



## **Volatile fatty acid production from saline cooked mussel processing wastewater at low pH**

Andrea Fra-Vázquez, Alba Pedrouso, Ángeles Val del Río, Anuska Mosquera-Corral

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3 cooked mussel processing wastewater at low  
4 pH

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6 *Andrea Fra-Vázquez, Alba Pedrouso\*, Angeles Val del Río and Anuska Mosquera-*

7 *Corral*

8 CRETUS Institute, Department of Chemical Engineering, Universidade de Santiago de

9 Compostela, Rua Lope Gomez de Marzoa, s/n, Campus Vida, E-15782, Santiago de

10 Compostela, Galicia, Spain.

11

12 \* Corresponding author: [alba.pedrouso@usc.es](mailto:alba.pedrouso@usc.es), Tel.: +34 881816779.

13

14 **ABSTRACT**

15 The production of VFA using as substrate the wastewater produced in a cooked

16 mussel processing factory, containing large COD ( $13.7 \pm 3.2$  g COD/L) and salt

17 concentrations ( $21.8 \pm 2.8$  g NaCl/L) and characterized by low pH ( $4.6 \pm 0.6$ ) was

18 evaluated. This wastewater was fed to a 5-L completely stirred tank reactor operated

19 in continuous mode. The conversion efficiency of its COD content into volatile fatty

20 acids (VFA) was evaluated. The maximum acidification of 43 % (total VFA on

21 soluble COD basis) was obtained when an organic loading rate of  $2.5 \pm 0.4$  g

22 COD/(L·d) was applied to the reactor and corresponded to a VFA volumetric

23 productivity of  $0.72 \pm 0.07$  g COD<sub>VFA</sub>/(L·d). Under steady-state conditions, the  
24 obtained mixture of VFA was composed by 80:18:2 as acetic:propionic:butyric acids  
25 (percentage of VFA on soluble COD basis). Carbohydrates were degraded up to 96 %  
26 while protein fermentation did not take place, probably due to the low pH value,  
27 limiting the maximum acidification of the wastewater. Batch experiments showed that  
28 the increase of the pH from 4.2 to 4.9 by the addition of NaHCO<sub>3</sub> resulted in the  
29 improvement of the acidification and changed the VFA mixture composition. Thus,  
30 this study demonstrates the opportunity of using complex substrates, as cooked mussel  
31 processing wastewater, to produce rich-VFA streams under unfavorable operational  
32 conditions, such as high salinity and low pH.

33 **Keywords:** Anaerobic fermentation; Biorefinery; Industrial wastewater; Protein  
34 degradation; Salinity; VFA.

35

36

## 37 **1. INTRODUCTION**

38 The fish and seafood canning industry is a crucial economic sector in Galicia (North-West of  
39 Spain) which nowadays amounts to 67 % and 80 % of the European and Spanish production,  
40 respectively (FAO, 2019). Indeed, Galicia is the third producer worldwide just after Thailand  
41 and China. More specifically, mussels are one of the most popularly consumed seafood, and  
42 Galicia represents 50 % of the worldwide production (OPMEGA, 2020). This industrial sector  
43 consumes an enormous amount of water, either freshwater and/or seawater, which on average is  
44 above 10 m<sup>3</sup>/tonne of raw mussel processed. As a consequence similar large volumes of highly  
45 polluted wastewater are generated (Bello Bugallo et al., 2012). The main environmental  
46 problem associated with this produced wastewater relates to the high organic matter (up to 42  
47 g/L), comprising proteins (15 - 20 % of wet weight) (Tay et al., 2005), and salt concentrations  
48 that could reach values over 20 g NaCl/L (Méndez et al., 1992). The discharge to the  
49 environment of these streams without appropriate treatment could provoke continual oxygen  
50 depletion, due to the contained organic matter, which causes the death of the aquatic life.  
51 Furthermore, the discharge of nitrogen from proteins favours algae overgrowth leading to the  
52 eutrophication of the receiving water body. In addition, if salty wastewater is not withdrawn  
53 directly into the sea but to freshwater water bodies is responsible for the increase of salinity of  
54 these ecosystems, similarly if it is treated in municipal wastewater treatment plants that  
55 discharge in interior areas.

56 The treatment of the fish and seafood processing wastewater is particularly challenging due to  
57 its complex characteristics (high organic matter and salt concentrations). In addition, the  
58 seasonal activity of the factories and the fact that they commonly process different products  
59 within one single week involves the generation of wastewater streams with different  
60 composition in the same facility. The wastewater characteristics depend on the processing step  
61 where it was generated: preliminary operations (reception, washing, brining, cutting...),  
62 processing (cooking, canning and trimming), final operations (sealing and sterilization) or  
63 auxiliary operations such as steam generation (Carrera et al., 2019; Cristóvão et al., 2016;  
64 Méndez et al., 1992). For example, a high volume of diluted washing wastewater is generated

65 while the volume of cooking process wastewater is highly polluted is low. Nevertheless, the  
66 different generated wastewater types are usually treated together after being homogenized in a  
67 tank (Cristóvão et al., 2016). The most common technologies applied for the treatment of fish  
68 and seafood processing wastewater are based on physical-chemical (membrane separation,  
69 chemical destabilization and electrochemical methods) and biological (anaerobic and aerobic)  
70 processes (Carrera et al., 2019; Cristóvão et al., 2012). Biological processes enable the recovery  
71 of resources from wastewater especially when the valorized stream contains large  
72 concentrations of organic matter, as it is the case of the fish and seafood canning processing  
73 wastewater attracting great interest.

74 Anaerobic digestion is suggested as a suitable treatment for seafood wastewater due to its high  
75 organic matter removal capacity, low energy consumption, low sludge production and energy  
76 production as biogas (mainly CH<sub>4</sub> and CO<sub>2</sub>) (Chowdhury et al., 2010). Anaerobic processes  
77 with high removal efficiencies (55 - 97 %) and treating organic loads of 1 - 4 kg COD/(m<sup>3</sup>·d)  
78 have been applied to treat these effluents (Méndez et al., 1992; Panpong et al., 2014; Prasertsan  
79 et al., 1994; Sillapacharoenkul and Sinbuathong, 2020). In the frame of the circular economy,  
80 the waste conversion into volatile fatty acids (VFA), which are short-chain fatty acids obtained  
81 as metabolic intermediates in the anaerobic digestion, has recently gained attention due to their  
82 wide variety of applications (Kleerebezem et al., 2015). VFA are intermediate products of the  
83 anaerobic digestion process. Thus, VFA-rich streams are produced in fermentation processes  
84 where the methanogenic step is suppressed (Wainaina et al., 2019). Application alternatives of  
85 the waste-derived VFA are the generation of biofuels, bulk chemicals, the biological removal of  
86 nutrients from wastewater and the production of bioplastics or food additives. For example,  
87 VFA can be used as a carbon source during the denitrification or the biological phosphorus  
88 removal processes. VFA act also as substrate in the production of polyhydroxyalkanoates  
89 (PHA), a type of bioplastic, by mixed microbial cultures (Atasoy et al., 2018; Wainaina et al.,  
90 2019).

91 Operational conditions of the anaerobic systems significantly influence the concentration, yield  
92 and composition of the VFA produced from wastes. Organic acid production is strongly

93 affected by the pH of the reaction media since it has a great influence on the growth rate of the  
94 microorganisms involved in the anaerobic digestion (Wainaina et al., 2019). Indeed, methane  
95 production is barely observed out of its optimal pH range (6.5 - 8.5). Nevertheless, hydrolytic  
96 and acidogenic microorganisms operate at an optimal pH range of 5 - 11 and cannot survive in  
97 extremely acidic (pH 3) or alkaline (pH 12) conditions (Jankowska et al., 2015; Wainaina et al.,  
98 2019). The optimal pH to maximize the acidification efficiency varies according to the waste  
99 characteristics and the operational conditions. Jankowska et al. (2015) observed that, in  
100 unbuffered systems, acidic pH promoted the VFA production at short retention time (5 days)  
101 while alkaline pH (10 - 11) maximized VFA accumulation at longer retention times (15 days).  
102 Wainaina et al. (2019) stated that acidic pH is suitable to produce VFA from a variety of easily  
103 degradable wastes while alkaline pH values are recommended when complex substrates are  
104 used. For example, different optimal pH values to obtain VFA were reported: from cheese whey  
105 is 5.2 - 5.5 (Bengtsson et al., 2008), from food waste and the organic fraction of municipal solid  
106 waste is 9.0 (Cheah et al., 2019; Moretto et al., 2019), from kitchen waste is 7.0 (Zhang et al.,  
107 2005) and from wasted activated sludge ranges from 9.5 to 11.0 (Chen et al., 2007; Liu et al.,  
108 2020).

109 Since most cooked mussel processing factories use seawater in their processes, another primary  
110 concern with the produced wastewater is its high salinity (Xiao and Roberts, 2010). Significant  
111 salt concentrations can inhibit the anaerobic processes, especially the methanogenesis step at  
112 concentrations above 10 g NaCl/L (Panpong et al., 2015). However, the adaptation of the  
113 anaerobic biomass to high salt concentrations (Artiga et al., 2008; Sudmalis et al., 2018; Zhang  
114 et al., 2017), or the use of halophilic inoculum (Aspé et al., 1997; Scoma et al., 2017; Tan et al.,  
115 2019) are suitable strategies to develop an anaerobic treatment process for saline wastewater.

116 The purpose of this study was to evaluate the suitability of the wastewater generated in a cooked  
117 mussel processing factory as feedstock to produce a VFA-rich effluent, with the novelty of  
118 operating the continuous acidifying reactor at very low pH and high salt concentration. Batch  
119 experiments were also performed to investigate the effect of the pH on the productivity and  
120 composition of the produced VFA.

## 121 2. MATERIALS AND METHODS

### 122 2.1 Cooked mussel processing wastewater characterization

123 The wastewater used in the present study was taken directly from the cookers of a mussel  
124 processing factory (Cocedero Suárez, Vilanova de Arousa, Spain). The pH of the mussel  
125 cooking wastewater at the time of the collection was approximately 7 but it dropped to 4 - 5  
126 (Table 1) after a couple of days stored at 4 °C. Wastewater was stored at low temperature to  
127 prevent the degradation of the organic matter. Carbohydrates were the predominant organic  
128 compounds (50 % of the soluble COD), followed by proteins (30 % of the soluble COD). The  
129 concentration of proteins and carbohydrates as chemical oxygen demand (COD) was calculated  
130 using the following factors: 1.5 g COD<sub>protein</sub>/g protein and 1.1 g COD<sub>carbohydrates</sub>/g carbohydrate  
131 (Mahmoud et al., 2004). The lipid concentration was not significant. The wastewater  
132 composition fluctuated due to changes in the factory process, and its variability defined the  
133 three operational stages carried out in the acidification reactor, as indicated in Table 1.

134

135 **Table 1.** Average values of the main characteristic parameters of the wastewater treated and  
136 reactor operational conditions.

Parameters	Units	Stage I	Stage II	Stage III
		0 - 59 days	60 – 279 days	280 - 400 days
OLR	g COD/(L·d)	7.3 ± 0.5	2.6 ± 0.4	2.2 ± 0.2
HRT	d	3.1	6.3	6.3
pH	--	4.7 ± 0.4	4.4 ± 0.5	5.1 ± 0.7
sCOD	g/L	18.3 ± 1.3	13.1 ± 0.4	11.1 ± 1.1
Carbohydrates	g/L	ND	5.5 ± 1.6	5.3 ± 1.3
Proteins	g/L	ND	2.8 ± 0.4	1.7 ± 0.2
VFA	g COD <sub>VFA</sub> /L	0.7 ± 0.3	2.2 ± 1.3	1.7 ± 0.7
Ammonium	g NH <sub>4</sub> <sup>+</sup> -N/L	0.09 ± 0.02	0.19 ± 0.06	0.19 ± 0.05
NaCl	g/L	19.1 ± 2.1	22.7 ± 2.4	22.1 ± 3.0

137 OLR: organic loading rate; HRT: hydraulic retention time; COD: chemical oxygen demand; VFA: volatile  
138 fatty acids; ND: Not determined.

139

## 140 **2.2 Experimental set-up**

### 141 *2.2.1 Continuous reactor for VFA production*

142 A continuous stirred tank reactor with a working volume of 5 L was used to produce VFA. It  
143 was directly fed with raw cooked mussel processing wastewater (Table 1). The temperature was  
144 maintained in the mesophilic range ( $37 \pm 1$  °C) using a thermostatic bath (Techne Inc., USA).  
145 The reactor was inoculated with anaerobic granular sludge from a pilot-scale up-flow anaerobic  
146 sludge blanket (UASB) reactor that treated mimicked municipal wastewater (Silva-Teira et al.,  
147 2017). Short solid retention times (SRT) were imposed to washout the methanogenic  
148 microorganisms from the anaerobic mixed culture as they present growth rates lower than the  
149 acidogenic bacteria (Khan et al., 2016). The gas-phase composition was measured during the  
150 first days of Stage I to check the absence of methane production due to the inhibition of  
151 methanogenic microorganisms.

152 The operation of the reactor lasted 400 days, divided into three different stages (Table 1).  
153 During Stage I (the first 59 days) an organic loading rate (OLR) of  $7.3 \pm 0.5$  g COD/(L·d) was  
154 applied, with a hydraulic retention time (HRT) of 3.1 days. Then in Stage II (days 60 to 279),  
155 the OLR was diminished to  $2.6 \pm 0.4$  g COD/(L·d) by increasing the HRT to 6.3 days. Finally,  
156 the OLR was further decreased in Stage III (days 280-400) to  $2.2 \pm 0.2$  g COD/(L·d) while HRT  
157 was maintained. The SBR operated under complete mixing conditions by means of the action of  
158 a mechanical stirrer at 120 rpm (Heidolph, Germany); therefore, the SRT was equal to the HRT.  
159 The pH of the media was not controlled.

160

### 161 *2.2.2 Acidification batch tests*

162 The acidification batch assays were carried out in 500 mL Pirex-glass bottles (400 mL of  
163 working volume), following the methodology described by Silva et al. (2013). The bottles were  
164 filled in with the corresponding volumes of substrate, macro- and micro-nutrients solutions and  
165 acidifying biomass from the continuous acidification reactor (Table 2). The substrate  
166 composition corresponded to Stage I of Table 1. The substrate to biomass ratio was set at 3 g  
167 COD/g VSS.



168 In total, 6 bottles were prepared with 3 different conditions (duplicates): two as control  
 169 experiments without inoculum addition for measuring the abiotic disappearance of the substrate  
 170 (E1); two without alkalinity addition (E2) and two containing NaHCO<sub>3</sub> in a ratio of 1:1 with  
 171 respect to VSS (E3). After the addition of the substrate, biomass and medium, the headspace of  
 172 each vial was bubbled with N<sub>2</sub> and the bottles were sealed with rubber stoppers and capped with  
 173 plastic seals. Then, bottles were incubated in a shaker (120 rpm) at 37 °C. VFA production was  
 174 monitored throughout time by the analysis of the periodically collected samples from the liquid  
 175 phase of each bottle. Before collecting these liquid samples, 1 mL-gas sample was taken and  
 176 measured by gas chromatography (Hewlett Packard 5890 Series II instrument) to assess the  
 177 occurrence of methane production. The evolution of the concentration of VFA (expressed as g  
 178 COD<sub>VFA</sub>/L) versus time was plotted. The specific acidogenic activity (g COD<sub>VFA</sub>/(g VSS·d))  
 179 was estimated as the ratio between the maximum slope of the appearance of VFA (g  
 180 COD<sub>VFA</sub>/(L·d)) and the concentration of biomass present in the bottles (g VSS/L).

181 **Table 2.** Initial operational conditions of the acidification batch experiments.

Volumes added of different compounds	Experiment		
	Control (E1)	No alkalinity (E2)	Alkalinity (E3)
Acidifying sludge (mL)	0	23	23
Wastewater (mL)	61.2	61.2	61.2
Macronutrients solution (mL)*	66	66	66
Micronutrients solution (mL)*	13	13	13
10 g NaHCO <sub>3</sub> /L solution (mL)	0	0	28

182 \*Compositions of macro- and micronutrient solutions described in Silva et al. (2013).

183

### 184 2.3 Analytical methods

185 Total suspended solids (TSS), volatile suspended solids (VSS), alkalinity and COD were  
 186 analysed according to *Standard Methods for the Examination of Water and Wastewater*  
 187 (APHA-AWWA-WEF, 2017). Liquid samples were filtered through a cellulose-ester filter of  
 188 0.45 µm of pore size (Advantec, Japan) for the quantification of total organic carbon (TOC),

189 ammonium ( $\text{NH}_4^+$ ), soluble chemical oxygen demand (sCOD), proteins, carbohydrates, VFA  
190 and other ions to determine salt concentration. Ammonium concentration was determined  
191 according to the Bower and Holm-Hansen method (Bower and Holm-Hansen, 1980). TOC  
192 concentration was determined by catalytic combustion (Analyser model TOC-L CSN,  
193 Shimadzu, Japan). VFA concentration was determined by gas chromatography (GC) (Hewlett  
194 Packard, USA). Protein and carbohydrate concentrations were measured according to Lowry et  
195 al. (1951) and Loewus (1952) methods, respectively. Anions (e.g.  $\text{Cl}^-$ ) and cations (e.g.  $\text{Na}^+$ )  
196 were determined by ion chromatography (861 Advanced Compact IC system, Metrohm,  
197 Switzerland).

198

#### 199 **2.4 Calculations**

200 The individual acid concentrations for acetic acid (HAc), propionic acid (HPr), butyric acid  
201 (HBu) and valeric acid (HVa) were converted to COD units by the application of corresponding  
202 coefficients: 1.07 g  $\text{COD}_{\text{HAc}}/\text{g HAc}$ , 1.51 g  $\text{COD}_{\text{HPr}}/\text{g HPr}$ , 1.82 g  $\text{COD}_{\text{HBu}}/\text{g HBu}$  and 2.04 g  
203  $\text{COD}_{\text{HVa}}/\text{g HVa}$ . The acidification percentage was calculated as the sum of the individual VFA  
204 measured by GC, converted to COD units (g  $\text{COD}_{\text{VFA}}$ ), and divided by the amount of COD at  
205 the beginning of the experiment ( $\text{COD}_i$ ), as indicated in the following equation:

$$\text{Acidification (\%)} = \frac{\text{g COD}_{\text{VFA}}}{\text{g COD}_i} \cdot 100$$

206 Statistical analysis of data was carried out using the software R version 3.5.1. The normality and  
207 homogeneity of variance were evaluated by means of the Shapiro-Wilk and Levene tests,  
208 respectively. ANOVA parametric test was used when both tests could be confirmed, and if not,  
209 non-parametric Kruskal-Wallis test was applied. Differences in the experimental values of the  
210 pH, acidification percentage and VFA concentration obtained in the acidification batch tests  
211 were compared with the calculation of the area under the curve (AUC) using the package PK.

212

213

214

## 215 **3. RESULTS AND DISCUSSION**

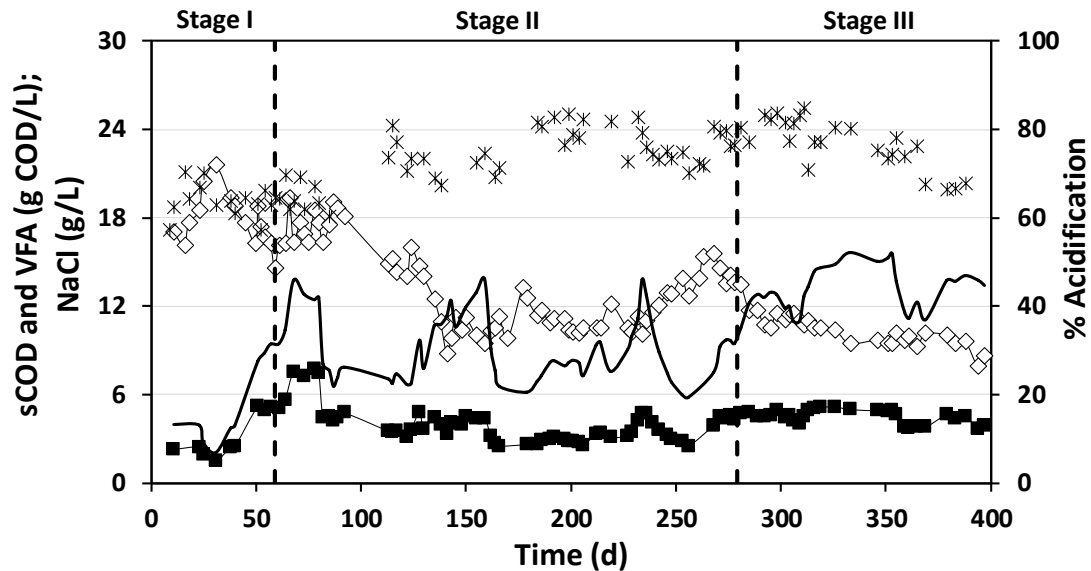
### 216 **3.1 Operation of the completely stirred acidogenic reactor**

#### 217 *3.1.1 VFA production at low pH*

218 The 5-L acidification reactor was operated for 400 days fed with wastewater from a cooked  
219 mussel processing factory (Table 1). Both in the raw wastewater and the effluent of the  
220 acidification reactor, the soluble COD (sCOD) corresponded approximately to 97 % of total  
221 COD (tCOD). Therefore, during the whole operation, the COD was expressed as sCOD.  
222 Although anaerobic biomass was used as inoculum, methane was not detected in the gas phase.  
223 Indeed, the mass balances of sCOD indicates a non-significant difference between influent and  
224 effluent, below 10 % that can be attributed to biomass growth and to inaccuracies in analytical  
225 determination. The acidogenic reactor was operated without pH control that, due to the low pH  
226 of the wastewater fed, was maintained below 5. Acidogenic populations are significantly less  
227 sensitive to pH than methanogenic ones. In this way, the low pH values achieved in the reactor  
228 favoured the natural selection of acidogenic over methanogenic microorganisms (Wainaina et  
229 al., 2019). Chen et al. (2007) reported the influence of pH on methane and VFA production and  
230 they observed a complete methanogenic activity inhibition at pH 4 and the acidification of 20 %  
231 of sCOD. In the present research work, the acidic conditions were caused by the accumulation  
232 of VFA in the reactor and the low buffer capacity of the wastewater (approximately 170 mg  
233 CaCO<sub>3</sub>/L).

234 The VFA production highly fluctuated during the 400 days of operation of the acidification  
235 reactor due to continuous variations in the substrate composition (Figure 1 and Table 3). During  
236 the first operational days, the VFA production was low (average 19 % of acidification),  
237 probably due to the high applied OLR ( $7.3 \pm 0.5$  g COD/(L·d)), which was then half reduced on  
238 day 60 of operation. From that day onwards, the acidification efficiency was enhanced, and the  
239 average productivity reached a value of  $0.62 \pm 0.19$  g COD<sub>VFA</sub>/(L·d) in Stage II. In Stage III, the  
240 operational conditions remained stable, with an average acidification percentage of  $42.9 \pm 5.6$   
241 %, which corresponded to a VFA productivity of  $0.72 \pm 0.07$  g COD<sub>VFA</sub>/(L·d). Both values were  
242 higher than in the previous operational period. This indicated that continuous operation allowed

243 the acclimation of the acidifying microorganisms to the unfavourable operational conditions  
 244 (low pH and high salinity). Statistical analysis showed no significant differences in the amount  
 245 of VFA produced between Stages I and II ( $p = 0.08$ ), but significant ones between Stages II and  
 246 III ( $p = 0.0002$ ), with 95 % confidence.



247 **Figure 1.** Evolution of sCOD ( $\diamond$ ), VFA ( $\blacksquare$ ) and NaCl ( $*$ ) concentrations, and acidification  
 248 percentage (-) in the effluent throughout the operation of the acidification reactor.

249

250 **Table 3.** Average values of the parameters measured in the effluent throughout the operation of  
 251 the acidification reactor.

Parameters	Units	Stage I	Stage II	Stage III
		0 - 59 days	60 - 279 days	280 - 400 days
pH	--	$4.4 \pm 0.2$	$3.8 \pm 0.2$	$4.2 \pm 0.1$
sCOD	g/L	$17.7 \pm 1.8$	$13.1 \pm 2.8$	$10.5 \pm 1.3$
VFA	g COD/L	$3.3 \pm 1.5$	$3.9 \pm 1.2$	$4.5 \pm 0.4$
Acidification	%	$18.7 \pm 9.9$	$30.6 \pm 7.6$	$42.9 \pm 5.6$
Carbohydrates	g/L	ND	$1.7 \pm 1.0$	$0.3 \pm 0.2$
Proteins	g/L	ND	$2.8 \pm 0.4$	$1.8 \pm 0.4$
Ammonium	g N/L	$0.17 \pm 0.04$	$0.23 \pm 0.06$	$0.20 \pm 0.04$
TSS	g/L	$3.5 \pm 0.4$	$3.4 \pm 0.8$	$3.4 \pm 0.3$
VSS	g/L	$2.5 \pm 0.2$	$2.2 \pm 0.5$	$2.3 \pm 0.3$
VSS/TSS	%	$70.5 \pm 7.9$	$64.4 \pm 8.8$	$68.9 \pm 3.9$
NaCl	g/L	$19.2 \pm 1.1$	$22.2 \pm 1.9$	$23.0 \pm 1.6$

252 ND: Not determined

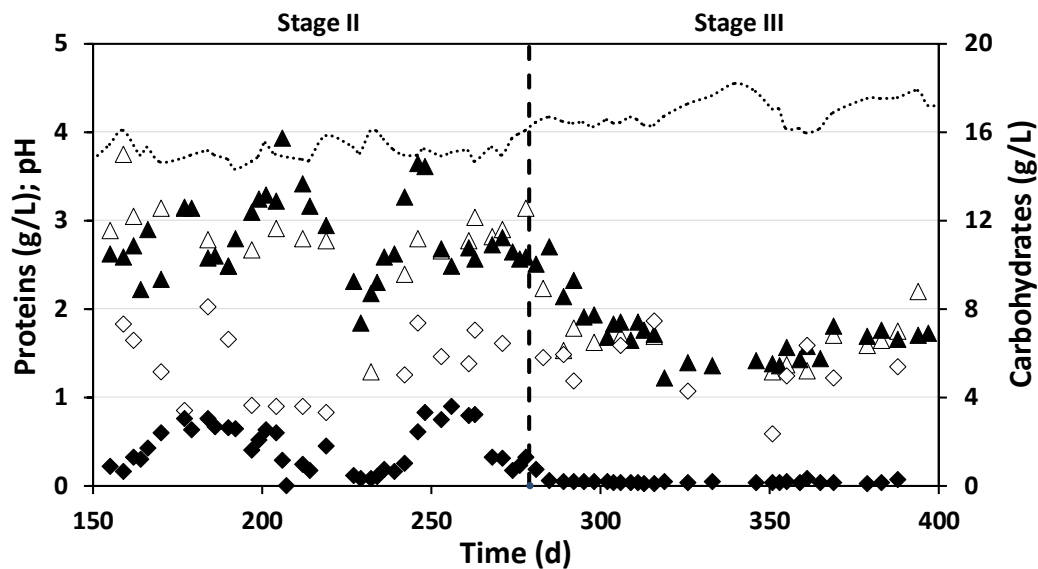
253 Differences between Stages II and III can be explained by different factor variations such as pH,  
254 OLR, salt, ammonium, carbohydrate or protein concentration in the fed wastewater (Table 1).  
255 Among these parameters only pH, OLR and protein concentration change significantly from  
256 Stage II to III, being the pH value the one that showed the highest increase, while the OLR  
257 remained in a quite small range and protein concentration are not relevant as they are neither  
258 degraded nor causing an inhibitory effect on acidification.

259 The effect of pH on the acidogenesis of different substrates was researched in previous studies.  
260 Most of them focused on the improvement of the solubilisation of solid wastes at alkaline  
261 conditions, such as tuna processing waste (Bermudez-Penabad et al., 2017), food waste (Cheah  
262 et al., 2019) or waste activated sludge (Chen et al., 2007; Liu et al., 2020). Alkaline conditions  
263 favoured the organic matter solubilisation as the hydrolysis of proteins and carbohydrates  
264 increases fostering the potential VFA production (Wainaina et al., 2019).

265 Acidic pH values (above 5) were demonstrated to promote the growth of acidogenic bacteria,  
266 with an inhibitory effect at pH values below 3 (Khan et al., 2016). Few studies have evaluated  
267 the acidification at pH values below 5, and different results were obtained. For example,  
268 Bengtsson et al. (2008) operated a chemostat reactor using cheese whey as substrate and they  
269 reported an acidification efficiency of 30 % at pH 3.6, which increased up to 84 % when the pH  
270 value rose to 6.0 in a chemostat reactor. Gouveia et al. (2017) also treated cheese whey  
271 obtaining an average acidification value of 64 % when pH varied from 5 to 7, but the VFA  
272 production decreased by 18 % when the pH dropped to 4.

273 In the present research work, the pH in the reactor was below 4.5 during most of the operational  
274 period, which could limit the acidogenic activity. Moreover, the cooked mussel processing  
275 wastewater consisted of 50 % carbohydrates and 30 % proteins, on sCOD basis. The  
276 carbohydrate concentration in the substrate slightly varied and showed an average value of  $5.5 \pm$   
277  $1.4 \text{ g}_{\text{carbohydrate}}/\text{L}$ , but the removal efficiency varied during the reactor performance (Figure 2 and  
278 Table 3). Until day 280 the average pH value was  $3.8 \pm 0.2$  and the degradation of  
279 carbohydrates was approximately 68 %. Then, from day 280 of operation onwards an increase

280 of the pH of the substrate (an average value of 5.04) provoked the increase of the pH inside the  
281 reactor up to  $4.2 \pm 0.1$ , which favoured the carbohydrate removal up to 96 %.



282 **Figure 2.** Evolution of the concentration of proteins in the influent ( $\triangle$ ) and effluent ( $\blacktriangle$ ),  
283 carbohydrates in the influent ( $\diamond$ ) and effluent ( $\blacklozenge$ ), and pH in the effluent ( $\cdots$ ) of the acidification  
284 reactor throughout the operational period of 150 - 400 days.

285

286 The protein concentration in the feeding was of  $2.3 \pm 0.7$   $g_{\text{protein}}/L$  until day 280, and  $1.7 \pm 0.3$   
287  $g_{\text{protein}}/L$  from that day onwards (Table 2). However, compared to carbohydrate removal, the  
288 protein degradation was almost negligible during the whole reactor performance (Figure 2 and  
289 Table 3). Thus, the VFA production from proteins was not considered. Since proteins are the  
290 second most important organic component of the substrate, its lack of degradation contributed  
291 to a low VFA production concerning the global sCOD in the wastewater. Previous studies  
292 demonstrated that hydrolytic and acidogenic microorganisms could degrade proteins more  
293 effectively under neutral or alkaline conditions using sewage sludge as substrate (Liu et al.,  
294 2012). Duong et al. (2019) found, using gelatine for mimicking a protein-rich stream, protein  
295 degradation inhibition when pH was shifted from 7 to 5. The low conversion of proteins under  
296 acidic conditions could be attributed to the decrease of enzymatic activity (Duong et al., 2019).  
297 Carbohydrate hydrolases are active at an optimal pH of 5, whereas the protease activity has an

298 optimal pH at higher values (6 - 7) (Parawira et al., 2005). The degradation efficiency of  
299 carbohydrates was demonstrated to be less pH-sensitive than that of proteins at pH 4 using dairy  
300 wastewater with a high carbohydrate and protein content (Yu and Fang, 2002), as the substrate  
301 of the present study. Thus, the acidic conditions of the present study could limit the protein  
302 degradation and therefore the maximum acidification throughout the performance of the reactor.

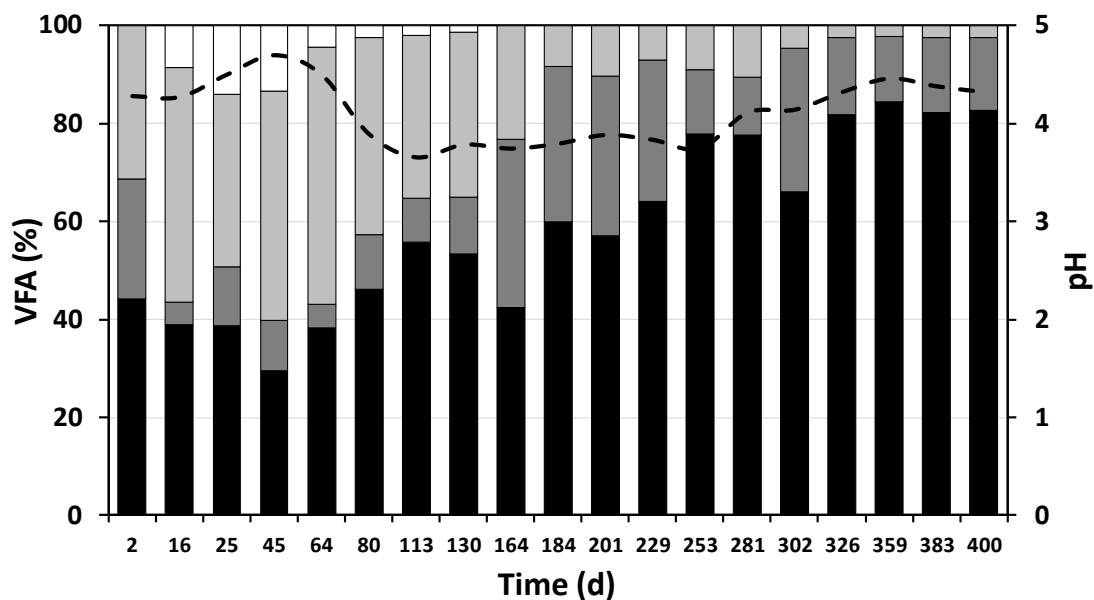
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### 304 *3.1.2 The composition of the VFA mixture*

305 Apart from the variable acidification percentage, different mixtures of VFA were generated  
306 during the operation of the acidification reactor (Figure 3). Acetic, propionic and butyric acids  
307 were the dominant compounds produced during the acidogenesis of the wastewater from mussel  
308 cookers. These short-chain fatty acids can be directly formed by degradation of carbohydrates,  
309 whereas the presence of higher molecular-weight VFA, such as valeric and caproic acids, is  
310 attributed to acidogenesis of proteins (Yu et al., 2018). In this way, the lack of protein  
311 degradation correlated with the low production of these acids. Operational conditions such as  
312 pH value, OLR or HRT, among others, not only affect the acidification degree but also the VFA  
313 composition (Atasoy et al., 2019; Wainaina et al., 2019). In the present study, HRT was only  
314 increased on day 60 (Table 3) while VFA composition varied throughout the reactor operational  
315 period. Thus, other parameters, such as the pH of the reactor medium, could be driving the VFA  
316 distribution in the following Stages.

317 During Stage I, the pH remained at an average value of 4.5. In terms of VFA composition,  
318 results indicated that the operational conditions promoted the production of butyric acid, which  
319 became the dominant VFA. At the end of Stage I the composition of the acids produced  
320 corresponded to 30:2:62:6 as HAc:HPr:HBU:HVa expressed as a percentage of VFA on COD  
321 basis. After the decrease of the HRT and, thus, the OLR on day 60, a shift of the VFA produced  
322 was clearly observed (Figure 3). During this stage, the production of acetic and propionic acid  
323 production increased, while the butyric acid concentration decreased. The VFA composition on  
324 day 281 of operation was of 78:12:10:0, corresponding to HAc:HPr:HBU:HVa. Results seem to  
325 indicate that the increase of the HRT from 3.1 to 6.2 days promoted a shift of the VFA

326 distribution. Bengtsson et al. (2008) investigated the effect of the retention time on the VFA  
 327 composition, and also observed a higher production of acetic and propionic acids when the  
 328 retention time was increased from 11 to 24 h, using paper mill wastewater. Similary, Jankowska  
 329 et al. (2015) obtained a decrease of butyrate and an increase of acetic and propionic acid  
 330 production during acidification of primary and waste activated sludge, when the retention time  
 331 was prolonged from 5 to 15 days and the pH was maintained at 4. Zhang et al. (2006) observed  
 332 evidence of wash-out effect on propionate producing populations after the shortening of the  
 333 HRT.  
 334



335 **Figure 3.** Evolution of the composition of the VFA produced in the acidification reactor and the  
 336 pH value throughout the operational period. Percentages corresponding to HAc: acetic acid (■),  
 337 HPr: propionic acid (■), HBu: butyric acid (■) and HVa: valeric acid (□); and pH (- - -) value.

338  
 339 From day 281 onwards (Stage III) the VFA composition was relatively stable, which correlated  
 340 with the improvement of the acidification shown in Figure 1 due to the increase of the pH value  
 341 above 4. During this period, the dominant component was acetic acid with an average  
 342 concentration in the effluent of  $3.5 \pm 0.3$  g COD<sub>HAc</sub>/L, followed by propionic acid ( $0.8 \pm 0.2$  g  
 343 COD<sub>HPr</sub>/L) and butyric acid ( $0.2 \pm 0.1$  g COD<sub>HBu</sub>/L). Even though the reactor was subjected to



344 changes in the composition of the cooked mussel processing wastewater during the whole  
345 operation, it showed more stability during the Stage III when the acidification degree and  
346 composition of the mixture of VFA remained relatively constant.

347

### 348 **3.2 Alkalinity effect on VFA production: proteins degradation**

349 Batch tests were performed to evaluate the influence of the pH value on the VFA production  
350 from cooked mussel processing wastewater (Figure 4 and Table S1 in Supporting Material).

351 Acidifying biomass from the reactor was collected on day 76 and used as inoculum. An  
352 experiment without acidifying sludge or alkalinity addition was carried out as control (E1).

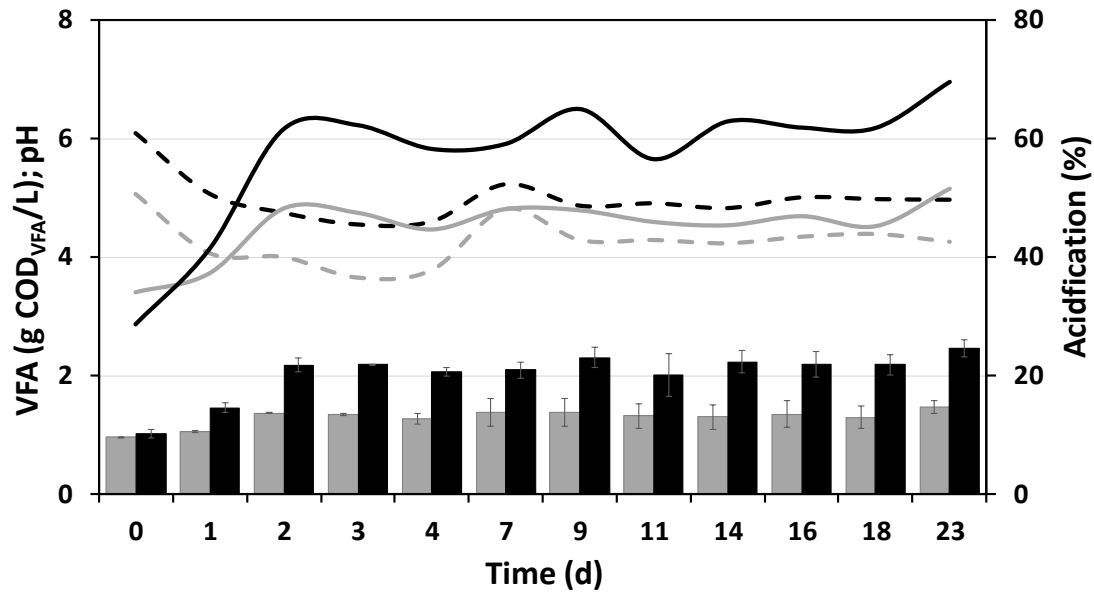
353 Then, the effect of the alkalinity was studied without (E2) and with (E3) the external addition of  
354  $\text{NaHCO}_3$ , in batch experiment that already contained the same inoculum and substrate  
355 concentrations. The initial VFA concentration in all bottles (E1, E2 and E3) was approximately  
356  $900 \text{ mg COD}_{\text{VFA}}/\text{L}$ . Even though the biomass collected from the acidification reactor was  
357 washed before the experiment, the inoculum media contained a remaining amount of VFA ( $<$   
358  $0.1 \text{ g COD}_{\text{VFA}}/\text{L}$ ). In all the bottles, no methane production was observed during the tests.

359 In the control flasks (E1), where only substrate was added, no differences in the VFA  
360 concentrations were observed throughout the batch test. Experiments E2 and E3 with substrate  
361 and acidifying biomass showed an increase of the VFA concentration during the first days of the  
362 batch experiment (Figure 4). However, the increase of the acidification in experiment E2 was  
363 lower than in E3 and the acidification values on day 2 were 48.2 % and 61.6 %, respectively.

364 From that day onwards the VFA concentration remained at approximately  $1.4 \pm 0.2 \text{ g}$   
365  $\text{COD}_{\text{VFA}}/\text{L}$  in E2, whereas in E3 reached a value of  $2.5 \pm 0.1 \text{ g COD}_{\text{VFA}}/\text{L}$  after 23 days of  
366 experiment. This latter value corresponded to an acidification degree of 70 % of initial COD.

367 Statistical analysis was applied by comparing the area under the curve (AUC) described by the  
368 VFA produced throughout the batch test and showed significant differences in the acidification  
369 percentage between the flasks without (E2) and with (E3) alkalinity ( $p = 0.061$ ), with 90 %  
370 confidence.

371



372 **Figure 4.** Evolution of the VFA concentrations (columns), percentage of acidification  
 373 (continuous lines) and pH value of the liquid media (discontinuous lines) in the acidification batch  
 374 experiments using cooked mussel processing wastewater. Grey colour corresponds to experiment  
 375 E2 and black colour to experiment E3. The error bars of the columns represent the standard  
 376 deviation of the point.

377

378 The specific acidogenic activity of  $0.79 \text{ g COD}_{\text{VFA}}/(\text{g VSS}\cdot\text{d})$  in E3, was almost three times  
 379 higher than in E2 ( $0.27 \text{ g COD}_{\text{VFA}}/(\text{g VSS}\cdot\text{d})$ ). The main difference in both experiments was the  
 380 pH value. Without alkalinity (E2) the pH value was  $4.2 \pm 0.3$ , whereas in E3 the addition of  
 381  $\text{NaHCO}_3$  promoted the maintenance of higher pH ( $4.9 \pm 0.1$ ). These results were in accordance  
 382 with the specific activities estimated for the acidifying reactor. During Stage I the acidogenic  
 383 activity was  $0.24 \pm 0.11 \text{ g COD}_{\text{VFA}}/(\text{g VSS}\cdot\text{d})$ , which was very similar to the value obtained in  
 384 E2. This value increased during Stage III when a higher pH was measured in the reactor and  
 385 correlated with an increase of the acidogenic activity, being the average value of  $0.33 \pm 0.03 \text{ g}$   
 386  $\text{COD}_{\text{VFA}}/(\text{g VSS}\cdot\text{d})$ . Therefore, batch results indicated that the increase in the pH, by addition of  
 387 alkalinity, had a positive effect in terms of conversion of VFA from the cooked mussel  
 388 processing wastewater. Yu and Fang (2002) also observed changes in the VFA production from

389 dairy wastewater at variable pH and obtained an increase of the microbial activity from 0.146 g  
390 COD/(g VSS·d) at pH 4 to 0.320 g COD/(g VSS·d) at pH 5.5.

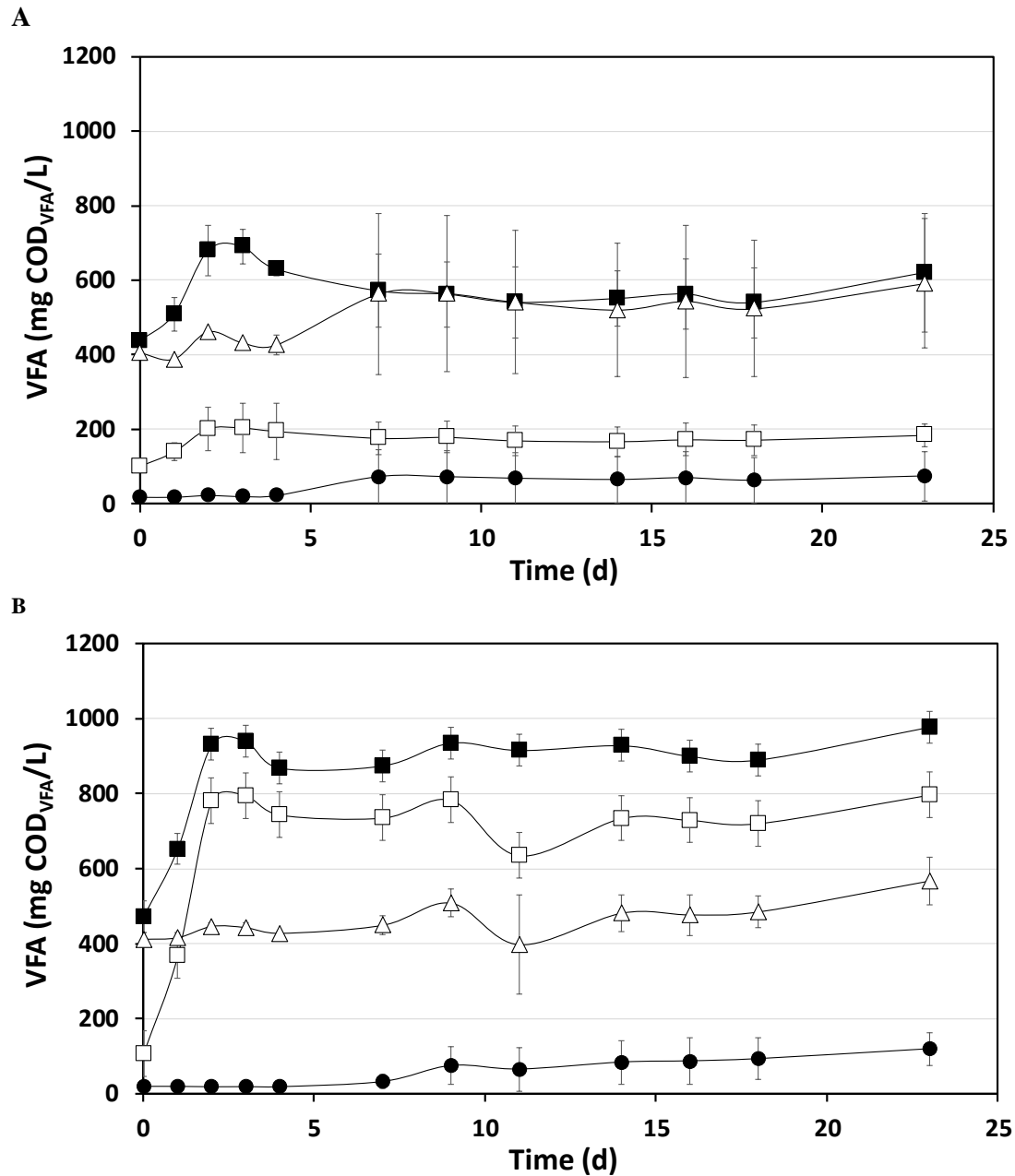
391 A shift of the VFA distribution was observed in experiments at different operational pH (Figure  
392 5 and Table S1 in Supporting Material). During the acidification experiments without (E2) and  
393 with (E3) alkalinity, acetic acid was the dominant organic acid, whereas valeric acid was  
394 produced at the lowest concentration. However, propionic and butyric acids showed inverse  
395 behaviour in the two experimental conditions (Figure 5). In E2 (lower pH), the butyric acid  
396 concentration increased and reached the same value as acetic acid from day 7 onwards (Figure  
397 5A). Propionic acid concentration slightly increased during the first days, and it remained stable  
398 during most part of the experiment. In E3 (higher pH), butyric acid concentration did not  
399 experience the same evolution as in E2 and approximately the same concentration was  
400 maintained until the end of the experiment. However, propionic acid production increased at the  
401 beginning of the assay and became the second most-produced acid after acetic (Figure 5B).

402 Previous studies have reported the influence of the pH not only on the concentration of VFA  
403 produced but also on the metabolic pathways in acidogenic fermentation and, therefore, of the  
404 product distribution. However, there are no consistent conclusions on the influence of pH on the  
405 composition of VFA (Zhou et al., 2018). In the batch experiments of the present research work,  
406 butyric acid production was improved under low pH conditions. These results agreed with  
407 previous studies that reported that the butyrate metabolic pathway was enhanced under acidic  
408 conditions (González-Cabaleiro et al., 2015; Jankowska et al., 2017; Temudo et al., 2007).

409 A positive effect of the acidic pH was observed in the reactor to select acidifying bacteria and  
410 wash out methanogenic microorganisms from the anaerobic mixed culture used as inoculum.

411 However, the acidogenic activity was limited by the low pH values (below 4 during most of the  
412 operational time). Results of the batch experiments showed that the addition of alkalinity  
413 improved the VFA production and modified the obtained products, with respect to the  
414 experiments without NaHCO<sub>3</sub> addition. However, the increase of pH up to 5 was insufficient to  
415 achieve complete acidification of the substrate. Even though the protein concentration was not

416 measured during the batch experiment, the 30 % of non-acidified COD probably corresponded  
417 **mainly** to the protein content of the substrate.



418 **Figure 5.** Concentrations of VFA produced in the batch assays without-E2 (A) and with-E3 (B)  
419 alkalinity. Acetic acid (■), propionic acid (□), butyric acid (△) and valeric acid (●). The error  
420 bars represent the standard deviation of the point.

421

422 Residual carbohydrate concentration is also expected due to kinetic and energetic or

423 thermodynamic conversion limitations (González-Cabaleiro et al., 2015). Considering the

424 carbohydrate affinity for the process of 1 mM (expressed as glucose) (González-Cabaleiro et al.,

425 2015), 0.2 g COD/L would remain as carbohydrates. Thus, protein partial degradation is  
426 suggested to contribute to the achievement of the 70 % of acidification in E3. If only  
427 carbohydrate were degraded, the acidification efficiency would be limited to 64 %. A more  
428 detailed study is required to optimise the pH via the long-term addition of  $\text{NaHCO}_3$  to the  
429 feeding of the reactor and to evaluate its effect on protein degradation and, eventually, on the  
430 amount of VFA produced.

431 To sum up, obtained results suggested that an increase in the pH of the reactor media could  
432 promote protein degradation fostering VFA production. However, a techno-economical study  
433 would be required to evaluate the process benefits in terms of acidification efficiency and  
434 increase of operational costs due to the addition of chemicals to adjust the pH value. Other  
435 factors like HRT and OLR should be considered to define the best operational strategy and set  
436 the optimal pH value. The obtained VFA-rich stream could be used to produce PHA, as carbon  
437 source for nutrient removal or purified to use the VFA as platform chemicals, among other  
438 applications. Depending on the final use, the composition of the VFA mixture will be relevant  
439 (as platform chemical or affecting the obtained PHA properties) or not (for nutrient removal)  
440 (Atasoy et al., 2018). The final application will also determine the downstream processes  
441 required to obtain the final product and a clean effluent for discharge. In the present study, it  
442 was demonstrated that mussel cooking wastewater is a good candidate to produce VFA-rich  
443 streams. Thus, this wastewater could be valorised, under uncontrolled pH conditions, instead of  
444 being just treated consuming resources like energy or chemicals. As in the present study the aim  
445 is to produce VFA subsequent treatment/processing steps are required to produce an effluent  
446 with the required composition to be discharged to the environment.

447

#### 448 **4. Conclusions**

449 Acidogenic fermentation of cooked mussel processing wastewater resulted in a significant VFA  
450 productivity of  $0.72 \pm 0.07$  g  $\text{COD}_{\text{VFA}}/(\text{L}\cdot\text{d})$ , considering the complex composition of the  
451 substrate, mainly characterized by high organic matter content ( $13.8 \pm 3.2$  g COD/L), high  
452 salinity ( $21.8 \pm 2.8$  g NaCl/L) and low pH ( $4.6 \pm 0.6$ ). The maximum acidification percentage

453 obtained was 43 % and the composition of the VFA mixture obtained was of 80:18:2 as  
454 HAc:HPr:HBu. Carbohydrate conversion reached up to 96 % and contributed to the production  
455 of VFA. However, the acidification efficiency was hindered by a deficient protein degradation,  
456 probably associated to the acidic conditions inside the reactor.  
457 Batch experiments showed that the increase of the pH from 4.2 to 4.9 by the addition of  
458 NaHCO<sub>3</sub> resulted in a higher acidification efficiency. In addition to increasing VFA production,  
459 the composition of the mixture switched from containing mostly acetic and propionic acids to  
460 containing mostly acetic and butyric. Nevertheless, part of the COD remained as non-acidified  
461 COD even at pH 5, probably due to the slight degradation of proteins.

462

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470

### 471 **References**

472 APHA-AWWA-WEF. Standard methods for the examination of water and wastewater.  
473 Washington DC, USA: American Public Health Association/American Water Works  
474 Association/Water Environment Federation, 2017.  
475 Artiga P, García-Toriello G, Méndez R, Garrido JM. Use of a hybrid membrane bioreactor for  
476 the treatment of saline wastewater from a fish canning factory. *Desalination* 2008; 221:  
477 518-525. doi: 10.1016/j.desal.2007.01.112.

478 Aspé E, Marti MC, Roeckel M. Anaerobic treatment of fishery wastewater using a marine  
479 sediment inoculum. *Water Research* 1997; 31: 2147-2160. doi: 10.1016/S0043-  
480 1354(97)00051-1.

481 Atasoy M, Eyice O, Schnürer A, Cetecioglu Z. Volatile fatty acids production via mixed culture  
482 fermentation: Revealing the link between pH, inoculum type and bacterial composition.  
483 *Bioresource Technology* 2019; 292: 121889. doi: 10.1016/j.biortech.2019.121889.

484 Atasoy M, Owusu-Agyeman I, Plaza E, Cetecioglu Z. Bio-based volatile fatty acid production  
485 and recovery from waste streams: Current status and future challenges. *Bioresource*  
486 *Technology* 2018; 268: 773-786. <https://doi.org/10.1016/j.biortech.2018.07.042>.

487 Bello Bugallo PM, Stupak A, Cristóbal Andrade L, Torres López R. Material Flow Analysis in  
488 a cooked mussel processing industry. *Journal of Food Engineering* 2012; 113: 100-117.  
489 doi: 10.1016/j.jfoodeng.2012.05.014.

490 Bengtsson S, Hallquist J, Werker A, Welander T. Acidogenic fermentation of industrial  
491 wastewaters: Effects of chemostat retention time and pH on volatile fatty acids  
492 production. *Biochemical Engineering Journal* 2008; 40: 492-499. doi:  
493 10.1016/j.bej.2008.02.004.

494 Bermudez-Penabad N, Kennes C, Veiga MC. Anaerobic digestion of tuna waste for the  
495 production of volatile fatty acids. *Waste Management* 2017; 68: 96-102. doi:  
496 10.1016/j.wasman.2017.06.010.

497 Bower CE, Holm-Hansen T. A Salicylate–Hypochlorite Method for Determining Ammonia in  
498 Seawater. *Canadian Journal of Fisheries and Aquatic Sciences* 1980; 37: 794-798. doi:  
499 10.1139/f80-106.

500 Carrera P, Campo R, Méndez R, Di Bella G, Campos JL, Mosquera-Corral A, et al. Does the  
501 feeding strategy enhance the aerobic granular sludge stability treating saline effluents?  
502 *Chemosphere* 2019; 226: 865-873. <https://doi.org/10.1016/j.chemosphere.2019.03.127>.

503 Cristóvão RO, Botelho CM, Martins RJE, Boaventura RAR. Chemical and biological treatment  
504 of fish canning wastewaters. *international Journal of Bioscience and Bioinformatics*  
505 2012; 2: 237-242. doi: 10.7763/IJBBB.2012.V2.108.

506 Cristóvão RO, Pinto VMS, Gonçalves A, Martins RJE, Loureiro JM, Boaventura RAR. Fish  
507 canning industry wastewater variability assessment using multivariate statistical  
508 methods. *Process Safety and Environmental Protection* 2016; 102: 263-276.  
509 <https://doi.org/10.1016/j.psep.2016.03.016>.

510 Cheah Y-K, Vidal-Antich C, Dosta J, Mata-Álvarez J. Volatile fatty acid production from  
511 mesophilic acidogenic fermentation of organic fraction of municipal solid waste and  
512 food waste under acidic and alkaline pH. *Environmental Science and Pollution  
513 Research* 2019; 26: 35509-35522. doi: 10.1007/s11356-019-05394-6.

514 Chen Y, Jiang S, Yuan H, Zhou Q, Gu G. Hydrolysis and acidification of waste activated sludge  
515 at different pHs. *Water Research* 2007; 41: 683-689. doi: 10.1016/j.watres.2006.07.030.

516 Chowdhury P, Viraraghavan T, Srinivasan A. Biological treatment processes for fish processing  
517 wastewater - A review. *Bioresource Technology* 2010; 101: 439-449. doi:  
518 10.1016/j.biortech.2009.08.065.

519 Duong TH, Grolle K, Nga TTV, Zeeman G, Temmink H, van Eekert M. Protein hydrolysis and  
520 fermentation under methanogenic and acidifying conditions. *Biotechnology for Biofuels*  
521 2019; 12: 254. doi: 10.1186/s13068-019-1592-7.

522 FAO. The canned seafood sector in Spain. *Globefish*. FAO. Food and Agriculture Organization  
523 of the United Nations, 2019.

524 González-Cabaleiro R, Lema JM, Rodríguez J. Metabolic Energy-Based Modelling Explains  
525 Product Yielding in Anaerobic Mixed Culture Fermentations. *PLOS ONE* 2015; 10:  
526 e0126739. 10.1371/journal.pone.0126739.

527 Gouveia AR, Freitas EB, Galinha CF, Carvalho G, Duque AF, Reis MAM. Dynamic change of  
528 pH in acidogenic fermentation of cheese whey towards polyhydroxyalkanoates  
529 production: Impact on performance and microbial population. *New Biotechnology*  
530 2017; 37: 108-116. doi: 10.1016/j.nbt.2016.07.001.

531 Jankowska E, Chwiałkowska J, Stodolny M, Oleskiewicz-Popiel P. Volatile fatty acids  
532 production during mixed culture fermentation – The impact of substrate complexity and  
533 pH. *Chemical Engineering Journal* 2017; 326: 901-910. doi: 10.1016/j.cej.2017.06.021.



534 Jankowska E, Chwiałkowska J, Stodolny M, Oleskowicz-Popiel P. Effect of pH and retention  
535 time on volatile fatty acids production during mixed culture fermentation. *Bioresource*  
536 *Technology* 2015; 190: 274-280. doi: 10.1016/j.biortech.2015.04.096.

537 Khan MA, Ngo HH, Guo WS, Liu Y, Nghiem LD, Hai FI, et al. Optimization of process  
538 parameters for production of volatile fatty acid, biohydrogen and methane from  
539 anaerobic digestion. *Bioresource Technology* 2016; 219: 738-748. doi:  
540 10.1016/j.biortech.2016.08.073.

541 Kleerebezem R, Joosse B, Rozendal R, Van Loosdrecht MCM. Anaerobic digestion without  
542 biogas? *Reviews in Environmental Science and Bio/Technology* 2015; 14: 787-801.  
543 doi: 10.1007/s11157-015-9374-6.

544 Liu H, Wang J, Liu X, Fu B, Chen J, Yu H-Q. Acidogenic fermentation of proteinaceous  
545 sewage sludge: Effect of pH. *Water Research* 2012; 46: 799-807. doi:  
546 10.1016/j.watres.2011.11.047.

547 Liu X, Du M, Yang J, Wu Y, Xu Q, Wang D, et al. Sulfite serving as a pretreatment method for  
548 alkaline fermentation to enhance short-chain fatty acid production from waste activated  
549 sludge. *Chemical Engineering Journal* 2020; 385: 123991.  
550 <https://doi.org/10.1016/j.cej.2019.123991>.

551 Loewus FA. Improvement in anthrone method for determination of carbohydrates. *Analytical*  
552 *Chemistry* 1952; 24: 1. doi: 10.1021/ac60061a050.

553 Lowry OH, Rosebrough NJ, Farr AL, Randall RJ. Protein measurement with the Folin phenol  
554 reagent. *Journal of Biological Chemistry* 1951; 193: 265-75.

555 Mahmoud N, Zeeman G, Gijzen H, Lettinga G. Anaerobic stabilisation and conversion of  
556 biopolymers in primary sludge—effect of temperature and sludge retention time. *Water*  
557 *Research* 2004; 38: 983-991.

558 Méndez R, Omil F, Soto M, Lema JM. Pilot plant studies on the anaerobic treatment of different  
559 wastewaters from a fish-canning factory. *Water Science and Technology* 1992; 25: 37-  
560 44.

561 Moretto G, Valentino F, Pavan P, Majone M, Bolzonella D. Optimization of urban waste  
562 fermentation for volatile fatty acids production. *Waste Management* 2019; 92: 21-29.  
563 doi: 10.1016/j.wasman.2019.05.010.

564 OPMEGA. The mussel cultivation. OPMEGA. Producers' Organization of Mussel from Galicia,  
565 2020.

566 Panpong K, Nuithitikul K, O-thong S, Kongjan P. Anaerobic Co-Digestion Biomethanation of  
567 Cannery Seafood Wastewater with *Microcystis* SP; Blue Green Algae with/without  
568 Glycerol Waste. *Energy Procedia* 2015; 79: 103-110. doi:  
569 10.1016/j.egypro.2015.11.487.

570 Panpong K, Srisuwan G, O-Thong S, Kongjan P. Anaerobic co-digestion of canned seafood  
571 wastewater with glycerol waste for enhanced biogas production. *Energy Procedia* 2014;  
572 52: 328-336. doi: 10.1016/j.egypro.2014.07.084.

573 Parawira W, Murto M, Read JS, Mattiasson B. Profile of hydrolases and biogas production  
574 during two-stage mesophilic anaerobic digestion of solid potato waste. *Process*  
575 *Biochemistry* 2005; 40: 2945-2952. doi: 10.1016/j.procbio.2005.01.010.

576 Prasertsan P, Jung S, Buckle KA. Anaerobic filter treatment of fishery wastewater. *World*  
577 *Journal of Microbiology and Biotechnology* 1994; 10: 11-13. doi: 10.1007/bf00357553.

578 Scoma A, Coma M, Kerckhof FM, Boon N, Rabaey K. Efficient molasses fermentation under  
579 high salinity by inocula of marine and terrestrial origin. *Biotechnology for Biofuels*  
580 2017; 10. 10.1186/s13068-017-0701-8.

581 Silva-Teira A, Sánchez A, Buntner D, Rodríguez-Hernández L, Garrido JM. Removal of  
582 dissolved methane and nitrogen from anaerobically treated effluents at low temperature  
583 by MBR post-treatment. *Chemical Engineering Journal* 2017; 326: 970-979.  
584 <https://doi.org/10.1016/j.cej.2017.06.047>.

585 Silva FC, Serafim LS, Nadais H, Arroja L, Capela I. Acidogenic fermentation towards  
586 valorisation of organic waste streams into volatile fatty acids. *Chemical and*  
587 *Biochemical Engineering Quarterly* 2013; 27: 467-476.

588 Sillapacharoenkul B, Sinbuathong N. Anaerobic biological treatment of frozen seafood  
589 wastewater. *Environmental Progress & Sustainable Energy* 2020; n/a: e13418.  
590 10.1002/ep.13418.

591 Sudmalis D, Gagliano MC, Pei R, Grolle K, Plugge CM, Rijnaarts HHM, et al. Fast anaerobic  
592 sludge granulation at elevated salinity. *Water Research* 2018; 128: 293-303.  
593 10.1016/j.watres.2017.10.038.

594 Tan X, Acquah I, Liu H, Li W, Tan S. A critical review on saline wastewater treatment by  
595 membrane bioreactor (MBR) from a microbial perspective. *Chemosphere* 2019; 220:  
596 1150-1162. <https://doi.org/10.1016/j.chemosphere.2019.01.027>.

597 Tay J-H, Show K-Y, Hung Y-T. *Treatment of Seafood Processing Wastewater. Waste treatment*  
598 *in the food processing industry, 2005, pp. 29-66.*

599 Temudo MF, Kleerebezem R, van Loosdrecht MCM. Influence of the pH on (open) mixed  
600 culture fermentation of glucose: a chemostat study. *Biotechnology and Bioengineering*  
601 2007; 98: 69-79. doi: 10.1002/bit.21412.

602 Wainaina S, Lukitawesa, Kumar Awasthi M, Taherzadeh MJ. Bioengineering of anaerobic  
603 digestion for volatile fatty acids, hydrogen or methane production: A critical review.  
604 *Bioengineered* 2019; 10: 437-458. doi: 10.1080/21655979.2019.1673937.

605 Xiao Y, Roberts DJ. A review of anaerobic treatment of saline wastewater. *Environmental*  
606 *Technology* 2010; 31: 1025-1043. doi: 10.1080/09593331003734202.

607 Yu HG, Fang HH. Acidogenesis of dairy wastewater at various pH levels. *Water Science and*  
608 *Technology* 2002; 45: 201-6.

609 Yu X, Yin J, Shen D, Shentu J, Long Y, Chen T. Improvement of acidogenic fermentation for  
610 volatile fatty acid production from protein-rich substrate in food waste. *Waste*  
611 *Management* 2018; 74: 177-184. doi: 10.1016/j.wasman.2017.11.047.

612 Zhang B, Zhang LL, Zhang SC, Shi HZ, Cai WM. The influence of pH on hydrolysis and  
613 acidogenesis of kitchen wastes in two-phase anaerobic digestion. *Environmental*  
614 *Technology* 2005; 26: 329-39. doi: 10.1080/09593332608618563.

615 Zhang Y, Alam MA, Kong X, Wang Z, Li L, Sun Y, et al. Effect of salinity on the microbial  
616 community and performance on anaerobic digestion of marine macroalgae. *Journal of*  
617 *Chemical Technology & Biotechnology* 2017; 92: 2392-2399. 10.1002/jctb.5246.

618 Zhang Z-P, Show K-Y, Tay J-H, Liang DT, Lee D-J, Jiang W-J. Effect of hydraulic retention  
619 time on biohydrogen production and anaerobic microbial community. *Process*  
620 *Biochemistry* 2006; 41: 2118-2123. doi: 10.1016/j.procbio.2006.05.021.

621 Zhou M, Yan B, Wong JWC, Zhang Y. Enhanced volatile fatty acids production from anaerobic  
622 fermentation of food waste: A mini-review focusing on acidogenic metabolic pathways.  
623 *Bioresource Technology* 2018; 248: 68-78. doi: 10.1016/j.biortech.2017.06.121.

624