

# Interdigitated back-contacted crystalline silicon solar cells fully manufactured with atomic layer deposited selective contacts

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## ABSTRACT

The interdigitated back-contacted (IBC) solar cell concept has been extensively studied for single-junction cells and more recently as a good choice for three-terminal tandem devices. In this work, carrier-selective contacts based on transition metal oxides deposited by atomic layer deposition (ALD) technique are applied to IBC c-Si(n) devices. In the first part of the study, we develop a hole-selective contact based on thin ALD vanadium oxide ( $V_2O_5$ ) layers without using an amorphous silicon interlayer. The ALD process has been optimised, i.e. number of ALD cycles and deposition temperature, as a trade-off between surface passivation and contact resistivity. Noticeable surface passivation with recombination current densities around  $100 \text{ fA/cm}^2$ , as well as reasonable contact resistivity values below  $250 \text{ m}\Omega\text{cm}^2$  are reached using 200 ALD  $V_2O_5$  cycles deposited at a deposition temperature of  $125 \text{ }^\circ\text{C}$  ( $\sim 10 \text{ nm}$  layer thickness). The optimised ALD  $V_2O_5$ -based contact is combined with both an ALD  $TiO_2$ -based electron-selective contact and an excellent surface passivation in non-contacted regions provided by ALD  $Al_2O_3$  films, to form a fully ALD IBC c-Si(n) solar cell scheme. Fabricated devices yield photovoltaic efficiencies and pseudo efficiencies, i.e. calculated without series resistance losses, of 18.6% and 21.1% respectively ( $3 \text{ cm} \times 3 \text{ cm}$  device area). These results reveal the potential of the ALD technique to deposit transition metal oxide (TMO) films as selective contacts on high efficiency devices, paving the way of using low thermal-budget, low cost and highly scalable processes for a highly demanding IBC solar cell architecture in the photovoltaic industry.

## 1. Introduction

The photovoltaic market is dominated by crystalline silicon (c-Si) solar cells [1]. The charge-carrier selectivity at the contacts of these devices is mainly achieved by phosphorous and boron diffusion species inside the c-Si substrate, the so-called pn junction. Another way to obtain contact selectivity, i.e. a good balance between resistance and passivated contact properties, is the use of a heterojunction structure (SHJ), in which doped hydrogenated amorphous silicon (a-Si:H) films act as selective contacts. In fact, the highest energy conversion efficiency is achieved with SHJ-based contacts with an efficiency of 26.7% [2]. Moreover, this record cell efficiency is accomplished by using an interdigitated back-contacted (IBC) scheme. In IBC cells both contacts, the electron (ETL) and the hole (HTL) transport layers, are placed on the back of the device. Thus, the front surface is free from metal pads and a-Si:H films, which cause losses due to shadowing [3] and parasitic

optical absorption [4], respectively. By doing so, light absorption in the c-Si substrate increases and consequently, the cell photocurrent and conversion efficiency are enhanced.

Recently, IBC solar cells have been proposed as the bottom cell of a three-terminal tandem device [5]. The main challenge of a monolithic two-terminal tandem structure is the current matching between the lower and upper cell. However, with an IBC bottom cell, a three-terminal tandem architecture is feasible, where the two generated photocurrents can be extracted separately, maximising the efficiency of both cells [6]. This concept broadens the interest of IBC cells, not only for their initial use, which was focused on concentrating solar applications, but also for emerging tandem architectures [7].

In laboratory and industrial solar cells, high conversion efficiency is usually achieved using pn-based or a-Si:H junctions. However, interesting approaches have been studied in the past to find alternatives that avoid the use of high temperature steps or flammable gaseous

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precursors, involved in these technologies. In this way, transition metal oxides (TMOs) [8], such as vanadium ( $V_2O_5$ ) [9], molybdenum ( $MoO_x$ ) [10], titanium ( $TiO_x$ ) [11] or magnesium ( $MgO_x$ ) [12] oxides, are promising candidates. TMOs have a wide range of work function values, which allow either an alignment of energy levels between the absorber and the metal electrode or the introduction of a highly inverted/accumulated region under the silicon-contact interface, improving in both cases the contact selectivity [13]. In addition, their wide bandgap ( $>3$  eV) makes them transparent [9], minimising parasitic optical absorption, as well as suitable antireflection or back-reflector contact materials. Benefits of TMOs applied to c-Si solar cells and in particular to an IBC structure are systemically studied and evaluated in the literature, see for instance Refs. [14–16]. Table 1 summarises the main reported contributions elsewhere using an IBC cell structure and TMO-based contacts highlighting their deposition technology.

TMOs described in the literature are usually deposited by thermal evaporation technique, which does not provide a simple scalable route for the photovoltaic industry. With this issue in mind, the atomic layer deposition (ALD) technique has sparked interest in TMO deposition [17–21], not only because of the excellent control of film growth and uniformity in large-area devices, but also because of the possibility of reasonable film deposition rates. Although the standard laboratory ALD process exhibits a slow deposition rate, it has already been reported that the spatial ALD technique, which is an ALD system with its reactors spatially separated [22], is capable of depositing alumina ( $Al_2O_3$ ) films at rates as high as 1.2 nm/s providing at the same time excellent surface passivation [23]. Another promising example is the use of spatial ALD to deposit  $MoO_x$  films as HTL at rates of 5.4 nm/min [17].

Finally, the ALD  $V_2O_5$  films have recently been published as a hole-selective contact in c-Si solar cells [18]. Although careful characterisations have been performed in the aforementioned work, such as passivation properties on p- and n-type c-Si substrates, the contact resistivity is only reported for p-type wafers. Moreover, the  $V_2O_5$ -based contact implemented in the solar cell is performed with the help of an intrinsic a-Si:H interlayer. In a recent work, we also reported the use of ALD  $V_2O_5$  films for c-Si(n) solar cells [24], in which the ALD  $V_2O_5$  film was placed on the front side together with an indium tin oxide (ITO) layer. Nonetheless, a conventional vertical cell structure and an n-doped a-Si:H stack as the electron-selective contact, were used for these devices.

This work focuses on applying the ALD  $V_2O_5$  films, without an a-Si:H interlayer, as hole-selective contacts on n-type c-Si solar cells using an IBC architecture. Furthermore, the IBC cell is fully implemented with ALD-based films, which means that both the hole-selective and the

electron-selective contacts are based on ALD  $V_2O_5$  and  $TiO_x$  films, respectively. In addition, the front and rear non-contacted surfaces are passivated with  $Al_2O_3$  films also deposited by ALD. The  $V_2O_5$  characterisation and its electrical/passivation behaviour as HTL is extensively reported in the next sections, exhibiting good surface passivation and relatively low contact resistivity. The ALD  $TiO_x$  characterisation was reported in our previous studies, see Ref. [20]. The main goal of this work is to demonstrate that fully ALD IBC solar cells could be developed circumventing the use of a-Si:H interlayers and reaching relevant efficiencies in  $3 \times 3$  cm<sup>2</sup> devices. These results pave the way for low thermal-budget, low cost and highly scalable ALD processes in combination with a highly demanding IBC solar cell architecture in the photovoltaic fabrication chain.

## 2. Experimental methods

### 2.1. ALD characterisation and film morphology

An ALD process and material characterisation of vanadium oxide layers were studied with FZ <100> c-Si(n) substrates with thickness and resistivity of 280  $\mu$ m and  $\sim 2$   $\Omega$ cm, respectively. After a HF (2%) dip for 30 s, the samples were introduced to the ALD equipment to deposit the corresponding  $V_2O_5$  film.

Vanadium oxide films were deposited by a thermal ALD system (Savannah S200, Cambridge Nanotech) with tetrakis (ethylmethylamino)-vanadium(IV) (VTIP) and deionised water (DI-H<sub>2</sub>O) as the vanadium precursor and oxidant species, respectively. The VTIP and water cylinders were set to 58 °C and room temperature, respectively. The influence of the main parameters involved in the ALD process, such as purges, precursor and oxidant pulse times, were evaluated by monitoring the film growth rate to ensure a self-limiting surface reacting regime. Moreover, the ALD process characterisation was studied for a temperature range from 80 °C to 200 °C.

The  $V_2O_5$  film structure and morphology were studied by X-ray photoelectron spectroscopy (XPS), using for the measurements a non-monochromatic Al-K $\alpha$  source (1486.6 eV) at  $3 \times 10^{-9}$  mbar (SPECS, hemispherical energy analyser PHOIBOS 150). High angle annular dark field (HAADF) scanning TEM images, in combination with energy dispersive X-ray spectroscopy (EDX) chemical composition analysis were executed by using a Cs-corrected FEI Titan (60–300 kV) transmission electron microscope. The FEI Titan was equipped with a high brightness Schottky emitter source (X-FEG gun), a monochromator and a Gatan 2k  $\times$  2k CCD camera. The cross-section lamellas were prepared from contact test samples, using a focused ion beam (FIB) lift-out technique. The samples were subjected to an oxygen plasma cleaning process before introducing them into the FEI Titan equipment.

### 2.2. Passivation test samples

The passivation properties of ALD  $V_2O_5$  films were studied in symmetrical samples using the same c-Si(n) substrates. A cleaning process with a 30 s dip in diluted HF (2%) was performed just before the introduction of the sample in the ALD equipment. In some test samples, c-Si(n) substrates were replaced using p-type counterparts with similar characteristics and same sample preparation.

The impact of the metal capping in the  $V_2O_5$ -based contact behaviour was assessed in another set of samples using the same c-Si(n) substrates. In this case, the  $V_2O_5$  film was deposited only in the front side and covered with a semi-transparent Ni film using an asymmetrical structure as follows (see Ref. [33] for details): first, after a RCA1/RCA2 and HF dip cleaning sequence [34], the samples were covered with a 50 nm thick ALD  $Al_2O_3$  layer on both sides deposited at 200 °C. Trimethylaluminium (TMA) and DI-H<sub>2</sub>O were used as the Al precursor and oxidant species, respectively. Next, the rear side was covered with a 25 nm thick silicon carbide layer (a-SiC). This close to stoichiometric a-SiC<sub>x</sub> film ( $x \sim 1$ ) was deposited by a plasma-enhanced chemical vapour deposition (PECVD)

**Table 1**

Summary of the main reported IBC solar cells using TMOs as selective contacts.

Ref.	Selective contact strategy (deposition method)		Efficiency (%)	Year
	HTL	ETL		
[25]	$MoO_x$ (thermal evap.)	$LiF_x$ (thermal evap.)	15.4	2016
[26]	$V_2O_5$ (thermal evap.)	$Cs_2CO_3$ (thermal evap.)	16.6	2016
[27]	$V_2O_5/Au/V_2O_5$ (thermal evap.)	$LiF_x$ (thermal evap.)	19.0	2017
[20]	$V_2O_5$ (thermal evap.)	$Al_2O_3/TiO_x$ (ALD)	19.1	2018
[28]	a-Si:H(i)/ $MoO_x$ (thermal evap.)	a-Si:H(i)/ $MgF_x$ (thermal evap.)	22.2	2018
[29]	PEDOT:PSS (spin-coating)	$MgO_x$ (thermal evap.)	16.3	2018
[30]	a-Si:H(i)/ $MoO_x$ (hot-wire sublimation)	a-Si:H(i)/ $SiO_x/TiO_x$ (spin-coating)	20.2	2019
[31]	a-Si:H(i)/ $MoO_x$ (thermal evap.)	a-Si:H(i)/ $LiF_x$ (thermal evap.)	20.3	2020
[32]	a-Si:H(i)/ $MoO_x$ (thermal evap.)	a-Si:H(i)/ $MgF_x$ (thermal evap.)	22.1	2020
<b>This work</b>	$V_2O_5$ (ALD)	$Al_2O_3/TiO_x$ (ALD)	<b>18.6</b>	–

process (13.56 MHz, from Electrorava S.p.A) at 300 °C, using methane and silane as precursor gases. The a-SiC layer provides an Al<sub>2</sub>O<sub>3</sub> film protection for subsequent chemical processes. At this point, the samples underwent an annealing treatment at 400 °C for 10 min in forming gas ambient to activate the surface passivation [35]. After etching the front Al<sub>2</sub>O<sub>3</sub> layer with a HF (2%) dip, the corresponding ALD V<sub>2</sub>O<sub>5</sub> film was deposited (200 ALD cycles at 125 °C). Afterwards, the V<sub>2</sub>O<sub>5</sub> film was covered with a thermally evaporated nickel film with a thickness of ~5 nm. The semi-transparent Ni film (~5 nm) allows reliable QSS-PC measurements in order to determine the influence of the metallic film on surface passivation.

Surface passivation was assessed by effective lifetime measurements by means of the quasi-steady-state photoconductance (QSS-PC) technique [36] using the WCT-120 instrument (Sinton Consulting).

### 2.3. Contact test samples

The contact properties of ALD V<sub>2</sub>O<sub>5</sub> films were also studied using the aforementioned c-Si(n) substrates. A cleaning process with a 30 s dip in diluted HF (2%) was conducted just before the introduction of the sample in the ALD equipment. In some test samples, c-Si(n) substrates were replaced using p-type counterparts with similar characteristics.

Contact characteristics were obtained using the transfer length method (TLM) [37,38]. Just after the ALD V<sub>2</sub>O<sub>5</sub> film deposition, TLM patterned metal-pads were evaporated above the V<sub>2</sub>O<sub>5</sub> film using a metallic shadow mask. Metallisation consists of a Ni/Al stack with a thickness of ~10/300 nm, respectively. The stack was thermally evaporated from pure source materials >99.95% using an SQC-310 deposition controller (Sigma instruments).

The electrical contact behaviour on c-Si(p) samples was assessed by fitting the dependence of the measured resistance of vertical dot-like structures as a function of the dot diameter, using the spreading resistance model [39]. In this case, just after the ALD V<sub>2</sub>O<sub>5</sub> film deposition on both sides of the sample, dot-like metal contacts (Ni/Al) were evaporated above the V<sub>2</sub>O<sub>5</sub> film using a metallic shadow mask (front side). Then, the same metal stack was evaporated on the back side, above the V<sub>2</sub>O<sub>5</sub> film, resulting in a fully contacted surface.

Electrical measurements were performed using a four-contact probe configuration by means of a current voltage (*I-V*) tracer (Keithley 3601B) at room temperature.

### 2.4. Solar cells

Finally, IBC solar cells of 3 × 3 cm<sup>2</sup> active area were fabricated using the same c-Si(n) substrates. The fabrication process starts with a front side random pyramid texturing by alkaline etching, using a tetramethylammonium hydroxide (TMAH) based solution. Then, the wafer was cleaned following a RCA1/2 sequence and a 50 nm thick Al<sub>2</sub>O<sub>3</sub> layer was deposited on both sides by ALD at 200 °C, using TMA and DI-H<sub>2</sub>O species. To activate the surface passivation provided by the alumina film, a 10 min annealing step was performed at 400 °C. Then a 25 nm thick a-SiC film was deposited on both sides in a similar way as explained before in the test samples (see section 2.2).

After a strip-like patterning on the c-Si back surface by tetrafluoromethane (CF<sub>4</sub>) plasma dry etching and a diluted RCA1/2 sequence, removing the a-SiC and Al<sub>2</sub>O<sub>3</sub> films, respectively, the ETL based on an Al<sub>2</sub>O<sub>x</sub>/TiO<sub>x</sub> stack was deposited by ALD at 100 °C. This TiO<sub>2</sub>-based contact scheme has been described in detail in one previous work of our group [20]. Afterwards, a Mg/Al stack was thermally evaporated resulting in 25 nm and 3 μm thick layers, respectively. Subsequently, the interdigitated electrodes were patterned by standard photolithography and wet etching. The whole back surface was covered with a structural photosensitive polyimide layer and the HTL strip-like regions were defined by photolithography. Thereafter, the a-SiC and alumina films were removed by a CF<sub>4</sub> dry etching and a subsequent HF dip. Finally, the ALD V<sub>2</sub>O<sub>5</sub> film was deposited and covered by a nickel capping layer

(~10 nm) and a 2 μm thick Al film. The whole metal stack was thermally evaporated using a shadow mask to avoid an additional photolithographic step, simplifying the fabrication process.

Photovoltaic parameters and illuminated *I-V* curves were measured under standard test conditions (1 kW/m<sup>2</sup> AM1.5G solar spectrum at a temperature of 25 °C) using an ORIEL 94021A (Newport) solar simulator. Light irradiance was properly calibrated by means of a pyranometer. External-quantum-efficiency (EQE) curves were measured using a commercial instrument (QEX10, PV measurements) with a white light bias of 0.1 Suns and a beam spot of 2 × 2 cm<sup>2</sup> centred within the active device area.

## 3. Results and discussion

### 3.1. ALD characterisation

Test samples of crystalline silicon covered with 600 ALD cycles of V<sub>2</sub>O<sub>5</sub> were made in order to characterise the film growth and optimise the ALD deposition parameters. The inset of Fig. 1 shows the growth per cycle (GPC) with respect to H<sub>2</sub>O and VTIP pulse durations with a process temperature of 125 °C. In all cases, the VTIP and water purge times were of 5 s. Two seconds H<sub>2</sub>O pulses were enough to achieve a GPC saturation condition, but a much longer pulse was required for the VTIP precursor. Thus, a 5 s VTIP pulse was chosen as a trade-off between the process duration and quasi self-saturation regime. Notice, that a GPC of 0.6 Å/cycle is achieved, which is comparable to other reported studies using the same vanadium precursor [40,41].

Then, the growth characteristics of the ALD V<sub>2</sub>O<sub>5</sub> film were investigated in a temperature range from 80 to 200 °C. The GPC is shown in Fig. 1, where the self-saturation ALD regime occurs in a wide temperature window between 80 and 150 °C, with a growth rate of ~0.6 Å/cycle. For higher temperatures, the growth rate quickly increases pointing out a chemical vapour deposition (CVD) regime.

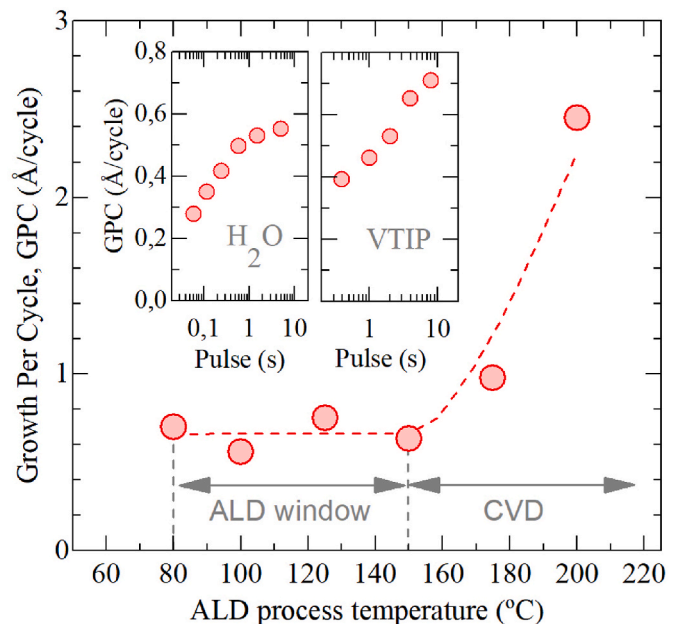


Fig. 1. Growth per cycle (GPC) rate as a function of the deposition temperature, using H<sub>2</sub>O and VTIP pulses of 2 and 5 s, respectively. In all cases purge times between precursor and water pulses were of 5 s (using N<sub>2</sub> flow). The insets show the GPC as a function of the H<sub>2</sub>O pulse duration with a fixed VTIP pulse of 2 s (left), and the VTIP pulse duration with a fixed H<sub>2</sub>O pulse of 2 s (right). In both cases using a deposition temperature of 125 °C.

### 3.2. Passivation and electrical properties

Once the  $V_2O_5$  ALD process was optimised, lifetime and transmission line method (TLM) measurements were carried out to determine the recombination current density ( $J_{0c}$ ) and the contact resistivity ( $\rho_c$ ), respectively. Low values of  $J_{0c}$  and  $\rho_c$  are mandatory to obtain good selective contact behaviour, and thus to obtain high efficiency c-Si solar cells.

The inset in Fig. 2a shows the measured lifetime on symmetrical samples covered with 200 ALD cycles of  $V_2O_5$  for different deposition temperatures from 100 to 150 °C. In all cases, the optimum ALD process condition described in section 3.1 was used, i.e. 2/5/5/5 s of  $H_2O$ /purge/VTIP/purge, respectively.  $J_{0c}$  values were extracted from effective lifetime ( $\tau_{eff}$ ) measurements [36]. A general trend can be observed in Fig. 2a, pointing out that a better passivation is achieved for lower ALD process temperatures. An implied open circuit voltage ( $iV_{oc}$ ) value of 655 mV and a  $J_{0c}$  value of 80 fA/cm<sup>2</sup> were achieved at 100 °C. For higher process temperatures, i.e. 125 °C and 150 °C, the  $J_{0c}$  parameter increases to 100 fA/cm<sup>2</sup> and 150 fA/cm<sup>2</sup> respectively. In any case, ALD  $V_2O_5$  films achieve a better passivation behaviour compared to thermally evaporated  $V_2O_5$  films, where  $J_{0c}$  values of 175 fA/cm<sup>2</sup> were obtained [33].

The impact of the  $V_2O_5$  film thickness, ranging from 50 to 300 ALD cycles, on the passivation behaviour is shown in Fig. 2b. In all cases, the process temperature was fixed at 125 °C. The film thickness has a lower impact on the passivation properties, showing only slight variations, with  $J_{0c}$  values of around 100 fA/cm<sup>2</sup>. This trend is not observed by other researchers; see for instance Ref. [18], where the  $J_{0c}$  values decrease for thicker films, yielding  $J_{0c}$  values from 95 to 40 fA/cm<sup>2</sup> for  $VO_x$  thickness from 4 to 9 nm, respectively.

Finally, the contact passivation provided by ALD  $V_2O_5$  films was also studied for p-type c-Si substrates, obtaining similar results, with a  $J_{0c}$  value of 100 fA/cm<sup>2</sup> (see Fig. 2b).

Additionally, the effect of an alumina interlayer between the c-Si and the  $V_2O_5$  layer was explored. Our previous reports indicate a passivation improvement by using an ultrathin ALD  $Al_2O_3$  film between the c-Si surface and the ALD  $TiO_2$  layer [20]. However, applied to  $V_2O_5$  films, 6 ALD cycles of an  $Al_2O_3$  interlayer considerably increased the  $J_{0c}$  value, i.e. worse contact passivation with a value of ~200 fA/cm<sup>2</sup>. Therefore, the alumina interlayer is not convenient for passivating  $V_2O_5$  contacts. This result agrees with other studies in which the alumina film was applied to contacts based on  $MoO_x$  layers showing a modest impact on selective properties [42].

TLM measurements were performed on c-Si(n) samples covered with

a 200 ALD cycles  $V_2O_5$  film and contacted with a Ni/Al stack. It is reported that the metal contact can affect the electrical properties on thin TMO films [43]. Additionally, in a previous result reported in Ref. [33] we concluded that a high-work function metal like Ni is preferred to contact thermally evaporated  $V_2O_5$  layers in comparison to low-work function metals like Al. More recently, other researchers have also used Ni as capping material for high-work function  $MoO_x$  films, resulting in a clear reduction of contact resistivity [17]. Thus, it is expected that Ni could also be a good candidate to contact the ALD  $V_2O_5$  films. Fig. 3a shows the contact resistivity ( $\rho_c$ ) as a function of the ALD process temperature. The TLM measurements confirm a minimum  $\rho_c$  value, lower than 250 mΩcm<sup>2</sup> using 200 cycles and an ALD process temperature of 125 °C.

The TLM measurements were also used to extract the sheet resistance parameter ( $R_{sh}$ ) of the depleted/inverted region beneath the HTL contact, obtaining values between 11 and 16 kΩ/sq for all the studied temperature range. The  $R_{sh}$  parameter was also measured by means of TLM structures on a glass substrate, as can be seen in the inset of Fig. 3a showing values higher than 5 GΩ/sq attributed to the  $V_2O_5$  layer. Consequently, the lower value obtained in the c-Si(n) substrates confirms the presence of an inverted p<sup>+</sup> layer on the n-type silicon surface underneath the film, reinforcing the hole-selective behaviour of the contact. It is interesting to highlight the relationship between the  $R_{sh}$  and surface passivation. The lower the  $R_{sh}$  value is the lower is also  $J_{0c}$ . This relation seems to indicate that a stronger inversion occurs inside the c-Si substrate, leading to a better passivated contact.

The impact of the  $V_2O_5$  film thickness, i.e. number of ALD cycles, on the contact resistivity was also studied considering a process temperature of 125 °C (see Fig. 3b). Notice that the film thickness has a high influence on the  $\rho_c$  parameter. For small thicknesses, the contact quality is very poor, achieving a high  $\rho_c$  value of ~1 Ωcm<sup>2</sup> for 50 ALD cycles. Nevertheless, a minimum  $\rho_c$  was found for 200 ALD cycles with a value of 250 mΩcm<sup>2</sup>, increasing again for thicker layers.

The influence of a thin ALD  $Al_2O_3$  interlayer in the contact properties was also included in the study. Again, the presence of this film worsens the contact behaviour, obtaining a  $\rho_c$  value of 550 mΩcm<sup>2</sup>. In addition, vertical test measurements were performed with c-Si(p) substrates following the sample preparation described in the experimental section and using 200 ALD cycles of  $V_2O_5$  film. Although the passivation was similar independent of the substrate type, the  $\rho_c$  shows a better behaviour using c-Si(p) substrates. A contact resistivity of 100 mΩcm<sup>2</sup> was obtained, which is comparable to the best values reported in the literature, for a c-Si(p)/ $VO_x$ /Ag contact scheme [18]. Hence, we can conclude that a Ni-capped ALD  $V_2O_5$  layer has a very good performance

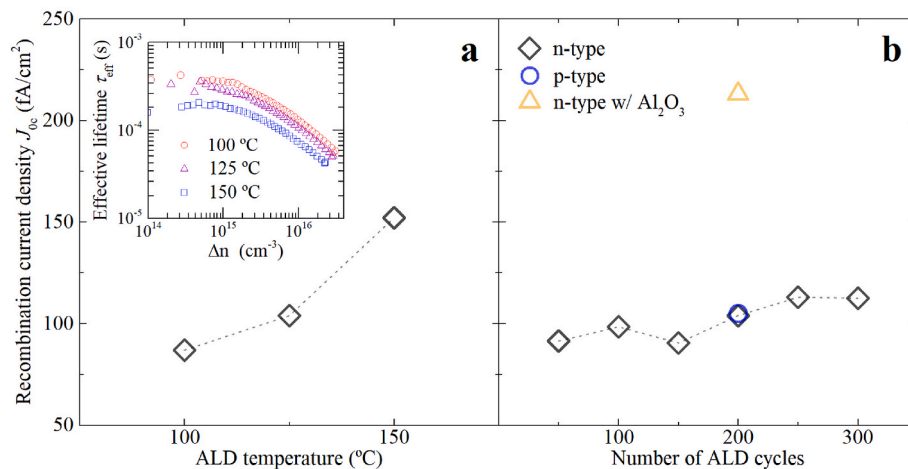
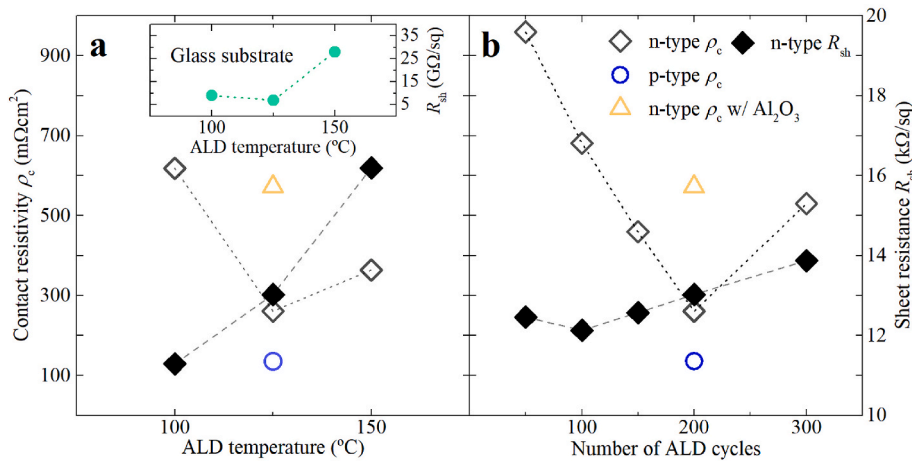


Fig. 2. Recombination current density ( $J_{0c}$ ) as a function of the ALD process temperature (left) and the number of ALD cycles (right). Measured lifetime ( $\tau_{eff}$ ) for different ALD process temperatures are also shown (inset). For the temperature study the c-Si was covered on both side with 200 ALD cycles of  $V_2O_5$  film. For the thickness study the ALD temperature was kept at 125 °C.



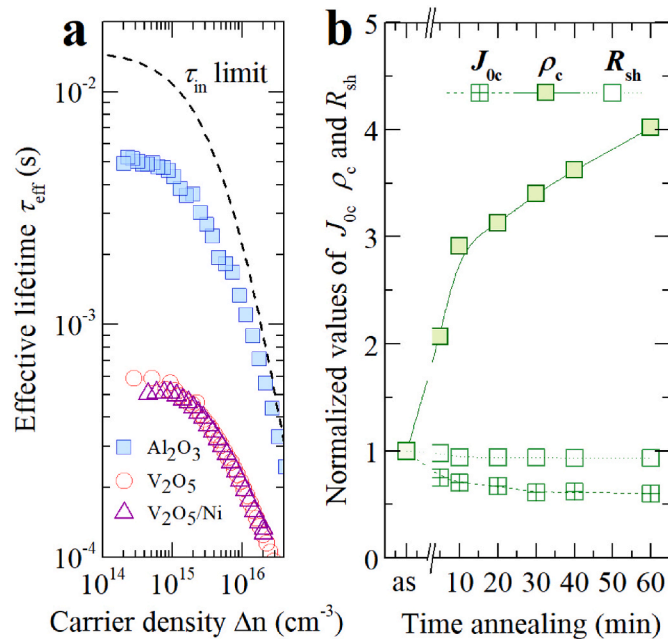
**Fig. 3.** Contact resistivity (empty symbols) and sheet resistance (filled symbols) as a function of the ALD process temperature (left) and the number of ALD cycles (right).  $R_{sh}$  values extracted from glass substrates are also shown in the inset. For the ALD temperature study (left), the c-Si was covered with 200 ALD cycles of a  $V_2O_5$  film. For the number of ALD cycles study (right), the ALD temperature was kept at 125 °C ( $\rho_c$  and  $R_{sh}$  values were extracted from TLM using Ni/Al pads).

to contact c-Si substrates.

Finally, the impact of Ni metallisation on surface passivation was evaluated using a very thin Ni film (~5 nm) deposited on the  $V_2O_5$  layer in order to mimic the final contacted structure in solar cell devices. In this case, an asymmetric scheme was used, in which the rear side was passivated with an  $Al_2O_3$ /a-SiC stack and the front side was passivated with a  $V_2O_5$  layer as explained in the experimental section. A film of  $V_2O_5$  consisting of 200 ALD cycles deposited at 125 °C was chosen as the best option considering the trade-off between  $\rho_c$  and  $J_{0c}$  values. The excellent passivation properties provided by ALD  $Al_2O_3$  layers [35], i.e. effective surface recombination velocity ( $S_{eff}$ ) values below 2 cm/s, allow discriminating the recombination contribution of the  $Al_2O_3$ -coated side, thus obtaining the recombination contribution of the  $V_2O_5$ -coated surface. Fig. 4a shows the measured lifetime of a both-sides

passivated sample with an ALD  $Al_2O_3$  film with its associated intrinsic lifetime ( $\tau_{in}$ ) [44] (upper limit), reaching an  $S$  value as low as 1.6 cm/s ( $J_{0c} \sim 5$  fA/cm $^2$ ) [45]. Comparing lifetime results of asymmetric samples with and without a Ni film (see Fig. 4a), we can conclude that the metal capping does not affect the passivation quality, with  $J_{0c}$  values around 100 fA/cm $^2$  in either case.

Fig. 4b shows the evolution of the normalised values (i.e. value $_{measured}$ /value $_{initial}$ ) of  $J_{0c}$ ,  $\rho_c$  and  $R_{sh}$  parameters for accumulative annealing times at 125 °C in  $N_2$ . Regarding surface passivation, the contact shows an improvement with the annealing time. Note that the  $J_{0c}$  value decreases by 30% after the initial 10 min annealing. However, the contact resistivity degrades strongly with the annealing time. The  $\rho_c$  value evidences a three-fold increase with an annealing of only 10 min. Therefore, the  $V_2O_5$ -based selective contact should be deposited at the last stages of the IBC fabrication process to avoid any high thermal steps which would jeopardise the good contact behaviour.

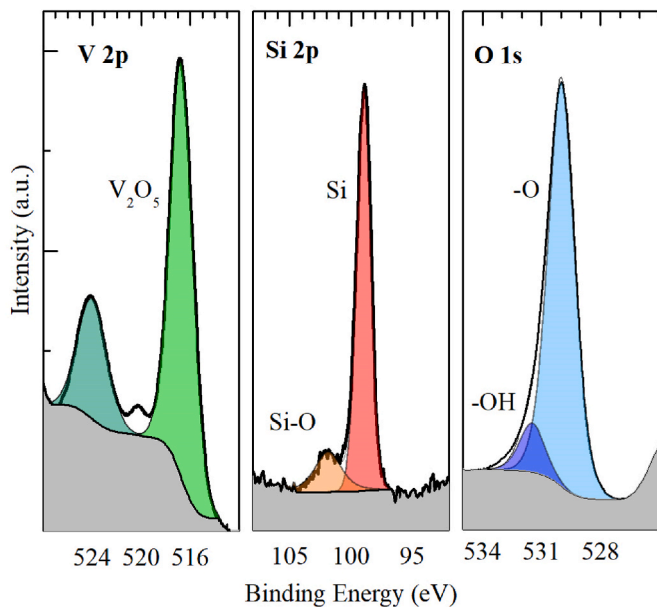


**Fig. 4.** Measured lifetime ( $\tau_{eff}$ ) for  $Al_2O_3$ /c-Si(n)/ $Al_2O_3$ ,  $V_2O_5$ /c-Si(n)/ $Al_2O_3$  and Ni/ $V_2O_5$ /c-Si(n)/ $Al_2O_3$  samples (left). Normalised recombination current density ( $J_{0c}$ ), contact resistivity ( $\rho_c$ ) and sheet resistance ( $R_{sh}$ ) as a function of the annealing accumulative time (right). All annealing stages were performed at 125 °C in  $N_2$  ambient.  $J_{0c}$  values were extracted from  $\tau_{eff}$  measurements and  $\rho_c$  and the  $R_{sh}$  values from TLM structures.

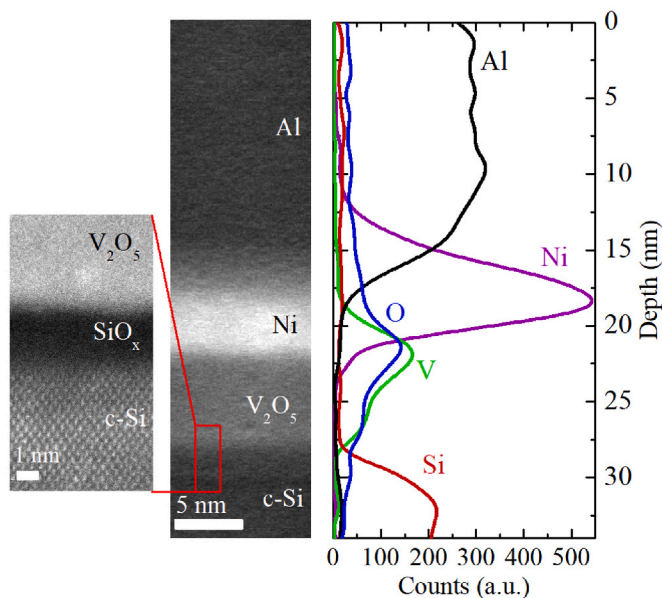
### 3.3. Morphological properties

Physical and morphological characterisation of the  $V_2O_5$ -based contact was analysed in order to determine the origin of the good electrical performance of the hole-selective contact. Firstly, an X-ray photoelectron spectroscopy (XPS) scan was performed on a 10 nm thick ALD  $V_2O_5$  film deposited on a c-Si substrate. Fig. 5 shows the XPS core level spectra for the  $V_2O_5$  film deposited at 125 °C. The V 2p core level was decomposed into a single peak centred at a binding energy of 516.9 eV, which can be attributed to the presence of  $V^{+5}$  cations [46]. This characteristic elucidates that the film has a stoichiometric  $V_2O_5$  phase and thus, no significant O vacancy defects are present. Hence, the main conduction mechanism through the layer might be a tunnelling process and not a trap-assisted process. The higher work function of stoichiometric films causes a stronger band bending inside the c-Si substrate, allowing holes to tunnel directly from the c-Si to the contact [17]. In addition, the Si 2p core level spectra are represented, in which a secondary peak centred at a binding energy of 101.8 eV is needed for the fitting. This binding energy is attributed to the presence of  $Si^{+3}$  oxidation states related to suboxidised  $SiO_x$  films, corroborated with the O 1s core level spectra.

Further analysis of the c-Si/ $V_2O_5$ /Ni/Al stack was performed by a high angle annular dark field (HAADF) scanning TEM image in combination with an energy dispersive X-ray spectroscopy (EDX) analysis. The EDX confirms the composition of the hole-selective contact structure (see Fig. 6), which is an ~10 nm thick  $V_2O_5$  layer and a ~7 nm thick Ni film.



**Fig. 5.** X-ray photoelectron spectroscopy core-level spectra of V 2p, Si 2p and O 1s for the ALD  $V_2O_5$  film deposited at 125 °C on c-Si(n) substrates.

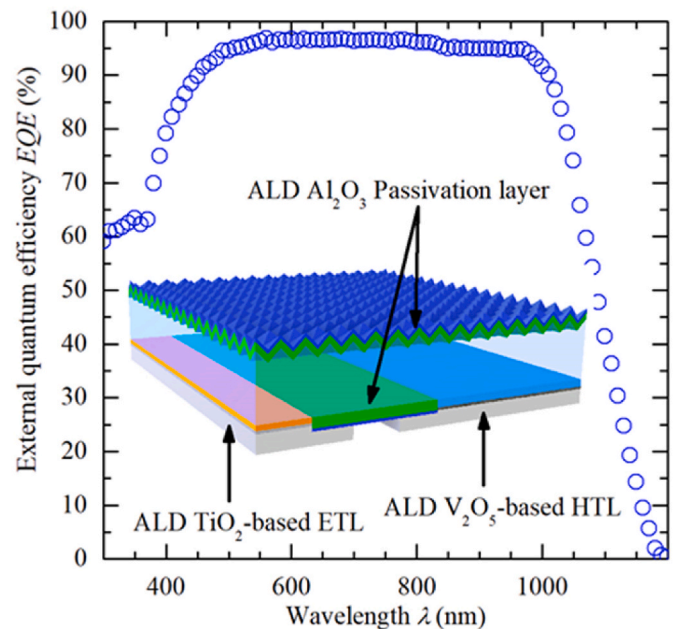


**Fig. 6.** Cross-sectional HR-TEM image of the c-Si/ $V_2O_5$  interface (left) and HAADF STEM image (middle) and EDX line scan of the c-Si/ $V_2O_5$ /Ni/Al structure with the Al, Ni, V, O and Si concentrations (right).

The presence of a thin interlayer between  $V_2O_5$  and c-Si is observed with the cross-sectional high-resolution transmission electron microscopy (HR-TEM) image, verifying the XPS analysis. The  $SiO_x$  interlayer has a thickness of about 1.6 nm. The formation of such silicon oxide layer has been previously observed in thermally evaporated TMOs [47] and also for the ALD process [17,18]. The good passivation properties of the TMOs are attributed, in part to the presence of this ultra-thin  $SiO_x$  interlayer.

### 3.4. IBC c-Si solar cells

The best ALD  $V_2O_5$ -based contact configuration was applied to fabricate proof-of-concept  $3 \times 3 \text{ cm}^2$  IBC c-Si(n) solar cells. Fig. 7 shows



**Fig. 7.** EQE curve of the best fully-ALD IBC solar cell. A 3D sketch of IBC solar cell is shown in the inset. Notice that the front surface and the gap between strip-like contacts are passivated with ALD  $Al_2O_3$  films.

a device 3D sketch highlighting that all surfaces of the silicon are covered with films deposited by the ALD technique. Specifically, a  $V_2O_5$  film (200 ALD cycles deposited at 125 °C) for the hole-selective contact, an  $Al_2O_3/TiO_x$  stack (6/20 ALD cycles) for the electron-selective contact [20] and a thick  $Al_2O_3$  layer (500 ALD cycles) to passivate non-contacted regions, i.e. both front surface and rear gap regions between contacts. To our knowledge, this is the first time that a c-Si solar cell with an IBC structure is fabricated entirely using ALD processes. Hence, this result opens the possibility to broaden the application of this deposition technique for cost-effective and high-volume manufacturing solar cells, increasing the ALD role in the future of photovoltaic industry [48,49].

The external-quantum-efficiency (EQE) of the best device is shown in Fig. 6 and its main photovoltaic parameters are summarised in Table 2. The excellent EQE values in the visible-NIR part of the spectrum, i.e. higher than 98% in the 500–1000 nm wavelength range, confirm an outstanding surface passivation, pointing out that carrier selective contacts based on ALD films are good enough to obtain high photovoltaic efficiencies. Open circuit voltage ( $V_{oc}$ ) values above 700 mV are usual when an a-Si:H(i) passivation interlayer is used between the c-Si and the TMO [18,50,51]. Nonetheless, when the TMO is directly deposited on the c-Si surface, low  $V_{oc}$  values below 600 mV are typically

**Table 2**

Photovoltaic parameters for the best IBC solar cell using ALD  $V_2O_5$  films (this work). Results are directly compared with an IBC counterpart where the  $V_2O_5$  was deposited by thermal evaporation (data extracted from Ref. [20]). IBC solar cells have an active area of  $3 \text{ cm} \times 3 \text{ cm}$  and were measured under standard test conditions (1  $\text{kW/m}^2$  AM1.5G spectrum at 25 °C).

Parameter	Selective contact process (HTL – ETL)	
	$V_2O_5 - Al_2O_3/TiO_x$	
	Evap. – ALD [20]	ALD – ALD [this work]
$J_{sc}$ ( $\text{mA/cm}^2$ )	40.0	39.4
$V_{oc}$ (mV)	633	652
FF (%)	75.4	72.5
pFF (%)	76.3	82.3
$r_s$ ( $\Omega\text{cm}^2$ )	0.19	1.97
$\eta$ (%)	19.1	18.6
pseudo- $\eta$ (%)	19.3	21.1

reported in the literature [9,26]. Consequently, the  $V_{oc}$  values of up to 652 mV achieved in this work can be considered a remarkable result. The other photovoltaic parameters listed in Table 2, such as the short circuit current density ( $J_{sc}$ ), the fill factor ( $FF$ ) and the power conversion efficiency ( $\eta$ ), with values of 39.4 mA/cm<sup>2</sup>, 72.5% and 18.6%, respectively, confirm the feasibility of ALD-based selective contacts for high efficiency IBC solar cells.

In order to get a better insight of the factors that may limit the performance of the device, we analysed the pseudo-light current density – voltage curve from Suns- $V_{oc}$  measurements [52,53]. Fig. 8a shows the illuminated  $J$ - $V$  curve for the best ALD  $V_2O_5$ -based IBC solar cell compared to the corresponding pseudo-light  $J$ - $V$  curve. The difference between both curves suggests that there is a relevant power efficiency loss due to series resistance. This fact is corroborated by the high value ( $\sim 2 \Omega\text{cm}^2$ ) of the specific series resistance ( $r_s$ ) parameter, as well as by the significant difference between the  $FF$  and the pseudo fill factor ( $pFF$ ) values. An estimation of the  $r_s$  parameter was calculated using the  $FF$  and  $pFF$  as follows;  $r_s \cong (1 - FF/pFF)V_{oc}/J_{sc}$  [53].

The relatively high  $r_s$  parameter can be not only attributed to a higher contact resistivity of the ALD  $V_2O_5$ -based contact, in comparison with the thermally evaporated counterpart, but also for some problems during the metallisation stage, i.e. either insufficient Al thickness or a poor metallic pad coverage. However, the promising pseudo efficiency obtained with a value of 21.1% indicates that there is room for improvement in the future to increase the efficiency.

On the other hand, we can observe an important improvement in the pseudo-efficiency compared to the case of evaporated  $V_2O_x$  films mainly coming from the  $pFF$ , i.e. the ideality of the current mechanisms at the junction. Fig. 8b shows the dark  $J$ - $V$  curves of two IBC solar cells, one based on ALD  $V_2O_5$  films (this work) and another which uses thermally evaporated  $V_2O_x$  films for the hole-selective contact (see Ref. [20]). As discussed above, the ALD-based cell exhibits a higher series resistance that can be observed at high applied voltages. By contrast, it has a better dark  $J$ - $V$  characteristic, i.e. a higher  $V_{oc}$  value than the evaporated counterpart, with an improvement of  $\sim 20$  mV (see Table 2). In addition, there is a significant reduction in recombination losses at low injection, which could be due to a better  $V_2O_5$  coverage at the edges of the HTL interdigitated regions provided by the ALD technique. The inset of Fig. 8b shows a cross section sketch explaining the potential coverage

problem at the HTL edges when thermally evaporated  $V_2O_x$  films are used which can lead to non-ideal current mechanisms, i.e. low  $pFF$  values. This phenomenon was recently studied, see Ref. [31], pointing out the influence of the edge recombination in silicon-based IBC solar cells with dopant-free heterojunctions. Thus, the use of the ALD technique could be a good choice to circumvent this issue due to the conformal nature of this deposition technique.

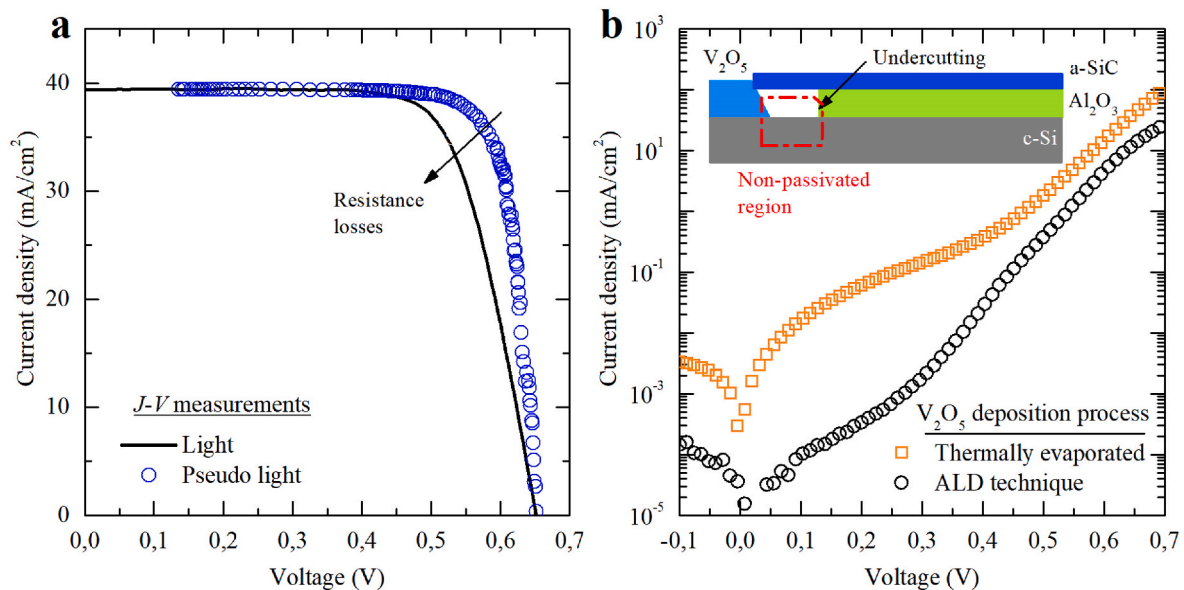
#### 4. Conclusions

In this work, we extensively report the characterisation of ALD  $V_2O_5$  films to be applied as hole-selective contacts for IBC solar cells. ALD deposition parameters were studied to obtain a self-saturation regime with a  $V_2O_5$  growth rate of  $\sim 0.6 \text{ \AA}/\text{cycle}$ . The X-ray photoelectron spectroscopy scan and its analysis for an ALD  $V_2O_5$  film deposited at 125 °C, indicate that the film has a stoichiometric composition. The presence of an inverted layer in the c-Si(n) surface underneath the  $V_2O_5$  film is confirmed by transfer length method (TLM) measurements, measuring sheet resistance ( $R_{sh}$ ) values in the 11–16 k $\Omega$ /sq range.

The good contact passivation provided by ALD  $V_2O_5$  films allowed recombination current densities ( $J_{0c}$ ) between 80 and 150 fA/cm<sup>2</sup> for an ALD deposition temperature from 100 to 150 °C. In addition, the presence of a Ni metal capping did not degrade the contact passivation that even improved after a temperature treatment in  $N_2$  ambient, i.e. a  $J_{0c}$  drop of 30% after 10 min annealing at 125 °C was measured.

Conduction properties of the ALD  $V_2O_5$ -based contact were studied by TLM measurements on c-Si(n) substrates. The ALD  $V_2O_5$  films have a strong dependence with the film thickness and temperature process, obtaining a minimum contact resistivity ( $\rho_c$ ) of 250 m $\Omega\text{cm}^2$  for 200 ALD cycles at 125 °C. For samples on c-Si(p) substrates, the  $\rho_c$  value is reduced to 100 m $\Omega\text{cm}^2$ . After an annealing step at 125 °C, although the passivation quality improves, but the contact resistivity is strongly degraded. Therefore, the  $V_2O_5$ -based selective contact should be deposited at the last stages of the IBC fabrication process to prevent any degradation during high thermal steps.

Finally, the optimised ALD  $V_2O_5$  film was applied to a proof-of-concept  $3 \times 3 \text{ cm}^2$  IBC c-Si(n) solar cell as a hole-selective contact. The  $TiO_2$ -based electron-selective contact is also deposited by ALD, as well as the  $Al_2O_3$  films to passivate the non-contacted surfaces.



**Fig. 8.** (a) Light and pseudo light current density – voltage ( $J$ - $V$ ) curves for the best IBC solar cell. The pseudo  $J$ - $V$  characteristic, free of series resistance effects, is determined from Suns- $V_{oc}$  measurements. (b) Comparison of the dark  $J$ - $V$  characteristic for the best IBC solar cell with a counterpart which uses thermal evaporated  $V_2O_5$  films. In both cases, the ETL is based on  $TiO_2$  films deposited by ALD. The inset shows a sketch of the undercutting phenomenon that could happen in the finger perimeter when thermal evaporation technique is used.

Consequently, to our knowledge, this is the first fully ALD IBC solar cell structure reported in the literature. A solar cell efficiency of 18.6% and a pseudo efficiency, i.e. calculated without losses due to parasitic series resistance, of 21.1% have been obtained. This work demonstrates the feasibility of applying the ALD technique to deposit carrier-selective contacts based on transition metal oxides for high efficiency IBC solar cells.

### CRedit authorship contribution statement

**Gerard Masmijà:** Writing – original draft, Methodology, Investigation, Formal analysis, Conceptualization. **Eloi Ros:** Investigation, Writing – review & editing. **Rosa Almache-Hernández:** Investigation, Formal analysis. **Benjamín Pusay:** Formal analysis, Investigation. **Isidro Martín:** Writing – review & editing, Methodology, Funding acquisition, Conceptualization. **Cristóbal Voz:** Conceptualization, Funding acquisition, Methodology, Writing – review & editing. **Edgardo Saucedo:** Funding acquisition, Conceptualization. **Joaquim Puigdollers:** Conceptualization, Funding acquisition, Methodology, Supervision, Writing – review & editing. **Pablo Ortega:** Writing – review & editing, Supervision, Methodology, Funding acquisition, Conceptualization.

### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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