservation for incompressible flow on non-uniform,
 129 staggered Cartesian grids. They emphasized the need for, counter-intuitive, geometry-
 130 independent interpolations for the fluxes. Higher-order finite-volume versions followed
 131 soon [145, 146, 150]. Early generalizations to unstructured staggered grids have been
 132 presented by Perot et al. [90, 153]. Later, Trias et al. included collocated grids [60,
 133 115, 133, 134].

134 **1.3. History - compressible flow.** Extensions to the equations for compress-
 135 ible flow have also been presented. Often, but not always, starting from the conserva-
 136 tive formulation and discretized with a finite-volume approach. Also here, early use
 137 of skew-symmetric forms can be mentioned, such as the formulations by Feiereisen

138 et al. [37], Tadmor [130] and Blaisdell et al. [9]. These, non-conservative, analytical
 139 forms are better combined with a finite-difference discretization, although some of
 140 them can be recast into a finite-volume discretization [28, 49]. Consistency between
 141 the individual discrete equations was found beneficial for stability [14, 18, 70, 97, 99].
 142 Even as early as 1967, Richtmyer and Morton [103, p. 142] in their study of the Burg-
 143 ers equation already noticed that some discretizations conserve an energy norm “thus
 144 ensuring stability”.

145 The use of entropy variables can be profitable, see e.g. [15, 22, 43, 53, 89, 113,
 146 129, 151], but often discrete momentum conservation is lost. The latter papers were
 147 mainly concerned with the numerical treatment of shock wave discontinuities, where
 148 monotonicity and TVD properties are relevant (e.g. [7, 98]). In contrast, and com-
 149 plementary, our interest is in the treatment of the relatively smooth (but possibly
 150 turbulent) part of the flow; hence our restriction to subsonic flow. Yet, due to the
 151 absence of numerical diffusion, our approach will not interfere with the, necessarily,
 152 dissipative character of numerical shock treatment.

153 In this paper, we would like to retain all primary conservation properties and to
 154 extend them with additional secondary conservation. Some finite-volume studies in
 155 this vein can be mentioned already, e.g. those by Ducros et al. [33], Jameson [58],
 156 Kok [62], Morinishi [77] and Rozema [108]. We will highlight the general principles
 157 behind these spatial discretization methods.

158 *Time integration.* Finally, after the above summary of spatial discretization de-
 159 velopments, we should mention the efforts to let the time integration preserve in-
 160 variants. In particular, symplectic methods [114], like the implicit midpoint rule,
 161 preserve kinetic energy. Such methods for incompressible flow have been studied,
 162 e.g., by Sanderse [112] and Capuano et al. [16]; thusfar, only implicit methods with
 163 these conservation properties have been found. It appears that energy-preserving time
 164 integration for compressible flow requires the introduction of the square root of the
 165 density $\sqrt{\rho}$ [46, 77, 108, 124]. Following the use of these ‘square-root variables’ in the
 166 time-integration method, spatial discretization studies were carried out based on the
 167 same variables; see e.g. Reiss et al. [12, 101, 102], Rozema et al. [105, 107, 110] and
 168 Cadieux et al. [15]. In particular, Rozema’s square-root formulation can preserve not
 169 only primary (mass, momentum and internal energy) and secondary (kinetic and to-
 170 tal energy) invariants through spatial and temporal discretization, but it additionally
 171 allows for a compressible formulation of regularization turbulence models [108, 109].
 172 A wider overview of energy-preserving time-integration methods for compressible flow
 173 can be found in [27].

174 *Similar ideas in adjacent areas.* Next to the above developments in the realm of
 175 discrete-grid methods, similar energy-preserving ideas have been proposed for other
 176 discretization paradigms like spectral methods [10, 42, 88] and SPH methods [39].
 177 Moreover, other application areas can be mentioned where energy conservation and
 178 similar properties are advantageous, like geophysical fluid dynamics [4, 32, 131] and
 179 multi-phase flow [41, 57, 135, 140]. The literature shows that preserving these desir-
 180 able conservation properties usually goes at the expense of mass and/or momentum
 181 conservation. Also for the shallow-water equations discrete energy conservation is
 182 actively pursued [119, 121, 136], sometimes in conjunction with one other discrete in-
 183 variant, e.g. enstrophy [120, 122]. Only a few exceptions with more than one discretely
 184 conserved invariant, viz. mass and momentum, have been presented [137, 138].

185 **1.4. Supra-conservative discretization.** The general idea behind many of the
 186 above methods is that they want to discretely conserve *more* (secondary) invariants

187 then just the (primary) ones directly featuring in the conservation laws. Therefore,
 188 these methods are coined *supra-conservative* [142]. To achieve this property requires
 189 sufficient compatibility between the discrete operators in the equations of motion:
 190 not only div, grad and curl, but also composite operators. Below, we will discuss the
 191 details of such a discrete compatibility for (stretched) structured and unstructured
 192 computational grids with staggered as well as collocated positioning of the unknowns.

193 Most of the above studies have been based on the properties of the analytical
 194 formulations, which are then ‘hopefully’ retained after discretization. In our discussion
 195 we will start, as advocated in [141], from the discrete finite-volume formulation of the
 196 basic equations (1.1), and never return to the analytical formulation. In this way we
 197 make sure that discrete conservation of the primary invariants is guaranteed from the
 198 start. Then, at the discrete level, the freedom left in the formulation will be used to
 199 generate additional properties like secondary invariants.

200 *Outline.* In the paper we focus in particular on the (secondary) conservation of energy
 201 in finite-volume methods. Necessary and sufficient criteria hereto will be derived.
 202 We restrict ourselves to subsonic flow (i.e. no shock waves) and stick to the conserva-
 203 tive formulation in primitive variables. In Sections 2 and 3 the derivation steps are
 204 discussed that are required to obtain energy conservation, first in the analytic case,
 205 thereafter mimicked in the discrete setting. Section 4 works out a supra-conservative
 206 method for incompressible flow discretized on a structured, staggered grid. In Sec-
 207 tion 5 the approach is generalized to compressible flow on an unstructured, collocated
 208 grid. Finally, the common line in the approach will be discussed in Section 6, followed
 209 by a section with conclusions.

210 **2. Conservation of energy - analytic.** The theoretical study of the invariants
 211 of the Euler flow equations thus far has mainly focused on the incompressible special
 212 case of the formulation as given in (1.1); here we treat the general case of compressible
 213 flow. As the flow equations are formulated in conservation form they ‘automatically’
 214 conserve mass, momentum and internal energy. Analysis shows that, as mentioned
 215 above, they additionally convectively preserve kinetic energy and total energy. The
 216 analytic derivation of this property is relevant for the discrete discussion in the sequel.
 217 We give it here as a starting point and guide line, as we want to mimic it step-by-step
 218 in the discretization.

$$\begin{aligned}
 219 \quad \frac{\partial}{\partial t}(\rho E_{\text{tot}}) &= - \underbrace{\frac{1}{2}(\mathbf{u} \cdot \mathbf{u}) \frac{\partial}{\partial t} \rho}_{\text{mass (1.1a)}} + \underbrace{\mathbf{u} \cdot \frac{\partial}{\partial t}(\rho \mathbf{u})}_{\text{momentum (1.1b)}} + \underbrace{\frac{\partial}{\partial t}(\rho e)}_{\text{internal energy (1.1c)}} \\
 220 \quad (2.1a) \quad &= \frac{1}{2}(\mathbf{u} \cdot \mathbf{u}) \nabla \cdot \mathbf{m} - \mathbf{u} \cdot \left\{ \nabla \cdot (\mathbf{m} \otimes \mathbf{u}) + \nabla p \right\} - \left\{ \nabla \cdot (\mathbf{m} e) + p \nabla \cdot \mathbf{u} \right\} \\
 221 \quad (2.1b) \quad &= \mathbf{u} \cdot \left\{ \frac{1}{2}(\nabla \cdot \mathbf{m}) \mathbf{u} - \nabla \cdot (\mathbf{m} \otimes \mathbf{u}) \right\} - \nabla \cdot (\mathbf{m} e) - \left\{ \mathbf{u} \cdot \nabla p + p \nabla \cdot \mathbf{u} \right\} \\
 &\quad \underbrace{\hspace{10em}}_{\text{Property 2.1}} \hspace{10em} \underbrace{\hspace{10em}}_{\text{Property 2.2}} \\
 222 \quad (2.1c) \quad &= \underbrace{- \nabla \cdot \left(\frac{1}{2} \mathbf{m} \mathbf{u}^2 \right) - \nabla \cdot (\mathbf{m} e)}_{\text{Property 2.3}} - \nabla \cdot (\mathbf{p} \mathbf{u}) \\
 223 \quad (2.1d) \quad &= - \nabla \cdot (\mathbf{m} E_{\text{tot}}) - \nabla \cdot (\mathbf{p} \mathbf{u}).
 \end{aligned}$$

225

226 From the primary conservation laws one can deduce secondary conservation laws
 227 for kinetic energy $\rho E_{\text{kin}} \equiv \frac{1}{2} \rho \mathbf{u}^2$ and total energy $\rho E_{\text{tot}} \equiv \rho(E_{\text{kin}} + e)$. The evolution

228 of the total energy can be calculated analytically as a weighted combination of the
 229 primary conservation laws (1.1a), (1.1b) and (1.1c). Equation (2.1) schematically
 230 shows how the derivation of the energy evolution proceeds. The divergence forms in
 231 the last two lines (2.1c) and (2.1d) not only induce global energy conservation but
 232 also local conservation. It is stressed that this derivation holds for *any* \mathbf{m} : its explicit
 233 value $\rho\mathbf{u}$ is not used.

234 The derivation in (2.1) reveals, by means of a background shading, how terms
 235 from the separate primary conservation laws have to be combined, requiring a certain
 236 level of compatibility. Analytically this is not an issue, but in a discrete setting it is
 237 not straightforward, and this will be the focal point in the presentation to follow.

238 In the last two steps, from (2.1b) to (2.1c) and from (2.1c) to (2.1d), three analytic
 239 properties between the operators are essential (although trivial at first sight). We will
 240 discuss these steps in detail, making a distinction between the various appearances of
 241 the ∇ -operator. Hereto, hopefully self-explaining, subscripts have been added to the
 242 operators to indicate in which conservation law they are featuring.

243 **PROPERTY 2.1 ((2.1b)→(2.1c)).** *The convection operator for momentum conser-*
 244 *vation $\nabla_{\text{mom_conv}}$ together with the divergence operator of mass conservation ∇_{mass}*
 245 *form a convective divergence expression with operator $\nabla_{\text{toten_conv}}$. This requires that*
 246 *(for any \mathbf{m}) the operator*

$$247 \quad (2.2) \quad \mathcal{A} : \mathbf{u} \rightarrow \nabla_{\text{mom_conv}} \cdot (\mathbf{m} \otimes \mathbf{u}) - \frac{1}{2}(\nabla_{\text{mass_div}} \cdot \mathbf{m})\mathbf{u} \text{ is skew symmetric.}$$

248 *Explanation.* First, let the L_2 -inner product for real-valued functions be defined
 249 through $((\phi, \psi)) \equiv \int_{\Omega} \phi\psi \, d\Omega$. Then, if an expression $\phi\mathcal{A}\phi$ can be rewritten as $\phi\mathcal{A}\phi \equiv$
 250 $\nabla\mathcal{B}(\phi)$ for some function \mathcal{B} , then (for all real-valued ϕ) $((\phi, \mathcal{A}\phi)) = \int_{\Omega} \phi\mathcal{A}\phi \, d\Omega =$
 251 $\int_{\Omega} \nabla\mathcal{B}(\phi) \, d\Omega = 0$ because of Gauss' theorem and our assumption that the outer
 252 boundaries of Ω do not contribute. That means that \mathcal{A} is skew-symmetric with respect
 253 to this L_2 -inner product. Indeed, we can rewrite (for any \mathbf{m} and ϕ) $\nabla \cdot (\mathbf{m}\phi) - \frac{1}{2}(\nabla \cdot$
 254 $\mathbf{m})\phi \equiv \frac{1}{2}\nabla \cdot (\mathbf{m}\phi) + \frac{1}{2}(\mathbf{m} \cdot \nabla)\phi$, which reveals the skew-symmetry as an operator
 255 acting on ϕ . \square

256 **PROPERTY 2.2 ((2.1b)→(2.1c)).** *The gradient operator $\nabla_{\text{mom_grad}}$ acting on the*
 257 *pressure is the negative transpose, with respect to the L_2 -inner product, of the diver-*
 258 *gence operator $\nabla_{\text{inten_div}}$ in the dilatation term of the internal energy equation:*

$$259 \quad (2.3) \quad ((\mathbf{u}, \nabla_{\text{mom_grad}} p)) = -((\nabla_{\text{inten_div}} \cdot \mathbf{u}, p)) \text{ for all } \mathbf{u} \text{ and } p.$$

260 In short hand, this property can be written as

$$261 \quad (2.4) \quad \nabla_{\text{mom_grad}} = -\nabla_{\text{inten_div}}^T (= -\nabla_{\text{mass}}^T).$$

262 Between parentheses the incompressible limit is given, when the conservation law for
 263 internal energy degenerates into the continuity equation [47, 61]; see also Appendix
 264 A.

265 **PROPERTY 2.3 ((2.1c)→(2.1d)).** *The divergence operator $\nabla_{\text{inten_conv}}$ in the con-*
 266 *vective term of the internal energy equation is the same as the divergence operator*
 267 *$\nabla_{\text{mom_conv}}$ from Property 2.1 in the momentum equation:*

$$268 \quad \nabla_{\text{inten_conv}} = \nabla_{\text{mom_conv}} \quad (\equiv \nabla_{\text{toten_conv}}).$$

269 This property allows to combine both convective terms into one term describing con-
 270 vection of total energy.

271 The above properties reveal that there is a close relation between the operators
 272 from the individual conservation laws. It is our intention to transfer these analytic
 273 properties towards the discrete setting. This will then give guide lines for the design
 274 of the supra-conservative discretization schemes.

275 **3. Conservation of energy - discrete.** The discretization will be carried out
 276 with finite-volume methods. Therefore, first the governing equations are reformulated
 277 as conservation laws (for an arbitrary control volume Ω_h with boundary Γ_h):

$$278 \quad (3.1a) \quad \int_{\Omega_h} \frac{\partial \rho}{\partial t} d\Omega_h + \int_{\Gamma_h} \mathbf{m} \cdot \mathbf{n} d\Gamma_h = 0,$$

$$279 \quad (3.1b) \quad \int_{\Omega_h} \frac{\partial \rho \mathbf{u}}{\partial t} d\Omega_h + \int_{\Gamma_h} (\mathbf{m} \cdot \mathbf{n}) \mathbf{u} d\Gamma_h = - \int_{\Gamma_h} p \mathbf{n} d\Gamma_h,$$

$$280 \quad (3.1c) \quad \int_{\Omega_h} \frac{\partial \rho e}{\partial t} d\Omega_h + \int_{\Gamma_h} (\mathbf{m} \cdot \mathbf{n}) e d\Gamma_h = - \int_{\Omega_h} p \nabla \cdot \mathbf{u} d\Omega_h.$$

282 Note that Ω_h is a generic notation for a control volume. For a collocated grid these will
 283 be the same for each conserved variable, while on a staggered grid for the individual
 284 variables different control volumes are usually pertinent.

285 The discretized versions of (3.1a)-(3.1c) in all grid volumes will be collected in
 286 matrix-vector notation and abbreviated as

$$287 \quad (3.2a) \quad \mathfrak{H} \frac{\partial \rho}{\partial t} + \mathfrak{D}_{\text{mass}} \mathbf{m} = 0,$$

$$288 \quad (3.2b) \quad \mathfrak{H} \frac{\partial \rho \mathbf{u}}{\partial t} + \mathfrak{C}_{\text{mom}}^{\mathbf{m}} \mathbf{u} = -\mathfrak{G}_{\text{mom}} p,$$

$$289 \quad (3.2c) \quad \mathfrak{H} \frac{\partial \rho e}{\partial t} + \mathfrak{C}_{\text{inten}}^{\mathbf{m}} e = -p \mathfrak{D}_{\text{inten}} \mathbf{u}.$$

291 Here \mathfrak{H} denotes a diagonal matrix operator containing the sizes of the control volumes
 292 Ω_h . The dependent variables are now discrete (vector) grid functions, but we will
 293 use the same (lower case) symbols as in the continuous case. The **Fraktur**-font operators
 294 denote *volume-consistent* [18, 71, 142] discrete approximations of the continuous
 295 differential operators, with subscripts to identify in which equation they are being
 296 used:

- 297 – $\mathfrak{D}_{\text{mass}}$ is a discrete divergence matrix operator acting on the mass flux vector \mathbf{m}
 298 in (3.1a). With the grid vector $\mathfrak{D}_{\text{mass}} \mathbf{m}$, a diagonal grid matrix $\text{diag}(\mathfrak{D}_{\text{mass}} \mathbf{m})$
 299 can be formed.
- 300 – $\mathfrak{C}_{\text{mom}}^{\mathbf{m}}$ is a discrete grid operator, acting on \mathbf{u} , for the convective term in the
 301 momentum equation (3.1b). Its coefficients depend on the mass flux \mathbf{m} .
- 302 – $\mathfrak{G}_{\text{mom}}$ is a discrete gradient operator in (3.1b) acting on the pressure p .
- 303 – $\mathfrak{C}_{\text{inten}}^{\mathbf{m}}$ is a discrete grid operator, acting on e and dependent on \mathbf{m} , for the
 304 convective term in the conservation law for internal energy (3.1c).
- 305 – $\mathfrak{D}_{\text{inten}}$ is a discrete divergence operator acting on the velocity \mathbf{u} in (3.1c).

306 Note that with the above finite-volume scaling, the sizes \mathfrak{H} of the control volumes are
 307 included in the operators, i.e. the scaling in (3.2) is volume consistent [18, 71, 142].
 308 In fact, analytic and discrete operators are related like $\text{div} \leftrightarrow \mathfrak{H}^{-1} \mathfrak{D}_{\text{mass}}$. This
 309 may look a bit awkward, but it fits naturally in the finite-volume setting, and the

310 symmetry properties of the discrete differential operators will come out more directly.
 311 The alternative would have been a scaling of the above operators by \mathfrak{H}^{-1} , which then
 312 would fit naturally in a finite-difference setting. Both notation choices have their pros
 313 and cons; in this paper we opt for the finite-volume related option.

314 With the notation from (3.2), and similar to Eq. (2.1), the discrete (finite-volume)
 315 evolution of total energy can be formulated locally as

$$\begin{aligned}
 316 \quad \mathfrak{H} \frac{\partial \rho E_{\text{total}}}{\partial t} &= \frac{1}{2} (\mathbf{u} \cdot \mathbf{u}) \mathfrak{D}_{\text{mass}} \mathbf{m} - \mathbf{u} \cdot (\mathfrak{C}_{\text{mom}}^{\mathbf{m}} \mathbf{u} + \mathfrak{G}_{\text{mom}} p) - \mathfrak{C}_{\text{inten}}^{\mathbf{m}} e - p \mathfrak{D}_{\text{inten}} \mathbf{u} \\
 317 \quad (3.3) \quad &= \mathbf{u} \cdot \left(\frac{1}{2} \text{diag}(\mathfrak{D}_{\text{mass}} \mathbf{m}) - \mathfrak{C}_{\text{mom}}^{\mathbf{m}} \right) \mathbf{u} - (\mathbf{u} \cdot \mathfrak{G}_{\text{mom}} p + p \mathfrak{D}_{\text{inten}} \mathbf{u}) - \mathfrak{C}_{\text{inten}}^{\mathbf{m}} e.
 \end{aligned}$$

318 The last line in (3.3) corresponds with line (2.1b) in the analytic derivation. From
 319 here, we would like to make the steps to (2.1c) and (2.1d) in this discrete version too.
 320 Therefore, let us find out which relations between the discrete operators have to be
 321 satisfied.

322 The evolution of the total amount of energy can be found by summing (3.3) over
 323 all grid cells (effectuated by multiplying with the grid vector $\mathbf{1}^T$ consisting of only
 324 ones):

$$\begin{aligned}
 325 \quad \mathbf{1}^T \mathfrak{H} \frac{\partial \rho E_{\text{total}}}{\partial t} &= -\mathbf{1}^T \mathbf{u} \cdot \left(\mathfrak{C}_{\text{mom}}^{\mathbf{m}} - \frac{1}{2} \text{diag}(\mathfrak{D}_{\text{mass}} \mathbf{m}) \right) \mathbf{u} \\
 326 \quad (3.4) \quad &\quad - \mathbf{1}^T (\mathbf{u} \cdot \mathfrak{G}_{\text{mom}} p + p \mathfrak{D}_{\text{inten}} \mathbf{u}) - \mathbf{1}^T \mathfrak{C}_{\text{inten}}^{\mathbf{m}} e.
 \end{aligned}$$

327 Because of the finite-volume scaling of (3.2), the left-hand side forms a consistent
 328 approximation of the total amount of energy in the domain: it reflects a midpoint
 329 quadrature rule. Other formulations are possible, as in the higher-order methods of
 330 Verstappen and Veldman [145, 146] which are related to Simpson's quadrature rule.
 331 This volume-consistent [18, 71, 142] scaling property motivated us to 'hide' the size of
 332 the control volumes into the definition of the discrete operators.

333 The first two summations in the right-hand side of (3.4) can be interpreted as
 334 inner products in the space of scalar and vector-valued grid functions. The symmetry
 335 properties that we will discuss below are with respect to these inner products. From
 336 here the requirements for discrete energy conservation can be derived. We will see in
 337 the sequel that this requires a certain amount of compatibility between the discrete
 338 operators.

339 **REQUIREMENT 3.1** (Compare [Property 2.1](#)). *The first summation in the right-*
 340 *hand side of (3.4) should vanish, i.e. the matrix operator between the first pair of*
 341 *brackets should satisfy*

$$342 \quad (3.5) \quad \mathfrak{C}_{\text{mom}}^{\mathbf{m}} - \frac{1}{2} \text{diag}(\mathfrak{D}_{\text{mass}} \mathbf{m}) \text{ is skew-symmetric.}$$

343 This necessary and sufficient condition for global discrete convective energy conser-
 344 vation has thus far been mentioned only a few times, e.g. by Kok [62], Morinishi [77],
 345 Van 't Hof et al. [137, 138], and implicitly by Chandrashekar [22, Sect. 3]. It provides a
 346 relation between the diagonal of $\mathfrak{C}_{\text{mom}}^{\mathbf{m}}$ and discrete mass conservation $\mathfrak{D}_{\text{mass}} \mathbf{m}$. The
 347 examples in Sect. 4 and 5 indicate that when starting from a finite-volume discretiza-
 348 tion one also has local energy conservation. It would be interesting to investigate
 349 which conditions govern local secondary conservation in the general case [27, 28, 90].

350 **REQUIREMENT 3.2** (Compare [Property 2.2](#)). *In order for the second sum in*
 351 *the right-hand side of (3.4) to vanish, the (pressure) gradient and the dilatational*
 352 *divergence should be each other's negative transpose:*

$$353 \quad (3.6) \quad \mathfrak{G}_{\text{mom}} = -\mathfrak{D}_{\text{inten}}^T (= -\mathfrak{D}_{\text{mass}}^T).$$

354 This is a necessary and sufficient condition to ensure that the pressure does not
 355 contribute to the global total energy. In this way, the two operators $\mathfrak{D}_{\text{inten}}$ and
 356 $\mathfrak{G}_{\text{mom}}$ combine into a meaningful discrete divergence expression for $\nabla(\rho\mathbf{u})$ in the
 357 virtual evolution of total energy. Alternatively, if we would have started in (1.1c)
 358 with a conservation law for total energy, then to achieve a physically meaningful
 359 exchange between internal and kinetic energy a similar consistency condition between
 360 the pressure gradient and the latter divergence would be required.

361 In (3.6), the right-hand side between parentheses corresponds with the incom-
 362 pressible limit, in which the equation for internal energy degenerates into the conti-
 363 nuity equation [47, 61]. Also, it leads to a symmetric negative-definite Laplacian in
 364 the often used pressure Poisson equation.

365 The final requirements concern the discretization of the equation for internal en-
 366 ergy. First of all, for discrete energy conservation it is necessary that it is conservative.
 367 As an additional property, for low Mach numbers [47, 61] we would like the discretiza-
 368 tion for compressible flow to approach a discretization for incompressible flow. This
 369 requires further consistency between the discrete operators; see Appendix A.

370 **REQUIREMENT 3.3** (Compare [Property 2.3](#)).

371 *A: Vanishing of the last sum in the right-hand side (3.4) requires*

372 (3.7) $\mathfrak{C}_{\text{inten}}^m$ is telescoping (like a finite-volume operator).

373 *B: To combine the momentum and internal-energy equations into a unified equation*
 374 *for total energy, the respective discrete convective operators should be the same:*

375 (3.8)
$$\mathfrak{C}_{\text{inten}}^m = \mathfrak{C}_{\text{mom}}^m.$$

376 *C: A smooth discrete transition from compressible flow to incompressible flow requires*
 377 *that the divergence operators in (3.1c) are consistent (in the incompressible limit) with*
 378 *the divergence operator in (3.1a):*

379 (3.9)
$$\mathfrak{D}_{\text{inten}} = \mathfrak{D}_{\text{mass}} \quad \vee \quad \mathfrak{C}_{\text{inten}}^m \rightarrow \rho_0 \mathfrak{D}_{\text{mass}} \mathbf{u}$$

380 (ρ_0 is the incompressible density).

381 While being sufficient, it is noted that these conditions are not strictly necessary to
 382 achieve global conservation of total energy. Also note that in view of the relations
 383 (3.8) and (3.5), the conditions in (3.9) will usually be satisfied.

384 The above requirements suggest to introduce the following definition of symme-
 385 try-preserving operators for (in)compressible flow:

386 **DEFINITION 3.4** (symmetry-preserving). *The triple of discrete finite-volume op-*
 387 *erators for the incompressible Euler equations $\{\mathfrak{C}_{\text{mom}}^m, \mathfrak{D}_{\text{mass}}, \mathfrak{G}_{\text{mom}}\}$, where $\mathfrak{C}_{\text{mom}}^m$*
 388 *is a discrete convection operator, $\mathfrak{D}_{\text{mass}}$ a discrete divergence and $\mathfrak{G}_{\text{mom}}$ a discrete*
 389 *gradient, is called symmetry-preserving when [Requirements 3.1](#) and [3.2](#) hold. For*
 390 *compressible flow, a convection operator $\mathfrak{C}_{\text{inten}}^m$ and a dilatation operator $\mathfrak{D}_{\text{inten}}$ for*
 391 *the internal-energy equation should be added, for which [Requirement 3.3](#) holds.*

392 With this definition, we can summarize our main result as:

393 **THEOREM 3.5.** *A (volume-consistent) finite-volume discretization of the Euler*
 394 *equations (1.1) for (in)compressible flow is supra-conservative with respect to global*
 395 *discrete energy if it is symmetry-preserving in the sense of [Definition 3.4](#). Hereto*
 396 *[Requirements 3.1](#) and [3.2](#) are not only sufficient but also necessary.*

397 The above requirements guide the way to construct finite-volume triples/quartets
 398 which all additionally conserve discrete kinetic energy. These triples/quartets cannot
 399 be chosen freely. In particular, the choice for the discretization of the convective term
 400 $\mathfrak{C}_{\text{mom}}^m$ induces *all* other discretizations:

- 401 1. Through [Requirement 3.1](#) the discretization of the conservation of mass $\mathfrak{D}_{\text{mass}}$
 402 is determined.
- 403 2. [Requirement 3.2](#) then determines the discrete pressure gradient $\mathfrak{G}_{\text{mom}}$ in the
 404 conservation of momentum, and the dilatational divergence $\mathfrak{D}_{\text{inten}}$ in the conser-
 405 vation of internal energy.
- 406 3. Finally, [Requirement 3.3](#) determines the discrete convective term $\mathfrak{C}_{\text{inten}}^m$ in the
 407 conservation of internal energy.

408 On staggered grids, where the individual unknowns are located at different positions,
 409 the above requirements may involve some form of interpolation; we will come back
 410 to this later. In the next sections we will work out the above requirements for some
 411 specific situations involving a finite-volume discretization.

412 It is remarked that the above requirements have been derived starting from the
 413 symbolic discrete formulation in (3.2). The finite-volume origin led in a natural way to
 414 a scaling for which the summation in the left-hand side of (3.4) represents an approx-
 415 imate volume integral, i.e. the scaling is volume consistent. But no other properties
 416 of a finite-volume method have been used. As a consequence, all requirements for
 417 discrete energy conservation hold for any discretization that can be written in the
 418 volume-consistent form (3.2); its analytical ‘provenance’ is less relevant [132].

419 Finally, a diffusive term can be added, i.e. the extension to the Navier–Stokes
 420 equations can be made, independently of the above discretizations. Of course, one
 421 would want the discretization of the viscous stresses to lead to a consistent, symmetric
 422 negative-definite operator. But no further requirements have to be imposed as far as
 423 we are concerned here, as in this way diffusion will not interfere with the physics of
 424 convection. Perot [92] gives guide lines on how to achieve this on arbitrary grids.

425 **4. Incompressible flow - staggered grid.** As a first example, we will work
 426 out the above requirements when discretizing the equations (1.1) in the special case of
 427 incompressible flow on a staggered grid, as shown in [Figure 1](#). The case of collocated
 428 grids will be discussed later on, when applied to the equations for compressible flow.

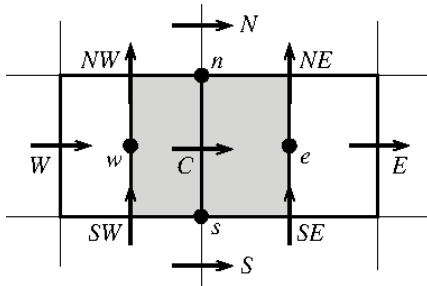


FIG. 1. A staggered control volume for the conservation of x -momentum (shaded area), covering half of two adjacent control volumes (grid cells) for mass conservation.

429 **4.1. Conservation of mass.** On a staggered grid, the velocity components are
 430 defined on the edges/faces of the computational cells. Also the momentum equation
 431 (3.1b) is discretized in those locations; see the shaded momentum control volume in
 432 [Figure 1](#). The continuity equation (3.1a) is discretized in cell centers, with the grid
 433 cells as control volumes.

434 In the right-hand cell in **Figure 1** (around the location e), the incompressible form
 435 of the conservative continuity equation (3.1a) can be discretized as

$$436 \quad 0 = \oint_{\Gamma_e} \mathbf{m} \cdot \mathbf{n} \, d\Gamma = \int_{\Gamma_E} m^x \, d\Gamma_E + \int_{\Gamma_{NE}} m^y \, d\Gamma_{NE} - \dots$$

$$437 \quad (4.1) \quad \equiv \tilde{m}_E^x + \tilde{m}_{NE}^y - \tilde{m}_C^x - \tilde{m}_{SE}^y \equiv \mathfrak{D}_{\text{mass}} \mathbf{m}|_e.$$

438 Here, \tilde{m} denotes a mass flux integrated over an (infinitesimal) edge $d\Gamma$ of the con-
 439 trol volume, e.g. (but not necessarily) by a midpoint integration rule (like $\tilde{m}_E^x \equiv$
 440 $m_E^x |d\Gamma_E|$). Note that (4.1) puts no further restrictions on the choice of \tilde{m} .

441 **4.2. Conservation of momentum.** Next, the discretization of the convective
 442 term and the pressure gradient on a staggered grid will be shown.

443 **Convection.** In the u -component of the momentum equation (3.1b), the discrete
 444 convective contribution from the shaded control volume in **Figure 1** reads approxi-
 445 mately

$$446 \quad \int_{\Gamma_h} (\mathbf{m} \cdot \mathbf{n}) u \, d\Gamma_h \approx u_e \int_{\Gamma_e} \mathbf{m} \cdot \mathbf{n} \, d\Gamma_e + u_n \int_{\Gamma_n} \mathbf{m} \cdot \mathbf{n} \, d\Gamma_n + \dots$$

$$447 \quad (4.2) \quad = \tilde{m}_e^x u_e + \tilde{m}_n^y u_n - \tilde{m}_w^x u_w - \tilde{m}_s^y u_s \equiv \mathfrak{C}_{\text{mom}}^{\mathbf{m}} \mathbf{u}|_C,$$

448 which defines the convection operator $\mathfrak{C}_{\text{mom}}^{\mathbf{m}}$ from (3.2b). To achieve symmetry in
 449 the coefficient matrix, it is necessary that the u -fluxes are chosen according to an
 450 equal-weighted ($\frac{1}{2}$ - $\frac{1}{2}$) interpolation between the faces of the continuity cells, even if
 451 the faces of the momentum control volume are not located in the cell centers:

$$452 \quad (4.3) \quad u_e = \frac{1}{2}(u_E + u_C), \quad u_n = \frac{1}{2}(u_N + u_C), \quad \text{etc.}$$

453 Then substitution of (4.3) into (4.2) yields

$$454 \quad \mathfrak{C}_{\text{mom}}^{\mathbf{m}} \mathbf{u}|_C = \frac{1}{2}[\tilde{m}_e^x(u_E + u_C) + \tilde{m}_n^y(u_N + u_C) - \tilde{m}_w^x(u_W + u_C) - \tilde{m}_s^y(u_S + u_C)]$$

$$455 \quad = \frac{1}{2}[\tilde{m}_e^x u_E - \tilde{m}_w^x u_W + \tilde{m}_n^y u_N - \tilde{m}_s^y u_S] + \frac{1}{2}[\tilde{m}_e^x - \tilde{m}_w^x + \tilde{m}_n^y - \tilde{m}_s^y] u_C.$$

456 It is clear that the coefficients of the neighboring grid points are skew symmetric due
 457 to the equal-weighted interpolation in (4.3). Whether the central coefficient (of u_C)
 458 vanishes is as yet unclear, and will be examined next.

459 In the diagonal coefficient $\text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{m}})|_C \equiv \frac{1}{2}[\tilde{m}_e^x - \tilde{m}_w^x + \tilde{m}_n^y - \tilde{m}_s^y]$ we recognize
 460 a discrete divergence operator over a momentum control volume, but not yet im-
 461 mediately the one from the discrete continuity equation given in (4.1). Skew symmetry
 462 (3.5) requires $\text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{u}}) - \frac{1}{2} \mathfrak{D}_{\text{mass}} \mathbf{m} = 0$. This is now a requirement for the con-
 463 struction of $\mathfrak{D}_{\text{mass}}$, which herewith becomes related to the diagonal entries given by
 464 $\text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{m}})$ (though it will require some interpolations between the staggered grid
 465 positions). The requirement can be satisfied by interpolating the mass fluxes \tilde{m} with
 466 equal weights, similar to the velocity components, i.e. we define

$$467 \quad (4.4) \quad \tilde{m}_e^x = \frac{1}{2}(\tilde{m}_E^x + \tilde{m}_C^x), \quad \tilde{m}_n^y = \frac{1}{2}(\tilde{m}_{NE}^y + \tilde{m}_{NW}^y), \quad \text{etc.}$$

468 For this choice of the mass fluxes, the central coefficient becomes

$$469 \quad \text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{m}})|_C = \frac{1}{4}[\tilde{m}_E^x - \tilde{m}_W^x + \tilde{m}_{NE}^y + \tilde{m}_{NW}^y - \tilde{m}_{SE}^y - \tilde{m}_{SW}^y],$$

470 which equals $\frac{1}{4} \times [\text{mass conservation of right- + left-hand cell}]$. As a result

$$471 \quad (4.5) \quad \text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{m}})|_C = \frac{1}{4}(\mathfrak{D}_{\text{mass}}\mathbf{m}|_e + \mathfrak{D}_{\text{mass}}\mathbf{m}|_w) = 0,$$

472 i.e. the diagonal of the convective operator vanishes. Thus, we have achieved our goal
473 **Requirement 3.1** of skew symmetry. It is remarked that the choice (4.4) is not unique,
474 as demonstrated in [137, Sect. 3.1].

475 The above guarantees global conservation of kinetic energy. Substitution of $\mathfrak{C}_{\text{mom}}^{\mathbf{m}}$
476 in (3.3) shows that energy is also conserved locally, with energy fluxes given by
477 $\frac{1}{2}\tilde{m}_e^x u_C u_E$, etc.

478 **Pressure gradient.** Finally, we have to consider the contribution of the pressure
479 to the evolution of kinetic energy. The pressure is defined in cell centers, e.g. the points
480 w and e in **Figure 1**. The contribution to the x -momentum equation (3.1b) can be
481 approximated as (with \mathbf{e}_x denoting the unit vector in x -direction)

$$482 \quad (4.6) \quad \oint_{\Gamma_h} p \mathbf{n} \, d\Gamma \approx \int_e p_e \mathbf{e}_x \, d\Gamma_e - \int_w p_w \mathbf{e}_x \, d\Gamma_w \equiv \mathfrak{G}_{\text{mom},x} p,$$

483 which defines the x -component of the discrete pressure gradient $\mathfrak{G}_{\text{mom}}$. Its coefficients
484 are equal to the size of the corresponding faces, similar to the discrete approximation
485 of the continuity equation in (4.1), with coefficients equal to the local size of the face
486 $d\Gamma$. Noting that the grid is rectangular, it follows that the discrete pressure gradient
487 and the discrete divergence satisfy **Requirement 3.2**.

488 The pressure can be computed by requiring that the solution of the discrete
489 momentum equation (3.2b) satisfies the discrete constraint (3.2a). I.e., there must
490 hold

$$491 \quad (4.7) \quad 0 = \frac{\partial}{\partial t} \mathfrak{D}_{\text{mass}} \mathbf{m}^{(*)} \equiv \mathfrak{D}_{\text{mass}} \frac{\partial \rho \mathbf{u}}{\partial t} = -\mathfrak{D}_{\text{mass}} \mathfrak{H}^{-1} (\mathfrak{C}_{\text{mom}}^{\mathbf{m}} \mathbf{u} + \mathfrak{G}_{\text{mom}} p),$$

492 which defines the Poisson equation for the pressure. Note that the discrete Poisson
493 operator is symmetric negative definite, due to **Requirement 3.2**. Also, note that the
494 step (*) in (4.7) is one of only two places in this paper where the equality between \mathbf{m}
495 and $\rho \mathbf{u}$ is needed.

496 **5. Compressible flow - collocated grid.** On a structured collocated grid, as
497 used commonly for compressible flow, all flow variables are defined in ‘cell centers’
498 with a liberal interpretation of the meaning of ‘center’ (centroid, circumcenter, ...);
499 see **Figure 2 (left)**. E.g., positioning the faces halfway the locations where the flow
500 variables are defined (known as a Voronoi grid) is a valid option, as in **Figure 2 (right)**
501 of an unstructured grid. No choice between the ‘center-options’ will be made in this
502 paper; we merely focus on the symmetry properties of the discrete operators.

503 **5.1. Conservation of mass.** With reference to **Figure 2**, it is natural to choose
504 the finite-volume form of the divergence term in the equation for mass conservation
505 (3.2a) as

$$506 \quad (5.1) \quad \mathfrak{D}_{\text{mass}} \mathbf{m}|_C \equiv \tilde{m}_e^x + \tilde{m}_n^y - \tilde{m}_w^x - \tilde{m}_s^y = \sum_{f \in \mathcal{F}_C} \tilde{\mathbf{m}}_f \cdot \mathbf{n}_f.$$

507 The right-hand side is formulated in a general notation for arbitrarily-shaped con-
508 trol volumes. The summation is over the faces f of the volume around C , together
509 constituting the set \mathcal{F}_C , and \mathbf{n}_f is an outward-pointing normal.

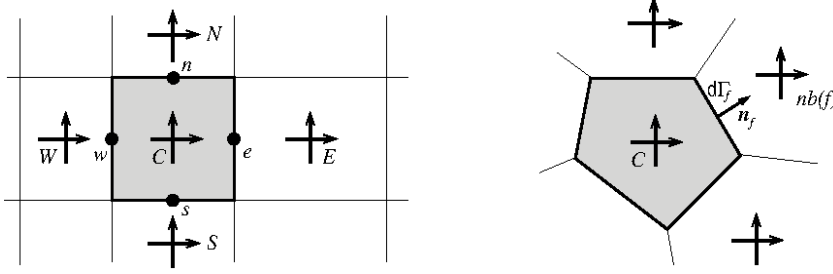


FIG. 2. Control volumes for collocated grids: (left) structured with \mathbf{u} -locations halfway faces (= cell-centered); and (right) unstructured with faces halfway \mathbf{u} -locations (= face- or vertex-centered).

5.2. Conservation of momentum.

511 **Convection.** With similar notation, the discrete convective contribution to the
 512 momentum equation reads

$$513 \quad (5.2) \quad \mathfrak{C}_{\text{mom}}^{\mathbf{m}} \mathbf{u}|_C \equiv \tilde{m}_e^x \mathbf{u}_e + \tilde{m}_n^y \mathbf{u}_n - \tilde{m}_w^x \mathbf{u}_w - \tilde{m}_s^y \mathbf{u}_s = \sum_{f \in \mathcal{F}_C} (\tilde{\mathbf{m}}_f \cdot \mathbf{n}_f) \mathbf{u}_f.$$

514 To compute the fluxes at the cell edges, again an equal-weighted ($\frac{1}{2}$ - $\frac{1}{2}$) interpolation
 515 for the velocity component u should be applied:

$$516 \quad (5.3) \quad \mathbf{u}_f = \frac{1}{2}(\mathbf{u}_C + \mathbf{u}_{nb(f)}),$$

517 where $nb(f)$ denotes the neighboring grid cell sharing the face f . As a direct conse-
 518 quence, the coefficients in the convective contribution are skew-symmetric outside the
 519 diagonal. The $\frac{1}{2}$ - $\frac{1}{2}$ interpolation is essential here, even when the faces are not half-way
 520 between the cell centers. Jameson, in the early 1980s [59], interprets the values in the
 521 cell ‘centers’ as averages over the cells, after which a $\frac{1}{2}$ - $\frac{1}{2}$ averaging at the separating
 522 face is natural. The ‘reward’ is discrete energy conservation [58], whereas the location
 523 of the cell center turns out to be not very critical. Jameson’s approach has become
 524 one of the most widely used CFD methods in the aircraft industry [1].

525 The interesting part is the coefficient on the diagonal of $\mathfrak{C}_{\text{mom}}^{\mathbf{m}}$. With the above
 526 interpolation (5.3), the central coefficient in the convection operator (5.2) becomes

$$527 \quad \text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{m}}) = \frac{1}{2} \sum_{f \in \mathcal{F}_C} (\tilde{\mathbf{m}}_f \cdot \mathbf{n}_f) \stackrel{(5.1)}{=} \frac{1}{2} \mathcal{D}_{\text{mass}} \mathbf{m}.$$

528 Hence the vector $\text{diag}(\mathfrak{C}_{\text{mom}}^{\mathbf{m}}) - \frac{1}{2} \mathcal{D}_{\text{mass}} \mathbf{m}$ vanishes. In fact, the latter requirement
 529 determines the choice of $\mathcal{D}_{\text{mass}}$. The ‘freedom’ we felt while choosing the discrete
 530 divergence operator for mass conservation as in (5.1) is just an illusion: if one in-
 531 sists on energy conservation, given (5.2) and (5.3), there is no other choice possible!
 532 Anyhow, the above discretization, (5.1)+(5.2) with interpolation (5.3), satisfies the
 533 main Requirement 3.1 for global energy conservation: $\mathfrak{C}_{\text{mom}}^{\mathbf{m}} - \frac{1}{2} \text{diag}(\mathcal{D}_{\text{mass}} \mathbf{m})$ is skew
 534 symmetric, for *all* choices of the mass fluxes $\tilde{\mathbf{m}}$. Also, we have local conservation with
 535 a kinetic energy flux given by $\frac{1}{2}(\tilde{\mathbf{m}}_f \cdot \mathbf{n}_f)(\mathbf{u}_C \cdot \mathbf{u}_{nb(f)})$.

536 Some freedom is left in the choice for the mass fluxes [110]). E.g., there is room
 537 to use geometry information to interpolate from the values of \mathbf{m} in the cell centers
 538 to the values of $\tilde{\mathbf{m}}$ at the faces. It would be interesting to explore this interpolation
 539 freedom on (highly) irregular grids.

540 **Pressure gradient.** A natural choice for the finite-volume form of the pressure
541 gradient is

$$542 \quad \mathfrak{G}_{\text{mom}} p|_C \equiv (\tilde{p}_e - \tilde{p}_w) \mathbf{e}_x + (\tilde{p}_n - \tilde{p}_s) \mathbf{e}_y = \sum_{f \in \mathcal{F}_C} \tilde{p}_f \mathbf{n}_f.$$

543 Once more using equal-weighted interpolation, as in (4.3), we define the pressure
544 ‘fluxes’ as

$$545 \quad \tilde{p}_f = \frac{1}{2}(p_C + p_{nb(f)}) |\text{d}\Gamma_f|.$$

546 The gradient operator can now be rewritten as

$$547 \quad (5.4) \quad \mathfrak{G}_{\text{mom}} p|_C = \sum_{f \in \mathcal{F}_C} \frac{1}{2} |\text{d}\Gamma_f| \mathbf{n}_f p_{nb(f)},$$

548 where the (central) coefficient of p_C vanishes because $\sum_{f \in \mathcal{F}_C} |\text{d}\Gamma_f| \mathbf{n}_f = 0$.

549 *Remark.* For collocated grids, in the incompressible limit the stencil of the pres-
550 sure Poisson equation (4.7) is prone to odd-even decoupling due to Requirement 3.2,
551 which is needed to maintain perfect discrete energy conservation. To resolve this is-
552 sue, provided all details are filled in correctly, the corresponding checkerboard mode
553 can be filtered out, as done, e.g., by Ham et al. [48] and Shashank et al. [117].

554 **5.3. Conservation of internal energy.** Similar to the definition of $\mathfrak{D}_{\text{mass}}$ in
555 (5.1), the discrete divergence operator $\mathfrak{D}_{\text{inten}}$ in the dilatation term of the energy
556 equation is defined as

$$557 \quad \mathfrak{D}_{\text{inten}} \mathbf{u}|_C \equiv \tilde{u}_e^x + \tilde{u}_n^y - \tilde{u}_w^x - \tilde{u}_s^y = \sum_{f \in \mathcal{F}_C} \tilde{\mathbf{u}}_f \cdot \mathbf{n}_f.$$

558 Again, equal-weighted ($\frac{1}{2}$ - $\frac{1}{2}$) interpolation is used to define the face fluxes:

$$559 \quad \tilde{\mathbf{u}}_f = \frac{1}{2}(\mathbf{u}_C + \mathbf{u}_{nb(f)}) |\text{d}\Gamma_f|.$$

560 The divergence operator can now be rewritten as

$$561 \quad (5.5) \quad \mathfrak{D}_{\text{inten}} \mathbf{u}|_C = \sum_{f \in \mathcal{F}_C} \frac{1}{2} |\text{d}\Gamma_f| \mathbf{n}_f \cdot \mathbf{u}_{nb(f)},$$

562 where the (central) coefficient of \mathbf{u}_C has vanished as in (5.4).

563 Looking at the evaluation of (5.5) in the neighboring cell, the coefficient of \mathbf{u}_C
564 in the neighboring divergence operator is $\frac{1}{2} |\text{d}\Gamma_f| \mathbf{n}_{nb(f)}$, with $\mathbf{n}_{nb(f)}$ pointing from
565 the neighboring cell towards C . This generates a minus sign when compared to the
566 coefficient of $p_{nb(f)}$ in the gradient operator (5.4) in C . Thus, $\mathfrak{D}_{\text{mass}} = \mathfrak{D}_{\text{inten}}$ and
567 $\mathfrak{G}_{\text{mom}}$ are each other’s negative transpose, as imposed by Requirement 3.2.

568 The convective term in the equation for internal energy reads

$$569 \quad (5.6) \quad \mathfrak{C}_{\text{inten}}^m e|_C \equiv \tilde{m}_e^x e_e + \tilde{m}_n^y e_n - \tilde{m}_w^x e_w - \tilde{m}_s^y e_s = \sum_{f \in \mathcal{F}_C} (\tilde{\mathbf{m}}_f \cdot \mathbf{n}_f) e_f.$$

570 Substitution of (5.4), (5.5) and (5.6) in (3.3) shows that, next to global energy con-
571 servation, we also have local energy conservation, with a thermodynamic flux given
572 by $[\frac{1}{2}(p_{nb(f)} \mathbf{u}_C + p_C \mathbf{u}_{nb(f)}) + \tilde{\mathbf{m}}_f e_f] \cdot \mathbf{n}_f$.

573 In Appendix A, see also [47,61], it is shown that in the limit of compressible flow
 574 the internal energy e becomes a constant, say e_0 . Also the density ρ approaches a
 575 constant ρ_0 . Then the convective term from (5.6) becomes

$$576 \quad \mathfrak{C}_{\text{inten}}^{\mathbf{m}} e|_C \approx \rho_0 e_0 \sum_{f \in \mathcal{F}_C} (\tilde{\mathbf{u}}_f \cdot \mathbf{n}_f),$$

577 where we used, for the second (and last) time in this paper, that $\mathbf{m} = \rho \mathbf{u}$. The above
 578 relation shows that in the incompressible limit the divergence operator in the con-
 579 vective term approaches the divergence $\mathfrak{D}_{\text{mass}} = \mathfrak{D}_{\text{inten}}$ from the continuity equation.
 580 Appendix A shows that this allows for a smooth transition from the compressible to
 581 the incompressible discretization.

582 **6. Discussion.** In the previous sections we have unraveled a strategy to de-
 583 rive supra-conservative finite-volume (semi-)discretizations for compressible Euler flow
 584 that possess additional discrete conservation properties as secondary invariants (like
 585 kinetic energy), assuming exact time integration. This paper focusses on the dis-
 586 crete conservation of energy, but, as mentioned in the Introduction, other secondary
 587 invariants could have been selected. More research is worthwhile to find out which in-
 588 variants are best chosen for a given physical application; see e.g. [17]. Also, the subtle
 589 difference between global and local conservation deserves more attention [27,28,90].

590 Mimicking the analytic derivation, the key ingredient of energy-preserving dis-
 591 cretizations is a close consistency between the discrete momentum equation and the
 592 discrete mass equation (Requirement 3.1). In particular, the diagonal of the discrete
 593 convection operator directly determines the discrete divergence in the mass equation
 594 and in the dilatation term of the internal energy equation (Requirement 3.3). Also,
 595 it determines the discrete pressure gradient (Requirement 3.2).

596 It is once more stressed, as Bryan [13] already did in 1966, that equal-weighted
 597 interpolations (for the velocity \mathbf{u} and the mass flux \mathbf{m}) from cell centers to cell faces
 598 are essential to achieve the required compatibility, irrespective of any stretching of
 599 the grid! Note that the volume-consistent scaling does contain info about the cell
 600 sizes and hence the stretching, and also the mass fluxes provide some freedom to
 601 incorporate geometry information.

602 In our examples, the cell faces are located halfway the positions where \mathbf{m} is
 603 defined for which an equal-weighted interpolation is natural. But also in other ge-
 604 ometrical configurations the same interpolation has to be used, even when a linear
 605 unequal-weighted interpolation would seem more logical from an approximation point
 606 of view. We already noted that Jameson’s [59] interpretation of this interpolation also
 607 points towards an equal weighting. The resulting skew-symmetry of the convective
 608 discretization turns out more important than local interpolation accuracy and the pre-
 609 cise location of cell ‘centers’. And, as Ham et al. [49] point out explicitly, on smooth
 610 grids (with a bounded ratio between the largest and the smallest grid cells) the re-
 611 spective truncation errors are all second order as usual. See Manteuffel and White [73]
 612 for a theoretical justification, and Felten and Lund [38] for practical experiences.

613 One ‘reward’ for this consistency in the discretization is the numerical stability of
 614 the semi-discretized equations without needing any numerical dissipation. This can
 615 be proven under the restriction that the density has a positive lower bound, as in the
 616 incompressible case. No rigorous proof has been found yet for the general compressible
 617 case, but in practice this appears to be mainly a theoretical issue. Another ‘reward’
 618 is that subtleties in (eddy-viscosity) turbulence models are not masked by excessive
 619 numerical dissipation. Neither will emerging instabilities, like the transition from

620 laminar to turbulent flow, be suppressed by an overdose of numerical artifacts [107].
 621 In this non-interfering way, an energy-preserving discretization forms an excellent
 622 basis to combine with low-dissipation turbulence models [106, 110].

623 Usually, this is the place to demonstrate the performance of such methods by
 624 showing results for a number of test cases. However, we think it is more convincing
 625 to point the reader to the original papers that are successfully using these methods.
 626 Many of these energy-preserving methods have been mentioned in the Introduction.
 627 Here, in Table 1, we restrict ourselves to a short overview of supra-conservative finite-
 628 volume methods for the Euler and/or Navier–Stokes equations. The table has been
 629 sorted according to the grid used (structured or unstructured) and the positioning of
 630 the unknowns (staggered or collocated). Also, higher-order (> 2) variants have been
 631 indicated, including the dispersion-relation preserving method by Kok [62].

TABLE 1

A sorted selection of supra-conservative finite-volume methods for the Euler/Navier–Stokes equations. The references marked [·] use higher-order methods.*

flow	grid	staggered	collocated
incompressible	structured	[137], [138, 144–146, 150]*	[38]
	unstructured	[60, 64, 90, 153]	[60, 66, 104, 115, 133]
compressible	structured	[77]	[28, 33, 58, 124], [62, 107, 108]*

632 **7. Conclusion.** The paper describes general, necessary and sufficient, require-
 633 ments for a (semi-)discretization method to conserve secondary invariants, in particu-
 634 lar kinetic energy. The essential ingredient is a close consistency between the discrete
 635 convection term in the momentum equation, the discrete pressure gradient and the
 636 discrete divergences in the conservation laws for mass and for internal energy. When
 637 the discrete convection is chosen, the discretization of all other terms is fixed (with
 638 freedom left for the mass flux only).

639 As a general message, it is demonstrated how finite-volume methods can be de-
 640 signed such that, next to the primary invariants, they also conserve one or more
 641 secondary invariants, i.e., they can be called supra-conservative. The bottom-line is
 642 that the steps in the analytical derivations should be mirrored in the discrete setting.
 643 It is expected that this philosophy will be useful independent of the selected secondary
 644 invariants, and will lead to requirements, like the above, on the discretization scheme.

645 The specific requirements to realize discrete energy conservation hold for any
 646 discretization which can be put in the form (3.2) studied here. It is left to the readers
 647 to figure out whether or not their favorite discretization approach can be made to
 648 satisfy these requirements.

649 Appendix A. The incompressible limit.

650 One may also wish for a smooth transition of a discretization scheme between
 651 compressible and incompressible flow. We will pursue this limit following the scaling
 652 by Klein [61] and Guillard and Viozat [47]. These authors consider the following
 653 expansions for the flow variables in the incompressible limit $c^* \rightarrow \infty$ (ρ^* , u^* and c^*

654 are characteristic values for density, velocity and speed of sound, respectively):

$$655 \quad \mathbf{u}/u^* = \mathbf{u}_0 + O(1/c^*), \quad \rho/\rho^* = \rho_0 + O(1/c^*),$$

$$656 \quad p/\rho^*c^{*2} = p_0 + O(1/c^*), \quad e/c^{*2} = e_0 + O(1/c^*).$$

657 Substitution of these expansions in the equation for internal energy (1.1c) yields for
658 the leading term of order c^{*2} :

$$659 \quad (\text{A.1}) \quad \frac{\partial \rho_0 e_0}{\partial t} + \nabla \cdot (\rho_0 e_0 \mathbf{u}_0) = -p_0 \nabla \cdot \mathbf{u}_0.$$

660 It can be shown that ρ_0 , p_0 and e_0 are constant in space and time. Then this equation
661 degenerates into

$$662 \quad (\rho_0 e_0 + p_0) \nabla \cdot \mathbf{u}_0 = 0.$$

663 We recognize the continuity equation for incompressible flow. But we also see that
664 this equation stems from both the convective term as well as the dilatation term in
665 the equation for internal energy.

666 Therefore, if one would like the discrete version of the equations for compressible
667 flow to smoothly approach the discrete equations for incompressible flow, then both
668 discrete divergence operators in (A.1) must be the same, and equal to the divergence
669 that describes conservation of mass. This is expressed in Requirement 3.3C.

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672

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