Preliminary Report of Glaciological Studies

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1. Introduction

During the traverse between Syowa Station and the South Pole in 1968-69 glaciological studies were carried out on the ice sheet of the East Antarctica with the main aim of investigating snow accumulation and snow condition. The items studied were as follows:

1) Measurements of temperature in the holes dug in the snow 10 m deep for seismic shot. The measurements were made at 23 sites (Observer: K. FUJIWARA).

2) Observations of the relief of snow surface at intervals of 2 or 4 km along the route (K. FUJIWARA).

3) Measurements of hardness and temperature on the surface layer of snow at intervals of 8 km between Syowa Station and the South Pole. In addition, measurement of density was made at intervals of 16 km between Syowa Station and the Plateau Station (M. Hosoya, and T. Eto).

4) Measurement of snow accumulation by the snow stakes placed in 1967-68 at intervals of 2 km along the route from Syowa Station to the Plateau Station (A. KOBAYASHI, I. KAWASAKI, and K. FUJIWARA).

5) Stratigraphical studies in the 2m pits dug at 44 sites for determining the annual snow accumulation (K. FUJIWARA).

6) Collection of snow core samples, 10 m long, taken out from the holes dug for seismic shot (K. FUJIWARA).

In this paper the results of studies on the item 1 to 5 are reported. The snow samples mentioned in item 6 were sent to the Institute of Low Temperature Science, Hokkaido University, Sapporo, and studies are now being carried out.

2. Mean Annual Air Temperature

In an ice sheet which never melts, the snow temperature at 10-15 m deep gives an approximate value of the mean annual air temperature at the surface. To obtain the annual air temperature, holes of 10 m depth were dug at 23 sites between Syowa Station and the South Pole, although at five sites the holes were shallower than 10 m.

The temperatures were determined by a thermistor thermometer, keeping

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Station No.	Botto	Date	
Station No.	Depth (m)	Snow temp. $(-^{\circ}C)$	Date
Syowa St.		(10.0)	
16	7.5	14.3	20 Apr. 1968
70	10.0	24.1	12 Feb. 1969
126	10.0	29.2	26 Apr. 1968
170	10.0	30.2	7 Feb. 1969
244	9.2	38.4	17 Oct. 1968
330	10.0	46.0	4 Feb. 1969
400	8.8	52.2	25 Oct. 1968
414	10.0	51.6	31 Jan. 1969
470	9.0	54.6	31 Oct. 1968
"	10.0	54.0	28 Jan. 1969
530	6.2	56.5	5 Nov. 1968
556	10.0	57.1	24 Jan. 1969
590	6.2	60.0	9 Nov. 1968
Plateau St.		(56.6)	
687	8.9	55.5	18 Nov. 1968
747	9.9	51.2	24 Nov. 1968
777	9.5	50.5	26 Nov. 1968
807	9.5	50.3	30 Nov. 1968
837	9.6	49.9	4 Dec. 1968
867	10.0	49.4	7 Dec 1968
897	9.8	49.3	10 Dec. 1968
927	10.0	49.1	12 Dec. 1968
957	9.8	49.2	15 Dec. 1968
975	9.8	49.8	18 Dec. 1968
South Pole		(50.8)	

Table 1. Snow temperature at the depth of 10 metres.

() Adopted from other studies.

enough time before final readings were taken. Care was taken not to leave boring scraps of snow at the bottom of the holes.

The temperatures are listed in Table 1, along with the mean annual air temperature at Syowa, the Plateau, and the South Pole. In Figs. 1 and 2, these snow temperatures at 10 m deep are plotted against the elevation and the distance from the coast along 43° E, respectively. As shown in Fig. 1, the decreasing in temperature with elevation was about 1.0° C/100 m on the marginal slope rising from Syowa Station (approximately sea level) up to St. 170 (2,000 m). The rate increased gradually towards the inland and attained to the value of 1.4° C/100 m in the region from St. 170 (2,000 m) to St. 414 (3,000 m). It reached 2.5^{\circ}C/100 m



Fig. 1. Snow temperature at the depth of 10 m plotted against surface elevation. Solid line: Queen Maud Land after the JARE South Pole Traverse. Broken line: Queen Mary Land after BOGOSLOVSKI.



Fig. 2. Snow temperture at the depth of 10 m plotted against distance from the coast. Solid line: Queen Maud Land after the JARE South Pole Traverse. Broken line: Queen Mary Land after Bocoslovski.

between St. 414 and St. 747, where is located the highest point (St. 556) called Fuji Divide (tentative) on the traverse route. Beyond the divide, the rate decreased to 0.3°C/100 m between St. 747 (3,400 m) and the South Pole (2,800 m). Such change in the lapse rate of temperature suggests that the temperature is influenced not only by elevation but also by latitude and distance from a coast. The increase in the rate from Syowa Station to the Fuji Divide is due to the increase in latitude and distance from a coast, and the decrease from the Fuji Divide to the South Pole is due to the decrease of distance from a coast.

3. Conditions of the Snow Surface

The surface conditions of snow along the traverse route were investigated by observing surface relief, hardness, and density of snow. The results indicated that the surface conditions were distinctly different in different topographic divisions of the East Antarctic ice sheet.

3.1. Surface relief and wind directions

Roughness of snow surface and other surface conditions such as orientation and size of surface relief were measured and photographed at intervals of 2 or



Fig. 3. Surface conditions along the traverse route.

4 km along the route (Photos 1-17). These surface features must have a close connection with the direction of the predominant wind. The observed surface reliefs can be divided into the following four types.

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Deposition type :	Drift form, barchanoid, etc.
Erosion type :	Sastrugi, pit, etc.
Reshuffling type:	An elevation formed by deposition of snow on the leeward side and simultaneous erosion on the windward side.

Faint mark type: Ripple marks, etc.

Table 2, Fig. 3, and General map inside of the back cover, respectively give the orientation, size, and type of surface relief, observed along the traverse route. As shown in Fig. 3, in the region from Syowa Station to 75°S, the surface relief is mostly of deposition, erosion, and reshuffling type and is fairly large in size (40-70 cm in height). A characteristic of surface relief in this region is that its orientations are different with the deposition and erosion types. Relief of the deposition type is oriented parallel to the contour lines while relief of the erosion type is oriented 40° off the direction of the maximum slope (see General map). Therefore, the winds giving rise to the two kinds of relief deviate in direction by $50^{\circ}(=90^{\circ}-40^{\circ})$ from each other. It is highly probable that surface relief of the deposition type is formed by katabatic winds. If this be correct, it would turn out that the influence of cyclonic storms is not confined to the marginal slope but extends into the interior as far as latitude 75°S.

On the antarctic plateau between 75°S and 81°S, relief of the deposition and erosion types was very obscure and no relief higher than 40 cm was found. Near the Fuji Divide, snow surfaces become so smooth that only faint marks like ripples were observed. Beyond the Fuji Divide, the direction of the maximum slope shifts from NNE to SW and so does also the wind direction. In this gently sloping region between 75°S and 81°S, the winds must be mild throughout the year.

Between 81°S and 86°S, no relief other than the reshuffling type was found. The relief was not higher than 40 cm and oriented in two directions of NNE and NNW.

To the south of 86°S, three types of relief, the deposition, the erosion, and the faint marks were observed, disappearing the reshuffling type. The relief was less than 30 cm in height and it changed remarkably in type and size at various portions of the undulations of ice sheet; on the top of the undulations, glazed surfaces were formed, whereas relief of the deposition and erosion types were formed on the bottom.

The angle of deviation between the directions of wind and maximum slope ranges from 60° to 90° in the region extending between $86^{\circ}S$ and the South Pole.

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Photo 1. Sastrugi, like a fine split, in the initial stage of development (at St. 144).



Photo 2. Severe sastrugi carved by a strong wind (at St. 178).



Photo 3. Glazed surface with polygonal pattern of cracks (at St. 186).

Photo 4. The prominent sastrugi with a hard surface. It was so large that the vehicle could not go over it (at St. 222).

Photo 5. Reshuffling type of surface relief. Carving of sastrugi and formation of soft barchan on its lee-side (at St. 272).

Photo 6. Reshuffling type of surface relief. Thin sastrugi and narrow banks are moving leeward on the smooth surface of compact snow (at St. 346).

Photo 7. Reshuffling type of surface relief. Wearing of sastrugi and expansion of thin friable banks with ripple marks (at St. 418).

Photo 8. Smooth surface marked with Y-shaped ripples and senile sastrugi scattered on them (at St. 548).

Photo 9. Typical Y-shaped ripples, interlacing and aligned along axes parallel to the wind direction, at the Fuji Divide (at St. 556).

Photo 10. Complicated surface relief indicating three wind directions near the Fuji Divide (at St. 586).

Photo 11. Friable bank abrased diagonally by a weak wind (at St. 636).

Photo 12. Wearing down of surface relief by wind erosion (at St. 702).

Photo 13. Pitted patterns developed on a smooth surface (at St. 723).

Photo 14. Two types of surface relief, deposition and erosion, showing the wind directions in crossing (at St. 772).

Photo 15. Zonal alignment of a smooth surface (toward lower half of the photograph) and a gullied surface (the distant view), according to the undulated topography of ice sheet (at St. 793).

Photo 16. Very thin barchanoia moving on a smooth surface, to the leeward (at St. 857).

Photo 17. Parallel pattern of cracks on a smooth surface (at St. 910).

Photo 18. Distinct tracks of the caterpillars of a vehicle of the previous year remain on a glazed surface (at St. 186).

Photo 19. The vehicle tracks intermittently covered with moving barchans (at St. 344).

Photo 20. Faint mark of tracks of the vehicle near the Fuji Divide (at St. 548).

Photo 21. Well-developed hoarfrost crystals by sublimation (at St. 690).

Photo 22. A mature sastrugi in the bending stage, on which layers of hoarfrost crystals were blown by winds of moderate intensity (at St. 776). Table 2. Snow accumulation at stakes and surface conditions.

Symbols of snow accumulation

- A: The period between Jan. 1968 and Oct.-Nov. 1968.
- B: The period between Oct.-Nov. 1968 and Jan. 1969.
- C: One year from Jan. 1968 to Jan. 1969.

Symbols of surface-relief size

A: Glazed surface.

- B: Smooth surface with some faint marks.
- C: Less than 10 cm in mean height.
- D: 10 to 20 cm in mean height.
- E: 20 to 40 cm in mean height.
- F: 40 to 70 cm in mean height.
- G: More than 70 cm in mean height.

Symbols of surface-relief type

- d: Deposition type.
- e: Erosion type.
- r: Reshuffling type.
- m: Faint marks.

Values with parentheses were measured by the JARE traverse 1967-68.

Station Eleva-		Height of stakes in the	Snow accumulation at stakes			Survival rate of	Microrelief of snow surface	
		return trip	A	В	С	track	Size	Direction and type
16	m 523	cm 167.0	cm	cm -20,0	cm	%		(61d, 80r)
18	584	103.5			45.5			
20	630							
22	720	118.0	61.0	-19.0	42.0			36d, 84r
24	784	90.3			60.7			
26	838	117.8			40.2			
28	892	120.0	41.5	6.0	47.5			40d, 84r
30	937	92.0			61.0			
32	969		62.0					(66d, 99r)
34	1006	112.2			56.8			
36	1042	103.5	54.5	- 7.5	47.0			(69d, 96r)
38	1073	111.8	41.2	- 1.3	41.2			
40	1098	78,5	59.0	17.5	71.5			(69d, 99r)
42	1128	103.4	58.0	- 6.4	51.6			
44	1150	116.7			41.3			
46	1178	117.5	62.5	-24.5	38.0			(60d, 92r)
48	1193	114.8			45.7			
50	1203	87.5	63.5	9.0	72.5			(69d, 97e)
52	1214	104.0	59.5	- 5.0	54.5			34d, 94r
54	1249	134.9	17.0	3.1	20. 1			

Station Eleva-	Height of stakes in the	Snow	Snow accumulation at stakes			Microrelief of snow surface		
No.	tion	return trip	Α	В	С	track	Size	Direction and type
5.6	m	cm	cm	cm	cm	%		(64d 94r)
50	1200	04.8		- 7.5	55.5 70.2			(010, 511)
50	1275	94.0 106.4	7 1. 5	- 1.5	10.2		!	(36d 89r)
62	1321	05.4	55.0	- 5.4	-5.0 60.6	i.		(35d, 93r)
64	1327	95.4 110.5	34 0	2.5	36.5			(56d - 103r)
66	1345	115.5	41 5	2.5	50.5			(000, 1001)
69	1300	110.7	11.5		30 R			
70	1302	172.0		10.0	55.0		С	34d 82r
70	1355	112.0	41.0	10.0	31.0		D D	014, 021
74	1410	115.0	47.5	-10.0	53.0		D	(50d - 97r)
74 76	1445	117.0	т7.J 49.5	5.5	35.0 35.2		ר ד	(000, 01)
70	1472	110.5	42.J	0.7	56.5			47d 102r
70	1510	119.5	52.5	- 5.0	47.5		D	170, 1021
00 92	1520	121.5	47 0	- 0.0	40.2		D C	(53d - 100r)
02	1529	127.0	47.0	0.0	10.2		D D	(350, 1001)
04	1550	140.2	2.5	-1.7	12.4		D	59d 109r
00	1570	141.0	20.0	-10.0	12.4	8		52u, 1021
00	1576	144.0	10.0	- 1.5	13.5			(25d - 72r)
90	1606	142.5	10.0 28.5	-7.0	16.5			(230, 721)
92	1692	142.5	20.5	- 12.0	20.6			
94	1620	140.4	21.0	- 0.1	20.0			(424 89r)
90	1059	140.0	51.0 10.5	- 5.0	25.4			(120, 051)
90	1675	156.5	19.5	- 0.5	12.5			(364 83n)
100	1693	168.0	7.0	- 0.5	12.5			(300, 051)
102	1607	100.0	7.0	5.0	10.0		17	(39d 86e)
104	1715	160.3	21 5	63	15.9		E	(33d, 36e) 41d 76e
100	1713	172.6	6.5	- 0.5	80		r F	11u, 70c
110	1730	172.0	0.5 81.0	2.T 0.5	0.5 91.5		E	(38d 85e)
112	1745	126.2	48 5	- <u> </u>	44 5		E F	(550, 550)
112	1900	148 4	-10.J 28.0		99 1		L C	(40d 87e)
116	1819	150.7	20.0 40 5	- 3.3	22.1 26.8			(104, 570)
118	1846	192.7	_ 3 5	- 13.7	7 5		n n	
120	1875	176 5	- 5.0	- 1.0 - 1.5	- 7.5 3 5		C C	(33d. 80r)
1 20	1881	144 0	5.0	- 1.5	5.5	1	c	(000, 001)
1 22	1893	183.7	- 45	_ 57	-10.2		Δ	(29d. 76r)
121	1913	178.9	<u> </u>	- 9.7 - 8.2	-10.2		C	36d. 71r
120	1015	150.5	- 2.0	- 0.2	90.0		E	

Station No.	Eleva- tion	Height of stakes in the	Snow	Snow accumulation at stakes		Survival rate of	Micror	elief of snow surface
		return trip	A	В	С	track	Size	Direction and type
130	1923 ^m	cm 114.3	cm - 1.5	cm 1, 2	-0.3	%	Е	(19d. 66e)
132	1942	165.1	_ 1.0	- 4.6	- 5.6		D	(104, 000)
134	1932	142.5	-		-		D	(30d. 77r)
136	1933	165.0	9.0	- 4.0	5.0		_	43d. 87r
138	1949	153.2	32.0	- 6.2	25.8	5		, -
140	1961	118.0	49.0	- 7.0	42.0	3	D	(32d, 79r)
142	1976	170.0	- 4.5	0	- 4.5	50	С	
144	1982	151.0	27.0	- 4.0	23.0	5	Е	
146	1984	165.3	- 1.0	- 5.3	- 6.3	46	D	39d, 75r
148	1987	154.8	- 2.0	- 3.8	- 5.8	28	D	
150	2001	154.2	- 1.5	10.3	8.8	95	А	(46d, 93r)
152	2001	151.7	11.5	- 4.7	6.8	52	Е	
154	2005	106.0	53.0	0	53.0	0	С	
156	2005	165.3	9.5	-10.8	- 1.3	20	D	(32d, 81r)
158	2023	153.6	9.0	- 7.6	1.4	60	D	
160	2032	144.0	31.5	-10.5	21.0	31	D	(38d, 85r)
162	2045	136.5	27.7	- 5.2	22.5	25	D	
164	2060	138.3	29.5	- 5.8	23.7	10	Е	
166	2052	137.7	23.5	- 5.2	18.3	2	Е	(32d, 81e)
168	2054	132.8	34.5	-10.3	24.2	5	F	43d, 80r
170	2062	102.5	76.0	-14.5	61.5	0	F	(44d, 91r)
172	2069	158.3	17.0	- 7.3	9.7	10	F	56d, 109r
174	2044	169.8	- 3.0	- 4.8	- 7.8	50	E	
176	2081	165.5	- 2.0	- 2.5	- 4.5	45	А	(44d, 91r)
178	2075	105.2	64.5	- 6.2	58.3	5	F	
180	2087	161.2	4.0	- 4.2	- 0.2	40	D	(52d, 99e)
182	2113	149.2			18.0	80	А	
184	2152	140.1	27.0	- 6.1	20.9	5	D	(50d, 97e)
186	2172	168.8	- 2.0	- 4.8	- 6.8	95	А	36d, 101r
188	2183	168.8	5.0	- 5.8	- 0.8	25	E	
190	2210	154.0		- 7.0		0	G	66d, 97e
192	2236	196.0	-26.0	- 7.0	-33.0		F	
194	2253	137.6			29.4	0	F	
196	2275	161.0			4.0	75	D	(46d, 83r)
198	2295	176.5	- 2.0	- 3.5	- 5.5	15	E	
200	2312	160.2	- 1.0	2.8	1.8	28	F	(52d, 99r)
202	2311	116.8			45.7	0	F	

Station Eleva- No. tion Height		Height of stakes in the	Snow	accumu at stakes	lation	Survival rate of	elief of snow surface	
		return trip	А	В	С	track	Size	Direction and type
204	m 2332	cm 176.2	cm - 1.5	cm - 6.2	cm	70	С	(46d, 96r)
206	2342	166.3	5.0	- 5.8	- 0.8		F	73d, 103e
208	2348	124.0	47.5	- 9.5	38.0	0	F	(54d, 101e)
210	2359	152.5	9.5	1.3	10.8	50	Е	
212	2373	162.0	- 1.0	- 3.0	- 4.0	58	С	
214	2394	179.8	- 0.5	- 3.8	- 4.3	43	С	(49d, 96r)
216	2407	131.5	-14.7	- 3.0	-11.7	5	Е	51d, 96r
218	2420	125.8	19.0	14.2	33.2	5	Е	
220	2427	164.7			13.3	30	D	(66d, 113r)
222	2444	160.5	7.0	- 7.5	- 0.5		F	
224	2460	145.8	2.0	10.2	12.2		F	
226	2478					50	Е	(48d, 95r)
228	2490	179.4	- 1.0	- 4.4	- 5.4	93	А	
230	2517	159.4	•	- 3.4	- 3.4	90	С	(51d, 98r)
232	2523	142.0			9.0	20	E	
234	2535	167.8	3.0	- 4.8	- 1.8	35	D	
236	2548	153.0	3.0	- 4.0	- 1.0	95	А	(65d, 112r)
238	2569	149.9	- 1.5	- 2.9	- 4.4	75	С	
240	2590	166.0	- 1.0	- 3.0	- 4.0	43	D	(53d, 100r)
242	2607	129.1	- 1.5	16.9	15.4		E	
244	2617	113.7	47.5	11.7	35.8	0	F	(63d, 110r)
246	2622	111.4	50.0	5.6	55.6	5	F	
248	2626	122.2	- 5.0	49.8	44.8	95	С	
250	2654	156.4	- 2.0	7.6	5.6	90	А	(56d, 103r)
252	2681	142.3	0	8.7	8.7	60	А	
254	2708	155.9	- 1.5	8.1	6.6	30	E	70d, 110r, 120r
256	2710	127.2	37.0	6.8	43.8	10	F	(63d, 110r)
258	2719	130.8	21.5	11.7	33.2	0	F	
260	2727	155.0	- 2.0	13.5	11.5	0	E	(65d, 112r)
262	2734	105.0	53.0	10.0	63.0	0	E	
264	2721	157.0	8.5	- 7.5	1.0	90	А	
266	2780	166.0	- 0.5	- 1.0	- 1.5	65	А	(63d, 110r)
268	2790	155.3	6.5	4.2	10.7	20	D	
270	2802	152.4	31.5	- 9.9	21.6	5	F	80d, 106e, 170e
272	2805	122.8	41.5	- 2.3	39.2	20	F	
274	2804	95.0	39.0	16.0	55.0	20	E	(59d, 106r)
276	2822	146.9	15.0	- 2.9	12.1	30	D	

Station No. Height of time Snow accumulation at stakes Survival track Microrlef of snow surface 278 2837 134.8 34.5 0.2 34.7 20% D 100r, 115e 280 2841 143.8 -4.0 -3.8 -7.8 55 D (69d, 116e) 282 2860 120.2 16.0 4.8 20.8 16 D 284 2887 175.0 -0.5 -2.1 -2.6 95 C 288 2936 192.2 -0.5 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F (62d, 112e) 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F 74d, 100r, 114e 296 2966 147.4 19.0 21.6 40.6 50 F (60d, 120e)									
No. Uth Instruction return trip A A B C track Size Direction and type 278 2837 134.8 34.5 0.2 34.7 20 D 100r, 115e 280 2841 143.8 - 4.0 - 3.8 - 7.8 55 D (69d, 116e) 282 2860 120.2 16.0 4.8 20.8 16 D 284 2887 175.0 - 0.5 - 2.1 - 2.6 95 C 2868 2921 155.0 - 1.5 - 2.0 - 3.5 50 D (64d, 114e) 288 2936 192.2 - 0.5 - 1.5 - 2.0 F (62d, 112e) 290 2942 151.6 29.0 2.4 31.4 5 F (62d, 112e) 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 - 0.5 - 1.5 - 2.0	Station	Eleva-	Height of stakes in the	Snow	accumu at stakes	lation	Survival rate of	Microre	lief of snow surface
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	INU.	tion	return trip	Α	В	С	track	Size	Direction and type
278 2837 134.8 34.5 0.2 34.7 20 D $100r, 115e$ 280 2841 143.8 -4.0 -3.8 -7.8 55 D $(69d, 116e)$ 282 2860 120.2 16.0 4.8 20.8 16 D 284 2887 175.0 -0.5 -2.1 -2.6 95 C 286 2921 155.0 -1.5 -2.0 -3.5 50 D $(64d, 114e)$ 288 2936 192.2 -0.5 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F $(62d, 112e)$ 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d, 100r, 114e$ 296 2966 147.4 19.0 21.6 40.6 50 F $(60d, 120e)$ 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 8.5 8.5 45 E 310 3054 138.9 40.0 <t< td=""><td>070</td><td>m</td><td>cm</td><td>cm</td><td>cm</td><td>cm</td><td>%</td><td></td><td></td></t<>	070	m	cm	cm	cm	cm	%		
280 2841 143.8 -4.0 -3.8 -7.8 55 D (69d, 116e) 282 2860 120.2 16.0 4.8 20.8 16 D 284 2887 175.0 -0.5 -2.1 -2.6 95 C 286 2921 155.0 -1.5 -2.0 -3.5 50 D (64d, 114e) 288 2936 192.2 -0.5 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F (62d, 112e) 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d$, 100r, 114e 296 2966 147.4 19.0 21.6 40.6 50 F (60d, 120e) 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d$, $104r$, $119e$ 302 3018 122.2 50.0 -2.2 47.8 25 E (65d, 115e) 306 3042 116.7 50.0 -2.2 47.8 25 E (65d, 115e) 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D 441 03	278	2837	134.8	34.5	0.2	34.7	20	D	100r, 115e
282 2800 120.2 16.0 4.8 20.8 16 D 284 2887 175.0 -0.5 -2.1 -2.6 95 C 286 2921 155.0 -1.5 -2.0 -3.5 50 D $(64d, 114e)$ 288 2936 192.2 -0.5 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F $(62d, 112e)$ 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d, 100r, 114e$ 296 2966 147.4 19.0 21.6 40.6 50 F $(60d, 120e)$ 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E 310 3054 138.9 40.0 1.1 41.1 5 D 314 3059 157.8 -1.5 -2.3 -3.8 30 F 314 3059 157.8 -1.5 -2.4 <td>280</td> <td>2841</td> <td>143.8</td> <td>- 4.0</td> <td>- 3.8</td> <td>- /.8</td> <td>55</td> <td>D</td> <td>(69d, 116e)</td>	280	2841	143.8	- 4.0	- 3.8	- /.8	55	D	(69d, 116e)
284 2867 175.0 -0.5 -2.1 -2.6 95 C 286 2921 155.0 -1.5 -2.0 -3.5 50 D $(64d, 114e)$ 288 2936 192.2 -0.5 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F $(62d, 112e)$ 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d, 100r, 114e$ 296 2966 147.4 19.0 21.6 40.6 50 F $(60d, 12ce)$ 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -5.6 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 118.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 <	282	2860	120.2	16.0	4.8	20.8	16	D	
286 2921 133.0 -1.5 -2.0 -3.5 50 D $(64d, 114e)$ 288 2936 192.2 -0.5 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F $(62d, 112e)$ 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d, 100r, 114e$ 296 2966 147.4 19.0 21.6 40.6 50 F $(60d, 120e)$ 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 118.9 40.0 1.1 41.1 5 D $64d$ 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 320 3094 182.4 2.5 -2.4	284	2887	175.0	- 0.5	- 2.1	- 2.6	95 50	С	/
266 2936 152.2 -0.3 -2.2 -2.7 30 E 290 2942 151.6 29.0 2.4 31.4 5 F (62d, 112e) 292 2938 62.0 70.5 23.0 93.5 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d$, 100r, 114e 296 2966 147.4 19.0 21.6 40.6 50 F ($60d$, 120e) 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d$, $104r$, $119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 37 E 318 3087 159.8 -1.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0	200	2921	155.0	- 1.5	- 2.0	- 3.5	50	D	(64d, 114e)
2502942151.629.02.431.45F(62d, 112e)2922938 62.0 70.5 23.0 93.5 60 E2942967 173.5 -0.5 -1.5 -2.0 F $74d$, 100r, 114e2962966 147.4 19.0 21.6 40.6 50 F $(60d, 120e)$ 2982979 134.3 12.5 19.7 32.2 50 G3003003 162.0 59.0 -56.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 322 3120 115.0 44.0 -4.0 40.0 20 F $65d$, $119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 </td <td>200</td> <td>2930</td> <td>192.2</td> <td>- 0.5</td> <td>- 2.2</td> <td>- 2.7</td> <td>30</td> <td>E</td> <td></td>	200	2930	192.2	- 0.5	- 2.2	- 2.7	30	E	
292 2938 62.0 70.3 23.0 93.3 60 E 294 2967 173.5 -0.5 -1.5 -2.0 F $74d, 100r, 114e$ 296 2966 147.4 19.0 21.6 40.6 50 F $(60d, 120e)$ 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d$, $119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 <td>290</td> <td>2942</td> <td>151.6</td> <td>29.0</td> <td>2.4</td> <td>31.4</td> <td>5</td> <td>F</td> <td>(62d, 112e)</td>	290	2942	151.6	29.0	2.4	31.4	5	F	(62d, 112e)
294 2967 173.3 -0.3 -1.3 -2.0 F $74d$, 100r, 114e 296 2966 147.4 19.0 21.6 40.6 50 F $(60d, 120e)$ 298 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E 308 3046 167.5 0 8.5 8.5 455 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d, 91r, 113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5	292	2936	02.0 172.5	70.5	23.0	93.5	60	E	
2962966147.419.021.640.650F(60d, 120e)2982979134.312.519.732.250G3003003162.059.0 -56.0 3.030G61d, 104r, 119e3023018122.250.0 -5.2 44.890C3043038160.2 -1.0 -1.8 -2.8 70D3063042116.750.0 -2.2 47.825E(65d, 115e)3083046167.508.58.545E3103054138.940.01.141.15D64d, 91r, 113e3123054111.033.535.569.00E3143059157.8 -1.5 -2.3 -3.8 30F3163069127.026.0 -2.5 23.530F(55d, 72r)3183087159.8 -1.5 -2.8 -3.8 37E3203094182.42.5 -2.4 0.120F66d, 119e3223120115.044.0 -4.0 40.020F65d, 119e3243143172.0 -1.0 -3.0 -4.0 55G3263150153.7 4.5 -1.7 2.850F(67d, 117e)3283163132.6 7.5 9.917.480D12.5 <td>294</td> <td>2967</td> <td>173.5</td> <td>-0.5</td> <td>- 1.5</td> <td>- 2.0</td> <td>50</td> <td>F</td> <td>74d, 100r, 114e</td>	294	2967	173.5	-0.5	- 1.5	- 2.0	50	F	74d, 100r, 114e
296 2979 134.3 12.5 19.7 32.2 50 G 300 3003 162.0 59.0 -56.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d, 91r, 113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6	290	2966	147.4	19.0	21.6	40.6	50	F	(60d, 120e)
300 3003 162.0 39.0 -36.0 3.0 30 G $61d, 104r, 119e$ 302 3018 122.2 50.0 -5.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d, 91r, 113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $65d, 119e$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12	296	2979	134.3	12.5	19.7	32.2	50	G	
302 3018 122.2 50.0 -3.2 44.8 90 C 304 3038 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d, 91r, 113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E $(67d, 117e)$	300	2010	102.0	59.0	- 36.0	3.0	30	G	61d, 104r, 119e
304 3036 160.2 -1.0 -1.8 -2.8 70 D 306 3042 116.7 50.0 -2.2 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E $(67d, 117e)$	302 204	3018	122.2	50.0	- 5.2	44.8	90	C	
300 3042 116.7 50.0 $= 2.2$ 47.8 25 E $(65d, 115e)$ 308 3046 167.5 0 8.5 8.5 45 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d$, $119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 455 E $(67d, 117e)$	304	2042	100.2	- 1.0	- 1.0	- 2.8	70	D	
306 3046 107.3 0 8.3 8.5 435 E 310 3054 138.9 40.0 1.1 41.1 5 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d$, $119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 455 E $(67d, 117e)$	300	2042	167.5	50.0	- 2.2	47.8	25	E	(65d, 115e)
310 3034 138.9 40.0 1.1 41.1 3 D $64d$, $91r$, $113e$ 312 3054 111.0 33.5 35.5 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 455 E $(67d, 117e)$	310	3040 2054	107.5	10 0	0.5	8.3	43 5	E	C41 01 119
312 3034 111.0 33.3 33.3 69.0 0 E 314 3059 157.8 -1.5 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F (69d, 119e) 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F (67d, 117e) 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E (67d, 117e) 332 3180 148.0 -1.5 14.0 12.5 20 F	310	2054	130.9	40.0	1.1	41.1	о О	D	64d, 91r, 113e
311 3033 137.8 -1.3 -2.3 -3.8 30 F 316 3069 127.0 26.0 -2.5 23.5 30 F $(55d, 72r)$ 318 3087 159.8 -1.5 -2.8 -3.8 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 -4.0 40.0 20 F $65d, 119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 455 E $(67d, 117e)$ 332 3180 148.0 -1.5 14.0 12.5 200 F </td <td>314</td> <td>3059</td> <td>111.0</td> <td>33.5</td> <td>33.3</td> <td>2 0</td> <td>20</td> <td>E</td> <td></td>	314	3059	111.0	33.5	33.3	2 0	20	E	
310 3003 127.0 20.0 $= 2.3$ 23.3 300 F $(33d, 72f)$ 318 3087 159.8 $= 1.5$ $= 2.8$ $= 3.8$ 37 E 320 3094 182.4 2.5 $= 2.4$ 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 $= 4.0$ 40.0 20 F $65d, 119e$ 324 3143 172.0 $= 1.0$ $= 3.0$ $= 4.0$ 55 G 326 3150 153.7 4.5 $= 1.7$ 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E $(67d, 117e)$ 332 3180 148.0 $= 1.5$ 14.0 12.5 20 F	316	3060	137.8	-1.5	- 2.5	- 5.0	30 20	r F	
310 3007 133.0 -1.3 -2.8 -3.6 37 E 320 3094 182.4 2.5 -2.4 0.1 20 F (69d, 119e) 322 3120 115.0 44.0 -4.0 40.0 20 F $65d$, $119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F (67d, 117e) 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E (67d, 117e) 332 3180 148.0 -1.5 14.0 12.5 20 F	318	3087	150.8	20.0	- 2.5	23.3	30 27	r F	(55d, 72f)
320 3034 102.4 2.3 $= 2.4$ 0.1 20 F $(69d, 119e)$ 322 3120 115.0 44.0 $= 4.0$ 40.0 20 F $65d, 119e$ 324 3143 172.0 $= 1.0$ $= 3.0$ $= 4.0$ 55 G 326 3150 153.7 4.5 $= 1.7$ 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E $(67d, 117e)$ 332 3180 148.0 $= 1.5$ 14.0 12.5 20 F	320	3007	182.4	- 1.5	- 2.0	- 5.0	37 20	E E	(60 + 110 +)
322 3120 113.0 41.0 40.0 20 F $63d$, $119e$ 324 3143 172.0 -1.0 -3.0 -4.0 55 G 326 3150 153.7 4.5 -1.7 2.8 50 F $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E $(67d, 117e)$ 332 3180 148.0 -1.5 14.0 12.5 20 F	320	3120	115.0	2. J 44_0	- 2.4	40.0	20	r F	(09d, 119e)
321 3113 112.0 -1.0 -3.0 -4.0 33 G 326 3150 153.7 4.5 -1.7 2.8 50 F (67d, 117e) 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E (67d, 117e) 332 3180 148.0 -1.5 14.0 12.5 20 F	322	3143	172.0	- 1.0	- 1.0	40.0	20 55	r C	03 a , 119e
326 3150 135.7 4.5 -1.7 2.6 30 1 $(67d, 117e)$ 328 3163 132.6 7.5 9.9 17.4 80 D 330 3177 143.6 12.5 0.9 13.4 45 E $(67d, 117e)$ 332 3180 148.0 -1.5 14.0 12.5 20 E	326	3150	153 7	- 1.0 4 5	5.0	- 4.0 2.8	50	G F	(67d 117a)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	328	3163	132.6	75	- 1.7	17 4	20 20	r D	(0/0, 11/2)
332 3180 148.0 -1.5 14.0 12.5 20 F	320	3177	143.6	12.5	9.9 0 9	17.7	45	D F	(67d 117a)
(1)	330	3180	148.0	-15	14 0	19.4 19.5	4J 20	E	(0/0, 11/2)
334 3194 6.5 50 F 89d 124e	334	3194	110.0	6.5	11.0	12.5	20 50	F	89d 124e
336 3204 131.0 23.0 5.0 28.0 40 F (61d 111r)	336	3204	131.0	23.0	5.0	28.0	30 40	F	(61d - 111r)
338 3210 90.0 42.5 20.0 62.5 5 G	338	3210	90.0	42.5	20.0	20.0 62.5	 5	G	
340 3220 123.2 -8.0 36.8 24.8 45 G (69d 115r 119e)	340	3220	123.2	- 8.0	20.0 36.8	24 8	45	6 G	(69d. 115r. 119e)
342 3228 136.3 -2.0 10.7 8.7 95 E	342	3228	136.3	-20	10 7	8.7	95	E	(004, 1101, 1100)
344 3247 153.2 -1.0 7.8 6.8 65 E 111r 128e	344	3247	153.2	- 1.0	7.8	6.8	65	E	111r. 128e
346 3263 142.2 15.5 -4.7 10.8 46 D $(71d \ 104r \ 121e)$	346	3263	142.2	15.5	- 4.7	10.8	46	D	(71d, 104r, 121e)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	348	3278	157.9	0.5	- 0.4	0.1	20	E	,,
350 3275 104.5 43.0 -13.5 56.5 5 F 88d, 120r, 138e	350	3275	104.5	43.0	-13.5	56.5	5	F	88d, 120r, 138e

Station No.	Eleva- tion	Height of stakes in the	Snow	Snow accumulation at stakes		Survival rate of	elief of snow surface	
		return trip	А	В	С	track	Size	Direction and type
352	m 3284	ст 136.9	-1.0	ст 25.1	cm 24.1	25	F	
354	3294	150.5	21.5	3.0	24.5	17	F	
356	3314	169.0	- 1.5	- 1.0	- 2.5	50	F	78d, 128e, 138e
358	3332	153.1	5.0	- 3.1	1.9	35	F	
360	3333	133.8	14.0	8.7	22.7	20	Е	82d, 120e
362	3335	174.5	- 2.0	- 0.5	- 2.5	35	Е	
364	3351	156.0	- 2.0	0.5	- 1.5	55	F	(65d, 115e)
366	3353	142.9	25.5	0.1	25.6	40	G	
368	3362	157.7	0	- 2.7	- 2.7	41	F	88d, 132e
370	3371	160.0	2.0	5.5	7.5	20	F	
372	3387	184.4	- 0.5	28.9	28.4	20	F	
374	3399	153.0	7.0	6.0	13.0	35	F	(58d, 98r, 114e)
376	3407	115.0	- 1.0	28.0	27.0	35	E	48r, 103r, 123e
378	3416	166.0	10.0	- 3.6	6.4	33	E	
380	3423	159.7	5.0	3.3	8.3	20	D	102r, 130e
382	3437	147.5	16.0	- 3.5	12.5	30	D	
384	3437	141.5	12.0	4.5	16.5	25	С	
386	3434	131.4	24.0	- 2.4	21.6	25	D	
388	3447	136.0	24.5	- 1.0	23.5	25	Е	
390	3450	138.3	-16.5	13.7	- 2.8	20	E	
392	3457	140.0	-14.0	3.0	17.0		E	
394	3461	136.5	13.5	7.5	21.0		F	f
396	3475	156.6	0	3.4	3.4		\mathbf{C}	
398	3480	156.0	5.5	1.5	7.0		D	78d, 108r, 130e
400	3478	150.3	4.5	7.2	11.7	20	D	
402	3483	163.4	1.5	- 3.4	- 1.9		D	73d, 118r
404	3483	143.4	9.0	12.1	21.1	25	D	
406	3495	119.4	28.5	8.1	36.6	30	D	100r, 136e
408	3500	160.9	1.0	- 0.9	0.1	20	Е	
410	3499	159.6	- 1.5	- 0.1	- 1.6		D	70d, 156e
412	3505	147.3	8.0	- 0.3	7.7		D	
414	3519	145.0	11.0	0	11.0	20	D	132e
416	3513	151.8	17.5	- 1.3	16.2	10	D	
418	3514	148.9	5.0	6.1	11.1		E	
420	3529	143.0	30.0	0	3.0		Ε	
422	3.526	148.8	8.5	8. 7	17.2	30	D	
424	3537	154.5	8.5	2.0	10.5		D	

Station No.	Eleva- tion	Height of stakes in the	Snow	v accumu at stakes	lation	Survival rate of	Micror	icrorelief of snow surface	
		return trip	А	В	С	track	Size	Direction and type	
426	m 3543	cm 151.8	cm 10_0	cm 3 2	cm 13-2	%	D	130r	
428	3546	157.8	1.0	3.2	4 2		D	1301 128r	
430	3547	139.6	8.0	10.4	18.4	25	F	1201	
432	3548	135.3	27.5	- 2.3	25.2		Ē		
434	3544	149.5	5.0	7.5	12.5	2	E		
436	3548	146.8	19.5	2.7	22.2	30	D		
438	3549	152.9	14.0	0.1	14.1		D		
440	3556	158.3	1.5	3.2	4.7		D		
442	3555	151.8	7.0	4.2	11.2		С	93d. 136r	
444	3556	164.8	1.0	3.2	4.2		\mathbf{C}		
446	3559	138.8	14.5	1.2	15.7		D		
448	3569	137.9	18.0	- 0.9	17.1		\mathbf{C}		
450	3584	138.2	8.0	3.8	11.8		С	j	
452	3591	150.2	- 3.0	4.8	1.8		С	93d, 138r	
454	3594	140.4	15.0	2.6	17.6		Λ		
456	3591	142.5	0	14.0	14.0		\mathbf{C}		
458	3594	158.8	3.0	2.2	5.2	ver.	F		
460	3604	145.5	- 1.5	7.5	6.0	co	Е		
462	3612	145.2	8.0	3.2	4.8	ŇO	Е		
464	3613	132.7	13.0	6.3	19.3	us	\mathbf{C}		
466	3614	145.2	9.5			hin	\mathbf{C}	137r	
468	3616	147.5	8.0	3.5	11.5	r t	\mathbf{C}		
470	3613	149.0	0	15.5	15.5	nde	D		
472	3617	139.6	16.5	- 2.1	14.4	n o	Е		
474	3622	130.8	21.0	0.2	21.2	race	Е	5	
476	3624	151.0	15.5	3.5	19.0	it t	F		
478	3629	128.8	22.5	1.7	24.2	air	Е		
480	3635		17.5				F		
482	3639	129.5	5.0	7.5	12.5		E	132r, 14 2 r	
484	3642	139.9	12.0	2.9	9.1		D		
486	3632	139.1	18.0	5.9	23.9		\mathbf{C}		
488	3637	149.0	6.0	2.0	8.0		\mathbf{C}		
490	3642	139.0	11.0	0.5	11.5		С		
492	3640	148.7	1.5	0.8	2.3		С		
494	3645	140.0	11.5	- 3.5	8.0		D	н. 1	
496	3646	145.7	14.5	- 1.2	14.3		D	102m, 132r	
498	3652	146.8	8.5	1.7	11.2		D		

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Station No.	Eleva-	Height of stakes in the	Snow accumulation at stakes		Survival rate of	Micror	elief of snow surface	
	tion	return trip	А	В	С	track	Size	Direction and type
500	m 3652	cm	cm	cm	cm	%	Л	· · · · · · · · · · · · · · · · · · ·
500	3648	141.0	12.0	-0.2	12.4		E	
502 504	3653	143.0	12.0	1.5	12.0		E	
506	3655	144 0	4 0	6.0	10.0		F	98r 138r
508	3672	132.2	10.0	16.8	26.8		E	501, 1001
510	3672	138.6	10.0	2.9	12.9		E	
512	3675	141 2	14.0	3.8	17.8		D	
514 ⁻	3673	149.0	12.5	2.0	14.5		C	
516	3674	146.3	14.0	2.7	16.7		С	
518	3675	130.8		0.2	-		С	132r, 139r
520	3673	133.4	-18.5	21.6	13.1		С	,
522	3683	148.3	1.0	1.7	2.7		С	1
524	3694	150.3	10.0	0.3	10.7		С	129r, 142r
526	3691	145.6	10.0	- 1.6	8.4	ovei	С	
528	3694	146.1	3.5	7.9	11.4	v v	С	
530	3696	152.5	1.5	2.0	3.5	Nou	С	
532	3699	156.2	0	1.8	1.8	u s	С	
534	3702	159.8	3.0	1.2	4.2	thi	В	
536	3698	146.0	8.0	4.0	12.0	der	В	
538	3693	152.5	4.0	9.0	13.0	nuc	В	
540	3710	146.5	14.5	- 3.5	11.0	lce	В	
542	3709	134.4	13.0	5.6	18.6	tra	В	
544	3704	143.6	12.0	- 0.6	11.4	tint	В	122m, 132r
546	3708	136.5	19.0	- 5.5	13.5	Fа	В	
548	3712	142.6	5.0	4.4	9.4		В	
550	3714	123.2	25.0	- 2.2	21.8		В	
552	3713	139.0	20.5	- 8.0	12.0		В	122m, 135r
554	3714	144.0	16.0	- 3.0	13.0		В	
556	3717	137.8	14.0	0.2	14.2		В	106m, 127m, 154r
558	3715	143.8	15.5	- 1.3	14.2		В	
560	3714	139.0	14.0	- 1.0	13.0		В	
562	3712	145.5	16.0	- 0.5	15.5		В	122m, 132e
564	3712	143.6	1.0	11.4	12.4		В	
566	3709	134.6	9.0	4.4	13.4		В	
568	3711	120.5	29.0	4.5	33.5		В	
570	3710	125.8	12.5	16.7	29.2		В	
572	3708	143.5	6.0	1.5	7.5		В	

Station No.	Eleva- tion	Height of stakes in the	Snow	/ accumu at stakes	lation	Survival rate of	Micror	elief of snow surface
	tion	return trip	А	В	С	track	Size	Direction and type
574	m 3707	cm 147 5	cm 2 5	cm	cm 8 0	%	R	
576	3702	151.0	11 0	0	11.0	5	B	57m, 102m, 117m,
578	3704	151.0	7.0	4.8	11.8		B	127e
580	3705	137.7	10.0	3.3	13.3		B	
582	3704	153.5	18.0	- 4.5	13.5		В	
584	3702	151.8	16.0	0.2	16.2		В	
586	3698	163.5	2.0	9.5	11.5		В	6m, 55m, 102m,
588	3693	155.7	10.0	- 1.7	9.3		В	120r, 120e
590	3694	156.4	3.5	1.1	4.6		В	
592	3685	146.5	6.5	1.0	7.5		В	
594	3683	159.0	6.0	0	6.0		В	
596	3681	150.4	14.0	0.6	14.6		В	
598	3682	159.0	7.0	- 1.0	6.0		В	66m, 106r
600	3679	138.8	19.5	3.7	22.2	er.	В	
602	3677	141.2			15.8	COV	В	6m, 63r, 78r,
604	3679	141.8	16.0	7.2	23.2	3	\mathbf{C}	1101
606	3674	152.2	4.0	3.8	7.8	snc	С	66r
608	3670	149.6	11.0	- 0.6	10.4	nic	С	
610	3670		8.5			r tl	В	
612	3668	148.5	13.0	- 2.5	10.5	nde	А	
614	3667	133.7	10.0	12.3	22.3	a D	В	
616	3665	146.3	11.0	7.7	18.7	race	В	
618	3662	138.1	0.5	14.4	14.9	it t	В	
620	3659	139.7	14.0	3.3	17.3	air	В	38m, 60r, 76r, 108r
622	3653	146.2	14.0	1.8	15.8	I	С	
624	3650		15.5	5.8			В	
626	3649	147.5	4.5	- 1.0	10.0		В	40 50 04
628	3650	147.0	11.5	- 1.5	10.5		В	42m, 52r 94e, 111r
630	3654	145.0	15.0	- 0 <u>.</u> 1	13.5		В	
632	3648	136.6	18.5	- 0.1	18.4		В	
634	3647	150.9	2.5	2.6	5. 1		В	
636	3647	133.5	16.5	3.0	19.5		В	84r, 108r
638	3639	150.0	14.0	- 1.0	13.0		В	
640	3629	145.5	11.0	3.0	14.0		В	
642	3628	147.5	12.0	3.5	15.5		В	
644	3622	128.0	32.0	- 5.0	27.0		С	66r
646	3613		9.0				С	

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Station No.	Eleva- tion	Height of stakes in the	Snow	/ accumu at stakes	lation	Survival rate of	elief of snow surface	
		return trip	Λ	В	С	track	Size	Direction and type
C40	m	cm	cm	cm	cm	%	0	
048	3017 2610	161.5	0.0	- 4.0	2.5		C C	
659	2616	141.0	13.0	1.0	14.0			
654	2619	151.4	21.0	- 0.4	12.4		с С	
656	3613	152.0	10.0	- 80	11.5		C C	11, 66,
658	3609	130.0	19.0	- 0.0	5.0		C C	111, 001
660	3613	153.0	2.J	2.5	3.0		C C	
662	3618	147 5	5.5 8.5	3.0	<i>5</i> .0		C C	
Plateau	3624	117.5	0.5	5.0	11.5		ŭ	Î
St. (663) 664	3619	133 5		0.5	i	1	С	40r 54r
665	3615	175 0		0			C	101, 011
666	3621	141.6		3.4	1		C	
667	3616	144.5		5.5			C	26m, 51r
668	3614	172,5		3,5			С	,
669	3609	153.2		- 2.2		:	С	
670	3599	135.8		0.2			С	
671	3603	178.0		1.0			С	
672	3609	151.0		4.0			С	26m, 51r
673	3604	168.0		5.0			С	
674	3592	166.2		- 4.2		1	В	
675	3584	134.3		1.7			В	26m, 36r
676	3584	146.5		4.5			D	
677	3583	144.4		12.6			D	26m, 36r
678	3582	156.0		3.0			D	
679	3581	177.5		- 7.5			D	
680	3579	137.5		1.5			Е	
681	3576	133.6		- 0.6	1		D	30m, 50r
682	3574	107.2		6.8			D	
683	3574	180.0		- 1.0		i i	С	
684	3569	131.2		- 0.2			С	357r, 19m, 47r
685	3570	135.0		2.0			С	
686	3568	131.2		- 1.2	[С	
687	3563	151.7		- 1.7			С	
688	3562	146.3		- 9.3			D	
689	3557	128.5		13.5			D	345r, 15m, 35r
690	3559	141.5		- 1.5			D	
691	3554	147.5		- 0.5			D	1

Station No	Eleva-	Height of stakes in the	Snow	v accumul at stakes	ation	Survival rate of	Micror	elief of snow surface
	non	return trip	А	В	С	track	Size	Direction and type
692	m 3558	cm 140.0	cm	-1.0	cm	%	С	
693	3561	143.3	i				С	15m, 35r
694	3564	147.6		0.4			\mathbf{C}	
695	3571	130.5		18.5			D	
696	3553	156.0		- 1.0			D	9m, 29r
697	3553	156.0		- 1.0			D	
698	3539	156.2		17.8			D	
699	3545	155.3		- 1.3			D	
700	3545	161.4		3.6			D	Or
701	3544	168.4		- 0.4			D	
702	3538	159.4		- 0.4			D	
703	3535	164.0		- 9.0			D	
704	3530	179.0					E	
705	3532	164.5		- 0.5			D	220- 250- 7
706	3526	158.6	ł	27.4			D	228r, 338r, 7m, 22r
707	3518	172.0		2.0			D	
708	3517	163.5		4.5			D	0r, 25r
709	3518	158.8		- 0.8			D	
710	3515	152.5					D	
711	3505	184.0		0			D	
712	3497	155.2		- 0.2			D	lr, 9m, 27r
713	3487	148.5		- 2.5			D	
714	3490	146.5		- 0.5			С	
715	3488	170.5		- 0.5			С	
716	3486	146.9		0.1			\mathbf{C}	
717	3481	150.0					D	
718	3471	174.0		0			D	į
719	3467	158.7		- 4.7			D	
720	3466	142.8		0.2			D	328r, 9r
721	3467	161.3		-0.3			D	007 054
722	3466	151.4		0.6			C	32/r, 354r
723	3468	162.5		-11.5			C	
724	3467	182,0					D	
/25	3461	166.3		- 0.3			D	214m 10m
/26	345/	164.7		1.3			E	544m, 19r
727	3460	163.4		2.0			D F	
/28	3459	149.5		- 0.5			E	

Station No.	Eleva- tion	Height of stakes in the	Snow	accumu at stakes	lation	Survival rate of	Micror	elief of snow surface
		return trip	А	В	С	track	Size	Direction and type
729	3457 m	cm	cm	c m	cm	%	n	341m 12r
72.)	3463	174.2		-2.2			D	JTIII, 121
731	3449	148 7		1 3			D	
732	3446	160.0	1	0			C	339r. 349m. 29r
733	3440	159.4	1	- 6.4			D	0001, 01011, 201
734	3436	162.0		2 0			E	
735	3432	165.3	1				Е	
736	3429	134.2		1.8			D	
737	3420	161.4		12.4			D	322r, 354e, 4r
738	3416	181.0		3.0			E	, ,
739	3417	151.7		- 0.7			С	
740	3413	145.0		-10.0			А	
741	3406	183.0		- 3.0			Е	
742	3407	167.2		- 1.2			D	348r, 14r
743	3401	146.5		- 1.5			D	
744	3391	143.3		- 0.3			E	
745	3394	159.0		10.0			E	
746	3402	162.5		- 0.5			С	
747	3407	153.6		- 0.6		-	D	348r, 14r
748	3404	160.3		0.3			D	
749	3411	159.7		- 0.3			D	
750	3412	150.5	:	0.5			В	
751	3402	150.8		0.8			E	
752	3399	155.5		5.5			E	339r, 14r
753	3402	158.7		8.7			E	
754	3404	155,5		5.5			D	
755	3407	156.2		6.2			D	
756	3405	159.0		1.0			D	332r, 18r
757	3404	161.0		- 1.0			D	
758	3399	162.3		- 2.3			D	
759	3402	169.0		- 1.0			А	
760	3397	160.4		- 0.4			E	
761	3399	158.0		2.0			С	
762	3392	149.0		11.0			А	333r, 359e, 18r
763	3391	156.0		4.0			А	
764	3384	157.0		3.0			Α	
765	3369	159.4		0.6			В	

Station	Eleva-	Height of stakes in the	Snow	accumul at stakes	ation	Survival rate of	Micror	elief of snow surface
No.	tion	return trip	Α	B	С	track	Size	Direction and type
766	m 3371	cm 180.4	cm	- 0.4	cm	%	F	353e, 13r
767	3379	181.5		- 0.5		1	Е	
768	3373	157.4	2	- 0.4			E	338r, 17r
769	3372	180. 4		2.6			E	
770	3374	160.5		- 0.5			E	
771	3370	150.0		0			D	
772	3370	159.0		1.0			D	
773	3372	152.8		- 0.8			\mathbf{C}	343r, 13r
774	3368	186.4		- 0.4			D	
775	3368	158.4		1.1			Е	
776	3368	160.8		- 0.8			D	
777	3362	155.7		- 0.2			\mathbf{C}	343r, 8r
778	3353	160.3		- 0.3			D	-
779	3362	160.3		0.3			В	
780	3363	159.3					С	
781	3361	161.8		0.2			E	330r, 20r
782	3356	161.5		- 1.5			А	
783	3353	157.0		<u> </u>			D	
784	3351	163.3		- 1.3			E	344m, 15r
785	3349	182. 3		- 0.3			С	
786	3352	171.4		0.6			D	
787	3348	171.4		- 0.4			В	
788	3343	159.7		0. 3			С	
789	3337	162.5		2.5		- particular and the second se	А	342 _m , 12 _r
790	3317	160.0		0.			A	
791	3313	177.5		- 0.5			D	
792	3312	160.3		- 0.3			D	337r, 7r
793	3307	156.7		0. 7			С	
794	3306	171.0		0			D	
795	3300	152.0		- 0.5			E	328r, 10r
796	3299	160.0		0			D	
797	3299	170.7		5.3			D	
798	3298						C	346r, 16r
799	3292	173. 4		- 0.4			D	
800	3298	172.0		0			D	
801	3296	160.0		0			E	343r, 19r
802	3290	172.4		- 0.4		l	D	

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Station	Eleva-	Height of stakes in the	Snow	accumul at stakes	ation	Survival rate of	Micror	elief of snow surface
110.		return trip	Λ	В	С	track	Size	Direction and type
803	m 3288	cm 115.0	cm	cm 0	cm	%	D	
804	3294	171.5		0.5			А	329m, 23r
805	3298	147.5		0.5			\mathbf{C}	,
806	3298	162.5		-2.5			\mathbf{C}	
807	3291			0			\mathbf{C}	326r, 11e, 26r
808	3291	148.0		0			D	
809	3292	179.8		0. 2			А	
810	3288	163. 5		- 9.5			D	334m, 22e
811	3290	149.0		- 1.0			E	
812	3290	153.2	,	- 0.2			А	
813	3282	158.7		6.3			D	337m, 13e
814	3276	164. 5		5.5			D	
815	3271	155.4		0.6	l		D	
816	3271	160. 2		— 0. 2	Í		D	
817	3263	154.5		6.5			\mathbf{C}	326r, 11r
818	3260	161.4	i	- 1.4			D	
819	3257	151.0	1	9.0			D	334r, 5r
820	3257	166. 0		_ 1.0			\mathbf{C}	
821	3253	147.5	ĺ	2.5			В	
822	3249	180. 2		_ 0.2			А	338r, 34r
823	3248	174. 5		0.5			\mathbf{C}	
824	3245	154.0	i j	1.0			D	1
825	3249	174.8		0.2			D	340r, 12e
826	3254	160.0	(0			А	
827	3357	160. 2		_ 0.2			А	
828	3253	155.0		0			В	
829	3248	150.0	1	0			В	
830	3237	149.0		1.0			А	
831	3234	112.0		0			D	340m, 14r
832	3220	155. 0		0			E	
833	3207	172.0		0			А	
834	3197	168. 2		<u> </u>			D	338r, 14r
835	3191	162. 5		0.5			D	
836	3194	140.0		0			\mathbf{C}	
837	3194	173. 7		0.3		;	D	ļ
838	3197	155. 2		0. 2			Е	
839	3195	144.8	:	- 0.2			\mathbf{C}	

Station No.	Eleva- tion	Height of stakes in the	Snow	accumula at stakes	ation	Survival rate of	Micror	elief of snow surface
		return trip	A	В	С	track	Size	Direction and type
840	m 3191	cm 145. 2	cm	cm 0.2	cır	w %	C	
841	3187	185.6	Ì	0.4			F	334r 14r
842	3190	155.0	1	0			F	5511, 111
843	3189	182. 0		0			Б	334r 4r
844	3188	154.6		0.4			E	55H, H
845	3188	155. 8	-	- 0.8		:	D	
846	3188	170. 5		- 0.5			E	
847	3186	160. 5		- 0.5			D	
848	3184	160.0		0			B	
849	3180	163.4		- 0.4			B	
850	3169	165. 3		- 0.3			D	334r. 9r
851	3166	171.0		- 1.0			D	,
852	3163	176.8		- 0.8		1	D	
853	3157	174. 5		0.5			D	335r. 359e
854	3155	177.8					D	-,
855	3154	165. 5		- 0.5			В	334r, 354e, 14r
856	3154	154. 3		0.7			А	
857	3152	161.0		- 1.0			А	
858	3146	184. 5		- 0.4			С	339r, 14r
859	3147	168.0		- 1.0			С	
860	3148	156.3		- 1.3			А	
861	3147	158.0		2.0			\mathbf{C}	
862	3142	163. 5	-	- 0.5			\mathbf{C}	333r, 0e
863	3137	160.0	:	0			\mathbf{C}	
864	3135	165. 0		0			\mathbf{C}	330r, 2e
865	3132	145.2		- 0.2			А	
866	3122	159. 0		0.6			А	
867	3116	158.6		1.4			А	332d, 353e
868	3107	170.0		0			\mathbf{C}	
869	3105	173. 4		3.6			С	
870	3102	153. 0		0			D	328d, 358e
871	3109	153. 7		1.3			D	
872	3107	180.8		- 0.8			С	
873	3103	154.5		1.1			А	326d, 346r
874	3090	160. 2		— 0.2			С	
875	3080	167.5		0.5			D	
876	3076	184. 0		1.0			Е	326d, 344r

Station No	Eleva-	Height of stakes in the	Snow	accumula at stakes	ation	Survival rate of	Micror	elief of snow surface
110.	non	return trip	А	B	С	track	Size	Direction and type
877	3079 ^m	cm 165.8	cm	cm = 0.8	cm	%	F	
878	3079	155.3		_ 0.3				
879	3072	117.0					D	3264 340
07 <i>5</i> 000	3065	191.0		0.2			D	520d, 540e
000	3064	150.2		- 0.2				
001	2050	150.2	Í	4.0			A	
882	3038	109.7	I	12.5			A	326d, 344e
883	3044	172.0		0			С	
884	3033	180. 5		1.5			\mathbf{C}	
885	3030	158.8		1.2			D	330d, 342e
886	3028	160.5		- 0.5			D	
887	3027	159.2	j	0.8			\mathbf{C}	
888	3016	185.0	and the second se	- 1.0			А	323d, 340e
889	3005	143.6		1.4			\mathbf{C}	
890	2995	155.8		- 0.8			D	
891	2994	150.7		- 0.7			А	
892	2980	155. 2		4.8			D	322d, 337e, 357r
893	2981	177.3		- 2.3			D	
894	2974	145.5		- 0.5			Δ	325d, 341e
895	2955	158.0	1	2.0			С	
896	2952	172.8		0.2			D	
897	2945	163.2		1.8			D D	
808	2915	180.6		0.6			C	2004 2224 2426
200	2016	171.4		- 0.0			D D	JU90, JJ20, J420
099	2052	165.0		- 0.4			D	
900	2955	105.0		- 1.0			B	0051 0101 040
901	2940	170.0		0			В	305d, 318d, 340e
902	2933	165.0		0			С	
903	2933	161. 2		- 0.2			С	
904	2944	144.8		0. 2			Λ	310d, 331m
905	2939	169.2		<u> </u>			В	
906	2944	160. 3		- 0.3			\mathbf{C}	
907	2945	160.9		- 0.9			A	311d, 341m
908	2942	159.2		0,8			A	
909	2958	102.0	İ	0.5			A C	
910	2910	100. J 159 A		- 0.5			С D	
912	2920	146.5		1.5			С С	
913	2932	154.0		0			C	
914	2926	164.0		1.0			D	

Station No	Eleva-	Height of stakes in the	Snow a	accumula t stakes	ation	Survival rate of	Survival Microrelief of snow sur rate of		
110.	non	return trip	Α	В	С	track	Size	Direction and type	
915	m 2910	cm 160. 0	cm	0 ^{cm}	cm	%	D	307d, 330e	
916	2904	160.0		1.0			D		
917	2901	160.0		0			D		
918	2897	156.0		0	Ì		D		
919	2899	162.8		0.2			D	309d, 333e	
920	2913	146.0		- 1.0			А		
921	2906	169. 5		0.5			А		
922	2894	154.5		0.5			А		
923	2873	169.2		0.8			D		
924	2866	169.7		0.3			D	311d, 334e	
925	2859	168.8		0.2			D		
926	2855	152.5		- 0.5			В		
927	2859	141.5		0			В	307m, 327e	
928	2859	142.0		1.0			В		
929	2868	170.5		- 0.5			С		
930	2857	149.5		0.5			В	311m, 334m	
931	2859	149.0		1.0			В		
932	2867	150.5		- 0.5			В		
933	2874	152.7		0.3			С	314m, 338m	
934	2863	149.6	f	0.4			С	,	
935	2856	150.8		- 0.8			С		
936	2841	165.0		0			в		
937	2814	160.3		- 0.3			В		
938	2819	179.5		0.5			в	336m, 16e	
939	2815	170.3		- 0.3			А	,	
940	2807	150.0		0			В		
941	2818	156.0					В	342m, 352e	
942	2820	150.0		0			В	,	
943	2827	159.4		0			Ā		
944	2829	167.0		0			A		
945	2832	157.8		2.2			C		
946	2823	174.7		0.3			C	342d, 352e	
947	2807	159.4		0.6			В	, -	
948	2807	149.7		0.3			B		
949	2810	154.5		0.5			- C	324m, 348e, 6d.	
950	2802	160.0		0			В	, , ,	
951	2791	160.0		0			B		

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Station	Eleva-	Height of stakes in the	Snow a	accumul at stakes	ation	Survival rate of	Micror	elief of snow surface
INO.	tion	return trip	Α	B	С	track	Size	Direction and type
050	m	cm	cm	cm	CIT	n %	D	000 0
952	2792	155.9		0.2			в	339m, 3e
953	2792	100.0		- 0.3		1	В	
954	2802	115.2		- 0.2			C D	
955 056	2011	147.0	1	0 4			b D	
956	2011	160.4		- 0.4			в	200
957	2010	145.2	į.	0		1	Б	520m, 540e
956	2023	145.5		- 0.5			D D	
919	2032	149.5		0.7			D D	2004 3-
900	2010	149.4		1.0			D	5260, Se
901	2010	149.0	i	1.0			C C	
902	2623	153.3		- 0.5			D D	
905	2015	154.4		0.0			D D	
904	2010	165.2	ļ	0.4			Б	2001 245
905	2010	163.5		0.5			C C	522a, 545e
900	2023	104.5		- 0.5			L D	
907	2031	137.0		- 0.5			Б	
900	2014	159.9		- 0.1			Б	
909	2015	157.0)	0			Б	210 220 01
970	2019	150.0		0 5			G	518m, 538e, 0d
079	2020	152.0	:	- 0.5			D D	
972	2019	154.9		1.1		1	Б	
975	2009	154.2		0.0			D C	1
974	2011	100.0		0			C	200d 224- 0d
076	2001	155.0					D D	J200, J546, 20
077	2000	162.0					D	
079	2005						D	
970	2750	160.0					и С	1
080	2733	155.0		1			C	
001 021	2007	160.0	:				R	
South	2007	100.0					D	
Pole	2000					1		

3.2. Hardness of snow

Hardness of snow was measured by Kinoshita's hardness-meter at the surface and at the depth of 10 cm at intervals of 8 km. In Fig. 4, moving average values of the surface hardness for 10 sites along the traverse route are shown.

As shown in Fig. 4, the hardness of surface snow measured on the return trip is lightly smaller than that measured on the trip to the South Pole. This would be due to changes in the conditions of snow surface during the summer season as will be mentioned later.

In the region between Syowa and 74.5°S, the average hardness of snow surface was about 10 kg/cm^2 , a value larger than any of the values obtained from other regions in the traverse route. However the hardness in this region varied largely between 2 and 50 kg/cm² according to the condition of the surface; for example, hardness shows small value of 2.5-3.1 kg/cm² on drifts while it reaches the value as large as 20-50 kg/cm² on glazed surface.

Beyond 75°S, the hardness decreased rapidly and showed the minimum value of 1 kg/cm^2 at the Fuji Divide. To the south of 81° S, the average hardness was 3-4 kg/cm², but it decreased again towards the South Pole.

Density of snow was measured from the surface to the depth of 2 m at

Fig. 4. Hardness of snow surface along the traverse route. Solid circle: Values measured on the trip to the South Pole. Open circle: Values measured in the return trip from the South Pole.

Cross mark: Average density from surface to 2 m depth.

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Table 3. Hardness and density of near-surface snows.Hardness in the table is the mean value of 3 or 4 data, except the maximum
and the minimum values among the measured 5 or 6 data.

	1			Ha	rdness	Snow tomp	Air tamp
Station No.	Dat	e	GMT	Surface (kg/cm²)	at 10cm deep (kg/cm²)	$(-^{\circ}C)$	$(-^{\circ}C)$
	1968						
16	Sept.	28		19		28.5	
21	I	11		2.5,13	1		
37		29		2.8, 36		35.5	
58	1	30		2.8,49		31.0	
70	Oct.	I		3.1, 53		32.5	
94		2		28	21	33.0	
98		"		29			
122		9	12	31		32	30
126		"	17	2.9		33	32
132		"	18	31	8.0	36	36
138		10	14	16	3.8	30	28
142		10	17	9. 2	4.4	32	32
154		11	14	10. 7	5. 1	31	30
158		"	15	6.0		30	31
162		11	16	6.0	10. 7	35	33
166	1	11	18	10. 7		36	36
174		13	11	10. 7	6. 0	29	28
178	ļ	"	14	9. 2	8.0	27	25
182		"	17	12.7	4. 2	30	30
186	l	11	19	10. 7	6. 5	34	33
194		14	13	5.5	7. 2	33	30
198		"	15	16	31	33	35
202		"	18	12.5	4.4	36	37
206	1	"	20	16		40	40
210		15		9.2		40	39
218		"		10.7	12.5	38	
226		16	10	9.2		40	38
230		"	12	E Contraction of the second se	5. 1	38	37
234		"		2.8		34	33
242	1	11	19	5.5	10. 7	40	40
246	i	18	80	6.5		40	34
250		"	10	10.7	7. 2	37	35

				Ha	rdness	Snow temp	Air temp
Station No.	Dat	te	GMT	Surface (kg/cm ²)	at 10cm deep (kg/cm²)	(-°C)	(-°C)
256	Oct.	18	17	2.8	6. 5	38	38
258		"	19	16	4.8	39	40
282		21	09	12.5	4.2	43	41
286		"		21	7.3	41	36
290		"	13	9. 2	10. 7	42	35
294		"		2. 7	12.5	36	35
298		"	18	8.0	12.5	38	37
306		22	08	9. 2	9. 2	44	39
310		"	10	12	12	41	35
314		"	12	7.1	4.9	36	35
318		"	14	7.8	16. 5	38	36
322		"	16	9.4	12	36	35
326		"	16	6.6	4.9	39	39
334		23	09	12	2. 5	44	42
346		24	07	6.6	16. 5	49	46
350		"	09	7.1	8. 4	46	42
358		"	15	9. 4	4. 1	41	39
362		"	17	8.4	4.4	40	37
366		"	19	7.8	16.5	44	44
370		"	21	10. 5	26	49	43
378		25	09	12		49	45
418		28	09	3.5		50	47
422		"	11	3. 5		48	46
534	Nov.	6	10	1.2	1.3	52	49
538		"	13	1.0	0.8	48	45
542		"	17	1.1	1.0	50	46
550			22	13		50	49
554		7	10	1.6	1.6	50	47
559			14	1.6	2 1	47	44
550		"	10	1.0	2.1	40	45
000		"	19	1.2	1.0	10	TJ AO
5/4		8		1.0	1.2	10	40
578		"	16	0.9	1. /	49	43
586		"		0.9	1.0	50	50
590		9	16	1.2		48	44
594		"	18	0.9	1.1	49	49
	1		1	1			

Station No.DateGMTSurface (kg/cm2)at l0cm deep (kg/cm2)Solve temp. ($-$ °C)Air temp. ($-$ °C)598Nov.9211.21.5505560210080.90.95549606 \star 101.62.35043610 \star 131.22.15039622 \star 201.62.44951626 \star 221.0545567717092.21.24540679 \star 121.61.74336683 \star 171.92.23938685 \star 191.90.9414168718141.92.04435689 \star 162.91.34036691 \star 181.92.04138693 \star 103.71.24036699 \star 122.81.34135701 \star 171.92.13836703 \star 182.64.33938705 \star 207.82.8393970720092.23.24037709 \star 112.33.54035711 \star 121.638 <th></th> <th></th> <th></th> <th>Har</th> <th>dness</th> <th></th> <th></th>				Har	dness		
598 Nov. 9 21 1.2 1.5 50 55 602 10 08 0.9 0.9 55 49 606 * 10 1.6 2.3 50 43 610 * 13 1.2 2.1 50 39 614 * 15 1.6 1.9 50 39 622 * 20 1.6 2.4 49 51 626 * 22 1.0 54 55 677 17 09 2.2 1.2 45 40 679 * 12 1.6 1.7 43 36 683 * 17 1.9 2.2 39 38 685 * 19 1.9 0.9 41 41 687 * 18 2.7 7.8 39 37 693 * 17 1.9 2.0 <td>Station No.</td> <td>Date</td> <td>GMT</td> <td>Surface (kg/cm²)</td> <td>at 10cm deep (kg/cm²)</td> <td>Snow temp. (-°C)</td> <td>Air temp. $(-C)$</td>	Station No.	Date	GMT	Surface (kg/cm²)	at 10cm deep (kg/cm²)	Snow temp. (-°C)	Air temp. $(-C)$
60210080.90.95549 606 *101.62.35043 610 *131.22.15039 614 *151.61.95039 622 *201.62.44951 626 *221.05455 677 17092.21.24540 679 *121.61.74336 681 *152.02.94335 683 *171.92.23938 685 *191.90.94141 687 18141.92.04435 689 *162.91.34036 691 *182.77.83937 693 *192.3,4.02.64240 695 19181.92.04138 697 *103.71.24036 699 *122.81.34135 701 *171.92.13836 703 *182.64.33938 705 *207.82.83939 707 20092.23.24037 709 *112.33.5 </td <td>598</td> <td>Nov. 9</td> <td>21</td> <td>1. 2</td> <td>1.5</td> <td>50</td> <td>55</td>	598	Nov. 9	21	1. 2	1.5	50	55
606*101.62.35043 610 *131.22.15039 614 *151.61.95039 622 *201.62.44951 626 *221.05455 677 17092.21.24540 679 *121.61.74336 681 *152.02.94335 683 *171.92.23938 685 *191.90.94141 687 18141.92.04435 689 *162.91.34036 691 *182.77.83937 693 *192.3,4.02.64240 695 19181.92.04138 607 *103.71.24036 699 *122.81.34135 701 *171.92.13836 703 *182.64.33938 705 *207.82.88939 707 20092.23.54035 711 *121.6383333 715 *5.63.739 <td>602</td> <td>10</td> <td>08</td> <td>0. 9</td> <td>0.9</td> <td>55</td> <td>49</td>	602	10	08	0. 9	0.9	55	49
610 $*$ 13 1.2 2.1 50 39 614 $*$ 15 1.6 1.9 50 39 622 $*$ 20 1.6 2.4 49 51 626 $*$ 22 1.0 54 55 677 17 09 2.2 1.2 45 400 681 $*$ 15 2.0 2.9 43 35 683 $*$ 17 1.9 2.2 39 38 685 $*$ 19 1.9 0.9 41 41 687 18 2.7 7.8 39 37 693 $*$ 16 2.7 7.8 39 37 693 $*$ 10 3.7 1.2 40 36 697 $*$ 10 3.7 1.2 40 36 701 $*$ 17 1.9 2.1 38 <t< td=""><td>606</td><td>11</td><td>10</td><td>1.6</td><td>2.3</td><td>50</td><td>43</td></t<>	606	11	10	1.6	2.3	50	43
614 * 15 1.6 1.9 50 39 622 * 20 1.6 2.4 49 51 626 * 22 1.0 54 55 677 17 09 2.2 1.2 45 40 679 * 12 1.6 1.7 43 35 681 * 15 2.0 2.9 43 35 683 * 17 1.9 2.2 39 38 685 * 19 1.9 0.9 41 41 647 18 14 1.9 2.0 44 35 689 * 16 2.9 1.3 40 36 691 * 18 2.7 7.8 39 37 693 * 19 2.3 4.0 2.6 42 40 699 * 12 2.8 1.3 41 35 701 * 17 1.9	610	11	13	1.2	2.1	50	39
622 $*$ 20 1.6 2.4 49 51 626 $*$ 22 1.0 54 55 677 17 09 2.2 1.2 45 40 679 $*$ 12 1.6 1.7 43 36 681 $*$ 15 2.0 2.9 43 35 683 $*$ 19 1.9 2.2 39 38 685 $*$ 19 1.9 0.9 41 41 687 18 14 1.9 2.0 44 35 689 $*$ 16 2.9 1.3 40 36 691 $*$ 18 2.7 7.8 39 37 693 $*$ 19 $2.3,4.0$ 2.6 42 40 695 19 18 1.9 2.0 411 38 697 $*$ 10 3.7 1.2 40 36 699 $*$ 12 2.8 1.3 41 35 701 $*$ 17 1.9 2.1 38 36 703 $*$ 18 2.6 4.3 39 38 705 $*$ 20 7.8 2.8 39 39 711 $*$ 19 3.2 7.8 40 35 711 $*$ 19 3.2 7.8 40 39 713 $*$ 16 4.9 0.9 39 37 <tr< td=""><td>614</td><td>"</td><td>15</td><td>1.6</td><td>1. 9</td><td>50</td><td>39</td></tr<>	614	"	15	1.6	1. 9	50	39
626* 22 1.0 54 55 677 17 09 2.2 1.2 45 40 679 * 12 1.6 1.7 43 36 681 * 15 2.0 2.9 43 35 683 * 17 1.9 2.2 399 38 665 * 19 1.9 0.9 41 41 687 18 14 1.9 2.0 44 35 689 * 16 2.9 1.3 40 36 691 * 18 2.7 7.8 399 37 693 * 19 $2.3,4.0$ 2.6 42 40 695 19 18 1.9 2.0 41 38 697 * 10 3.7 1.2 40 36 699 * 12 2.8 1.3 41 35 701 * 17 1.9 2.1 38 36 703 * 18 2.6 4.3 39 38 705 * 20 7.8 2.8 39 39 711 * 11 2.3 3.5 40 35 711 * 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$	622	11	20	1.6	2.4	49	51
677 17 09 2.2 1.2 1.6 1.7 43 36 679	626	"	22	1.0		54	55
679 $*$ 121.61.74336 681 $*$ 152.02.94335 683 $*$ 171.92.23938 685 $*$ 191.90.94141 687 18141.92.04435 689 $*$ 162.91.34036 691 $*$ 182.77.83937 693 $*$ 192.3,4.02.64240 695 19181.92.04138 697 $*$ 103.71.24036 699 $*$ 122.81.34135 701 $*$ 171.92.13836 703 $*$ 182.64.33938 705 $*$ 207.82.83939 707 20092.23.24037 709 $*$ 112.33.54035 711 $*$ 121.63833 713 $*$ 164.90.93936 715 $*$ 163.73937 717 $*$ 193.74.33532 725 22097.21.53329 727 $*$ 105.62.53426 729 $*$ 15<	677	17	09	2. 2	1.2	45	40
681*152.02.94335 683 *171.92.23938 685 *191.90.94141 687 18141.92.04435 689 *162.91.34036 691 *182.77.83937 693 *192.3,4.02.64240 695 19181.92.04138 697 *103.71.24036 699 *122.81.34135 701 *171.92.13836 703 *182.64.33938 705 *207.82.83939 707 20092.23.24037 709 *112.33.54035 711 *121.63833 713 *164.90.93936 715 *5.63.73937 725 22097.21.53329 727 *105.62.53426 729 *153.05.73126 733 *173.0302623 741 *152.92624	679	11	12	1.6	1.7	43	36
683*171.92.23938 685 *191.90.94141 687 18141.92.04435 689 *162.91.34036 691 *182.77.83937 693 *192.3,4.02.64240 695 19181.92.04138 697 *103.71.24036 699 *122.81.34135 701 *171.92.13836 703 *182.64.33938 705 *207.82.83939 707 20092.23.24037 709 *112.33.54035 711 *121.63833 713 *164.90.93936 715 *5.63.73937 727 *105.62.53426 729 *153.05.73126 737 2309112.52926 741 *152.9262534	681	4	15	2. 0	2. 9	43	35
685 \varkappa 191.90.94141 687 18141.92.04435 689 \varkappa 162.91.34036 691 \varkappa 182.77.83937 693 \varkappa 192.3,4.02.64240 695 19181.92.04138 697 \varkappa 103.71.24036 699 \varkappa 122.81.34135 701 κ 171.92.13836 703 κ 182.64.33938 705 \varkappa 207.82.83939 707 20092.23.24037 709 κ 112.33.54035 711 κ 121.63833 713 κ 164.90.93936 715 κ 193.74.33532 725 22097.21.53329 727 κ 105.62.53426 733 κ 173.03026 737 2309112.52926 741 κ 152.92623	683	11	17	1.9	2. 2	39	38
68718141.92.04435 689	685	"	19	1. 9	0. 9	41	41
689	687	18	14	1.9	2.0	44	35
691* 18 2.7 7.8 39 37 693 * 19 $2.3, 4.0$ 2.6 42 40 695 19 18 1.9 2.0 41 38 697 * 10 3.7 1.2 40 36 699 * 12 2.8 1.3 41 35 701 * 17 1.9 2.1 38 36 703 * 18 2.6 4.3 39 38 705 * 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 * 11 2.3 3.5 40 35 711 * 12 1.6 38 33 713 * 16 4.9 0.9 39 36 715 * 5.6 3.7 39 37 717 * 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 * 10 5.6 2.5 34 26 733 * 17 3.0 30 26 734 4 15 2.9 26 23	689	"	16	2.9	1.3	40	36
693 \checkmark 19 $2.3, 4.0$ 2.6 42 40 695 19 18 1.9 2.0 41 38 697 \checkmark 10 3.7 1.2 40 36 699 \checkmark 12 2.8 1.3 41 35 701 \checkmark 17 1.9 2.1 38 36 703 \checkmark 18 2.6 4.3 39 38 705 \checkmark 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 \checkmark 11 2.3 3.5 40 35 711 \checkmark 12 1.6 38 33 713 \checkmark 16 4.9 0.9 39 36 715 \checkmark 16 4.9 0.9 39 37 717 \checkmark 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 733 \checkmark 17 3.0 30 26 737 23 09 11 2.5 29 26 741 \checkmark 15 2.9 26 23	691	"	18	2. 7	7.8	39	37
695 19 18 1.9 2.0 41 38 697 \checkmark 10 3.7 1.2 40 36 699 \checkmark 12 2.8 1.3 41 35 701 \checkmark 17 1.9 2.1 38 36 703 \checkmark 18 2.6 4.3 39 38 705 \checkmark 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 \checkmark 11 2.3 3.5 40 35 711 \checkmark 12 1.6 38 33 713 \checkmark 16 4.9 0.9 39 36 715 \checkmark 16 4.9 0.9 39 37 717 \checkmark 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 729 \checkmark 15 3.0 5.7 31 26 737 23 09 11 2.5 29 26 23 743 \checkmark 15 2.9 26 23	693	"	19	2. 3, 4. 0	2.6	42	40
697 $*$ 10 3.7 1.2 40 36 699 $*$ 12 2.8 1.3 41 35 701 $*$ 17 1.9 2.1 38 36 703 $*$ 18 2.6 4.3 39 38 705 $*$ 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 $*$ 11 2.3 3.5 40 35 711 $*$ 12 1.6 38 33 713 $*$ 16 4.9 0.9 39 36 715 $*$ 5.6 3.7 39 37 717 $*$ 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$ 10 5.6 2.5 34 26 733 $*$ 17 3.0 30 26 737 23 09 11 2.5 29 26 743 $*$ 15 2.9 26 23	695	19	18	1.9	2.0	41	38
699 $*$ 12 2.8 1.3 41 35 701 $*$ 17 1.9 2.1 38 36 703 $*$ 18 2.6 4.3 39 38 705 $*$ 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 $*$ 11 2.3 3.5 40 35 711 $*$ 12 1.6 38 33 713 $*$ 16 4.9 0.9 39 36 715 $*$ 5.6 3.7 39 37 717 $*$ 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$ 10 5.6 2.5 34 26 733 $*$ 17 3.0 30 26 737 23 09 11 2.5 29 26 741 $*$ 15 2.9 26 23	697	"	10	3.7	1.2	40	36
701* 17 1.9 2.1 38 36 703 * 18 2.6 4.3 39 38 705 * 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 * 11 2.3 3.5 40 35 711 * 12 1.6 38 33 713 * 16 4.9 0.9 39 36 715 * 5.6 3.7 39 37 717 * 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 * 10 5.6 2.5 34 26 733 23 09 11 2.5 29 26 741 * 15 2.9 26 23	699	"	12	2.8	1.3	41	35
703 $*$ 18 2.6 4.3 39 38 705 $*$ 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 $*$ 11 2.3 3.5 40 35 711 $*$ 12 1.6 38 33 713 $*$ 16 4.9 0.9 39 715 $*$ 5.6 3.7 39 37 717 $*$ 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$ 10 5.6 2.5 34 26 729 $*$ 15 3.0 5.7 31 26 733 $*$ 17 3.0 30 26 737 23 09 11 2.5 29 26 741 $*$ 15 2.9 26 23	701	"	17	1.9	2. 1	38	36
705 \checkmark 20 7.8 2.8 39 39 707 20 09 2.2 3.2 40 37 709 \checkmark 11 2.3 3.5 40 35 711 \checkmark 12 1.6 38 33 713 \checkmark 16 4.9 0.9 39 36 715 \checkmark 5.6 3.7 39 37 717 \checkmark 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 729 \checkmark 15 3.0 5.7 31 26 733 \checkmark 17 3.0 30 26 741 \checkmark 15 2.9 26 23	703	"	18	2.6	4.3	39	38
707 20 09 2.2 3.2 40 37 709 $*$ 11 2.3 3.5 40 35 711 $*$ 12 1.6 38 33 713 $*$ 16 4.9 0.9 39 36 715 $*$ 5.6 3.7 39 37 717 $*$ 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$ 10 5.6 2.5 34 26 729 $*$ 15 3.0 5.7 31 26 733 $*$ 17 3.0 30 26 734 $*$ 15 2.9 26 23 743 $*$ 17 2.6 20 20 21	705	"	20	7.8	2.8	39	39
709 $*$ 11 2.3 3.5 40 35 711 $*$ 12 1.6 38 33 713 $*$ 16 4.9 0.9 39 36 715 $*$ 5.6 3.7 39 37 717 $*$ 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$ 10 5.6 2.5 34 26 729 $*$ 15 3.0 5.7 31 26 733 $*$ 17 3.0 30 26 741 $*$ 15 2.9 26 23 743 $*$ 17 2.6 20 21	707	20	09	2.2	3.2	40	37
711 $*$ 12 1.6 38 33 713 $*$ 16 4.9 0.9 39 36 715 $*$ 5.6 3.7 39 37 717 $*$ 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $*$ 10 5.6 2.5 34 26 729 $*$ 15 3.0 5.7 31 26 733 $*$ 17 3.0 30 26 737 23 09 11 2.5 29 26 741 $*$ 15 2.9 26 23	709	"	11	2.3	3. 5	40	35
713 \checkmark 16 4.9 0.9 39 36 715 \checkmark 5.6 3.7 39 37 717 \checkmark 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 729 \checkmark 15 3.0 5.7 31 26 733 \checkmark 17 3.0 30 26 737 23 09 11 2.5 29 26 741 \checkmark 15 2.9 26 23	711	"	12	1.6		38	33
715 \checkmark 5.6 3.7 39 37 717 \checkmark 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 729 \checkmark 15 3.0 5.7 31 26 733 \checkmark 17 3.0 30 26 737 23 09 11 2.5 29 26 741 \checkmark 15 2.9 26 23	713	"	16	4.9	0.9	39	36
717 \checkmark 19 3.2 7.8 40 39 721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 729 \checkmark 15 3.0 5.7 31 26 733 \checkmark 17 3.0 30 26 737 23 09 11 2.5 29 26 741 \checkmark 15 2.9 26 23	715	"		5.6	3. 7	39	37
721 21 19 3.7 4.3 35 32 725 22 09 7.2 1.5 33 29 727 $"$ 10 5.6 2.5 34 26 729 " 15 3.0 5.7 31 26 733 " 17 3.0 30 26 737 23 09 11 2.5 29 26 741 " 15 2.9 26 23	717	"	19	3.2	7.8	40	39
725 22 09 7.2 1.5 33 29 727 \checkmark 10 5.6 2.5 34 26 729 \checkmark 15 3.0 5.7 31 26 733 \checkmark 17 3.0 30 26 737 23 09 11 2.5 29 26 741 \checkmark 15 2.9 26 23	721	21	19	3.7	4. 3	35	32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	725	22	09	7. 2	1. 5	33	29
729 * 15 3.0 5.7 31 26 733 * 17 3.0 30 26 737 23 09 11 2.5 29 26 741 * 15 2.9 26 23 743 * 17 2.6 30 34	727	"	10	5.6	2. 5	34	26
733 \checkmark 17 3.0 30 26 737 23 09 11 2.5 29 26 741 \checkmark 15 2.9 26 23 743 \checkmark 17 2.6 30 24	729	"	15	3.0	5. 7	31	26
737 23 09 11 2.5 29 26 741 * 15 2.9 26 23 743 * 17 2.6 30 34	733	"	17	3.0		30	26
741 * 15 2.9 26 23 743 * 17 2.6 30 34	737	23	09	11	2. 5	29	26
	741	"	15	2.9		26	23
715 % 17 2.0 30 24	743	"	17	2.6		30	24

			На	rdness	S	A *
Station No.	Date	GMТ	Surface (kg/cm ²)	at 10cm deep (kg/cm²)	(-°C)	(-°C)
747	Nov. 23	20	4.4		29	26
751	24	18	6.6	1.2	29	25
753	"	20	3.8	1. 9	33	26
755	25	09	7.2	2.0	35	33
757	"	10	3. 2	9. 7	35	34
759	"	12	3.7	4.6	35	31
761	"	16	1.6			
763	"	17	1.9	0. 9	33	33
765	"	20	6. 5	7. 2	36	35
767	26	09	1.3	5. 7	35	33
769	"	10	1.4	7. 2	35	30
773	"	16	4.8	3. 7	33	28
775	"	18	6. 1	7.5	33	28
777	"	20	2. 1, 4. 8	1. 7	34	32
779	27	16	6.6	5. 1	32	28
781	"	18	1.1	7. 2	30	29
783	"	20	4.0	2.0	32	30
785	28	09	7.7	2.8	33	30
787	11	10	4.0	4.0	33	33
789	"	12	1. 7	1. 1	33	29
793	"	17	3. 2	1. 5	33	31
795	"		3.0	2.3	34	33
797	29	09	2.8	1.9	35	34
799	"	10	3. 4	3. 1	34	30
801	"	12	2.8	1. 5	34	30
803	"	15	5. 1	3.4	32	30
805	"	17	1.6	2. 1	31	29
807	"	19	5. 1	9.7	32	30
809	30	16	2. 5	2. 7	32	29
811	"	17	2. 9	2.7	31	30
813	"	20	8.4	3. 0	32	30
815	Dec. 1	08	4.8	1. 3	33	31
817	"	10	3.4	1.5	32	31
819	"	12	4.6	2. 7	32	28
821	"	15	4.2	1. 2	29	29
823	"	17	8.4	2. 3	32	28
825	"	19	1.3	1. 7	33	31

Kenzo Fujiwara, and Yasoichi Endo

			Har	dness	Snowtown	Ain tomp
Station No.	Date	GMT	Surface (kg/cm ²)	at 10cm deep (kg/cm²)	(-°C)	(−°C)
827	Dec. 2	09	2.0	2. 5	33	30
829	"	10	1.6	1.2	33	28
831	"	12	1.2	1.2	29	27
833	"	15	11	5.4	29	30
835	"	17	6.6	2. 9	32	31
837	4	13	3. 1	3. 7	33	31
839	11	16	1.1	8.4	32	29
841	4	18	8.4	2.6	32	28
843	"	20	2.1	1.7	33	31
845	5	09	1. 3	1.2	33	32
847	"	10	2. 3	1.7	32	30
849	"	13	5. 4	1.3	30	30
851	"	15	4.6	3.5	32	29
853	"	17	5. 1	4.4	32	28
855	"	19	2.4	2.3	34	31
857	6	09	1.7	1.2	32	31
8.59	"	10	4.2	1.6	33	29
861	"	13	2.3		31	27
863	"	15	1.8	2.3	31	26
865	"	17	2.6	7.2	30	27
867	"	19	3. 7	4.4	33	29
869	7	16	4.0	2. 2	31	28
871	"	18	5. 1	4.4	29	29
873	"	20	2. 7	6.6	30	29
875	8	09	2.4	1.5	32	30
877	"	10	5. 7	4.4	31	29
879	"	14	7. 2	6.2	30	28
881	"	15	1.3	1.2	28	28
883	"	17	2.3	2.4	29	27
885	"	19	5.4	4.4	31	28
887	9	09	1.2	3.5	30	30
889	"	10	2. 7	4.0	30	30
891	"	12	3.2	1.5	29	28
893	"	15	2, 2	1.6	31	27
895	"			3.2	29	28
897	10	19	0.0	4.2	31	29
899	10	16	2.1	4.4	29	28

		1 -1 1.48.57.	Ha	rdness	e le richini churcha.		
Station No.	Date	GMT	Surface (kg/cm ²)	at 10cm deep (kg/cm²)	(-°C)	(−°C)	
901	Dec. 10	17	1.2	1.1	30	28	
903	11	20	1.2	1.3	30	29	
905	11	09	0. 9	7.8	31	29	
908	"	11	1.7	1.6	27	28	
909	11	14	1.7		28	27	
911	"	16	1. 9	7. 2	28	26	
913	"	18	0.8	1.1	27	25	
915	"	20	1.5	2. 3	29	27	
917	12	09	2.1	1.4	30	29	
919	"	11	1.4		30	28	
921	"	14	1.5	3.2	29	27	
923	"	16	1.8	1.6	28	27	
925	"	17	8.4	0. 7	29	26	
927	"	20	1.2	0.8	30	27	
929	13	16	1.5	0. 7	30	27	
931	"	18	1.4	1.4	32	27	
933	"	21	5. 6	0. 9	31	31	
935	14	09	2.0	1.2	32	26	
937	"	10	3. 5	2.6	31	25	
939	"	14	1.7	1.5	28	26	
941	"	15	2. 2	1.2	31	24	
943	"	17	1.6	0. 9	33	26	
945	"	20	2.0	1.9	33	28	
947	15	09	6. 6	1.4	31	23	
949	"	10	3. 5	1.2	30	24	
951	11	14	1.4	1. 9	32	28	
953	11	15	1.2	0. 7	29	31	
955	11	17	1.6	0. 7	30	32	
957	11	23	2.8	1.2	31	29	
959	16	10	1.4	0. 7	29	28	
961	"	11	1.2	0.8	28	28	
962	"	12	1.3	1.1	32	28	
965	"	16	1.4	1.4	29	32	
967	11	18	2. 1	0. 7	33	30	
969	"	19	4. 3	1.5	29	32	
971	"	21	1.1	1.1	29	32	
973	"	23	3. 1	2. 1	31	30	

				Hai	rdness		
Station No.	Dat	e	GMT	Surface (kg/cm²)	at 10cm deep (kg/cm²)	Snow temp. $(-^{\circ}C)$	Air temp. $(-^{\circ}C)$
975	Dec	18	11	93	0.9	35	32
975	Det.	10	13	1.5	0. 5	30	29
979		"	13	2.3	0. 8	30	30
979		25	10	11		28	28
975		20	15	1.1		32	31
971		26	14	0.7		26	29
967		20	18	1.5		23 28	30
963		" "	99	1.5		28	27
959		97	10	1.1		27	30
955		21	15	1.5		26	29
951			17	9.7		26 26	-0 29
947	i		17 91	2.7		20	30
943			08	, <u> </u>		30	28
030		20	11	1.5		30	26
959			14	1.2		30	20
935			16	· 1.9		30	20
991 097			10	1.5		21	20
927		20	19	U. 0 9-9		30 30	20
925		29	14	2.3		30	20
915		"	17	1.7		30	20
915		<i>i</i> //	20	1.0		21	20
911		30	07	2. 3		51 90	29
907		"	09	1.2		20	24
903		"	12	1.7	1	26	23
899		"	14	2.3		26	23
895		11	18	2.9		24	24
891		"	20	2. 1		26	24
887		31	07	5.4		28	26
883		"	09	4.6		28	22
879		"	12	3.0		26 96	25
873 871		"	15	2.5	Ì	20 97	25 28
867	1969 Jan	1	09	2.т 9.9		27 90	20 28
007 Q55	Jall.	I A	19	2. Z 9. G		29 97	20
655 851		<i>"</i> 9	09	2.0 9 Q		21	23
847		-	11	2. 5		25	23
842		"	14	3.0	i.	26	23
839	1	"	17	0.8		27	24

			Har	dness	Snow tamp	Ain town
Station No.	Date	GMT	Surface (kg/cm ²)	at 10cm deep (kg/cm²)	(-°C)	$(-^{\circ}C)$
835	Jan. 4	13	3.0		26	. 24
831	"	16	5.1		26	24
827	"	19	2.4		26	24
823	"	22	2.1		27	25
819	5	08	2.6		28	27
815		11	3. 2		27	25
807	"	17	1.2		26	26
803	6	07	3. 7		30	29
799	"	. 09	2. 2		28	27
791	"	18	1.1		26	26
787	7	07	7.2		27	26
7 83	"	10	1.7		26	24
779	"	13	5.4		25	22
7 75	"	16	1.6		26	22
771	"	18	3. 5		27	24
767	8	15	1.3		25	24
763	"	18	2.8		26	25
759	"	21	1.5		29	29
755	9	16	1.5		27	25
751	"	18	1.6		27	26
747	10	07	5.4		29	29
7 3 9	"	12	3.0		28	25
731	"	18	4.4		27	27
727	"	20	1. 3		30	31
723	11	07	4. 4		33	34
719	"	10	3. 5		29	27
715	"	13	2.2		29	28
707	12	07	2. 7		33	34
703	"	12	1.6		29	28
699	11	15	0.8		28	29
695	"	19	1.4		30	31
691		21	4.4		31	33
602	13	08			35	34
005 679		15	U. U 1 Q		3U 2Q	29 99
675	"	19	1.9		30	2 <i>3</i> 30
671	14	07	0.6		33	29
666	"	11	1.3		28	26

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		Ì		Har	dness	Snow	Air	Der	nsity
Station No.	Da	ite	GMT	Surface (kg/cm²)	at 10 cm deep (kg/cm²)	temp. $(-^{\circ}C)$	$(-^{\circ}C)$	Surface (g/cm³)	at 10 cm deep (g/cm ³)
662	Jan.	20	10	1.2	2.8	34	31		
654		"	17	1.6	1.4	32	32	0.24	0.33
650		"	20			35	35	0.35	0. 33
646		21	08	2.3	2.6	35	35	0.34	0. 28
638		"	12	0.8	0. 7	34	32	0.37	0.34
630		"	16	0.8	0. 7	32	32	0.37	0.31
622		11	20	1.0	0. 7	33	35	0.32	0.34
620		1.	22			36	38	0.32	0.33
614		22	09	0. 7	1.2	38	36	0. 30	0.30
606		"	14	0. 9	0. 8	34	32	0.31	0.36
598		"	18	0. 7	0. 7	35	34	0.32	0.34
590		"	23	0. 7	0.4	38	41	0.32	0.35
582		23	10	0.5	0.5	35	32	0. 30	0.43
574		"	15	0. 5	0. 9	33	32	0.32	0.33
-566		11	19	0. 5	0.4	35	36	0.30	0. 33
558		24	10	1.4	0. 4	39	38	0.36	0. 32
550		25	17	1.0	0. 9	35	35	0.34	0.35
542		"	22	1.9	0. 9	38	40	0.34	0.35
534		26	09	0. 5	0.9	40	37	0.34	0. 33
526		"	13	0.6	0. 7	35	33	0.35	0.35
518		"	17	0.9	0. 7	34	33	0.33	0.31
510		"	21	1.2	2.3	38	40	0.31	0.34
502		27	10	2. 7	1.2	37	34	0.36	0.37
494		"	15	1.6	1.1	33	31	0.28	0.33
486		"	19	0. 7	0.8	33	33	0.34	0.32
478		28	09	2.6	1.4	39	36	0.42	0.38
470		"	13	1.6	1.3	34	30	0.36	0.35
462		29	11	3.8	3. 1	35	33	0.45	0.40
454		"	15	2.0	1.3	30	29	0.33	0.35
446		"	19	2.3	2.1	33	35	0.34	0. 37
438		30	08	2.5	0.9	40	37	0.38	0.36
430		"	11	3.0	5. 7	35	34	0.41	0.32
422		"	15	1.1	1.1	32	32	0.35	0.36
414		"	20	4.8	1.3	35	38		
406	Feb.	2	09	4.6	2.4	43	40	0.41	0.42
398		"	12	5. 7	4.8	37	37	0.42	0. 38
390		"	14	2.6	3. 2	36	33	0.31	0.34

			Har	dness	Snow	Air	Dei	nsity
Station No.	Date	GMT	Surface (kg/cm²)	at 10 cm deep (kg/cm ²)	temp.	$\begin{array}{c} \text{All} \\ \text{temp.} \\ (-^{\circ}\text{C}) \end{array}$	Surface (g/cm³)	at 10 cm deep (g/cm ³)
382	Feb. 2	17	3.7	2.8	33	34	0.35	0. 41
374	"	20	4.6	2.3	38	44	0.39	0.34
366	3	09	9. 7	9.7	40	39	0.40	0.44
358	"	12	3.8	7.2	38	35	0.38	0.38
350	"	15	27	4.8	34	32	0.45	0.38
342	11	18	14.5	5.4	33	33	0.38	0.43
334	3	21	4.0	1.3	36	39	0.39	0.48
326	4	10	4.0	21.5	33	33	0.46	0.44
318	"	14	8.4	4.0	30	29	0. 38	0.43
310	"	18	9. 7	6.6	32	31	0.42	0.39
302	"	20	3.5	7.8	32	33	0.42	0.39
294	5	09	41	3.5	33	34	0.41	0.46
286	"	11	7. 7	4.8	31	30	0.43	0.41
278	11	15					0.42	0.40
270	11	18	6.6	5.7	37	38	0.36	0.39
262	6	07	4.4	11	31	30	0.42	0.45
254	"	10	3. 8	2.8	28	26	0.39	0.36
246	11	14	14.5	14.5	23	21	0.45	0.40
238	11	17	14.5	2.1	20	20	0.42	
230	"	20	3.5	4.4	21	20	0.38	0.37
222	7	07	8.4	3.4	25	26	0.44	0.46
214	"	12	5.4	5. 7	20	20	0. 41	0.42
206	11	15	4.0	12.5	23	24	0.36	0.42
198	11	16	11	3.3	30	30	0.45	0.48
190	8	80	21	6.2	24	23	0. 47	0.44
182	11	13	4.8	7.8	15	15	0.46	0.45
174	"	16	5.4	5. 7	15	15	0.41	0.48
166	9	09	7.2	5.4	23	23	0. 47	0.46
158	"	13	2. 7	4.4	17	16	0. 37	0.39
150	"	16	14.5	2. 7	17	16	0.52	0.37
142	"	18	41	2.3	19	19	0.46	0.39
134	10	09	41	8.4	23	21	0.46	0.44
126	"	11	16.5	2. 7	18	16	0.46	0.37
122	"	16	21	12.5	14	13		
118	"							0.50
110	11	11	3. 5	5.4	16	16	0.46	0.41
102	11	15	6.6	3. 2	13	11	0. 43	0.46

				Har	dness	Snow	Air	Dei	nsity
Station No.	Da	ate	GMT	Surface (kg/cm²)	at 10 cm deep (kg/cm²)	temp. (-°C)	$ \begin{array}{c} \text{temp.} \\ (-^{\circ}\text{C}) \end{array} $	Surface (g/cm ³)	at 10 cm deep (g/cm ³)
94	Feb.	11	18	8.4	2.3	13	13	0.48	0.45
86		12	80	4.2	6.2	16	15	0.41	0.41
78		"	11	8.4	4.4	13	12	0.40	0.41
70		11	1.4		2.7	14	13	0.44	0.46
62		13	09	5.4	11	20	21	0. 25	0.42
54		"	11	14.5	3.4	16	16	0.42	0.39
46		"	14	4.6	3.4	12	11	0.44	0. 43
38		"	18	2.6	5.4	14	15	0. 21	0.42

intervals of 50-70 km along the whole traverse route (Table 4). Besides the above measurements, density of snow surface was measured at intervals of 16 km between Syowa Station and the Plateau Station (see Table 3). In Fig. 5, values of average density from the surface to the depth of 2m are shown by cross marks and moving average of the surface densities for 5 sites are plotted by solid circles.

The density of snow seems to change from one region to another with the relief and the hardness. On the marginal slope, snow density exceeds 0.40 g/cm^3 , but near the Fuji Divide and the South Pole, it is less than 0.35 g/cm^3 .

3.4. Some observations on the surface of snow

3.4.1. Glazed surface and crack

The distribution of glazed surfaces along the traverse route is shown by letter Λ in Table 2 and Fig. 3. Glazed surface was found to have been developed on the upper part of the mound formed on the ice sheet, where accumulated snow was scarcely found (see Table 2 and Photos 3 and 18). When such a place was passed one month later during the return trip, some of the glazed surfaces were decorated with hoarfrost while the others were covered by a thin cover of snow.

Most of the cracks observed were located on these glazed surfaces. They were patterned in the form of polygons and of parallel strips (Photos 3 and 17). Cracks were often observed also on the smooth surface without sastrugi. In this case, cracks were almost in the pattern of parallel strips. Although the cracks were mostly narrow with the width less than several centimetres, cracks wider than the width of caterpillar of snow vehicle were found at times. Sketches of vertical sections of two kinds of cracks are shown in Fig. 6.

3.4.2. Tracks of snow vehicle

On the snow surface, we found the tracks left by the snow vehicles that carried the traverse party from Syowa Station to the Plateau Station and back one year before by JARE 1967-68. Table 2 shows the survival rate of the track

Fig. 6. Cross sections of cracks developed on the glazed and smooth surfaces.

of snow vehicle. "The survival rate of track" is defined as the ratio of the length of survived track of the snow vehicle to a certain distance run by the vehicle; for example, if the vehicle covers 500 m and the track mark remains 200 m, then the survival rate is 40%.

Survival rates greater than 80% were found mostly in the zones of small snow accumulation and of glazed snow surface (Photo 18). This fact shows that snow accumulates in the zone of glazed surfaces only in a negligibly small amount, if any, throughout the whole period of a year. In the zones of large snow accumulation and of rough surface, the rate was less than 10%.

In the region between 70°S and 74.5°S, the survival rate varied in accordance with the repetitive change in snow accumulation, and nearly constant values of 20-30% were obtained in the region between 74.5°S and 76°S (Photo 19). In the region of the Fuji Divide, the tracks were covered with a thin snow layer but could easily be recognized (Photo 20). These regional changes in the survival rate coincide with changes in the annual snow accumulation measured by snow stakes, and this will be discussed later.

3.4.3. Changes in the snow surfaces during the summer season

Since the party returned from the South Pole in the late summer, hoarfrost on the snow surface was frequently observed (Photo 21). The crystals of hoarfrost can be divided into two types; the spike-like type and the scale-like type. Spike-like crystals formed only in such cases when the weather was calm and fine for a particularly long period. The hoarfrosts of this type were easily broken by the winds of about 7-8 m/s, and deposited around snow drifts of sastrugi (Photo 22). The layers of scale-like crystals began to form towards the end of November when the weather was calm and the air temperature become higher than -30° C, and grew to the thickness of 2-3 cm within 3-4 days in the midsummer.

The hoarfrosts grew faster on the sloped flanks of drifts than on the horizontal flat surface on snow; for example, the layers of spike-like crystals on the drifts grew up to the thickness of 1.5–2.0 cm in 2 days, whereas those on the flat surfaces remained less than 1.0 cm in thickness. Repetition of such a process of formation and deposition of hoarfrost crystals might cause a gradual wearing down of the rough surface of snow and at the same time redistributed the snow more uniformly over the surface.

4. Snow Accumulation

4.1. Measurements of snow accumulation by snow stakes

In December 1967, and January 1968, the traverse party of JARE 1967-68 installed snow stakes at intervals of 2 km from the Plateau Station to Syowa Station. Measurements of snow accumulation using these stakes were carried out in April 1968, in September-November 1968, in January-February 1969. Table 2 shows the values of annual and seasonal accumulation obtained on the above three trips. In Figs. 7 and 8, moving averages of annual and scasnonal accumulations obtained at 10 sites are plotted.

As shown in Fig. 7, the annual snow accumulation showed a general tendency of decrease from Syowa to the Plateau. On the steep marginal slope between St. 16 and St. 70, the accumulation was about $20 \text{ g} \cdot \text{cm}^{-2} \cdot \text{year}^{-1}$, the greatest of the values obtained in the whole route. Between the marginal slope and 74.5°S, the accumulation varied in places within the range of 0 to $15 \text{ g} \cdot \text{cm}^{-2} \cdot \text{year}^{-1}$. In the plateau area between 74.5°S and the Plateau Station, the accumulation was nearly constant at $4 \text{ g} \cdot \text{cm}^{-2} \cdot \text{year}^{-1}$.

This difference in the values of accumulation observed to the north and to the south of 74.5°S will be due to the different topography and weather conditions in the two regions. In the southern region, the slope is more gentle, snow surfaces are more flat and smooth, and winds are lower than in the northern region. The recurrent changes in accumulation to the north of 74.5°S are probably due to the large scale undulation of ice sheet.

In the region between St. 16 and St. 144 near Syowa Station, measurements of accumulation were conducted in January, April, October, 1968 and in following February. Results thus obtained are shown in Fig. 8. The snow accumulation was large in the winter season (from April to October, during about 160 days). In the summer season (October to February, during about 130 days), the accumulation was negative, that is, ablation occurs instead of accumulation.

Fig. 7. Annual accumulation of snow along the traverse route from Syowa Station to the Plateau Station. Solid circle: Accumulation measured by snow stakes. Cross mark: Accumulation determined by snow stratigraphy.

Fig. 8. Seasonal accumulation of snow profile from St. 16 to St. 144 near Syowa Station. Measurements of accumulation by snow stakes were carried out on January 7–13, April 22–27, September 28-October 10, 1968 and February 9–15, 1969.

4.2. Measurement of snow accumulation from snow stratigraphy

For the purpose of estimating the average snow accumulation, stratigraphy, density, hardness, and grain size of snow cover were examined in 2-m pits dug at 44 sites on the traverse route.

The summer layers are coarse-grained and have depthhoar, are of low density and hardness. The winter layers are fine grained, rather homogeneous, and of high density and hardness. These seasonal variations in the snow layers composing the snow cover were used as the criteria for distinguishing the annual snow layers.

Table 4. Snow and water accumulation.

	Depth	Snow accu	imulation	De	ensity	Water accu	umulation	Сс	Snow		
Station No.	of pit (cm)	Min. (cm/year)	Max. (cm/year)	Average (g/cm ³)	Number of measure- ment	Min. (cm/year)	Max. (cm/year)	in a pit wall con tio		of ice sheet	
16	450	90.0	90, 0						Gullied	Slope down to the W	
31	110	22.0	27.5	0.438	21	8.8	12.0	Uniform	Smooth	Gentle slope down to the W	
70	175	19.5	21.8	0.429	35	8.4	9.4	"	"	"	
90	196	15.1	17.8	0.407	28	6.2	7.2	"	Gullied	Top of dominant saddle	
122	173	17.3	21.6	0.426	15	7.4	9.2	Very irregular	"	Bottom of trough	
140	230	20.9	23.0	0. 428	24	9.0	9.8	"	11	Gentle slope down to the N	
170	138	19.7	27.6	0.407	25	8.0	11.2	Irregular	"	Shallow besin	
212	114	19.0	22.8	0.412	17	7.8	9.4	Uniform	"	Northside of saddle	
244	195	21.7	24.3	0.422	10	9.2	10.3	Irregular	"	Southside of trough	
270	190	21.1	23.7	0. 421	11	8.9	10.0	"	"	Top of broad saddle	
304	190	11.9	12.6	0. 386	8	4.6	4.9	Uniform	Glazed	Top of dominant mound	
330	194	19.4	19.4	0.389	39	7.6	7.6	Irregular	Gullied	Bottom of trough	
376	185	16.8	16.8	0.360	11	6.1	6.1	"	11	Even feature	
414	194	12.9	16.1	0.363	40	4.7	5.8	Uniform	Smooth	Top of broad mound	
440	115	12.8	14.3	0.353	8	4.5	5.0	"	11	Even feature	
470	156	11.1	13.0	0.342	12	3.8	4.4	Irregular	Gullied	Gentle slope down to the N	
494	202	11.2	13.4	0.340	20	3.8	4.6	Uniform	Smooth	Even feature	
530	196	8.5	10.3	0.332	18	2.8	3.4	11	11	"	
552	165	8.7	10.3	0.333	14	2.9	3.4	"	11	"	
556	202	11.8	12.6	0. 333	21	3.9	4.2	Irregular	"	"	
590	176	8.8	10.3	0. 337	16	3.0	3. 5	Uniform	"	"	
626	169	8.9	10.5	0.317	15	2.8	3. 3	11	"	Faint step on a gentle slope	
646	153	10.9	10.9	0. 348	18	3.8	3.8	"	11	Bottom of shallow basin	
Plateau		10	. 5*	0.335**	6	3.	5		"	Top of faint mound	

0	Depth	Snow acc	umulation	De	nsity	Water acc	umulation		Snow	
Station No.	of pit (cm)	Min. (cm/year)	Max. (cm/year)	Average (g/cm ³)	Number of measure- ment	Min. (cm/year)	Max. (cm/year)	in a pit wall	surface condi- tion	Surface topography of ice sheet
675	180	10.6	11.2	0.345	15	3.7	3.9	Irregular	Gullied	Even feature
687	178	10.5	11.1	0.343	20	3.6	3.8	Uniform	"	"
705	170	11.3	13.0	0.352	17	4.0	4.6	Irregular	"	"
723	198	11.6	12.3	0.321	20	3.7	3.9	Uniform	Smooth	Faint saddle
735	193	13.8	16.0	0.368	39	5.1	5.9	Irregular	Gullied	Even feature
753	194	13.8	14.9	0.364	24	5.0	5.4	Very irregular	"	Bottom of narrow trough
765	201	15.5	15.5	0.376	30	5.8	5.8	Irregular	Glazed	Northside of trough
783	192	17.5	17.5	0.397	37	7.0	7.0	"	Gullied	"
795	206	17.2	18.7	0.380	39	6.5	7.1	11	"	Even feature
813	196	14.1	14.1	0.377	38	5.3	5.3	"	Glazed	Gentle slope down to the
825	200	18.1	20.0	0.378	38	6.8	7.6	"	Gullied	J
837	318	19.9	22.7	0.394	49	7.6	8.9	"	"	"
855	205	14.6	17.0	0.365	40	5.3	6.2	"	"	Even feature
873	198	16.5	18.0	0.362	26	6.0	6.5	Very irregular	"	Southside of saddle
885	201	20.1	20.1	0.388	38	7.8	7.8	"	"	Gentle slope down to the
903	194	17.6	17.6	0.376	34	6.6	6.6	Uniform	Smooth	Bottom of shallow basin
915	192	17.5	19.2	0.374	31	6.6	7.2	Irregular	Gullied	Southside of dominant
933	193	17.5	19.3	0.349	37	6.1	6.7	"	Smooth	Top of dominant mound
945	199	18.1	19.9	0.363	38	6.6	7.2	"	"	"
957	200	16.7	22.2	0.344	38	5.7	7.6	Uniform	11	Northside of mound
975	203	20.3	22.5	0.356	40	7.2	8.0	"	"	Bottom of shallow basin
South Pole		22	2. 8*	0.334***	4	7	. 6			

* Meteorological data of each station.

** Average density of near surface snow (0-20 cm deep) at Sts. 646 and 675.

*** Average density of near surface snow (0-20 cm deep) at St. 975.

Fig. 9. Pit diagrams at Sts. 70, 330, 556, 753, 837, and 945.

Table 4, and Fig. 2 in p. 46 (FUJIWARA *et al.*, 1971) give the annual snow accumulation determined by the snow stratigraphy. In Fig. 7, in which the accumulations obtained from the snow stakes are plotted, the accumulations from the stratigraphy are shown by cross marks. The values of accumulation from the stakes and stratigraphy agree fairly well, except at St. 30, St. 70, and St. 122.

Reference

FUJIWARA, K., S. KAKINUMA, and Y. YOSHIDA (1971): Survey and some considerations on the antarctic ice sheet. JARE Scient. Rep., Special Issue, No. 2, 30-48.