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Enio Filho*

Pedro Miguel Santos*

Ricardo Severino

Anis Koubâa*

Eduardo Tovar*

*CISTER Research Centre

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Enio Filho*, Pedro Miguel Santos*, Ricardo Severino, Anis Koubâa*, Eduardo Tovar*

*CISTER Research Centre

Polytechnic Institute of Porto (ISEP P.Porto)

Rua Dr. António Bernardino de Almeida, 431

4200-072 Porto

Portugal

Tel.: +351.22.8340509, Fax: +351.22.8321159

E-mail: enpvf@isep.ipp.pt, pss@isep.ipp.pt, sev@isep.ipp.pt, aska@isep.ipp.pt, emt@isep.ipp.pt

<https://www.cister-labs.pt>

Abstract

Cooperative Vehicular Platooning (Co-VP) is one of the most prominent and challenging applications of Intelligent Traffic Systems. To support such vehicular communications, the ETSI ITS G5 standard specifies event-based communication profiles, triggered by kinematic parameters such as speed. The standard defines a set of threshold values for such triggers but no careful assessment in realistic platooning scenarios has been done to confirm the suitability of such values. In this work, we investigate the safety and performance limitations of such parameters in a realistic platooning co-simulation environment. We then propose more conservative threshold values, that we formalize as a new profile, and evaluate their impact in the longitudinal and lateral behaviour of a vehicular platoon as it carries out complex driving scenarios.

Furthermore, we analyze the overhead introduced in the network by applying the new threshold values. We conclude that a pro-active message transmission scheme leads to improved platoon performance for highway scenarios, notably an increase greater than 40% in the longitudinal performance of the platoon, while not incurring in a significant network overhead. The obtained results also demonstrated an improved platoon performance for semi-urban scenarios, including obstacles and curves, where the heading error decreases in 26%, with slight network overhead.

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Improving the Performance of Cooperative Platooning With Restricted Message Trigger Thresholds

ENIO VASCONCELOS FILHO¹, PEDRO M. SANTOS¹, RICARDO SEVERINO¹, ANIS KOUBAA^{1,2}, AND EDUARDO TOVAR¹, (Member, IEEE)

¹CISTER Research Centre, ISEP, 4200-135 Porto, Portugal

²Robotics and Internet of Things Research Laboratory, Prince Sultan University, Salahuddin, Riyadh 12435, Saudi Arabia

Corresponding author: Enio Vasconcelos Filho (enpvf@isep.ipp.pt)

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ABSTRACT Cooperative Vehicular Platooning (Co-VP) is one of the most prominent and challenging applications of Intelligent Traffic Systems. To support such vehicular communications, the ETSI ITS G5 standard specifies event-based communication profiles, triggered by kinematic parameters such as speed. The standard defines a set of threshold values for such triggers but no careful assessment in realistic platooning scenarios has been done to confirm the suitability of such values. In this work, we investigate the safety and performance limitations of such parameters in a realistic platooning co-simulation environment. We then propose more conservative threshold values, that we formalize as a new profile, and evaluate their impact in the longitudinal and lateral behaviour of a vehicular platoon as it carries out complex driving scenarios. Furthermore, we analyze the overhead introduced in the network by applying the new threshold values. We conclude that a pro-active message transmission scheme leads to improved platoon performance for highway scenarios, notably an increase greater than 40% in the longitudinal performance of the platoon, while not incurring in a significant network overhead. The obtained results also demonstrated an improved platoon performance for semi-urban scenarios, including obstacles and curves, where the heading error decreases in 26%, with slight network overhead.

INDEX TERMS Cooperative awareness messages, cooperative vehicular platooning, ETSI ITS-G5, safety, vehicular networks.

I. INTRODUCTION

Intelligent Transportation Systems (ITS) are key in meeting the transportation and mobility needs of the future in a safer and greener way. Connectivity among vehicles (V2V) and infrastructure (V2I) supports information sharing among road users, enabling a variety of advanced applications. Cooperative Vehicular Platooning (Co-VP) is an application enabled

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by wireless connectivity. In a connected platoon, vehicles can travel at higher speeds with inferior inter-vehicle distance, thus reducing fuel consumption by taking advantage of the slipstream while retaining all safety guarantees [1]–[3], such as improving longitudinal safety [4] and increasing the road capacity [5]. Co-VPs also reduce the risk for soldiers in military theaters by reducing the need for drivers on military convoys [6] and increase passenger capacity in public transport [7]. The development of connected platoons is present in the plans of automakers, developers and governments

worldwide [8]–[10] with an agenda for implementation until 2030 [11].

The European Telecommunications Standards Institute (ETSI) ITS-G5 [12] and the Wireless Access in Vehicular Environments (WAVE) [13] has become the leading standards defining vehicular communication. These operate on top of existing PHY/MAC technologies, such as the IEEE 802.11p-based Direct Short Range Communications (DSRC) or the 3GPP's C-V2X (that englobes LTE-V2X and NR-V2X) [14], [15]. In addition, the ETSI ITS-G5 standard defines the transmission of Cooperative Awareness Messages (CAM) (similarly, WAVE defines Basic Safety Messages - BSM) to enable cooperative perception, augmenting each vehicle's situational awareness and knowledge horizon. CAM messages can be transmitted periodically, at a pre-defined time interval, or can be event-triggered when a kinematic threshold is crossed, e.g., when speed or heading angle crosses a given value. While not referred to as such in the standard, we call to a set of threshold values of kinematic events as a service profile.

In the absence of a dedicated communication protocol for sharing relevant platooning control information, vehicles can rely solely on received CAMs for setting up a platoon. In such cases, the CAM trigger thresholds play a fundamental role in keeping the platoon's lateral and longitudinal coherence and stability. In this work, we investigate the behavior of a platoon as we vary the threshold values of the CAM triggers over a selected range (organized into five candidate service profiles) in terms of efficiency and safety of the vehicles. Ultimately, from the five candidate service profiles, we select the one that performs best for the particular application of platooning and present it as the Platoon Service Profile (PSP) to be considered for integration into the standard. PSP improves the performance of the Co-VP lateral and longitudinal controllers in scenarios with complex trajectories, such as a sequence of curves or while overtaking obstacles, reducing the distance and heading errors and increasing the platoon's stability. Finally, we evaluate the network overhead incurred by this new profile in terms of throughput and inter-message delays. The Packet Delivery Rate (PDR) under PSP is also evaluated, specifically in congested network conditions. These results extend previous work [16], [17] by carrying out an integrated analysis of the control and networking perspective in four Co-VP scenarios.

The contributions of our work are the following:

- 1) We assess the impact of the standard event-based Service Profiles (SPs), in scenarios of abrupt maneuvers (acceleration, deceleration) and sequential curves involving obstacle avoidance, on the performance of the platoon's stability (distance and heading errors). This was done by relying on a high-fidelity analysis of Co-VP lateral and longitudinal dynamics over a six-vehicle Co-VP over a realistic simulation framework called CopaDrive [18].
- 2) We identified a set of scenarios where standard settings provided decreased performance and could

compromise the platoon's safety. Hence, we explore new Service Profiles that can mitigate this problem with negligible implications to the standard. We assess these new SP and show that they increase the Co-VP overall safety, reducing lateral and longitudinal errors in multiple scenarios.

- 3) The network performance was analyzed to evaluate the impact of a new profile in the occupation of the channel. We demonstrate that the proposed PSP does not significantly increase network usage even under a heavy traffic environment compared with the ETSI ITS-G5 profiles.

The rest of this work is structured as follows. Relevant literature is reviewed in Section II. In Section III, we present our model for the connected platoon. A review of the ETSI ITS-G5 standard kinematic triggers and the description of tentative service profiles for platooning can be found in Section IV. Finally, results of platoon safety and network usage over a range of scenarios are presented in Section V. Section VI presents conclusions and future work.

II. RELATED WORKS

A. COMMUNICATION IMPACT ON COOPERATIVE PLATOON PERFORMANCE

The impact of vehicular communications on the performance of autonomous vehicle applications has been extensively studied [19]–[22], but not explicitly related to platooning applications. The works presented in [23] and [24] analyze the performance of a cooperative platoon in a scenario of constant-time headway, with a multiple predecessor-follower Information Flow Topology (IFT) and a multiple preceding and following IFT including random packet losses. The authors determine the upper bound for communication delay for longitudinal control to guarantee platoon stability. However, this work does not address communication standards and the trigger conditions presented in realistic scenarios.

In [25], the authors investigate the impact of the packet loss ratio and time message delay in the Co-VP controllers, considering DSRC and LTE C-V2X networks. This work assumes a fixed inter-message delay and a packet loss model based on the Bernoulli distribution. The authors observed that longitudinal and lateral errors increase with message delay and packet loss and proposed a limit to both variables. However, the work does not investigate any scenario with both network conditions. A similar strategy was applied in [26] to evaluate the impact of a deliberate communication failure in one of the vehicles and the consequences on platooning stability. This work used a simulated 14-vehicle platooning with WAVE communication with fixed time delays.

In contrast with the usual steady-state communication analysis, the time-varying performance of IEEE 802.11p Co-VP communication is discussed in [27]. The authors consider the impact of a disturbance in the leader's behavior and derive the time-dependent states of the followers. Finally, the authors used the packet loss and the message delay as metrics, concluding that the IEEE 802.11p can keep

the platooning stability under a disturbance. However, this work considers a leader-followers IFT, which reduces the number of sent messages. A similar evaluation was performed in [16], using the ETSI ITS-G5 standard and the leader predecessor-followers IFT. This work identifies the phenomena that decrease communication performance based on the messages synchronization after sequential disturbances in Co-VP speed.

B. TRIGGER THRESHOLDS FOR MESSAGE TRANSMISSION

The performance of the cooperative platoon also depends on the message trigger strategy: time-triggered and event-triggered. Although the ETSI ITS-G5 defines the event-triggered strategy as a standard, many implementations have been performed with time-triggered strategies [28]–[30]. Time-triggered messages can increase platoon safety if a high message frequency ratio is used, at the cost of increased packet collision probability due to a crowded medium [31]. In turn, the event-trigger solution reduces the network channel busy rate (CBR), enhancing vehicular network dissemination performances [21].

The event-triggered communication studied can be divided into two groups. The first group, such as presented in [32], assumes that the V2V communication is fully reliable. The authors of [32] developed a framework for event-triggered coordination of nonlinear vehicles dynamics with general controllers and a lower limit inter-event time. The second group investigates the impact of the network instabilities in event-triggered platooning [33]. In [34], an event-triggered message control is defined for a Co-VP application with time-varying delay and sensor faults. The event-triggering mechanism is a function of the present value of the sensor faults (and not the parameters defined in the ITS-G5 standard). In [35], it is proposed a flexible event-triggering strategy based on tunable parameters for each platooning vehicle, reducing the communication burden.

An external observer is proposed in [36] to create a distributed and adaptive event-triggered control mechanism, based on the estimation of the leader state matrix. However, none of the above studies leverages an active ITS communication standard, which distances their conclusions from real deployment scenarios. An evaluation of the delay between messages in a cooperative platoon is conducted with ETSI ITS-G5 in [37]. The authors compare message delay using the ETSI event-triggered specifications against a fixed frequency of 10Hz. In both modes, the authors consider a random transmission delay. The authors conclude that the platoon performance at fixed frequency outperforms the one with the ITS-G5 standard, especially at higher speeds. However, they do not address the CBR and its effects on the platoon.

We claim that event-triggered solutions can offer satisfactory platoon safety and efficient performance while improving the medium capacity and reducing network congestion. The latter aspect is relevant on account of co-existence: the platoon’s internal communications should not become so intense as to degrade the communications of the other road

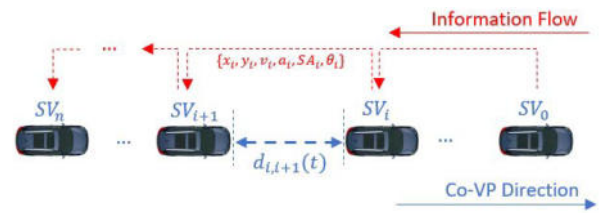


FIGURE 1. Co-VP Model with PF-IFT.

TABLE 1. Terms and corresponding variables.

Variable	Term
$m_{i,i+1}$	Message from SV_i to SV_{i+1}
$D_{SV_i,SV_{i+1}}$	Inter-vehicle distance
d_{ref}	Objective Distance
SD	Safety Distance
e_i^δ	Distance Error
e_i^θ	Heading Error
b_i	Bearing Error
α_i	Steering Angle

users around the platoon. While several works have studied event-triggered solutions, as far as we know, none have evaluated their performance under the ETSI ITS-G5 standard, particularly in a realistic approach, which encompasses both control and kinematic properties of vehicles alongside the communication aspects. This work fulfills this gap by presenting an in-depth analysis of the ETSI ITS-G5 event-triggered message transmission and a microscopic evaluation of the platoon’s longitudinal and lateral error under representative road scenarios.

III. VEHICLE PLATOON MODEL AND SAFETY METRICS

Table 1 presents some of the most used variables throughout this section and the paper.

A. CONTROL MODEL

We assume a platoon of $n + 1$ vehicles under a ITS-G5 communication environment using a Predecessor-Follower IFT (PF-IFT) [38], [39], as presented in Fig. 1. Each vehicle has sensors to measure its global position, speed, acceleration, and heading. The vehicles in the platoon are referred to as *subject vehicles* and identified by SV_i (where $i \in \{0 \leq i \leq n, i \in \mathbb{N}\}$), with SV_0 being the platoon leader. Each SV_i can be both a local leader of SV_{i+1} and a follower of SV_{i-1} .

The vehicle controller is the Look-Ahead PID Controller [40], which manages the longitudinal and lateral behavior of the vehicle. In this Co-VP model, each follower (SV_{i+1}) decides their behavior based solely on the CAM messages received from SV_i , transmitted upon activation of the kinematic triggers. Each SV_i sends a message $m_{i,i+1}(t)$ containing its current global position $(x_i(t), y_i(t))$, speed $(v_i(t))$, acceleration $a_i(t)$, steering angle $\alpha_i(t)$ and heading $\theta_i(t)$ to SV_{i+1} . The inter-vehicle spacing policy is the *Constant Time-Headway Policy* (CTHP) [41], that uses the current speed of SV_{i+1} to define the safety distance SD . In CTHP, the objective range d_{ref} is $d_{ref}(t) = SD + T_h v_{i+1}(t)$, where T_h is the defined time headway (typically between 0.5 and 2 seconds), and $v_{i+1}(t)$ is the follower’s speed.

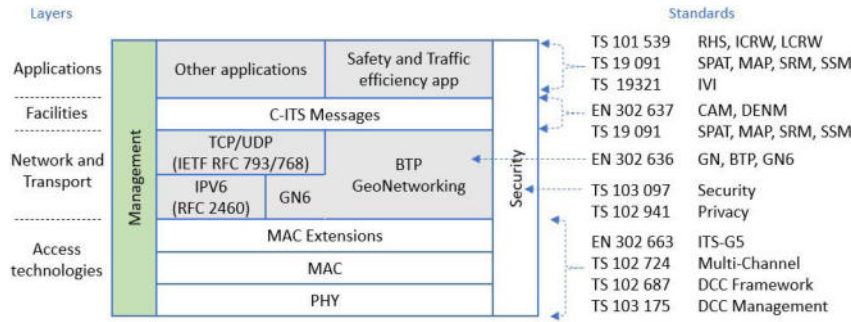


FIGURE 2. ETSI ITS-G5 stack.

B. METRICS OF PLATOON SAFETY

1) DISTANCE ERROR (OR LONGITUDINAL ERROR) e_i^δ
 between the current and the desired inter-vehicle distance is defined simply as:

$$e_{i+1}^\delta(t) = d_{i,i+1}(t) - d_{ref} \tag{1}$$

where $d_{i,i+1}(t)$ is the Euclidean distance between $SV_i(t)$ and $SV_{i+1}(t)$.

2) STABILITY

We consider the **local platoon stability**, described by the following transfer function of the steady state error:

$$H(s) = e_{i+1}^\delta / e_i^\delta, \tag{2}$$

based on the \mathcal{L}_2 norms. The platoon stability is guaranteed if $\|H(s)\|_\infty \leq 1$ and $h(t) > 0$, where $h(t)$ is the impulse response corresponding to $H(s)$ [42]. In [43], the authors define the stability of the platoon as \mathcal{L}_∞ , guaranteeing the non-overshoot for a signal while it propagates throughout the platoon as a *global platoon stability*. This metric defines the worst case performance in the sense of measuring the peak magnitude of the spacing distance between vehicles.

3) HEADING ERROR (OR LATERAL ERROR) e_i^θ

in the platooning application, SV_{i+1} should perform the same path as SV_i based only on the received information (in the form of a message $m_{i,i+1}$). In a longitudinal-only Co-VP application, the controller of vehicle SV_{i+1} uses $m_{i,i+1}(t)$ to define and correct $e_{i+1}^\delta(t)$. If longitudinal and lateral control is considered, vehicle SV_{i+1} compares $\theta_{i+1}(t)$ with $\theta_i(t - T_0)$, where T_0 is the time that SV_{i+1} takes to reach a similar position to SV_i when $m_{i,i+1}(t - T_0)$ was sent. This means that, as $d_{ref}(t) \geq SD$, when SV_i is in position $(x_i(t), y_i(t))$, SV_{i+1} is in position $(x_{i+1}(t), y_{i+1}(t))$, with a speed of $(v_{i+1}(t) \cos(\theta_{i+1}(t)), v_{i+1}(t) \sin(\theta_{i+1}(t)))$, the $m_{i,i+1}(t)$, sent by SV_i , will be received by SV_{i+1} in $t + \zeta$, where ζ is the message delay between the sent and receiving time. The information contained in $m_{i,i+1}(t)$ will be immediately used to calculate $e_{i+1}^\delta(t)$, while $m_{i,i+1}(t - T_0)$ will be used to calculate the **heading error** ($e_{i+1}^\theta(t)$), defined as:

$$e_{i+1}^\theta(t) = \theta_i(t - T_0) - \theta_{i+1}(t) \tag{3}$$

IV. EXPLORING TRIGGER THRESHOLDS FOR CAM MESSAGES

A. CURRENT ETSI ITS TRIGGERS

The ETSI ITS stack is described as a family of ETSI standards, with the key one being ETSI EN 302.665 [44], as it describes the communication architecture. Fig. 2 (adapted from [45]) presents the protocol stack and reference architecture for ETSI ITS-S, and lists the key standards of the European ITS standard. The Cooperative Awareness Messages (CAMs), defined in ETSI EN 302 637-2 [46], can be event-triggered or periodic. The CAM event-triggered mechanism is kinematic-dependent: each vehicle generates new CAMs depending on updates of its current position, speed, and heading [16]. In other words, an On-board Unit (OBU) adjusts the periodicity of CAM messages to the vehicle's dynamics, increasing the frequency as it accelerates or decelerates, at high speeds, or when performing abrupt maneuvers.

Then, when detecting a variation in any of the parameters, the sensors must inform the controller so that it triggers a new CAM message. This action is critical in hard braking circumstances, where acceleration decreases quickly, and the platoon must be informed to avoid a collision. The same can be inferred in a quick change of direction, where the heading varies rapidly and, in order for the other vehicles to be able to correct their trajectories smoothly, new messages are fired, allowing the route to be corrected.

The CAM trigger threshold values are defined in [46]; for convenience, we refer to this set of values as the **Basic Service [Transmission Trigger] Profile (BSP)**, following [17]. The threshold values triggers are defined within an upper (T_{max}) and lower (T_{min}) messages bound times and kinematics triggers to check e_{i+1}^δ and e_{i+1}^θ comparing SV_{i+1} data with the received one from SV_i . These rules are checked latest every 100ms, which is defined as $\Delta = T_CheckCamGen$, and are stated as follows:

- Maximum time (T_{max}) interval between CAM generations: 1s;
- Minimum time (T_{min}) interval between CAM generations: 0.1s;
- Heading difference (τ_{Head}): absolute difference between current and last heading provided in a CAM; a CAM is triggered if $\tau_{Head} > 4^\circ$;

- Position difference (τ_{Pos}): a CAM is triggered if $\tau_{Pos} > 4m$;
- Speed difference (τ_{Speed}): a CAM is triggered if $\tau_{Speed} > 0.5m/s$;

Thus, in BSP, assuming a straight-line trajectory, with a vehicle traveling at $12 m/s$, the τ_{Pos} is activated at $3 Hz$. If this speed is increased up to $15 m/s$, the CAM trigger frequency becomes $3.75 Hz$, and if increased up to $20 m/s$, it becomes $5 Hz$. This adaptation of the messaging system to vehicle conditions increases responsiveness to variations, although it also increases network traffic as the number of messages increases. The reverse also happens, with the messaging frequency decreasing with speed reduction and movement stabilization.

In [12], ETSI defines some ITS use cases, including a Co-VP situation, where it reduces T_{max} to $0.5ms$. This use case is defined as BSP for platooning (BSP-P) in [17]. This change causes that, in a straight line, a platoon member whose constant velocity is greater than or equal to $6.67m/s$ will transmit a CAM by trigger τ_{Speed} instead of T_{max} , unless another trigger is detected. The ETSI standard [46] also specifies that T_{max} of a kinematic trigger assumes the value elapsed between the last two CAMs ($T_{max} = t_{CAM}$), until one new trigger is fired or until three messages limited by the new T_{max} are sent. If all three messages are sent and no trigger is activated, T_{max} returns to the original value defined in the communication profile.

B. TENTATIVE SERVICE PROFILES

In related works, the performance of communication profiles specified in the ETSI ITS architecture have been evaluated in cooperative platooning conditions, typically following straight lines without obstacles. In such scenarios, platoon safety is evaluated solely on its ability to keep the distance between vehicles as the leader changes its speed. In such conditions, the safety and stability of the platoon are usually guaranteed since τ_{Speed} is, even in its default value, very conservative.

However, a natural condition to analyze the performance of the Co-VP application suggests the presence of curves and obstacles on the track. Keeping speed constant, the trigger values τ_{Head} and τ_{Pos} must assume a more significant role in the controller response. Thus, we propose the analysis of different trigger values than the ones proposed by ITS-G5, defining five Service Profiles (SPs), as shown in Table 2. Considering that the value of τ_{Speed} in the ETSI ITS is already quite restrictive, we chose to analyze the impact of reducing the values of τ_{Head} and τ_{Pos} in these SP. So, initially, in SP_1 and SP_2 , we reduced the τ_{Head} , respectively, to 2° and 1° to check their influence over the heading error. Nevertheless, in SP_3 , SP_4 , and SP_5 , we changed τ_{Pos} to $2m$, reducing the maximum speed for triggering by t_{min} from $40m/s$ to $20m/s$. Thus, it is possible to analyze the network congestion caused by this condition by the increased messages concerning the expected increase in performance. For

TABLE 2. Service Profiles.

Profile	BSP	BSP-P	SP_1	SP_2	SP_3	SP_4	SP_5
T_{max} (s)	1.0	0.5	1.0	1.0	1.0	1.0	1.0
T_{min} (s)	0.1	0.1	0.1	0.1	0.1	0.1	0.1
τ_{Head} ($^\circ$)	> 4	> 4	> 2	> 1	> 4	> 2	> 1
τ_{Pos} (m)	< 4	> 4	> 4	> 4	> 2	> 2	> 2
τ_{Speed} (m/s)					< 0.5		

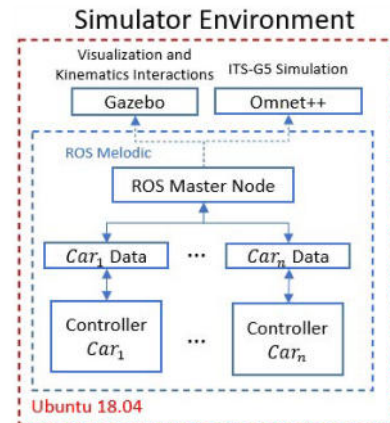


FIGURE 3. CopaDrive Framework Architecture.

complete analysis, SP_3 , SP_4 , and SP_5 mirror the values of τ_{Head} from BSP , SP_1 , and SP_2 , respectively.

V. EVALUATION OF THE SERVICE PROFILES

We use the CopaDrive framework [18], which integrates a 3D robotic simulator (Gazebo) with an ETSI ITS stack provided by the Artery project [47], running on the network simulator OMNET++. The communication between Gazebo and Artery is made through messages exchanged under Robotic Operating System (ROS). Within a hybrid architecture between events and real-time, OMNET++ waits for events generated in the Gazebo to perform the communication between the vehicles. Thus, the kinematic events that trigger messages are performed in ROS/Gazebo and interpreted in OMNET++, which evaluates if the triggers should be activated and trigger new CAM messages. CopaDrive allows a realistic evaluation of the platoon behavior at a microscopic scale and accurate simulation of network events, thus enabling us to study the impact of different trigger conditions in more complex settings. The architecture of CopaDrive is presented in Fig. 3. Furthermore, the possibility of integration with a robotic testbed [48] for future validation of the obtained data was seen as an advantage in choosing the tool. In this work, CopaDrive operates in a Linux Ubuntu 18.04.6 Bionic, with Gazebo 9.0 and ROS Melodic. The PC running the simulations is an Intel® Core® i7-975H CPU, with 16 GB RAM memory and a NVIDIA Geforce GTX 1650.

A. EVALUATED SCENARIOS

We defined four scenarios involving different challenges to the platoon's safety. In all scenarios, the vehicles carry out

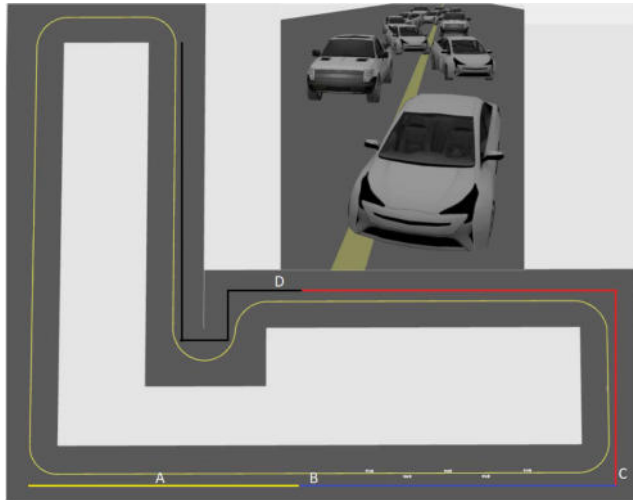


FIGURE 4. Track for Simulations.

a trajectory in the track presented in Fig. 4; the track is divided into four sections to facilitate the discussion of the platoon performance in each scenario: A (yellow), B (blue), C (red) and D (black). In scenarios 1, 2, and 3, we consider a platoon composed of six autonomous vehicles was used, the first being SV_0 , the platoon leader, and the last SV_5 . In all scenarios, the leader performs its trajectory by following a line drawn in the track and applying a line following the algorithm. Each profile was evaluated using five complete tests, and the values presented are the average of these measurements. These tests have statistically validated the results of the experiments since the simulator shows only slight variations between each simulation performed.

Straight Line Scenario (Scenario 1) was developed to analyze the Co-VP performance while the vehicles travel on a straight road, without obstacles. This scenario encompasses sections A (yellow) and B (blue) of the track. In this scenario, the leader starts moving, increasing speed from 0 m/s to 16 m/s, after which it maintains a constant speed for approximately 500m, until a complete break occurs. A video of the SC1 simulation of BSP and SP3 can be found at <https://youtu.be/TEiSW1XFLJg>.

Multi-curve Scenario (Scenario 2) extends SC1 with four curves, as presented in <https://youtu.be/MCDcIEtaF8Y>. It encompasses sections A, B, C, and D (black) of the track, with the two closed curves. The leader accelerates in the same way as in SC1, running through a straight line and performing three left curves and a sharp right curve. Then, it will run for 400m and then stop altogether. This scenario evaluates the Co-VP capacity to follow the leader's trajectory, including sharp curves in 90° and one of 180° . As long as the maximum vehicle steering angle is $|0.52|rad$, the vehicles will perform the curves through several small movements, affecting the system's stability. In this case, the lateral error increases its importance since it will demonstrate the followers' ability to perform the same path as the leader. We can assume that the Co-VP speed error performance is similar to the one

TABLE 3. Model Parameters.

Parameters	Definition
Vehicles (Scen. 1 to 3)	6
Max steering angle	0.52 rad
Safety distance (DS)	5.5 m
Time headway (TH)	0.5 s
Leader speed	16 m/s
Longitudinal: K_P, K_I, K_D	2.0, 0.005, 2.0
Lateral: K_P, K_I, K_D	2.5, 0.001, 1.0

presented in SC1 since the acceleration and deceleration time is the same in both scenarios. However, as the trajectory diverges and the path is different, the e_5^δ tends to increase.

Obstacle Scenario (Scenario 3) adds five static obstacles on the track, represented by pickups. This scenario encompasses sections A, B, and C of the track. Such obstacles are placed on different sides of the track, as shown in Fig. 4, and their function is to force the platoon leader and his followers to perform a *slalom* maneuver. Thus, the vehicles must perform maneuvers with minimum error to avoid collisions with each other and with obstacles, receiving as information only the data from the SV_{i-1} . Thus, the leader follows the same acceleration profile presented in SC1 and SC2, reaching the desired speed, maintaining a constant speed to avoid obstacles, and aligning himself again to perform the curves indicated in the red color path, performing complete braking at the end of this excerpt. This scenario is presented in <https://youtu.be/F3zGpP2XBBU>.

High Medium Occupation (Scenario 4) encompasses sections A, B, and C of the track. Scenario 4 repeated the SC3 trajectory but increased the vehicle's number from 10 to 100 to evaluate the network congestion due to the proposed profiles. In a congested network, it is common for messages not to be delivered or to be delivered late. Therefore, it negatively impacts the performance of the platoon, leading to unsafe situations. Furthermore, by not receiving the messages in time, the followers may collide and fail to correctly follow the leader's trajectory. Thus, even with restricted triggers, their information does not reach the destination in time to cause the correct safety action.

The main scenario, kinematic and control parameters enforced are presented in Table 3:

B. METRICS

As Co-VP errors propagate and accumulate from the first to the last follower, we focus our discussion on the performance of the subject vehicle SV_5 . It is important to note that the triggers are analyzed individually car-by-car and that there is a difference in the subsequent processing of triggering the CAMs of each vehicle belonging to the platoon. Due to this option, the effects of synchronization analyzed in [16] are practically mitigated due to the decoupling between vehicles. On the other hand, this effect makes the reaction times of each vehicle slightly different and consequently more complex to be analyzed. Finally, we analyze the error between SV_{i+1} and SV_i or between SV_{i+1} and SV_0 . The different trigger

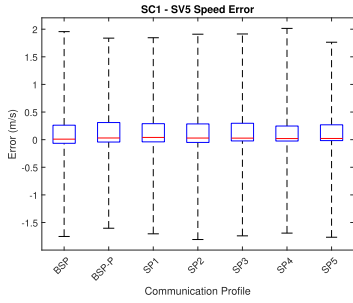


FIGURE 5. SC1 - SV₅ Speed Error Comparison.

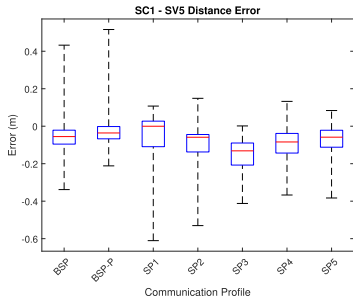


FIGURE 6. SC1 - SV₅ Distance Error Comparison (e_5^δ).

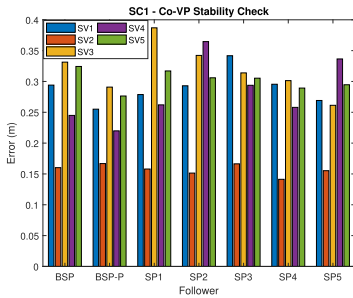


FIGURE 7. SC1 - Co-VP Stability Check.

conditions happen because, although slight, there are variations in the trajectory of SV_0 in each simulation, which affect the movements and activation of their followers' triggers. In each scenario, the behavior of the network was analyzed in terms of **throughput**, **number of sent messages**, and **inter-message delay (IMD)**. The throughput is defined as presented in eq. 4.

$$Throughput = \frac{ReceivedMessages * MessageSize}{time * BitRate} \quad (4)$$

C. STRAIGHT LINE SCENARIO—SC1

1) PLATOON SAFETY

Fig. 5 presents the quantiles of the speed error for SV_5 throughout Scenario 1. The median speed error is close to zero in all profiles, while maximum velocity errors approach $2.0m/s$. The distance error of SV_5 , e_5^δ , is depicted in Fig. 6. We observe that the median of the distance errors tends to be under-estimate (the vehicle is farther than the estimate). 50% of BSP errors fall in a limited range (-0.1 to $0m$), but the profile also overestimates the most. This justifies the

Profile	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	Total
BSP	435	79	292	508	1314
BSP-P	652	47	239	538	1476
SP1	621	64	285	400	1370
SP2	775	60	270	382	1487
SP3	16	639	253	390	1298
SP4	22	644	253	389	1308
SP5	19	650	245	391	1305

FIGURE 8. SC1 - Total Triggers per Profile.

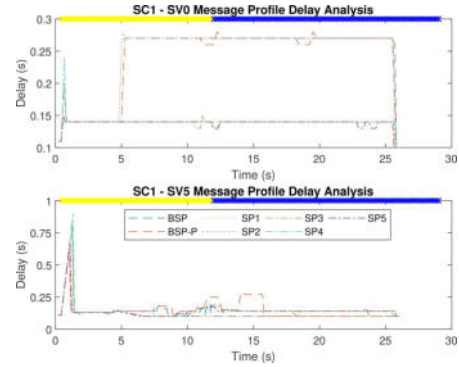


FIGURE 9. SC1 - Message Profile Delay Analysis.

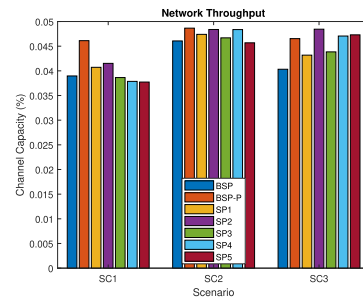


FIGURE 10. Scenarios Throughput.

introduction of BSP-P, in which the behavior is inverted: distances tend to be underestimated. SP1 to SP5 also tend to underestimate distances and have an inferior range of occurrence of error w.r.t. BSP-P, with SP3 having the smallest range (-0.4 to $0m$). Finally Fig. 7 presents the local stability condition for all SPs, demonstrating that the platoon stability is guaranteed since $\mathcal{L}_\infty(e_5^\delta) < \max_1^4(\mathcal{L}_\infty(e_i^\delta))$. These results show that the new profiles do not degrade performance regarding the established profiles (BSP/-P), but even improve it as SP3, SP4, and SP5 reduce e_5^δ in 28% (Fig. 6), as a consequence of the reduction of τ_{Pos} in these specific profiles.

2) NETWORK PERFORMANCE

The inter-message delay (IMD) is shown in Fig. 9 for SV_0 (top) and SV_5 (bottom). The IMD of SV_0 at the start of the trajectory is small for all profiles since it is the speed difference threshold τ_{Speed} that triggers the CAMs. After 5s, when the speed stabilizes, the profiles with higher values of τ_{Pos} trigger messages with low frequencies. This means that the leader occupies less transmission medium in the BSP, BSP-P,

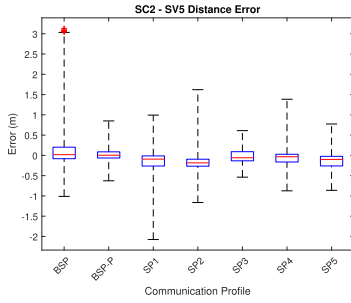


FIGURE 11. SC2 - SV₅ Distance Error (e_5^δ).

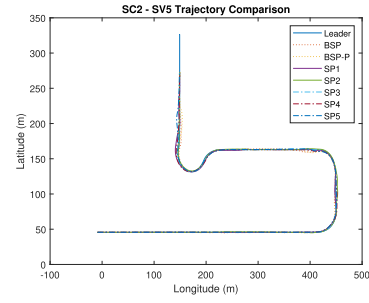


FIGURE 14. SC2 - SV₅ Trajectory Comparison.

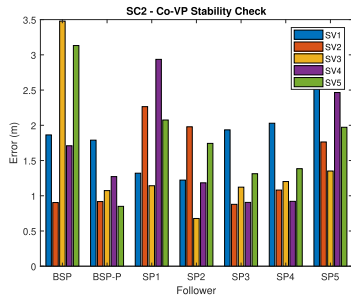


FIGURE 12. SC2 - Co-VP Stability Check.

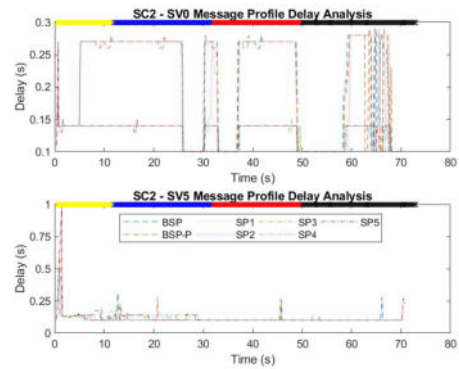


FIGURE 15. SC2 - Message Profile Delay Analysis.

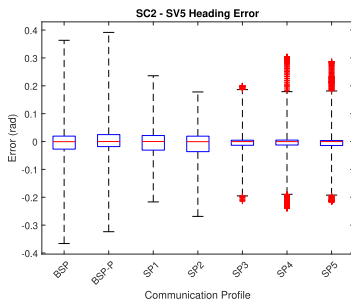


FIGURE 13. SC2 - SV₅ Heading Error (e_5^θ).

Profile	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	Total
BSP	2372	109	254	1011	3746
BSP-P	2435	95	139	1151	3820
SP1	2506	161	267	677	3611
SP2	2914	98	280	505	3797
SP3	1527	957	241	917	3642
SP4	1773	848	232	846	3699
SP5	2055	788	232	659	3734

FIGURE 16. SC2 - Total Triggers per Profile.

SP1, and SP2. However, the bottom of the figure shows that the IMD of SV₅ is nearly the same for all the profiles. This similarity confirms that all the profiles for this vehicle’s quantities produce a similar network load. Fig. 10 shows the vehicle’s throughput, calculated with eq. 4, with a bit rate of 6Mbps [46]. This figure demonstrates that the throughput variation between all profiles does not reach 0.01% of the channel capacity, showing that the better performance of CSP3, CSP4, and CSP5 does not imply considerable overhead in network usage.

3) DISCUSSION

As followers diverge from the leader, they transmit messages at higher rates while correcting their trajectories in profiles with higher errors (BSP, BSP-P, SP1, and SP2). In profiles with a more conservative τ_{Pos} , more messages are fired due to the values of e_i^δ . The cost of sending more messages caused by the tighter trigger values on SP3, SP4, and SP5 is offset by the number of sent messages by other profiles. The last column of

Fig. 8 illustrates this cost, in which the best performing profile (SP3) had 1% fewer messages than the worst performing one (BSP). Furthermore, the minor distance error profiles had the slightest trajectory corrections caused by τ_{Head} .

D. MULTI-CURVE SCENARIO—SC2

1) PLATOON SAFETY

Fig. 11 shows distance error e_5^δ ; as this scenario is more complex than scenario 1, the error tends to increase along the trajectory. This error is a consequence of the Euclidean distance used to calculate $d_{i,i+1}(t)$, since it is affected by the lateral deviation of the vehicles. Due to this, the distance error e_i^δ tends to increase on curves in order to reduce the e_i^θ , avoiding the *cutting-corner effect*. It demonstrates that the maximum variation of the distance error e_5^δ has a 25% reduction with SP1 in comparison with BSP and about 70% with SP3. The SP3 also outperforms the BSP-P in $\approx 15\%$. It means that the reducing τ_{Pos} has a larger influence on the

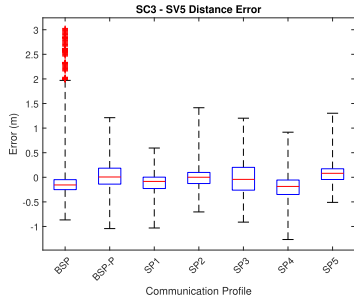


FIGURE 17. SC3 - SV5 Distance Error (e_5^δ).

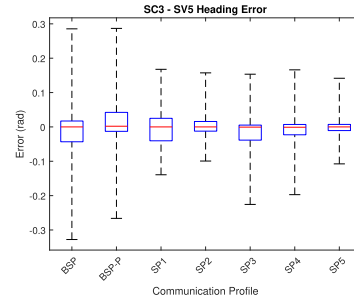


FIGURE 20. SC3 - SV5 Heading Error (e_5^θ).

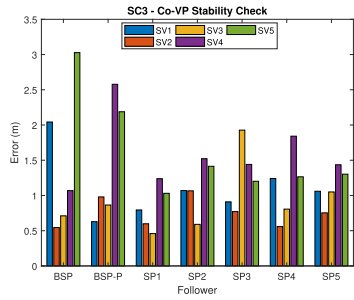


FIGURE 18. SC3 - Co-VP Stability Check.

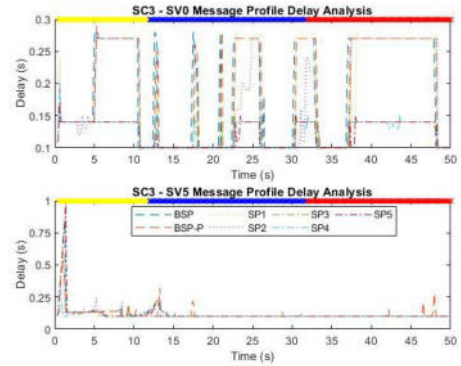


FIGURE 21. SC3 - Message Profile Delay Analysis.

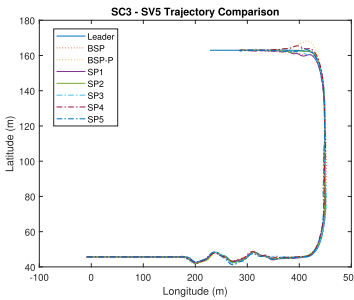


FIGURE 19. SC3 - SV5 Trajectory Comparison.

distance adjustment of the platoon members than τ_{Head} , given that SP3 outperforms SP4 and SP5. In this scenario, BSP end up overestimating e_5^δ , while SP1 underestimates it. Thus, it is possible to observe that the platoon's performance is improved with SP3 since this profile presents the slightest variation (-0.5 to $0.6m$), still having the average value very close to zero. It is also interesting to notice that in the SP1 and SP2 profiles, the more restrictive value of τ_{Head} , without the reduction of τ_{Pos} , causes a slight downward shift in the average of e_5^δ , due to the corrections triggered not by position, but by the heading variation.

The Co-VP performance regarding the distance error is confirmed in the stability check, illustrated in Fig. 12. All the profiles satisfy the *local* stability criteria, and the overall distance error of SP3 for all vehicles is smaller than the other profiles.

In scenario 2, a well-performed trajectory implies a small heading error e_i^θ , which indicates how well followers perform curves concerning the leader. Fig. 14 shows that the leader and vehicle SV5 perform a similar path in all profiles, apart from minor oscillations after the first and the last curves.

Profile	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	Total
BSP	1623	79	294	676	2672
BSP-P	1745	64	271	758	2838
SP1	1876	74	258	509	2717
SP2	2085	60	240	414	2799
SP3	1419	445	253	653	2770
SP4	1633	395	248	532	2808
SP5	1805	409	249	488	2951

FIGURE 22. SC3 - Total Triggers per Profile.

These oscillations can be better visualized in Fig. 13; the worst heading error of SV5, e_5^θ , is near to $0.4rad$ with BSP/P. Again, the best performance is obtained with SP3, since its application reduced the maximum value of e_5^θ in $\approx 50\%$, to $0.2rad$, even with complex curves, also decreasing the total variation between extreme error values.

Fig. 13 also demonstrates that exclusively reducing τ_{Head} leads to a better heading error e_5^θ performance, as SP1 and SP2 lowered it in $\approx 38\%$ in comparison with BSP/P. The analysis of the maximum of e_5^θ in SP4 and SP5 indicates that the impact of reducing τ_{Pos} is greater than reducing τ_{Head} in the proposed profiles.

The impact in the number of transmitted messages relating to the threshold values of the heading difference τ_{Head} and position difference τ_{Pos} in SC2 can be observed in Fig. 16. The threshold of parameter τ_{Head} is the most activated due to the numerous trajectory adjustments of followers to execute the scenario's curves. Under SP3, the combination of a reduced τ_{Pos} with the standard τ_{Head} produces the best general Co-VP performance, reducing distance and lateral

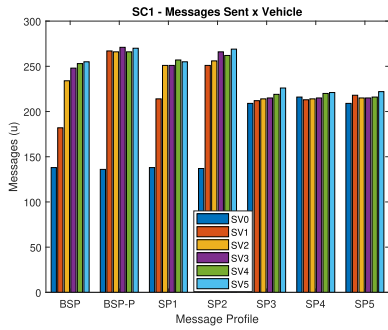


FIGURE 23. SC1 - Sent Messages per Vehicle.

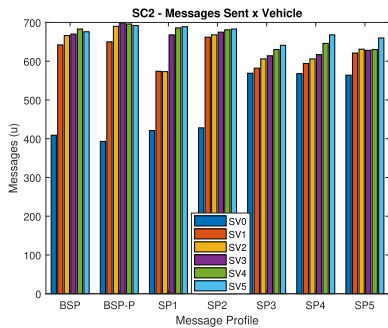


FIGURE 24. SC2 - Sent Messages per Vehicle.

errors (e_5^δ and e_5^θ). These results confirm that reducing τ_{Pos} reduces the longitudinal and lateral errors, as observed in SC1 and SC2. Furthermore, under these conditions, the SP3 reduction improves the BSP-P performance both in e_5^δ and e_i^θ , also reducing the number of sent messages. Reducing τ_{Head} also does so, although to an inferior extent.

2) NETWORK PERFORMANCE

The inter-message delay (IMD) is shown in Fig. 15 for SV_0 (top) and SV_5 (bottom). As SC2 is an extension of SC1, the first interval between 0 – 25s presents a similar behavior. However, after the first curve, at the end of the blue section and the beginning of the red section, we observe in vehicle SV_0 a few periods of high-frequency/slight inter-message delay. These high-frequency periods are caused by the path’s curves and occur in all profiles. After this occurrence, the less restrictive profiles return to a lower message transmission frequency, as expected.

Nevertheless, the message delay of SV_5 presents a low IMD in all profiles, from the beginning to the end of SC2, due to the vehicle’s trajectories adjustments. As in scenario 1, the propagation of control information hop-by-hop, from SV_1 to SV_5 , leads to SV_5 constantly requiring more abrupt adjustments, hence the increased transmission frequency. Fig. 16 illustrates that all profiles have transmitted a similar number of packets at the end of SC2, as in SC1.

3) DISCUSSION

Overall, we observe that SP3 has the best performance in the control metrics, with a saving of transmitted messages, with a reduced τ_{Pos} . This supports our claim that, by altering the

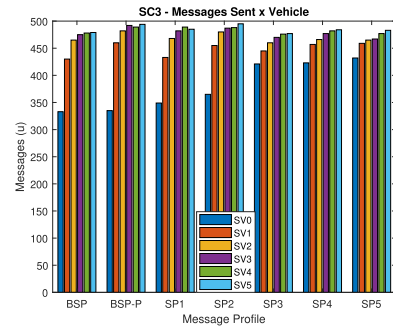


FIGURE 25. SC3 - Sent Messages per Vehicle.

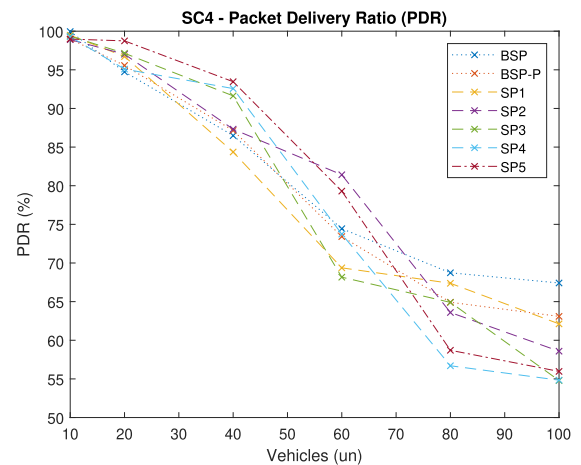


FIGURE 26. SC4 - Packet Delivery Ratio.

message trigger thresholds (τ_{Pos} and τ_{Head}) to become more sensitive, the platoon safety performance is improved without burdening the network, reducing the errors e_i^δ and e_i^θ .

E. OBSTACLE SCENARIO—SC3

1) PLATOON SAFETY

The distance error e_5^δ , presented in Fig. 17, shows that BSP has a similar performance regarding the maximum error variation as in SC2, $\approx 3.5m$, showing that the obstacles cause little or no difference in both scenarios for this profile. However, as in SC1 and SC2, the proposed profiles and the BSP-P present a better e_5^δ performance, reducing the error variation to $\approx 2.0m$, albeit at a larger error than in SC2. This result is expected since obstacles negatively impact the longitudinal platoon performance.

Even under these conditions, the platoon *local* stability is granted in all the proposed profiles, as depicted in Fig. 18, albeit with larger errors than the presented in SC1 and SC2. However, the BSP fails to provide Co-VP stability in SC3, since $\|H(s)\|_\infty > 1$.

As in SC2, the Co-VP performance in SC3 regards the follower’s capacity to perform the same trajectory as the leader, with smaller e_i^θ as possible. So, the SV_5 trajectory in all profiles is presented in Fig. 19, and confirms that all followers avoid the obstacles. However, the accumulated error of the SV_5 trajectory limits the ability of the platoon to perform the

		SV0				SV1				SV2				SV3				SV4				SV5			
Scen.	SP	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}	τ_{Head}	τ_{Pos}	τ_{Speed}	T_{max}
SC1	BSP	1	42	42	53	37	24	44	77	91	6	49	89	108	2	46	93	96	2	55	101	102	3	56	95
	BSP-P	1	37	33	65	122	2	35	108	130	2	41	93	128	0	42	101	136	4	44	82	135	2	44	89
	SP1	1	41	42	54	82	15	43	74	134	5	45	68	132	2	53	65	145	1	48	64	127	0	54	75
	SP2	1	43	40	55	124	9	42	89	147	4	43	68	162	3	44	68	163	0	51	51	178	1	50	51
	SP3	1	107	39	62	1	111	40	60	1	108	40	66	0	109	41	66	4	109	43	64	9	95	50	72
	SP4	5	108	41	65	1	111	40	62	1	112	40	62	0	104	42	70	7	102	40	72	1	107	50	64
	SP5	1	105	39	65	6	112	40	64	1	108	41	66	0	109	40	67	1	112	41	63	10	104	44	66
SC2	BSP	168	82	38	121	400	13	40	189	419	7	41	199	449	5	42	174	467	0	45	171	469	2	48	157
	BSP-P	154	76	16	147	414	17	14	205	455	2	23	210	472	0	23	204	470	0	28	198	470	0	35	187
	SP1	184	81	40	116	371	39	39	125	390	38	43	102	501	3	50	114	517	0	50	119	543	0	45	101
	SP2	196	79	38	115	524	9	40	89	538	5	47	78	545	3	51	76	552	2	51	76	559	0	53	71
	SP3	171	225	39	134	212	203	39	128	246	159	39	162	263	145	39	167	306	125	41	158	329	100	44	168
	SP4	174	225	38	131	249	183	39	123	265	159	39	143	304	139	39	135	362	98	37	149	419	44	40	165
	SP5	181	221	37	125	336	133	38	114	357	125	37	112	371	115	38	104	372	122	35	101	438	72	47	103
SC3	BSP	159	50	41	85	254	17	43	118	287	7	45	128	310	1	56	110	307	3	55	115	306	1	54	120
	BSP-P	167	41	38	102	290	12	35	136	312	5	46	134	324	1	53	129	321	3	52	128	331	2	47	129
	SP1	184	46	42	79	284	19	42	90	329	7	43	90	362	2	32	87	351	0	49	91	366	0	50	72
	SP2	208	38	39	87	340	13	39	67	377	5	41	66	391	1	36	60	382	1	45	64	387	2	40	70
	SP3	161	129	40	95	210	95	37	107	230	75	41	118	256	53	42	122	280	46	42	111	282	47	51	100
	SP4	171	122	40	92	256	76	39	90	270	58	38	102	301	44	41	93	321	49	45	72	314	46	45	83
	SP5	210	115	40	88	296	75	39	82	301	70	38	95	310	61	41	78	339	46	43	71	349	42	48	74

FIGURE 27. Triggers Profile per Vehicle.

second curve (in the red road area) in the same trajectory as the platoon Leader. In this scenario, the BSP-P has more significant oscillation, while the SP1 suffers from the *cutting-corner* effect. As the e_i^δ tends to increase over the curves to reduce the e_i^θ , this effect explains why the SP1 has a slightly better result than the others profiles, as presented in Fig. 17.

The *slalom* maneuver performed in this scenario relies on several curves produced by the leader’s trajectory. So, the τ_{Head} have a direct impact over the in Co-VP heading error (e_i^θ), as illustrated in Fig. 20, while the influence of τ_{Pos} to e_i^θ is reduced, due to the required adjustments, given curves proximity. This figure demonstrates that the SP2 and SP5, with more restricted τ_{Head} values, have a better e_i^θ performance, presenting an improvement of 45% in comparison with the BSP-P. The SP3 also outperforms the ETSI triggers performance in 26%.

2) NETWORK PERFORMANCE

The IMD is directly affected by the *slalom* maneuver, which triggers message transmissions at high frequency in all profiles, as visible in Fig. 21. As in SC1 and SC2, the period between 0 – 10s has similar behaviors, with two well-defined levels, for the BSP, BSP-P, SP1, and SP2, and others for SP3 and SP4 and SP5. However, when the SV_0 starts the object avoidance algorithm, the IMD is directly affected, being reduced for the profile T_{min} . This occurrence indicates where SV_0 avoids the obstacles and when it returns to a straight trajectory before performing the two curves and finally stops at the end of the scenario. As expected, the load on the network caused by SV_0 is slightly smaller in BSP, SP1, and SP2, while the BSP-P has the biggest number of triggered messages. However, as in previous scenarios, this behavior does not correspond to the other platoon vehicles. The bottom figure highlight that the network load caused by SV_5 is the same for all the profiles due to the constant adjustments. However, in this scenario, the restricted τ_{Head} produces a network overhead, as presented in Fig. 10 and confirmed

in Fig. 22. Thus, SP5 implies a 10% overhead over sent messages and about 0.005% over the network capacity.

3) DISCUSSION

In this scenario, the impact of the τ_{Head} restriction becomes more evident since the leader’s *slalom* to avoid obstacles forces the other vehicles to make quick turns to correct their route. While the standard profiles in ETSI ITS G5 present a similar performance in scenarios 1 and 2, the proposed profiles still produce better performance, with lower distance and heading errors. Even the reduction of T_{max} in BSP-P does not reduce the e_i^θ as the proposed profiles. However, this scenario presents an overhead of profiles with a more restricted τ_{Head} , affecting a more crowded network scenario.

The comparison between the SPs standardized by ETSI and those presented here takes into account not only the reduction of e_i^δ and e_i^θ , but also their impact on the network. The analysis of the SC1, SC2, and SC3 results shows that SP1-5 reduces errors compared to BSP in all scenarios and also outperforms BSP-P to a lesser extent in reducing e_i^δ and with great advantage in reducing e_i^θ . The comparison of the cost of the higher constraint triggers can be seen in the Figures 8, 16, and 22, and also reinforced with the Figs. 23, 24, and 25, which illustrate the amount of messages sent by each vehicle in each scenario in each profile tested. These figures show that the evaluated profiles do not increase the number of messages sent by each car and show that BSP, even in simpler scenarios, tends to send more messages to obtain a performance inferior to SP3, for example.

F. NETWORK PERFORMANCE–SC4

The results on network performance presented for Scenarios 1, 2, and 3 showed that proposed SPs have a residual impact on the number of transmitted messages compared to ETSI profiles. In Scenario 4, we extend SC3, the best performing SP, by increasing the number of communicating vehicles to simulate high-density vehicle occupation conditions and,

accordingly, high occupation of the wireless medium. For simplicity, additional 'virtual' vehicles were simulated as if they were in the same position as the leader. This setup, while very pessimistic, allows us to study performance in almost worst-case conditions: when the leader fires a message, the 'virtual' vehicles also send it, inducing an extensive medium usage at that instant. Tests were run with 10, 20, 40, 60, 80, and 100 cars. In SC4, our analysis is limited to Packet Delivery Rate (PDR) related to the increasing number of vehicles.

Fig. 26 shows PDR for each proposed profile as the number of vehicles increases. We assume that a better PDR leads to better Co-VP performance since more messages are being delivered to the followers. However, in this paper, we will not address the PDR decreasing impact on the platooning performance, but just the analysis of how the PDR decreases with the rising number of vehicles in each profile.

Beginning with 10 vehicles, PDR is close to 100% in all profiles, from BSP to SP5, meaning that we can believe that the performance obtained in SC1, SC2, and SC3 should be maintained. Meanwhile, for 20 cars, the variation between the best and the worst PDR is 4%. Thus, under these conditions, the SP5 PDR is $\approx 99\%$ while the BSP PDR is nearly 95%. On the other hand, SP1, SP2, and SP3 PDRs remain around 97%, and SP4 and BSP-P deal with 96%. Therefore, the decreasing PDR should not have a high impact on the Co-VP performance in these conditions. This analysis also shows that the more significant restriction of τ_{Head} and τ_{Pos} does not severely impact the number of packets since the drop in the PDR is directly related to the increase in collisions.

The best PDR response decays to 94% in SP5 while increasing the number of vehicles to 40. On the other hand, the worst PDR response is obtained from the SP1, with 94%. SP3 and SP4 have a similar PDR response as SP5, while BSP, BSP-P, and SP2 have a PDR near 87%.

As expected, when the number of vehicles increases up to 60, the PDR response decreases in all the profiles. However, the best PDR response is obtained in SP2, with 82%, while SP5 decays to 80%. BSP, BSP-P, and SP4 have a PDR of 75%. The SP3 and SP1 have the worst PDR result, close to 69%. Finally, raising the car quantity to 80 and 100 leads the PDR response to under 70% in all the profiles, which indicates a communication link that may cause safety concerns [49].

Discussion The analysis of the PDR chart in Fig. 26 confirms that the profiles proposed with the restriction of τ_{Pos} and τ_{Head} do not cause more network congestion than the ETSI profiles. Furthermore, although their PDR also declines with the increase in network congestion, their performance in SC1, SC2, and SC3 scenarios proves that this is an option that tends to increase the safety of the platoon by reducing errors e_i^δ and e_i^θ .

Considering the proposed scenarios and the results presented, we reinforce the thesis that a greater restriction of the ITS-G5 τ_{Pos} and τ_{Head} triggers positively impacts platooning performance without causing overhead on the communications network. Thus, in adverse conditions, such as obstacles

and curves, the SP1-5 profiles present better performance than those established by ETSI. Moreover, among the profiles presented, it was possible to observe that the SP3 profile represents the best cost-benefit, as it reduces the errors e_5^δ and e_5^θ in all scenarios, without providing overhead concerning the profiles proposed by ETSI. The PDR response of SP3 also indicates this profile's applicability regarding the proposed conditions, with reduced errors and similar network performance compared with other profiles. So, for an up-limited scenario of 40 vehicles, the 94% PDR suits as an acceptable compromise for a Co-VP application, but further investigation is necessary to evaluate the platoon safety condition under more congested scenarios.

Thus, based on the results obtained, we propose the implementation of the Platoon Service Profile (PSP), based on SP3, with a more restricted τ_{Pos} , aiming to increase the platoon's performance, reducing longitudinal and lateral errors. This profile showed an improvement in e_5^δ of 74% on SC2 and 44% on SC3 compared to BSP/P. Also, improved e_5^θ by 42% on SC2 and 50% on SC3 over the same profiles, without increasing overhead. As the scenario proposed in SC3 can be considered extreme, due to the presence of the "slalom", this profile would successfully meet the needs of Co-VP systems in a diversity of scenarios not covered by the ETSI BSP/P.

VI. CONCLUSION AND FUTURE WORKS

This work presented five new Service Profiles, using different message threshold values over triggers τ_{Head} and τ_{Pos} , compared to the BSP and BSP-P profiles proposed in the ETSI specifications. The performance observed in the studied scenarios shows that the proposed adjustments in τ_{Head} and τ_{Pos} positively impact the Co-VP safety performance, reducing both longitudinal and lateral errors.

In SC1 and SC2, SP3 presented the best results, with τ_{Pos} adjusted, while in SC3, the best lateral error was achieved with the τ_{Head} adjustment. Thus, the integrated analysis of all scenarios showed that the joint reduction of the triggers τ_{Head} and τ_{Pos} did not necessarily show the best result in all scenarios in lateral and longitudinal terms. The different results are affected by triggering conditions that cause different adjustments and corrections in the platoon, often increasing longitudinal errors to correct lateral errors.

Furthermore, the need for corrections arising from errors accumulated throughout the platoon and the activated triggers also implied an increase in network load. Thus, it was observed that the use of more restricted triggers did not significantly increase the load on the network since these triggers implied fewer corrections and, consequently, fewer messages sent. Such observation is extended to a scenario of an increase in the number of vehicles, where less restricted triggers do not represent a significant gain in terms of network performance, burdening it in a very similar way in all profiles.

We conclude that reducing the value of τ_{Pos} proposed by the ETSI ITS standard can increase the safety conditions of the platoon in complex scenarios involving curves and even with the presence of obstacles. So, we propose a Platoon

Service Profile (PSP) based on the τ_{Pos} reduction from $4m$ to $2m$. Furthermore, it should also be noted that the reduction of τ_{Head} in very close obstacle scenarios also improves the lateral error, ensuring system safety.

In future work, we will investigate the impact of the drop in PDR with the increase of vehicles on the safety conditions of the platoon. This scenario also suggests the possibility of validating a flexible trigger profile based on road conditions.

APPENDIX A: TRIGGERS ACTIVATION LIST

See Fig. 27.

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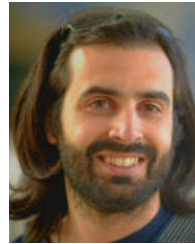
ENIO VASCONCELOS FILHO received the B.Sc. degree in automation and control and the M.Sc. degree in mechatronics systems from the Universidade de Brasília (UnB), in 2006 and 2012, respectively. He is currently pursuing the Ph.D. degree in electrical and computer engineering with the University of Porto (FEUP), Portugal. In 2018, he joined the CISTER Research Unit, working with cyber-physical cooperative systems, notably in vehicular communications. He is currently an

Assistant Professor with the Federal Institute of Goiás (IFG). His most significant research interests include cyber-physical systems, communication networks, and artificial intelligence in real-time applications.



PEDRO M. SANTOS received the B.Sc. and M.Sc. degrees in electrical and computer engineering from the University of Porto, in 2009, and the Ph.D. degree from the University of Porto, in collaboration with the Instituto de Telecomunicações (Portuguese research and development institution), in 2017.

He has been a postdoctoral researcher in numerous national (P2020), European (FP7), and international projects (CMU/Portugal Program), and a Visitor at Carnegie Mellon University for three months (through the CMU/PT Vital Responder project). He is a reviewer for a number of forums on communications and networking (IEEE TRANSACTIONS ON WIRELESS COMMUNICATIONS, VNC, and VTC, among others) and served or serves as a TPC Member for IEEE VNC, WCFS, and EAI Future5V. He is currently an Assistant Researcher at CISTER and an Invited Assistant Lecturer at the University of Porto. His research interests include wireless propagation, vehicular networking, and the Internet-of-Things for smart cities.



RICARDO SEVERINO received the B.Sc., Licentiate, and M.Sc. degrees in electric and computer engineering from the School of Engineering, Polytechnic Institute of Porto, Portugal, in 2004, 2006, and 2008, respectively, and the Ph.D. degree in electrical and computer engineering from the University of Porto, Portugal, in 2015. He was an Integrated Researcher at the CISTER Research Unit, and currently conducts his research at the

Porto Research, Technology, and Innovation Center, Polytechnic Institute of Porto. He has over 15 years' experience on large-scale WSAN infrastructures and the IoT, particularly focusing on their QoS properties. His current research interests include cyber-security, safety, and reliability of wireless communication technologies for cooperative autonomous cyber-physical systems, focusing on the interplay between control and communications. He has also been involved in multiple open-source projects, mostly related to the implementation of the IEEE 802.15.4/ZigBee protocols, in particular within the Open-ZB framework and in the context of the TinyOS15.4-WG and ZigBee-WG working groups, of which he was also a founding member.



ANIS KOUBAA is currently a Professor in computer science, an Advisor to the Rector of Research Governance, the Director of the Research and Initiatives Center, and the Director of the Robotics and Internet of Things Research Laboratory, Prince Sultan University. He is also a Senior Researcher at CISTER/INESC TEC and ISEP-IPP, Porto, Portugal. He is a Senior Fellow of the Higher Education Academy (HEA) in the U.K. He received several distinctions and awards,

including the Rector Research Award at Al-Imam Mohamed bin Saud University, in 2010, and the Rector Teaching Award at Prince Sultan University, in 2016. He is on the list of top 2 of carrier-based scientists worldwide by Stanford University.



EDUARDO TOVAR (Member, IEEE) received the Licentiate, M.Sc., and Ph.D. degrees in electrical and computer engineering from the University of Porto, Porto, Portugal, in 1990, 1995, and 1999, respectively. He is currently a Professor with the Department of Computer Engineering, School of Engineering (ISEP), Polytechnic Institute of Porto (P.Porto), where he is also engaged in research on real-time distributed systems, wireless sensor networks, multiprocessor systems, cyber-

physical systems, and industrial communication systems. He heads the CISTER Laboratory, an internationally renowned research center focusing on RTD in real-time and embedded computing systems. He is currently the Vice-Chair of ACM SIGBED and is a member of the Executive Committee of the IEEE Technical Committee on Real-Time Systems (TC-RTS). He is currently deeply involved in the core team setting-up a Collaborative (industry-academic) Laboratory on Cyber-Physical Systems and Cyber-Security Systems.

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