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Processing of AC-coupled n-in-p pixel detectors on MCz silicon using atomic layer deposited aluminium oxide

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Abstract

We report on the fabrication of capacitively (AC) coupled n⁺-in-p pixel detectors on magnetic Czochralski silicon substrates. In our devices, we employ a layer of aluminium oxide (Al₂O₃) grown by atomic layer deposition (ALD) as dielectric and field insulator, instead of the commonly used silicon dioxide (SiO₂). As shown in earlier research, Al₂O₃ thin films exhibit high negative oxide charge, and can thus serve as a substitute for p-stop/p-spray insulation implants between pixels. In addition, they provide far higher capacitance densities than SiO₂ due to their high dielectric constant, permitting more efficient capacitive coupling of pixels. Furthermore, metallic titanium nitride (TiN) bias resistors are presented as an alternative to punch-through or poly-Si resistors.

Devices obtained by the above mentioned process are characterized by capacitance-voltage and current-voltage measurements, and by 2 MeV proton microprobe. Results show the expected high negative charge of the Al₂O₃ dielectric, uniform charge collection efficiency over large areas of pixels, and acceptable leakage current densities.

Keywords: Atomic Layer Deposition (ALD), Al₂O₃, pixel detector, capacitive coupling

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1. Introduction

Upon transition to the HL-LHC in 2026, the radiation levels at the innermost silicon layers of the experiments' tracking detectors will increase up to e.g. $2.3 \times 10^{16} \text{ n}_{eq} \text{ cm}^{-2}$, or 12 MGy, in the CMS Tracker detector [1]. Due to extensive radiation damage to the silicon material caused in these conditions, the charge carrier trapping time and electron saturation drift velocity product will limit the distance where the signal charge is collected. The degradation of detector efficiency can be prevented through the detector design, by decreasing the pixel pitch to be comparable with charge collection distance, and optimizing the geometry to enhance weighting field effects [2]. This also provides better spatial resolution through increased granularity of the detector.

Approaches in defect-engineering of Si towards higher radiation hardness include the use of substrates grown by the magnetic Czochralski (MCz) method, where the Si ingot is pulled from a melt in a quartz crucible and therefore has an intrinsically higher oxygen concentration of around $(5-10) \times 10^{17} \text{ cm}^{-3}$. MCz silicon substrates have exhibited better radiation tolerance than detectors grown by the dominantly used float zone (Fz) method and are thus a candidate for application in HL-LHC conditions [3, 4].

When considering the reduction of pixel size in order to counter the decrease in charge collection distance after irradiation of the detector, one challenge is the need for electrical insulation between pixels. To benefit from the higher mobility of electrons compared to the holes in Si, modern detectors are realized with segmented n^+ implants, on a p-type substrate. However, the traditionally used field insulator dielectric in pixel detectors, silicon dioxide (SiO_2) obtained by thermal oxidation, possesses a weak positive oxide charge that increases with irradiation [5, 6]. In reverse-biased n-in-p detectors, this positive charge would lead to a loss of spatial resolution, as the electron-collecting segments are effectively connected to each other. This is usually avoided by the use of an additional p-type implant between the pixels, referred to as p-spray or p-stop, depending on its width and concentration. However, p-spray/p-stop implants require additional implantation and high-temperature process steps, as well as more space on the detector.

An alternative to the combination of SiO_2 and insulation p^+ implants is the use of a different oxide with negative charge. The main candidate is aluminium oxide (Al_2O_3), which is widely used as surface passivation layer in the silicon photovoltaics industry [7]. The superior performance of Al_2O_3 includes contribution from both chemical passivation by termination of dangling bonds on the Si surface, and field-effect passivation due to its high negative oxide charge, which repels

32 electrons and therefore prevents them from recombining at remaining interface and near-interface
33 defects [8, 9].

34 One established way to fabricate Al_2O_3 thin films is by atomic layer deposition (ALD). This
35 method is based on the successive, separated, and self-terminating gas-solid reactions of typically
36 two gaseous precursors separated by a purge of inert gas [10–12]. An example schematic visualizing
37 the growth of a layer of Al_2O_3 in tri-methyl aluminum (TMA, $\text{Al}(\text{CH}_3)_3$) + H_2O process, one of
38 the most well-known ALD processes [13], is shown in Figure 1.

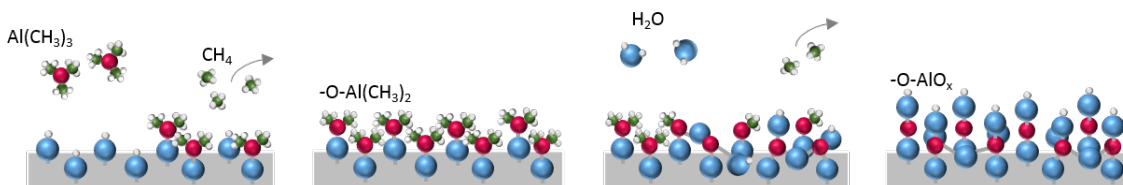


Figure 1: Illustration representing one ALD cycle of the Al_2O_3 process using TMA and water.

39 The use of Al_2O_3 deposited by ALD in particle and radiation detectors has been demonstrated
40 for Si photodiodes [14] and for strip detectors [15, 16], and has been proposed also for pixel detectors
41 [17]. This paper presents in detail the fabrication process of pixel detectors and reference structures
42 on high-resistivity MCz silicon using Al_2O_3 thin films as field insulator and passivation layers. In
43 addition, titanium nitride (TiN) thin film biasing resistors are used in place of standard punch-
44 through or poly-Si resistors. As opposed to [16], where Al_2O_3 was applied after conventional strip
45 detector processing, following our previous work [15, 17] Al_2O_3 was fully integrated into the detector
46 fabrication process, without any remaining SiO_2 in the final devices.

47 2. Detector processing

48 Detector fabrication was carried out in the facilities of Micronova Nanofabrication Centre. The
49 process was implemented on 6-inch Magnetic Czochralski silicon wafers supplied by Okmetic Oyj,
50 with a thickness of $320\ \mu\text{m}$ and crystal orientation $\langle 100 \rangle$. The wafers were boron-doped to a
51 resistivity specified as 4-8 $\text{k}\Omega\text{cm}$.

52 The wafer layout consisted of the following devices:

- 53 • AC-coupled detectors with 4160 pixels in a 80×52 double-column structure, with pixel pitch
54 $100\ \mu\text{m}$ resp. $150\ \mu\text{m}$, to match the CMS PSI46dig read-out chip used in the Phase I pixel

55 detector upgrade [18].

- 56 • DC-coupled pixel detectors with 400×192 pixels of $50 \times 50 \mu\text{m}^2$ pixel pitch, corresponding
57 to the geometry of the RD53A read-out chip [19].
- 58 • $7 \times 7 \text{ mm}^2$ pad diodes with broader central guard ring and a series of outer guard rings.
- 59 • MOS capacitors with diameter of 9.4 mm.
- 60 • Arrays of various test components, most importantly single-pixel biasing resistor structures.

61 A schematic presentation of processing steps is shown in Figure 2a, with a fully processed wafer
62 in Figure 2b. The highlighted boxes represent the steps which are presented as a novelty to pixel
63 detector processing in this article, and are discussed in more details in separate subsections. The
64 other steps are summarized below. Lithography was carried out by standard techniques including
65 priming, resist development, baking, and resist stripping. Photoresist patterning was performed
66 with a mask aligner in soft-contact mode.

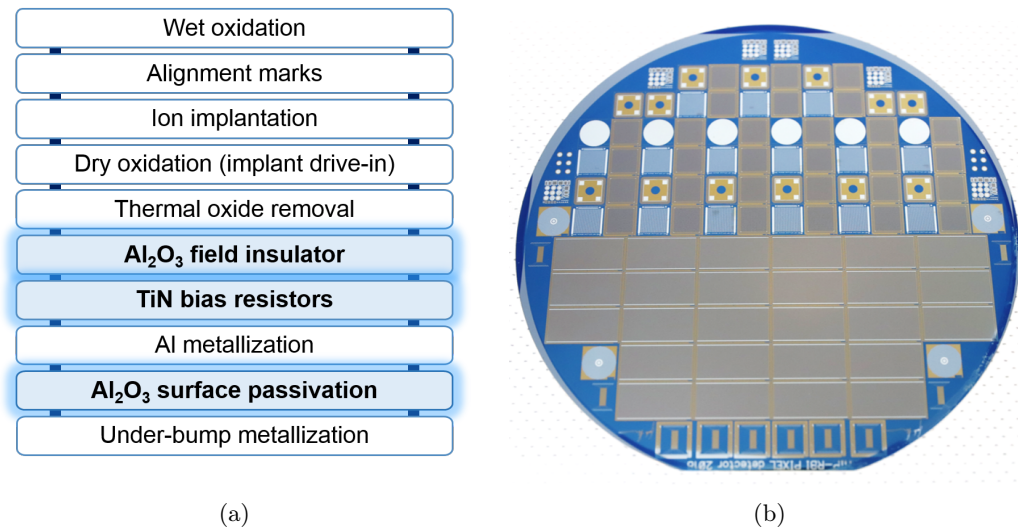


Figure 2: a) Schematic of the detector process flow presented in this paper. b) Photograph of a full 6-inch wafer before dicing.

67 First, wafers underwent wet oxidation at $1000 \text{ }^\circ\text{C}$ in order to obtain an approximately 300 nm
68 thick thermal oxide as hard mask for ion implantation. The oxidation was preceded by standard

69 chemical cleaning sequence (RCA cleaning) [20]. Alignment marks were etched by reactive ion
70 etching (RIE), using CHF_3 and SF_6 ions to etch SiO_2 and Si, respectively. For ion implantation,
71 the SiO_2 on the wafer front surface was patterned by wet etching with a buffered hydrofluoric acid
72 (BHF) etchant solution at 30 °C. The oxide on the back surface was removed completely. Ion
73 implantation was carried out in an Eaton 8200 Ion implanter, implanting the front side with 60
74 keV phosphorous ions and the back side with 20 keV boron ions, both to target total doses of
75 $1 \times 10^{15} \text{ cm}^{-2}$. After implantation, the mask oxide was etched away with BHF, the wafers were
76 RCA-cleaned, and subjected to a 46 min anneal at 1100 °C in dry oxidation conditions, in order to
77 diffuse the implanted ions deeper into the bulk. The resulting fresh thermal SiO_2 was again removed
78 with BHF, and RCA cleaning was repeated. This was followed by the deposition and patterning of
79 Al_2O_3 as field insulator and titanium nitride as bias resistor material (cf. Subsections 2.1 and 2.2).
80 For the metal contacts, aluminium was deposited by direct current (DC) sputtering along with a
81 capping layer of TiN and patterned with a commercial $\text{H}_3\text{PO}_4\text{-HNO}_3$ Al etchant at 50 °C. This
82 second layer of TiN served as an etch stop in the passivation oxide patterning later in the process.
83 Capacitive coupling from pixel to readout was achieved by contacting only the pixel implant in a
84 small corner, while the largest part of the metal pad with the bump connection to the read-out was
85 situated on a continuous layer of oxide without contact opening. For surface passivation, another
86 thinner layer of Al_2O_3 was deposited (cf. Subsection 2.1). Surface passivation by SiN_x was avoided
87 due to this material's positive charge [21], which would pose a risk to the envisioned field-effect
88 passivation through the negative charge of Al_2O_3 . Finally, a gold (Au) under-bump metallization,
89 with an underlying adhesive layer of titanium tungsten (TiW), was deposited by alternating current
90 (RF) sputtering. In this case, photoresist was applied prior to deposition, and the TiW-Au layer
91 was patterned by a lift-off technique.

92 *2.1. Atomic layer deposition of Al_2O_3*

93 Al_2O_3 was deposited at 200 °C in a Beneq TFS-500 batch-type ALD reactor, using $\text{Al}(\text{CH}_3)_3$
94 as the metal precursor. A H_2O pulse as primary reactant was complemented by an additional
95 ozone (O_3) pulse. Al_2O_3 films deposited by this combination of oxidants have been found to retain
96 the excellent surface passivation and low-defect interface of films deposited by the TMA+ H_2O
97 process, while exhibiting more effective negative oxide charge [22, 23]. Furthermore, the addition of
98 O_3 has been observed to prevent local delamination, also known as blistering, of Al_2O_3 films, which

99 may occur upon low-temperature annealing of films deposited using only water as the oxidant [24,
100 25]. This phenomenon must be prevented especially in highly segmented devices, such as the pixel
101 detectors described in this work, since it poses a severe risk for short-circuits between neighboring
102 pixels, as well as for sparking between the sensor and read-out chip in high electric fields.

103 One ALD cycle consisted of a 200+200 ms TMA pulse, followed by a 7 s N₂ purge, and subse-
104 quent 200+200 ms H₂O and 3.5+3.5 s O₃ pulses, again with a 7 s N₂ purge.

105 The same ALD process was used twice in detector fabrication: first to deposit the field insulator
106 dielectric, and a second time as surface passivation on top of the processed pixel structures. For field
107 insulation deposition, the number of ALD cycles was 700, for surface passivation 300, resulting in
108 film thicknesses of 84 and 33 nm, respectively, as determined by ellipsometry. Film thicknesses were
109 also examined after completed processing by cross-sectional scanning electron microscope (SEM)
110 imaging of a diode, which also shows the conformal and pinhole-free deposition of the Al₂O₃ thin
111 films (see Figure 3).

112 Etching of both films was performed using a commercial Honeywell PWS 80-16-4 phosphoric acid
113 etchant at 50 °C. Etch rates for metallic Al and Al₂O₃ in this solution are sufficiently different for
114 the chemical to also be used later in the process for patterning of the Al metallization layer without
115 significant damage to the Al₂O₃ field insulation. During the passivation opening step, however, the
116 underlying metal contacts need to be protected from the etchant, in this work by a passive layer
117 of TiN which is not related to the bias resistor layer. For the future, other high- κ oxides, such as
118 hafnium oxide (HfO₂) are considered as a replacement to Al₂O₃ as surface passivation in order to
119 provide chemical compatibility in passivation opening etching. After patterning, Al₂O₃ films were
120 sintered for 30 min at 370 °C in order to improve their stability in the following processing, and to
121 establish the negative oxide charge. In case of the annealing of the Al₂O₃ surface passivation, this
122 simultaneously served as sintering step for the Al metallization.

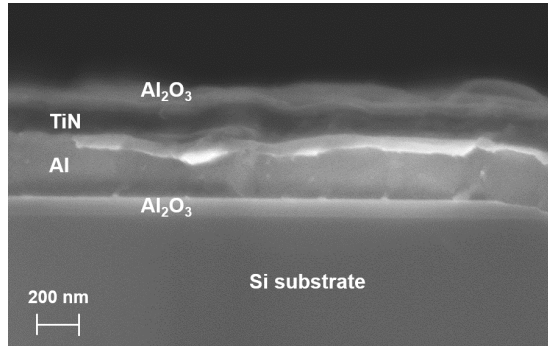


Figure 3: SEM cross-section of a pad detector, showing very uniform Al₂O₃ layers.

123 *2.2. Fabrication of titanium nitride bias resistors*

124 As presented earlier in a preliminary study [17], TiN biasing resistors were employed to provide
 125 individual bias resistors for all pixels on the sensor. As opposed to this previous study, the TiN
 126 films were now deposited by reactive RF sputtering for technical reasons.

127 Films were deposited by sputtering a Ti metal target in Ar (18 sccm) as plasma gas, with
 128 additional N₂ gas flow (72 sccm). The plasma power was 800 W. A sputtering time of 800 s resulted
 129 in a film with sheet resistance of 62 Ω/sq, and thickness of approximately 50 nm. Patterning of
 130 the films was performed by wet etching with 30% H₂O₂ at 50°C. Although comparatively slow at
 131 an etch rate of around 5 nm/min, this method allows batch processing of wafers (unlike our RIE
 132 equipment) and does not attack Al₂O₃.

133 The AC-coupled pixel detectors were realized in two groups with slightly different pixel biasing
 134 schemes, as shown in Figure 4. The actual TiN bias resistor part remained unchanged; however,
 135 the bias line connecting each pixel resistor to the common bias rail surrounding the detector was
 136 implemented either in the metal layer, or earlier as an additional n⁺ implant grid. Simulations
 137 indicated that such an implant may improve the breakdown properties of the sensor between pixels,
 138 while also being less vulnerable to scratches on the surface that could interrupt the metallic bias
 139 line on the surface.

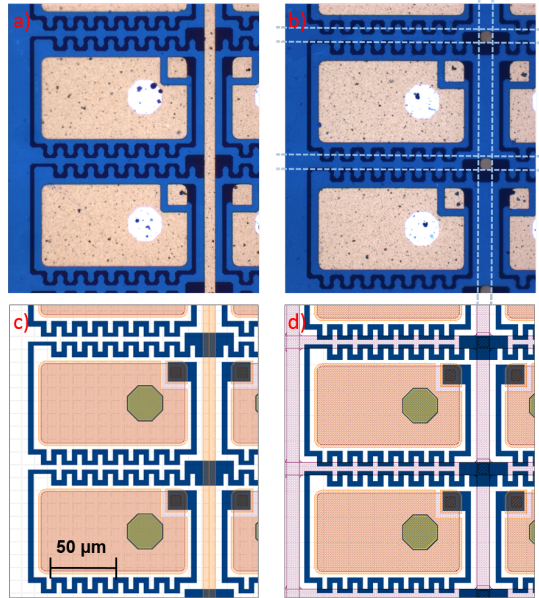


Figure 4: Two different biasing schemes used in our pixel detectors, with microscope images on the top and corresponding layout on the bottom: bias through metal line (left) or through an additional n^+ implant grid not visible in the picture, indicated by the dashed lines (right). The width of the bias resistor is nominally $4 \mu\text{m}$, dimension of pixels n^+ implants is $60\mu\text{m} \times 100\mu\text{m}$ (width / length) and the passivation opening for the solder bumps is $30 \mu\text{m}$.

140 3. Characterization

141 The electrical properties of the various components in the AC-coupled pixel detectors were
 142 studied primarily using reference devices - diodes, MOS capacitors and resistor test structures - due
 143 to the more straightforward nature of the corresponding measurements.

144 Leakage current densities, depletion voltage, and silicon bulk capacitance after full depletion were
 145 determined by current-voltage (IV) and capacitance-voltage (CV) measurements on pad diodes.

146 The effective charge, as well as an estimation of mobile charges, of Al_2O_3 was examined through
 147 CV measurements on MOS capacitors. The total resistance of a bias resistor for a single pixel
 148 was extracted from an IV measurement on a simple reference resistor structure between two metal
 149 pads. IV measurements on the AC-coupled pixel detectors were also performed, however, in a
 150 configuration with floating guard rings (which did not have passivation openings, as visible in
 151 Figure 7a) and the current read from the bias rail. This does not provide any separation of pixel
 152 leakage currents from possible high edge and surface currents, and is therefore interpreted as an
 153 overestimation of the leakage current in the detector during real operation, where the bias rail is

154 grounded.

155 For IV measurements, a Keithley 2410-C SourceMeter unit was used to supply the bias voltage
156 through the probe station chuck to the backplane of the device, and simultaneously to measure the
157 total current. Pad currents were read by a Keithley 6487 PicoAmmeter connected through a probe
158 needle to the device's metal pad. In diodes, the main guard ring was grounded through a second
159 probe needle.

160 For CV, the device was connected by probe needle through a current-potential decoupling box to
161 an Agilent E4980A Precision LCR meter, with the Keithley 2410-C still supplying the DC bias.
162 Capacitances were recorded at an AC frequency of 1 kHz.

163 An AC-coupled pixel detector with implanted bias line was studied by ion beam induced current
164 (IBIC) method. The IBIC measurements were performed at the Laboratory for Ion Beam Inter-
165 actions of the Ruđer Bošković Institute with 2 MeV protons from a 1.0 MV HVE Tandetron. The
166 beam frequency was set to around 1 kHz with beam current level at 20 pA. Due to the limited scan-
167 ning range of the beam in a single measurement, only selected areas of approximately $1 \times 1 \text{ mm}^2$
168 were studied. The beam centroid was moved over the selected area with scanning speed of about
169 1.3 ms per measurement point. The detectors were irradiated through the front plane which was
170 connected to ground through a 50Ω resistor. The bias voltage was applied to the backplane. The
171 detectors were biased and read out through an Ortec 142 pre-amplifier, and the resulting signals
172 were further amplified with Ortec 572 amplifier. After the amplification, the signal was passed
173 through an analogue to digital converter (ADC) to a field-programmable gate array, and mapped
174 with the SPECTOR system [26], [27]. More details of the microbeam readout chain and the IBIC
175 mapping can be found in [28].

176 4. Results

177 An illustrative example of a diode C-V curve is shown in Figure 5a. It indicates full depletion
178 (defined as the point where capacitance remains constant) at around -50 V. This corresponds to
179 an effective doping concentration of $6.3 \times 10^{15} \text{ cm}^{-3}$ and a resistivity of 22 k Ω cm, which is clearly
180 higher than the original wafer specifications. Such a difference may be due to a deviation of substrate
181 properties in the manufacturing process, for example a change in oxygen concentration across the
182 silicon ingot. Alternatively, this could be an indication that thermal donors were introduced into
183 the MCz substrate at some stage of the detector fabrication process, lowering the effective p-type

184 doping concentration. In principle, a lower full depletion voltage is seen as an advantageous property
 185 regarding detector operation.

186 The MOS capacitor C-V curve shown in Figure 5b demonstrates a high positive flat-band voltage
 187 (V_{fb}). Curves were recorded both from accumulation of the gate towards inversion, i.e, in this case
 188 for p-type substrate, starting from negative gate voltages or zero, and vice-versa. The absence of
 189 significant hysteresis between the two indicates that the density of mobile charges at the oxide-silicon
 190 interface is negligible.

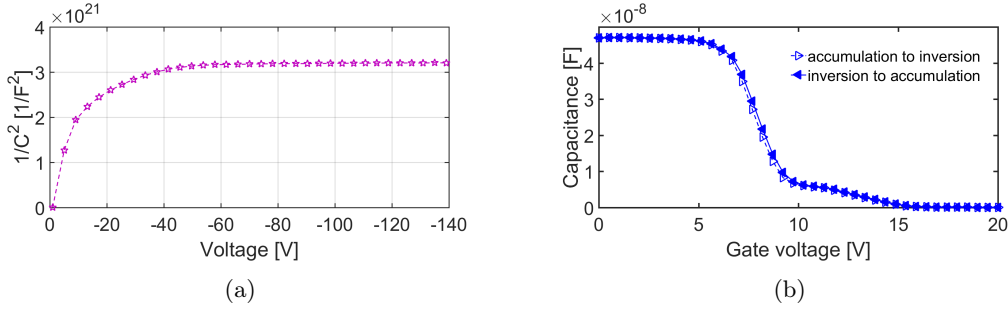


Figure 5: a) A typical diode reciprocal capacitance curve. b) C-V curve for a typical MOS capacitor.

191 Neglecting interface states and thus the effect of substrate doping, the oxide charge Q_{eff} can
 192 be estimated from V_{fb} according to Equation 1:

$$Q_{eff} = -C_{ox}\Delta V_{fb} \quad (1)$$

193 Using a V_{fb} value of 8 V, this yields an effective oxide charge of -3.5×10^{12} qcm^{-2} . This value
 194 is in good agreement with the literature, as well as the contactless CV measurements on thin film
 195 reference samples.

196 The illustrative I-V curves of a diode and an AC-coupled pixel detector are presented in Fig-
 197 ures 6a and 6b, respectively. The leakage current of the simple diode structure at full depletion is
 198 low, in the order of magnitude of 7 nA/cm². The pixel detector current is much higher, as expected.
 199 It appears to increase proportionally to \sqrt{V} until the detector is depleted, after which the current
 200 rises more sharply. This indicates either early breakdown, likely between pixels, or the formation
 201 of an Ohmic current path along the detector surface.

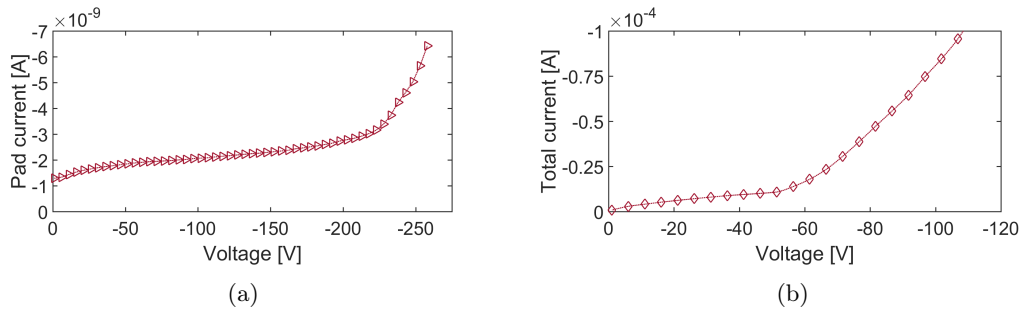


Figure 6: a) Diode IV. b) Pixel detector IV.

202 The biasing resistors' resistances were calculated as the reciprocal slope of a resistor test struc-
 203 tures' I-V curve (not displayed here). This method gave resistance values of around $15 \text{ k}\Omega$ for a
 204 resistor around a single pixel.

205 The IBIC map of an AC-coupled pixel detector with an implanted bias line grid is shown in
 206 Figure 7, along with a microscope image of the detector's corner section where the map was recorded.
 207 Bias rail, pixel and bias line implants are clearly visible as areas with higher current, thus implying
 208 that these areas are collecting charge. The collected charge over several rows and columns of pixels
 209 is uniform and the individual pixels are clearly separated from each other. The measurements also
 210 demonstrate that the additional bias line implant may result in reduced charge collection efficiency
 211 of the pixels, since some signal is collected at the bias line and transferred to the common bias rail,
 212 which would be grounded in final detector operation.

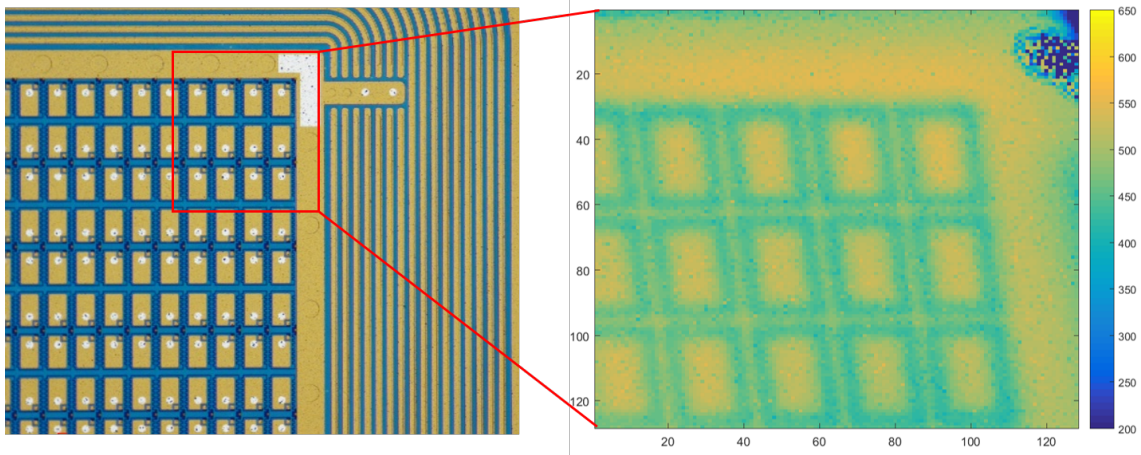


Figure 7: Microscope image of an AC-coupled pixel detector (left), with a section of it scanned by proton microprobe (right). Charge collection efficiency is in arbitrary units.

213 5. Conclusions

214 We demonstrated the integration of Al_2O_3 as field insulation dielectric and surface passivation
 215 layer into a pixel detector fabrication process. We were able to deposit blister-free, uniform Al_2O_3
 216 layers with highly negative oxide charge. TiN bias resistors with suitable resistance were fabricated.
 217 The performed C-V and I-V measurements on pad detectors show low leakage currents and suffi-
 218 ciently high breakdown voltage of the devices, which is very promising for the operation of more
 219 complex, pixelated detectors. The obtained IBIC map indicate that our AC-coupled pixel detectors
 220 are functional and have uniform charge collection efficiency, despite high initial leakage currents.

221 Further studies on the characterization of MCz devices with Al_2O_3 as field insulator, and their
 222 behavior in gamma irradiation [29] are left for a subsequent publication. In addition, a produc-
 223 tion of AC-coupled pixel detector/CMS PSI46dig read-out chip assemblies and assessment of their
 224 performance by test-beam campaigns is ongoing.

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