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Hexagonal YbMnO₃ revisited

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#####
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_journal_date_accepted    2001-09-13
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_journal_year      2001
_journal_volume      57
_journal_issue      10
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_journal_page_last      i89
_journal_paper_category      EI
_publ_contact_author_name      'Dr A. Meetsma'
_publ_contact_author_address
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Solid State Chemistry Laboratory
Materials Science Centre
University of Groningen
Nijenborgh 4
NL-9747 AG Groningen
The Netherlands
;
_publ_contact_author_email      a.meetsma@fwn.rug.nl
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_publ_contact_author_phone      '+31 50 3634368'
_publ_section_title      'Hexagonal YbMnO~3~ revisited'
loop_
  _publ_author_name
  _publ_author_address
    'Aken, Bas B. van'
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;
'Meetsma, Auke'

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;
'Palstra, Thomas T. M.'

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Materials Science Centre
University of Groningen
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The Netherlands.

;
data_I
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_chemical_formula_iupac 'Yb Mn O3'
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y, x, z
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-x, -x+y, z
-y, -x, 1/2+z
x-y, -y, z
x, x-y, 1/2+z
_cell_length_a 6.0584(6)
_cell_length_b 6.0584(6)
_cell_length_c 11.3561(7)
_cell_angle_alpha 90
_cell_angle_beta 90
_cell_angle_gamma 120
_cell_volume 360.97(6)
_cell_formula_units_Z 6
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_cell_special_details

;

Unit cell parameters (Duisenberg, 1992) and orientation matrix were determined from a least-squares treatment of SET4 (de Boer & Duisenberg, 1984) setting. Reduced cell calculations did not indicate any higher metric lattice symmetry and examination of the final atomic coordinates of the structure did not yield extra symmetry elements (Spek, 1988; Le Page 1987, 1988)

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_diffn_reflns_limit_l_min      -20
_diffn_reflns_limit_l_max      20
_diffn_reflns_reduction_process
;
Intensity data were corrected for Lorentz and polarisation effects, scale
variation, for absorption and reduced to  $F_o \sim F^2$ 
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_diffn_standards_decay_%       0
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  _diffn_standard_refl_index_k
  _diffn_standard_refl_index_l
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  2 2 4
  2 0 2
_refine_special_details
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Refinement of  $F^2$  against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on  $F^2$ , conventional R-factors R are based on F,

```

with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sqrt{F^2}$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

```

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      'w = 1/[\sqrt(Fo^2)+(0.0494P)^2] where P = (Fo^2+2Fc^2)/3'
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  _atom_site_thermal_displace_type
  _atom_site_occupancy
  _atom_site_type_symbol
  Yb1 .00000 .00000 .27336(5) .00427(11) Uani 1.000 Yb
  Yb2 .33333 -.33333 .23061(3) .00472(7) Uani 1.000 Yb
  Mn .3333(5) .00000 -.00194(14) .0054(2) Uani 1.000 Mn
  O1 .3030(12) .00000 .1617(6) .0039(10) Uani 1.000 O
  O2 .3610(15) .00000 -.1658(6) .0074(11) Uani 1.000 O
  O3 .00000 .00000 -.0268(16) .004(2) Uani 1.000 O
  O4 .33333 -.33333 .0192(9) .0059(17) Uani 1.000 O

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  _atom_site_aniso_U_23
  Yb1 .0047(2) .0047(2) .0035(2) .00230(10)
                                           .0000 .0000
  Yb2 .00350(10)
                                           .00360(10)
                                           .0071(2) .00180(10)
                                           .0000 .0000
  Mn .0069(4) .0048(4) .0039(2) .0024(6) .0002(3) .0000
  O1 .0050(14) .0017(18) .0041(19) .0009(9) -.0019(15) .0000
  O2 .014(2) .0001(18) .0033(17) .0000(9) .0002(19) .0000
  O3 .003(2) .003(2) .005(6) .0016(10) .0000 .0000
  O4 .009(3) .009(3) .000(3) .0047(13) .0000 .0000

```

_geom_special_details

```

;
Bond distances, angles etc. have been calculated using the rounded fractional
coordinates. All esds are estimated from the variances of the (full)
variance-covariance matrix. The cell esds are taken into account in the
estimation of distances, angles and torsion angles

```

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  Yb1 O1 . . 2.231(7) yes
  Yb1 Yb2 . 1_455 3.5313(4) no
  Yb1 Yb2 . 1_565 3.5313(4) no
  Yb1 Mn . 2_555 3.254(3) no
  Yb1 O2 . 2_555 2.294(8) yes
  Yb1 O3 . 2_555 2.269(18) yes
  Yb1 O3 . 1_555 3.409(18) yes
  Yb1 O1 . 3_555 2.231(6) no
  Yb1 Mn . 4_555 3.254(3) no
  Yb1 O2 . 4_555 2.294(9) no
  Yb1 O1 . 5_555 2.231(7) no
  Yb1 Mn . 6_555 3.254(3) no
  Yb1 O2 . 6_555 2.294(7) no
  Yb1 Yb2 . 7_545 3.5313(4) no
  Yb1 Yb2 . 7_555 3.5313(4) no
  Yb1 Yb2 . 7_655 3.5313(4) no
  Yb2 O1 . . 2.257(5) yes
  Yb2 O4 . . 2.401(10) yes
  Yb2 O4 . 10_555 3.277(10) yes
  Yb2 O2 . 2_545 2.270(8) yes
  Yb2 O1 . 3_545 2.257(6) no
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```

```

Mn O1 . . 1.867(7) yes
Mn O2 . . 1.868(7) yes
Mn O3 . . 2.039(4) yes
Mn O4 . . 2.034(4) yes
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O1 Yb1 O2 . . 4_555 162.9(3) no
O1 Yb1 O1 . . 5_555 90.9(2) no
O1 Yb1 O2 . . 6_555 77.23(17) no
O2 Yb1 O3 2_555 . 2_555 72.47(18) no
O1 Yb1 O2 3_555 . 2_555 77.2(3) no
O2 Yb1 O2 2_555 . 4_555 111.3(2) no
O1 Yb1 O2 5_555 . 2_555 162.9(2) no
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O2 Yb1 O3 4_555 . 2_555 72.47(18) no
O1 Yb1 O3 5_555 . 2_555 124.64(18) no
O2 Yb1 O3 6_555 . 2_555 72.47(17) no
O1 Yb1 O2 3_555 . 4_555 77.23(17) no
O1 Yb1 O1 3_555 . 5_555 90.9(2) no
O1 Yb1 O2 3_555 . 6_555 162.9(2) no
O1 Yb1 O2 5_555 . 4_555 77.2(2) no
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O1 Yb2 O2 3_545 . 4_655 169.1(2) no
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O2 Mn O3 . . . 87.2(6) no

```

O2 Mn O4 . . . 94.2(3) no
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O3 Mn O4 . . . 120.54(8) yes
O3 Mn O4 . . 7_655 120.54(18) no
O4 Mn O4 . . 7_655 118.62(19) yes
Yb1 O1 Yb2 . . . 103.8(2) no
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Mn O4 Mn . . 3_545 118.6(2) yes
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Mn O4 Mn 3_545 . 5_655 118.63(19) no