

Reducing the hydrogen content in liquid helium

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ABSTRACT

Helium has the lowest boiling point of any element in nature at normal atmospheric pressure. Therefore, any unwanted substance like impurities present in liquid helium will be frozen and will be in solid form. Even if these solid impurities can be easily eliminated by filtering, liquid helium may contain a non negligible quantity of molecular hydrogen. These traces of molecular hydrogen are the cause of a known problem worldwide: the blocking of fine capillary tubes used as flow resistors in helium evaporation cryostats to achieve temperatures below 4.2 K. This problem seriously affects a wide range of cryogenic equipment used in low temperature physics research and leads to a dramatic loss of time and costs due to the high price of helium. Here, we present first the measurement of molecular hydrogen content in helium gas. Three measures to decrease this molecular hydrogen are afterward proposed; (i) improving the helium quality, (ii) release of helium gas in the atmosphere during purge time for the regeneration cycle of the helium liquefier's internal purifier, and (iii) installation of two catalytic converters in a closed helium circuit. These actions have eliminated all blockages of capillaries at low temperatures now for more than two years.

1. Introduction

Even though helium (He) is the second most common element in the universe, there is only a limited amount available on the earth. Helium resources of the world were estimated to be about 35.2 billion cubic meters [1]. The locations and volumes of the significant deposits, in billion cubic meters, are Qatar, 10.1; Algeria, 8.2; Russia, 6.8; USA, 3.9; Canada, 2.0; and China, 1.1. With the current worldwide helium consumption being around 160 million cubic meters per year [1], the worldwide reserves are estimated to sustain the supply for ≈ 220 years at the present consumption rates. Although the long term prospect is not as severe as the short term landscape of helium supply, helium remains an unrecoverable natural resource. Unless recycled, any use cuts into the limited reserves and pushes us closer to the days when it is used up. As demand from high-tech manufacturing, including demand from China, is also rising, the problem is, helium is being used up faster than it can be produced these days. That created chaos in the helium supply chain in 2018, as roughly 30 percent of the global supply was taken off the market. The price has gone up by 50 to 100%, depending on local circumstances and position in the supply chain. Therefore, scientific laboratories are seeking to recycle helium. This is precisely the policy of the Department of Physics at the University of Basel and will be detailed later.

Another concern about liquid helium is the hydrogen (H_2) content. The blocking of fine capillary tubes used as flow resistors in He evaporation cryostats to achieve temperatures below 4.2 K is generally attributed to nitrogen or air impurities entering these tubes from the main bath [2]. However, even if one prevents these impurities from entering the capillary tubes, blocking of the capillary tubes frequently occurred. This points to hydrogen as the source of blocking. Many research laboratories around the world have faced this issue at a considerable financial cost because the affected systems have to be warmed up to room temperature to recover their typical low temperature operation performance [3–7]. In 2016, Gabal et al. [3] and, also in a recent paper, Will et al. [8], reported that even hydrogen concentrations within parts per billion are sufficient to block the helium flow within a few hours of operation. On the other hand, hydrogen impurities in liquid helium are easy to detect using a dedicated sensor developed at the University of Zaragoza [3]. It consists of a test capillary that is connected to a vacuum pump (see Fig. 2 in reference [9]) and has been successfully tested elsewhere [8]. Here, we report on another approach for the quantification of hydrogen impurities H_2 in liquid helium. In this work, we focus on the determination and reducing the amount of H_2 in liquid He. In the following, improvement of helium quality from 4.6 to 5.0, the release of He gas into the atmosphere during the purge time for the regeneration cycle of helium liquefier's internal purifier and the

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installation of two catalytic converters in the closed helium circuit will be discussed.

2. Liquefier

The Department of Physics at the University of Basel is equipped for more than 20 years with a helium liquefier. In September 2016, a new liquefier L70 [10] from Linde Kryotechnik was installed. It has been reported by Berdais et al. [11], its further developments were explained by Clausen et al. [12], and improvement of the redesigned internal purifier was presented by Decker et al. [13]. The liquefaction performance is at about 30 l/h without liquid pre-cooling. To avoid the release of helium into the atmosphere and reduce the depletion of helium reserves in the coming years [1], we have been equipped with a complete helium recovery plant. The recovery plant is schematically presented in Fig. 1, as well as in reference [14]. With this installation, the amount of helium gas recovered varied from ca. 78 to 86%, depending on the year. To address the resistor blockage, we have additionally equipped the liquefier with a setup for nitrogen (N_2) and H_2 measurements (Fig. 1). The locations, at which H_2 and N_2 concentration can be measured, were marked in red, labelled 1 to 4.

Hydrogen quantification is carried out using a continuous analyzer (Nova 430LRM Series Low Range Hydrogen Analyzer) [15] in a range of 0–200 parts per million (ppm) and with a resolution of 1 ppm. It is operating in a continuous mode for the measurement of low levels of H_2 in air, N_2 , or He samples, containing oxygen. If oxygen is not present, then an air supply system is usually included. H_2 is detected using a long life electrochemical sensor, composed of an anode, cathode, and a suitable electrolyte sealed together. When exposed to hydrogen, the unit produces a small output current, corresponding to the concentration of H_2 present in the sample. This output is then amplified and directed to the digital display meter. Regular calibrations were performed using a bottle of nitrogen 6.0 containing 100 ppm of H_2 and a nitrogen bottle purity 6.0 containing less than 0.5 ppm of H_2 . The results give ± 1.5 ppm error bars. For the measurement of N_2 a continuous Binary Gas Analyzer (BGA244 Stanford Research Systems) has been employed.

3. Results

In commercially available helium liquefiers, the internal gas purity is determined by adjusting the cold end temperature, the cold flow, the regeneration completion temperature, and the heater temperature. Typically, the internal purifier operating mode of a helium liquefier starts purification by going through the processes of purge, cool down 1, standby, and cool down 2 and then performs regeneration and enters the purge mode again [14]. As shown in the internal purifier flow diagram

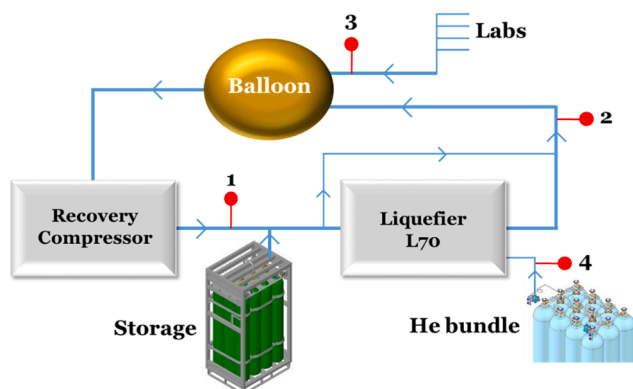


Fig. 1. Helium recovery plant including the L70 liquefier, the balloon, the recovery compressor including storage, and the feeding of fresh He delivered in gas bundles. Hydrogen and nitrogen measurements are possible at locations 1 to 4.

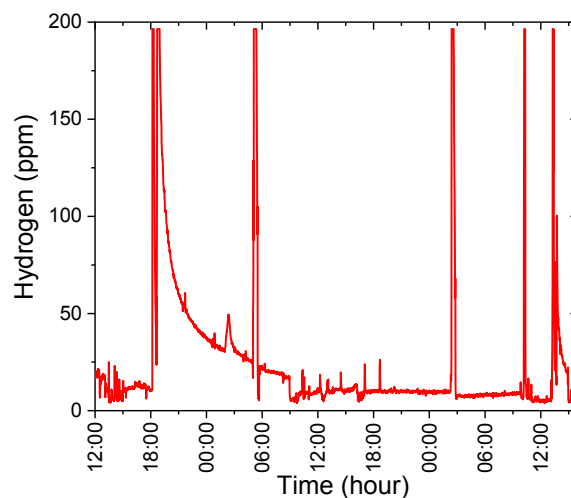


Fig. 2. Hydrogen content measured at location 2 of Fig. 1.

in Fig. 1 of reference [4], the operating conditions of the internal purifier are determined by setting the cold end temperature TI3475, cold flow F3410, regeneration completion temperature TI3465, and heater control output R3470. For Ikeda et al. [4], the operating conditions of a Linde liquefier (L280) were set to a cold end temperature at TI3475 at 32.5 K, cold flow F3410 at 120 l/min, regeneration completion temperature TI3465 at 140 K, and heater control output R3470 at 18%. In our case, while using a liquid helium liquefier (L70), the parameters were 31 K, 65 l/min, 130 K, and 15%, respectively. With this configuration, the hydrogen amount measured at location 2 (Fig. 1) is plotted in Fig. 2. We noticed that during the purge process, the H_2 amount was above 200 ppm and was saturating the analyzer. Such purge events are seen in the plot as the large signals. Additionally, over a longer time range, a high content of H_2 was measured.

The blockage of fine capillary tubes used as flow resistors was first observed at the Department of Physics in 2017. By changing the cold end temperature of the internal purifier (TI3475) from 32.5 to 22 K, Ikeda et al. succeeded in improving the recovered gas purity during purifier regeneration operation from 33.5 to 99% [4]. The same procedure was then tested with our L70 liquefier. The change from 31 to 26 K (or even lower) of the cold end temperature was not successful here. Therefore, a set of measures were taken to address this problem: (i) improving the helium quality from 4.6 to 5.0, (ii) release of helium gas into the atmosphere during the purge time for the regeneration cycle of helium liquefier's internal purifier, and (iii) installation of two catalytic converters in the closed helium circuit.

3.1. Change of the helium purity

It has been known for a long time that molecular H is naturally present in helium gas as obtained from natural gas sources. Different methods are typically applied to eliminate it before large scale helium liquefaction for its distribution worldwide [16,17]. For example, in the case of Palmerston helium plant, in Wickham Point (Australia), the product quality is liquid helium at a 99.999% purity level, containing less than 10 ppm total impurity within a maximum of 1 ppm of H_2 [17]. Moreover, ultra high pure commercial grade He gas, 99.9999% pure (quality 6.0), containing less than 1 ppm of total impurities in volume, may contain up to 0.5 ppm in volume of H_2 .

In the case of our recovery plant, less than ca. 20% of He gas is lost in the closed circuit, new helium bundles are regularly fed into our loop (Fig. 1). The quality of the He bundle was changed from 4.6 (purity $\geq 99.996\%$) to 5.0 (purity $\geq 99.999\%$) with $H_2 < 1$ ppm. For the 5.0 quality, oxygen, hydrogen and water are less than 3 ppm. In position 4 (Fig. 1) the H_2 content was measured for He 4.6 and 5.0 to be in the

range of 7–13 ppm and below 1 ppm, respectively. In Fig. 3, H₂ content measured at location 2 for 4.6 He quality without purge and with 5.0 He quality with a purge is presented. Even if the purge effect has to be taken into account, the total content of H₂ has been reduced from 24.3 to 0.8 ml. The concept of this “purge” will be explained in the following section.

3.2. Release of helium gas into the atmosphere during the purge time for the regeneration cycle of the internal purifier

As reported by Decker et al., a new 20 K adsorber has been installed downstream of the heat exchanger E3470 for the regeneration cycle of the liquefier’s internal purifier (Fig. 3 of reference [13]). This small adsorber (A3474) entraps traces of hydrogen and neon up to 100 ppm (in volume) in sum per cycle. For the liquefier purification phase, as specified by Linde company, the gas trapped by the adsorber has been released to the closed circuit. To avoid an increase in the H₂ concentration over time, the procedure was modified to implement a release into the atmosphere during the purge time at the end of the regeneration cycle. For this purpose, a new valve (V3410-1) has been installed in parallel to the V3410 (Fig. 3 of reference [13]). By adjusting the time of the release to the atmosphere, the maximum H₂ level has successfully been lowered by a factor of 10 (Fig. 4).

3.3. Installation of two catalytic converters in the closed helium circuit.

As reported by Haberstroh, car catalytic converter was already implemented by the University of Frankfurt (Germany) in 2013 [5]. Common catalysts are most often a mix of precious metals, mostly from the platinum group and typically palladium. Two catalytic converters were installed in the helium recovery plant to reduce hydrogen. Hydrogen molecules are chemisorbed in a dissociated form onto the catalyst surface and further oxidized to H₂O (g) by the O₂ impurities present in the incoming gas. One of the catalytic converters has been installed at the high pressure part (Hydrogen burner NEO312 neo hydrogen sensors GmbH) before the dryer shown in Fig. 3 of reference [12]. The other catalytic converter, a natural gas car exhaust (VW-Touran), was mounted before the recovery compressor (Fig. 1). For test purposes, both catalytic converters were mounted directly before the hydrogen measurement analyzer. Using a bottle of nitrogen containing 100 ppm of H₂ and oxygen gas flowing through the catalytic converter, we measured the hydrogen content release for several catalytic converter temperatures. Comparing Fig. 5a) and b), we noticed that hydrogen burner NEO312 has to be chemically activated through heat. At 60 C, half of the H₂ amount is oxidized, and at 100 C no more H₂ is released. The reaction onset temperature is the temperature where a

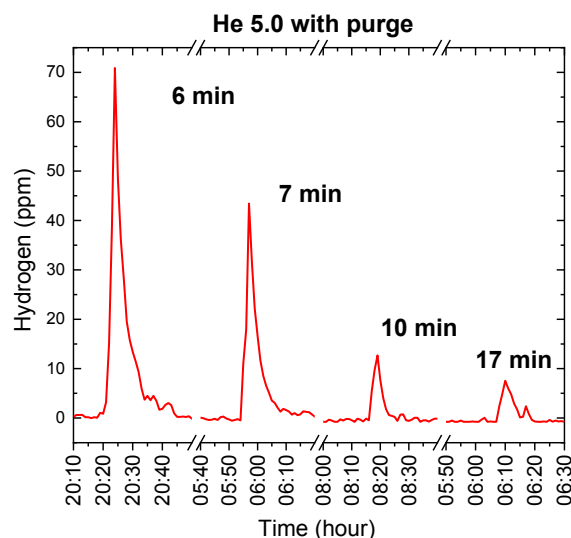


Fig. 4. Hydrogen content measured in position 2 of Fig. 1 for several purge run times during the regeneration cycle of the internal purifier.

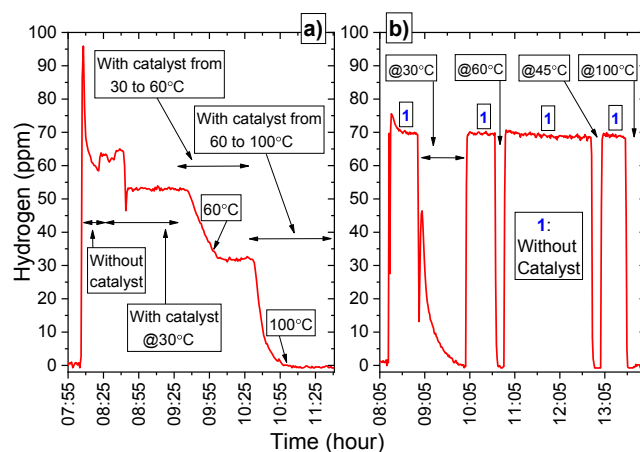


Fig. 5. Hydrogen concentration measured using both catalytic converters for several temperatures: a) Hydrogen burner NEO312 and b) natural gas car exhaust (VW-Touran).

significant fuel consumption begins. For this particular catalytic converter, at 30 C a low amount of H₂ is oxidized and at 60 C, half of the H₂ amount is reduced, i.e., the reaction onset temperature is between 30 and 60 C. In comparison, the natural gas car exhaust can already oxidize the entire H₂ content at 30 C. Following, the consumption rate of H₂ is increased for a temperature of 45 C as compared to 30 C (Fig. 5b).

4. Conclusion

To address the capillary blocking issue that started to occur at the Department of Physics at the University of Basel in 2017 using helium evaporation cryostats, a set of countermeasures were: (i) improving the helium quality from 4.6 to 5.0, (ii) release of helium gas into the atmosphere during the purge time for the regeneration cycle of the helium liquefier’s internal purifier and (iii) installation of two catalytic converters in the closed helium circuit. After one year of implementing and testing these three measures, their validity has been continuously demonstrated from the beginning of 2018 by producing hydrogen free liquid helium. No further blocking of capillary tubes were reported. As reported, all three measures contributed to reducing the total amount of hydrogen overall, but it was not possible to quantify whether one

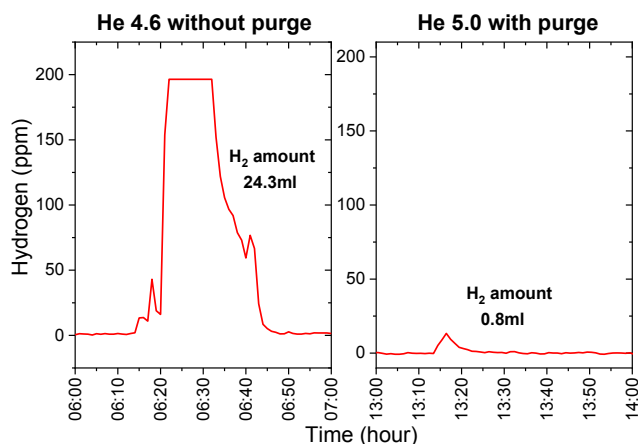


Fig. 3. Hydrogen content measured at location 2 of Fig. 1 with He 4.6 without purging and He 5.0 with purging.

measure was more effective than another. Further experiments are required to answer this question.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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References

- [1] Mineral Commodity Summaries, 2020. <https://pubs.er.usgs.gov/publication/mcs2020>.
- [2] M. Gabal, J. Sesé, C. Rillo, S. Spagna, "Clean" Liquid Helium, in: R. Zivieri (Ed.), *Superfluids Supercond.*, InTech, 2018. <https://doi.org/10.5772/intechopen.74907>.
- [3] Gabal M, Arauzo A, Camón A, Castrillo M, Guerrero E, Lozano MP, et al. Hydrogen-Free Liquid-Helium Recovery Plants: The Solution for Low-Temperature Flow Impedance Blocking. *Phys. Rev. Appl.* 2016;6. <https://doi.org/10.1103/PhysRevApplied.6.024017>.
- [4] Ikeda H, Kondo Y. Improvement of the Operational Settings of a Helium Purifier, Leading to a Higher Purity of the Recovered Gas. *Phys. Procedia.* 2015;67:1153-6. <https://doi.org/10.1016/j.phpro.2015.06.179>.
- [5] Haberstroh, Christoph, Neuartige Probleme durch H₂-Kontaminationen in LHe, in: Düsseldorf, 2014. http://www.knvk.nl/user/file/2014_dkv_tagung_programmheft.pdf.
- [6] Feng G, Xu P, Gong L, Li Z, Zhu W, Jia Q, et al. Experimental investigation on the cooling helium circulation of the internal purifier pilot plant. *Cryogenics* 2018;94: 26-30. <https://doi.org/10.1016/j.cryogenics.2018.03.009>.
- [7] M. Gabal, J. Sese, C. Rillo, Et Al., The purity of liquid helium revisited., (2017). <https://doi.org/10.18462/IIR.CRYO.2017.0117>.
- [8] Will J, Haberstroh C. Hydrogen contamination in liquid helium. *IOP Conf. Ser. Mater. Sci. Eng.* 2020;755:012117. <https://doi.org/10.1088/1757-899X/755/1/012117>.
- [9] J. Weiss, A. Chuquitarqui, Searching for hydrogen impurities in liquid helium, (2019). <https://qd-europe.com/de/en/news/product-application-news-spectrum/searching-for-hydrogen-impurities-in-liquid-helium/>.
- [10] Standard helium liquefier/refrigerator L70/LR70, (2019). https://www.lin.de-kryotechnik.ch/wp-content/uploads/2016/10/Datasheet_L70-LR70-E.pdf.
- [11] K.-H. Berdais, H. Wilhelm, Th. Ungricht, J.G. Weisend, J. Barclay, S. Breon, J. Demko, M. DiPirro, J.P. Kelley, P. Kittel, A. Klebaner, A. Zeller, M. Zagarola, S. Van Sciver, A. Rowe, J. Pfothhauer, T. Peterson, J. Lock, IMPROVEMENTS OF HELIUM LIQUEFACTION/REFRIGERATION PLANTS AND APPLICATIONS, in: AIP Conf. Proc., AIP, Chattanooga (Tennessee), 2008: pp. 825-829. <https://doi.org/10.1063/1.2908676>.
- [12] J. Clausen, Considerations for small to medium liquefaction plants, in: Spokane, Washington, USA, 2012: pp. 1447-1454. <https://doi.org/10.1063/1.4707072>.
- [13] L. Decker, A. Meier, H. Wilhelm, Improvement of Linde Kryotechnik's internal purifier, in: Anchorage, Alaska, USA, 2014: pp. 957-961. <https://doi.org/10.1063/1.4860808>.
- [14] Decker L, Blum L. Very Efficient and Highly Reliable Standard Helium Liquefiers and Refrigerators In the service of Japanese science, TEION KOGAKU. *J. Cryog. Supercond. Soc. Jpn.* 2018;53:81-5. <https://doi.org/10.2221/jcsj.53.81>.
- [15] Mova Analytical systems 430L Series PPM hydrogen Analyser, (n.d.). <http://www.gasanalyzerchina.com/wp-content/uploads/2016/10/430L-Process-PPM-H2-Analyser.pdf>.
- [16] P. Froehlich, J.J. Clausen, J.G. Weisend, J. Barclay, S. Breon, J. Demko, M. DiPirro, J.P. Kelley, P. Kittel, A. Klebaner, A. Zeller, M. Zagarola, S. Van Sciver, A. Rowe, J. Pfothhauer, T. Peterson, J. Lock, LARGE SCALE HELIUM LIQUEFACTION AND CONSIDERATIONS FOR SITE SERVICES FOR A PLANT LOCATED IN ALGERIA, in: AIP Conf. Proc., AIP, Chattanooga (Tennessee), 2008: pp. 549-556. <https://doi.org/10.1063/1.2908596>.
- [17] U. Lindemann, S. Boeck, L. Blum, K. Kurtcuoglu, J.G. Weisend, TURNKEY HELIUM PURIFICATION AND LIQUEFACTION PLANT FOR DARWIN, AUSTRALIA, in: Tucson (Arizona), 2010: pp. 271-274. <https://doi.org/10.1063/1.3422363>.