

# Oscillatory periodic pattern dynamics in hyperbolic reaction-advection-diffusion models

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## Abstract

In this work we consider a quite general class of two-species hyperbolic reaction-advection-diffusion system with the main aim of elucidating the role played by inertial effects in the dynamics of oscillatory periodic patterns. To this aim, first, we use linear stability analysis techniques to deduce the conditions under which wave (or oscillatory Turing) instability takes place. Then, we apply multiple-scale weakly nonlinear analysis to determine the equation which rules the spatio-temporal evolution of pattern amplitude close to criticality. This investigation leads to a cubic complex Ginzburg Landau (CCGL) equation which, owing to the functional dependence of the coefficients here involved on the inertial times, reveals some intriguing consequences. To show in detail the richness of such a scenario, we present, as an illustrative example, the pattern dynamics occurring in the hyperbolic generalization of the extended Klausmeier model. This is a simple two-species model used to describe the migration of vegetation stripes along the hillslope of semiarid environments. By means of a thorough comparison between analytical predictions and numerical simulations, we show that inertia, apart from enlarging the region of the parameter plane where wave instability occurs, may also modulate the key features of the coherent structures, solution of the CCGL equation. In particular, it is proven that inertial effects play a role, not only during transient regime from the spatially-homogeneous steady state toward the patterned state, but also in altering the amplitude, the wavelength, the angular frequency and even the stability of the phase winding solutions.

**Keywords:** wave instability; hyperbolic model; weakly nonlinear analysis; inertial effects, cubic complex Ginzburg-Landau equation.

## 1 Introduction

Pattern formation and modulation is an active branch of mathematics, not only from the perspective of fundamental theory but also for its huge applications in many fields of physics, ecology, chemistry, biology and other sciences [1–6]. In 1952, Alan Turing proposed the mechanism through which a pattern-forming instability develops [7]. It arises from the coupling of diffusion and reaction kinetics,

30 and is based on the destabilization of a spatially uniform steady state due to a perturbation of a  
31 given wavenumber.

32 The occurrence of such an instability is theoretically investigated by addressing, first, linear and,  
33 then, weakly-nonlinear stability analysis.

34 Linear Stability Analysis (LSA) is aimed at defining the critical threshold of the control parameter  
35 responsible for the instability. When addressing this study, it should be kept in mind that the  
36 simplest bifurcation of a spatially uniform steady state may result in the spontaneous formation  
37 of patterns that are: oscillatory in time and uniform in space, stationary in time and periodic in  
38 space or oscillatory in time and periodic in space. The primary bifurcations associated to these  
39 classes of patterns are classically identified as Hopf, Turing and wave (also named Turing-Hopf or  
40 oscillatory-Turing), respectively [8].

41 Weakly-Nonlinear stability Analysis (WNA) is focused on deducing the equation governing the  
42 evolution of pattern amplitude (or envelope) close to criticality. In spatially extended systems,  
43 pattern amplitude is usually ruled by the well-known (real or complex) Ginzburg-Landau equation,  
44 which represents a general normal-form type of equation, valid for a large class of bifurcations and  
45 nonlinear wave phenomena occurring in many areas of sciences [1, 2, 5, 6, 9–18]. In particular, when  
46 applied to the study of oscillatory periodic patterns, the Ginzburg-Landau equation has complex  
47 coefficients and doesn't have a Lyapunov functional [1, 2, 5, 6, 19–23]. Its simplest solutions are in  
48 the form of coherent structures, among which plane-wave (or traveling-wave) solutions represent the  
49 easiest and most intuitive example.

50 In this work we focus our attention on the occurrence of wave instability with the goal of charac-  
51 terizing the dynamics of traveling patterns in one-dimensional *hyperbolic* reaction-advection-diffusion  
52 systems for two interacting species. In particular, by using the above-mentioned tools of LSA and  
53 WNA, we aim at elucidating the role played by inertia in modifying the instability threshold, the  
54 key features of the emerging patterns and their stability.

55 This work is an attempt to provide a step forward towards a deeper understanding of the un-  
56 derlying mechanisms involved into the formation of traveling patterns in hyperbolic models. Indeed,  
57 the goal is to extend the literature of hyperbolic systems that encloses several related works focusing  
58 for instance on: wave instability in systems where one species diffuses and the other ones undergoes  
59 advection, by adopting LSA only [24]; Turing and wave instabilities in the presence of cross-diffusion,  
60 with no advection, by adopting LSA and WNA in limited domains [25] or LSA only [8, 26]; Turing  
61 instability in the absence of advection, by using LSA and WNA in extended domains with con-  
62 stant [27–29] and non-constant [30] inertial times; traveling fronts in models with advection [31, 32]  
63 or in its absence considering self-diffusion [33] and cross-diffusion [34].

64 As widely outlined in all the above-mentioned works, the use of an hyperbolic framework has  
65 a manifold justification. First, it is well known that parabolic models suffer from the paradox of  
66 infinite propagation speed of disturbances, whereas hyperbolic models overcome this problem by  
67 accounting for relaxational effects due to the delay of the species in adopting one definite mean  
68 speed and direction to propagate [32]. Therefore, these latter are better suited to describe transient  
69 regimes, especially those involving long time scales. Moreover, the inertial (delay) times constitute  
70 additional degrees of freedom that may be used to better mimic experimental observations and, at  
71 the same time, offer a richer scenario of dynamics [28, 29, 35–45].

72 The theoretical predictions here carried out are then corroborated by numerical investigations  
73 on the so-called extended Klausmeier model, taken into account as an illustrative example of a two-  
74 species system where the combination of kinetics, diffusion and advection gives rise to oscillatory

75 periodic patterns. It is a conceptual model for surface water and vegetation biomass, used to describe  
76 the formation and migration of vegetation patterns over sloping terrains of semi-arid ecosystems. This  
77 model, among many others [46–50], aims at exploring the processes of desertification occurring in such  
78 drylands areas [51–55]. In its original formulation [56], this model accounted for the isotropic diffusion  
79 of vegetation and the anisotropic advection of water along the hillslope. Later [57], this model has  
80 been extended to account also for diffusion of water and, in [58], it has been further generalized  
81 to include the phenomenon of secondary-seed dispersal. All the above models are able to capture  
82 the uphill migration of vegetation bands, which are believed to be observed experimentally [45, 59].  
83 Moreover, to account for the relevance of biological inertia in plant communities to ecology of arid  
84 ecosystems [36, 42, 44] as well as to provide a proper description of long transient pattern dynamics  
85 [60–63], hyperbolic generalizations of Klausmeier model have been proposed in [24, 27, 30, 31].

86 The paper is outlined as follows. In Section 2, we present the class of hyperbolic reaction-  
87 advection-diffusion models and characterize the phenomenon of wave instability through LSA and  
88 WNA. In Section 3, we compare our results of analytical predictions to those arising from numerical  
89 simulations, carried out on the hyperbolic version of the extended Klausmeier model. Conclusions  
90 are given in the last section.

## 91 2 Model formulation and analytical investigations

92 We consider a class of hyperbolic reaction-advection-diffusion systems for two species  $u(x, t)$  and  
93  $w(x, t)$  satisfying the following hypotheses: dynamics takes place at time  $t$  and along a preferred  
94 direction  $x$ ;  $w$  undergoes both diffusion and advection with a velocity denoted by  $\nu$ , whereas  $u$  has  
95 a diffusive character only; the  $w$ -by- $u$  diffusion ratio is termed  $d$ ; the inertial times associated to  
96 the two species are denoted by  $\tau^u$  and  $\tau^w$ , which are assumed to be constant; kinetic terms are  
97 generically indicated by  $f(u, w)$  and  $g(u, w)$ . Following the guidelines of Extended Thermodynamics  
98 (ET) theory [64], we also introduce two additional field variables representing the diffusive fluxes,  
99  $J^u(x, t)$  and  $J^w(x, t)$ , each of them obeying a thermodynamically-consistent balance equation that,  
100 in the parabolic limit approximation,  $\tau^u \rightarrow 0$  and  $\tau^w \rightarrow 0$ , recover the classical constitutive Fick's  
101 law.

102 According to these assumptions, the hyperbolic system can be expressed in vector form as:

$$\mathbf{U}_t + M\mathbf{U}_x = \mathbf{N}(\mathbf{U}), \quad (1)$$

103 being:

$$\mathbf{U} = \begin{bmatrix} u \\ w \\ J^u \\ J^w \end{bmatrix}, \quad M = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & -\nu & 0 & 1 \\ \frac{1}{\tau^u} & 0 & 0 & 0 \\ 0 & \frac{d}{\tau^w} & 0 & 0 \end{bmatrix}, \quad \mathbf{N}(\mathbf{U}) = \begin{bmatrix} f(u, w) \\ g(u, w) \\ -\frac{J^u}{\tau^u} \\ -\frac{J^w}{\tau^w} \end{bmatrix} \quad (2)$$

104 where the subscript stands for the partial derivative with respect to the indicated variable.

105 Note that the model (2) belongs to a more general class of  $n$ -species hyperbolic reaction-advection-  
106 diffusion systems deduced via ET and reported in [31].

107 In the following subsections, we will address LSA and WNA on the steady states admitted by  
108 this model with particular emphasis on the occurrence of wave instability.

## 2.1 Linear Stability Analysis

Let  $\mathbf{U}^* = (u^*, v^*, 0, 0)$  be a positive spatially-homogeneous steady-state satisfying  $\mathbf{N}(\mathbf{U}) = \mathbf{0}$ . By looking for solutions of system (1) of the form  $\mathbf{U} = \mathbf{U}^* + \widehat{\mathbf{U}} \exp(\omega t + i k x)$ , we derive the following dispersion relation which gives the growth factor  $\omega$  as a function of the wavenumber  $k$ :

$$\tau^u \tau^w \omega^4 + (\widetilde{A}_3 - ik\nu \tau^u \tau^w) \omega^3 + (\widehat{A}_2 k^2 + \widetilde{A}_2 + ik\nu \widehat{b}_2) \omega^2 + \left[ \widehat{A}_1 k^2 + \widetilde{A}_1 + ik\nu (\widehat{b}_1 - \tau^w k^2) \right] \omega + \widetilde{A}_0 + ik\nu \widehat{b}_0 = 0 \quad (3)$$

with

$$\begin{aligned} \widetilde{A}_3 &= \tau^u + \tau^w - (f_u^* + g_w^*) \tau^u \tau^w \\ \widehat{A}_2 &= d\tau^u + \tau^w \\ \widetilde{A}_2 &= 1 - (\tau^u + \tau^w) (f_u^* + g_w^*) + \tau^u \tau^w (f_u^* g_w^* - f_w^* g_u^*) \\ \widehat{b}_2 &= \tau^u \tau^w f_u^* - \tau^u - \tau^w \\ \widehat{A}_1 &= d + 1 - \tau^w g_w^* - d\tau^u f_u^* \\ \widetilde{A}_1 &= (\tau^u + \tau^w) (f_u^* g_w^* - f_w^* g_u^*) - (f_u^* + g_w^*) \\ \widehat{b}_1 &= (\tau^u + \tau^w) f_u^* - 1 \\ \widetilde{A}_0 &= dk^4 - (df_u^* + g_w^*) k^2 + f_u^* g_w^* - f_w^* g_u^* \\ \widehat{b}_0 &= f_u^* - k^2 \end{aligned} \quad (4)$$

where the asterisk denotes that the function is evaluated at the steady state  $\mathbf{U}^*$ .

It is straightforward to ascertain that, for homogeneous perturbation  $k = 0$ , the equation (3) can be easily factorized and its solutions are:

$$\omega_1 = -\frac{1}{\tau^u} < 0 \quad \omega_2 = -\frac{1}{\tau^w} < 0 \quad \omega_{3,4} = \frac{1}{2} \left( f_u^* + g_w^* \pm \sqrt{(f_u^* + g_w^*)^2 - 4(f_u^* g_w^* - f_w^* g_u^*)} \right). \quad (5)$$

Therefore  $\mathbf{U}^*$  is stable with respect homogeneous perturbation iff:

$$f_u^* + g_w^* < 0, \quad f_u^* g_w^* - f_w^* g_u^* > 0. \quad (6)$$

As far as non-homogeneous perturbations are concerned, we notice that a non-vanishing advection term ( $\nu \neq 0$ ) prevents the occurrence of Turing instability, because the expression  $\widetilde{A}_0 + ik\nu \widehat{b}_0$  is nonzero for all values of  $k$ . Therefore, we focus our attention on the occurrence of wave instability as a control parameter, say  $B$ , is varied. To this aim, we look for solutions of the characteristic equation (3) having null real part for some  $k \neq 0$  and require the transition from negative to positive real part to occur via a maximum. More precisely, we assume  $\omega = -isk$ , with  $s = s(k) \in \mathbb{R}$  so that any perturbation can be recast in the form of a travelling plane wave with speed  $s$ , i.e.  $\widehat{\mathbf{U}} \exp[ik(x - st)]$ . Then, by substituting the previous ansatz into the characteristic equation and taking the derivative of this latter with respect to  $k$ , we obtain:

$$\begin{cases} k^4 - \delta_2 k^2 + \delta_4 = 0 \\ \delta_1 k^2 - \delta_3 = 0 \\ 2k(2k^2 - \delta_2) + \left( \frac{\partial \delta_4}{\partial s} - \frac{\partial \delta_2}{\partial s} k^2 \right) \frac{\partial s}{\partial k} = 0 \\ (\delta_1 \delta_2 - 2\delta_3) \left( \delta_1 \frac{\partial \delta_3}{\partial s} - \delta_3 \frac{\partial \delta_1}{\partial s} \right) - \delta_1^2 \left( \delta_1 \frac{\partial \delta_4}{\partial s} - \delta_3 \frac{\partial \delta_2}{\partial s} \right) = 0 \end{cases} \quad (7)$$

127 where

$$\begin{aligned}
\delta_1 &= \frac{\nu + \widehat{A}_1 s + \nu \widehat{b}_2 s^2 - \widetilde{A}_3 s^3}{(\tau^u s^2 - 1)(\tau^w s^2 + \nu \tau^w s - d)}, \\
\delta_2 &= \frac{\widetilde{A}_2 s^2 - \widehat{b}_1 \nu s + d f_u^* + g_w^*}{(\tau^u s^2 - 1)(\tau^w s^2 + \nu \tau^w s - d)}, \\
\delta_3 &= \frac{\nu f_u^* - \widetilde{A}_1 s}{(\tau^u s^2 - 1)(\tau^w s^2 + \nu \tau^w s - d)}, \\
\delta_4 &= \frac{(f_u^* g_w^* - f_w^* g_u^*)}{(\tau^u s^2 - 1)(\tau^w s^2 + \nu \tau^w s - d)}.
\end{aligned} \tag{8}$$

128 System (7) defines implicitly the critical value  $B_c$  of the control parameter at which wave insta-  
129 bility develops, together with the critical wavenumber  $k_c$ , the wave speed  $s$  and its derivative with  
130 respect to the wavenumber  $\partial s / \partial k$ . Therefore, we can draw a first conclusion that the presence of  
131 inertia affects not only the instability threshold but also the wavenumber of the emerging pattern.  
132 This result differs from what observed in the case of pure stationary Turing patterns, where hyper-  
133 bolicity does not affect such quantities but plays an active role during transient regime [27, 30].

134  
135 Notice that in the limit case  $\tau^u \rightarrow 0$  and  $\tau^w \rightarrow 0$  the hyperbolic model (1),(2) reduces to the  
136 corresponding *parabolic* one. Details on the structure of the parabolic model, the characteristic  
137 equation and the locus of wave instability are given in Appendix A.

## 138 2.2 Multiple-scale weakly nonlinear analysis

139 As it is well known, LSA is only valid for small times and infinitesimal perturbations. For this reason,  
140 the transition to the new spatially nonuniform state is usually investigated by means of WNA which,  
141 by using a standard perturbative approach, provides an approximate analytical description of the  
142 perturbation dynamics. In this Section, we shall employ the multiple scale method to derive the  
143 amplitude equation describing the dynamics close to the critical bifurcation parameter  $B_c$  at which  
144 instability develops [5, 6, 25, 27–29, 65–67].

145 We recast the original system (1) in the following form:

$$\overline{\mathbf{U}}_t + M \overline{\mathbf{U}}_x = L^* \overline{\mathbf{U}} + \mathbf{NL}^*, \tag{9}$$

146 where the matrix  $L^*$ , the vectors  $\overline{\mathbf{U}}$  and  $\mathbf{NL}^*$  are defined as

$$\overline{\mathbf{U}} = \mathbf{U} - \mathbf{U}^* \tag{10}$$

$$L^* = (\nabla \mathbf{N})^* \tag{11}$$

$$\mathbf{NL}^* = \sum_{k \geq 2} \frac{1}{k!} \left[ (\overline{\mathbf{U}} \cdot \nabla)^{(k)} \mathbf{N} \right]^* \tag{12}$$

147 and  $\nabla = \partial / \partial \mathbf{U}$ , for a generic vector  $\mathbf{V}$ , the expression  $(\mathbf{V} \cdot \nabla)^{(j)}$  stands for the operator

$$\mathbf{V} \cdot \nabla = V_1 \frac{\partial}{\partial u} + V_2 \frac{\partial}{\partial w} + V_3 \frac{\partial}{\partial J^u} + V_4 \frac{\partial}{\partial J^w} \tag{13}$$

148 applied  $j$  times.

149 First, we expand the field vector  $\bar{\mathbf{U}}$  as well as the control parameter  $B$  with respect to a small  
 150 positive parameter  $\varepsilon \ll 1$  and introduce two time and spatial scales as follows:

$$\begin{aligned}\bar{\mathbf{U}} &= \varepsilon \bar{\mathbf{U}}_1 + \varepsilon^2 \bar{\mathbf{U}}_2 + \varepsilon^3 \bar{\mathbf{U}}_3 + O(\varepsilon^4) \\ B &= B_c + \varepsilon^2 B_2 + O(\varepsilon^4) \\ \frac{\partial}{\partial t} &\rightarrow \frac{\partial}{\partial t} + \varepsilon^2 \frac{\partial}{\partial T_2} \\ \frac{\partial}{\partial x} &\rightarrow \frac{\partial}{\partial x} + \varepsilon \frac{\partial}{\partial X}\end{aligned}\tag{14}$$

151 The use of two spatial scales is justified whenever patterns emerge and propagate over large spatial  
 152 domains in the form of traveling wavefronts.

153 Then, substituting all the above expansions into the governing system (9) and collecting terms  
 154 of the same orders of  $\varepsilon$  we obtain the following set of linear partial differential equations:

$$\begin{aligned}\text{at order 1} \quad & \frac{\partial \bar{\mathbf{U}}_1}{\partial t} + M \frac{\partial \bar{\mathbf{U}}_1}{\partial x} = L_c^* \bar{\mathbf{U}}_1 \\ \text{at order 2} \quad & \frac{\partial \bar{\mathbf{U}}_2}{\partial t} + M \frac{\partial \bar{\mathbf{U}}_2}{\partial x} + M \frac{\partial \bar{\mathbf{U}}_1}{\partial X} = L_c^* \bar{\mathbf{U}}_2 + \frac{1}{2} \left( \bar{\mathbf{U}}_1 \cdot \nabla \right)^{(2)} \mathbf{N}|_c^* \\ \text{at order 3} \quad & \frac{\partial \bar{\mathbf{U}}_3}{\partial t} + \frac{\partial \bar{\mathbf{U}}_1}{\partial T_2} + M \frac{\partial \bar{\mathbf{U}}_3}{\partial x} + M \frac{\partial \bar{\mathbf{U}}_2}{\partial X} = \\ & = L_c^* \bar{\mathbf{U}}_3 + B_2 \left. \frac{dL^*}{dB} \right|_c \bar{\mathbf{U}}_1 + \left( \bar{\mathbf{U}}_1 \cdot \nabla \right) \left( \bar{\mathbf{U}}_2 \cdot \nabla \right) \mathbf{N}|_c^* + \frac{1}{6} \left( \bar{\mathbf{U}}_1 \cdot \nabla \right)^{(3)} \mathbf{N}|_c^*\end{aligned}\tag{15}$$

155 where the subscript “ $c$ ” denotes that the quantity is evaluated at the critical value of the control  
 156 parameter. We now look for solution  $\bar{\mathbf{U}}_i = \bar{\mathbf{U}}_i(z)$  with  $z = x - st$ , so that the system (15) can be  
 157 written as a system of ordinary differential equations:

$$\text{at order 1} \quad \frac{d\bar{\mathbf{U}}_1}{dz} = K_c^* \bar{\mathbf{U}}_1\tag{16}$$

$$\text{at order 2} \quad \frac{d\bar{\mathbf{U}}_2}{dz} = K_c^* \bar{\mathbf{U}}_2 + (M - sI)^{-1} \left\{ \frac{1}{2} \left( \bar{\mathbf{U}}_1 \cdot \nabla \right)^{(2)} \mathbf{N}|_c^* - M \frac{\partial \bar{\mathbf{U}}_1}{\partial X} \right\}\tag{17}$$

$$\begin{aligned}\text{at order 3} \quad & \frac{d\bar{\mathbf{U}}_3}{dz} = K_c^* \bar{\mathbf{U}}_3 + (M - sI)^{-1} \times \\ & \times \left\{ B_2 \left. \frac{dL^*}{dB} \right|_c \bar{\mathbf{U}}_1 + \left( \bar{\mathbf{U}}_1 \cdot \nabla \right) \left( \bar{\mathbf{U}}_2 \cdot \nabla \right) \mathbf{N}|_c^* + \frac{1}{6} \left( \bar{\mathbf{U}}_1 \cdot \nabla \right)^{(3)} \mathbf{N}|_c^* - \frac{\partial \bar{\mathbf{U}}_1}{\partial T_2} - M \frac{\partial \bar{\mathbf{U}}_2}{\partial X} \right\}\end{aligned}\tag{18}$$

158 where  $I$  is the identity matrix and

$$K_c^* = (M - sI)^{-1} L_c^*\tag{19}$$

159 According to WNA developed in Appendix B, the solutions of systems (16) and (17), satisfying periodic  
 160 boundary conditions, take respectively the following structures:

$$\bar{\mathbf{U}}_1 = \Omega(X, T_2) e^{ik_c z} \mathbf{d}^{(ik_c)} + \bar{\Omega}(X, T_2) e^{-ik_c z} \mathbf{d}^{(-ik_c)}\tag{20}$$

$$\bar{\mathbf{U}}_2 = \frac{\partial \Omega}{\partial X} e^{ik_c z} \mathbf{g} + \frac{\partial \bar{\Omega}}{\partial X} e^{-ik_c z} \bar{\mathbf{g}} + \Omega^2 e^{2ik_c z} \mathbf{q} + \bar{\Omega}^2 e^{-2ik_c z} \bar{\mathbf{q}} + 2\mathbf{q}_0 |\Omega|^2\tag{21}$$

162 where the complex pattern amplitude  $\Omega$  obeys the Cubic Complex Ginzburg–Landau (CCGL) equation

$$\frac{\partial \Omega}{\partial T_2} = (\rho_1 + i\rho_2) \frac{\partial^2 \Omega}{\partial X^2} + (\sigma_1 + i\sigma_2) \Omega - (L_1 - iL_2) \Omega |\Omega|^2.\tag{22}$$

163 The coefficients appearing in (20)-(22) are given in Appendix B.

164 As known, two different qualitative dynamics of the CCGL equation can be observed:  $L_1 > 0$  corresponds  
 165 to the supercritical bifurcation case while  $L_1 < 0$  to the subcritical one. The former exists for above-  
 166 threshold values of the control parameter only, exhibits a small amplitude close to onset and the wavelength  
 167 of the excited pattern is close to the critical value  $2\pi/k_c$ . The latter exists for both below- and above-  
 168 threshold values, exhibits hysteresis and has a large amplitude at onset such that the WNA may only  
 169 provide qualitative information on the excited patterns [1, 5, 6].

170 **Remark 1.** The CCGL equation (22) deduced in the more general framework of hyperbolic systems appears  
 171 formally unchanged with respect to the classical one deduced in *parabolic* models [67]. It can be indeed  
 172 verified that the expressions of the coefficients there appearing may be obtained from the ones appearing  
 173 in (22) by setting the inertial times to zero. Of course, each of these coefficients encloses a dependence on  
 174 the inertial times which, acting as additional degrees of freedom, offers a richer scenario of spatio-temporal  
 175 dynamics with respect to the parabolic counterpart, as it will be shown below.  $\square$

## 176 2.2.1 Coherent structure solutions of the CCGL equation

177 Let us now focus our attention on those solutions of the CCGL equation that are referred to as *coherent*  
 178 *structures*, and in particular to the one-parameter family of solutions localized in space characterized by  
 179 features uniformly translating with a constant velocity  $v$  [1, 5, 19–23], i.e:

$$\Omega(X, T_2) = Q(\xi)e^{i\phi(\xi)}, \quad \xi = X - vT_2 \quad (23)$$

180 Substituting this ansatz into the CCGL equation (22) and indicating by  $\kappa = \phi_\xi$ , we get a system of three  
 181 ordinary differential equations:

$$\begin{cases} Q_\xi = R \\ \rho_2 Q \kappa_\xi - \rho_1 R_\xi = (v - 2\rho_2 \kappa) R + (\sigma_1 - \rho_1 \kappa^2) Q - L_1 Q^3 \\ \rho_2 R_\xi + \rho_1 Q \kappa_\xi = -2\rho_1 \kappa R + (\rho_2 \kappa^2 - \sigma_2 - v\kappa) Q - L_2 Q^3 \end{cases} \quad (24)$$

182 The dynamical system (24) admits two fixed points in the form  $\mathbf{F}^* = (R^*, Q^*, \kappa^*)$  given by:  $\mathbf{F}_1^* = (0, 0, \kappa_0)$ ,  
 183 with  $\kappa_0$  an arbitrary constant, and  $\mathbf{F}_2^* = (0, \tilde{Q}, \tilde{\kappa})$ , where the constants  $\tilde{Q}$  and  $\tilde{\kappa}$  are defined by:

$$\begin{aligned} \tilde{Q} &= \sqrt{\frac{\sigma_1 - \rho_1 \tilde{\kappa}^2}{L_1}} \\ (\rho_1 L_2 + \rho_2 L_1) \tilde{\kappa}^2 - v L_1 \tilde{\kappa} - (\sigma_2 L_1 + \sigma_1 L_2) &= 0 \end{aligned} \quad (25)$$

184 The fixed point  $\mathbf{F}_1^*$  defines a null-amplitude patterned state  $\Omega = 0$  that is representative of the spatially-  
 185 homogeneous steady state  $\mathbf{U}^*$  undergoing the spatially-driven destabilization. On the other hand, the  
 186 plane-wave solution of the CCGL equation associated to the fixed point  $\mathbf{F}_2^*$ , i.e.

$$\Omega(X, T_2) = \tilde{Q} e^{i(\tilde{\kappa}X + \tilde{\omega}T_2)} \quad \text{with} \quad \tilde{\omega} = -\tilde{\kappa}v \quad (26)$$

187 represents a particular case of coherent structure named *phase winding* solution [1, 5, 21, 23, 68] and describes  
 188 a traveling pattern characterized by a total wavenumber  $k_{tot} = k_c + \tilde{\kappa}$  and angular frequency  $\omega_{tot} = k_c s - \epsilon^2 \tilde{\omega}$ .  
 189 If the wave bifurcation is supercritical ( $L_1 > 0$ ), under the assumptions that  $\sigma_1 > 0$  and  $\rho_1 > 0$ , according  
 190 to (25)<sub>1</sub>, such a solution exists if

$$-\sqrt{\frac{\sigma_1}{\rho_1}} < \tilde{\kappa} < +\sqrt{\frac{\sigma_1}{\rho_1}} \quad (27)$$

191 so that there is a band of permitted wavenumbers around  $\tilde{\kappa} = 0$  and the second-order correction of the  
 192 angular frequency takes the form:

$$\tilde{\omega} = \left[ (\sigma_2 L_1 + \sigma_1 L_2) - (\rho_1 L_2 + \rho_2 L_1) \tilde{\kappa}^2 \right] / L_1 \quad (28)$$

193 Since we deal with three unknowns ( $\tilde{\kappa}$ ,  $\tilde{Q}$  and  $\tilde{\omega}$ ) and two conditions arising from the CCGL equation, one  
 194 parameter needs to be estimated from numerical simulations. For instance,  $\tilde{\kappa}$  can be deduced by comparing  
 195 the numerically-computed value of the total wavenumber  $k_{tot}$  with the theoretical critical wavenumber  $k_c$ ,  
 196 whereas the values of amplitude  $\tilde{Q}$  and angular frequency  $\tilde{\omega}$  can be consequently obtained via (25)<sub>1</sub> and  
 197 (28), respectively.

198 To investigate the stability of the phase winding solution, we can proceed, as usual in the literature, by  
 199 perturbing the amplitude (26) as follows:

$$\begin{aligned} \Omega(X, T_2) &= [1 + a(X, T_2)] \tilde{Q} e^{i(\tilde{\kappa}X + \tilde{\omega}T_2)} \\ a(X, T_2) &= \Psi(T_2) e^{i l X} + \bar{\Xi}(T_2) e^{-i l X} \end{aligned} \quad (29)$$

200 with  $l$  the small perturbation of the wavenumber  $\tilde{\kappa}$ , namely we look for long-wave effects. After some  
 201 algebraic manipulations, we end up with the system:

$$\begin{cases} \Psi_{T_2} = \left[ -l(l + 2\tilde{\kappa})(\rho_1 + i\rho_2) - \tilde{Q}^2(L_1 - iL_2) \right] \Psi - (L_1 - iL_2) \tilde{Q}^2 \Xi \\ \Xi_{T_2} = \left[ -l(l - 2\tilde{\kappa})(\rho_1 - i\rho_2) - \tilde{Q}^2(L_1 + iL_2) \right] \Xi - (L_1 + iL_2) \tilde{Q}^2 \Psi \end{cases} \quad (30)$$

202 where  $\bar{\Xi}$  is the complex conjugate of  $\Xi$ .

203 Then, looking for the usual exponential dependence of  $\Psi$  and  $\Xi$  on  $T_2$ , in the limit of large wavelengths  
 204 (small  $l$ ), one retrieves a necessary condition for the stability of plane wave structures, named *Benjamin-*  
 205 *Feir-Newell* condition [1, 2, 6, 23, 67], that reads:

$$1 - \frac{\rho_2 L_2}{\rho_1 L_1} > 0. \quad (31)$$

206 **Remark 2.** It should be finally noticed that all the features characterizing the phase winding solution,  
 207 i.e. amplitude  $\tilde{Q}$ , wavenumber  $\tilde{\kappa}$  and angular frequency  $\tilde{\omega}$ , together with its stability, inherit the functional  
 208 dependence on the inertial times from the coefficients of the CCGL equation (22). Therefore, it is expected  
 209 that hyperbolicity effects may manifest, not only during the transient regime from the homogeneous steady  
 210 state toward the patterned state (the heteroclinic orbit of (24) joining  $\mathbf{F}_1^*$  and  $\mathbf{F}_2^*$ ) but also modifying the  
 211 value of the above-mentioned key features of the phase winding solution and, possibly, its stability.  $\square$



### 212 3 An illustrative example: the extended Klausmeier model

213 As an illustrative example, let us take into account the hyperbolic generalization [24, 27, 30, 31] of the  
 214 extended Klausmeier model [57, 67], whose dimensionless 1D version belongs to the class of systems (1),(2).  
 215 In this framework, the field variables  $u(x, t)$  and  $w(x, t)$  assume the meaning of densities of plant biomass  
 216 and surface water, respectively, at location  $x$  (positive direction being uphill) and time  $t$ . In this model, the  
 217 motion of surface water accounts for two different mechanisms. First, the downhill water flow on slopes is  
 218 accounted by an advection term. Second, dispersal of surface water is mimicked via a diffusion term that  
 219 aims at capturing the movement induced by spatial differences in infiltration rate [57]. The coefficient  $d$  is  
 220 here representative of the water-to-plant diffusion ratio whereas  $\nu$  is the water advection speed along the  
 221 hillslope. The source terms, unchanged with respect to those originally proposed by Klausmeier [56], are  
 222 given by:

$$\begin{aligned} f(u, w) &= w u^2 - B u \\ g(u, w) &= A - w - w u^2 \end{aligned} \quad (32)$$

223 where the dimensionless coefficients  $A$  and  $B$  are related to the rates of average annual rainfall and plant  
 224 loss, respectively. Previous investigations suggest that realistic values of plant loss and rainfall rate belong  
 225 to the ranges  $B \in (0, 2)$  and  $A \in (0, 3)$ , respectively [47, 56, 69].

226 It is known that, for  $A \geq 2B$  this model admits three spatially-homogeneous steady states given by:

$$\begin{aligned} \mathbf{U}_D^* &= (0, A, 0, 0) \\ \mathbf{U}_L^* &= (u_L, B/u_L, 0, 0) \\ \mathbf{U}_S^* &= (u_S, B/u_S, 0, 0) \end{aligned} \quad (33)$$

227 where:

$$u_L = \frac{A - \sqrt{A^2 - 4B^2}}{2B}, \quad u_S = \frac{A + \sqrt{A^2 - 4B^2}}{2B}, \quad 0 < u_L < 1 < u_S, \quad (34)$$

228 the first being representative of the desert state and the other ones of uniformly-vegetated areas. For  
 229  $A < 2B$ , the desert state becomes the only steady state admitted by the model.

230 It can be easily checked that the desert state  $\mathbf{U}_D^*$  is always stable whereas the vegetated state  $\mathbf{U}_L^*$  is  
 231 always unstable. On the contrary, the state  $\mathbf{U}_S^*$  is stable with respect to homogeneous perturbations. Indeed,  
 232 by considering that:

$$f_u^* = f_u(\mathbf{U}_S^*) = B, \quad f_w^* = f_w(\mathbf{U}_S^*) = u_S^2, \quad g_u^* = g_u(\mathbf{U}_S^*) = -2B, \quad g_w^* = g_w(\mathbf{U}_S^*) = -(1 + u_S^2), \quad (35)$$

233 conditions (6) become:

$$f_u^* + g_w^* = B - 1 - u_S^2 < 0, \quad f_u^* g_w^* - f_w^* g_u^* = B(u_S^2 - 1) > 0, \quad (36)$$

234 that are fulfilled for any realistic values of  $B$  and  $u_S$ .

235 To prove that the state  $\mathbf{U}_S^*$  may be destabilized via non-homogeneous perturbations, and can thus  
 236 undergo wave instability, we need to solve the system (7),(8). Unfortunately, owing to its highly nonlinear  
 237 nature, information on the locus of wave instability, together with the dependence of the critical parameters  
 238 on the inertial times, cannot be obtained analytically. Therefore, by solving the above system numerically,  
 239 we found that it admits real solutions representing the values of the control parameter  $B_c$ , wavenumber  $k_c$ ,  
 240 wave speed  $s$  and its derivative with respect to  $k$ , at the onset of instability. Results of this investigation  
 241 are shown in Fig.1, where the locus of wave instability depicted in the  $(B, A)$  parameter plane (solid lines)  
 242 is obtained by fixing the parameters  $d = 100$  [57, 70] and  $\nu = 182.5$  [56] and varying the two inertial times  
 243  $\tau^u$  and  $\tau^w$ . In the same figure we also represent by circles the locus obtained in the parabolic case, i.e. from

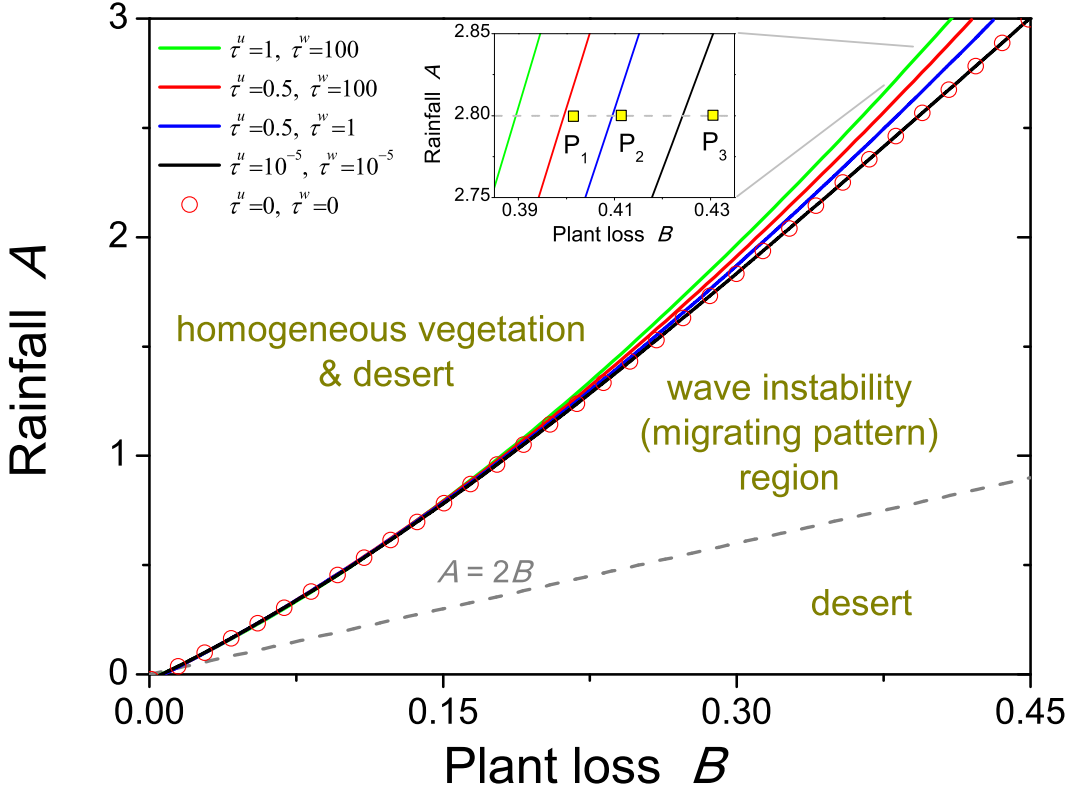


Figure 1: Solid lines represent the loci of wave instability in the  $(B, A)$  parameter plane obtained by solving numerically the system (7),(8) for different values of inertial times. Symbols denote the locus obtained in the parabolic case, resulting from integration of equation (A.4). The bottom dashed line defines the condition  $A = 2B$ , below which the only desert state exists. Fixed parameters:  $d = 100$  and  $\nu = 182.5$ .

244 the numerical solution of (A.4), which gives real and positive root by taking the plus sign. As it can be  
 245 noticed, this latter coincides with the locus deduced for very small inertial times (black line), as expected.  
 246 It is worth noticing that, when the system moves away from the parabolic limit, the locus of wave instability  
 247 progressively shifts up so enlarging the region where non-stationary patterns may be observed. This is  
 248 consistent with our previous results obtained for the hyperbolic generalization of the original Klausmeier  
 249 model, so confirming that the hyperbolicity destabilizes the system and allows to observe oscillatory periodic  
 250 patterns, i.e. uphill migrating banded vegetation in the context of dry-land ecology, over a wider region of  
 251 the parameter plane [24].

252 A first check on the validity of these analytical predictions has been carried out by inspecting the  
 253 wavenumber dependence of the four roots of the characteristic polynomial (3) at the three points  $P_1$ ,  $P_2$   
 254 and  $P_3$  indicated in the inset of Fig.1, for different couples of inertial times. Results are shown in Fig.2 (top  
 255 row panels (a)-(c) correspond to  $P_1$ , middle row panels (d)-(f) to  $P_2$  and bottom row panels (g)-(i) to  $P_3$ )  
 256 for the largest eigenvalue only (being the real part of the other three roots always negative). For brevity, we  
 257 refer to the couple  $(\tau^u, \tau^w) = (10^{-5}, 10^{-5})$  (whose corresponding locus is the black curve in Fig.1) as setup  
 258  $I$ ; the couple  $(0.5, 1)$  as setup  $II$  (blue curve in Fig.1) and  $(0.5, 100)$  as setup  $III$  (red curve in Fig.1). Setup  
 259  $I$  is representative of the behavior close to the parabolic limit, while setups  $II$  and  $III$  mimic dynamics  
 260 that progressively deviate away from it.

261 Let us investigate, first, the locus of roots related to  $P_1$ . Results related to setups *I* and *II* (panels (a) and  
262 (b)) reveal that all roots have negative real part, denoting that the state  $\mathbf{U}_S^*$  is also stable with respect to non-  
263 homogeneous perturbations. On the contrary, in setup *III* (panel (c)), there exists a range of wavenumber  
264 where one root has positive real part and non-null imaginary part, so pointing out a destabilization of the  
265 steady state. These observations are consistent with the predictions reported in Fig.1 because, in setups *I*  
266 and *II*, the investigated point is outside the wave instability region but, in setup *III*, it is located inside.  
267 About the point  $P_2$ , in setups *II* and *III* (panels (e),(f)) there exists a range of  $k$  where the real part of the  
268 most unstable root becomes positive. On the contrary, in setup *I* (panel (d)), the real part of this root keeps  
269 negative, consistently with its location with respect to the bifurcation loci. Finally, at point  $P_3$ , for each of  
270 the chosen setups (panels (g),(h),(i)), there exists a range of  $k$  where the real part of the most unstable root  
271 becomes positive, consistently with the fact that this point always lies inside the wave instability region.

272 Another confirmation of the analytical predictions carried out in Section 2.1 may be achieved by inte-  
273 grating numerically the governing system (1),(2),(32) together with periodic boundary conditions and  
274 using small sinusoidal fluctuations about the steady state  $\mathbf{U}_S^*$  as initial conditions. Simulations have been  
275 performed by means of COMSOL Multiphysics<sup>®</sup> [71] over a time window  $t \in [0, 50]$ , considering a spatial  
276 domain of length  $l_D = 100$  (unless specified differently). Results of this investigation, which make use of the

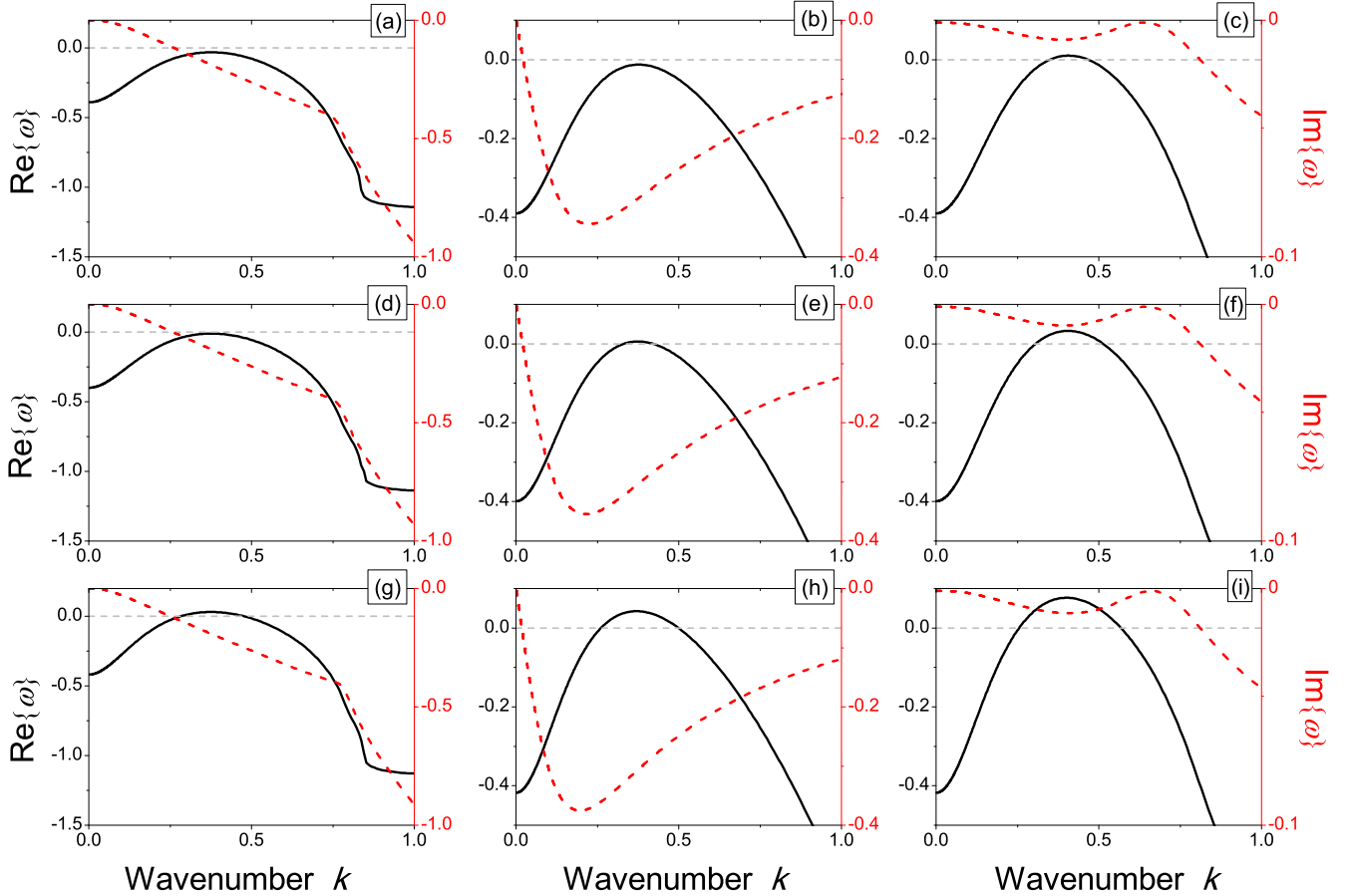


Figure 2: Wavenumber dependence of the real (left axes, continuous lines) and imaginary (right axes, discontinuous lines) part of largest root of (3) evaluated for  $A = 2.8$  at the points  $P_1$  ( $B = 0.40$ , panels (a)-(c)),  $P_2$  ( $B = 0.41$ , panels (d)-(f)) and  $P_3$  ( $B = 0.43$ , panels (g)-(i)) indicated in Fig.1, for different couples of inertial times  $(\tau^u, \tau^w)$ . In detail, setup *I*:  $(10^{-5}, 10^{-5})$ , panels (a),(d),(g); setup *II*:  $(0.5, 1)$ , panels (b),(e),(h); setup *III*:  $(0.5, 100)$ , panels (c),(f),(i).

277 same parameter set as the one used in Fig.2, are reported in Fig.3. To provide an immediate and intuitive  
 278 view of the underlying dynamics, the colormap used for the density plots of vegetation biomass  $u(x, t)$  ranges  
 279 between yellow (desert) and green (vegetated areas). In agreement with the above-mentioned predictions,  
 280 it is possible to notice that, when all the roots have negative real parts, the initial perturbation dies out  
 281 and the system converges toward the stable, spatially-uniform, vegetated state  $\mathbf{U}_S^*$ , see panels (a),(b),(d).  
 282 On the contrary, if there exists a range of unstable wavenumbers, then the system evolves toward a periodic  
 283 patterned state that oscillates in time, representative of an uphill migrating vegetation band, see panels  
 284 (c),(e)-(i).

285 We can also numerically verify whether the range of unstable wavenumbers depends on inertia. It is  
 286 known that, if a non-homogeneous perturbation is applied to a state  $\mathbf{U}^*$  falling within the wave instability  
 287 region, the system tends to form a traveling pattern whose wavenumber is close to the one of the most  
 288 unstable mode, i.e. the mode exhibiting the largest growth rate. The range of unstable wavenumbers that  
 289 is created when the control parameter is above the critical value  $B_c$  degenerates into the single value  $k_c$  at  
 290 onset. To address this point, we track the variations in the  $(B, k)$  plane of the root of the characteristic  
 291 polynomial (3) associated to the most unstable mode, for different values of inertial times. Results are  
 292 shown in Fig.4, where the wavenumber of the mode exhibiting the largest growth rate is depicted by dashed  
 293 lines whereas the range of unstable wavenumbers is delimited by solid lines. When we move away from  
 294 the parabolic limit (from black to red curves in the figure), the role played by inertia becomes manifold: it  
 295 decreases the lowest value of the control parameter (plant loss) at which instability may form, it modifies the  
 296 wavenumber of the most unstable mode and also enlarges significantly the range of unstable wavenumbers.

297 Furthermore, by solving numerically the system defining theoretically the wave bifurcation locus (7),(8),  
 298 we can quantitatively estimate the wave speed  $s$  at the onset of instability as a function of inertial times.  
 299 From the analysis of the results depicted in Fig.5, we infer that the values of the inertial times affect directly  
 300 and indirectly through the variation of  $B_c$  the migrating speed at the onset of instability, as it varies from  
 301 about 0.8 (close to the parabolic limit) to 1.0 (away from it), i.e. hyperbolicity may increase the wave  
 302 speed up to 30%. To get a validation of these results, we integrate again numerically the governing system  
 303 (1),(2),(32) over a larger time window  $t \in [0, 200]$  and a larger spatial domain  $l_D = 200$ . We use the  
 304 parameter set corresponding to the points  $Q_1$  and  $Q_2$  depicted in Fig.5 and choose the control parameter  
 305  $B$  in such a way the distance from the threshold is  $\epsilon^2 = 10^{-3}$  in both cases. Then, in order to extract  
 306 the critical values of angular frequency  $\omega_c$  and wavenumber  $k_c$ , we perform two Fast-Fourier-Transforms  
 307 (FFTs) on the variable  $u(x, t)$ , by fixing either space or time. In detail, in the former case, the solution  
 308  $u(x, t)$  is evaluated at  $x = l_D/2$  while, in the latter case, it is set at  $t = t_{end}$ . According to the results  
 309 shown in Fig.6, each resulting spectrum contains several peaks, the dominant of which gives information  
 310 on the angular frequency  $\omega_c$  and the wavenumber  $k_c$  of the main mode, respectively. Finally, the migrating  
 311 speed value is simply given by the ratio  $s = \omega_c/k_c$ . Following this procedure, we get: for the point  $Q_1$ ,  
 312  $s = 0.301/0.376 = 0.801$ , in excellent agreement with the value extracted from system (7),(8), that is equal  
 313 to  $s = 0.807$ ; for the point  $Q_2$ , the value  $s = 0.380/0.410 = 0.926$ , in good agreement with the theoretical  
 314 value  $s = 0.923$ . These results reinforce our previous conclusion on the non-negligible role played by inertial  
 315 times: apart from affecting the migrating speed, they also alter both angular frequency and wavenumber of  
 316 the emerging pattern.

317 So far, we have validated all the theoretical predictions connected to LSA developed in Section 2.1. Let  
 318 us now focus on those arising from multiple-scale WNA whose general formulation has been given in Section  
 319 2.2. In the specific case of the hyperbolic extension of the Klausmeier model, the explicit expressions of the  
 320 quantities here involved are reported in Appendix B.

321 As known, the sign of the real part of the Landau coefficient determines the supercritical (if  $L_1 > 0$ ) or  
 322 subcritical (if  $L_1 < 0$ ) character of the generated patterns. Here, we aim at inspecting how such a character  
 323 could be altered by a suitable combination of inertial times. In Fig.7 we have addressed numerically this  
 324 investigation, by using the same set of parameters as those used to build Fig.5. In the figure, the colored

325 (white) areas denote a supercritical (subcritical) behavior. These results reveal that, for relatively small  
 326 values of the inertial times, namely close to the parabolic limit (bottom left corner of the figure), patterns  
 327 exhibit a supercritical behavior. For increasing values of inertial times, hyperbolicity may give rise to a  
 328 subcritical instability.

329 Let us now inspect whether these predictions may be corroborated by numerical simulations. First,  
 330 the supercritical character associated to the points  $Q_1$  and  $Q_2$  can be extracted from Fig.6, where patterns  
 331 slightly above threshold exhibit small amplitude, don't exist for sub-threshold values of the control parameter  
 332 and have a wavenumber very close to  $k_c$ . Indeed, the numerically-deduced values, i.e.  $k_c = 0.376$  in Fig.6(c)  
 333 and  $k_c = 0.410$  in Fig.6(f), are in close agreement with the theoretical ones deduced from (7),(8),(B.2),  
 334 i.e.  $k_c = 0.376$  and  $k_c = 0.403$ , respectively. To test whether a subcritical instability takes place at  $Q_3$ ,  
 335 we perform simulations where the initial condition is set, at first, as a small sinusoidal perturbation of the  
 336 steady state and the control parameter is slightly smaller than the critical value. Results indicate that the  
 337 initial perturbation simply dies out and the system converges towards the stable homogeneously vegetated  
 338 area, see Fig.8(a). Then, we increase the control parameter slightly above threshold and, as expected, large  
 339 amplitude patterns are generated, see Fig.8(b) (notice the larger scale in the color bar in comparison with  
 340 those of Fig.6(a),(d)). Finally, we take the final state of this latter simulation as the initial condition of a new

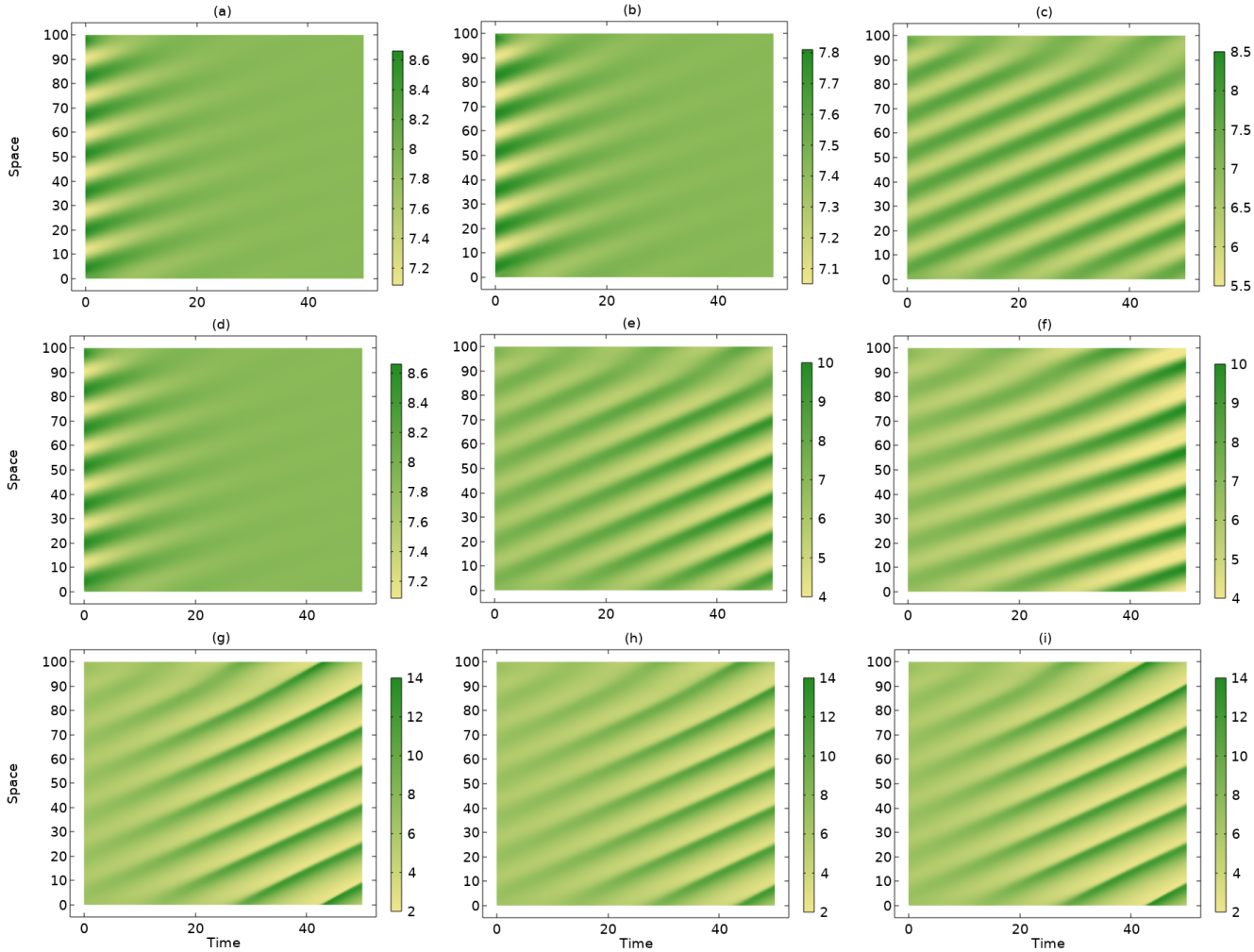


Figure 3: Spatio-temporal dynamics of vegetation biomass  $u(x, t)$  corresponding to the panels shown in Fig.2 obtained via numerical integration of system (1),(2),(32).

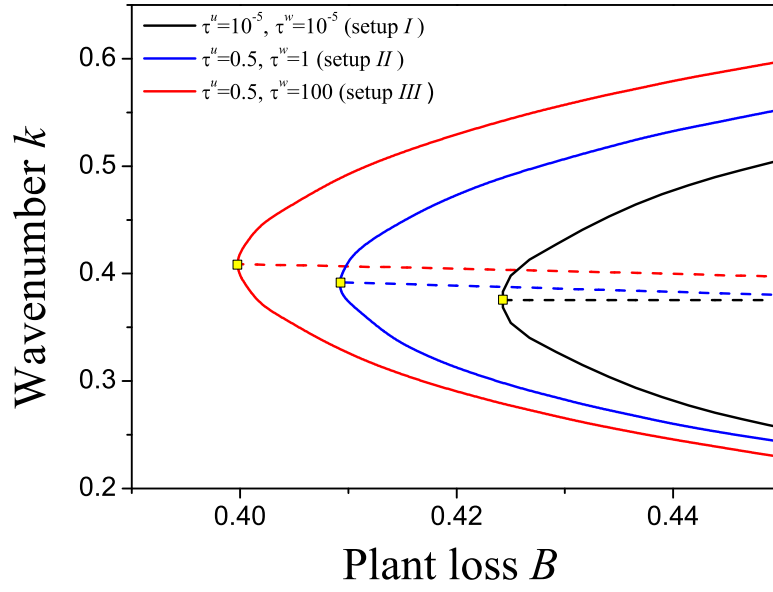


Figure 4: (Solid lines) Range of unstable wavenumbers as a function of the plant loss  $B$  for different values of inertial times. (Dashed lines) The wavenumber of the perturbation with the larger growth rate. (Squares) The lowest plant loss value  $B_c$  at which that steady state  $U_S^*$  undergoes wave instability and that identifies the critical wavenumber  $k_c$ .

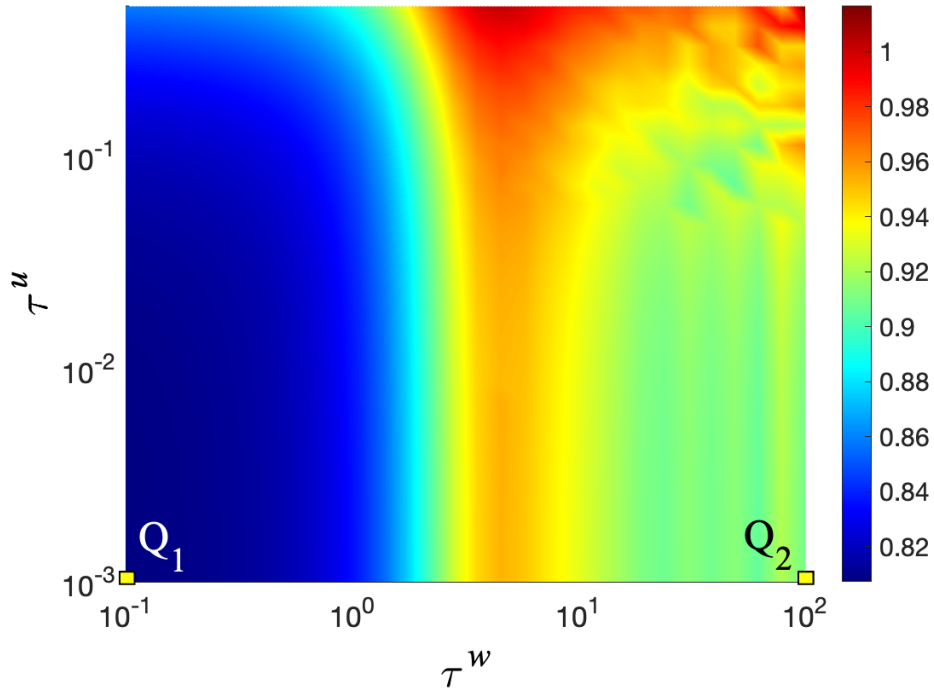


Figure 5: Density plot of migrating speed  $s$  at onset of instability ( $B = B_c$ ) as a function of the inertial times  $\tau^u$  and  $\tau^w$ . Fixed parameters:  $\nu = 182.5$ ,  $d = 100$ ,  $A = 2.8$ .

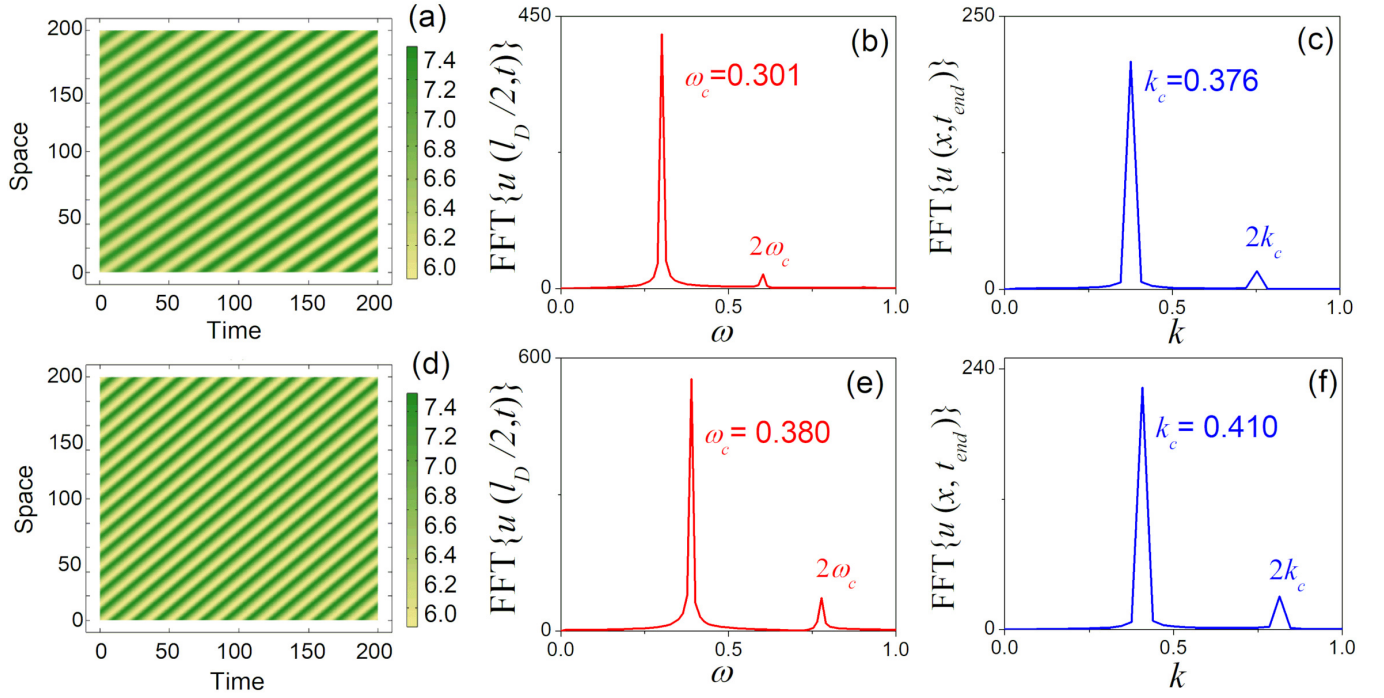


Figure 6: (a,d) Snapshots of migrating vegetation patterns. (b,e) FFT of the *time*-dependent solution evaluated at a fixed location within the domain,  $u(l_D/2, t)$ . (c,f) FFT of the *space*-dependent solution evaluated at the final simulation time,  $u(x, t_{end})$ . Panels in the top (bottom) row are obtained by using the parameter set corresponding to point  $Q_1$  ( $Q_2$ ) depicted in Fig.5. Note that the arising FFT spectra contain some higher-order harmonics (mainly, the component proportional to  $\exp(2ik_c z)$ ) due to the slow modulation of the pattern close to the onset [19].

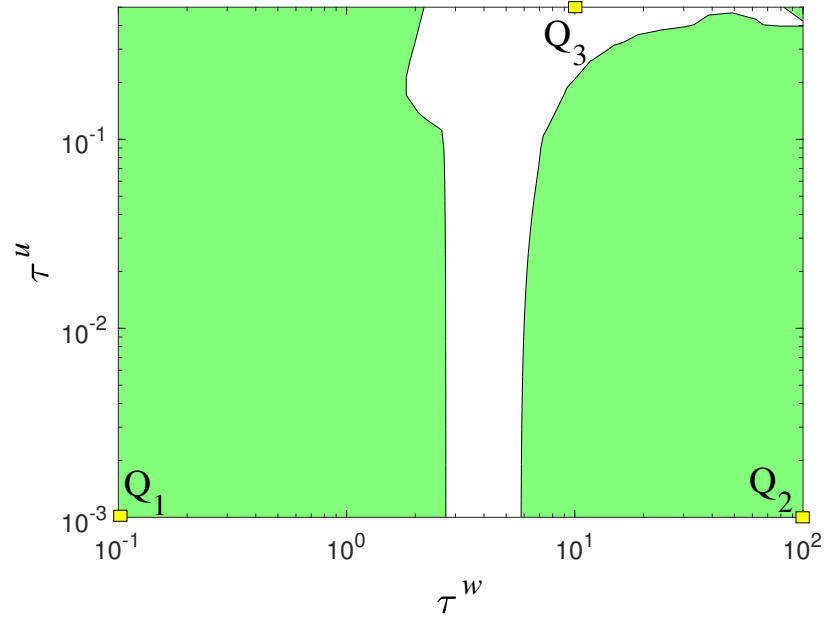


Figure 7: Contour plot of  $L_1$  as a function of the inertial times  $\tau^u$  and  $\tau^w$ . Colored (white) areas denote positive (negative) values of  $L_1$ . The parameter set is the same as the one reported in Fig.5.



341 simulation where the control parameter is set to the same below-threshold value as the one used to build  
 342 Fig.8(a). Interestingly, patterns still survive, so denoting the hysteretic behavior typical of a subcritical  
 343 instability.

344 Finally, we investigate on the one-parameter family of coherent structures, solutions of the CCGL equa-  
 345 tion, and address again a comparison between the analytical predictions reported in Section 2.2.1 and  
 346 numerical simulations . We shall limit the discussion to the supercritical regime by considering those re-  
 347 gions of the  $(\tau^w, \tau^u)$  plane where the real part of the Landau coefficient keeps positive (colored areas in  
 348 Fig.7). Then, we study the sign of the necessary condition for stability given by the Benjamin-Feir-Newell  
 349 criterion (31) and report the results in Fig.9. Here, the white (orange) color denotes an area where patterns  
 350 are unstable (may be stable). Our results indicate that, in a wide region enclosing the parabolic limit  
 351 (point  $Q_1$ ), i.e. for  $\tau^w < 2$  and independently of the value of  $\tau^u$ , the abovementioned criterion is always  
 352 satisfied and patterns may be stable. In this region, a slow modulation of travelling patterns is observed,  
 353 as shown in Fig.10(a). Far away from the parabolic limit, there exist values of inertial times that may  
 354 lead to destabilization of patterns, as it happens in the subregion of the  $(\tau^w, \tau^u)$  plane depicted in Fig.9.  
 355 Indeed, considering the inertial times corresponding to point  $Q_4$ , the wavetrain structure may break up into  
 356 a sequence of unequal pulses [5], as depicted in Fig.10(b).

357 Then, we inspect the role of inertial effects on phase winding solutions, i.e. on the fixed points  $\mathbf{F}_1^*$  and  
 358  $\mathbf{F}_2^*$  of system (24). In this analysis, we set the inertial times in such a way they correspond to points  $Q_1$  and  
 359  $Q_2$  and keep the dimensionless distance from the threshold fixed at  $\epsilon^2 = 10^{-2}$ . We integrate the governing  
 360 system (1),(2),(32) over a larger time window  $t \in [0, 1000]$  in order to allow transient regime to expire and  
 361 the system to reach a steady travelling patterned configuration. These are depicted in Figs.11(a),(b) by  
 362 solid lines. To determine the extra parameter involved in the phase-winding solution  $\tilde{\kappa}$ , we compare the  
 363 theoretical critical value  $k_c$  with the total wavenumber of the observed pattern  $k_{tot}$ . This value is then  
 364 used in (25),(28) to compute the amplitude  $\tilde{Q}$  and the second-order correction of the angular frequency  $\tilde{\omega}$ ,  
 365 respectively. Then, the corresponding analytical phase winding solutions are built via (26). Results are  
 366 represented in the previously mentioned figures via dashed lines and reveal a satisfying agreement with  
 367 those arising from numerical simulations. Moreover, we integrate system (24) to describe the heteroclinic  
 368 orbits joining the fixed points  $\mathbf{F}_1^*$  (unstable) and  $\mathbf{F}_2^*$  (stable) in the two configurations represented by the  
 369 points  $Q_1$  and  $Q_2$ . The initial condition is set as a small perturbation of  $\mathbf{F}_1^*$  in both cases. The resulting  
 370 fronts are depicted in Fig.11(c) and confirm that inertial effects take a relevant role, not only in modulating  
 371 the duration of the transient regime from the homogeneous steady state to the patterned state, but also in  
 372 modifying the amplitude, the wavenumber and the angular frequency of the traveling patterns.

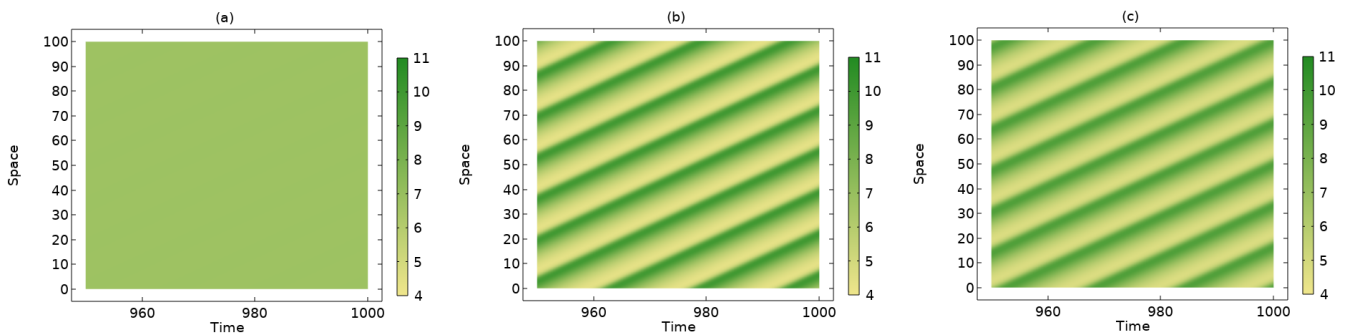


Figure 8: Snapshots of spatio-temporal evolution of vegetation biomass corresponding to the point  $Q_3$  shown in Fig.7 for (a)  $B = 0.403$ , (b)  $B = 0.405$  and (c)  $B = 0.403$ . The initial condition in simulations (a) and (b) is taken as a small periodic perturbation of the steady state  $\mathbf{U}_S^*$  whereas in (c) it is given by the final state of (b). The critical value of the control parameter is  $B_c = 0.404$ .



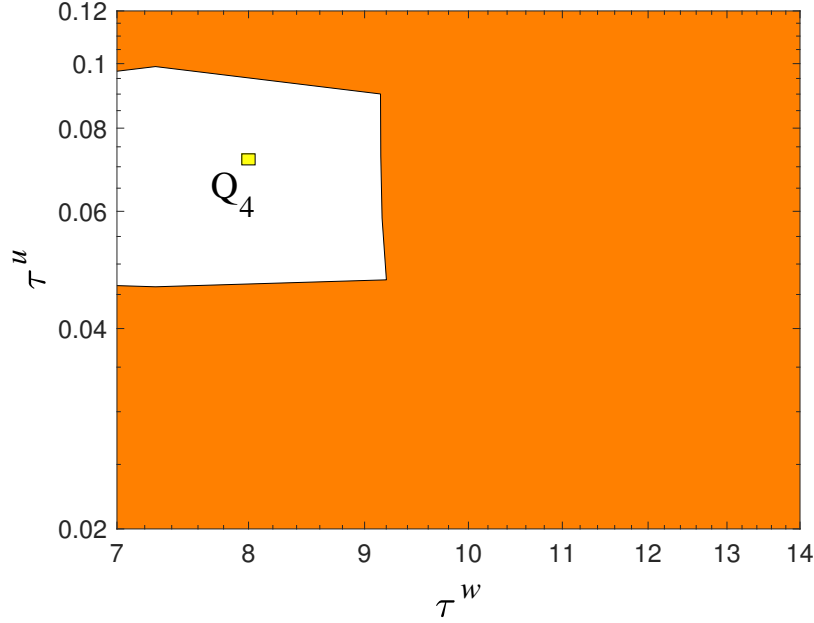


Figure 9: Plot of the Benjamin-Feir-Newell necessary condition for stability in the supercritical regime. Colored (white) areas denote regions where the condition (31) is (is not) fulfilled.

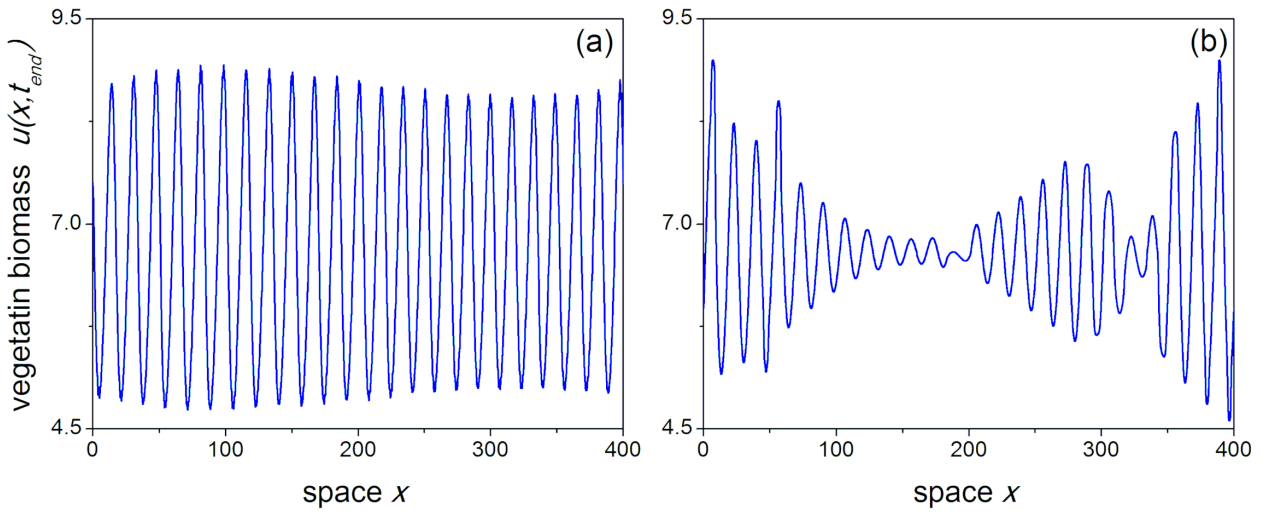


Figure 10: Proof of the Benjamin-Feir-Newell instability condition showing the spatial profiles of the patterned configurations obtained at points  $Q_1$  (a) and  $Q_4$  (b) represented in Fig.9(a). To improve the visibility of the wavetrain structure breaking, the computational domain has been enlarged to  $l_D=400$ .

## 373 4 Conclusions

374 In this manuscript, we have considered a class of hyperbolic reaction-advection-diffusion system for two  
 375 species, one of which undergoes both diffusion and advection while the other one has a diffusive character  
 376 only. The hyperbolic structure of the model accounts for the biological inertia of both the involved species  
 377 and allows a better description of transient phenomena characterized by waves evolving in space over a  
 378 finite time. On this general framework, we have carried out, first, linear stability analysis to deduce the

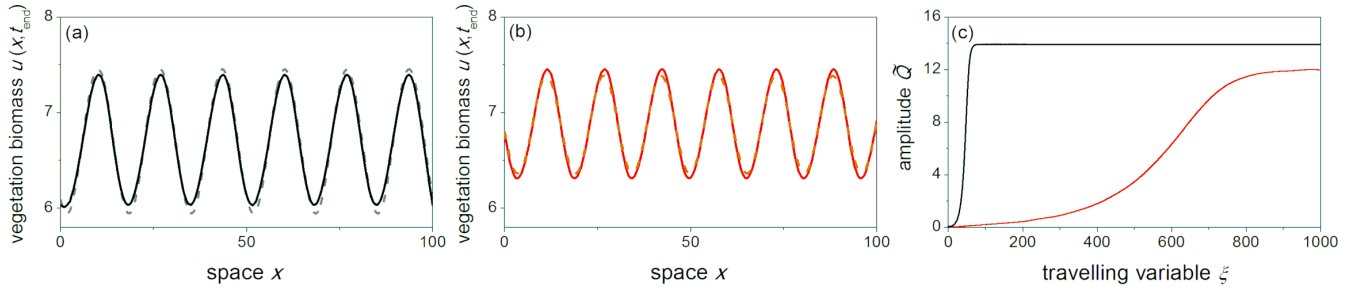


Figure 11: (a,b) Comparison between the numerical simulation arising from integration of the governing system (1),(2),(32) (solid lines) and the analytically-deduced phase winding solution  $\bar{\mathbf{U}} = \varepsilon \bar{\mathbf{U}}_1$  together with (20),(25)-(28) (dashed lines). The set of parameters correspond to the points  $Q_1$  (a) and  $Q_2$  (b) with  $\varepsilon^2 = 10^{-2}$ . (c) Results of numerical integration of system (24) representative of the heteroclinic orbits joining the fixed points  $\mathbf{F}_1^*$  and  $\mathbf{F}_2^*$  [black (red) curve stands for dynamics around point  $Q_1$  ( $Q_2$ )]. The initial condition is set as a small perturbation of  $\mathbf{F}_1^*$ .

379 conditions under which wave instability, responsible for the occurrence of non-stationary spatial patterns,  
 380 takes place. Then, by applying multiple-scale weakly nonlinear analysis we have determined the amplitude  
 381 equation describing the slow modulation in space and time near criticality.

382 All our theoretical findings enclose the parabolic limit as particular case, when the inertial times tend  
 383 to zero. In particular, it has been shown that the resulting CCGL equation is formally unchanged with  
 384 respect to the classical one obtained in parabolic framework, but the coefficients here involved exhibit a  
 385 strong dependence on inertial times.

386 Moreover, to better emphasize the role of hyperbolicity, we have also inspected coherent structures of  
 387 the CCGL equation whose fixed points are in the form of phase winding solutions. For this class of solutions  
 388 we have determined the expressions of the key features and established the necessary condition for stability.

389 The previous theoretical predictions have been tested on an illustrative example, the extended Klausmeier  
 390 model, describing the formation and the migration of vegetation patterns over a sloping semiarid terrain.  
 391 Numerical investigations have validated our findings and have allowed to draw several conclusions about the  
 392 role played by inertia. It has been indeed proven that inertial times:

- 393 i) enlarge both the wave instability region in the parameter plane where traveling patterns may be observed  
 394 and is less selective on the range of unstable wavenumbers. Thus, inertia allows to destabilize the  
 395 spatially homogeneous steady state over a wider set of model parameters (see Figs.1-4);
- 396 ii) vary the key features associated to migrating patterns, speed, wavelength and angular frequency, leaving  
 397 all the other model parameters unchanged (see Figs.5,6);
- 398 iii) affect the supercritical or subcritical nature of patterns at onset (see Figs.7,8);
- 399 iv) exert influence on localized coherent structures, and in particular on the fronts connecting the plane-  
 400 wave state to the unstable spatially-homogeneous steady state. In particular, it has been shown that  
 401 inertia takes a role, not only during transient regime, but also modifies the amplitude, the wavenumber,  
 402 the angular frequency and the stability of the phase winding solution associated to the plane wave  
 403 (see Figs.9,11).

404 In the light of the above statements, it has to be emphasized that hyperbolic models provide additional  
 405 degrees of freedom that can be used to better modeling experimental observations.

406 We plan to extend our hyperbolic framework to the case in which both species undergo diffusion and  
 407 advection, so enabling the possibility of exploring an even richer set of dynamics.

## 408 Acknowledgements

409 This research was funded by MIUR (Italian Ministry of University and Research) through project PRIN2017  
 410 no.2017YBKNCE, “Multiscale phenomena in Continuum Mechanics: singular limits, off-equilibrium and  
 411 transitions” and by INdAM-GNFM. Gabriele Grifó also acknowledges support from INdAM-GNFM through  
 412 “Progetto Giovani GNFM 2020” entitled “Analisi di biforcazione e teoremi di buona posizione in modelli  
 413 matematici multi-scala di interesse”.

## 414 Appendix A: Wave instability in parabolic reaction-advection- 415 diffusion models

416 In this Appendix we give some details on the occurrence of wave instability in *parabolic* reaction-advection-  
 417 diffusion models. In this framework, diffusion occurs through Fick’s laws,  $J^u = -u_x$  and  $J^w = -dw_x$ , and  
 418 the governing system is cast as:

$$\tilde{\mathbf{U}}_t + \tilde{M}\tilde{\mathbf{U}}_x + D\tilde{\mathbf{U}}_{xx} = \tilde{\mathbf{N}}(\tilde{\mathbf{U}}), \quad (\text{A.1})$$

419 with:

$$\tilde{\mathbf{U}} = \begin{bmatrix} u \\ w \end{bmatrix}, \quad \tilde{M} = \begin{bmatrix} 0 & 0 \\ 0 & -\nu \end{bmatrix}, \quad D = \begin{bmatrix} -1 & 0 \\ 0 & -d \end{bmatrix}, \quad \tilde{\mathbf{N}}(\tilde{\mathbf{U}}) = \begin{bmatrix} f(u, w) \\ g(u, w) \end{bmatrix}. \quad (\text{A.2})$$

420 The resulting spatially-homogeneous steady-states are denoted by  $\tilde{\mathbf{U}}^* = (u^*, v^*)$  and the dispersion relation  
 421 reduces to a quadratic equation:

$$\omega^2 + \left[ k^2(d+1) - (f_u^* + g_w^*) - ik\nu \right] \omega + \tilde{A}_0 + ik\nu\hat{b}_0 = 0 \quad (\text{A.3})$$

422 with  $\tilde{A}_0$  and  $\hat{b}_0$  given in (4). Conditions (6) for the stability of  $\tilde{\mathbf{U}}^*$  against homogeneous perturbations hold  
 423 for both hyperbolic and parabolic models.

424 By applying the same procedure as the one discussed in Section 2.1 in the hyperbolic framework, but  
 425 exploiting the lower complexity of the characteristic equation (A.3) with respect to (3), the locus of wave  
 426 instability can be defined implicitly via the following equation:

$$(4\chi_2^3 + 2\chi_0\chi_2 + \chi_1)(4\chi_2^3 + 2\chi_0\chi_2 - \chi_1) = 0 \quad (\text{A.4})$$

427 whereas the critical wavenumber is given by:

$$k_c^2 = -\frac{\chi_3}{\chi_4} \pm \chi_2 \quad (\text{A.5})$$

428 and the wave speed obeys:

$$s = \nu \left( f_u^* - k_c^2 \right) / \left[ k_c^2(d+1) - f_u^* - g_w^* \right]. \quad (\text{A.6})$$

429 The expressions of the coefficients  $\chi_i$  ( $i = 0, \dots, 4$ ) appearing in (A.4),(A.5) are given by:

$$\chi_0 = \frac{8\chi_4\chi_8 - 3\chi_3^2}{8\chi_4^2}, \quad \chi_1 = \frac{8\chi_4^2\chi_9 - 4\chi_4\chi_3\chi_8 + \chi_3^3}{8\chi_4^3}, \quad \chi_2 = \frac{1}{2} \sqrt{-\frac{2}{3}\chi_0 + \frac{1}{3\chi_4} \left( \chi_5 + \frac{\chi_6}{\chi_5} \right)}, \quad (\text{A.7})$$

$$\chi_3 = d\nu^2 - (d+1)^2 (g_w^* + df_u^*) - 2d(d+1) (f_u^* + g_w^*), \quad \chi_4 = d(d+1)^2$$

430 where

$$\begin{aligned}
\chi_5 &= \sqrt[3]{\frac{\chi_7 + \sqrt{\chi_7^2 - 4\chi_6^3}}{2}}, & \chi_6 &= 12\chi_4\chi_{10} - 3\chi_3\chi_9 + \chi_8^2, \\
\chi_7 &= 27\chi_4\chi_9^2 - 72\chi_4\chi_8\chi_{10} + 27\chi_3^2\chi_{10} - 9\chi_3\chi_8\chi_9 + 2\chi_8^3, \\
\chi_8 &= d(f_u^* + g_w^*)^2 + 2(d+1)(f_u^* + g_w^* - \nu^2)(g_w^* + df_u^*) + (d+1)^2(f_u^*g_w^* + f_w^*g_u^*), \\
\chi_9 &= \nu^2 f_u^*g_w^* - (g_w^* + df_u^*)(f_u^* + g_w^*)^2 - 2(d+1)(f_u^* + g_w^*)(f_u^*g_w^* + f_w^*g_u^*), \\
\chi_{10} &= (f_u^* + g_w^*)^2(f_u^*g_w^* + f_w^*g_u^*).
\end{aligned} \tag{A.8}$$

431 Note that, in the parabolic case, the critical value of the control parameter  $B_c$  is defined implicitly by  
432 the sole highly nonlinear equation (A.4), which results to be decoupled from the others. Moreover, the sign  
433 in (A.5) has to be chosen in such a way it gives real and positive values for  $B_c$  and  $k_c$ .

## 434 Appendix B: Derivation of Cubic Complex Ginzburg-Landau 435 equation

436 In this Appendix we fully describe the procedure to deduce the CCGL equation (22) for the hyperbolic  
437 reaction-advection-diffusion model (1)-(2).

438 First of all, substituting the expansion (14) into the governing system (9) and looking for solution  
439  $\bar{\mathbf{U}}_i = \bar{\mathbf{U}}_i(z)$  with  $z = x - st$ , the set of ordinary differential equations (16)-(18), to be solved sequentially, is  
440 obtained. At the first perturbative order, the system reads:

$$\frac{d\bar{\mathbf{U}}_1}{dz} = K_c^* \bar{\mathbf{U}}_1 \tag{B.1}$$

441 where the matrix  $K_c^*$ , defined in (19), admits four complex eigenvalues given by

$$\lambda_{1,2} = \mp i k_c \quad \text{with} \quad k_c^2 = \frac{\delta_3}{\delta_1} \Big|_c \tag{B.2}$$

442 and

$$\lambda_{3,4} = \alpha \mp i\beta \quad \text{with} \quad \alpha = -\frac{\delta_1}{2} \Big|_c \quad \text{and} \quad \beta = \sqrt{\left(\frac{\delta_1\delta_4}{\delta_3} - \frac{\delta_1^2}{4}\right)} \Big|_c \tag{B.3}$$

443 to which there correspond the following right eigenvectors

$$\mathbf{d}^{(\pm i k_c)} = \begin{bmatrix} r_1 \pm i \hat{r}_1 \\ r_2 \pm i \hat{r}_2 \\ r_3 \pm i \hat{r}_3 \\ r_4 \pm i \hat{r}_4 \end{bmatrix}, \quad \mathbf{d}^{(\alpha \pm i\beta)} = \begin{bmatrix} y_1 \pm i \hat{y}_1 \\ y_2 \pm i \hat{y}_2 \\ y_3 \pm i \hat{y}_3 \\ y_4 \pm i \hat{y}_4 \end{bmatrix}. \tag{B.4}$$

444 The general solution of the homogeneous linear system (B.1) can be expressed as:

$$\mathbf{U}_1 = P e^{Qz} P^{-1} \mathbf{C}(T_2) \tag{B.5}$$

445 where the vector  $\mathbf{C}(T_2)$  is determined by boundary conditions, whereas  $P$  and  $Q$  are, respectively, the  
446 eigenvectors and eigenvalues matrices of  $K_c^*$  given by

$$P = \begin{bmatrix} r_1 + i \hat{r}_1 & r_1 - i \hat{r}_1 & y_1 + i \hat{y}_1 & y_1 - i \hat{y}_1 \\ r_2 + i \hat{r}_2 & r_2 - i \hat{r}_2 & y_2 + i \hat{y}_2 & y_2 - i \hat{y}_2 \\ r_3 + i \hat{r}_3 & r_3 - i \hat{r}_3 & y_3 + i \hat{y}_3 & y_3 - i \hat{y}_3 \\ r_4 + i \hat{r}_4 & r_4 - i \hat{r}_4 & y_4 + i \hat{y}_4 & y_4 - i \hat{y}_4 \end{bmatrix}, \quad Q = \begin{bmatrix} i k_c & 0 & 0 & 0 \\ 0 & -i k_c & 0 & 0 \\ 0 & 0 & \alpha + i\beta & 0 \\ 0 & 0 & 0 & \alpha - i\beta \end{bmatrix}. \tag{B.6}$$

447 Then, solution of (B.1) reads:

$$\bar{\mathbf{U}}_1 = \Omega(X, T_2) e^{ik_c z} \mathbf{d}^{(ik_c)} + \bar{\Omega}(X, T_2) e^{-ik_c z} \mathbf{d}^{(-ik_c)} \quad (\text{B.7})$$

448 where the complex pattern amplitude  $\Omega$  remains undetermined at this stage and  $\bar{\Omega}$  denotes its complex  
449 conjugate.

450 At the second order, the governing system is the following:

$$\frac{d\bar{\mathbf{U}}_2}{dz} - K_c^* \bar{\mathbf{U}}_2 = (M - sI)^{-1} \left\{ \frac{1}{2} (\bar{\mathbf{U}}_1 \cdot \nabla)^{(2)} \mathbf{N}|_c^* - M \frac{\partial \bar{\mathbf{U}}_1}{\partial X} \right\} \quad (\text{B.8})$$

451 whose general solution is given by

$$\mathbf{U}_2 = P e^{Qz} P^{-1} \mathbf{C}(T_2) + P e^{Qz} \int e^{-Qz} (MP)^{-1} \mathbf{F} dz \quad (\text{B.9})$$

452 where  $\mathbf{F}$  is the non-homogeneous term at the right-hand side of (B.8).

453 Now, taking into account (B.9) and inserting (B.7) into the non-homogeneous linear system (B.8), the  
454 solution at the second perturbative order satisfying periodic boundary conditions reads:

$$\bar{\mathbf{U}}_2 = \frac{\partial \Omega}{\partial X} e^{ik_c z} \mathbf{g} + \frac{\partial \bar{\Omega}}{\partial X} e^{-ik_c z} \bar{\mathbf{g}} + \Omega^2 e^{2ik_c z} \mathbf{q} + \bar{\Omega}^2 e^{-2ik_c z} \bar{\mathbf{q}} + 2\mathbf{q}_0 |\Omega|^2 \quad (\text{B.10})$$

455 where the vectors:

$$\mathbf{g} = \begin{bmatrix} g_1 + i\hat{g}_1 \\ g_2 + i\hat{g}_2 \\ g_3 + i\hat{g}_3 \\ g_4 + i\hat{g}_4 \end{bmatrix}, \quad \mathbf{q} = \begin{bmatrix} q_1 + i\hat{q}_1 \\ q_2 + i\hat{q}_2 \\ q_3 + i\hat{q}_3 \\ q_4 + i\hat{q}_4 \end{bmatrix}, \quad \mathbf{q}_0 = \begin{bmatrix} q_{01} \\ q_{02} \\ 0 \\ 0 \end{bmatrix} \quad (\text{B.11})$$

456 fulfill the linear systems:

$$\begin{aligned} [L_c^* - ik_c(M - sI)] \mathbf{g} &= M \mathbf{d}^{(ik_c)} \\ [L_c^* - 2ik_c(M - sI)] \mathbf{q} &= -\frac{1}{2} (\mathbf{d}^{(ik_c)} \cdot \nabla)^{(2)} \mathbf{N}|_c^* \\ L_c^* \mathbf{q}_0 &= -\frac{1}{2} (\mathbf{d}^{(ik_c)} \cdot \nabla) (\mathbf{d}^{(-ik_c)} \cdot \nabla) \mathbf{N}|_c^* \end{aligned} \quad (\text{B.12})$$

457 with

$$\begin{aligned} \mathbf{l} M \mathbf{d}^{(ik_c)} &= \mathbf{0}, \\ \mathbf{l} [L_c^* - ik_c(M - sI)] &= \mathbf{0}, \end{aligned} \quad (\text{B.13})$$

458 whereas  $\bar{\mathbf{g}}$  and  $\bar{\mathbf{q}}$  are the complex conjugate of  $\mathbf{g}$  and  $\mathbf{q}$ , respectively.

459 Finally, by substituting (B.7) and (B.10) into (18), from the removal of secular terms, we deduce that  
460 the pattern amplitude  $\Omega(X, T_2)$  satisfies the CCGL equation:

$$\frac{\partial \Omega}{\partial T_2} = (\rho_1 + i\rho_2) \frac{\partial^2 \Omega}{\partial X^2} + (\sigma_1 + i\sigma_2) \Omega - (L_1 - iL_2) \Omega |\Omega|^2 \quad (\text{B.14})$$

461 where:

$$\begin{aligned} \rho_1 + i\rho_2 &= [(n_1 e_1 + n_2 e_2) + i(n_2 e_1 - n_1 e_2)] / (e_1^2 + e_2^2) \\ \sigma_1 + i\sigma_2 &= B_2 [(m_1 e_1 + m_2 e_2) + i(m_2 e_1 - m_1 e_2)] / (e_1^2 + e_2^2) \\ L_1 - iL_2 &= (p_1 - ip_2) / (e_1^2 + e_2^2) \end{aligned} \quad (\text{B.15})$$

462 with:

$$\begin{aligned}
n_1 &= [(g_4 - \nu g_2) f_u^* - g_3 g_u^*] E_{1r} + [(g_4 - \nu g_2) f_w^* - g_3 g_w^*] E_{2r} + (f_u^* g_w^* - f_w^* g_u^*) (dg_2 E_{4r} - g_1 E_{3r}), \\
n_2 &= [(g_4 - \nu g_2) f_u^* - g_3 g_u^*] E_{1i} + [(g_4 - \nu g_2) f_w^* - g_3 g_w^*] E_{2i} + (f_u^* g_w^* - f_w^* g_u^*) (dg_2 E_{4i} - g_1 E_{3i}), \\
m_1 &= -(s_1 r_1 + s_2 r_2) (E_{1r} f_u^* + E_{2r} f_w^*) + (s_1 \hat{r}_1 + s_2 \hat{r}_2) (E_{1i} f_u^* + E_{2i} f_w^*) + \\
&\quad + (h_1 r_1 + h_2 r_2) (E_{1r} g_u^* + E_{2r} g_w^*) - (h_1 \hat{r}_1 + h_2 \hat{r}_2) (E_{1i} g_u^* + E_{2i} g_w^*), \\
m_2 &= -(s_1 r_1 + s_2 r_2) (E_{1i} f_u^* + E_{2i} f_w^*) - (s_1 \hat{r}_1 + s_2 \hat{r}_2) (E_{1r} f_u^* + E_{2r} f_w^*) + \\
&\quad + (h_1 r_1 + h_2 r_2) (E_{1i} g_u^* + E_{2i} g_w^*) + (h_1 \hat{r}_1 + h_2 \hat{r}_2) (E_{1r} g_u^* + E_{2r} g_w^*), \\
p_1 &= (b_1 f_u^* - a_1 g_u^*) (E_{1r} e_1 + E_{1i} e_2) - (b_2 f_u^* - a_2 g_u^*) (E_{1i} e_1 - E_{1r} e_2) + \\
&\quad + (b_1 f_w^* - a_1 g_w^*) (E_{2r} e_1 + E_{2i} e_2) - (b_2 f_w^* - a_2 g_w^*) (E_{2i} e_1 - E_{2r} e_2), \\
p_2 &= (b_1 f_u^* - a_1 g_u^*) (E_{1i} e_1 - E_{1r} e_2) - (b_2 f_u^* - a_2 g_u^*) (E_{1r} e_1 + E_{1i} e_2) + \\
&\quad + (b_1 f_w^* - a_1 g_w^*) (E_{2i} e_1 - E_{2r} e_2) - (b_2 f_w^* - a_2 g_w^*) (E_{2r} e_1 + E_{2i} e_2), \\
e_1 &= (r_1 g_u^* - r_2 f_u^*) E_{1r} - (\hat{r}_1 g_u^* - \hat{r}_2 f_u^*) E_{1i} + (r_1 g_w^* - r_2 f_w^*) E_{2r} - (\hat{r}_1 g_w^* - \hat{r}_2 f_w^*) E_{2i} + \\
&\quad + (f_u^* g_w^* - f_w^* g_u^*) (\tau^u r_3 E_{3r} - \tau^w r_4 E_{4r} - \tau^u \hat{r}_3 E_{3i} + \tau^w \hat{r}_4 E_{4i}), \\
e_2 &= (r_1 g_u^* - r_2 f_u^*) E_{1i} + (\hat{r}_1 g_u^* - \hat{r}_2 f_u^*) E_{1r} + (r_1 g_w^* - r_2 f_w^*) E_{2i} + (\hat{r}_1 g_w^* - \hat{r}_2 f_w^*) E_{2r} + \\
&\quad + (f_u^* g_w^* - f_w^* g_u^*) (\tau^u r_3 E_{3i} - \tau^w r_4 E_{4i} + \tau^u \hat{r}_3 E_{3r} - \tau^w \hat{r}_4 E_{4r}), \\
E_{1r} + i E_{1i} &= \hat{r}_4 (y_1 \hat{y}_3 - y_3 \hat{y}_1) + \hat{r}_3 (y_4 \hat{y}_1 - y_1 \hat{y}_4) + \hat{r}_1 (y_3 \hat{y}_4 - y_4 \hat{y}_3) + \\
&\quad i [r_4 (y_1 \hat{y}_3 - y_3 \hat{y}_1) + r_3 (y_4 \hat{y}_1 - y_1 \hat{y}_4) + r_1 (y_3 \hat{y}_4 - y_4 \hat{y}_3)], \\
E_{2r} + i E_{2i} &= \hat{r}_4 (y_2 \hat{y}_3 - y_3 \hat{y}_2) + \hat{r}_3 (y_4 \hat{y}_2 - y_2 \hat{y}_4) + \hat{r}_2 (y_3 \hat{y}_4 - y_4 \hat{y}_3) + \\
&\quad i [r_4 (y_2 \hat{y}_3 - y_3 \hat{y}_2) + r_3 (y_4 \hat{y}_2 - y_2 \hat{y}_4) + r_2 (y_3 \hat{y}_4 - y_4 \hat{y}_3)], \\
E_{3r} + i E_{3i} &= \hat{r}_4 (y_2 \hat{y}_1 - y_1 \hat{y}_2) + \hat{r}_2 (y_1 \hat{y}_4 - y_4 \hat{y}_1) + \hat{r}_1 (y_4 \hat{y}_2 - y_2 \hat{y}_4) + \\
&\quad i [r_4 (y_2 \hat{y}_1 - y_1 \hat{y}_2) + r_2 (y_1 \hat{y}_4 - y_4 \hat{y}_1) + r_1 (y_4 \hat{y}_2 - y_2 \hat{y}_4)], \\
E_{4r} + i E_{4i} &= \hat{r}_3 (y_2 \hat{y}_1 - y_1 \hat{y}_2) + \hat{r}_2 (y_1 \hat{y}_3 - y_3 \hat{y}_1) + \hat{r}_1 (y_3 \hat{y}_2 - y_2 \hat{y}_3) + \\
&\quad i [r_3 (y_2 \hat{y}_1 - y_1 \hat{y}_2) + r_2 (y_1 \hat{y}_3 - y_3 \hat{y}_1) + r_1 (y_3 \hat{y}_2 - y_2 \hat{y}_3)],
\end{aligned} \tag{B.16}$$

$$h_1 = \left. \frac{df_u}{dB} \right|_c^*, \quad h_2 = \left. \frac{df_w}{dB} \right|_c^*, \quad s_1 = \left. \frac{dg_u}{dB} \right|_c^*, \quad s_2 = \left. \frac{dg_w}{dB} \right|_c^*$$

463 and

$$\begin{aligned}
a_1 + i a_2 = & f_{uu}|_c^* \left\{ r_1(2q_{01} + q_1) + \widehat{r}_1 \widehat{q}_1 + i [\widehat{r}_1(2q_{01} - q_1) + r_1 \widehat{q}_1] \right\} + \\
& f_{uw}|_c^* \left\{ r_1(2q_{02} + q_2) + \widehat{r}_1 \widehat{q}_2 + r_2(2q_{01} + q_1) + \widehat{r}_2 \widehat{q}_1 + \right. \\
& \left. i [\widehat{r}_1(2q_{02} - q_2) + r_1 \widehat{q}_2 + \widehat{r}_2(2q_{01} - q_1) + r_2 \widehat{q}_1] \right\} + \\
& f_{ww}|_c^* \left\{ r_2(2q_{02} + q_2) + \widehat{r}_2 \widehat{q}_2 + i [\widehat{r}_2(2q_{02} - q_2) + r_2 \widehat{q}_2] \right\} + \\
& \frac{1}{2} f_{uuu}|_c^* (r_1^2 + \widehat{r}_1^2) (r_1 + i \widehat{r}_1) + \frac{1}{2} f_{www}|_c^* (r_2^2 + \widehat{r}_2^2) (r_2 + i \widehat{r}_2) + \\
& \frac{1}{2} f_{uww}|_c^* \left\{ 2r_1 \widehat{r}_1 \widehat{r}_2 + r_2(3r_1^2 + \widehat{r}_1^2) + i [2r_1 \widehat{r}_1 r_2 + \widehat{r}_2(r_1^2 + 3\widehat{r}_1^2)] \right\} + \\
& \frac{1}{2} f_{uwu}|_c^* \left\{ 2r_2 \widehat{r}_1 \widehat{r}_2 + r_1(3r_2^2 + \widehat{r}_2^2) + i [2r_1 \widehat{r}_1 r_2 + \widehat{r}_1(r_2^2 + 3\widehat{r}_2^2)] \right\},
\end{aligned} \tag{B.17}$$

$$\begin{aligned}
b_1 + i b_2 = & g_{uu}|_c^* \left\{ r_1(2q_{01} + q_1) + \widehat{r}_1 \widehat{q}_1 + i [\widehat{r}_1(2q_{01} - q_1) + r_1 \widehat{q}_1] \right\} + \\
& g_{uw}|_c^* \left\{ r_1(2q_{02} + q_2) + \widehat{r}_1 \widehat{q}_2 + r_2(2q_{01} + q_1) + \widehat{r}_2 \widehat{q}_1 + \right. \\
& \left. i [\widehat{r}_1(2q_{02} - q_2) + r_1 \widehat{q}_2 + \widehat{r}_2(2q_{01} - q_1) + r_2 \widehat{q}_1] \right\} + \\
& g_{ww}|_c^* \left\{ r_2(2q_{02} + q_2) + \widehat{r}_2 \widehat{q}_2 + i [\widehat{r}_2(2q_{02} - q_2) + r_2 \widehat{q}_2] \right\} + \\
& \frac{1}{2} g_{uuu}|_c^* (r_1^2 + \widehat{r}_1^2) (r_1 + i \widehat{r}_1) + \frac{1}{2} (g_{www})|_c^* (r_2^2 + \widehat{r}_2^2) (r_2 + i \widehat{r}_2) + \\
& \frac{1}{2} g_{uww}|_c^* \left\{ 2r_1 \widehat{r}_1 \widehat{r}_2 + r_2(3r_1^2 + \widehat{r}_1^2) + i [2r_1 \widehat{r}_1 r_2 + \widehat{r}_2(r_1^2 + 3\widehat{r}_1^2)] \right\} + \\
& \frac{1}{2} g_{uwu}|_c^* \left\{ 2r_2 \widehat{r}_1 \widehat{r}_2 + r_1(3r_2^2 + \widehat{r}_2^2) + i [2r_1 \widehat{r}_1 r_2 + \widehat{r}_1(r_2^2 + 3\widehat{r}_2^2)] \right\}.
\end{aligned}$$

464 In the particular case of the hyperbolic extension of the Klausmeier model, taking into account

$$\begin{aligned}
f_u^* &= B, & f_w^* &= u_S^2, & g_u^* &= -2B, & g_w^* &= -(1 + u_S^2), \\
f_{uu}^* &= 2B/u_S, & f_{uw}^* &= 2u_S, & f_{ww}^* &= 0, \\
g_{uu}^* &= -2B/u_S, & g_{uw}^* &= -2u_S, & g_{ww}^* &= 0, \\
f_{uuu}^* &= f_{uww}^* = f_{wuw}^* = 0, & f_{uuw}^* &= 2, \\
g_{uuu}^* &= g_{uww}^* = g_{wuw}^* = 0, & g_{uuw}^* &= -2,
\end{aligned} \tag{B.18}$$

465 the components of the right eigenvectors  $\mathbf{d}^{(\pm i k_c)}$  and  $\mathbf{d}^{(\alpha \pm i \beta)}$  reported in (B.4) become:

$$\begin{aligned}
r_1 &= 1, & \hat{r}_1 &= 0, \\
r_2 &= \frac{k_c^2 - B_c - (\tau^u)^2 k_c^2 s^2 B_c}{u_{S_c}^2 [k_c^2 s^2 (\tau^u)^2 + 1]}, & \hat{r}_2 &= -\frac{k_c s [1 + k_c^2 \tau^u (\tau^u s^2 - 1)]}{u_{S_c}^2 [k_c^2 s^2 (\tau^u)^2 + 1]}, \\
r_3 &= \frac{k_c^2 s \tau^u}{k_c^2 s^2 (\tau^u)^2 + 1}, & \hat{r}_3 &= -\frac{k_c}{k_c^2 s^2 (\tau^u)^2 + 1}, \\
r_4 &= \frac{k_c d (\hat{r}_2 + k_c s r_2 \tau^w)}{1 + (\tau^w)^2 k_c^2 s^2}, & \hat{r}_4 &= \frac{k_c d (-r_2 + k_c s \hat{r}_2 \tau^w)}{1 + (\tau^w)^2 k_c^2 s^2}, \\
y_1 &= 1, & \hat{y}_1 &= 0, \\
y_2 &= \frac{(\alpha s \tau^u - 1) l_1 + \beta s \tau^u l_2}{u_{S_c}^2 [(\alpha s \tau^u - 1)^2 + \beta^2 s^2 (\tau^u)^2]}, & \hat{y}_2 &= \frac{(\alpha s \tau^u - 1) l_2 - \beta s \tau^u l_1}{u_{S_c}^2 [(\alpha s \tau^u - 1)^2 + \beta^2 s^2 (\tau^u)^2]}, \\
y_3 &= \frac{\alpha (\alpha s \tau^u - 1) + \beta^2 s \tau^u}{(\alpha s \tau^u - 1)^2 + \beta^2 s^2 (\tau^u)^2}, & \hat{y}_3 &= -\frac{\beta}{(\alpha s \tau^u - 1)^2 + \beta^2 s^2 (\tau^u)^2}, \\
y_4 &= \frac{d [(\alpha y_2 - \beta \hat{y}_2) (\alpha s \tau^w - 1) + \beta s \tau^w (\beta y_2 + \alpha \hat{y}_2)]}{(\tau^w \alpha s - 1)^2 + \beta^2 s^2 (\tau^w)^2}, & \hat{y}_4 &= \frac{d [(\beta y_2 + \alpha \hat{y}_2) (\alpha s \tau^w - 1) + \beta s \tau^w (\beta \hat{y}_2 - \alpha y_2)]}{(\tau^w \alpha s - 1)^2 + \beta^2 s^2 (\tau^w)^2},
\end{aligned} \tag{B.19}$$

466 where

$$l_1 = (\alpha^2 - \beta^2) (1 - s^2 \tau^u) + \alpha s (1 - B_c \tau^u) + B_c, \quad l_2 = 2\alpha\beta (1 - s^2 \tau^u) + \beta s (1 - \tau^u B_c). \tag{B.20}$$

467 Moreover, the coefficients occurring in (B.17) reduce to:

$$\begin{aligned}
a_1 + i a_2 &= 2B_c / u_{S_c} [r_1 (2q_{01} + q_1) + \hat{r}_1 \hat{q}_1] + 2r_1 \hat{r}_1 \hat{r}_2 + r_2 (3r_1^2 + \hat{r}_1^2) + \\
&\quad + 2u_{S_c} [r_1 (2q_{02} + q_2) + \hat{r}_1 \hat{q}_2 + r_2 (2q_{01} + q_1) + \hat{r}_2 \hat{q}_1] + \\
&\quad + i \left\{ 2B_c / u_{S_c} [\hat{r}_1 (2q_{01} - q_1) + r_1 \hat{q}_1] + 2r_1 \hat{r}_1 r_2 + \hat{r}_2 (r_1^2 + 3\hat{r}_1^2) + \right. \\
&\quad \left. + 2u_{S_c} [\hat{r}_1 (2q_{02} - q_2) + r_1 \hat{q}_2 + \hat{r}_2 (2q_{01} - q_1) + r_2 \hat{q}_1] \right\}, \\
b_1 + i b_2 &= -(a_1 + i a_2).
\end{aligned} \tag{B.21}$$

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