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# **Efficient Double- and Triple-Junction** Nonfullerene Organic Photovoltaics and **Design Guidelines for Optimal Cell** Performance

Yuliar Firdaus,\* Carr Hoi Yi Ho, Yuanbao Lin, Emre Yengel, Vincent M. Le Corre, Mohamad I. Nugraha, Emre Yarali, Franky So, and Thomas D. Anthopoulos\*

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Metrics & More

he advent of new nonfullerene acceptor (NFA)

(OPVs).<sup>1-4</sup> To increase the efficiency of OPVs further, the

absorption range of the photoactive materials is essential,

which in general can be achieved via two main approaches.

The first is to construct a binary or ternary single-junction (SJ)

device, where the active layer is composed of donor and

acceptor materials with complementary absorption.<sup>2-7</sup> Very

recently, a new electron-deficient-core-based fused ring NFA,

namely Y6,<sup>3</sup> with the features of a high electron mobility, longrange exciton diffusion length,<sup>8</sup> and broad absorption range up

to 930 nm was reported. When paired with polymer donor

PM6 (absorb up to 700 nm), the PM6:Y6-based OPVs

achieved a breakthrough in PCE of 15.7%.<sup>3</sup> Since then, the

PCE of SJ OPVs has reached over 18% using Y6 and its

or hybrid where two or more subcells with complementary

absorption spectra are connected in series.<sup>11-16</sup> Unfortunately, most of the reported tandem [double-junction (DJ)] OPVs currently exhibit PCEs below 15% (Table S1), with only a handful of values reaching >16%.<sup>13,17</sup> The same is true for

An alternative approach is to construct a multijunction OPV

molecules has led to a rapid increase in the power conversion efficiency (PCE) of organic photovoltaics



20

15

2012

6

2014

Article Recommendations

SUPPORTING Information

Efficient multi-junction OPVs

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Publication Year

2018

Double-junction

Triple-junction

2020

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2016



triple-junction (TJ) OPVs where only a few studies reported cells with PCE > 13% (Table S3).<sup>18,19</sup> One common technical challenge often associated with multijunction OPVs' performance limitations is the lack of efficient, wide-bandgap (optical bandgap,  $E_g > 1.7 \text{ eV}$ ) active-layers for the front cell.<sup>11,12,17,20</sup> This is because the field of NFA-based SJ OPVs has focused almost exclusively on the development of low bandgap materials (<1.5 eV),<sup>2,3,21,22</sup> while wide-bandgap NFAs have received significantly less attention.<sup>12,20</sup> However, it is not apparent which aspects of the wide-bandgap NFA still need to be improved. Moreover, the use of subcells with minimal absorption overlap is critical to achieving high-efficiency multijunction OPVs, which again has proven challenging to realize experimentally.<sup>23</sup> Thus, in order to improve the

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derivatives as the acceptor.<sup>4–7,9,10</sup>



Figure 1. (a) Chemical structure of active-layer (donor and acceptor) materials used. (b) Normalized absorbance of the photoactive blends used for the front-cell (FC) (PBDB-T:F-M) and the back-cell (BC) (PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM) of the double-junction (DJ) OPVs. The absorbance of the middle-cell (MC) (PM6:IT-4F) used in the TJ device (Figure 4) is also shown. (c) Energy levels of the donor and acceptor materials used in this work.<sup>2,3,17,20</sup>

performance of multijunction OPVs further, the factors limiting their performance need to be identified and addressed.

Here, we describe the development of efficient DJ and TJ OPVs while simultaneously drawing important cell-design rules to aid the development of higher-efficiency multijunction OPVs. First, we show that a DJ device with a high PCE of 16.5% can be obtained when PBDB-T:F-M and PTB7-Th:CO<sub>3</sub>8DFIC:PC<sub>71</sub>BM (full chemical names are given in the Supporting Information) are used as the front-cell (FC) and the back-cell (BC), respectively. For the interconnecting layer (ICL) we employ the recently reported PEDOT:PSS HTL Solar (HSolar) as the hole transport layer (HTL) and ZnO nanoparticle (NP) as the electron transport layer (ETL).<sup>13</sup> Second, we demonstrate TJ OPVs with PCE of 14.9%, one of the highest values reported to date. We achieved this using FC, middle-cell (MC), and BC with optical bandgaps of 1.75, 1.53, and 1.3 eV, respectively. Our modeling analyses show that one of the critical parameters for high performing DJs is the low bimolecular recombination in PBDB-T:F-M FC. We also find that the carrier mobility in PBDB-T:F-M FC ( $<10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>) limits the device performance and would need to be increased in order to achieve PCEs of >18%. Moreover, reducing the bimolecular recombination rate and the energy-loss in the back cell could boost the PCE to >19%. Our calculations also suggest that complementary absorption between the three subcells in the TJ device could be further optimized when bandgaps of 2, 1.57, and 1.2 eV for the FC, MC, and BC, respectively, are employed. This combined with an increase in the carrier mobilities to  $>10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> for all subcells is predicted to yield maximum PCE of >26%.

Figure 1a shows the chemical structures of the donor polymers and acceptors used as active materials in this work, while Figure 1b displays the absorbance of the donor and acceptor blend films. The PBDB-T:F-M blend absorbs strongly in the visible range between 450 and 710 nm, and the PM6:IT-4F blend absorbs in the range of 550–820 nm; the PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM blend absorbs in the spectral range of 550–1000 nm. Figure 1c depicts the corresponding energy levels of the materials used.

To fabricate DJ cells, PBDB-T:F-M BHJ<sup>20</sup> was used as the FC and combined with the near-infrared (NIR) absorbing PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM<sup>24</sup> BHJ as the BC. The two subcells were integrated to form two-terminal inverted DJ OPVs (Figure 2a) using solution processing,<sup>13</sup> except for the top MoO<sub>3</sub>/Ag electrode which was thermally evaporated. Further details on the cell fabrication can be found in the Supporting Information. The schematic energy diagram of each layer in the DJ is shown in Figure 2b, indicating the proper energy level alignment of each component in the device. The optimization of DJ OPVs was supported by optical and electrical simulation, the combination of which enabled us to predict the optimal active layer thicknesses of each subcell.<sup>12,25</sup> The MATLAB program combines optical transfer matrix modeling and the analysis of the measured current density-voltage (I-V) curves for the SI devices used as the subcells. First, the I-V curve of each SI device of different thicknesses is measured, and the current values for each J-Vcurve are normalized to the respective  $J_{SC}$ . Next, we use transfer matrix modeling and calculate the SJ quantum efficiency (QE) term to predict the  $J_{SC}$  of each subcell when incorporated in the DJ device. The predicted  $J_{SC}$  values for



Figure 2. (a) DJ solar cell device structure. (b) Energy diagram of each layer of the DJ device. Figures of merit of DJ solar cell devices predicted from optical-electrical modeling: (c)  $V_{OC}$ , (d) FF, (e)  $J_{SC}$ , and (f) PCE.

each subcell were then multiplied by their respective normalized SJ J-V curves to predict the complete J-Vcharacteristic of each subcell in the DJ OPV. Last, we apply Kirchhoff's laws to construct the overall I-V curve for the DJ OPV device.<sup>26</sup> Figure S1 provides the optical constant of the layers in the DJ cell and the measured I-V curves of PBDB-T:F-M and PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM-based SJ cells with different thicknesses. Figure 2c-f describes the modeling analyses, emphasizing the specific subcell thickness combinations amenable to the best DJ figure of merits. The model predicts that  $V_{\rm OC}$  and FF would decrease, whereas  $J_{\rm SC}$  would increase to >14 mAcm<sup>-2</sup> when the subcells' thicknesses increase (Figure 2c-e). PCE values in excess of 16% are predicted for various subcell thickness combinations, and particularly when an FC with thickness between 100 and 140 nm and a BC with a thickness in the range of 60-110 nm are utilized (Figure 2f). The model also predicts that DJ OPVs utilizing FCs and BCs with thicknesses of 125 and 85 nm, respectively, should yield the highest PCE of 16.7%.

DJ solar cells based on PBDB-T:F-M as the FC and PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM as the BC were constructed with optimal subcell thickness combinations chosen in the ranges established from the optical and electrical modeling analyses. Using a thickness combination of 130 nm for the FC and 100 nm for the BC, a DJ OPV with a maximum PCE of 16.5% (Figure 3a and Table 1) was obtained, a result consistent with the predicted PCE for this specific combination of subcell thicknesses. The experimental J-V curves for the constructed DJ OPVs and those predicted by the model are superimposed in Figure 3a, while the figures of merit of the corresponding DJ device are summarized in Table 1 for comparison. Optimized DJ cells exhibit an FF of 71.8%,  $V_{\rm OC}$  of 1.66 V, and a maximum  $J_{\rm SC}$  of 13.9 mA cm<sup>-2</sup>.

The box charts in Figure 3b present the statistical distribution of the various figure of merits of the DJ cells calculated from 30 devices. Evidently, the DJ OPVs show a small  $V_{\rm OC}$  variation of less than 0.01 V. On the other hand, the  $J_{\rm SC}$  varies between 13.6 and 14.3 mA cm<sup>-2</sup>, while FF shows a small variation of 1.28% between devices, which is believed to originate mainly from unintentional changes in active layer thickness in agreement with our simulations. The ensuing DJ OPVs yield PCE values of >16%, in agreement with the modeling predictions (Figure 2f). Overall, all devices show excellent performance with small PCE variation (average PCE = 16.3%). The efficiency enhancement factor of the DJ devices, defined as the percentage increase of PCE of the DJ cell from the more efficient SJ cell utilized, is nearly 30% (Table 1) and demonstrates the success of the approach.



Figure 3. (a) J-V curves of the DJ cells and PBDB-T:F-M, and PTB7-Th:CO<sub>1</sub>8DFIC:PC<sub>71</sub>BM SJ cells with their thicknesses optimized for the DJ cells. J-V curves of the DJ cells superimposed with that predicted from optical and electrical modeling (125 nm FC and a 85 nm BC). (b) Box charts of measured  $V_{OC'} J_{SC'}$  FF, and PCE of the DJ device (total number of devices is 30). (c) EQE of the optimized DJ solar cells. (d) Comparison of organic DJ PCEs reported from 2016 onward.<sup>12,13,17,18,20,24,27-55</sup> Details about the DJ cells from the literature are given in Table S1.

Table 1. Photovoltaic Parameters of Optimized SJs (with Respective Active-Layer Used As Subcells in DJ OPV) and DJ OPVs Obtained Experimentally (Exp) and from Simulations (Sim)<sup>a</sup>

cell type/BHJ	thickness (nm)	condition	$V_{\rm OC}$ (V)	$J_{\rm SC}~({\rm mA~cm^{-2}})$	FF (%)	PCE (%)		
PBDB-T:F-M SJ	130	average maximum	$0.98 \pm 0.004$ 0.99	$15.4 \pm 0.26$ 15.7	$71.7 \pm 0.95$ 73.1	$10.9 \pm 0.26$ 11.3		
PTB7-Th: CO <sub>i</sub> 8DFIC:PC <sub>71</sub> BM SJ	110	average	$0.71 \pm 0.003$	$25.5 \pm 0.37$	$70.4 \pm 0.68$	$12.7 \pm 0.17$		
DJ device (Exp)	130/100	average	$1.66 \pm 0.01$	$13.9 \pm 0.26$	71.0 $70.5 \pm 1.28$	15.1 $16.3 \pm 0.11$		
DJ device (Sim)	125/85	maximum	1.66 1.66	13.9 13.9	71.8 72.5	16.5 16.7		
<sup>a</sup> The deviation for each parameter was calculated from 30 devices.								

To better understand the origin of the improved cell performance, we performed EQE measurements. Optimized DJ devices (Figure 3c) show an average EQE of 67% in the absorption range from 300 to 1000 nm. The FC's EQE was also evaluated by exciting it with 850 nm light bias using an inorganic light-emitting diode (LED). The obtained EQE spectra show a strong response between 300 to 730 nm with a maximum EQE of 77% at around 570 nm. The BC's EQE (obtained by applying 595 nm light bias) absorbs mainly low energy photons in the range 700–1050 nm with a maximum EQE of  $\approx 64\%$ . The FC gave an integrated  $J_{\rm SC}$  of 13.8 mAcm<sup>-2</sup> closely matching the integrated  $J_{\rm SC}$  of 13.9 mAcm<sup>-2</sup> measured under simulated solar illumination (Table 1).

To compare our results with those found in the literature, we plotted all high PCE values reported for DJ OPVs from 2016 onward (Figure 3d).<sup>12,13,17,18,20,24,27–55</sup> Evidently, the maximum PCE of DJ OPVs developed here is among the highest values reported to date (details of the DJ cells found in

the literature are provided in Table S1). In particular, DJ OPVs with PCE of over 16% have been reported only twice before, one study by Meng et al. (PCE = 17.3%)<sup>17</sup> and our own recent study by Ho et al., (PCE of 16.1%),<sup>13</sup> with all three studies (including this work) relying on the use of PBDB-T:F-M for the FC. Previously, we showed that the PCE for DJ OPVs is maximized when the FC and BC's optical bandgap is in the range of 1.6-2.0 eV and 1.2-1.5 eV, respectively.<sup>11</sup> Therefore, PBDB-T:F-M cells offer attractive absorption spectrum as an FC (1.75 eV) yielding high  $J_{SC}$  and FF. The PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM- BC on the other hand has an  $E_g$  of ~1.3 eV and as such provides the required complementary absorption to PBDB-T:F-M, along with high  $J_{SC}$  and FF (Table 1).

Next, we examined the potential of TJ architecture as it offers additional opportunities to improve the  $V_{\rm OC}$ , which is important for various energy-related applications such as water splitting.<sup>25,62</sup> We fabricated TJ OPVs by employing PM6:IT-4F<sup>63</sup> as the MC and with the same FC and BC as those used in





Figure 4. (a) Triple-junction (TJ) solar cell device structure. (b) Energy diagram of each layer of the TJ device. (c) PCE of TJ cells predicted from combined optical and electrical modeling for subcells combination shown in Figure 4a. (d) J-V curves of measured TJ cell with an optimized thickness combination (75 nm front cell, a 110 nm MC, and a 60 nm back cell). J-V curves of the PBDB-T:F-M, PM6:IT-4F, PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM SJ are also shown (their respective thicknesses optimized for the TJ cells). (e) Comparison of organic TJ PCEs reported from 2013 onward.<sup>18,19,25,56-61</sup> Details about the TJ cells from the literature can be found in Table S3.

Table 2. Photovoltaic Parameters of	Optimized SI	s (with Res	pective Active-La	ver Used	as Subcells in T	I OPV)	and TJ OPVs"
		<b>`</b>		/			5

cell type/BHJ	thickness (nm)	condition	$V_{\rm OC}$ (V)	$J_{\rm SC}~({\rm mA~cm^{-2}})$	FF (%)	PCE (%)		
PBDB-T:F-M SJ	75	average	$1.00 \pm 0.002$	$12.5 \pm 0.07$	$74.5 \pm 1.33$	$9.4 \pm 0.22$		
		maximum	1.00	12.5	75.6	9.5		
PM6:IT-4F SJ	110	average	$0.83 \pm 0.008$	$18.8 \pm 0.51$	$74.5 \pm 0.63$	$11.7 \pm 0.25$		
		maximum	0.83	19.1	75.4	11.95		
PTB7-Th: CO <sub>i</sub> 8DFIC:PC <sub>71</sub> BM SJ	65	average	$0.71 \pm 0.005$	$22.5 \pm 0.81$	$69.3 \pm 2.06$	$11.1 \pm 0.29$		
		maximum	0.71	23.2	71.0	11.7		
TJ device (Exp)	75/110/65	average	$2.49 \pm 0.015$	$8.1 \pm 0.24$	$70.5 \pm 1.21$	$14.2 \pm 0.34$		
		maximum	2.49	8.4	70.8	14.9		
TJ device (Sim)	80/110/60		2.54	8.2	71.3	14.9		
<sup>a</sup> From experiment (Exp) and simulation (Sim). Device statistics from 15 devices.								

the DJ OPVs previously. We chose the PM6:IT-4F BHJ ( $E_{\sigma}$ : 1.53 eV) as it provides complementary absorption with the two other subcells (Figure 1b). Figure 4a illustrates the TJ device configuration using the same HSolar/ZnO NP ICL between the three subcells. The schematic energy diagram of each layer in the TJ is shown in Figure 4b. Following the same approach as depicted for the DJ solar cells, we first examined the expected performance of the TJ devices using combined optical and electrical modeling (Figure 4c). Figure S2a,b provides the optical constant of the PM6:IT-4F and the measured J-V curves of PM6:IT-4F-based SJ cells with different thicknesses. The model predicts PCEs as high as 14.9% for a TJ device composed of an 80 nm FC, a 110 nm MC, and a 60 nm BC. The EQEs of the PBDB-T:F-M, PM6:IT-4F, and PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM-based SJ devices at those respective thicknesses are shown in Figure S2c. We then constructed the corresponding TJ device, demonstrating a champion device with FF = 70.8%,  $J_{SC}$  = 8.4 mAcm<sup>-2</sup>,  $V_{\rm OC}$  = 2.49 V, and a superb PCE of 14.9% (Figure 4d), in good agreement with our simulation (Table 2). The PCE is the highest achieved to date with a TJ OPV

(Figure 4e).<sup>18,19,25,56–61</sup> As depicted in Figure 4d, the TJ solar cells also yield remarkably high operating voltages ( $V_{\text{Pmax}}$ ) of 2.1 V; defined as the voltage at the maximum power point ( $J_{\text{Pmax}} \approx 7 \text{ mA cm}^{-2}$ ).

To examine the key factors that limit the performance of the DJ OPV, we performed drift-diffusion simulations (Setfos 4.6, FLUXIM AG)<sup>11,12,64,65</sup> for the PBDB-T:F-M and ternary PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM SJ cells. The simulation describes charge transport and recombination with the latter following a reduced Langevin recombination given by<sup>12,66</sup>

$$k_{\rm BMR} = \gamma_{\rm pre} k_{\rm L} = \gamma_{\rm pre} \frac{q}{\varepsilon_{\rm r} \varepsilon_0} (\mu_{\rm h} + \mu_{\rm e}) \tag{1}$$

Here,  $\gamma_{\rm pre}$  is the recombination prefactor,  $k_{\rm L}$  is the Langevin recombination,  $\varepsilon_{\rm r}\varepsilon_0$  is the material dielectric constant, and  $\mu_{\rm h}/\mu_{\rm e}$  are the hole/electron mobilities. Details about the simulation can be found in the Supporting Information.

We simulated PBDB-T:F-M, PBDB-T:IDTTA, and the ternary PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM SJ cells of different thicknesses using a value of  $k_{\text{BMR}}$  (eq 1) and the appropriate space charge limited current (SCLC) charge-carrier mobilities



Figure 5. Experimentally measured (symbol) and simulated (solid line) fill-factor (FF) and short-circuit current density  $(J_{SC})$  versus activelayer thickness for (a) PTB7-Th:CO<sub>1</sub>8DFIC:PC<sub>71</sub>BM and (b) PBDB-T:F-M BHJ solar cells. The legends in both figures show the corresponding bimolecular recombination rate employed in the simulation. The input parameters used for the simulation can be found in Table S2.

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DJ Design Rule <sup>a</sup>									
case	$e \qquad E_{\rm CT} \ ({\rm eV})$	$k_{\rm BMR,FC}~({\rm cm}^3~{\rm s}^{-1})$	$k_{\rm BMR,BC}$	$\mu_{\rm FC} (\mu_{\rm h} = \mu_{\rm e}) (\rm cm^2 V^{-1} s^{-1})$	$V_{\rm OC}$ (V)	$J_{\rm SC}~({\rm mAcm}^{-2})$	FF (%)	PCE (%)	
1. FC/	BC1 1.57/1.30	10 <sup>-12</sup>	$4 \times 10^{-12}$	$2 \times 10^{-4}$	1.67	13.1	77	16.9	
				$5 \times 10^{-4}$	1.67	13.5	80	18.1	
				$1 \times 10^{-3}$	1.67	13.5	82	18.5	
				$2 \times 10^{-3}$	1.67	13.5	83	18.8	
				$5 \times 10^{-3}$	1.66	13.5	84	18.9	
2. FC/	BC1 1.57/1.30	10 <sup>-12</sup>	$10^{-12}$	$2 \times 10^{-4}$	1.70	13.5	77	17.6	
				$5 \times 10^{-4}$	1.70	13.6	82	18.9	
				$1 \times 10^{-3}$	1.70	13.6	84	19.4	
				$2 \times 10^{-3}$	1.70	13.6	85	19.7	
				$5 \times 10^{-3}$	1.70	13.6	86	19.8	
3. FC/	BC2 1.57/1.40	10 <sup>-12</sup>	$10^{-12}$	$2 \times 10^{-4}$	1.70	13.8	77	18.9	
				$5 \times 10^{-4}$	1.70	13.8	82	20.3	
				$1 \times 10^{-3}$	1.70	13.8	84	20.9	
				$2 \times 10^{-3}$	1.70	13.8	85	21.2	
				$5 \times 10^{-3}$	1.70	13.8	86	21.4	
TJ Design Rule <sup>b</sup>									
case	$E_{\rm CT}$ [FC/MC/BC] (eV	$\mu_{\rm h} = \mu_{\rm e}  \left( {\rm cm}^2  {\rm V}^2 \right)$	$^{-1} s^{-1}$ ) IQ	$ (\%) \qquad th_{\rm FC}/th_{\rm MC}/th_{\rm BC}{}^c \ ({\rm nm}) $	$V_{\rm OC}$ (V)	$J_{\rm SC}~({\rm mAcm^{-2}})$	FF (%)	PCE (%)	
1	1.95/1.52/1.25	$5 \times 10^{-4}$		90 100/80/65	3.03	9.0	88	23.9	
2	1.95/1.52/1.15	$5 \times 10^{-4}$		90 130/110/65	2.90	9.6	87	24.1	
3	1.95/1.41/1.25	$5 \times 10^{-4}$		90 100/80/65	2.92	8.4	89	21.8	
4	1.95/1.41/1.15	$5 \times 10^{-4}$		90 190/80/95	2.79	10.0	84	23.4	
5	1.65/1.52/1.25	$5 \times 10^{-4}$		90 100/110/65	2.73	8.1	87	19.4	
6	1.65/1.52/1.15	$5 \times 10^{-4}$		90 100/110/65	2.61	8.3	88	19.2	
7	1.65/1.41/1.25	$5 \times 10^{-4}$		90 100/80/65	2.63	7.9	87	18.0	
8	1.65/1.41/1.15	$5 \times 10^{-4}$		90 100/110/95	2.50	9.1	86	19.7	
9	1.95/1.52/1.25	10 <sup>-3</sup>		95 100/80/65	3.04	9.5	89	25.7	
10	1.95/1.52/1.15	10 <sup>-3</sup>		95 130/110/95	2.90	10.2	88	26.0	
a Additio	nal DI simulation nar	amatara, charga mah	ilitar for all h	a alt call in DI simulation. 4 – 4	$6 \times 10^{-4} \text{ cm}^2$	$V^{-1} = 1 = 0$	$10^{-4}$ cm <sup>2</sup> V	-1 -1. IOE	

"Additional DJ simulation parameters: charge mobility for all back-cell in DJ simulation:  $\mu_h = 6 \times 10^{-4} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ ,  $\mu_e = 5 \times 10^{-4} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ ; IQE for all subcells = 90%;  $E_{\text{CT}}$ , charge-transfer state energy. <sup>b</sup>Additional TJ device simulation:  $E_{\text{CT}} = E_g - 0.05 \text{ eV}$ ;  $k_{\text{BMR}} = 10^{-12} \text{ cm}^3 \text{ s}^{-1}$ ; charge mobilities of FC, MC, and BC are the same. <sup>c</sup>th: thicknesses of the subcells.

from Table S2. Only one fit parameter,  $\gamma_{\rm pre}$ , was used to simulate a wide variety of experimental devices with FF varying from 60% to 75%. We obtained an excellent agreement between the experimental and simulated FF and  $J_{\rm SC}$  for the ternary PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM device for different BHJ thicknesses when a recombination prefactor ( $\gamma_{\rm pre} = k_{\rm BMR}/k_{\rm L}$ ) of 0.007 and a  $k_{\rm L}$  value of 6.1 × 10<sup>-10</sup> cm<sup>3</sup> s<sup>-1</sup> were used as fitting parameters (Table S2).

The relatively high charge mobility (Table S2) and low  $\gamma_{\text{pre}}$  explain why the FFs of the ternary devices are high (>65%) for

a wide range of active layer thicknesses up to 200 nm (Figure 5a). Similar analyses performed on PBDB-T:F-M cells show that the FFs are >65% when the active layer thicknesses are <180 nm (Figure 5b). We attribute this to the low  $\gamma_{\rm pre}$  value of the cell (0.005), although the electron mobility is low too (<10<sup>-4</sup> cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>). For comparison, another wide bandgap PBDB-T:IDTTA blend reported recently exhibits comparable charge transport but higher  $\gamma_{\rm pre}$  (0.016) that leads to lower FF (Figure S3a).<sup>12</sup> The  $\gamma_{\rm pre}$  value of the PBDB-T:IDTTA device obtained from the modeling analyses is in excellent agreement

with the  $\gamma_{\rm pre}$  value inferred from the transport and recombination analyses.<sup>12,66</sup> Because of its lower FF, the DJ utilizing PBDB-T:IDTTA as the FC yields a maximum PCE of 15%.

Given the above analysis, the high FF and PCE of DJ OPV can be achieved because of the low  $\gamma_{pre}$  of devices. However, we also notice that the electron mobility of PBDB-T:F-M BHJ is only  $\sim 10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>, which limits the PCE of the DJ cells. To verify this hypothesis we calculated the PCE of the DJ following our previous approach,<sup>11</sup> which is similar to the analysis described for Figure 2c-f. In brief, the J-V curve of each individual subcell was simulated using the numerical simulator Setfos 4.4 and subsequently combined with transfer matrix modeling (MATLAB) to construct the J-V curve of the DJ device. Figure S3b shows the extinction coefficients of the FC and BC used in the simulation and inferred from ellipsometry measurements. The FC's absorption is based on PBDB-T:F-M blend absorption, whereas the BC absorption is based on different blends (BC1, ternary PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM; BC2, PM6:Y6). The specific BC absorption profiles were chosen because they provide complementary absorption to the PBDB-T:F-M-based FC. For a DJ cell with absorption profiles of FC/BC1 (case 1), and assuming different  $\mu_{\rm h,e}$  and  $k_{\rm BMR}$  (Table 3), the PCE is predicted to increase to 18.1% and 18.9% if the FC carrier mobility increases to  $5 \times 10^{-4}$  and  $5 \times 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>, respectively (Table 3 and Figure S3c;  $J_{SC}$ ,  $V_{OC}$ , and FF plots are also shown in Figure S3d-f). Reducing the  $k_{BMR}$  further to  $10^{-12}$  cm<sup>3</sup> s<sup>-1</sup> (case 2), leads to a DJ cell with PCE of nearly 20%. To this end, owing to the recent development of Y6 NFA<sup>3</sup> and its derivatives,  $^{10,21,22}$  high PCEs > 18% have been reported with very low energy loss for OPV ( $E_{loss} \approx 0.5 \text{ eV}$ ;<sup>4,10</sup> energy loss in OPV is typically between 0.7 and 1 eV),<sup>67</sup> which makes it appealing as a BC in the DJ-OPVs. For comparison, the PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM blend which has a similar  $E_g$  with PM6:Y6 exhibits higher energy loss of ~0.6 V. Our simulation predicts (Table 3) that DJ devices composed of BC with similar absorption profile to Y6-based blend (BC2, case 3) and with low energy loss ( $\sim 0.5 \text{ eV}$ ) could potentially reach higher PCEs of >21%. We also note that our previous calculations show that PCEs of >25% can also be achieved by DJ OPV cells by further optimizing the subcells' optical bandgap, increasing the charge mobilities ( $\geq 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>), and further lowering  $k_{\text{BMR}}$  (10<sup>-12</sup> cm<sup>3</sup> s<sup>-1</sup>).<sup>11</sup>

We note that neither predicted nor experimental results indicate that the TJ device can be amenable to PCEs higher than those of the DJ solar cells probably because of the large absorption overlaps between the subcells. Because of this, the  $J_{\rm SC}$  of the TJ device (8.4 mAcm<sup>-2</sup>) significantly drops compared to the respective SJ device with the lowest  $J_{SC}$ (12.5 mAcm<sup>-2</sup>, Table 2). To better understand the optimal subcell bandgap combinations and the practical efficiency limits of TJ OPVs, we combined the optical transfer matrix modeling with drift-diffusion electrical modeling. As shown in Figure S4a, the absorption profiles of the BHJs used for the FC, MC, and BC were chosen to be complementary with their bandgaps ranging from 1.2 to 2 eV. Specifically, their bandgaps were set as 2 or 1.7 eV (for FC), 1.57 or 1.46 eV (for MC), and 1.3 or 1.2 eV (for BC), respectively. Similar to our previous calculation,<sup>11</sup> we assume that the charge-transfer energy  $(E_{\rm CT})$  values used to account for the  $V_{\rm OC}$  in our simulation follow the relation  $E_{CT} = E_g - 0.05$  eV (see Table 3). The results presented in Figure S4b,c and summarized in

**Table 3** indicate that high PCE values of up to 24% (case 2:  $\mu_h = \mu_e = 5 \times 10^{-4} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  and IQE = 90%) and up to 26% (case 10:  $\mu_h = \mu_e = 10^{-3} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  and IQE = 95%) can be achieved when FC, MC, and BC with optical bandgaps of 2, 1.57, and 1.2 eV are used (Table 3) and assuming a  $k_{\text{BMR}}$  of  $10^{-12} \text{ cm}^3 \text{ s}^{-1}$ . The aforementioned PCE values were calculated assuming no losses from series and shunt resistance, which results in a high FF of up to 89%. If the effect of these parasitic resistances is considered and assuming an FF of 81% (currently achievable for OPVs^{21,68}), the predicted PCE of the TJ OPV becomes 22.4% and 23.9% for cases 2 and 10, respectively.

The optimum subcell's thicknesses and simulated results for different subcell bandgap combinations are also shown in Table 3. The simulated PCE is 19.4% ( $J_{SC} = 8.13 \text{ mAcm}^{-2}$ ) for FC/MC/BC bandgap combination of 1.7/1.57/1.3 eV (Table 3, case 5,  $\mu_{\rm h} = \mu_{\rm e} = 5 \times 10^{-4} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ ). The PCE increases significantly to 24.1% ( $J_{SC} = 9.6 \text{ mAcm}^{-2}$ ) if the FC's bandgap is increased to 2 eV while that of the BC's is reduced to 1.2 eV (case 2), further highlighting the need to reduce the absorption overlap between subcells. Importantly, we note that efficient NFA-based OPVs that combine a bandgap of >1.7 eV with electron mobility of  $>10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> are scarce, as can clearly be seen in Figure S5 where we plot the  $\mu_e$  versus the optical bandgap of NFAs-based BHJs reported to date in the literature. This is an important observation that highlights the need for developing wider bandgap organic BHJs, particularly for use in multijunction OPVs.

In summary, we have developed DJ NFA-based OPVs with a maximum PCE of 16.5% in excellent agreement with our theoretical predictions. The high efficiency along with the excellent  $V_{\rm OC}$  (1.66 V), high  $J_{\rm SC}$  (13.9 mAcm<sup>-2</sup>), and good FF (71.8%) positions our devices among the best-performing DJ OPVs reported to date.<sup>13,17</sup> Going a step further, we developed TJ OPVs utilizing PBDB-T:F-M as the FC, PM6:IT-4F as the MC, and PTB7-Th:CO<sub>i</sub>8DFIC:PC<sub>71</sub>BM as the BC. Optimized cells yielded a PCE of 14.9%; a high  $V_{\rm OC}$  of 2.49 V; a  $J_{\rm SC}$  of 8.42 mA cm<sup>-2</sup>; and a remarkable, for a TJ OPV, FF of 71%. Our device modeling suggests three design rules that can aid further development of high-performance multijunction OPV devices:

- (i) Increasing the carrier mobilities of the active-layer used as FC to ≥5 × 10<sup>-4</sup> cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> is needed to boost the DJ and TJ OPVs performance further.
- (ii) Strong absorption overlap in TJ devices remains a major issue, and minimizing the photon competition between subcells is required to increase the performance of TJ OPVs further (e.g., calculated optimal optical bandgaps are 2, 1.57, and 1.2 eV for FC, MC, and BC, respectively).
- (iii) TJ OPVs have the potential to reach PCE values up to 26% by increasing the carrier mobilities to  $>10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> while simultaneously reducing  $k_{\rm BMR}$  to  $10^{-12}$  cm<sup>3</sup> s<sup>-1</sup> for all subcells. Newly developed approaches, such as molecular doping of the BHJ,<sup>9</sup> could help achieve this target.

The present study provides important insights into cell design aspects while highlighting practical guidelines for the development of next-generation multijunction NFA-based OPVs.

## ACS Energy Letters

### ASSOCIATED CONTENT

## **Supporting Information**

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsenergylett.0c02077.

Materials, device fabrication, characterization and simulation details; optical constant and J-V of single-cells used for simulation; double-junction OPV devices reported in the last five years; measured and simulated FF and  $J_{SC}$  of PBDB-T:IDTTA devices for different thicknesses; input parameters used for simulations; triple-junction simulation; and electron mobility of nonfullerene-based devices versus energy bandgap from the literature (PDF)

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#### Notes

The authors declare no competing financial interest.

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